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(54) **Process and apparatus to reduce NO_x emissions from a fluid catalytic cracking unit.**

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Description

This invention relates to a process for regenerating fluidized cracking catalyst.

The field of catalytic cracking, and particularly fluid catalyst operations, has undergone significant development and improvements due primarily to advances in catalyst technology and product distribution obtained therefrom. With the advent of high activity catalysts, and particularly crystalline zeolite cracking catalysts, new areas of operating technology have been encountered, requiring even further refinements in processing techniques to take advantage of the high catalyst activity, selectivity and operating sensitivity.

By way of background, the hydrocarbon conversion catalyst usually employed in a fluid catalytic cracking (FCC) installation is preferably a high activity crystalline zeolite catalyst of a fluidizable particle size. The catalyst is transferred in suspended or dispersed phase condition generally upwardly through one or more riser conversion zones (fluid catalytic cracking zones), providing a hydrocarbon residence time in each conversion zone in the range of 0.5 to about 10 seconds, and usually less than about 8 seconds. High temperature risers and 0.5 to 4 seconds hydrocarbon residence time in the riser may be used to make cracked products.

During cracking carbonaceous deposits accumulate on the catalyst. Entrained hydrocarbons are removed from the catalyst in a stripping zone. Cracked products and stripped materials are combined and typically passed to a product fractionation step. Stripped catalyst (spend catalyst) containing deactivating amounts of carbonaceous material, hereinafter referred to as coke, is then regenerated.

In catalyst regeneration, oxygen burns off coke. The hydrogen-containing components in coke form water which causes hydrothermal degradation.

U. S. Patent No. 4,336,160 to Dean et al attempts to reduce hydrothermal degradation by staged regeneration. However, the first stage of the regeneration process of Dean et al employs a dense bed which provides an opportunity for hydrothermal deactivation.

A major trend in fluid catalytic cracking processing has been modifications to the process to permit it to accommodate a wider variety of feedstocks, in particular, stocks that contain more nitrogen than had previously been permitted in a feed to a fluid catalytic cracking unit.

Many FCC feeds contain a lot of nitrogen. There is a trend to heavier, dirtier feeds. There is also a growing concern about the amount of NO_x in the regenerator flue gas. Some attempts have been made to minimize the amount of NO_x discharged to

the atmosphere through the flue gas by employing multiple beds in a fluid catalytic cracking regenerator.

U. S. Patent No. 4,325,833 to Scott discloses a three-stage regenerator directed to NO_x removal. Scott discloses that his middle stage contains a substantially oxygen-free atmosphere to convert NO_x to N_2 . However, flue gas from lower beds contact with catalyst from upper beds. This is detrimental because the flue gas contains water which can deactivate the catalyst by hydrothermal degradation.

It would be advantageous to provide a process which both minimizes NO_x and hydrothermal degradation.

Accordingly, the present invention provides a process for fluidized bed regeneration of coke contaminated catalyst as defined in claim 1.

Further features of the invention are defined in the dependent claims.

Reference is now made to the accompanying drawings, in which :

Fig. 1 is a partial cross-sectional view of a regenerator for carrying out the present invention;

Fig. 2 is a partial cross-sectional view of a second embodiment of a regenerator for carrying out the present invention;

Fig. 3 is a partial cross-sectional view of a third embodiment of a regenerator for carrying out the present invention; and

Fig. 4 is a schematic of a fourth embodiment of a regenerator for carrying out the invention.

The fluid catalytic cracking (FCC) process employs a catalyst in the form of fine particles which act as a fluid when aerated with a vapor. The fluidized catalyst is circulated continuously between a reactor and a regenerator and transfers heat from the regenerator to the reactor. The FCC process converts heavy hydrocarbons into more valuable gasoline and lighter products.

Fig. 1 shows FCC regenerator, which regenerates spent catalyst stream 2, from an FCC reactor (not shown). The spent catalyst is conventional. Preferably it comprises intermediate pore zeolite catalyst, most preferably ZSM-5 and a large pore zeolite such as zeolite Y. The spent catalyst combines with a first airstream 4, and preferably a regenerated recycle catalyst 52 from an optional standpipe 50, to form a mixture. The mixture passes through a first regenerator riser 6. Preferably, the mixture passes through riser 6 in plug flow at 538° to 677°C (1000° and 1250°F). Enough air is added via line 4 to sustain combustion at the inlet and partly through the riser 6. This burns off coke and forms H_2O and NO_x . Because the mixture through the riser 6 is basically in plug flow and oxygen is consumed, by combustion, the

oxygen concentration varies along the riser 6. When the spent catalyst initially combines with airstream 4, the initial oxygen concentration is sufficiently high to promote combustion. Then as combustion continues, the oxygen concentration lessens sufficiently to shift equilibrium, denoted by the following reaction, to convert NO_x , produced during combustion, to N_2 :



The mixture is oxygen-lean, preferably having an oxygen concentration between 0 and 1 mole %, most preferably between 0 and 0.5 mole %, when it exits the riser 6. This converts a portion of the NO_x to N_2 prior to exiting the riser 6. The mixture is discharged from the first riser 6 and passes into a plurality of discharge arms 14 which impart downward momentum to the mixture. The discharge arms 14 are housed within a riser cover 20.

