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(54) Title: A COMPOSITION AND SLURRY USEFUL FOR METAL CMP		
(57) Abstract <p>A chemical mechanical polishing precursor composition comprising at least one catalyst having multiple oxidation states, and at least one stabilizer, the composition being useful when admixed with an oxidizing agent prior to use to remove metal layers from a substrate. Also disclosed is a chemical mechanical polishing composition comprising an oxidizing agent and at least one catalyst having multiple oxidation sites, the composition being useful when combined with an abrasive or an abrasive pad to remove metal layers from a substrate.</p>		

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TITLE**A COMPOSITION AND SLURRY USEFUL FOR METAL CMP**

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BACKGROUND OF THE INVENTION**1. Field of the Invention**

This invention concerns a chemical mechanical polishing composition including at least one oxidizer and a catalyst. The chemical mechanical polishing composition is useful alone or in combination with other chemicals and abrasives for polishing metal layers and thin-films associated with semiconductor manufacturing. More particularly this invention concerns a chemical mechanical polishing slurry that is especially adapted for polishing multiple metal layers and thin-films where one of the layers or films is comprised of tungsten and another layer or thin film is comprised of titanium or a titanium containing alloy such as titanium nitride. This invention also concerns a chemical mechanical polishing composition including at least one oxidizer, at least one catalyst, and at least one stabilizer. Finally, this invention relates to a chemical mechanical polishing precursor composition which may be later mixed at the point of use with an oxidizing agent.

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2. Description of the Related Art

Integrated circuits are made up of millions of active devices formed in or on a silicon substrate. The active devices, which are initially isolated from one another, are united to form functional circuits and components. The devices are interconnected through the use of well-known multilevel interconnections. Interconnection structures normally have a first layer of metallization, an interconnection layer, a second level of metallization, and sometimes a third and subsequent levels of metallization. Interlevel dielectrics such as doped and undoped silicon dioxide (SiO_2), are used to electrically isolate the different levels of metallization in a silicon substrate or well. The electrical connections between different interconnection levels are made through the use of metallized vias. U.S. Patent No. 4,789,648, which is incorporated herein by reference,

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describes a method for preparing multiple metallized layers and metallized vias in insulator films. In a similar manner, metal contacts are used to form electrical connections between interconnection levels and devices formed in a well. The metal vias and contacts are generally filled with tungsten and generally employ an adhesion layer such as titanium nitride (TiN) and/or titanium to adhere a metal layer such as a tungsten metal layer to SiO₂. At the contact level, the adhesion layer acts as a diffusion barrier to prevent tungsten and SiO₂ from reacting.

In one semiconductor manufacturing process, metallized vias or contacts are formed by a blanket tungsten deposition followed by a chemical mechanical polish (CMP) step. In a typical process, via holes are etched through an interlevel dielectric (ILD) to interconnection lines or to a semiconductor substrate. Next, a thin adhesion layer such as titanium nitride and/or titanium is generally formed over the ILD and is directed into the etched via hole. Then, a tungsten film is blanket deposited over the adhesion layer and into the via. The deposition is continued until the via hole is filled with tungsten. Finally, the excess metal is removed by chemical mechanical polishing (CMP) to form metal vias. Processes for manufacturing and/or CMP of ILD's are disclosed in U.S. Patent Nos. 4,671,851, 4,910,155 and 4,944,836.

In a typical chemical mechanical polishing process, the substrate is placed in direct contact with a rotating polishing pad. A carrier applies pressure against the backside of the substrate. During the polishing process, the pad and table are rotated while a downward force is maintained against the substrate back. An abrasive and chemically reactive solution, commonly referred to as a "slurry" is deposited onto the pad during polishing. The slurry initiates the polishing process by chemically reacting with the film being polished. The polishing process is facilitated by the rotational movement of the pad relative to the substrate as slurry is provided to the wafer/pad interface. Polishing is continued in this manner until the desired film on the insulator is removed.

The slurry composition is an important factor in the CMP step. Depending on the choice of the oxidizing agent, the abrasive, and other useful additives, the polishing slurry can be tailored to provide effective polishing to metal layers at desired polishing rates while minimizing surface imperfections, defects, corrosion, and erosion.

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Furthermore, the polishing slurry may be used to provide controlled polishing selectivities to other thin-film materials used in current integrated circuit technology such as titanium, titanium nitride and the like.

Typically CMP polishing slurries contain an abrasive material, such as silica or alumina, suspended in an oxidizing, aqueous medium. For example, U.S. patent No. 5,244,523 to Yu et al. reports a slurry containing alumina, hydrogen peroxide, and either potassium or ammonium hydroxide that is useful to remove tungsten at predictable rates with little removal of the underlying insulating layer. U.S. Patent 5,209,816 to Yu et al. discloses a slurry comprising perchloric acid, hydrogen peroxide and a solid abrasive material in an aqueous medium. U.S. Patent 5,340,370 to Cadien and Feller discloses a tungsten polishing slurry comprising approximately 0.1M potassium ferricyanide, approximately 5 weight percent silica and potassium acetate. Acetic acid is added to buffer the pH at approximately 3.5.

Most of the currently available CMP slurries contain large concentrations of dissolved, ionic metallic components. As a result, the polished substrates can become contaminated by the adsorption of charged species into the interlayers. These species can migrate and change the electrical properties of the devices at gates and contacts and change the dielectric properties of the SiO₂ layers. These changes may reduce the reliability of the integrated circuits with time. Therefore, it is desirable to expose the wafer only to high purity chemicals with very low concentrations of mobile metallic ions.

Known, non-metallic oxidizers suffer from typically low tungsten polishing rates. Because it is difficult to polish the tungsten at a high rate, the polishing step must be lengthened to remove the last traces of the deposited tungsten layer. Lengthening the polishing step exposes layers, such as SiO₂, to overpolishing and to undesirable erosion. This erosion makes it more difficult to print high resolution lines during subsequent photolithography steps increasing the number of wafer failures. In addition, lengthened polishing steps reduce the throughput of an IC fabrication plant and increase the cost of the resulting IC.

A new CMP slurry is, therefore, required that is both essentially free of potential integrated circuit contaminants and that polishes at high rates. In addition, a new CMP

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slurry and composition is needed that remains stable and active long after the compositions and slurry is prepared.

SUMMARY OF THE INVENTION

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The present invention is directed to a single chemical mechanical polishing composition that is essentially metal free in that it will generally include less than about 3000 ppm of metals or metal ions. Such a metal free chemical mechanical polishing composition will produce polished substrates with fewer defects that are generally attributed to the presence of metals and metal contaminants in CMP slurries.

