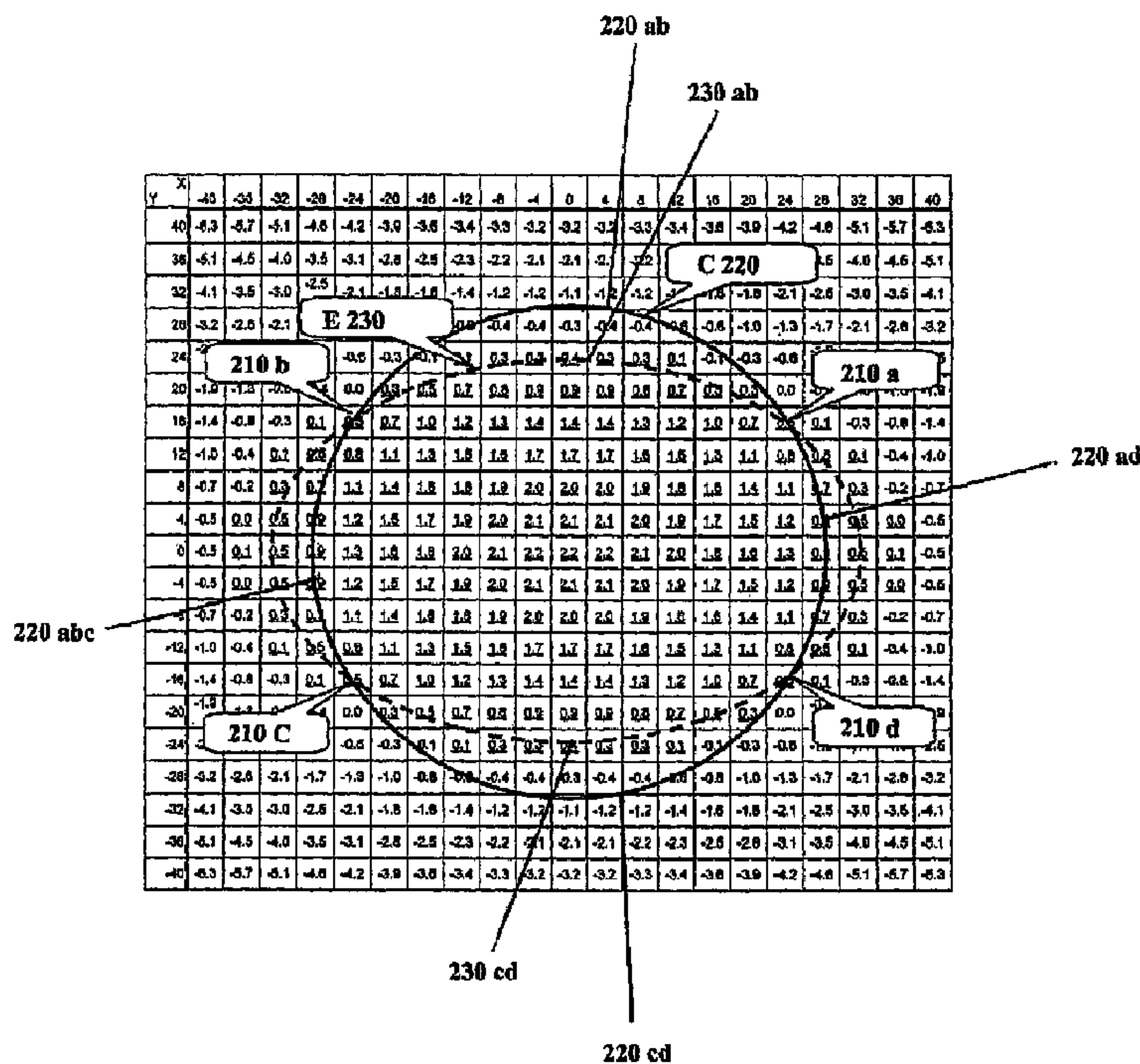




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(54) **Titre : PROCEDE DE FABRICATION DE VERRES DE LUNETTES**
 (54) **Title: PROCESS FOR THE MANUFACTURE OF SPECTACLE LENSES**



(57) **Abrégé/Abstract:**

A method for determining a blunt edge contour B (310) of a spectacle lens comprising the steps of :
 a) determining a minimum edge thickness (16) for an uncut lens;
 b) using the minimum edge thickness (16) to determine a thickness requirement;
 c) calculating a thickness function t of the uncut lens;
 d) calculating a cribbed diameter of the uncut lens;
 e) using the thickness function and cribbed diameter to determine a first set of points (220 ab, 220 cd) that does not satisfy the thickness requirement and a second set of points (220 bc, 220 ad) that satisfies the thickness requirement;
 f) determining a third set of points (230 ab, 230 cd) that describe a diameter contained within the cribbed diameter; and
 g) combining the second set of points with the third set of points to provide the blunt edge contour B (310) for the uncut lens.

ABSTRACT

A method for determining a blunt edge contour B (310) of a spectacle lens comprising the steps of :

- a) determining a minimum edge thickness (16) for an uncut lens;
- b) using the minimum edge thickness (16) to determine a thickness requirement;
- c) calculating a thickness function t of the uncut lens;
- d) calculating a cribbed diameter of the uncut lens;
- e) using the thickness function and cribbed diameter to determine a first set of points (220 ab, 220 cd) that does not satisfy the thickness requirement and a second set of points (220 bc, 220 ad) that satisfies the thickness requirement;
- f) determining a third set of points (230 ab, 230 cd) that describe a diameter contained within the cribbed diameter; and
- g) combining the second set of points with the third set of points to provide the blunt edge contour B (310) for the uncut lens.