After exiting the discharge arms 14, flue gas is removed as a first flue gas stream 22. The catalyst from the mixture continues down into the first catalyst bed 16, located in a lower portion 10 of a second regenerator riser 8. Riser 8 is a fast fluid bed riser. A fast fluid bed riser is disclosed in U. S. Patent No. 4,444,722 to Owen. The lower portion 10 has a larger inside diameter than an attached upper portion 12. A second airstream 18 passes through a header 19 into the first catalyst bed 16 to promote further regeneration. Stream 18 may be preheated by indirect heat exchange with the first flue gas stream 22 in a heat exchanger 24. The amount of air passed into the first catalyst bed 16 is preferably just enough to sustain combustion in the bed 16 and partly through the second riser 8. This burns off the coke and forms NO_x . However, the mixture is sufficiently oxygen-lean to shift equilibrium to favor converting NO_x to N_2 . Preferably the oxygen concentration is 0 to 1 mole %, most preferably 0 to 0.5 mole % as gas exits the riser 8. This converts a portion of the NO_x to N_2 prior to exiting the second riser 8. Bed 16 is preferably 28°C (50°F) or more hotter than the riser 6 exit, but not above 704°C (1300°F).

The airstream 18 and combustion products formed in bed 16 elutriate a first catalyst stream 26 up from first bed 16 into the upper portion 12 of the second regeneration riser 8. A second catalyst stream can be withdrawn from bed 16 through an optional conduit 17 and sent to a fluid catalytic cracking reactor (not shown).

The catalyst stream 26 passes through upper portion 12, which is located within a catalyst collecting chamber 30. Stream 26 discharges from upper portion 12 into a plurality of discharge arms 32 which impart downward momentum to the stream 26. The discharge arms 32 are housed

within a riser cover 38. The downwardly directed catalyst countercurrently contacts combustion gases from a second catalyst bed 34 located therebelow. The combustion gases displace gaseous material upwardly and away from the downwardly directed catalyst. The displaced gases form a second flue gas stream 40 which exits the chamber 30 and indirectly preheats an airstream 44 in indirect heat exchanger 42. The catalyst continues downwardly to the second catalyst bed 34. A third airstream 36 passes through a header 37 into the second bed 34 to contact catalyst in bed 34. Enough air is added to bed 34 to sustain combustion with minimal hydrothermal degradation and minimal NO_x formation. The NO_x formation is also minimized because a substantial portion of nitrogen originally in stream 2 has been removed by the first and second stages. Bed 34 is preferably at least 14°C (25°F) hotter than bed 16 but below 871°C (1600°F).

Some hot regenerated catalyst is preferably withdrawn from bed 34 via standpipe 50 and recycled to mix with spent catalyst stream 2, as discussed above. Regenerated catalyst is withdrawn from bed 34 via conduit 54 and passed to a fluid catalytic cracking reactor (not shown). Combustion gases from second bed 34, which do not exit with second flue gas stream 40, pass up through the collecting chamber 30 to a cyclone 60, which separates gas from entrained catalyst and discharges gas via conduit 62, plenum chamber 70 and conduit 74 as a third flue gas stream 72. A number of cyclones, such as cyclone 60, in series or parallel, or both, may be provided within chamber 30. Catalyst recovered by cyclone 60 returns to second catalyst bed 34 through dipleg 61.

This embodiment is particularly advantageous when the catalyst comprises some intermediate pore zeolites catalyst, such as ZSM-5, or particles comprising large pore zeolite catalysts, such as zeolite Y. It is desirable to subject the larger pore zeolite catalysts to more regeneration than the intermediate pore zeolite catalysts, because the larger pore zeolite catalysts tend to deactivate with coke more readily than the intermediate pore zeolite catalysts.

In a second embodiment of the present invention, shown in Fig. 2, the combination of discharge arms 32 and riser cover 38 of Fig. 1 is replaced by a series of closed cyclones. Like-numbered features in Figs. 1 and 2 operate the same way. U.S. Patent No. 4,404,095 to Haddad et al discloses discharge arms and a riser cover applied to a stripping section of a fluid catalytic cracking reactor vessel. U. S. Patent No. 4,502,947 to Haddad et al shows a closed cyclone system applied to a fluid catalytic cracking reactor vessel. As shown in Fig. 2, the catalyst stream 2, airstream 4 and recycled

hot regenerated catalyst 52 are combined and pass up through riser 6 into a second stage regenerator 108 having a lower portion 110 attached to an upper portion 112. A flue gas stream 22 is separated from the catalyst discharged from the riser 6 and the remaining catalyst from the mixture passes to a first catalyst bed 16. A dilute phase catalyst and gas stream 26 passes up from bed 16 through the upper portion 112 of the second riser 108. Optionally, a portion of catalyst may be withdrawn from bed 16 by an optional conduit 17 and recycled to a fluid catalytic cracking reactor (not shown).

The catalyst stream 26 discharges from the upper portion 112 into a riser cyclone inlet conduit 114 to a riser cyclone 120. The gas from riser cyclone 120 discharges via conduit 128 to cyclone 130 via conduit 122. Cyclone 130 may be attached to downstream cyclones (not shown) by a conventional enclosed conduit (not shown). Overhead gas from cyclone 130, or downstream cyclones in series (not shown), forms a second flue gas stream which exits vessel 30 through an overhead conduit 132.