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In addition, the chemical mechanical polishing composition of this invention is able to polish tungsten, titanium, and titanium nitride layers at high rates.

This invention is also a chemical mechanical polishing composition that presents fewer disposal problems due to its very low metals content.

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In addition, this invention is a state-of-the-art chemical mechanical polishing composition that is able to polish tungsten at very high rates with minimal impurity defects and that can be easily disposed of once used.

This invention is also a chemical mechanical polishing slurry and composition that has a long shelf life.

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Another aspect of this invention is a chemical mechanical polishing precursor composition that lacks an oxidizing agent and is later combined with an oxidizing agent prior to use to give a useful CMP slurry.

Furthermore, this invention is directed to methods for using the chemical mechanical polishing composition of this invention in a slurry to polish a plurality of metal layers in an integrated circuit.

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In one embodiment, this invention is a chemical mechanical polishing composition comprising an oxidizing agent and at least one catalyst having multiple oxidation states.

In another embodiment, this invention is a chemical mechanical polishing slurry comprising an abrasive, ferric nitrate, and from about 1.0 to about 10.0 weight percent of an oxidizing agent selected from the group consisting of hydrogen

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peroxide and monopersulfate. When the oxidizing agent is hydrogen peroxide, then the slurry includes from about 0.01 to about 0.05 weight percent ferric nitrate. When the oxidizing agent is monopersulfate, then the slurry includes from 0.1 to about 0.5 weight percent ferric nitrate.

5 In another embodiment, this invention is a chemical mechanical composition including at least one oxidizing agent and the product of the mixture of at least one catalyst having multiple oxidation states and at least one stabilizer. The composition is most useful in CMP methods for polishing substrates comprising tungsten.

10 In still another embodiment, this invention is a method for polishing a substrate, including at least one metal layer, comprising the steps of preparing CMP slurry by admixing at least one abrasive, at least one oxidizing agent, at least one catalyst having multiple oxidation states and deionized water. Next, the CMP slurry is applied to the substrate, and at least a portion of the metal layer is removed from the substrate by bringing a pad into contact with the substrate. In this embodiment,
15 the CMP precursor composition described herein may also be utilized.

In yet another embodiment, this invention is a method for polishing a substrate including a tungsten layer. The method is accomplished by preparing a CMP slurry by admixing from about 1.0 to about 15.0 weight percent silica, from about 0.01 to about 1.0 weight percent ferric nitrate, from about 0.50 to about 10.0
20 weight percent of an oxidizing agent selected from the group consisting of hydrogen peroxide, monopersulfates and mixtures thereof, and deionized water. Next, the chemical mechanical polishing slurry is applied to the substrate, and at least a portion of the tungsten layer is removed from the substrate by bringing a pad into contact with the substrate and moving the pad in relation to the substrate.

25 Also disclosed is a multi-package system useful for preparing a chemical mechanical polishing slurry. The multiple package system includes a first container comprising at least one oxidizing agent and a second container comprising at least one catalyst having multiple oxidation states.

DESCRIPTION OF THE CURRENT EMBODIMENT

The present invention relates to a chemical mechanical polishing composition that comprises at least one oxidizer and at least one catalyst that promotes a chemical reaction between the oxidizer and a substrate metal layer. The chemical mechanical polishing composition is used to polish at least one metal layer associated with a substrate selected from the group including silicon substrates, TFT-LCD glass substrates, GaAs substrates, and other substrates associated with integrated circuits, thin films, multiple level semiconductors, and wafers. In particular, the chemical mechanical polishing slurry of this invention has been found to exhibit excellent polishing performance when used to polish a substrate including one or more layers of tungsten, titanium, and titanium nitride in a single step, multiple metal layer chemical mechanical polishing process.

Before describing the details of the various preferred embodiments of this invention, some of the terms that are used herein will be defined. The "chemical mechanical composition" refers to the combination comprising of at least one oxidizer and at least one catalyst that may be used in conjunction with an abrasive pad to remove one or more layers of metal from a multiple layer metallization.

The term chemical mechanical polishing slurry, ("CMP slurry"), refers to another useful product of this invention that comprises the chemical mechanical composition of this invention and at least one abrasive. The CMP slurry is useful for polishing a multiple level metallization which may include but are not limited to semi-conductor thin-films, integrated circuit thin-films, and for polishing any other films, surfaces and substrates where CMP processes are useful.

One aspect of this invention is a chemical mechanical composition comprising an oxidizing agent and catalyst that is useful in oxidizing metal layers in polishing applications. This chemical mechanical composition is useful when incorporated in a chemical mechanical polishing slurry to oxidize a metal layer to its corresponding oxide or ions. For example, the combination can be used to oxidize tungsten to tungsten oxide, aluminum to aluminum oxide and copper to copper oxide. The oxidizing agent - catalyst combinations disclosed herein are useful when incorporated

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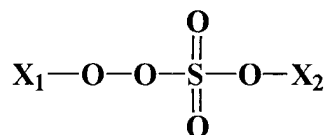
into a CMP slurry or when used alone in conjunction with an abrasive pad to polish metals and metal based components including tungsten, titanium, titanium nitride, copper, aluminum and various mixtures and combinations thereof.

The chemical mechanical composition of this invention includes at least one oxidizing agent that has an electrochemical potential greater than the electrochemical potential necessary to oxidize the catalyst. For example an oxidizing agent having a potential of greater than 0.771 volts versus normal hydrogen electrode is necessary when a hexa aqua iron catalyst is oxidized from Fe(II) to Fe(III). If an aqua copper complex is used, an oxidizing agent having a potential of greater than 0.153 volts versus normal hydrogen electrode is necessary to oxidize Cu(I) to Cu(II). These potentials are for specific complexes only, and may change, as will the useful oxidizers, upon the addition of additives such as ligands (complexing agents) to the compositions of this invention.

The oxidizing agent is preferably an inorganic or organic per-compound. A per-compound as defined by *Hawley's Condensed Chemical Dictionary* is a compound containing at least one peroxy group (-O-O-) or a compound containing an element in its highest oxidation state. Examples of compounds containing at least one peroxy group include but are not limited to hydrogen peroxide and its adducts such as urea hydrogen peroxide and percarbonates, organic peroxides such as benzoyl peroxide, peracetic acid, and di-t-butyl peroxide, monopersulfates (SO_5^-), dipersulfates ($\text{S}_2\text{O}_8^{2-}$), and sodium peroxide. Examples of compounds containing an element in its highest oxidation state include but are not limited to periodic acid, periodate salts, perbromic acid, perbromate salts, perchloric acid, perchloric salts, perboric acid, and perborate salts and permanganates. Examples of non-per compounds that meet the electrochemical potential requirements include but are not limited to bromates, chlorates, chromates, iodates, iodic acid, and cerium (IV) compounds such as ammonium cerium nitrate.

