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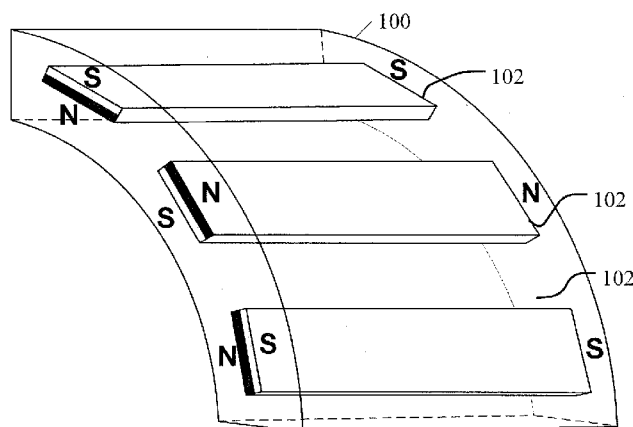


FIG. 1A

(57) Abstract: A permanent magnet machine with a hybrid cage and methods for operating same are disclosed. According to one aspect, the subject matter described herein includes a rotor and hybrid cage for an electrical machine, the rotor comprising a rotor body having a central axis and including a plurality of permanent magnets positioned to create a plurality of rotor magnetic poles distributed around a peripheral surface of the rotor. The rotor also includes a hybrid cage that includes conductive loops around each of the rotor magnetic poles, where the conductive loops are controllable to form a closed circuit or an open circuit around each of the rotor magnetic poles. A closed circuit may be created when a magnetic field having a field strength or change of field strength that exceeds a threshold magnitude is present, such as during a fault condition, and an open circuit may be created when a magnetic field having a field strength or change of field strength that exceeds a threshold magnitude is not present, such as during normal operation.



DESCRIPTION

PERMANENT MAGNET MACHINE WITH HYBRID CAGE AND METHODS
FOR OPERATING SAME

PRIORITY CLAIM

This application claims the benefit of U.S. Provisional Patent
5 Application Serial No. 61/737,724 filed December 14, 2012; the disclosure of
which is incorporated herein by reference in its entirety.

TECHNICAL FIELD

The subject matter described herein relates to permanent magnet
10 machines. More particularly, the subject matter described herein relates to
permanent magnet machines having a hybrid cage and methods for
operating same.

BACKGROUND

15 Brushless permanent magnet (PM) machines use a rotor in which
permanent magnets are embedded, arranged so that multiple magnetic
poles project from the rotor radially, axially or transversely. The stator
contains electromagnets which generate magnetic poles that move around
the perimeter of the stator. The attraction and repulsion of the moving poles
20 created by the current through the stator windings to the magnetic poles
created by the PMs embedded within the rotor create torque.

Induction motors, on the other hand, don't include magnets on the
rotor but instead include loops of conductors, e.g., "coils". In the presence of
the moving poles created by flux created by current through the stator
25 windings, the changing magnetic flux generated by the stator windings
induce currents in the conducting loops, which gives rise to opposing
magnetic fields. The attraction and repulsion between the moving stator
fields and the magnetic fields induced on the rotor coils create torque.
Because the topology of the loops of coils located around the rotor
30 resembles a squirrel cage in common construction, the conductive structure
is commonly referred to as a "cage".

Some machines use permanent magnets on the rotor but also include a cage structure to provide additional torque at start-up. For example, these machines may be called line start permanent magnet machines. Also, field wound synchronous machines commonly have loops of conductive material that circumscribe and surround the poles of the rotor, to aid startup of the machine, as well as dampen transient behavior on the machine and electrical network. The additional magnetic fields produced by the cage(s) is(are) proportional to the current in the cage loops, which is proportional to the change of flux imposed on the cage loop. When there is large relative difference in speed between rotor and stator fields, the change in magnetic flux seen by a cage loop is relatively high, which induces a relatively large current and produces a relatively large opposing magnetic pole. The stronger magnetic attraction and repulsion that is created between the magnetic poles of the rotor and the magnetic poles of the stator manifests itself as additional torque. The resultant torque tends to force the rotor and stator to synchronize in speed. As the relative speed between rotor and stator decreases, the current induced in the cage loops becomes smaller, as does the additional magnetic flux contributed by the cage. If the speed of the rotor is synchronous to that of the fields created by the stator windings, the current in the cage(s) becomes zero, and the cage stops providing the benefit of additional magnetic flux, as well as torque that would restore synchronism between stator and rotor. At this point, the rotor is operating using only the attraction and repulsion between the PMs on the rotor and the moving poles created by the stator windings.

While a wound field synchronous machine may be directly connected the power network without an intermediate power electronic converter, a PM machine without a cage requires a power electronic converter. This power electronic converter acts as a medium between the fixed amplitude and frequency of the power network and that of the voltage amplitude and frequency of the synchronous machine being driven, so that the mechanical system being driven by the motor or generator may be controlled in an effective manner. (The control of the field current in the wound field

synchronous machine allows control of the amplitude of the stator voltage, the permanent magnet machine does not allow this type of control.)

A drawback of the power electronic converter is that there tends to exist variations in the current waveforms between the converter and machine being driven. These variations in the current waveforms will no longer allow the poles of the stator and of the rotor to rotate in a synchronous manner. These variations in current are often called time harmonics, and will create losses and torque pulsations in the machine. The torque pulsations may be reduced by providing the rotor pole with a conducting cage. While the conductive cage acts to dampen torque pulsations, the resultant currents which create the damping torques in the cages create losses, which are not preferred under normal operation.

Due to these losses, cages are not preferred in PM machines, as the magnets are quite sensitive to the temperature rise from the losses. The magnets are selected based on temperature and field requirements. Magnets that are capable of operating at higher temperatures and lower fields are more expensive, and have lower remanence, due to the inclusion of Dysprosium, in particular. In this way, it is preferred to have a rotor that is cooler or protects the magnets from low field levels. The low field levels are not usually a difficulty when under normal operation, but become limiting when a transient event occurs, such as a short circuit.

There are a number of advantages to having a combination of permanent magnet and cage. For example, a cage can moderate the effects of sudden changes of magnetic flux, i.e., flux linkage, and thus can smooth changes in rotor speed, dampen the effects of ripple currents in the stator windings, etc. For line-start synchronous machines, the cage provides additional torque during startup. There are disadvantages to having a cage, as well. The presence of a cage induces a loss that reduces the efficiency of a PM machine and results in non-trivial rotor heating. Because of this, brushless PM machines typically do not include a cage of any kind.

Figure 1A is a section of a rotor of a conventional permanent magnet electrical machine without a protective cage. Rotor **100** contains permanent magnets **102** embedded within the rotor body to create a pattern of

alternating north (N) and south (S) magnetic poles around the outer diameter of the rotor. In the conventional rotor **100** shown in Figure 1A, the magnets are positioned so that the magnetic field produced by each magnet has a vector that is normal to the outer surface of rotor **100**.

5 Figure 1B is a section of another rotor of a conventional permanent magnet electrical machine without a protective cage. In the conventional rotor **100** shown in Figure 1B, permanent magnets **102** are arranged in pairs to produce a pattern of alternating north (N) and south (S) magnetic poles around the outer diameter of the rotor. Each pair of magnets is arranged in
10 a V shape such that the magnetic field produced by each pair has a vector that is normal to the outer surface of rotor **100**.

Because neither of the conventional rotors shown in Figures 1A and 1B include a conducting cage structure, the permanent magnets contained within these conventional rotors are susceptible to damage in response to
15 being subjected to low magnetic flux density in the magnetized direction, such as may occur during startup conditions or during fault conditions. However, a large change in magnetic flux induces voltage in and around the rotor, which when constructed with conductive elements, allow significant currents to flow, which act to create a countervailing magnetic flux and thus
20 protect the permanent magnet from being demagnetized. The eddy currents within the body of the magnet tend to be smaller than the eddy currents at the periphery of the magnet, and due to geometry and magnetic fringing, the countervailing magnetic flux within the body of the magnet tends to be larger than the countervailing magnetic flux at the periphery of the magnet. As a
25 result, the periphery of the magnet has less protection than the rest of the magnet body, and thus the edges of the magnet tend to suffer more demagnetization than is suffered by the core of the magnet. A coupled effect is that the eddy currents create significant additional losses, and within the short circuit time frame, this energy does not propagate throughout the
30 magnet, so the periphery of the magnet exhibits significant temperature rise.