The riser cyclone overhead conduit 122 includes a lower vertical conduit 124, attached to the cyclone 120, which is inserted into an upper vertical conduit 126. Conduit 126 is attached to cyclone inlet conduit 128. The annulus between conduit 124 and conduit 126 admits gas from catalyst bed 34. Preferably, the annulus is sized such that the gas velocity in it is between 1.5 and 30 m/s (5 and 100 feet per second). Catalyst recovered by cyclones 120 and 130 passed through diplegs 121, 131 to the second catalyst bed 34. Combustion gases from bed 34 which do not exit as part of the second flue gas stream pass into one or more cyclones 60 and exit through overhead conduit 62 to plenum chamber 70 and through the withdrawal conduit 74 as a third flue gas stream 72. Catalyst separated in cyclone 60 returns to the second catalyst bed 34 through a dipleg 61.

Similar to the first embodiment, the risers 6, 108 operate at oxygen-lean conditions. The first and second airstreams 4, 18 preferably supply enough air so that the mixtures exiting the first riser 6 and fast fluid bed riser 108 comprise gas having an oxygen concentration between 0 and 1 mole %, most preferably between 0 and 0.5 mole %. Exiting the first riser 6 is defined as when the mixture passes into discharge arms 14. Exiting the fast fluid bed riser is defined as when the mixture passes out of riser upper portion 112 into conduit 114. Airstream 36 preferably provides the minimum amount of air necessary to sustain combustion to bed 34.

These oxygen-lean conditions promote conversion of NO_x produced during coke combustion, to

N_2 .

In a third embodiment of the present invention, shown in Fig. 3, the combination of discharge arms 14 and riser cover 20 of Fig. 2 is replaced by a series of closed cyclones. In Figs. 2 and 3, like-numbered features operate in the same way. As shown in Fig. 3, the catalyst stream 2, airstream 4 and first portion of regenerated catalyst 52 are combined and pass upwardly through a first regenerator riser 142 into a second regenerator riser 108 having a lower portion 110 attached to an upper portion 112. A closed cyclone system separates a flue gas stream 22 from the catalyst discharged from the riser 142, as discussed below. The remaining catalyst from the mixture passes to a first catalyst bed 16. A catalyst stream 26 passes upwardly from bed 16 through the upper portion 112 of the second riser 108. Optionally, a portion of catalyst may be withdrawn from bed 16 by an optional conduit 17 and recycled to a fluid catalytic cracking reactor (not shown).

The closed cyclone system separates the flue gas stream 22 from the catalyst discharged from the riser 142 as follows. The catalyst stream discharges from the riser 142 into a riser cyclone inlet conduit 144 to a riser cyclone 150. The riser cyclone 150 is connected to a primary cyclone 160 by means of a riser cyclone overhead conduit 152. The primary cyclone 160 may be attached to a secondary cyclone (not shown) by a conventional enclosed conduit (not shown). Overhead gas from the primary cyclone 160, or second cyclones in series (not shown), forms the first flue gas stream 22 which exits the second riser 108 through an overhead conduit 162.

The riser cyclone overhead conduit 152 includes a lower vertical conduit 154, attached to the cyclone 150, which is inserted into an upper vertical conduit 156. Conduit 156 is in turn attached to a primary cyclone inlet conduit 158. An annulus is formed between conduit 154 and conduit 156 so that a portion of gas from catalyst bed 16 may pass into upper conduit 156. Preferably, the annulus is sized such that the velocity of the gas into the annulus is between 1.5 and 30 m/s (5 and 100 feet per second). Catalyst separated in cyclones 150 and 160 passes through diplegs 151, 161 to the first catalyst bed 16.

Similar to the second embodiment, the risers 142, 108 operate at oxygen-lean conditions. The first and second airstream 4, 18 preferably supply enough air so that the mixtures exiting the first riser 142 and fast fluid bed riser 108 comprise gas having an oxygen concentration between 0 and 1 mole %, most preferably between 0 and 0.5 mole %. The first riser 142 exit is the cyclone inlet conduit 144. The bed 108 exit is at the entrance to conduit 114. Airstream 36 preferably provides the

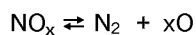
minimum amount of air necessary to sustain combustion in bed 34.

Fig. 4 discloses a fourth embodiment of a regenerator for carrying out the present invention. The fourth embodiment is a transport-type regenerator reactor comprising a transport conduit 200 provided with a plurality of oxygen-containing airstreams 230, 232, 234, 236 and 238 sequentially provided along a portion of the conduit 200 at respective injection points 240, 242, 244, 246, 248. Each injection point 240, 242, 244, 246, 248 represents one or more injection nozzles about the perimeter of the conduit 200. The conduit 200 may be horizontal or vertical.

A spent catalyst stream 210, from a fluid catalytic cracking reactor (not shown), and an oxygen-containing airstream 212 pass into the conduit 200 and form a mixture. The mixture passes through the conduit 200 and sequentially contacts the plurality of oxygen-containing airstreams 230, 232, 234, 236, 238 at regenerating conditions.