The most preferred oxidizing agents are hydrogen peroxide and its adducts, and monopersulfates. Monopersulfates are compounds which include the oxidizing SO_5^- group as shown below:

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where X_1 and X_2 are each individually H , $\text{Si}(\text{R}')_3$, NH_4 , $\text{N}(\text{R}'')_4$ and alkali earth metals such as Li, Na, K, and so forth; where R' is an alkyl group having from 1 to 10 or more carbon atoms, and wherein R'' is H, an alkyl group, an aryl group, or mixtures thereof including, for example, NMe_4 , NBu_4 , NPh_4 , NMeBu_3 , NHEt_3 and so forth. One well known and preferred class of monopersulfates are combinations of KHSO_5 , KHSO_4 and K_2SO_4 . This combination is known as a triple salt.

The oxidizing agent may be present in the overall chemical mechanical polishing slurry in an amount ranging from about 0.5 to about 50.0 weight percent. It is preferred that the oxidizer is present in the slurry in an amount ranging from about 0.5 to about 10.0 weight percent.

The chemical mechanical composition of this invention includes at least one catalyst. The purpose of the catalyst is to transfer electrons from the metal being oxidized to the oxidizer (or analogously to transfer electrochemical current from the oxidizer to the metal). The catalyst or catalysts chosen may be metallic, non-metallic, or a combination thereof and the catalyst must be able to shuffle electrons efficiently and rapidly between the oxidizer and metal substrate surface. Preferably, the catalyst is chosen from metal compounds that have multiple oxidation states, such as but not limited to Ag, Co, Cr, Cu, Fe, Mo, Mn, Nb, Ni, Os, Pd, Ru, Sn, Ti and V. The term "multiple oxidation states" refers to an atom and/or compound that has a valence number that is capable of being augmented as the result of a loss of one or more negative charges in the form of electrons. Most preferred metal catalysts are compounds of Ag, Cu and Fe and mixtures thereof. Especially preferred are iron catalysts such as but not limited to inorganic salts of iron, such as iron (II or III) nitrate, iron (II or III) sulfate, iron (II or III) halides, including fluorides, chlorides, bromides, and iodides, as well as perchlorates, perbromates and periodates, and

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ferric organic iron (II or III) compounds such as but not limited to acetates, acetylacetonates, citrates, gluconates, oxalates, phthalates, and succinates, and mixtures thereof.

The catalyst may be present in the chemical mechanical polishing composition in an amount ranging from about 0.001 to about 2.0 weight percent. It is preferred that the catalyst will be present in the chemical mechanical polishing composition in an amount ranging from about 0.005 to about 0.5 weight percent. It is most preferred that the catalyst will be present in the composition in an amount ranging from about 0.01 to about 0.05 weight percent. At this preferred catalyst loading level, *i.e.*, 0.05 weight percent or less, and when a non-metallic oxidizing agent such as hydrogen peroxide, urea hydrogen peroxide or monopersulfate is used, the chemical mechanical polishing composition is essentially metal and "metallic ion free" in comparison to commercially available ferric nitrate based slurries.

The amount of catalyst in the chemical mechanical composition of this invention may be varied depending upon the oxidizing agent used. When the preferred oxidizing agent hydrogen peroxide is used in combination with a preferred catalyst such as ferric nitrate, the catalyst will preferably be present in the composition in an amount ranging from about 0.005 to about 0.20 weight percent (approximately 7 to 280 ppm Fe in solution). When the preferred oxidizing agent is a triple salt of monopersulfate and a preferred catalyst such as ferric nitrate is used, the catalyst will preferably be present in the composition in an amount ranging from about 0.05 to about 1.0 weight percent (approximately 70 to about 1400 ppm Fe in solution).

The concentration ranges of catalyst in the chemical mechanical polishing slurry of this invention are generally reported as a weight percent of the entire compound. The use of high molecular weight metal containing compounds that comprise only a small percentage by weight of catalyst is well within the scope of catalysts in this invention. The term catalyst when used herein also encompasses compounds wherein the catalytic metal comprises less than 10% by weight of the metal in the composition and wherein the metal catalyst concentration in the CMP slurry is from about 2 to about 3000 ppm of the overall slurry weight.

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The chemical mechanical composition of this invention may be combined with at least one abrasive to produce a CMP slurry. The abrasive is typically a metal oxide abrasive. The metal oxide abrasive may be selected from the group including alumina, titania, zirconia, germania, silica, ceria and mixtures thereof. The CMP
5 slurry of this invention preferably includes from about 1.0 to about 20.0 weight percent or more of an abrasive. It is more preferred, however, that the CMP slurry of this invention includes from about 3.0 to about 7.0 weight percent abrasive.

The metal oxide abrasive may be produced by any techniques known to those skilled in the art. Metal oxide abrasives can be produced using any high temperature
10 process such as sol-gel, hydrothermal, plasma process, or by processes for manufacturing fumed or precipitated metal oxides. Preferably, the metal oxide is a fumed or precipitated abrasive and, more preferably it is a fumed abrasive such as fumed silica or fumed alumina. For example, the production of fumed metal oxides is a well-known process which involves the hydrolysis of suitable feedstock vapor
15 (such as aluminum chloride for an alumina abrasive) in a flame of hydrogen and oxygen. Molten particles of roughly spherical shapes are formed in the combustion process, the diameters of which are varied through process parameters. These molten spheres of alumina or similar oxide, typically referred to as primary particles, fuse with one another by undergoing collisions at their contact points to form
20 branched, three dimensional chain-like aggregates. The force necessary to break aggregates is considerable and often considered irreversible. During cooling and collecting, the aggregates undergo further collision that may result in some mechanical entanglement to form agglomerates. Agglomerates are thought to be loosely held together by van der Waals forces and can be reversed, *i.e.*, de-
25 agglomerated, by proper dispersion in a suitable media.

Precipitated abrasives may be manufactured by conventional techniques such as by coagulation of the desired particles from an aqueous medium under the influence of high salt concentrations, acids or other coagulants. The particles are filtered, washed, dried and separated from residues of other reaction products by
30 conventional techniques known to those skilled in the art.

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A preferred metal oxide will have a surface area, as calculated from the method of S. Brunauer, P.H. Emmet, and I. Teller, J. Am. Chemical Society, Volume 60, Page 309 (1938) and commonly referred to as BET, ranging from about 5 m²/g to about 430 m²/g and preferably from about 30m²/g to about 170 m²/g. Due to stringent purity requirements in the IC industry the preferred metal oxide should be of a high purity. High purity means that the total impurity content, from sources such as raw material impurities and trace processing contaminants, is typically less than 1 % and preferably less than 0.01 % (*i.e.*, 100 ppm).