Figure 2A is a cross section of a rotor **100** having magnets **102** arranged in a V shape showing damage caused by exposure of the magnets to strong magnetic fields. A stator **200** has coils **202** for generating a set of

moving magnetic poles. Figure 2A shows that a portion of magnets **102** have been demagnetized as a result of exposure to large changes of magnetic flux. The shaded portions **204** indicate parts of the magnet that tend to become demagnetized easier than other regions. Magnets that include NdFeB, Ferrite, SmCo, or Alnico, for example, are susceptible to such demagnetization.

Figure 2B is a graph that illustrates the conditions upon which a magnet becomes demagnetized, shown as an inflection point, or “knee” in the graph. The point at which demagnetization occurs depends upon temperature of the magnet, and the flux density that passes through the magnet. The presence of a cage allows for a minimization that in the reduction of flux density in the magnet that occurs during transient type events, specifically an accidental or purposeful short circuit of one or more of the stator windings. The machine design may be so that under normal operation, the magnet operating point of 110 [C] and 0.4 [T] is obtained. Without a cage, the flux density in portions of the magnet may be reduced to 0.0 [T], for example. As the flux density at 110 [C] is below the knee of about 0.19 [T], these portions of the magnet that fall below the knee are demagnetized. The presence of a cage prevents the flux density from falling below the knee, thus preventing the demagnetization of the magnet.

Some conventional electric machines, such as synchronous machines for example, include cage structures. If the conducting cage is a closed circuit that surrounds the magnetic pole created by the permanent magnet, a change in magnetic flux linked in that cage induces a current in the loop, which creates its own countervailing magnetic field.

Thus, a PM electrical machine with a conductive cage has greater protection from damage to the permanent magnets caused by changes in magnetic flux, but suffers a loss of efficiency during normal operation. A PM electrical machine without a conductive cage has greater efficiency during normal operation, but is susceptible to damage to the permanent magnets during startup or fault conditions.

Accordingly, in light of these disadvantages associated with both machines with cages and machines without cages, there exists a need for

PM machines with cages that can be controlled such that the cage conducts when needed and does not conduct when needed, i.e., PM machine with a hybrid cage and methods for operating same.

5

SUMMARY

According to one aspect, the subject matter described herein includes a rotor and hybrid cage for a permanent magnet electrical machine, the rotor comprising a rotor body having a central axis and including a plurality of permanent magnets positioned to create a plurality of rotor magnetic poles distributed around a peripheral surface of the rotor. The rotor also includes a hybrid cage that includes conductive loops around each of the rotor magnetic poles, where the conductive loops are controllable to form a closed circuit or an open circuit around each of the rotor magnetic poles.

According to another aspect, the subject matter described herein includes a permanent magnet electrical machine with a hybrid cage. The machine includes a stator having a central axis and a plurality of windings for generating a rotating field of stator magnetic poles, and a rotor having a central axis which coincides with the central axis of the stator, the rotor including a plurality of permanent magnets positioned to create a plurality of rotor magnetic poles distributed around a peripheral surface of the rotor. The rotor also includes a hybrid cage that includes conductive loops around each of the rotor magnetic poles, where the conductive loops are controllable to form a closed circuit or an open circuit around each of the rotor magnetic poles.

According to another aspect, the subject matter described herein includes a method for operating a permanent magnet electrical machine with a hybrid cage. The method includes providing, at an electrical machine that includes a rotor having a plurality of permanent magnets positioned to create a plurality of rotor magnetic poles distributed around a peripheral surface of the rotor, a hybrid cage comprising conductive loops around each of the rotor magnetic poles, wherein the conductive loops are controllable to form a closed circuit or an open circuit around each of the rotor magnetic poles. The method also includes controlling the conductive paths to form a closed circuit around each of the rotor magnetic poles in response to the presence

of a magnetic field having a field strength that exceeds a threshold magnitude, and controlling the conductive paths to form an open circuit around each of the rotor magnetic poles in response to the absence of a magnetic field having a field strength that exceeds a threshold magnitude.

5 The subject matter described herein can be implemented in software in combination with hardware and/or firmware. For example, the subject matter described herein can be implemented in software executed by a processor. In one exemplary implementation, the subject matter described herein can be implemented using a non-transitory computer readable
10 medium having stored thereon computer executable instructions that when executed by the processor of a computer control the computer to perform steps. Exemplary computer readable media suitable for implementing the subject matter described herein include non-transitory computer-readable media, such as disk memory devices, chip memory devices, programmable
15 logic devices, and application specific integrated circuits. In addition, a computer readable medium that implements the subject matter described herein may be located on a single device or computing platform or may be distributed across multiple devices or computing platforms.

20 BRIEF DESCRIPTION OF THE DRAWINGS

Preferred embodiments of the subject matter described herein will now be explained with reference to the accompanying drawings, wherein like reference numerals represent like parts, of which:

25 Figures 1A and 1B are sections of rotors of a conventional permanent magnet electrical machine without a protective cage;

Figure 2A is a cross section of a rotor showing damage to the rotor permanent magnets caused by exposure of the magnets to strong magnetic fields;

30 Figure 2B is a graph that illustrates the conditions upon which a magnet becomes demagnetized;

Figures 3A and 3B illustrate sections of exemplary rotors for a permanent magnet electrical machine with a hybrid cage according to embodiments of the subject matter described herein;

Figures 4A and 4B illustrate sections of exemplary rotors for a permanent magnet electrical machine with a hybrid cage according to other embodiments of the subject matter described herein;

Figures 5A, 5B, and 5C illustrate circuit topologies of rotors with hybrid cages according to embodiments of the subject matter described herein;

Figures 6 through 10B illustrate cross sections of exemplary permanent magnet electrical machines having a hybrid cage according to embodiments of the subject matter described herein;

Figure 11 is a graph showing the benefits of a protective hybrid cage according to an embodiment of the subject matter described herein; and

Figure 12 is flow chart illustrating an exemplary process for operating a permanent magnet electrical machine with a hybrid cage according to an embodiment of the subject matter described herein.

DETAILED DESCRIPTION

In accordance with the subject matter disclosed herein, permanent magnet machines having a hybrid cage and methods for operating same are provided.

Reference will now be made in detail to exemplary embodiments of the present invention, examples of which are illustrated in the accompanying drawings. Wherever possible, the same reference numbers will be used throughout the drawings to refer to the same or like parts.

In order to have the benefits that the presence of a cage structure provides and also have the benefits that the absence of a cage structure provides, a hybrid cage structure is hereby presented, in which the conductive paths of the cage are controllable to form a closed circuit or an open circuit. When the conductive paths of the cage form a closed circuit, the hybrid cage operates to protect the rotor permanent magnets from damage. When the conductive paths of the cage form an open circuit, the hybrid cage does not reduce the efficiency of the machine in normal operation.

Figures 3A and 3B illustrate sections of exemplary rotors for a permanent magnet electrical machine with a hybrid cage according to embodiments of the subject matter described herein.

Figure 3A illustrates a section of a rotor **300** having magnets **102** that
5 are surrounded by conductive paths **302A**, **302B**, and **302C**, which are herein collectively referred to as conductive paths **302**. Each conductive path includes a switching device **303A**, **303B**, **303C**, where are herein collectively referred to as switching devices **303**. The combination of conductive paths **302** and switching devices **303** create a hybrid cage
10 around rotor **300**.

In one mode of operation, switching devices **304** electrically conduct, forming a closed circuit loop around each magnet **102**. In another mode of operation, switching devices **304** do not electrically conduct, breaking the closed circuit loop around each magnet **102**, i.e., causing an open circuit. In
15 the embodiment illustrated in Figure 3A, each switching device has its own respective control input **306A**, **306B**, and **306C**, where are herein collectively referred to as control inputs **306**. In one embodiment, each switching device may be controlled individually. In another embodiment, switching devices **304** may be controlled as a group.

20 Thus, in the embodiment illustrated in Figure 3A, conductive paths **302** form conductive loops around each magnet **102**, and each loop is controllable to be an open circuit or a closed circuit. In the embodiment illustrated in Figure 3A, all loops are connected together electrically on the right side of each loop. Figure 3A illustrates an embodiment in which the
25 conductive paths are positioned relatively close to the periphery of its respective permanent magnet.