The regenerating conditions in the conduit 200 include a gas residence time between 1 and 60 seconds, preferably between 1 and 25 seconds, and a mixture temperature between 538° and 871° C (1000° and 1600° F). The gas residence time between contacting the mixture with each airstream 230, 232, 234, 236, 238 is preferably at least 0.5 seconds. Said mixture passes through said transport conduit 200 in basically plug flow. Each portion of conduit 200 between the sequential injection points 240, 242, 244, 246, 248 acts as another regeneration stage.

The oxygen concentration varies along conduit 200. When the catalyst initially contacts the airstreams 212, 230, 232, 234, 236, 238, the initial oxygen concentration is sufficiently high to promote combustion. Then, as combustion continues, the oxygen is depleted so that the mixture passes through a region A of relatively lower oxygen concentration. The oxygen concentration in the region A is sufficiently low to shift equilibrium, denoted by the following reaction to convert NO_x, produced during regeneration, to N₂:



A regenerated mixture 250 then exits the conduit 200 and passes to a cyclone, or other gas-solid separation device (not shown), to separate into a flue gas stream and a regenerated catalyst stream. The regenerated catalyst may then undergo further regeneration or pass to a fluid catalytic cracking reactor (not shown) for combination with fluid catalytic cracking hydrocarbon feed. Further regeneration may occur by recycling, the separated catalyst to conduit 200, or in subsequent regenerator stages. For example, the conduit 200

may substitute for riser 6 of Figs. 1 and 2, or riser 142 of Fig. 3.

The first, second and third embodiments of the present invention have the advantage that regenerating fluid catalytic cracking catalyst in stages, and quickly removing flue gas from the catalyst in each stage, minimizes hydrothermal degradation and minimizes NO_x formation.

The fourth embodiment provides multistage regeneration, to reduce NO_x, in a single transport conduit. This is particularly useful in retrofitting FCC regenerators.

Claims

1. A process for fluidized bed regeneration of coke contaminated catalyst by combining a stream of coked catalyst with a stream of hot regenerated catalyst and a first oxygen-containing gas stream to form a first mixture of catalyst and gas and regenerating the catalyst by burning the coke characterized by
 - passing the mixture through a first stage regenerator comprising a first regenerator riser having an upper end and a lower end and maintaining a low oxygen concentration in the upper end of the riser to form a catalyst and first flue gas stream;
 - discharging the catalyst and flue gas stream from the riser and separating the catalyst and flue gas stream into a catalyst rich stream which is discharged downwardly to form a first catalyst bed located in a lower portion of a second stage regenerator and a first flue gas stream from the regenerator;
 - adding a second oxygen-containing stream to the first catalyst bed to form a second mixture of catalyst and gas which passes to an upper portion of the second stage regenerator and maintaining a low oxygen concentration in the upper portion of the second stage regenerator;
 - discharging from the upper portion of the second stage regenerator catalyst with reduced coke content and flue gas and separating catalyst with reduced coke content from the flue gas and forming a second bed of catalyst and a second flue gas stream, removing both first and second flue gas streams from the first and second stage regenerators; and
 - recycling to the first stage regenerator a hot regenerated catalyst stream from the second bed.
2. The process of claim 1 further characterized by:
 - separating a flue gas stream from the cata-

lyst and flue gas from the second stage regenerator to recover a catalyst rich stream which is discharged to form a second catalyst bed located in a third stage regenerator;

adding a third oxygen-containing stream to catalyst in the second bed to complete catalyst regeneration; and

withdrawing a flue gas stream from above the second bed.

3. The process of claim 1 or 2, further characterized in that flow through the first riser is plug flow, and gas discharged from the riser has less than 1 mole % molecular oxygen.

4. The process of any preceding claim further characterized by plug flow of the second mixture through the upper portion of the second stage regenerator, a gas residence time of 1 to 20 seconds in the second stage regenerator, and gas discharged therefrom has less than 1 mole % molecular oxygen.

5. The process of any preceding claim further characterized in that the first riser regenerator temperature is 538° to 677° C (1000° to 1250° F), the first bed is at least 28° C hotter, but does not exceed 704° C (1300° F), and the second bed is at least 14° C hotter than the first bed but does not exceed 871° C (1600° F) and gas discharged from each stage of the regenerator has less than 1.0 mole % oxygen.

6. The process of any preceding claim further characterized in that the gas discharged from each stage of the regenerator has less than 0.5 mole % oxygen.

7. The process of any preceding claim further characterized in that the mixture discharged from at least one stage of the regenerator is downwardly directed by contact with a first plurality of arms extending radially from the discharge end and the arms are in a cover.

8. The process of any preceding claim further characterized in that the mixture discharged from at least one stage of the regenerator is discharged directly into a cyclone which separates flue gas from catalyst.

9. The process of any preceding claim further characterized by heating at least one of the oxygen-containing streams by indirect heat exchange with at least one flue gas stream.