In this preferred embodiment, the metal oxide abrasive consists of metal oxide aggregates having a size distribution less than about 1.0 micron, a mean aggregate diameter less than about 0.4 micron and a force sufficient to repel and overcome the van der Waals forces between abrasive aggregates themselves. Such metal oxide abrasive has been found to be effective in minimizing or avoiding scratching, pit marks, divots and other surface imperfections during polishing. The aggregate size distribution in the present invention may be determined utilizing known techniques such as transmission electron microscopy (TEM). The mean aggregate diameter refers to the average equivalent spherical diameter when using TEM image analysis, *i.e.*, based on the cross-sectional area of the aggregate. By force is meant that either the surface potential or the hydration force of the metal oxide particles must be sufficient to repel and overcome the van der Waals attractive forces between the particles.

In another preferred embodiment, the metal oxide abrasive may consist of discrete, individual metal oxide particles having a primary particle diameter less than 0.4 micron (400nm) and a surface area ranging from about 10 m²/g to about 250 m²/g.

It is preferred that the metal oxide abrasive is silica having a surface area of from about 120m²/g to about 200m²/g.

Preferably, the metal oxide abrasive is incorporated into the aqueous medium of the polishing slurry as a concentrated aqueous dispersion of metal oxides, which concentrated aqueous dispersion of metal oxide abrasives typically ranges from about 3 % to about 45 % solids, and preferably between 10 % and 20 % solids. The aqueous

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dispersion of metal oxides may be produced utilizing conventional techniques, such as slowly adding the metal oxide abrasive to an appropriate media, for example, deionized water, to form a colloidal dispersion. The dispersion is typically completed by subjecting it to high shear mixing conditions known to those skilled in the art. The pH of the slurry may be adjusted away from the isoelectric point to maximize colloidal stability.

Other well known polishing slurry additives may be incorporated alone or in combination into the chemical mechanical polishing slurry of this invention. A non-inclusive list is inorganic acids, organic acids, surfactants, alkyl ammonium salts or hydroxides, and dispersing agents.

An additive which may be useful with this invention is one which stabilizes the oxidizer in the presence of the metal complex. It is well known that hydrogen peroxide is not stable in the presence of many metal ions without the use of stabilizers. For this reason, the CMP composition and slurries of this invention may include a stabilizer. Without the stabilizer, the catalyst and the oxidizing agent may react in a manner that degrades the oxidizing agent rapidly over time. The addition of a stabilizer to compositions of this invention reduces the effectiveness of the catalyst. Therefore the choice of the type and amount of stabilizer added to the composition is important and has a significant impact on CMP performance.

The addition of a stabilizer to the compositions and slurries of this invention is presently understood to create a stabilizer/catalyst complex that inhibits the catalyst from reacting with the oxidizing agent. For purpose of this disclosure the term "product of the mixture of at least one catalyst having multiple oxidation states and at least one stabilizer" refers to an admixture of both ingredients as used in a composition and slurry whether or not the combination of ingredients forms a complex in the end product.

Useful stabilizers include phosphoric acid, organic acids (*e.g.*, adipic, citric, malonic, orthophthalic, and EDTA), phosphonate compounds, nitriles and other ligands which bind to the metal and reduce its reactivity toward hydrogen peroxide decomposition and mixture thereof. The acid stabilizers may be used in their conjugate form, *e.g.*, the carboxylate can be used instead of the carboxylic acid. For

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purposes of this application the term "acid" as it is used to describe useful stabilizers also means the conjugate base of the acid stabilizer. For example the term "adipic acid" means adipic acid and its conjugate base. Stabilizers can be used alone or in combination and significantly decrease the rate at which oxidizing agents such as hydrogen peroxide decomposes.

Preferred stabilizers include phosphoric acid, phthalic acid, citric acid, adipic acid, oxalic acid, malonic acid, benzonitrile and mixtures thereof. The preferred stabilizers will be added to the compositions and slurries of this invention in an amount ranging from about 1 equivalent per catalyst to about 3.0 weight percent or more. As used herein, the term "equivalent per catalyst" means one molecule of stabilizer per catalyst ion in the composition. For example 2 equivalents per catalyst means two molecules of stabilizer for each catalyst ion.

Most preferred stabilizers include from about 2 equivalents per catalyst to about 15 equivalents per catalyst of malonic acid, from about 3 equivalents per catalyst to about 3.0 weight percent phthalic acid, and the combination of from about 0 equivalents per catalyst to about 3 equivalents per catalyst oxalic acid and from about 0.2 to about 1.0 weight percent adipic acid.

The chemical mechanical polishing composition of this invention has been found to have a high tungsten (W) polishing rate as well as good polishing rates towards titanium (Ti). In addition, the chemical mechanical polishing composition exhibits desirable low polishing rates towards the dielectric insulating layer.

The composition of this invention may be produced using any techniques known to those skilled in the art. In one method, the oxidizing agent and catalyst are mixed into the aqueous medium, such as deionized or distilled water, at pre-determined concentrations under low shear conditions until such components are completely dissolved in the medium. A concentrated dispersion of the metal oxide abrasive, such as fumed silica, is added to the medium and diluted to the desired loading level of abrasive in the final CMP slurry. In addition, the catalyst and additive such as one or more stabilizers, may be added to the slurry by any method that is able to incorporate metal catalytic compounds of this invention in an aqueous solution.

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In another method, the stabilizer and catalyst are admixed to form a complex prior to combining the complex with an oxidizing agent such as hydrogen peroxide. This may be accomplished by admixing the stabilizer and a metal oxide abrasive dispersion to give an abrasive/stabilizer dispersion followed by admixing the catalyst with the abrasive/stabilizer dispersion to give a catalyst/stabilizer complex in a metal oxide dispersion. The oxidizing agent is then added to the admixture. When the metal oxide abrasive is alumina, then the stabilizer and catalyst should be admixed to form a complex prior to admixing the complex with the alumina abrasive, otherwise the catalyst may be rendered ineffective.

The compositions of the present invention may be supplied as one package system (at least one oxidizing agent, at least one catalyst, optional abrasive, and optional additives in a stable aqueous medium). To avoid possible composition degradation, however, it is preferred that at least a two package system is used where the first package comprises at least one oxidizing agent, and the second package comprises at least one catalyst. Optional components, such as an abrasive and any optional additives may be placed in either the first container, the second container or in a third container. Furthermore, the components in the first container or second container may be in dry form while the components in the corresponding container are in the form of an aqueous dispersion. For example, the first container may comprise an oxidizer, such as hydrogen peroxide, in liquid form while the second container comprises a catalyst, such as ferric nitrate, in dry form. Alternately, the first container may comprise a dry oxidizing agent while the second container may comprise an aqueous solution of at least one catalyst. Other two-container, and three or more container combinations of the ingredients of the chemical mechanical composition and CMP slurry of this invention are within the knowledge of one of ordinary skill in the art.