In one embodiment, a controller may produce the control inputs **304** according to whether having a closed loop is desired, such as during startup or a fault condition, or having an open loop is desired, such as during normal
30 operation of the machine. Example switching devices **304** include but are not limited to diodes, silicon-controlled rectifiers (SCRs), metal oxide semiconductor field effect transistors (MOSFETs), insulated gate bipolar transistors (IGBTs), mechanical relays, or any other type of switch.

Embodiments which use diodes, for example, have the added benefit that no control inputs **306** are needed, which simplifies design and construction. By providing a cage that implements a closed loop, the eddy current losses are forced to the cage elements, with the result that, during short circuits, the magnet does not experience the kind of significant local heating that may lead to damage. The presence of a conducting loop, in other words, helps the magnet remain healthy. Such protection is particularly beneficial for magnets that contain NdFeB, Ferrite, SmCo, or Alnico.

Figure 3B illustrates another version of the hybrid cage structure shown in Figure 3A, except that each loop shares a conductive path with the loop on either side of it. In the embodiment illustrated in Figure 3B, there is only one conductor between each pair of magnets **102**, rather than the pair of conductors shown in Figure 3A. In the embodiment illustrated in Figure 3B, switching devices **304** are located at one end of rotor **300**, but other configurations are contemplated. For example, there could be switching devices at the other end, at both ends, or even along the conductive paths that run between and parallel to the magnets. In other words, switching devices **304** may be located anywhere along the conducting loop such that they can controllably create an open circuit or a closed circuit.

Figures 4A and 4B illustrate sections of exemplary rotors for a permanent magnet electrical machine with a hybrid cage according to other embodiments of the subject matter described herein.

Figure 4A illustrates a section of a rotor **400** that contains conductive paths **302** that surround and circumscribe each rotor magnetic pole. The conductive paths **302** and switching devices **304** comprise the hybrid cage. This illustrates the principle that the controllable conductive paths that surround the rotor magnetic poles may surround multiple magnets, or magnets a variety of configurations. This configuration is herein referred to as a "loop per pole" topology. In the embodiment illustrated in Figure 4A, each of the switching devices **304** require a control input **306**, but in another embodiment the hybrid cage may use switching devices, such as diodes, that do not require control inputs. The circuit topology of the cage shown in Figure 4A differs from the one shown in Figure 3A in that in Figure 3A, each

loop is connected to adjacent loops on only one side, i.e., the side of the loop closest to switching devices **304**, while in Figure 4A, each loop is connected to adjacent loops on two sides. The topology shown in Figure 4A creates closed loops between each pole, but the effect of these loops on the efficiency of the machine may be negligible, depending on the actual dimensions, etc.

Figure 4B shows another variation of a hybrid cage comprised of conductive paths **302** and switching devices **304** in which individual magnets have their own controllable loop, herein referred to as a “loop per magnet” topology. Figure 4B also illustrates the principle that multiple loops may be controlled by a single control signal **306**.

In addition to the various physical configurations of magnets, conductive paths, switches, etc. that are contemplated by the instant application, multiple electrical configurations are contemplated. Figures 5A through 5C show a few examples of the many electrical or circuit topologies that are possible according to embodiments of the subject matter described herein.

Figure 5A illustrates the circuit of a hybrid cage according to one embodiment of the subject matter described herein. For simplicity, the “unrolled” surface of rotor **500** is shown in a two-dimensional representation. The left edge of rotor **500** would be joined to the right edge of rotor **500** to form the cylindrical surface of a three-dimensional rotor. The dashed and dotted lines indicate conducting loops **502A**, **502B**, **502C**, and **502D**, which are herein collectively referred to as conducting loops **502**. In one embodiment, the dashed lines indicate the presence of a physical conductor separate from the rotor body while the dotted lines indicate a conductive path through the rotor body, either through a conductor embedded or cast within the rotor body or through the rotor body itself, if the rotor body is made of an electrically conductive material. Each dotted or dashed line may represent a single conductor or multiple conductors. The pair of dashed lines between each pair of magnetic poles may be a single conducting path instead of the pair of conducting paths as shown. There may be a number of conductors axially passing through the rotor, which may or may not be

connected based on specific constructions, as well as current and voltage ratings.

In the embodiment illustrated in Figure 5A, switching devices **504A**, **504B**, **504C**, and **504D**, which are herein collectively referred to as switching devices **504**, are located at one end of rotor **500**. Switching devices **504** are closed on command to form conductive loops that surround each rotor magnetic pole, shown as labels "North" and "South" to indicate the direction of the magnetic pole. Each magnetic pole projects normal to the surface of rotor **500**, i.e., toward the viewer. The embodiment illustrated in Figure 5A provides a controllably conductive loop around each rotor magnetic pole. Each pole may be created by a single magnet, as shown in Figure 3A, or by multiple magnets, as shown in Figure 4A.

Figure 5B illustrates a hybrid cage according to another embodiment of the subject matter described herein. The embodiment illustrated in Figure 5B may be used with rotors where each pole is made of multiple magnet sections, such as shown in Figure 4B. In this manner each magnet section may be separately protected. This circuit construction may be used with a variety of rotor designs, especially where a rotor magnetic pole is created a magnet assembly constructed of multiple individual magnet segments, which may be individually protected by this cage concept. The choice of number of coils would depend upon voltage and currents induced, which would largely depend upon size of the machine, e.g., via application of Faraday's law.

Figure 5C illustrates a hybrid cage according to yet another embodiment of the subject matter described herein. The embodiment illustrated in Figure 5C provides separate cages and circuits for protection of a given portion of magnet or for dynamic sequencing of the cages. In this embodiment, a first cage **502** is shown as dashed or dotted lines and a second cage **508** is indicated using lines with a "dash-dot-dash-dot" pattern. First cage **502** includes a first set of switching devices, only one of which is labeled as switching device **504**. First cage **510** includes its own, separate set of switching devices, only one of which is labeled as switching device **510**. In one embodiment, one cage may provide protection in one direction

and another cage may provide protection in another direction. For example, second cage **508** may provide additional protection along the q-axis.

For all circuit topologies, including those shown in Figures 5A-5C and also including circuit topologies not shown, all circuits may be connected in multiple series and parallel paths, including multiple conductive turns about a single magnet or magnet assembly to attain preferable current and voltage characteristics. These characteristics would be determined by the geometry of the machine, as well as the current, voltage, and other ratings of the devices in which open and close the cage circuits.

Figure 6 illustrates a hybrid cage according to yet another embodiment of the subject matter described herein. Figure 6 illustrates a cross section of a surface magnet type motor, having a stator **600** and a rotor **300** separated by an air gap. Magnets **102** are positioned on the outer surface of rotor **300**. The text 'magnet' is oriented such that the magnet would be oriented in the direction of reading of the text. Each magnet is surrounded by a cage **502** having conductors seen in cross section as shaded boxes. In the embodiment illustrated in Figure 6, the conductors that make up the cage are located in close proximity to the magnets, and thus resembles the embodiment illustrated in Figure 3A and the circuit shown in Figure 5A.

Figure 7 illustrates a hybrid cage according to yet another embodiment of the subject matter described herein. The embodiment illustrated in Figure 7 is similar to the embodiment illustrated in Figure 6, except that a single conductor shared between each pair of magnets **102**, and thus resembles the embodiment illustrated in Figure 3B. This construction uses fewest parts, which possibly protecting the magnets to the greatest degree from air gap field variations for this rotor construction.

Figure 8 illustrates a hybrid cage according to yet another embodiment of the subject matter described herein. The embodiment illustrated in Figure 8 is also similar to the embodiment illustrated in Figure 6, except that cage **502** is embedded within the body of rotor **300**, e.g., within the laminations that make up the rotor core. This configuration is well suited for higher speed machines, since the conductors are securely held into place

by the rotor laminations. Figure 8 also illustrates the presence of a second cage located along the q-axis and thus resembles the circuit shown in Figure 5C.