PROCESS FOR THE MANUFACTURE OF SPECTACLE LENSES

Field of the Invention

The present invention relates to ophthalmic lenses. In particular, the invention provides a process for the elimination of sharp lens edges in the manufacturing of spectacle lenses.

Background of the Invention

The use of spectacle lenses for the correction of ametropia is well known. Typically, a polymeric article, conventionally known as a lens blank, is manufactured by casting or machining, which blank has a first surface having at least one refractive power. The second surface of the blank is then machined to provide what is known as an "uncut lens", the second surface of which has at least one additional refractive power. Prior to machining of the second surface, the diameter of the blank or uncut lens typically is reduced by cutting to a round shape, which cutting process is known as cribbing.

The machining of the second surface can result in formation of a sharp edge at the periphery of the uncut lens. The sharp edge is disadvantageous in that it is prone to cracking or chipping resulting in one or both of contamination of subsequent cleaning or coating steps of the manufacturing process and an unusable uncut lens. Additionally, the sharp edge makes the uncut harder to handle either manually or by machine. Finally, uncut lenses with sharp edges are more likely to exhibit coating defects and be rejected as unacceptable from a cosmetic basis.

In conventional lens manufacturing processes, any sharp edge that remains after machining is eliminated by hand-filing or grinding of the edge. Alternatively, the periphery of the blank or uncut lens may be cut, or cribbed, to an elliptical shape to eliminate the sharp edge. These methods are disadvantageous in that they either

add labor and, thus, cost to lens production or the sharp edges are not eliminated in all cases.

Summary of Invention

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In one aspect of the invention, a method for manufacturing a spectacle lens comprises using a thickness that is at least a minimum edge thickness, at least one of a plurality of a set of points associated with a thickness function, and at least one of a plurality of a set of points within a cribbed diameter to determine a contour for cutting an uncut lens blank having at least the thickness that is at least a minimum edge thickness.

In some embodiments, the thickness function can be determined using a model of a front and a back surface of the uncut lens to attain an optical prism target and a lens center thickness. In some embodiments, the minimum edge thickness is about 0.1 mm to about 2 mm.

In certain embodiments, the method can further comprising using a prism reference point of the front and back surface and a slope of the front and back surface at the prism reference point to attain the optical prism target and the lens center thickness. The cribbed diameter can be determined using a blocking location, wherein the coordinate system of the blocking location coincides with the coordinate system of the thickness function.

The method can further comprise using at least one of a plurality of a set of points meeting a minimum alloy allowance requirement to determine the contour for cutting the uncut lens blank.

The method can further comprise using at least one of a plurality of a set of points meeting an edging allowance requirement to determine the contour for cutting the uncut lens blank.

A cribbed uncut lens is disclosed comprising a thickness that is at least a minimum edge thickness and an edge contour within a cribbed diameter. In some embodiments, the cribbed uncut lens can have a minimum edge thickness of about 0.1 mm to about 2 mm. The cribbed uncut lens can have an edge contour which

further meets a minimum alloy allowance requirement. The cribbed uncut lens can have an edge contour which further meets an edging allowance requirement.

In another embodiment, the method for manufacturing a spectacle lens comprises the steps of: a.) determining a minimum edge thickness for an uncut lens; b.) using the minimum edge thickness to determine a thickness requirement; c.) calculating a thickness function t of the uncut lens; d.) calculating a cribbed diameter of the uncut lens; e.) using the thickness function and cribbed diameter to determine a first set of points that does not satisfy the thickness requirement and a second set of points that satisfies the thickness requirement; f.) determining a third set of points that describe a diameter contained within the cribbed diameter; and g.) combining the second set of points with the third set of points to provide a blunt edge contour for the uncut lens

The method of calculating a thickness function t of the uncut lens can further comprise (i) using an optical prism target and a lens center thickness and (ii) using a mathematical model of a front and a back surface of the uncut lens in a coordinate system wherein a prism reference point of each surface and a slope of each surface at the prism reference point is such that the optical prism target and center thickness will be attained.

The method of calculating a thickness function t of the uncut lens can further comprise using a blocking location and a crib diameter wherein the coordinate system of the blocking location is coincident with the coordinate system of step c.).

The method for manufacturing a spectacle lens can further comprise a step h.) comprising (i) representing a perimeter of an alloy as a set of points A , (ii) defining an alloy allowance by a set of distances AA wherein $AA = B - A$, and (iii) determining if a minimum alloy allowance has been exceeded.

The method for manufacturing a spectacle lens can further comprise a step i.) comprising (i) representing a final edged periphery of the lens as a set of points F , (ii) defining an edging allowance by a set of distances EA wherein $EA = B - F$, and (iii) determining if a minimum edging allowance has been exceeded.

The invention also relates to the production of a lens according to a method comprising using a thickness that is at least a minimum edge thickness, at least one of a plurality of a set of points associated with a thickness function, and at least one of a plurality of a set of points within a cribbed diameter to determine a contour for cutting an uncut lens blank having at least the thickness that is at least a minimum edge thickness. The lens may also be produced according to a method further comprising a thickness function is determined using a model of a front and a back surface of the uncut lens to attain an optical prism target and a lens center thickness.

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Brief Description of the Drawing

Figure 1 depicts a cross-sectional view of a lens.

Figure 2 depicts a grid of lens thickness values at their respective X and Y coordinate positions.