Due to potential concerns about shipping CMP slurries containing oxidizing agents, and especially where hydrogen peroxide is used, it is preferred that the CMP composition and CMP slurries of this invention are prepared and packaged as a CMP precursor, shipped to a customer or other point of use, and combined with hydrogen peroxide or any other oxidizing agent at the designated facility prior to use.

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Therefore, a further aspect of this invention is a CMP precursor composition and/or slurry comprising one or more ingredients selected from the group including catalysts, abrasives, and stabilizers in dry or aqueous form but lacking an oxidizing agent. The CMP precursor composition is then combined with at least one oxidizing agent and preferably hydrogen peroxide.

A preferred CMP precursor composition does not include an oxidizing agent but will include the product of the combination of at least one catalyst having multiple oxidation sites and at least one stabilizer with or without one or more abrasives. A most preferred CMP precursor composition will not include any oxidizing agent and will include from about 3.0 to about 7.0 weight percent silica, from about 0.01 to about 0.05 weight percent ferric nitrate, and about 2 equivalents per catalyst to about 15 equivalents per catalyst of malonic acid. As stated above, the oxidizing agent is then mixed with the CMP precursor composition at the point of use.

A single or multi-package (or multi-container) chemical mechanical composition or CMP slurry of this invention may be used with any standard polishing equipment appropriate for use on the desired metal layer of the wafer. The multi-package system includes one or more CMP components in aqueous or dry form in two or more containers. The multi-package system is used by combining the components from the various containers in the desired amounts to give a CMP slurry comprising at least one oxidizing agent, at least one catalyst, and an optional abrasive in amounts described above.

EXAMPLES

We have discovered that a composition including an oxidizer and a catalyst is capable of polishing a multiple metal layer comprising tungsten and titanium at high rates while exhibiting an acceptable low polishing rate towards the dielectric layer.

The following examples illustrate preferred embodiments of this invention as well as preferred methods for using compositions of this invention.

EXAMPLE 1

Polishing slurries were prepared in order to evaluate the performance of the resulting CMP slurries on tungsten wafer CMP. Performance parameters measured included tungsten polishing rates. A standard abrasive slurry including 5.0 weight percent colloidal silica and deionized water was used for all runs. Various oxidizing agents and catalysts were added to the standard abrasive slurry in order to evaluate the effect of various CMP slurry compositions on tungsten polishing rates. The polishing slurries were prepared by combining appropriate amounts of SCE fumed silica-based dispersion manufactured by Cabot Corporation and sold under the trademark CAB-O-SPERSE® with the recited amounts of oxidizing agent, catalyst, and, if appropriate, additional additives.

The CMP slurries were applied to chemically-mechanically polish tungsten blanket wafers having thickness of approximately 8000 Å using a SUBA 500/SUBA IV pad stack manufactured by Rodel, Inc. The polishing was performed using a IPEC/WESTECH 472 CMP tool for one minute at a down force of 5 psi, a slurry flow rate of 150 ml/min, a table speed of 60 rpm, and a spindle speed of 65 rpm.

EXAMPLE 2

Five polishing slurries were prepared according to the method of Example 1 to investigate the effect of the addition of a ferric nitrate catalyst, and/or a hydrogen peroxide oxidizing agent to a CMP slurry on tungsten rates. Each slurry included 5.0 wt % fumed silica. The concentrations of hydrogen peroxide and ferric nitrate in each slurry are indicated in Table 1.

Table 1

Slurry	H ₂ O ₂ wt %	Ferric Nitrate wt %	W CMP Rate (Å/min)
1	0	0	43
2	0	0.2	291
3	5.0	0	385
4	5.0	0.02	4729
5	5.0	0.05	6214

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As shown in Table 1, the control samples (slurries 1-3) polish tungsten at unacceptably low rates. In particular, neither hydrogen peroxide alone nor catalytic amounts of ferric nitrate alone achieve significant tungsten rates. Slurries 4 and 5, however, demonstrate that when an oxidizing agent and a catalyst are used in combination, there is a strong synergistic effect that results in tungsten rates on the order of 5000 Å/min and greater. The addition of catalytic amounts of ferric nitrate to hydrogen peroxide (or conversely the addition of hydrogen peroxide to ferric nitrate) results in greater than one order of magnitude increase in tungsten rates.

EXAMPLE 3

Five polishing slurries were prepared and tested according to the methods set forth in Example 1 in order to investigate the effect of the addition of ferric nitrate catalyst and/or monopersulfate oxidizing agent to a CMP slurry on tungsten chemical mechanical polishing rates. The source of monopersulfate used in this Example is Oxone® monopersulfate manufactured by DuPont. Oxone® consists of the triple salt: $2\text{KHSO}_5 \cdot \text{KHSO}_4 \cdot \text{K}_2\text{SO}_4$, and is approximately 50% monopersulfate by weight. Each slurry included 5.0 wt % fumed silica. The concentrations of ferric nitrate and monopersulfate in the slurries are set forth in Table 2 below.

Table 2

Slurry	Oxone® wt %	Ferric nitrate wt %	W CMP Rate Å/min
1	0.0	0.0	43
2	0.0	0.2	291
3	10.0	0.0	264
4	20.0	0.0	413
5	10.0	0.2	3396

As shown in Table 2, the control samples, (slurries 1-4), polish tungsten at unacceptably low rates. Slurry 5, a combination of 5.0 wt. % monopersulfate and 0.2 wt. % ferric nitrate catalyst was able to polish a tungsten layer at a very high rate, once

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again demonstrating the synergistic effect of combining an electron shuffling catalyst with an oxidizing agent that has an electrochemical potential greater than the potential necessary to oxidize the catalyst.

EXAMPLE 4

Eight polishing slurries, each including varying amounts of hydrogen peroxide and ferric nitrate were prepared and tested according to the methods set forth in Example 1. Each slurry included 5.0 wt % fumed silica. The concentrations of ferric nitrate and hydrogen peroxide in the slurries are set forth in Table 3 below.

