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(54) **Title**: DEVICE AND METHOD FOR REAL-TIME MEASUREMENT OF PARAMETERS OF MECHANICAL STRESS STATE AND BIOMECHANICAL PROPERTIES OF SOFT BIOLOGICAL TISSUE

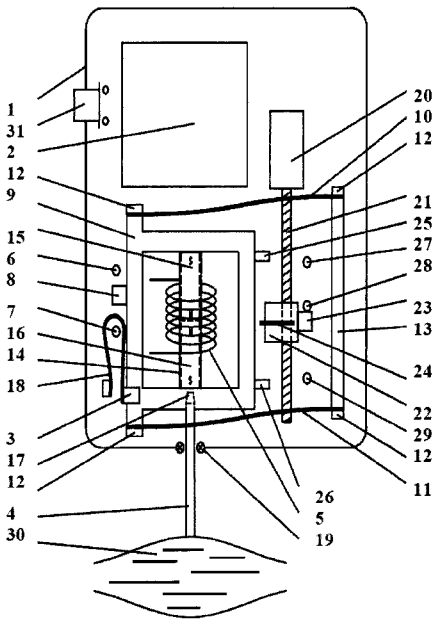

FIG 1

(57) **Abstract**: A device and a method for simultaneous recording, in real time, of the parameters characterising the mechanical tension, elasticity, dynamical stiffness, creepability and mechanical stress of soft biological tissue is provided. By means of the myometer, a constant external pre-pressure is created, independently of the device's position, between the tissue and the testing end of the device. Next, the tissue is subjected to a short-term external dynamic influence. The mechanical change in the shape of the tissue and its mechanical response are registered as a graph of the tissue's oscillations. For calculating the parameters, the time span on the graph is used which involves the oscillation period from the beginning to the end of the effect on the tissue plus its subsequent first 1.5 self-oscillation period. Invention enables recording and data-processing to be carried out simultaneously as well as statistically significant estimates to be made in real time.

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DEVICE AND METHOD FOR REAL-TIME MEASUREMENT OF PARAMETERS OF MECHANICAL STRESS STATE AND BIOMECHANICAL PROPERTIES OF SOFT BIOLOGICAL TISSUE

FIELD OF THE INVENTION

This invention belongs to the realm of medical technology, it is designed to measure the mechanical stress and biomechanical properties of the parameters of soft biological tissues and to statistically assess their state in real time.

BACKGROUND OF THE INVENTION

The biomechanical properties of soft biological tissue involve its elasticity, dynamical stiffness, creepability, and mechanical stress relaxation time.

In evidence-based medicine, both the parameters characterising the stress of superficial soft biological tissues, for example of skeletal muscle, and its biomechanical properties are used as a supplementary source of information. The said parameters allow specialists to quantitatively determine the extent of pathological processes, and the efficiency of various massage techniques, physiotherapeutic procedures, medication and training programmes, as well as ascertaining the tone of tissues during an operation, and fixing the time of death in forensics.

Until now, many attempts have been made to measure the stress (tone) of soft biological tissues by various methods, but neither has such a device been invented nor such a method found yet that would measure all the variables characterising the abovementioned parameters in a way that is universal and realisable/applicable in daily clinical practice in real time.

Tone is defined as the mechanical stress of skeletal muscle with no voluntary contraction of the muscle. If we multiply the numerical value of the skeletal muscle stress by its cross-section area, we get the value of the force by which the tendon of skeletal muscle is pulling the periosteum of the bone.

There are three types of tone:

1) The passive resting tone - a state of skeletal muscle with no contraction in the muscle when the muscle is not balancing force torques on the observed joint axis caused by the force of gravity with its mechanical tension. There is no electomyographic (EMG) signal.

2) The resting tone (relaxation) - a state of mechanical stress (or tension) of skeletal muscle without voluntary contraction with EMG activity due to, for instance, an emotional or pathological condition. Such a state is more variable than the passive resting tone. The muscle force torques in antagonist muscles are balanced.

3) The postural tone is a state of skeletal muscle in which the muscle is balancing the force torques of body segments caused by the force of gravity in order to maintain the equilibrium position. When keeping the position, the muscle tension and stiffness are changing persistently, the variability of which is several times greater than in passive relaxed tone. The state of mechanical tension and stiffness level are also significantly higher.

The tone of the skeletal muscle cannot be decreased at will. The level of the tone depends on intramuscular pressure - the higher the intramuscular pressure, the greater the mechanical tensile stress in the muscle (Vain A. 2006 The Phenomenon of Mechanical Stress Transmission in Skeletal Muscles. Acta

Academiae Olympiquae Estoniae, Vol 14, No. 1/2 pp. 38-48). If the intramuscular pressure is high, the outflow of venous blood from the muscle will slow down because the veins have no substantial internal blood pressure and when the intramuscle pressure rises, then the veins' cross-section area will decrease. In the case of passive rest, this causes the situation that skeletal muscles' ability to work is restored slowly. Additionally, the ergonomic efficiency of muscle activity in performing movements will decrease since the momentum of force caused by antagonist muscles for turning the part of the body on the axis of the joint increases on account of the work needed to stretch the antagonist muscles. The amount of work A done when stretching the antagonist muscles can be calculated by the following formula:

$$A = F_{resistance} * s \ (J)$$

where $F_{resistance}$ - resistant force (N),

s - extent of stretch (m),

whereas $F_{resistance} = 2*v*f*D*m \ (N)$,

where v - speed of stretching (m/s),

f - muscle's natural oscillation frequency (Hz),

D - logarithmic decrement of a muscle's natural oscillation,

m - mass of the muscle being stretched (kg).