Figures 9A and 9B illustrate a hybrid cage according to yet another embodiment of the subject matter described herein. Figures 9A and 9B illustrate cross sections of motor having a stator **600** and a rotor **400** attached to a shaft **900**, where the laminations of rotor **400** contain 'V' mounted or embedded magnets. In the embodiment illustrated in Figure 9A, conductors of cage **502** are in close proximity to the magnets. For example, the bars may be connected in circuits that encompass each magnet, such as shown in Figure 4B. In the embodiment illustrated in Figure 9B, conductors of cage **502** are located in close proximity to the magnets, but only on the side of the magnets that are close to the air gap, such as shown in Figure 4A. Benefits of this embodiment include lower cost due to the fact that this construction uses fewest parts, and the additional benefit that it may give to the magnets a greater degree of protection from air gap field variations.

Figures 10A and 10B illustrate a hybrid cage according to yet another embodiment of the subject matter described herein. Figures 10A and 10B illustrate cross sections of motor having a stator **600** and a rotor **100** attached to a shaft **900**, where the laminations of rotor **1000** contain 'spoke' mounted or embedded magnets. In the embodiment illustrated in Figure 10A, conductors of cage **502** are in close proximity to the magnets. For example, the bars may be connected in circuits that encompass each magnet. In the embodiment illustrated in Figure 10B, conductors of cage **502** are located in close proximity to the magnets, but only on the side of the magnets that are close to the air gap.

The conductors or bars of the hybrid cage may be of any shape, cross-section, etc., as appropriate. For example, the short circuiting bars may be of many different shapes, due to cross section constraints of minimizing leakage flux during normal operation and under active cage events, as well as structural and manufacturing considerations.

The figures above illustrate the application of a hybrid cage in a rotor having magnetic poles that project radially outward from the surface of the

rotor, but the subject matter described herein is not limited to radial flux machines. The concepts and principles disclosed herein may be applied to other types of machines, including axial flux and transverse flux permanent magnet machines. Regardless of the orientation of the rotor magnetic poles – radial, axial, transverse, etc., – a hybrid cage may be provided that implements a controllably conductive loop around the magnetic poles.

Figure 11 is a graph showing the benefits of a protective cage. Figure 11 illustrates the flux density within a permanent magnet of a rotor with a cage (thin line) and without a cage (thick line) during the course of a large change in flux density generated by a stator. As shown in Figure 11, the magnet flux density [T] drops in response to the external field, and that this drop occurs very quickly, during a 10 microsecond window. The flux density of the magnet or portions of the magnet not protected by a cage becomes strongly negative after just 5 microseconds, and does not recover after the external field is removed, 5 microseconds after that – i.e., the magnet has suffered some demagnetization as a result of exposure to the external field. The magnet that is protected by the cage, on the other hand, also suffers a loss of flux density, but not as great a loss as suffered by the unprotected magnet.

Figure 12 is flow chart illustrating an exemplary process for operating a permanent magnet electrical machine with a hybrid cage. At a permanent magnet electrical machine that includes a stator having a central axis and a plurality of windings for generating a rotating field of stator magnetic poles, a rotor having a central axis which coincides with the central axis of the stator, the rotor including a plurality of permanent magnets positioned to create a plurality of rotor magnetic poles distributed around a peripheral surface of the rotor:

At step **1200**, provide, at an electrical machine that includes a rotor having a plurality of permanent magnets positioned to create a plurality of rotor magnetic poles distributed around a peripheral surface of the rotor, a hybrid cage comprising conductive loops around each of the rotor magnetic poles, wherein the conductive loops are controllable to form a closed circuit or an open circuit around each of the rotor magnetic poles. The rotor

magnetic poles may be created by one or more permanent magnets. In one embodiment, the conductive loops individually surround each of the one or more permanent magnets that create the rotor magnetic pole. In another embodiment, each of the conductive loops surrounds an assembly of
5 permanent magnets that collectively create the rotor magnetic pole. In one embodiment, some but not all of the rotor magnetic poles are surrounded by its own conductive loop.

At step **1202**, determine whether a magnetic field having a field strength that exceeds a threshold magnitude is present, e.g., determine
10 whether the rotor magnetic pole is being subject to a potentially harmful level of magnetic flux.

At step **1204**, in response to the presence of a magnetic field having a field strength or change in field strength that exceeds a threshold magnitude (e.g., in response to determining that the rotor magnetic pole is being subject
15 to a potentially harmful level of magnetic flux), control the conductive path to form a closed circuit around the rotor magnetic pole.

At step **1206**, in response to the absence of a magnetic field having a field strength or change in field strength that exceeds a threshold magnitude (e.g., in response to determining that the rotor magnetic pole is not being
20 subject to a potentially harmful level of magnetic flux), control the conductive path to form an open circuit around the rotor magnetic pole.

The process then returns to step **1202**, repeating as necessary to protect the rotor magnetic pole from potentially harmful conditions when they occur and breaking the circuit of the conductive loop and thus improving the
25 efficiency of the permanent magnet electrical machine when potentially harmful conditions are not present.

There are a number of circumstances which may give rise to the rotor magnetic pole being subject to potentially harmful levels of magnetic flux. For example, the failure of a stator coil, stator coil controller, or stator coil
30 power supply could cause a fault condition in which the rotor magnetic poles are subject to a magnetic field having a field strength that exceeds a threshold value. A mechanical failure of the machine could likewise cause the presence of potentially harmful levels of magnetic flux.

There are several ways to determine whether a rotor magnetic pole is or is not being subject to a potentially harmful level of magnetic flux, including monitoring for failure of stator coils, controllers, or power supplies, and direct monitoring of magnetic field strength, such as via the use of Hall effect transistors for direct measurement of fields and monitor coils for indirect measurement of fields in and around the poles, as well as sensing on stator windings, etc.

The measurement may be made from either the rotor itself or from stationary mounted devices or sensors, from which signals are conveyed to device triggering circuit(s).

In addition to the hybrid cage structures described above, additional protection may be provided by the inclusion of a thermally insulating material between the cage and the permanent magnets to reduce propagation of thermal energy from the cage to the magnets.

It will be understood that various details of the subject matter described herein may be changed without departing from the scope of the subject matter described herein. Furthermore, the foregoing description is for the purpose of illustration only, and not for the purpose of limitation.

CLAIMS

What is claimed is:

1. A rotor and hybrid cage for an electrical machine, the rotor comprising:
 - 5 a rotor body having a central axis and including a plurality of permanent magnets positioned to create a plurality of rotor magnetic poles distributed around a peripheral surface of the rotor; and
 - a hybrid cage comprising conductive loops around each of the rotor magnetic poles, wherein the conductive loops are controllable to form a closed circuit or an open circuit around each of the rotor magnetic poles.
- 10 2. The rotor of claim 1 wherein the conductive loops include switching devices controllable to form a closed circuit or an open circuit around each of the rotor magnetic poles.
- 15 3. The rotor of claim 2 wherein the switching devices comprise at least one of a diode, a silicon controlled rectifier, an insulated gate bipolar junction transistor, a metal oxide semiconductor, a field effect transistor, a mechanical switch, and an electromechanical switch.
- 20 4. The rotor of claim 1 comprising a control circuit for controlling the conductive loops to form closed circuits or open circuits around the rotor magnetic poles.
5. The rotor of claim 1 wherein at least one of the conductive loops circumscribes a permanent magnet.
- 25 6. The rotor of claim 1 wherein at least one of the conductive loops circumscribes a magnetic pole created by a plurality of permanent magnets.
7. The rotor of claim 1 wherein at least one of the plurality of permanent magnets is comprised of NdFeB, Ferrite, SmCo, or Alnico.

8. The rotor of claim 1 wherein the conductive loops are controlled to form a closed circuit around each of the rotor magnetic poles in response to the presence of a magnetic field having a field strength or change in field strength that exceeds a threshold magnitude.
- 5 9. The rotor of claim 1 wherein the conductive loops are controlled to form an open circuit around each of the rotor magnetic poles in response to the absence of a magnetic field having a field strength or change in field strength that exceeds a threshold magnitude.
- 10 10. The rotor of claim 1 wherein the rotor magnetic poles are radially, axially, or transversely oriented relative to the rotor.
11. The rotor of claim 1 comprising a thermally insulating material for thermally insulating the conductors of the hybrid cage from the rotor permanent magnets to reduce propagation of thermal energy from the cage to the magnets.
- 15 12. An electrical machine with a hybrid cage, the machine comprising:
a stator having a central axis and a plurality of windings for generating a rotating field of stator magnetic poles; and
a rotor having a central axis which coincides with the central
20 positioned to create a plurality of rotor magnetic poles distributed around a peripheral surface of the rotor and a hybrid cage comprising conductive loops around each of the rotor magnetic poles, wherein the conductive loops are controllable to form a closed circuit or an open circuit around each of the rotor magnetic poles.
- 25 13. The machine of claim 12 wherein at least one of the conductive loops includes a switching device controllable to form a closed circuit or an open circuit.
14. The machine of claim 12 wherein the switching device comprises at least one of a diode, a silicon controlled rectifier, an insulated gate

bipolar junction transistor, a metal oxide semiconductor, a field effect transistor, a mechanical switch, and an electromechanical switch.