Table 3

Slurry	H ₂ O ₂ wt %	Ferric Nitrate wt %	W CMP Rate Å/min
1	0.1	0.20	717
2	1.0	0.05	2694
3	2.0	0.02	3019
4	3.0	0.01	2601
5	3.0	0.02	3420
6	3.0	0.05	4781
7	5.0	0.01	3374
8	5.0	0.02	4729
9	5.0	0.05	6214

As shown in Table 3, tungsten polishing rates vary depending upon both the amount of hydrogen peroxide and the amount of ferric nitrate catalyst in the slurry. Furthermore, the results reported in Table 3 also demonstrate that only a very small amount of catalyst -- 0.05 weight percent or less -- is very effective in catalyzing tungsten polishing using a CMP slurry comprising hydrogen peroxide.

EXAMPLE 5

Nine polishing slurries were prepared and tested according to the methods set forth in Example 1 in order to investigate the effect of varying the amount of ferric

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nitrate catalyst and/or monopersulfate (Oxone®) oxidizing agent in a CMP slurry on tungsten chemical mechanical polishing rates. Each slurry included 5.0 wt % fumed silica. The concentrations of ferric nitrate and monopersulfate in the slurries are set forth in Table 4 below.

5

Table 4

Slurry	Oxone [®] wt %	Ferric Nitrate wt %	W CMP Rate Å/min
1	5.0	0.05	1925
2	5.0	0.14	2921
3	5.0	0.2	3178
4	5.0	0.35	3401
5	10.0	0.036	1661
6	10.0	0.2	3396
7	10.0	0.5	3555
8	15.0	0.05	2107
9	15.0	0.35	3825

The results of the tungsten CMP reported in Table 4 demonstrates that varying the amount of monopersulfate in the CMP slurry has a lesser effect on tungsten polishing rates than varying the amount of catalyst in the CMP slurry.

10

EXAMPLE 6

Eleven CMP slurries were prepared and tested according to the method set forth in Example 1 in order to investigate the effect of varying the catalyst type and oxidizing agent type on tungsten chemical mechanical polishing rates. Each slurry included 5.0 wt % fumed silica. The type and concentrations of catalyst and oxidizing agent used in each CMP slurry are set forth in Table 5 below.

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Table 5

Slurry	Oxidizer wt %	Catalyst wt %	W CMP Rate Å/min
1	5.0% H ₂ O ₂	28 ppm Cu	1417
2	5.0% H ₂ O ₂	70 ppm Cu, 7 ppm Fe	2134
3	5.0% H ₂ O ₂	28 ppm Ag	561
4	5.0% H ₂ O ₂	28 ppm Fe	4729
5	5.0% Oxone [®]	560 ppm Cu	1053
6	5% Oxone [®]	700 ppm Ag	608
7	5.0% Oxone [®]	280 ppm Fe	3178
8	5.0% (NH ₄) ₂ S ₂ O ₈	70 ppm Cu	712
9	5.0% (NH ₄) ₂ Ce(NO ₃) ₆	70 ppm Fe	1501
10	5.0% K-Iodate	70 ppm Fe	1203
11	5.0% H ₂ O ₂ , 1.0% Oxone [®]	280 ppm Fe	7840

Each slurry tested exhibited tungsten polishing rates superior to slurries including only an oxidizing agent (Example 2 - slurry 3; Example 3 - slurries 3 & 4) and superior to slurries including catalyst alone (Example 2 - slurry 2; Example 3 - slurry 2).

EXAMPLE 7

Two polishing slurries were prepared in order to evaluate their performance on patterned device wafers. Each wafer consisted of a W/TiN/Ti metallization deposited over a patterned PETEOS layer. The initial W layer thickness was 8000 Å, the TiN layer 400 Å, and the Ti layer 250 Å. Each wafer was polished until the W/TiN/Ti metallization was cleared from the entire wafer. The polishing conditions set forth in Example 1 were used. Slurries 1 and 2 contained 5.0 weight percent fumed silica. The type and concentrations of the catalyst and oxidizing agent used in each slurry are set forth in Table 6. A third commercially available slurry including 3 weight percent alumina abrasive and 5.0 weight percent ferric nitrate was also evaluated.

Table 6

Slurry	Oxidizer (wt %)	Catalyst	Time to Clear
1	5% H ₂ O ₂	28 ppm Fe	90 seconds
2	5% H ₂ O ₂ & 1% Oxone [®]	280 ppm Fe	70 seconds
3	Commercial Slurry - 5 wt % Ferric Nitrate		170 seconds

Excellent polishing performance was achieved using slurries 1 and 2. The slurries were observed to have high polishing rates on each of the metallization layers, resulting in a minimum time to clear the metallization. Both catalyst containing slurries exhibited superior performance in comparison to the commercially available slurry. Examination of the polished wafers with atomic force microscope demonstrated that the device wafers were successfully planarized, with acceptable low levels of erosion and dishing of stud and line features. Furthermore, the underlying PETEOS layer was smooth with no evidence of scratches or pits.

EXAMPLE 8

This example demonstrates the enhancement of oxidizing agent longevity caused by adding various stabilizers to a chemical mechanical polishing slurry. Two chemical mechanical polishing slurries were evaluated. The first slurry consisted of 5.0 wt % silica, 0.02 wt % ferric nitrate•(H₂O)₉ catalyst, 5.0 wt % H₂O₂ oxidizing agent, the amount of stabilizer set forth in Table 7 below, and deionized water. The second slurry consisted of 5.0 wt % silica, 0.036 wt % ferric nitrate•(H₂O)₉ catalyst, 6 or 8 wt % H₂O₂ oxidizing agent, the amount of stabilizer set forth in Table 8 below, and deionized water. The silica used in both slurries is a fumed silica based dispersion manufactured by Cabot Corporation and sold under the trademark CAB-O-SPERSE[®].

The slurries were prepared and applied to tungsten wafers according to the method of example 1. The slurries were then allowed to age for several days after which a known amount of the aged slurry was sampled and titrated with potassium permanganate to determine the amount of active peroxide remaining. The titration and polishing results are reported in Tables 7 and 8 below.

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Table 7

Stabilizer	% hydrogen peroxide remaining after 8 days	W Polishing rate (Å/min)	Silica Surface Area (m ² /g)
1.1 equiv. phosphonic acid	94	670	90
4.9 equiv. phosphoric acid	93	1600	90
6.0 equiv. phthalic acid	91	2200	90
3-5 equiv. citric acid	72-89	2200	90
3-5 equiv. malonic acid	79-85	2500	90
None	0	4300	90

Table 8

Stabilizer	% hydrogen peroxide remaining after 6 days	W polishing rate (Å/min)	Silica Surface Area (m ² /g)
1% adipic acid	76%	3451	150
0.5% adipic acid 1 equiv oxalic acid e	84%	4054	150
5 equiv malonic acid	83%	3802	90

The results indicate that the hydrogen peroxide activity was maintained in each slurry that included a stabilizer in comparison to the slurry containing no stabilizer which had no hydrogen peroxide activity after 8 days. The polishing results are acceptable and demonstrate that stabilizers effect the catalyst efficiency of the slurry. Therefore, there is a balance between a chemically stable slurry and the high tungsten rates that are promoted by the catalyst/oxidizing agent combinations.