It is technically complicated to measure skeletal muscle's state of mechanical stress. However, there has been revealed a functional connection between a material's natural oscillation frequency and its mechanical stress, which in the case of short-term measurements makes it possible to characterise the mechanical state of skeletal muscle.

The logarithmic decrement of a muscle's natural oscillation shows how much mechanical energy dissipates during one period

of the muscle's natural oscillation. Hence, the elasticity of skeletal muscle (one of the biomechanical qualities of the muscle) can be characterised via the logarithmic decrement of the muscle's natural oscillation. Elasticity of soft biological tissue means its ability to restore its former shape after the deforming force is removed. The opposite term to elasticity is plasticity. If an elastic body changes its shape as a result of an impulse transmitted by external forces, then simultaneously mechanical energy of elasticity is stored in the morphological structures of skeletal muscle which possess elasticity properties. When the impulse from the deforming force ends, then the stored mechanical energy will restore the body's initial shape at a velocity that accords to the value of the logarithmic decrement - very quickly if the value approaches zero, and more slowly if the value is higher. Hence, in a device built to register the parameter characterising elasticity, the effect of oscillation damping must be brought to a minimum.

In a working muscle, contraction and relaxation alternate. The duration of each may vary. Sometimes it may last only a split of a second. If the relaxation period is short and the muscle's logarithmic decrement is big, then the initial shape of skeletal muscle fails to be completely restored, the muscle's internal pressure falls insufficiently and, as a result, the outflow of venous blood from the muscle is slowed down. The time taken for the muscle's work capacity to be restored increases, its fatigue also increases, and the danger of a muscle overload trauma becomes a reality.

Stiffness is a biomechanical property of skeletal muscle which consists in its resistance to any force changing its shape. The property inversely proportional to stiffness is compliance. The unit of measurement of both is N/m. How economical and how accurately co-ordinated a person's movements are depends on the stiffness of his/her skeletal muscles. Creepability is a biomechanical property of soft

biological tissue to deform permanently under constant stress. The creepability property of liquids has been quantitatively measured (US4534211, Molina O. G. 1985).

The creepability property of soft biological tissue might be characterised, for example, by the Deborah number D_e. The Deborah number is a quantity whose dimension is 1; this number is used to characterise the viscoelasticity of tissues (or creepability of materials). The latter is expressed as the ratio of relaxation time, $t_{material}$, representing the intrinsic properties of tissue, and the characteristic time scale of an experiment, or deformation time, $t_{process}$:

$$D_e = \frac{t_{material}}{t_{process}}.$$

The relaxation property of skeletal muscle tissue is defined as the tissue's ability to relieve itself of mechanical stress in the case of constant length.

The viscoelastic properties of skeletal muscle tissue are characterised by creepability and relaxation (Fung Y. C. 1981 Biomechanics. Mechanical Properties of Living Tissues p. 41). Various attempts have been made to measure the state of mechanical stress and biomechanical properties of soft biological tissues *in vivo*. As a result, humanity knows a host of instruments for measuring mechanical stress and stiffness, but no ways have been invented as yet to express creepability and relaxation time of mechanical stress in numerical terms. No such devices or methods are known that would simultaneously measure muscle tone and all the four abovementioned biomechanical properties in real time.

The principal problem is how to evaluate the state of a person's skeletal muscles on the basis of measurement data, while the parameters characterising this state are constantly changing due to their involvement in biological processes.

Therefore, it is insufficient to represent the state of soft biological tissue by one parameter only, which reflects the level of measurable quantities; considering the aspect of diagnostic information, it is relevant that a characteristic describing the variation of levels be added. For assessment of variety, it is important that the reading of the measuring device be repeated in short-term measuring scales (e.g. measuring after every 1 second). In this case, measuring should be carried out and monitored by measuring software (firmware), in order to collect in short term a sufficient amount of measurement data for statistical assessment. No such methods of measurement are known as yet in the diagnostics of soft biological tissues.

Indeed, both methods and devices are available for numerical characterisation of biological tissues' viscoelasticity (e.g., WO2007144520 Method of measuring Viscoelastic Properties of Biological Tissue Employing an Ultrasonic Transducer, EchoSens S.A., 2006), but neither methods nor devices have been disclosed to date that would separately characterise creepability and relaxation properties of soft biological tissues.

None of the earlier solutions allow measurement to be repeated in short term because the impact on soft biological tissue tends to change the measurable quantities, the character of the measurements is not standardised, and the impact does not end with quick release.

Among the known solutions, the method closest to the present invention is the myometer, a device and method for recording of mechanical oscillations in soft biological tissues (EE03374B1, Vain A. 2001). The essence of the myometer lies in causing a short-term effect on soft biological tissue by giving it a mechanical impulse and subsequently recording the

tissue's mechanical response by means of an electromechanical sensor (acceleration sensor).

One drawback of this solution of the closest prior art is that while the obtained acceleration graph enables calculation of the tissue's natural oscillation frequency, indicating its state of stress as well as the logarithmic decrement characterising its elasticity and dynamic stiffness, it does not make it possible to determine the parameters describing creepability and relaxation time of mechanical stress. Secondly, the parameters characterising the tissue's state of mechanical stress, elasticity and stiffness are calculated at different moments of the oscillation, which yields varying results since the mass participating in the oscillation process decreases constantly due to dissipation of mechanical energy in the case of damped oscillation.
Resulting from the construction of said device (inclusion of a lever), the impulse may be followed by resonance oscillations of the parts exerting impact. If the size of the device is reduced, then the shoulder of the lever will become so short that it will cause a 'scraping' impact, which may yield incorrect results as the direction of the tissue's deformation changes during stimulation. Another shortcoming is the constructional solution of the above prior art device, in which bending of the signal cable attached to the acceleration sensor during oscillation will bring about dissipation of the energy of impact.