Figure 3 depicts the graph of Figure 1 overlaid by two sets of contours, C and E, and points a, b, c, and d at which C and E intersect.

Figure 4 depicts the graph of Figure 1 overlaid by a blunt edge contour B resulting from Equation IV.

20

Detailed Description

Referring to Figure 1, in one embodiment, a method for manufacturing a spectacle lens 10 includes: a.) determining a minimum edge thickness 16 for an uncut lens; b.) using the minimum edge thickness 16 to determine a thickness requirement; c.) calculating a thickness function t for the uncut lens; d.) determining a cribbed diameter function for the uncut lens; e.) using the thickness function and cribbed diameter to determine a first set of points that does not satisfy the thickness requirement and a second set of points that satisfies the thickness requirement; f.) determining a third set of points that describe a contour contained within the cribbed

diameter; and g.) combining the second set of points with the third set of points to provide a blunt edge contour for the uncut lens.

The present invention provides methods, and lenses produced by those
5 methods, for eliminating sharp edges that typically result during the production of uncut lenses. The methods of the invention may be used to produce any type of spectacle lens, such as single vision and multifocal lenses.

Referring again to Figure 1, a "lens blank" or "blank" 10 means a shaped,
10 optically transparent article capable of refracting light that is suitable for use in producing a spectacle lens, one surface of which blank provides at least one refractive power. Typically, the lens blank has a front surface 12 that is nearest the object being viewed through a worn lens in which the blank is used and a back surface 14, which is the surface that is nearest the wearer's eye. The first refractive
15 power may be all, or a portion, of the distance vision, near vision, intermediate vision, or cylinder power desired for the finished lens, or a combination thereof.

The lens blank production may be carried out by any convenient manner such as by casting, thermoforming, molding, machining, or a combination thereof.
20 Materials suitable for use in forming the blank are any materials capable of use as a spectacle lens material. Illustrative materials include, without limitation, polycarbonates, such as bisphenol A polycarbonates, allyl diglycol carbonates, such as diethylene glycol bisallyl carbonate (CR-39™), allylic esters, such as triallyl cyanurate, triallyl phosphate and triallyl citrate, acrylic esters, acrylates,
25 methacrylates, such as methyl- ethyl- and butyl methacrylates and acrylates, styrenics, polyesters, and the like and combinations thereof. Additionally, the lens blank 10 may be formed from one or more of the phosphine oxides disclosed in U.S. Patent No. 6,008,299.

30 In a first step of the method, a minimum edge thickness 16, ET_{min} , is determined. The minimum edge thickness 16 is the desired minimum edge

thickness 16 for the uncut lens to be produced from the lens blank. The edge thickness 18 is the thickness between the front and back surfaces of the uncut lens at the lens perimeter or the farthest point from the geometric center of the lens at any given angular position. The ET_{min} will be determined based on a consideration of the minimum edge thickness 16 at which there will be no cracks or chips, that will facilitate handling, and that will alleviate formation of coating defects. Preferably, the ET_{min} value will be about 0.1 mm to about 2 mm. The ET_{min} is also used to establish a thickness requirement for the uncut lens, which requirement is $t \geq ET_{min}$.

Referring to Figure 2, the thickness 18, t , of the uncut lens is then calculated as a function of two-dimensional coordinates on the uncut lens. The coordinates calculated may be polar ($t = f(r, \theta)$), Cartesian ($t = f(x, y)$), or any convenient coordinates system. This calculation may be carried out by any convenient method. Preferably, the calculation is carried out by using the optical prism target and lens center thickness 20 targets, obtained using commercially available optical laboratory management software such as VISION™ software by Digital Vision, Inc., OPTIFACTS™ software by Optifacts, Inc, LABZILLA™ software by C.C. Systems, or the like. A mathematical model of the front and back surfaces of the lens may then be used in which the coordinate system of each surface is coincident with the prism reference point (“PRP”) of each surface and in which the slope of each surface at the PRP is such that the desired optical prism will be achieved. For example, $Frt(x, y)$ and $Bck(x, y)$ may represent the front and back surface models, respectively, in Cartesian coordinates and can be used to define the thickness function as:

$$t(x, y) = Bck(x, y) - Frt(x, y) + Dto \quad (I)$$

wherein Dto is the desired center thickness 20 for the uncut lens.

Figure 2 is a chart, calculated using Equation 1, showing lens thickness values at their respective x and y coordinate positions.

The cribbed diameter, C_{diam} , of the uncut lens may then be calculated as a
 5 function of two-dimensional coordinates on the uncut lens. The coordinates may be polar, Cartesian, or any convenient coordinate system. The calculation may be carried out by any convenient method and preferably is carried out using the blocking location and crib diameter obtained from commercially available lab management software and in which the coordinate system of the blocking location
 10 and crib diameter are coincident with the PRP of the lens. For example, $(X_{\text{BL}}, Y_{\text{BL}})$ may represent the blocking location, in Cartesian coordinates and can be used to define the cribbed diameter functions as:

$$C_{\text{diam}} = 2 * ((X - X_{\text{BL}})^2 + (Y - Y_{\text{BL}})^2)^{0.5} \quad \text{(II)}$$

The thickness function t and cribbed diameter function C_{diam} are then used to determine a first set of points $C^{[-]}$ existing on the continuous contour C 220 of the
 20 cribbed diameter that describe a portion of, or all of the cribbed diameter, at which the thickness does not satisfy the thickness requirement or, in other words, at which $t < ET_{\text{min}}$, such as C_{ab} 220ab and C_{cd} 220cd as shown on Figure 3. As shown on Figure 3, a, b, c, and d 210a-d are points at which contour C 220 intersect with contour E 230. Contour E 230 is the contour at which $t = ET_{\text{min}}$. One ordinarily skilled in the art will realize that, if a set of points $C^{[-]}$ does not exist and the
 25 thickness requirement is satisfied, no additional calculations are necessary.