EXAMPLE 9

Tungsten wafers were polished according to the method of Example 1 using a slurry including an alumina abrasive. The alumina dispersion used in each slurry was W-A355 manufactured by Cabot Corporation. The slurry compositions tested and their polishing results are set forth in Table 9, below.

Table 9

Slurry	H ₂ O ₂ (wt %)	Alumina (wt%)	ferric nitrate •(H ₂ O) ₉	Stabilizer (wt%)	W Rate (A/min)
1	5.0%	3.0%	0.02%	None	566
2	5.0%	3.0%	0.02%	1% citric acid	1047
3	6.0%	3.0%	0.036%	0.091% Potassium Hydrogen Phthalate	1947
4	6.0%	3.0%	0.036%	0.1066% Tetrafluoro phthalate	2431
5	6.0%	3.0%	0.036%	0.0466% g Malonic Acid	2236

As illustrated from slurries 2-5 of Table 9, alumina, when combined with an oxidizing agent and a catalyst stabilizer complex, is effective in polishing a tungsten substrate.

5 While the present invention has been described by means of specific embodiments, it will be understood that modifications may be made without departing from the spirit of the invention. The scope of the invention is not to be considered as limited by the description of the invention set forth in the specification and examples, but rather as defined by the following claims.

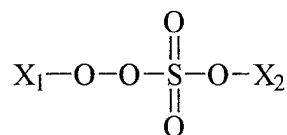
10 For example, although the examples above have described the preparation of CMP slurries with metal catalysts, it is to be understood that non-metal catalysts having multiple oxidation states may be incorporated into useful CMP compositions and slurries of this invention.

15 What is claimed is.

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CLAIMS

1. A chemical mechanical polishing composition comprising:
at least one oxidizing agent; and
5 at least one catalyst having multiple oxidation sites.
2. The chemical mechanical polishing composition of claim 1 wherein the oxidizing agent has an electrochemical potential greater than the electrochemical potential necessary to oxidize the catalyst.
- 10 3. The chemical mechanical polishing composition of claims 1-2 wherein the oxidizing agent is an organic per compound, an inorganic per compound, a non-per compound including bromates, chlorates, chromates, iodates, iodic acid, cerium (IV) compounds, and mixtures thereof.
- 15 4. The chemical mechanical polishing composition of claims 1-3 wherein the oxidizing agent is a monopersulfate, persulfate, peroxide, periodate and mixtures thereof.
- 20 5. The chemical mechanical polishing composition of claims 4 wherein the oxidizing agent includes at least one monopersulfate having the formula:



- 25 where X_1 , X_2 are each individually H, $\text{Si}(\text{R}')_3$, NH_4 , $\text{N}(\text{R}'')_4$ and alkali earth metals such as Li, Na, K; where R' is an alkyl group having from 1 to 10 or more carbon atoms; and wherein R'' is H, an alkyl group, an aryl group, or mixtures thereof.

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6. The chemical mechanical polishing composition of claims 4 or 5 including from about 0.5 to about 20 weight percent monopersulfate.

5 7. The chemical mechanical polishing composition of claims 4-6 including from about 1 to about 20 weight percent $2\text{KHSO}_5 \cdot \text{KHSO}_4 \cdot \text{K}_2\text{SO}_4$.

8. A chemical mechanical polishing precursor composition comprising:
the product of the mixture of at least one catalyst having multiple oxidation sites
10 and at least one stabilizer.

9. A chemical mechanical polishing composition comprising:
at least one oxidizing agent; and
the product of the mixture of at least one catalyst having multiple oxidation sites
15 and at least one stabilizer.

10. The composition of claims 8 or 9 wherein the stabilizer is an organic acid, an inorganic acid, a nitrile, and mixtures thereof.

20 11. The composition of claims 8-10 wherein the stabilizer is selected from the group consisting of phosphoric acid, phthalic acid, citric acid, malonic acid, phosphonic acid, oxalic acid, adipic acid, benzonitrile, and mixtures thereof.

12. The composition of claims 8-11 wherein the stabilizer is the admixture of from
25 about 0 equivalents per catalyst to about 3 equivalents per catalyst of oxalic acid, and from about 0.2 to about 1.0 weight percent adipic acid.

13. The composition of claims 8-11 wherein the stabilizer is from about 2 equivalents per catalyst to about 15 equivalents per catalyst of malonic acid.

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14. The composition of claims 8-11 wherein the stabilizer is from about 3 equivalents per catalyst to about 3.0 weight percent phthalic acid.

15. The composition of claim 9-14 wherein the oxidizing agent is an organic compound, inorganic compound, and mixtures thereof.

16. The composition of claims 1-7 or 9-15 wherein the oxidizing agent is between about 0.1 to about 50 weight percent hydrogen peroxide.

17. The composition of claims 1-7 or 9-16 wherein the oxidizing agent is between about 0.5 to about 10 weight percent hydrogen peroxide.

18. The composition of claims 1-17 wherein the catalyst is a metal catalyst.

19. The composition of claim 18 wherein the metal catalyst is a compound of Ag, Co, Cr, Cu, Fe, Mo, Mn, Nb, Ni, Os, Pd, Ru, Sn, Ti, V and mixtures thereof having multiple oxidation states.

20. The composition of claim 19 wherein the metal catalyst is a compound of iron, copper, silver, and any combination thereof having multiple oxidation states.

21. The composition of claims 1-20 wherein the catalyst is an iron catalyst selected from the group consisting of inorganic iron compounds and organic iron compounds having multiple oxidation states.