A shortcoming of the cited prior art device is also the feature that the construction of the measuring apparatus involves rotating details, which need fine tuning to minimise resistance caused by mechanical friction. But the greater the resistance, the less sensitive the device.

An additional drawback of the said closest prior art device is that in such cases when the direction of the testing end with respect to the Earth's gravitational field is changed, the pre-pressure exerted by the mass of the testing end on the superficial tissues covering the muscle will decrease. However, preservation of constant pre-pressure is necessary for delivering the impact energy to the muscle and thereby making it oscillate. If the pre-pressure decreases, the role of superficial tissues grows both in recording the muscle's natural oscillation frequency and in the resulting measurements.

Thus, there exists a need for such a device and method that would allow us to measure in real time, simultaneously, quickly and accurately soft biological tissue's mechanical state of stress and parameters characterising its four biomechanical properties: elasticity, dynamic stiffness, creepability and mechanical stress relaxation time, and achieve, irrespectively of the position of the device in the gravitation field, high sensivity of the device as well as repeatability and reliability of the results.

DISCLOSURE OF THE INVENTION

The aim of the present invention is to provide a universal device and method for simultaneous measuring, in real time, of parameters characterising the state of mechanical stress, elasticity, dynamic stiffness, creepability and mechanical stress relaxation time of soft biological tissues.

To achieve this aim, a device (myometer) comprises the body (1), the processor and controller for governing the measuring process and for calculating parameters (a control means) (2), a recorder, e.g. acceleration sensor (3), the testing end (4), the drive, of the testing end position sensors (6, 7) of a moving frame (9), and a shutter (8) of the said position

sensors, whereas the drive of the testing end is operable in translational motion, without mechanical friction, and is having the same direction as the testing end, and where in the drive of the testing end comprises a testing end mechanism including a moving frame (9) and elastic elements, e.g. elastic plates (10 and 11), whose one ends are inflexibly fastened by collet-type coupling (12) to the base (13), and the other ends are inflexibly fastened by collet-type coupling (12) to a moving frame (9) and whereas the centre of the moving frame (9) surrounds a sleeve (14) which is containing permanent magnets (15, 16) oriented with poles of the same name facing each other and placed in the centre of a solenoid (5), and a testing end (4) whose electrical-steel (i.e. remagnence-free (free of residual magnetism)) cone-shaped end (17), fixed vis-à-vis the directing inflexible moving frame (9), is located in the pulling zone of one of the permanent magnets within the moving frame (9), and said device is equipped with a friction-free element, e.g. a flexible flat cable (18) for direction of the recorder's (3) signal from the moving frame (9) to the control means (2), and the device involves light and/or sound signals placed around an aperture (19) in the testing end (4), and an arresting system involving a drive (20), an actuating screw (21), a slider (22) moving on unmoving base (13) and having an shutter (23), and a means (24) for avoiding mechanical damage to the arresting system, and stoppers (25, 26) of the moving frame together with position sensors (27, 28 and 29). The device is operated by a computer program product stored in the processor memory and comprising portions of the software code adapted to perform the method by stages when the program is running in the processor.

The device's construction and software (computer program) enable the user to achieve repeatability and reliability of the measuring results, allowing simultaneous measurement of

the parameters and processing of data as well as making statistically significant judgements in real time.

The technical solution of the construction elements of the current invention makes it easy to assemble the device. Nor will the device need any fine tuning once it has been assembled. There is no need for tuning joints, e.g. the measuring mechanism.

The method for simultaneous measurement of the parameters characterising the biological tissue's state of mechanical pressure, elasticity, dynamic stiffness, creepability and mechanical stress relaxation time involves the following stages:

Stage A

1) a means for marking the area to be investigated and for facilitating the contact between the testing end and tissue without damaging the latter's integrity and function is attached either to the testing end or the surface of the tissue;

2) the device disclosed above (myometer) is moved close to the surface being measured, in the course of which, irrespectively of the positioning of the device, the gravitation field and the user, the device causes between the tissue under investigation and the testing end a constant external influence (pre-pressure) with force equalling the gravity of the mass of the testing end mechanism. The pre-pressure is maintained in stages B-D throughout the series of measurement;

3)the placing of the device is stopped when either the light or sound signal of the device changes, indicating that the necessary pre-pressure has been achieved and the elastic

element is stress-free, i.e. the preconditions for starting a series of measurements have been met;

Stage B

The device described above exerts on soft biological tissue external single impact for a prescribed number of times by a single impulse of the solenoid's constant electrical power, each impact ends with a quick release. At the start of the impact, the elastic element is stress-free. Throughout the series of measurements, during the prescribed time, the device is kept in the same position until a change of either the light or sound signal indicates the end of the series.

The parameters of a single external mechanical impulse are chosen, depending on the aims of the diagnostic information, from the following ranges: specific power from the range 0.01-0.2 W/mm^2, the quick release from the range 0.1-15 ms, and the time for achieving the maximum impulse from the range 1-5 ms.

Stage C

The mechanical change in the tissue's shape and the tissue's subsequent mechanical response are recorded, in real time, as graphs of the tissue's natural oscillations, for instance, as graphs of acceleration following each impulse in stage B.

Stage D

In addition to calculating the state of mechanical stress, elasticity and dynamic stiffness, simultaneously the parameters characterising the tissue's creepability and relaxation time of mechanical stress together with statistical assessment of all the calculated parameters are computed in real time; for calculating the parameters characterising soft biological tissue's state of mechanical stress, elasticity, dynamic stiffness, creepability and

relaxation time of mechanical stress, the time range from the measured tissue's natural oscillations graph is used, for instance, the time range shown by the accelerations graph, which involves the period from the start to the end of the impact and 1.5 oscillation periods of the tissue's subsequent natural oscillations.