- 5
15. The machine of claim 12 comprising a control circuit for controlling the conductive loops to form closed circuits or open circuits around the rotor magnetic poles.
16. The machine of claim 12 wherein at least one of the conductive loops circumscribes a permanent magnet.
- 10
17. The machine of claim 12 wherein at least one of the conductive loops circumscribes a magnetic pole created by a plurality of permanent magnets.
18. The machine of claim 12 wherein at least one of the plurality of permanent magnets is comprised of NdFeB, Ferrite, SmCo, or Alnico.
- 15
19. The machine of claim 12 wherein the conductive loops are controlled to form a closed circuit around each of the rotor magnetic poles in response to the presence of a magnetic field having a field strength or a change of field strength that exceeds a threshold magnitude.
- 20
20. The machine of claim 12 wherein the conductive loops are controlled to form an open circuit around each of the rotor magnetic poles in response to the absence of a magnetic field having a field strength or a change of field strength that exceeds a threshold magnitude.
21. The machine of claim 12 wherein the rotor magnetic poles are radially, axially, or transversely oriented relative to the rotor.
- 25
22. The machine of claim 12 wherein the rotor includes a thermally insulating material for thermally insulating the conductors of the hybrid cage from the rotor permanent magnets to reduce propagation of thermal energy from the cage to the magnets.
23. A method for operating a permanent magnet electrical machine with a hybrid cage, the method comprising:

5 providing, at an electrical machine that includes a rotor having a plurality of permanent magnets positioned to create a plurality of rotor magnetic poles distributed around a peripheral surface of the rotor, a hybrid cage comprising conductive loops around each of the rotor magnetic poles, wherein the conductive loops are controllable to form a closed circuit or an open circuit around each of the rotor magnetic poles;

10 controlling the conductive paths to form a closed circuit around each of the rotor magnetic poles in response to the presence of a magnetic field having a field strength that exceeds a threshold magnitude; and

15 controlling the conductive paths to form an open circuit around each of the rotor magnetic poles in response to the absence of a magnetic field having a field strength that exceeds a threshold magnitude.

24. The method of claim 23 wherein controlling the conductive loops to form open or closed circuits around each of the rotor magnetic poles comprises controlling switching devices located within the conductive loops.

20 25. A non-transitory computer readable medium having stored thereon executable instructions that when executed by the processor of a computer control the computer to perform steps comprising:

25 at an electrical machine that includes a rotor having a plurality of permanent magnets positioned to create a plurality of rotor magnetic poles distributed around a peripheral surface of the rotor and a hybrid cage comprising conductive loops around each of the rotor magnetic poles, wherein the conductive loops are controllable to form a closed circuit or an open circuit around each of the rotor magnetic poles:

30 controlling the conductive paths to form a closed circuit around each of the rotor magnetic poles in response to the presence of a magnetic field having a field strength that exceeds a threshold magnitude; and

controlling the conductive paths to form an open circuit around each of the rotor magnetic poles in response to the absence of a magnetic field having a field strength that exceeds a threshold magnitude.