In the case in which the thickness requirement is not satisfied, the thickness function t and cribbed diameter function C_{diam} are used to determine a second set of
 30 points $C^{[+]}$ on C 220 that describe the portion of the cribbed diameter at which the thickness t does satisfy the thickness requirement, or $t \geq ET_{\text{min}}$. The set of points $C^{[+]}$ will remain with the desired blunt edge profile for the uncut lens, such as C_{bc}

220bc and C_{ad} 220ad shown in the example used in Figure 3. The mathematical union of the sets of points $C^{[-]}$ and $C^{[+]}$ represents C 220 where:

$$C = C^{[-]} \cup C^{[+]} \quad (III)$$

For Figure 3, $C^{[-]} = (C_{ab} \cup C_{cd})$ and $C^{[+]} = (C_{bc} \cup C_{da})$

In the next step of the methods, the thickness function t , contour E 230 and the cribbed diameter contour C 220 are used to determine a third set of points $E^{[+]}$ on E 230 contained within the contour C 220, such as E_{ab} 230ab and E_{cd} 230cd shown in the example used in Figure 3.

The sets of points $E^{[+]}$ and $C^{[+]}$ may then be combined to provide a continuous, composite, blunt edge contour B 310, as shown in Figure 4, where:

$$B = E^{[+]} \cup C^{[+]} \quad (IV)$$

For Figure 4, $E^{[+]} = (E_{ab} \cup E_{cd})$. Once the blunt edge contour is determined, either the blank or uncut lens is cut to contour B310 using any commercially available and convenient machine capable of performing non-round perimeter cutting, such as a computer-numerically controlled ("CNC") lens surfacing machine. Cribbing the lens with contour B 310 will result in a blunt edge on the entire perimeter of the uncut lens.

In an optional, but preferred step, the impact of forming the blunt edge contour can be weighed against one manufacturing constraint as follows. A circular disk of bonding alloy is commonly formed between the lens blank and a holding

block to attach the lens blank to the holding block prior to cribbing, cutting, or surfacing. The size of the alloy can be any one of a variety of diameters. The alloy is an expensive, low melting point, heavy metal. It is desirable to maintain greater than a minimum amount of lens material, or minimum alloy allowance, AA_{\min} ,
5 between the uncut lens perimeter, represented by the blunt edge contour B 310, and the alloy perimeter such that alloy cutting is avoided. The contour representing the perimeter of the alloy can be represented as a set of points A and the alloy allowance can be defined by a set of distances, AA, where:

10

$$AA = B - A$$

(V)

15 Equation V may be used to determine if the AA_{\min} has been exceeded, $AA < AA_{\min}$. If so, adjustments can be made to one or more of the alloy diameter, the blocking location, and the targeted lens center thickness 20 and then a new iteration of the above steps can be performed.

20 Yet another optional step is directed to lens edging. Uncut lenses must be removed from the alloy holding block and then be cut to the shape of the spectacle frame or rimless pattern. It is typically desirable to allow a minimum amount of material, EA_{\min} , between the uncut lens perimeter and the frame or rimless contour to account for processing variability and ensure the edged lens will completely fill
25 the spectacle frame or rimless pattern. The contour representing the final edged lens periphery can be represented as a set of points, F, and the edging allowance can be defined by a set of distances, EA, where:

$$EA = B - F$$

30

(VI)

Equation (VI) may be used to determine if the EA_{\min} has been exceeded, $EA < EA_{\min}$. In the case that it is exceeded, adjustments can be made to one or more of the cribbed diameter size, the cribbed diameter location, or the targeted lens center thickness 20 and then a new iteration of the steps of the method.

- 5 The scope of the claims should not be limited by the preferred embodiments set forth in the examples, but should be given the broadest interpretation consistent with the description as a whole

CLAIMS

1. A method for manufacturing a spectacle lens comprising cutting an uncut lens blank following a blunt edge contour determined by using a method for determining a blunt edge contour B (310) of a spectacle lens comprising the steps of :

- a) determining a minimum edge thickness (16) for an uncut lens;
- b) using the minimum edge thickness (16) to determine a thickness requirement;
- c) calculating a thickness function t of the uncut lens;
- d) calculating a cribbed diameter of the uncut lens;
- e) using the thickness function and cribbed diameter to determine a first set of points (220 ab, 220 cd) that does not satisfy the thickness requirement and a second set of points (220 bc, 220 ad) that satisfies the thickness requirement;
- f) determining a third set of points (230 ab, 230 cd) that describe a diameter contained within the cribbed diameter; and
- g) combining the second set of points with the third set of points to provide the blunt edge contour B (310) for the uncut lens.

2. The method of claim 1, wherein step c) further comprises (i) using an optical prism target and a lens center thickness (20) and (ii) using a mathematical model of a front (12) and a back (14) surface of the uncut lens in a coordinate system wherein a prism reference point of each surface and a slope of each surface at the prism reference point is such that the optical prism target and center thickness (20) will be attained.

3. The method of claim 2, wherein step d) further comprises using a blocking location and a crib diameter wherein the coordinate system of the blocking location is coincident with the coordinate system of step c) .