The measuring series consists of single measurements in which the first measurement starts with stage A and is followed by stages B, C, and D. The next measurement in the series proceeds with repetition of stages B, C, and D until completion of the prescribed number of measurements.

To perform stages A to D and calculate the parameters, specially designed software (firmware) is used, which has been stored in the device's processor, comprises portions of software code, and has been adapted to perform stages A to D when the device's firmware is used in the processor. Measuring will be repeated in minimum 1-second intervals for as many times as required for statistical assessment.
By means of the device's firmware, preliminary processing will then be carried out for statistical assessment; the information obtained will enable us to give reliable answers within a few seconds after the end of the measurement, and the repeatability and reliability of the results will be sufficiently accurate to assess both the current state of the soft biological tissue and the longitudinal trends. The above device and method for measuring soft biological tissue's state of mechanical stress and parameters of biomechanical properties allow monitoring the object under investigation in the event of different body postures and various levels of gravitation fields, as well as doing it repeatedly, autonomously, portatively, and in anon-disturbing, non-invasive and cost-effective way (cheaply).

DESCRIPTION OF DRAWINGS

Fig. 1 Principal schematic representation of the device.

Fig. 2 Graph of soft biological tissue's natural oscillation, where

t_T - instant at which the drive of the testing end starts impacting the soft biological tissue mechanically;

t_s - the drive of the testing end is switched off;

t_1 - the beginning of the mechanical influence of the soft biological tissue on the testing end;

t_2 - the end of the restoration of its former shape by the soft biological tissue;

$t_1 - t_T$ - duration of the mechanical impact on the soft biological tissue;

$t_R - t_1$ - time taken by the soft biological tissue to restore its former shape after deformation;

a_1 - maximum acceleration of deformation of the soft biological tissue;

$t_4 - t_1$ - 1.5 natural oscillation periods;

a - graph of the acceleration of the testing end;

v - graph of the velocity of the testing end;

s - graph of the trajectory of the testing end.

DESCRIPTION OF THE EMBODIMENTS

The device for recording the state of mechanical stress and biomechanical properties of soft biological tissues (Fig. 1) comprises the body 1, with a means at its top holding a processor and controller for monitoring the measuring process and for calculating the parameters (a control means 2), a recorder 3 and a moving frame 9 fastened to an inflexibly base 13 by an elastic element, such as elastic plates 10 and 11. The moving frame 9 incorporates a sleeve 14 containing two permanent magnets 15 and 16, whose same-name poles are oriented face to face, while the testing end 4 has been attached to the permanent magnet 16 by means of a cone-shaped

end 17 made of either electrical steel or some other suitable material. To the bottom part of the moving frame 9, a acceleration sensor 3 has been inflexibly fastened and to the middle of the frame, a shutter 8.

Above and beneath the shutter 8, the position sensors 6 and 7, respectively, have been inflexibly fastened to the body 1. In the upper and lower parts of the moving frame 9 are located inflexibly fastened stoppers 25 and 26.

The arresting system of the moving frame 9 comprises a drive 20, an actuating screw 21, a slider 22 with a shutter 23 and a means 24 for preventing mechanical damage to the arresting system. Along the axis of movement of the arresting system are placed position sensors 27 (upper), 28 (middle) and 29 (lower), which are inflexibly connected with the body 1.

A solenoid 5 has been inflexibly fastened to the body 1, lying in the middle of the moving frame 9.

When the measuring process is triggered by turn of the switch 31, the solenoid 5 is activated by electric current directed by the signal picked up from the axis of the acceleration sensor 3, depending on how the body 1 is oriented in the gravitation field. Constant current in the solenoid 5 gives rise to a constant force affecting the two permanent magnets 15 and 16 located in its magnetic field, as a result of which constant pressure is exerted on the slider 22 by the stopper 25 of the moving frame 9. This pressure is then conveyed by the testing end 4 to the biological tissue being measured. Subsequently, the position sensors 6 and 7 of the moving frame 9 are activated, and the slider 22 is positioned by means of the drive 20 and actuating screw 21 from the topmost to the middle position determined by the position sensor 28. As a result, the shutter 8 of the moving frame 9 will expose the light beam proceeding from the position sensor 6 (in the measuring position vis-à-vis the body 1), and cover the light beam proceeding from the position sensor 7 (vis-à-vis the

body 1); the testing end 4 will emerge from the opening in the body and the signal lights surrounding the aperture 19 in the testing end will be switched on. Starting from this moment, the device is ready to perform measurements.

The method applied when using the device comprises the following. To carry out measurement, the testing end 4 is placed on the tissue 30 under investigation, causing a deformation ΔS (Fig.2). Next, the body 1 of the device is moved towards the tissue until the discontinued beam of light from the position sensor 7 (in the measuring position vis-à-vis the body 1 is exposed by the shutter 8, whereas the shutter 8 has not yet covered the light beam proceeding from the sensor 6 (in the measuring position). In the position when the shutter 8 is between the position sensors 6 and 7 and has not yet covered their beam of light, the colour of the light proceeding from the aperture 19 changes, indicating the position of the moving frame 9 in which the elastic plates 10 and 11 are stress-free. Subsequently, impulses of current with a fixed shape, duration and frequency are transmitted to the solenoid 5.

Following each impulse, the soft biological tissue undergoes a dynamic transformation Δl (Fig.2), which ends with a quick release, after which the biological tissue 30, in accordance with its elasticity properties, undergoes a series of free damping co-oscillations along with the testing end 4, the moving frame 9, and the recorder 3. The tissue's natural oscillation is registered by the recorder 3, and the processor will calculate, in real time, the parameters characterising the tissue's mechanical stress and biomechanical properties, as well as the criteria required for assessment.