Revendications

1. Un procédé de régénération en lit fluidisé de catalyseur contaminé par du coke par combinaison d'un courant de catalyseur cokéfié avec un courant de catalyseur chaud régénéré et d'un premier courant de gaz contenant de l'oxygène pour former un premier mélange de catalyseur et de gaz et la régénération du catalyseur par combustion du coke, caractérisé par:

- le passage du mélange dans un premier étage d'un régénérateur comprenant une première colonne ascendante (riser) de régénération ayant une extrémité supérieure et une extrémité inférieure et le maintien d'une concentration en oxygène faible dans l'extrémité supérieure de la colonne ascendante pour former un catalyseur et un premier courant de gaz de combustion;
- la décharge du catalyseur et du courant de gaz de combustion issu de la colonne ascendante et la séparation du catalyseur et du courant de gaz de combustion en un courant riche en catalyseur qui s'écoule vers le bas pour former un premier lit catalytique disposé dans la partie inférieure du premier étage du régénérateur et un premier courant de gaz de combustion issu du régénérateur;
- l'addition d'un second courant contenant de l'oxygène au premier lit catalytique pour former un second mélange de catalyseur et de gaz qui passe dans la partie supérieure du deuxième étage du régénérateur et le maintien d'une concentration en oxygène faible dans la partie supérieure du deuxième étage du régénérateur;
- la décharge à partir de la partie supérieure du catalyseur issu du régénérateur de seconde étape avec une teneur en coke réduite et des gaz de combustion et la séparation du catalyseur avec une teneur en coke réduite des gaz de combustion et la formation d'un second lit de catalyseur et d'un second courant de gaz de combustion, le retrait des premier et second courants de gaz de combustion des premier et deuxième étages de régénérateur; et
- le recyclage vers le premier étage du régénérateur d'un courant de catalyseur régénéré chaud issu du second lit.

2. Le procédé selon la revendication 1, caractérisé en outre par:

- la séparation d'un courant de gaz effluent du catalyseur et du gaz effluent issu du

- deuxième étage du régénérateur pour récupérer un courant riche en catalyseur qui est évacué pour former un second lit catalytique localisé dans un troisième étage du régénérateur;
- l'addition d'un troisième courant contenant de l'oxygène au catalyseur dans le second lit pour compléter la régénération catalytique; et
 - le retrait d'un courant de gaz effluent de la partie supérieure du second lit.
3. Le procédé selon la revendication 2, caractérisé de plus en ce que le flux dans la première colonne ascendante est en écoulement essentiellement laminaire, et en ce que le gaz déchargé de la colonne ascendante a une teneur en oxygène moléculaire inférieure à 1% molaire.
4. Le procédé selon l'une quelconque des revendications précédentes, caractérisé de plus par un écoulement laminaire du second mélange dans la partie supérieure du deuxième étage du régénérateur, par un temps de séjour pour le gaz de 1 à 20 secondes dans le deuxième étage du régénérateur, et par le fait que le gaz qui en est retiré a une teneur en oxygène moléculaire inférieure à 1% molaire.
5. Le procédé selon l'une quelconque des revendications précédentes, caractérisé de plus en ce que la température de la première colonne ascendante de régénérateur est comprise entre 538 et 677 °C (1000 à 1250 °F), en ce que le premier lit est à une température au moins supérieure de 28 °C, mais qui n'excède pas 704 °C (1300 °F), et en ce que le second lit est à une température au moins supérieure de 14 °C à celle du premier lit mais qui n'excède pas 871 °C (1600 °F) et en ce que le gaz rejeté à chaque étage du régénérateur a une teneur en oxygène inférieure à 1% molaire.
6. Le procédé selon l'une quelconque des revendications précédentes, caractérisé de plus en ce que le gaz rejeté de chacun des étages du régénérateur a une teneur en oxygène inférieure à 0,5% molaire.
7. Le procédé selon l'une quelconque des revendications précédentes, caractérisé de plus en ce que le mélange rejeté d'au moins un étage du générateur est dirigé vers le bas par contact avec une première pluralité de bras s'étendant radialement à partir de l'extrémité de rejet et en ce que les bras sont disposés dans un couvercle.

8. Le procédé selon l'une quelconque des revendications précédentes, caractérisé de plus en ce que le mélange rejeté d'au moins un étage du régénérateur est rejeté directement dans un cyclone qui sépare le gaz de combustion du catalyseur.
9. Le procédé selon l'une quelconque des revendications précédentes, caractérisé de plus par chauffage d'au moins un des courant contenant de l'oxygène par échange de chaleur indirect avec au moins un courant de gaz de combustion.

Patentansprüche

1. Verfahren zur Regenerierung eines mit Koks verunreinigten Katalysators im Wirbelschichtbett durch Kombination eines Stroms des verkokten Katalysators mit einem Strom von heißem regeneriertem Katalysator und einem ersten sauerstoffhaltigen Gasstrom, um eine erste Mischung aus Katalysator und Gas zu bilden, und Regenerierung des Katalysators durch Abbrennen des Koks, gekennzeichnet durch:
- Leiten dieser Mischung durch einen Regenerator der ersten Stufe, der einen ersten Regenerator-Riser mit einem oberen und einem unteren Ende umfaßt, und Beibehaltung einer geringen Sauerstoffkonzentration im oberen Ende des Risers, um einen Strom aus Katalysator und erstem Abgas zu bilden;
- Abgabe des Stroms aus Katalysator und Abgas aus dem Riser und Trennung des Stroms aus Katalysator und Abgas in einen mit Katalysator angereicherten Strom, der nach unten abgegeben wird, um ein erstes Katalysatorbett, das im unteren Abschnitt des Regenerators der zweiten Stufe angeordnet ist, und einen ersten Abgasstrom aus dem Regenerator zu bilden;
- Zugabe eines zweiten sauerstoffhaltigen Stroms zum ersten Katalysatorbett, um eine zweite Mischung aus Katalysator und Gas zu bilden, die zum oberen Abschnitt des Regenerators der zweiten Stufe strömt, und Beibehaltung einer geringen Sauerstoffkonzentration im oberen Abschnitt des Regenerators der zweiten Stufe;
- Abgabe des Katalysators mit reduziertem Koksgehalt und des Abgases vom oberen Abschnitt des Regenerators der zweiten Stufe und Abtrennung des Katalysators mit reduziertem Koksgehalt vom Abgas und Bildung eines zweiten Katalysatorbettes und eines zweiten Abgasstroms, Entfernung sowohl des ersten als auch des zweiten Abgasstroms aus den Regeneratoren der ersten und zweiten Stufe;