4. The method of claim 1, further comprising step h) comprising (i) representing a perimeter of an alloy as a set of points A, (ii) defining an alloy allowance by a set of distances AA wherein $AA = B - A$, and (iii) determining if a minimum alloy allowance has been exceeded.

5. The method of claim 4, further comprising step i) comprising (i) representing a final edged periphery of the lens as a set of points F, (ii) defining an

edging allowance by a set of distances EA wherein $EA = B - F$, and (iii) determining if a minimum edging allowance has been exceeded.

6. The method of claim 1 wherein the minimum edge thickness (16) is about 0.1 mm to about 2 mm.

7. A computer program product comprising one or more stored sequences of instructions that are accessible to a processor and which, when executed by the processor, cause the processor to carry out the steps of the method for determining a blunt edge contour of a spectacle lens according to any one of claims 1 to 6.

8. A computer-readable medium carrying one or more sequences of computer-executable instructions of the computer program product of claim 7.

Figure 1

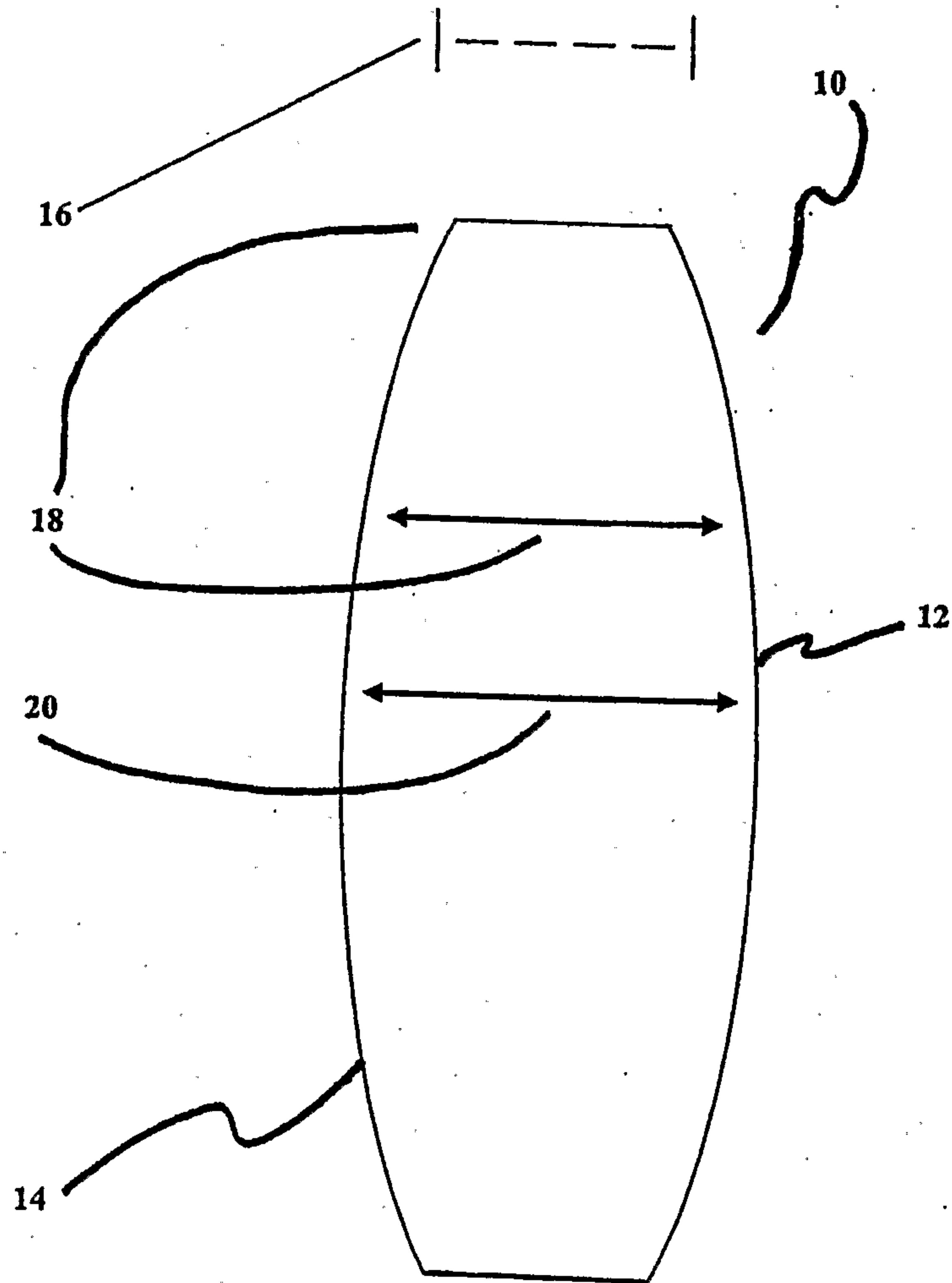


Figure 2

Y \ X	-40	-36	-32	-28	-24	-20	-16	-12	-8	-4	0	4	8	12	16	20	24	28	32	36	40
40	-5.3	-5.7	-5.1	-4.6	-4.2	-3.9	-3.6	-3.4	-3.3	-3.2	-3.2	-3.2	-3.3	-3.4	-3.6	-3.9	-4.2	-4.6	-5.1	-5.7	-6.3
36	-5.1	-4.6	-4.0	-3.5	-3.1	-2.8	-2.5	-2.3	-2.2	-2.1	-2.1	-2.1	-2.2	-2.3	-2.5	-2.8	-3.1	-3.5	-4.0	-4.5	-5.1
32	-4.1	-3.6	-3.0	-2.5	-2.1	-1.8	-1.6	-1.4	-1.2	-1.2	-1.1	-1.2	-1.2	-1.4	-1.6	-1.8	-2.1	-2.5	-3.0	-3.5	-4.1
28	-3.2	-2.6	-2.1	-1.7	-1.3	-1.0	-0.8	-0.6	-0.4	-0.4	-0.3	-0.4	-0.4	-0.6	-0.8	-1.0	-1.3	-1.7	-2.1	-2.6	-3.2