If during the measuring session the device leaves the space between the sensors 6 and 7 marking the measuring position of the moving frame 9, or if one of the named position sensors' beams is discontinued by the shutter 8, then the control

means 2 of the device will stop the measuring process and the colour of the light will change. The initial colour of the light source will not be restored, unless the position of the moving frame 9 with respect to the sensors 6 and 7 of the measuring position is restored and the measuring session can resume from where it stopped.

After the measuring session has been completed, the arresting system will fix the moving frame 9 in its upper limiting position.

By means of the above device and method the parameters of the biomechanical properties of the state of mechanical stress - elasticity, dynamic stiffness, creepability and mechanical stress relaxation time - were measured in the *Biceps brachii*, *Flexor c.rad.*, *Extensor digitorum* muscles and *Tendo calcanei* simultaneously in real time, after which the data were processed and statistical assessment made.
The named procedures were performed as follows:

Stage A

1) To the testing end of the device (myometer) described above a marker was fastened for marking the area chosen for measurement and for connecting the testing end with the muscle being measured without changing the integrity and function of the biological tissue, i.e., without damaging the tissue, and the testing end was then placed on the surface of the soft tissue to be measured;

2) the device indicated in item 1) was then brought close to the surface being measured until the device's light or sound signal changed;

3) next, irrespectively of the position of the device vis-à-vis the gravitation field, an external influence was exerted on the tissue by the testing end by force equalling the

weight of the testing end mechanism; thus, a static deformation ΔS of the tissue was brought about (Fig. 2);
4)the device was held in the same position (for a prescribed time period) until the light or sound signal changed.

Stage B

An external impact was exerted on soft biological tissue by a single constant electrical impulse of the solenoid, which ended with a quick release, while the elastic element of the device was stress-free. The specific power of the impulse was 0.1 W/mm^2, the quick release lasted 0.1 ms, and the maximum of the impulse was achieved in 3 ms. As a result, the dynamic transformation Δl was caused on the tissue (Fig.2).

Stage C

The mechanical transformation of the tissue was recorded together with the tissue's subsequent mechanical response in the form of a acceleration graph of the tissue's natural oscillation. The recordings were performed a certain prescribed number of times within intervals less than 1 sec (Fig.2).

Stage D

On the basis of the acceleration graph of the tissue's natural oscillation, in real time and simultaneously, the parameters of the measured tissue's mechanical stress, elasticity, dynamic stiffness and mechanical stress relaxation time were calculated, using the time span on the natural oscillations acceleration graph which consisted of the oscillation period starting with the impact and lasting until its end plus subsequent 1.5 periods of the tissue's first natural oscillation.

The natural oscillation diagram, results of measurement and the orientation of the device were stored by means of a computer program in the memory of the device.

The repeated measurements were carried out after min. 1-second intervals for a sufficient number of times for making statistical estimations. The results were displayed on the LCD screen of the recorder.

The acceleration curve obtained by measurements made by the device (myometer) described above (Fig. 2) enabled calculation of the natural oscillation f of the oscillating muscle mass (together with the mass of the testing end), which is expressed as the inverse value of the oscillation period T

$$f = 1/T \text{ [Hz]},$$

dynamic stiffness $C = m_t * a_1 / \Delta l$ [N/m],

where m_t - is the mass of the moving part in kg,

a_1 - acceleration at the time when the testing end is dug deepest in the tissue - m/s^2,

logarithmic decrement

$$\Theta, = \ln(a_1/a_3).$$

Also, it became possible to calculate, in the myometric method described above, the relaxation time t_{rel} of the tissue, which is expressed by the formula

$$t_{rel} = t_2 - t_1..$$

The Deborah number characterising the creepability of the tissue was calculated by the following formula:

$$D_e = \frac{t_2 - t_1}{t_1 - t_T}$$

The results of the measurement are given in Table 1 below.

Table 1. Measurements of the muscle tone and biomechanical properties of a 24-year-old male athlete at rest.

Object	Side of body	Statistics	Frequency Hz	Decre-ment	Dynamic stiffness N/m	Creepabili-ty	Relaxa-tion time ms
Biceps brahii	Right	Average	13.15	1.17	192	1.36	22.65
		Median	13.14	1.18	193	1.36	22.50
		St-deviation	0.23	0.04	7.9	0.06	0.97
		Var.coeff %	1.76	3.60	4.1	4.36	4.27
	Left	Average	12.93	1.13	180	1.33	22.28
		Median	12.99	1.13	180	1.33	22.20
		St-deviation	0.17	0.02	4.0	0.04	0.39
		Var.coeff %	1.32	2.16	2.2	2.73	1.74
Student t-test (<5%)			**YES**	**YES**	**YES**	**YES**	**NO**
Extensor digitorum	Right	Average	15.22	0.81	216	1.01	16.94
		Median	15.28	0.79	218	1.01	16.90
		St-deviation	0.30	0.05	12.7	0.04	0.53
		Var.coeff %	1.98	5.87	5.9	4.09	3.11
	Left	Average	14.24	0.97	192	1.17	19.48
		Median	14.29	0.97	195	1.20	19.70
		St-deviation	0.22	0.02	8.5	0.07	0.74
		Var.coeff %	1.57	2.38	4.4	6.37	3.82
Student t-test (<5%)			**YES**	**YES**	**YES**	**YES**	**YES**
Flexor carpi radialis	Right	Average	15.66	1.35	247	1.05	16.84
		Median	15.69	1.35	247	1.06	16.90
		St-deviation	0.13	0.03	6.1	0.03	0.27
		Var.coeff%	0.83	2.12	2.5	2.43	1.59
	Left	Average	15.80	1.30	253	0.97	15.65
		Median	15.80	1.29	253	0.96	15.60
		St-deviation	0.29	0.06	9.9	0.04	0.53
		Var.coeff %	1.83	4.58	3.9	3.87	3.40
Student t-test (<5%)			**NO**	**YES**	**YES**	**YES**	**YES**
Tendo calcanei	Right	Average	30.32	1.11	605	0.44	6.50
		Median	30.77	1.18	607	0.45	6.60
		St-deviation	0.96	0.13	12.1	0.01	0.15
		Var.coeff %	3.15	11.24	2.0	2.42	2.26
	Left	Average	35.09	1.04	672	0.38	5.59
		Median	35.16	1.03	671	0.38	5.60
		St-deviation	0.41	0.02	12.6	0.01	0.15
		Var.coeff%	1.17	1.93	1.9	3.52	2.74
Student t-test (<5%)			**YES**	**YES**	**YES**	**YES**	**YES**