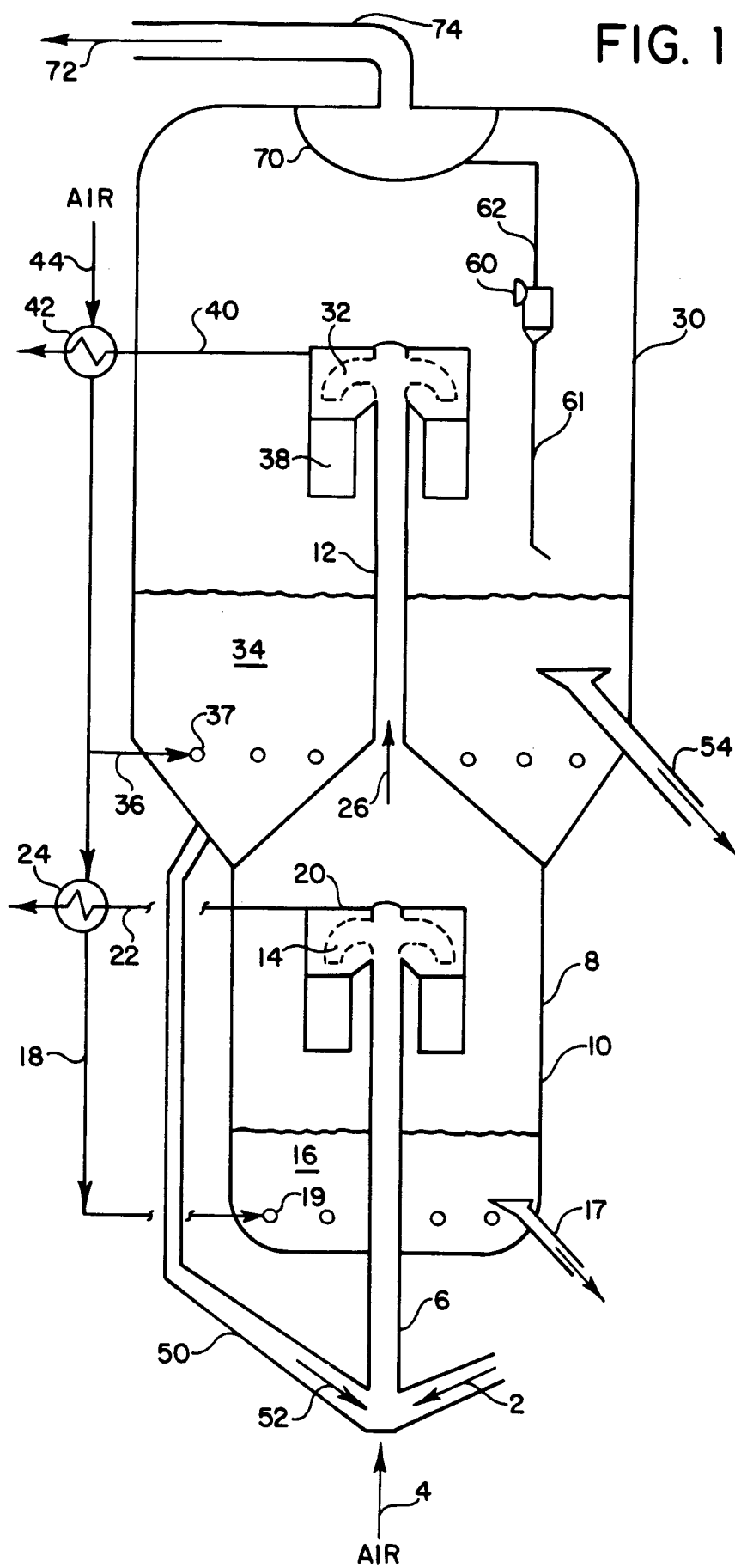
Rezirkulierung des heißen regenerierten Katalysatorstroms vom zweiten Bett zum Regenerator der ersten Stufe.