5

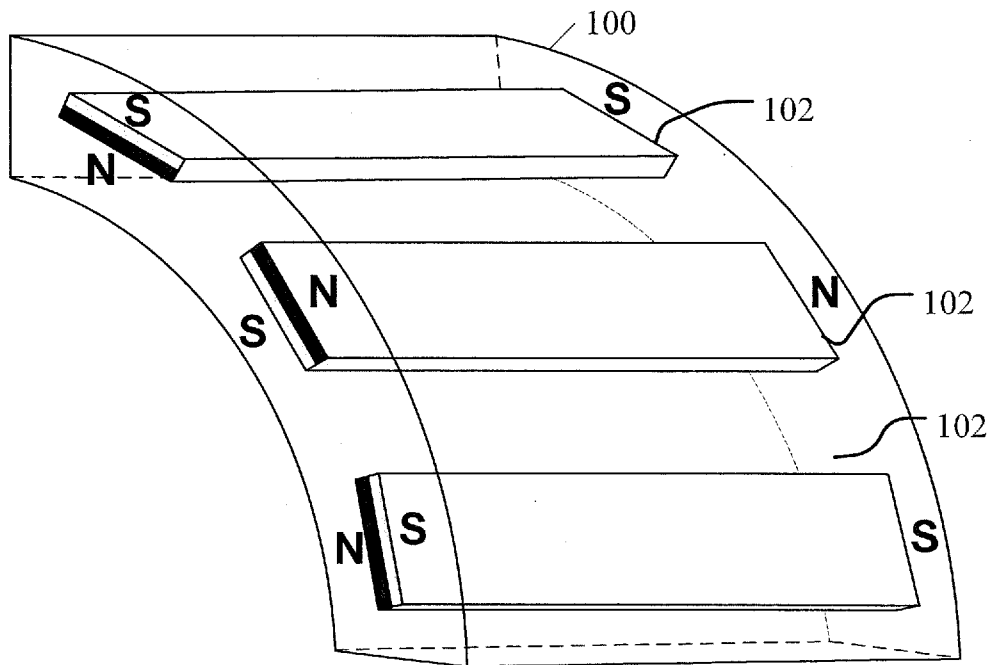


FIG. 1A

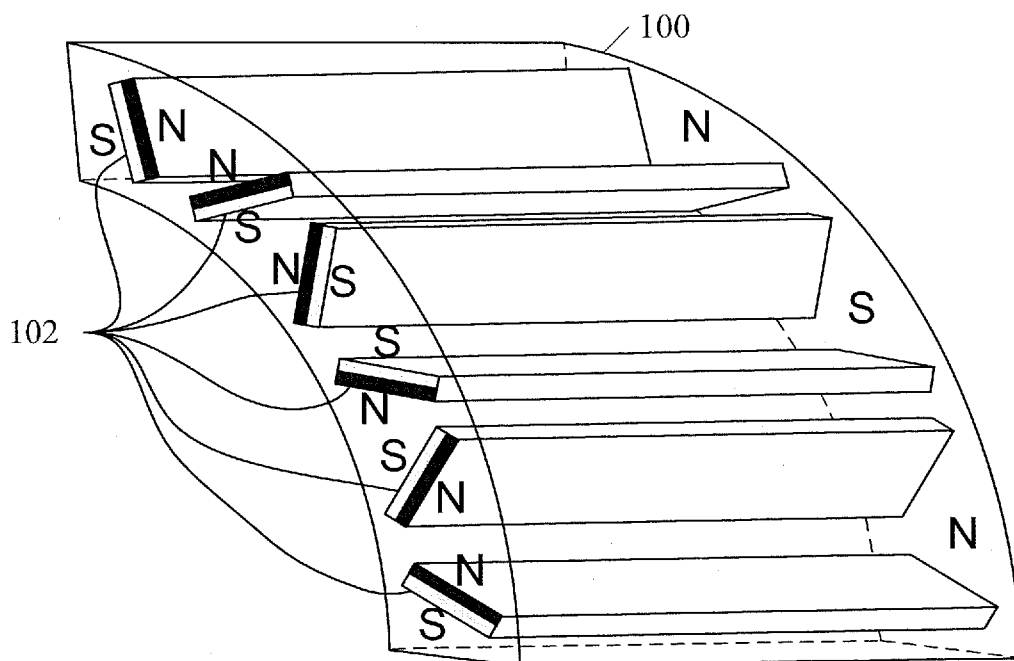


FIG. 1B

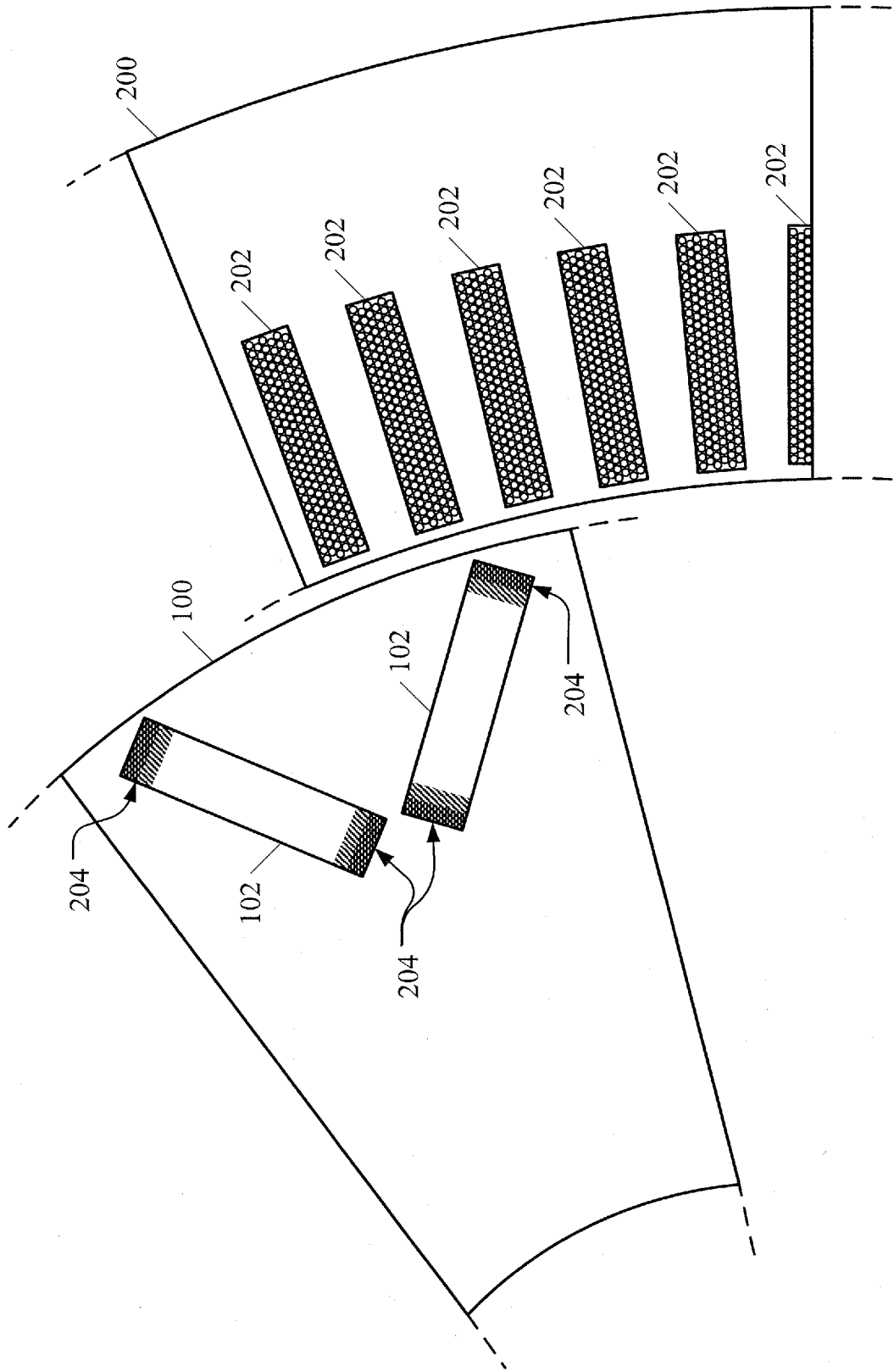