24	-2.5	-1.9	-1.4	-1.0	-0.6	-0.3	-0.1	0.1	0.3	0.3	0.4	0.3	0.3	0.1	-0.1	-0.3	-0.6	-1.0	-1.4	-1.9	-2.5
20	-1.9	-1.3	-0.8	-0.4	0.0	0.3	0.5	0.7	0.8	0.9	0.9	0.9	0.8	0.7	0.5	0.3	0.0	-0.4	-0.8	-1.3	-1.9
16	-1.4	-0.8	-0.3	0.1	0.5	0.7	1.0	1.2	1.3	1.4	1.4	1.4	1.3	1.2	1.0	0.7	0.5	0.1	-0.3	-0.8	-1.4
12	-1.0	-0.4	0.1	0.5	0.8	1.1	1.3	1.5	1.6	1.7	1.7	1.7	1.6	1.5	1.3	1.1	0.8	0.5	0.1	-0.4	-1.0
8	-0.7	-0.2	0.3	0.7	1.1	1.4	1.6	1.8	1.9	2.0	2.0	2.0	1.9	1.8	1.6	1.4	1.1	0.7	0.3	-0.2	-0.7
4	-0.5	0.0	0.5	0.9	1.2	1.5	1.7	1.9	2.0	2.1	2.1	2.1	2.0	1.9	1.7	1.5	1.2	0.9	0.5	0.0	-0.5
0	-0.5	0.1	0.5	0.9	1.3	1.6	1.8	2.0	2.1	2.2	2.2	2.2	2.1	2.0	1.8	1.6	1.3	0.9	0.5	0.1	-0.5
-4	-0.5	0.0	0.5	0.9	1.2	1.5	1.7	1.9	2.0	2.1	2.1	2.1	2.0	1.9	1.7	1.5	1.2	0.9	0.5	0.0	-0.5
-8	-0.7	-0.2	0.3	0.7	1.1	1.4	1.6	1.8	1.9	2.0	2.0	2.0	1.9	1.8	1.6	1.4	1.1	0.7	0.3	-0.2	-0.7
-12	-1.0	-0.4	0.1	0.5	0.8	1.1	1.3	1.5	1.6	1.7	1.7	1.7	1.6	1.5	1.3	1.1	0.8	0.5	0.1	-0.4	-1.0
-16	-1.4	-0.8	-0.3	0.1	0.5	0.7	1.0	1.2	1.3	1.4	1.4	1.4	1.3	1.2	1.0	0.7	0.5	0.1	-0.3	-0.8	-1.4
-20	-1.9	-1.3	-0.8	-0.4	0.0	0.3	0.5	0.7	0.8	0.9	0.9	0.9	0.8	0.7	0.5	0.3	0.0	-0.4	-0.8	-1.3	-1.9
-24	-2.5	-1.9	-1.4	-1.0	-0.6	-0.3	-0.1	0.1	0.3	0.3	0.4	0.3	0.3	0.1	-0.1	-0.3	-0.6	-1.0	-1.4	-1.9	-2.5
-28	-3.2	-2.6	-2.1	-1.7	-1.3	-1.0	-0.8	-0.6	-0.4	-0.4	-0.3	-0.4	-0.4	-0.6	-0.8	-1.0	-1.3	-1.7	-2.1	-2.6	-3.2
-32	-4.1	-3.5	-3.0	-2.5	-2.1	-1.8	-1.6	-1.4	-1.2	-1.2	-1.1	-1.2	-1.2	-1.4	-1.6	-1.8	-2.1	-2.5	-3.0	-3.5	-4.1
-36	-5.1	-4.5	-4.0	-3.5	-3.1	-2.8	-2.5	-2.3	-2.2	-2.1	-2.1	-2.1	-2.2	-2.3	-2.5	-2.8	-3.1	-3.5	-4.0	-4.5	-5.1
-40	-5.3	-5.7	-5.1	-4.6	-4.2	-3.9	-3.6	-3.4	-3.3	-3.2	-3.2	-3.2	-3.3	-3.4	-3.6	-3.9	-4.2	-4.6	-5.1	-5.7	-6.3