2. Verfahren nach Anspruch 1, weiterhin gekennzeichnet durch:
Abtrennung eines Abgasstroms vom Katalysator und Abgas vom Regenerator der zweiten Stufe, um einen mit Katalysator angereicherten Strom zu gewinnen, der abgegeben wird, um ein zweites Katalysatorbett zu bilden, das im Regenerator der dritten Stufe angeordnet ist; Zugabe eines dritten sauerstoffhaltigen Stroms zum Katalysator im zweiten Bett, um die Katalysatorregenerierung abzuschließen; Abziehen des Abgasstroms oberhalb des zweiten Bettes. 5 10 15
3. Verfahren nach Anspruch 1 oder 2, weiterhin dadurch gekennzeichnet, daß der Strom durch den ersten Riser eine ideale Strömung ist und das aus dem Riser abgegebene Gas weniger als 1 Mol-% molekularen Sauerstoff aufweist. 20
4. Verfahren nach einem der vorstehenden Ansprüche, weiterhin durch eine ideale Strömung der zweiten Mischung durch den oberen Abschnitt des Regenerators der zweiten Stufe, eine Gasverweilzeit von 1 bis 20 s im Regenerator der zweiten Stufe gekennzeichnet, wobei das davon abgegebene Gas weniger als 1 Mol-% molekularen Sauerstoff aufweist. 25 30
5. Verfahren nach einem der vorstehenden Ansprüche, weiterhin dadurch gekennzeichnet, daß die Temperatur im ersten Regenerator-Riser 538° bis 677° C (1000° bis 1250° F) beträgt, das erste Bett mindestens 28° C wärmer, jedoch 704° C (1300° F) nicht übersteigt, und das zweite Bett mindestens 14° C wärmer als das erste Bett ist, jedoch 871° C (1600° F) nicht übersteigt, und das von jeder Stufe des Regenerators abgegebene Gas weniger als 1,0 Mol-% Sauerstoff aufweist. 35 40 45
6. Verfahren nach einem der vorstehenden Ansprüche, weiterhin dadurch gekennzeichnet, daß das aus jeder Stufe des Regenerators abgegebene Gas weniger als 0,5 Mol-% Sauerstoff aufweist. 50
7. Verfahren nach einem der vorstehenden Ansprüche, weiterhin dadurch gekennzeichnet, daß die von zumindest einer Stufe des Regenerators abgegebene Mischung durch Kontakt mit einer ersten Vielzahl von Armen nach unten gerichtet wird, die sich von der Ausgabe-seite radial erstrecken, wobei sich diese Arme 55

in einer Abdeckung befinden.

8. Verfahren nach einem der vorstehenden Ansprüche, weiterhin dadurch gekennzeichnet, daß die von zumindest einer Stufe des Regenerators abgegebene Mischung direkt in einen Zyklon gegeben wird, der das Abgas vom Katalysator trennt.
9. Verfahren nach einem der vorstehenden Ansprüche, weiterhin dadurch gekennzeichnet, daß zumindest ein Teil der sauerstoffhaltigen Ströme durch indirekten Wärmeaustausch mit zumindest einem Abgasstrom erwärmt wird.