Due to the small values of standard deviation, the differences between the parameters of the right and left side of the body are statistically significant even in the case of

small values, which shows the great sensitivity and accuracy of the device. The decrement characterising the elasticity of *tendo calcanei* of the left side of the body has 11.24% variation, calling for the need to repeat the measurement and disclose what causes the instability before appearance of pathological symptoms.

Table 2. Statistical indices of the measurements performed on the test body SonarAid130 by the device of the closest prior art and the device corresponding to the invention, (n=30).

Device	Statistical parameter	Frequency Hz	Loga-rithmic decrement	Dynamic stiffness N/m	Creepa-bility	Relaxation time ms
Device of the closest prior art	Average	22.12	0.65	500	--	--
	Mediaan	22.1	0.66	501	--	--
	Standard dev.	0.13	0.02	9	--	--
	Var.coeff%	0.59	3.07	1.8	--	--
Device of the current inven-tion	Average	22.98	0.29	391	0.78	9.81
	Median	23.02	0.29	395	0.78	9.7
	Standard dev.	0.15	0.01	13.28	0.02	0.18
	Var.coeff %	0.64	2.72	3.4	2.78	1.88

By comparing the measurements performed on the test body by means of the prior art and the device corresponding to the current invention it appeared that the decrement was twice as small when measuring by the device corresponding to the invention, which points at the named device's substantially higher sensitivity.

Application of the device corresponding to the invention, the method and the computer program enables one to

- measure simultaneously, in real time, soft biological tissue's mechanical stress and parameters characterising its four biomechanical properties – elasticity, dynamic stiffness, creepability and mechanical stress relaxation time;
- measure and assess the state of stress and biomechanical properties of soft biological tissue with greater accuracy;
- repeat the measuring procedure within small time intervals, as the parameters for impacting on soft biological tissue by means of a single impulse are chosen so that in the course of measurements they will change neither the stress nor biomechanical properties of the tissue under investigation;
- perform measurements at different angles, maintaining the constant pre-pressure when doing so;
- measure following a prescribed algoritm;
- obtain, owing to good repeatability of measurements, within a short period of investigation, a sufficient number of measurements for statistical evaluation and/or comparison of the state of soft biological tissues with reference values;
- obtain standardised criteria of assessment which are released by the firmware immediately after completion of the measurements;
- raise the sensitivity of the device;
- reduce the user's influence on the measurements.

CLAIMS

1. A device for simultaneous measurement of the parameters characterising the mechanical stress, elasticity, dynamic stiffness, creepability and mechanical stress relaxation time of soft biological tissue, comprising the body (1), a means comprising a processor and controller for management the measuring process and calculating the parameters (a control means) (2), a recorder, e.g. an acceleration sensor (3), a testing end (4), a drive of the testing end comprising a solenoid (5), position sensors (6, 7) of a moving frame (9) and a shutter (8) of the position sensors, c h a r a c t e r i s e d in that the drive of the testing end is operable in translational motion and without mechanical friction, and said drive is having the same direction as the testing end, and includes a testing end mechanism comprising a moving frame (9) and elastic elements, e.g. elastic plates (10 and 11) whose one ends are inflexibly fastened to a moving frame (9) and the other ends are inflexibly fastened to a base (13) by means of collet-type coupling (12), whereas the moving frame (9) contains a sleeve (14) with permanent magnets (15, 16) oriented with same-name poles face to face and placed in the centre of a solenoid (5), and testing end (4), whereas the electrical steel cone-shaped tip (17) of testing end (4) is placed in the pull zone of the permanent magnet(16) which is located closer to the testing end, whereas said cone-shaped tip (17) is fixed selfrigidly vis-à-vis the moving frame (9), and said device is equipped with a friction-free element, e.g. a flexible flat cable (18) for direction of the recorder's (3) signals from the moving frame (9) to the control means (2) and the device includes light and/or sound signals, which are placed around the aperture (19) of the testing end (4), as well as an arrester system comprising a drive (20), an actuating screw

(21), a slider (22) moving on an unmoving base (13), whereas the slider (22) is equipped with a shutter (23) and in the slider (22) are located a means (24) for preventing mechanical injuries to the arrester system, and stoppers (25, 26) at the extreme positions of the moving frame together with position sensors (27, 28, and 29).