22. The composition of claims 1-21 wherein the catalyst is ferric nitrate.

23. The composition of claim 22 wherein the iron catalyst is between 0.01 to about 0.5 weight percent ferric nitrate.

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24. The composition of claims 1-22 including from about 0.001 to about 2.0 weight percent catalyst.
- 5 25. The composition of claims 1-22 or 24 including from about 0.005 to about 0.2 weight percent catalyst.
- 10 26. The composition of claims 1-4 or 9-24 wherein the oxidizing agent is hydrogen peroxide and the catalyst is from about 0.01 to about 0.5 weight percent of an iron catalyst.
27. The composition of claims 1-7 or 9-24 wherein the oxidizing agent is monopersulfate and wherein the catalyst is from about 0.05 to about 1.0 weight percent of an iron catalyst.
- 15 28. The composition of claims 1-27 which further comprises an abrasive.
29. The composition of claims 1-28 wherein the abrasive is at least one metal oxide.
- 20 30. The composition of claims 1-29 wherein the metal oxide abrasive is selected from the group including alumina, ceria, germania, silica, titania, zirconia, and mixtures thereof.
- 25 31. The composition of claims 1-30 wherein the abrasive is an aqueous dispersion of a metal oxide.
32. The composition of claims 1-31 wherein the metal oxide abrasive consists of metal oxide aggregates having a size distribution less than about 1.0 micron and a mean aggregate diameter less than about 0.4 micron.
- 30 33. The composition of claims 1-32 wherein the metal oxide abrasive consists of discrete, individual metal oxide spheres having a primary particle diameter less

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than 0.400 micron and a surface area ranging from about 10 m²/g to about 250 m²/g.

34. The composition of claims 1-33 wherein the abrasive has a surface area ranging from about 5 m²/g to about 430 m²/g.

35. The composition of claims 1-34 wherein the abrasive has a surface area of from about 30 m²/g to about 170 m²/g.

36. The composition of claims 1-35 wherein the abrasive is precipitated abrasives or fumed abrasives.

37. The composition of claims 1-36 wherein the abrasive is precipitated silica, fumed silica or fumed alumina.

38. The chemical mechanical polishing composition of claim 1 which comprises:
an abrasive;

an iron catalyst; and

from about 1.0 to about 10.0 weight percent of an oxidizing agent selected from the group consisting of hydrogen peroxide and monopersulfate wherein when the oxidizing agent is hydrogen peroxide, then the slurry includes from about 0.01 to about 0.05 weight percent ferric nitrate and when the oxidizing agent is monopersulfate, then the slurry includes from about 0.1 to about 0.5 weight percent ferric nitrate catalyst.

39. A chemical mechanical polishing slurry comprising:

from about 1.0 to about 15.0 weight percent silica;

from about 0.1 to about 0.5 weight percent ferric nitrate catalyst; and from about 1.0 to about 10.0 weight percent monopersulfate.

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40. A chemical mechanical polishing slurry comprising:
from about 1.0 to about 15.0 weight percent silica;
from about 0.01 to about 0.05 weight percent ferric nitrate catalyst; and from
about 1.0 to about 10.0 weight percent hydrogen peroxide.

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41. A chemical mechanical polishing slurry comprising:
from about 3.0 to about 7.0 weight percent silica;
from about 0.01 to about 0.05 weight percent ferric nitrate catalyst; and
the product of the admixture of from about 0.5 to about 10.0 weight percent
hydrogen peroxide and from about 2 equivalents per catalyst to about 15
equivalents per catalyst malonic acid.

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42. The slurry of claim 41 wherein the silica has a surface area between about 120
 m^2/g to about 200 m^2/g .

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43. A chemical mechanical polishing precursor composition comprising an aqueous
solution of from about 3.0 to about 7.0 weight percent silica, and the product of
the admixture of from about 0.01 to about 0.05 weight percent ferric nitrate
catalyst and from about 2 equivalents per catalyst to about 15 equivalents per
catalyst malonic acid.

20

44. A method for polishing a substrate including at least one metal layer comprising
the steps of:

- (a) admixing the compositions of claims 8, 10-14, 18-25, 29-37 or 43 and
deionized water to give a chemical mechanical polishing precursor;
- (b) admixing the chemical mechanical polishing precursor of step (a) with an
oxidizing agent to give a chemical mechanical polishing slurry;
- (c) applying the chemical mechanical polishing slurry to the substrate; and
- (d) removing at least a portion of the metal layer from the substrate by
bringing a pad into contact with the substrate and moving the pad in
relation to the substrate.

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45. A method for polishing a substrate including at least one metal layer comprising the steps of:

- (a) admixing the chemical mechanical polishing compositions of claims 1-7 or 9-42 and deionized water to give a chemical mechanical polishing slurry;
- (b) applying the chemical mechanical polishing slurry to the substrate; and
- (c) removing at least a portion of the metal layer from the substrate by bringing a pad into contact with the substrate and moving the pad in relation to the substrate.

46. The method of claims 44-45 wherein the substrate includes a tungsten containing metal layer wherein at least a portion of the tungsten layer is removed in step (c).

47. The method of claims 44-46 wherein the substrate further includes a titanium and/or titanium nitride metal layer wherein at least a portion of the titanium nitride layer is removed in step (c).

48. A chemical mechanical polishing composition multi-package system comprising:

- (a) a first container comprising the composition of claims 8, 10-14, 18-25, 29-37 or 43; and
- (b) a second container comprising an oxidizing agent.

INTERNATIONAL SEARCH REPORT

International application No.
PCT/US97/22083

A. CLASSIFICATION OF SUBJECT MATTER

IPC(6) :B24B 1/00; H01L 21/00

US CL : 438/692, 693; 252/182.32, 186.1; 216/53

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 438/692, 693; 252/182.32, 186.1, 183.4, 182.1 ; 216/53; 510/175;

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

APS

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 5,340,370 A (CADIEN et al.) 23 August 1994, col 6 line 36 - col 7 line 34	1-3
X	US 4,885,106 A (LAPHAM et al.) December 1989, col 2 lines 33-44	1-3
X	US 5,354,490 A (YU et al.) 11 October 1994, col 2 line 37 - col 3 line 52	1-3
Y	US 5,527,423 A (NEVILLE et al.) 18 June 1996, col 5 line 8- col 6 line 5, Examples 1-5	8-9, 38, 41-43
X	US 3,877,938 A (SHINOZAKI et al.) 15 April 1975, col 3 line 42 - col 4 line 2	8-9, 41, 43
A	US 4,671,851 A (BEYER et al.) 09 June 1987	



Further documents are listed in the continuation of Box C.



See patent family annex.

* Special categories of cited documents:	*T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
A document defining the general state of the art which is not considered to be of particular relevance	*X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
E earlier document published on or after the international filing date	*Y* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
L document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	*&* document member of the same patent family
O document referring to an oral disclosure, use, exhibition or other means	
P document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search

04 MARCH 1998

Date of mailing of the international search report

28 APR 1998

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INTERNATIONAL SEARCH REPORT

International application No.
PCT/US97/22083

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 4,789,648 A (CHOW et al.) O6 December 1988	
A	US 4,910,155 A (COTE et al.) 20 March 1990	
A	US 4,944, 836 A (BEYER et al.) 31 July 1990	
A	US 5,209,816 A (YU et al.) 11 May 1993	
A	US 5,244,534 (YU et al.) 14 September 1993	