FIG. 2A

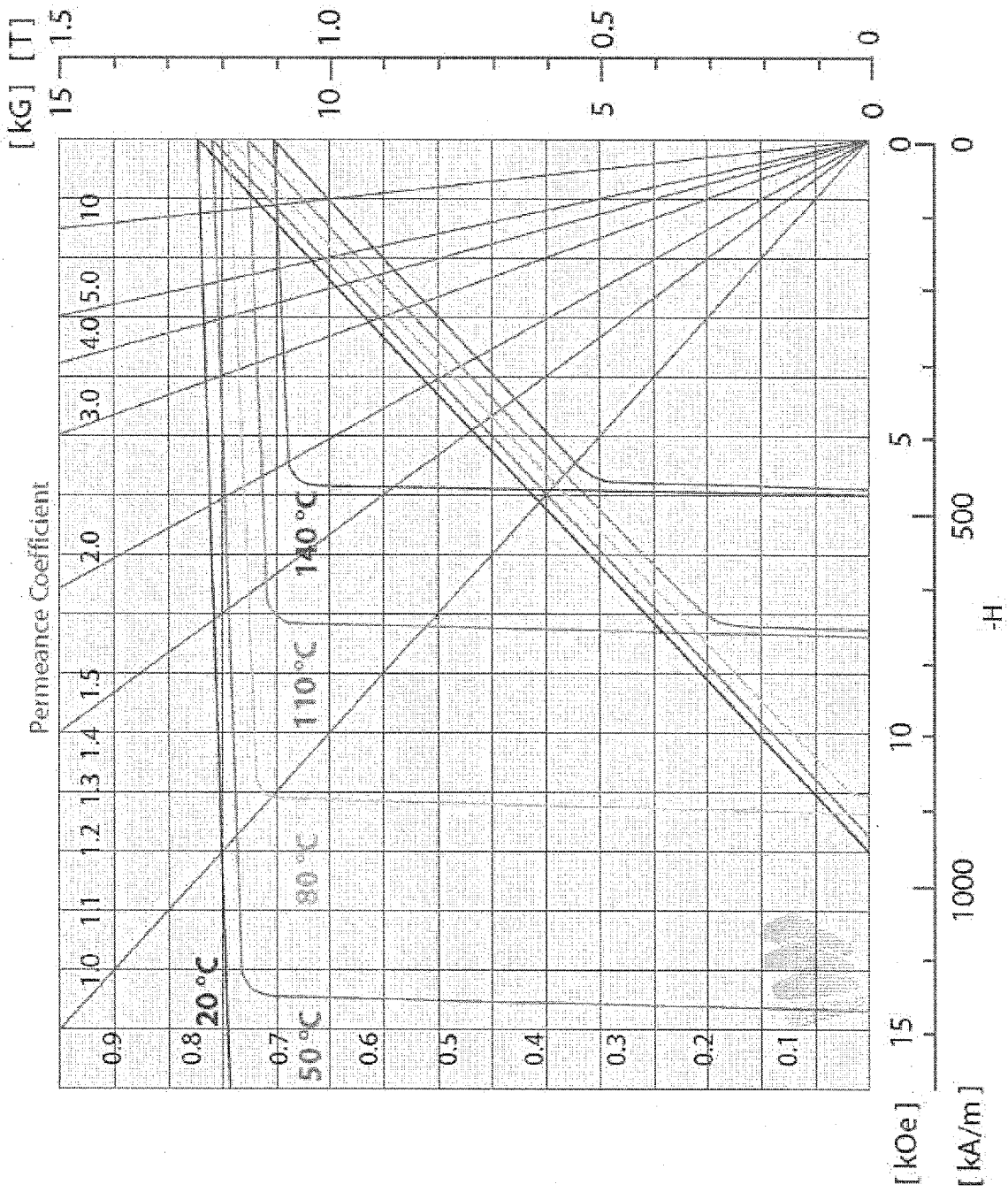


FIG. 2B

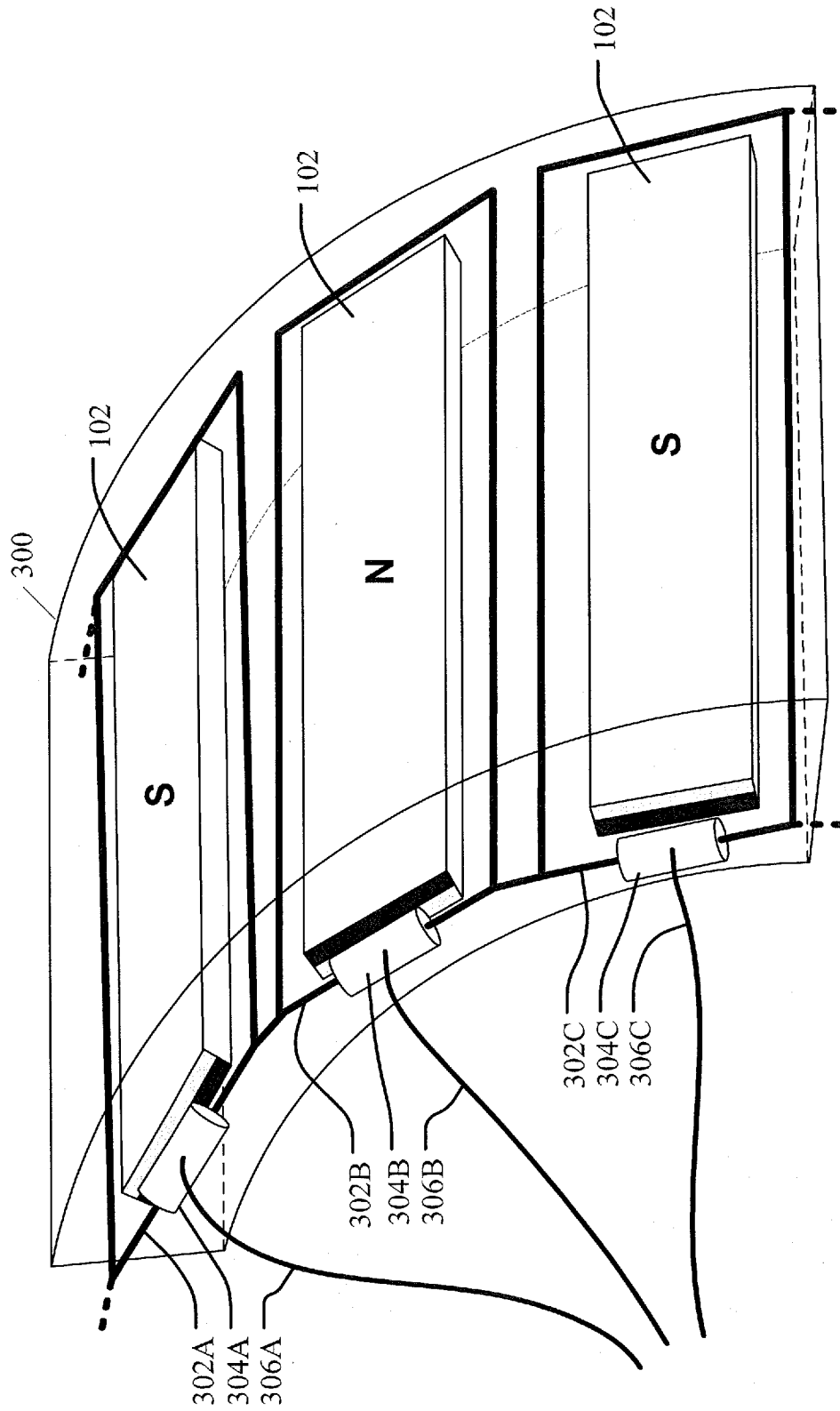


FIG. 3A

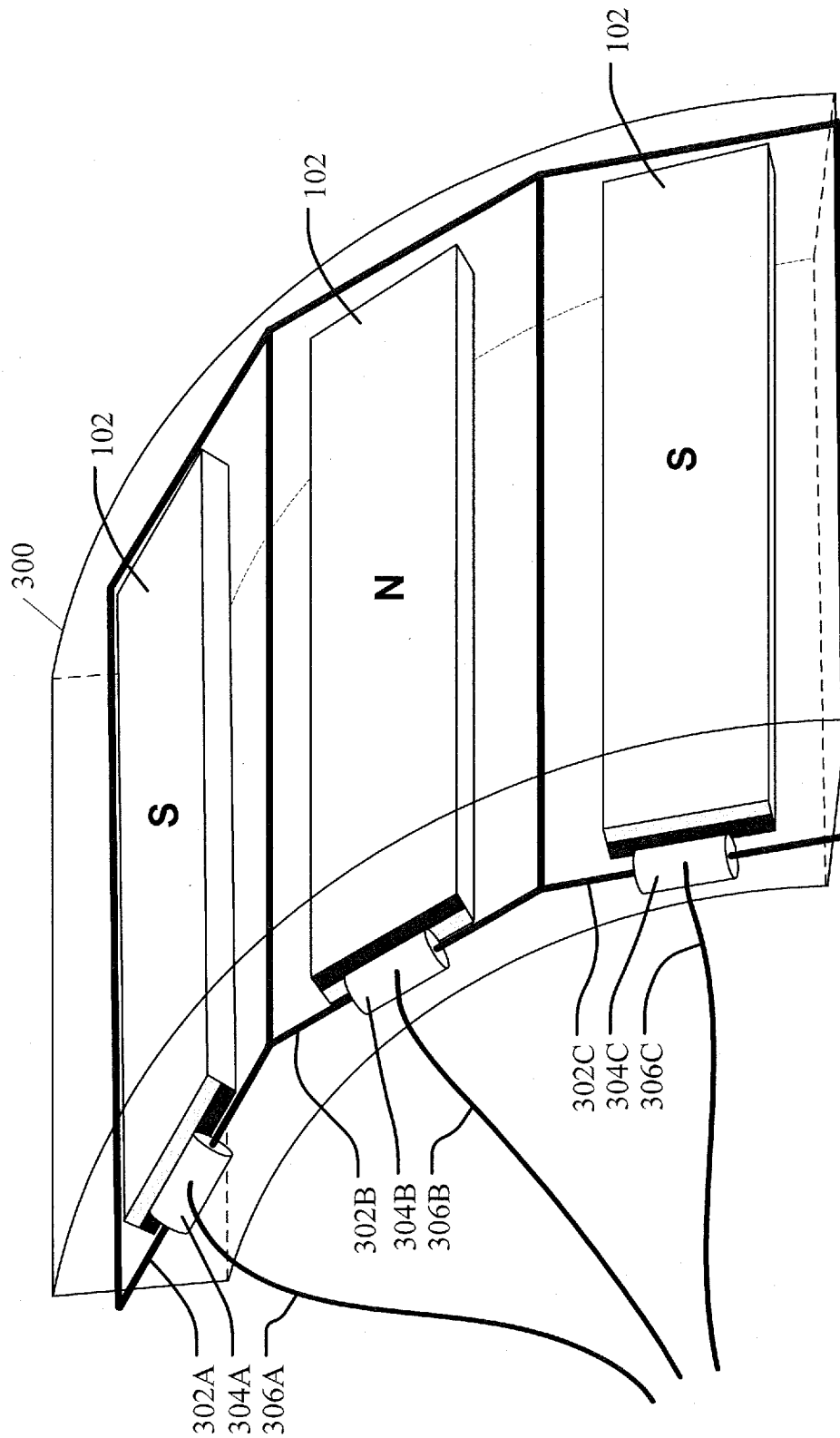