2. A method for simultaneous measuring, in real time, of the parameters characterising soft biological tissue's mechanical stress, elasticity, dynamic stiffness, creepability and mechanical stress relaxation time, comprising the following stages:

A.on the surface of soft biological tissue under investigation a means is attached for marking the area of the soft biological tissue to be examined and for joining the testing end with the biological tissue with neither damaging the latter's integrity nor changing its functions,

B.the soft biological tissue is externally impacted by a single constant impulse of electric power from the solenoid, which ends with a quick release,

C.the mechanical deformation of the tissue and the tissue's subsequent mechanical response are recorded in the form of a graph, e.g. an acceleration graph, of the tissue's natural oscillation,

D. on the basis of the acceleration graph, the parameters of the tissue's mechanical stress, elasticity and dynamic stiffness are calculated,

c h a r a c t e r i s e d in that the following procedures are performed:

in Stage A

1) either to the testing end of the device described in Claim 1, or to the surface of the tissue a means is attached for marking an area to be investigated and for

joining the testing end with the tissue without either damaging the integrity of the tissue or changing its function, and the testing end is placed on the surface of the soft biological tissue under investigation;

2) the device described in Claim 1 is brought near the surface being measured, in the course of which the device causes, irrespectively of its position, gravitational field and user, a constant external influence (pre-pressure) between the tissue under investigation and the testing end with force equalling the gravity of the mass of mechanism of the testing end, and the pre-pressure is maintained during the stages B-D throughout the whole series of measurements;

3) nearing the device to the tissue is stopped when the light and/or sound signal of the device changes, indicating that the necessary pre-pressure has been achieved and the elastic element is stress-free, i.e. the preconditions for starting a series of measurements have been met;

in stage B
the device described in Claim 1 exerts an external impact on soft biological tissue for a prescribed number of times by means of a single constant electric power impulse from a solenoid, whereas each impact ends with a quick release, and the device is held in the same position throughout the measuring series until a change in the light and/or sound signal indicates the end of the measuring series;

in stage C
the mechanical deformation of the tissue and subsequent mechanical response are recorded in real time in the form of a graph of the tissue's natural oscillations in stage B after each single impulse;

in stage D
are additionally calculated, in real time, the parameters characterising the creepability and mechanical tension relaxation time together with statistical assessments of all the calculated parameters, whereas for calculating the parameters characterising soft biological tissue's mechanical state of stress, elasticity, dynamic stiffness, creepability and mechanical stress relaxation time the time span from the tissue's natural oscillations graph is used which involves the oscillation period from the start until the end of the impact and subsequent 1.5 (one and a half) periods of the tissue's natural oscillation.

3. The method according to Claim 2, wherein at stage B the specific power of a single external mechanical impulse ranks between 0.01 and 0.2 W/mm^2, the quick release lasts between 0.1 and 15 ms, and the time taken to achieve maximum impulse is between 1 and 5 ms.

4. The method according to Claims 2-3, wherein the time interval between performing single measurements of a measuring series does not exceed one (1) second and the measurements are performed as many times as necessary for statistical assessment.

5. A computer program product stored in processor memory of a device and including software code portions, adapted to perform the stages A - D of the method of Claim 2, when the computer program is running in the processor.

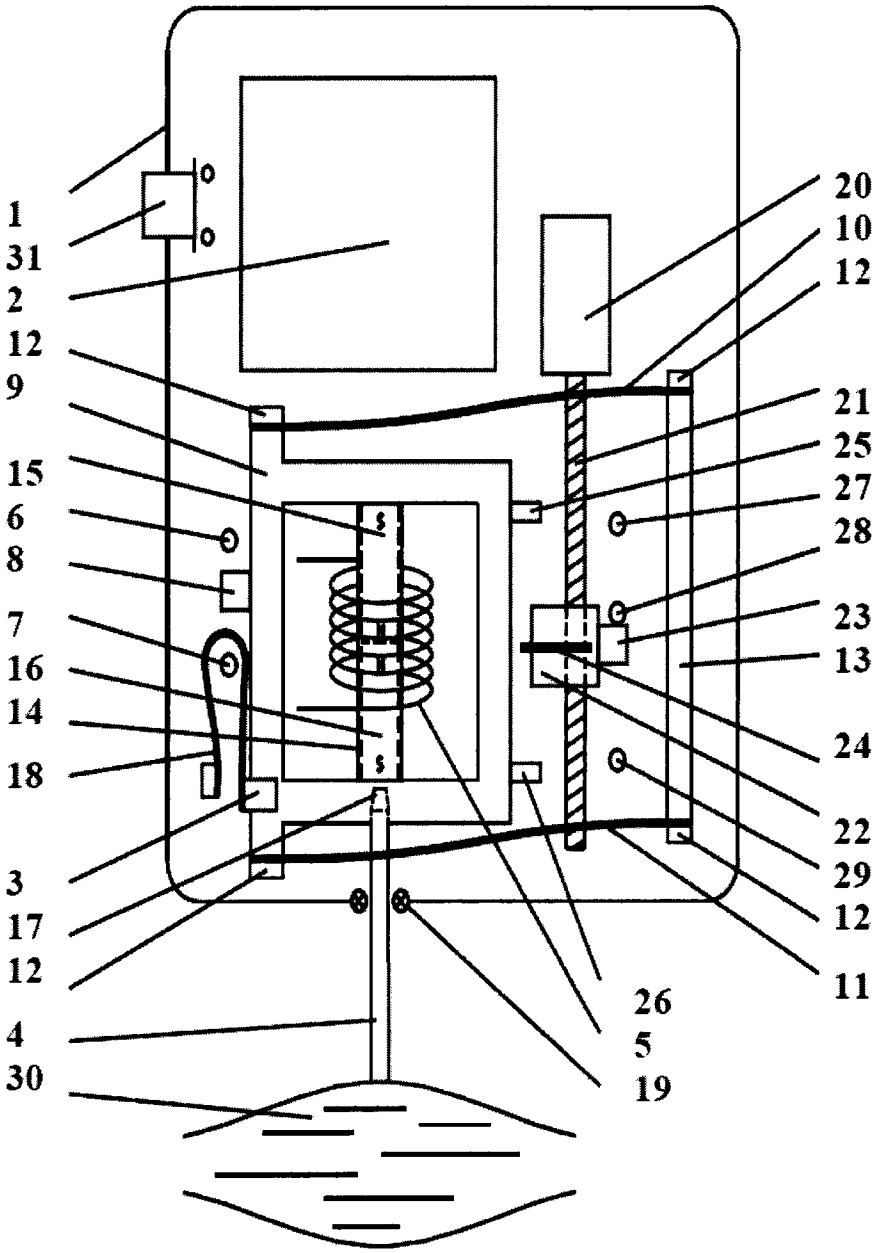
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FIG 1