100

Figure 3

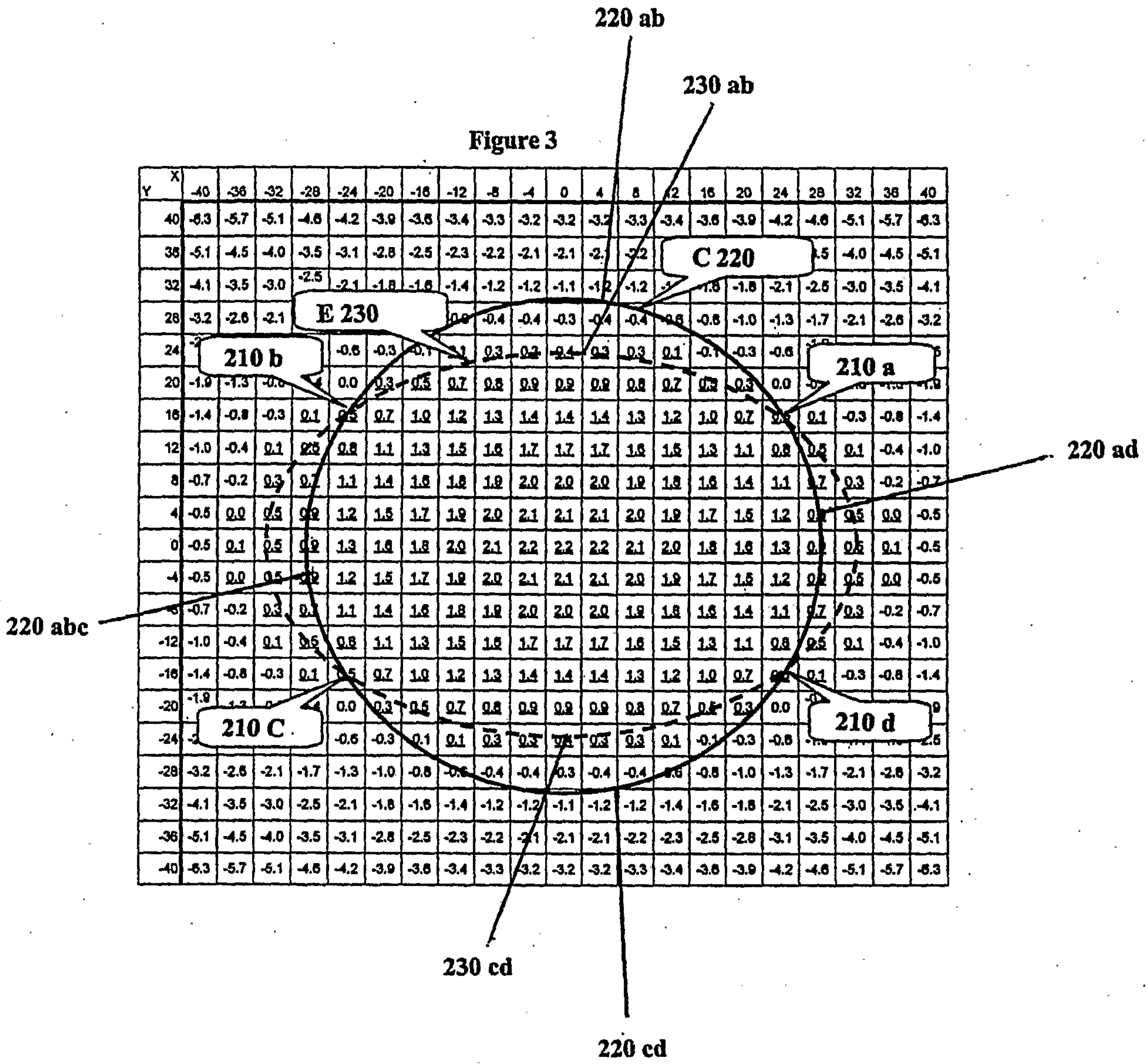
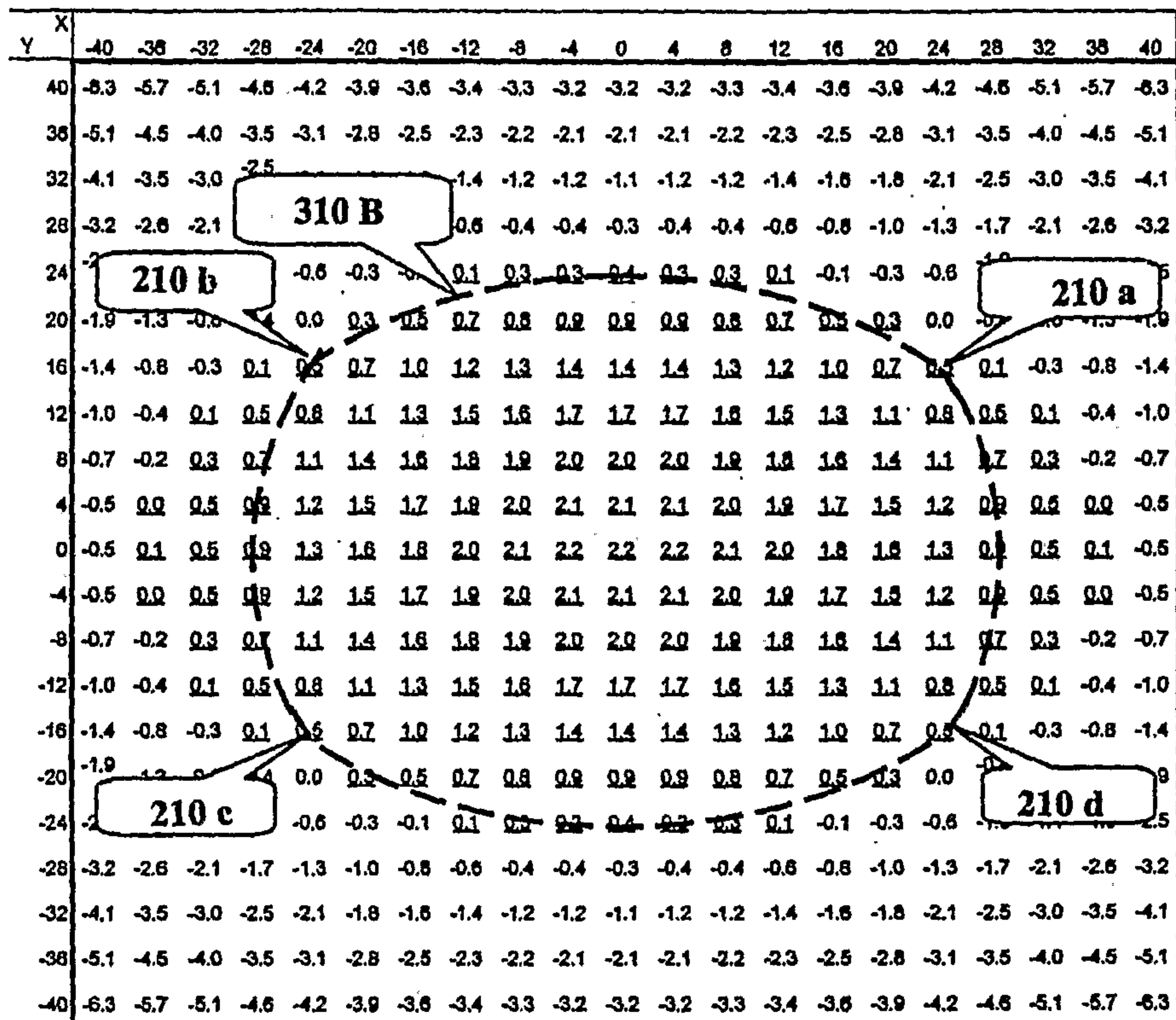