FIG. 1



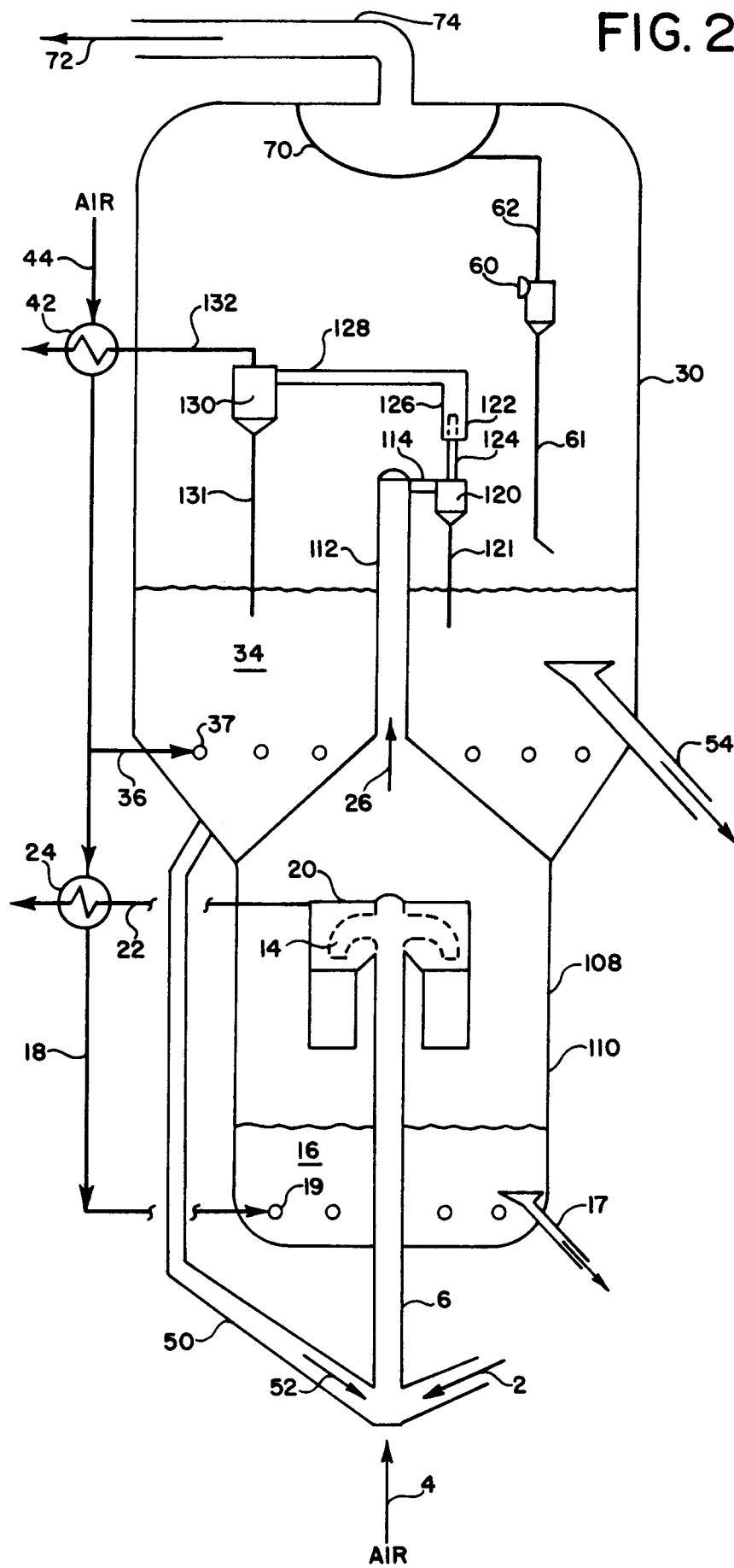


FIG. 3

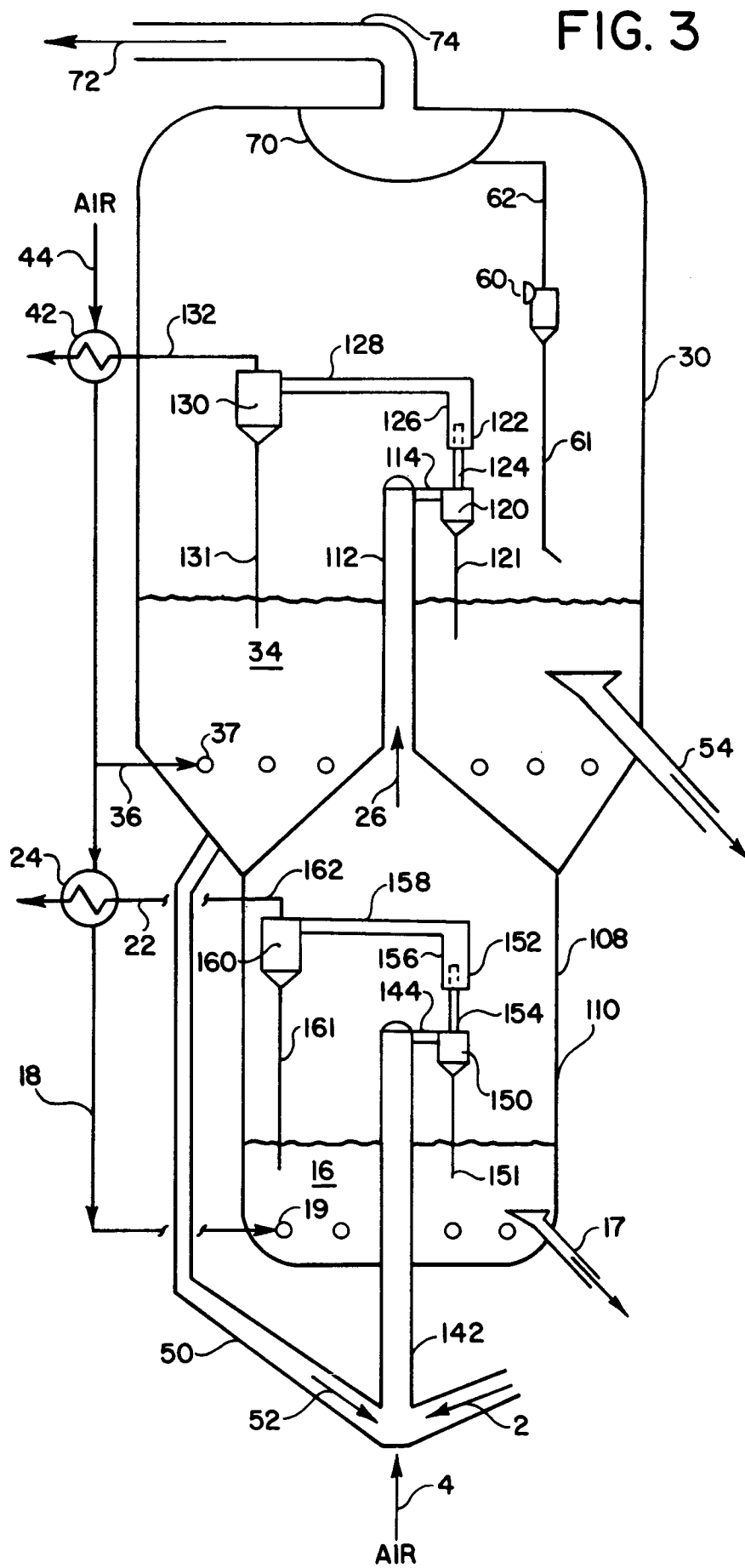


FIG. 4