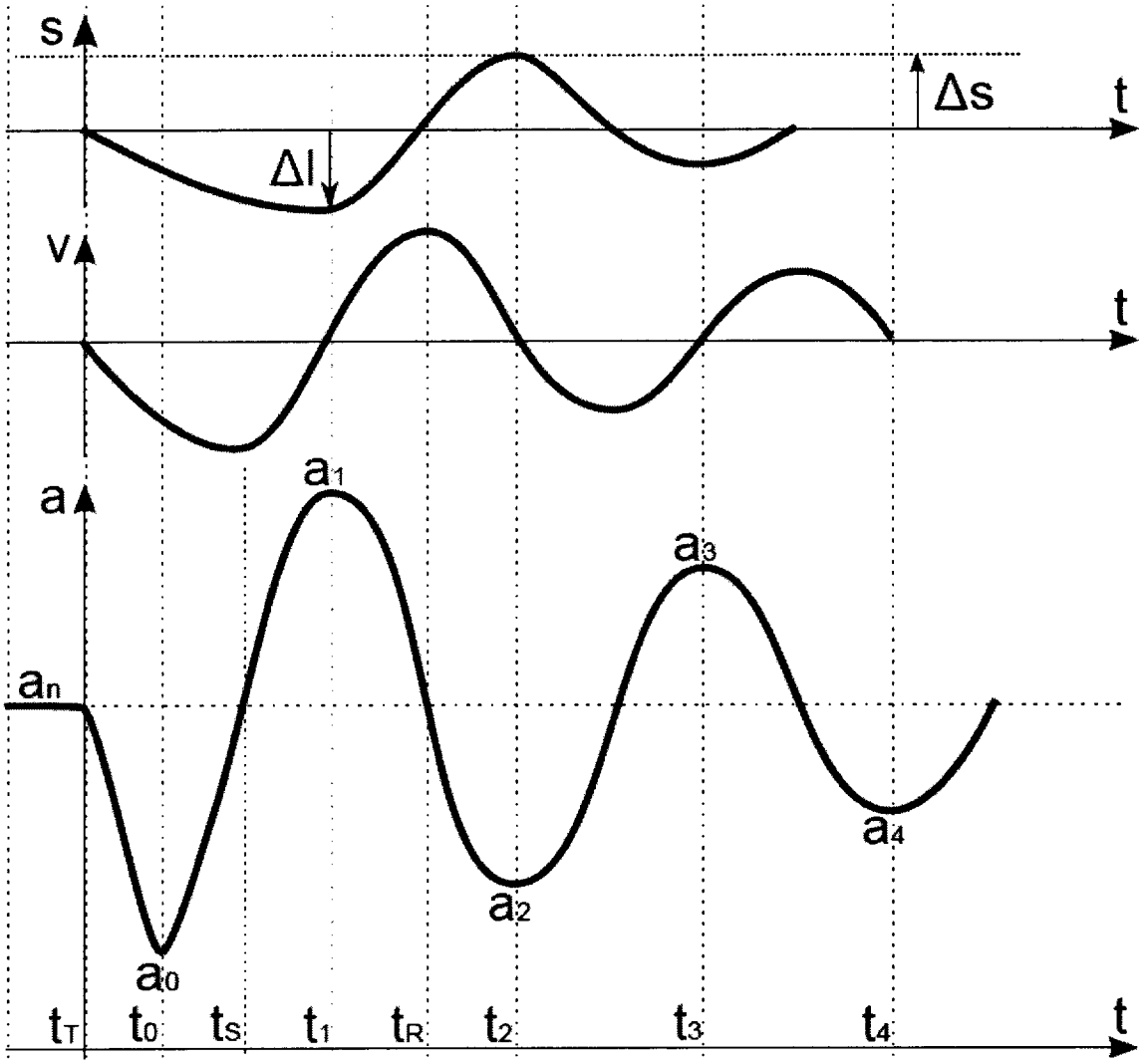

FIG 2

INTERNATIONAL SEARCH REPORT

International application No
PCT/EE2011/000009

A. CLASSIFICATION OF SUBJECT MATTER
INV. A61B5/103 A61B9/00
ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
A61B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)
EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 6 132 385 A (VAIN ARVED [EE]) 17 October 2000 (2000-10-17) cited in the application the whole document	1-5
A	WO 2008/081276 A1 (BG INFORMATICA S R L [IT]; VESPASIANI GIACOMO [IT]) 10 July 2008 (2008-07-10) page 4 - page 8; figures 1-3	1-5
A	US 4 177 798 A (GRAS GILBERT [FR] ET AL) 11 December 1979 (1979-12-11) figure 4 abstract	1-5
A	US 2009/056427 A1 (HANSMA PAUL [US] ET AL) 5 March 2009 (2009-03-05) figure 1 column 4	1-5

☐ Further documents are listed in the continuation of Box C.

☒ See patent family annex.

* Special categories of cited documents :

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"E" earlier document but published on or after the international filing date

"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

"&" document member of the same patent family

Date of the actual completion of the international search	Date of mailing of the international search report
7 November 2011	23/11/2011

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INTERNATIONAL SEARCH REPORT

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PCT/EE2011/000009

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