Figure 4



220 ab

230 ab

Y \ X	-40	-36	-32	-28	-24	-20	-16	-12	-8	-4	0	4	8	12	16	20	24	28	32	36	40	
40	-6.3	-6.7	-5.1	-4.6	-4.2	-3.9	-3.6	-3.4	-3.3	-3.2	-3.2	-3.2	-3.2	-3.3	-3.4	-3.6	-3.9	-4.2	-4.6	-5.1	-5.7	-6.3
36	-5.1	-4.5	-4.0	-3.5	-3.1	-2.8	-2.5	-2.3	-2.2	-2.1	-2.1	-2.1	-2.1	-2.2	-2.3	-2.5	-2.8	-3.1	-3.5	-4.0	-4.5	-5.1
32	-4.1	-3.5	-3.0	-2.5	-2.1	-1.8	-1.6	-1.4	-1.2	-1.2	-1.1	-1.2	-1.2	-1.2	-1.3	-1.5	-1.8	-2.1	-2.5	-3.0	-3.5	-4.1
28	-3.2	-2.6	-2.1	-1.6	-1.2	-0.9	-0.7	-0.6	-0.4	-0.4	-0.3	-0.4	-0.4	-0.4	-0.5	-0.6	-0.8	-1.0	-1.3	-1.7	-2.1	-2.6
24	-2.3	-1.7	-1.2	-0.7	-0.3	0.0	0.1	0.1	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.2	0.1	0.0	-0.2	-0.5	-1.0
20	-1.4	-0.8	-0.3	0.1	0.4	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5	0.5
16	-0.5	0.0	0.5	0.9	1.2	1.4	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5	1.5
12	0.4	0.9	1.3	1.6	1.8	1.9	1.9	1.9	1.9	1.9	1.9	1.9	1.9	1.9	1.9	1.9	1.9	1.9	1.9	1.9	1.9	1.9
8	1.3	1.8	2.2	2.5	2.7	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8	2.8
4	2.2	2.7	3.1	3.4	3.6	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7	3.7
0	3.1	3.6	4.0	4.3	4.5	4.6	4.6	4.6	4.6	4.6	4.6	4.6	4.6	4.6	4.6	4.6	4.6	4.6	4.6	4.6	4.6	4.6
-4	4.0	4.5	4.9	5.2	5.4	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5	5.5
-8	4.9	5.4	5.8	6.1	6.3	6.4	6.4	6.4	6.4	6.4	6.4	6.4	6.4	6.4	6.4	6.4	6.4	6.4	6.4	6.4	6.4	6.4
-12	5.8	6.3	6.7	7.0	7.2	7.3	7.3	7.3	7.3	7.3	7.3	7.3	7.3	7.3	7.3	7.3	7.3	7.3	7.3	7.3	7.3	7.3
-16	6.7	7.2	7.6	7.9	8.1	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2	8.2
-20	7.6	8.1	8.5	8.8	9.0	9.1	9.1	9.1	9.1	9.1	9.1	9.1	9.1	9.1	9.1	9.1	9.1	9.1	9.1	9.1	9.1	9.1
-24	8.5	9.0	9.4	9.7	9.9	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
-28	9.4	9.9	10.3	10.6	10.8	10.9	10.9	10.9	10.9	10.9	10.9	10.9	10.9	10.9	10.9	10.9	10.9	10.9	10.9	10.9	10.9	10.9
-32	10.3	10.8	11.2	11.5	11.7	11.8	11.8	11.8	11.8	11.8	11.8	11.8	11.8	11.8	11.8	11.8	11.8	11.8	11.8	11.8	11.8	11.8
-36	11.2	11.7	12.1	12.4	12.6	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7
-40	12.1	12.6	13.0	13.3	13.5	13.6	13.6	13.6	13.6	13.6	13.6	13.6	13.6	13.6	13.6	13.6	13.6	13.6	13.6	13.6	13.6	13.6

C 220

E 230

210 b

210 a

220 ad

220 abc

210 c

210 d

230 cd

220 cd