FIG. 3B

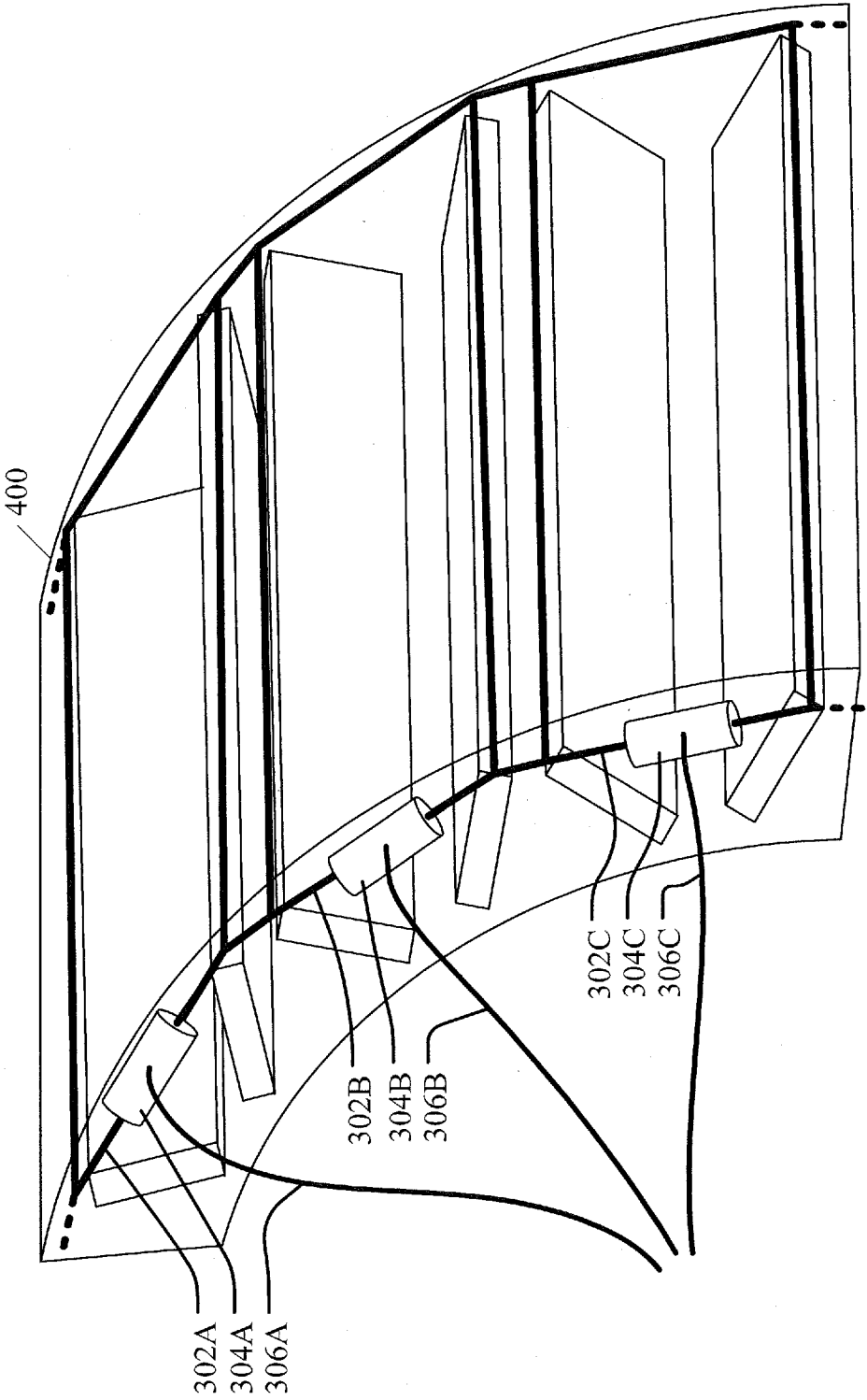


FIG. 4A

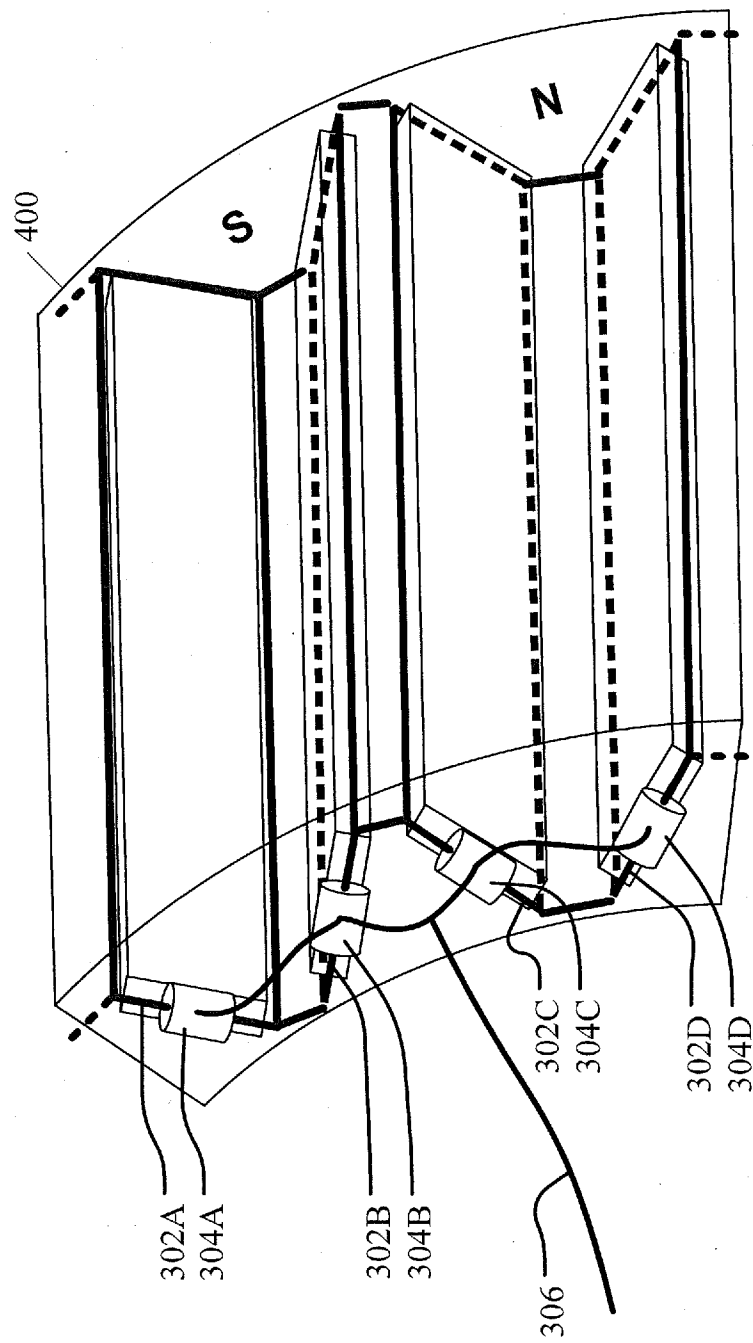
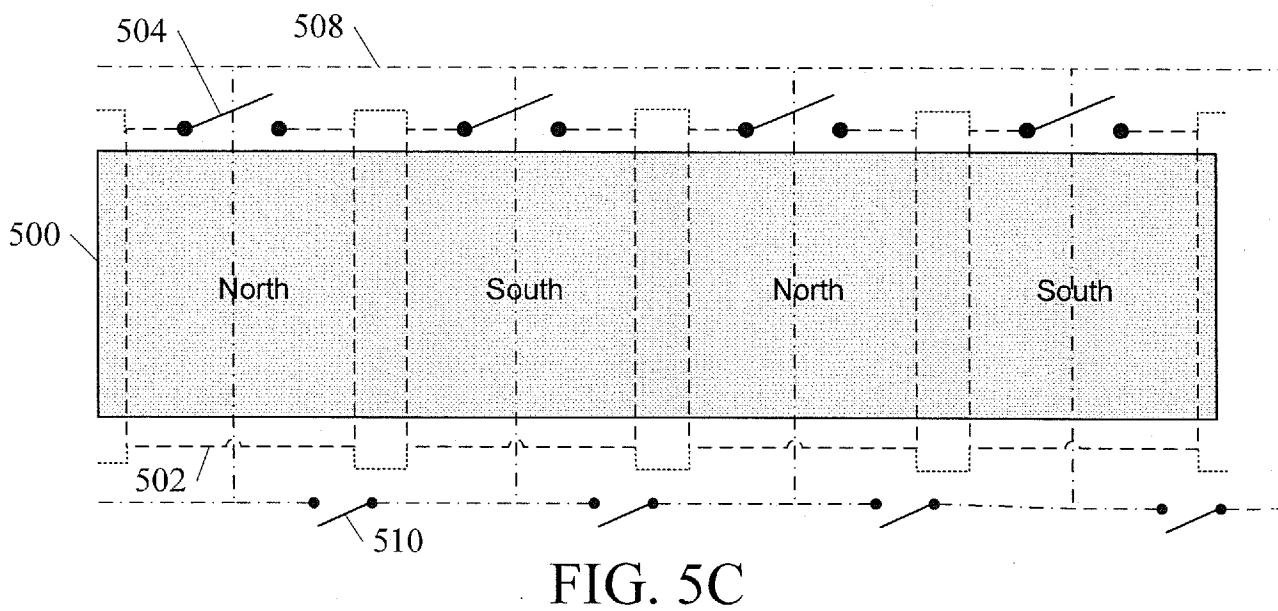
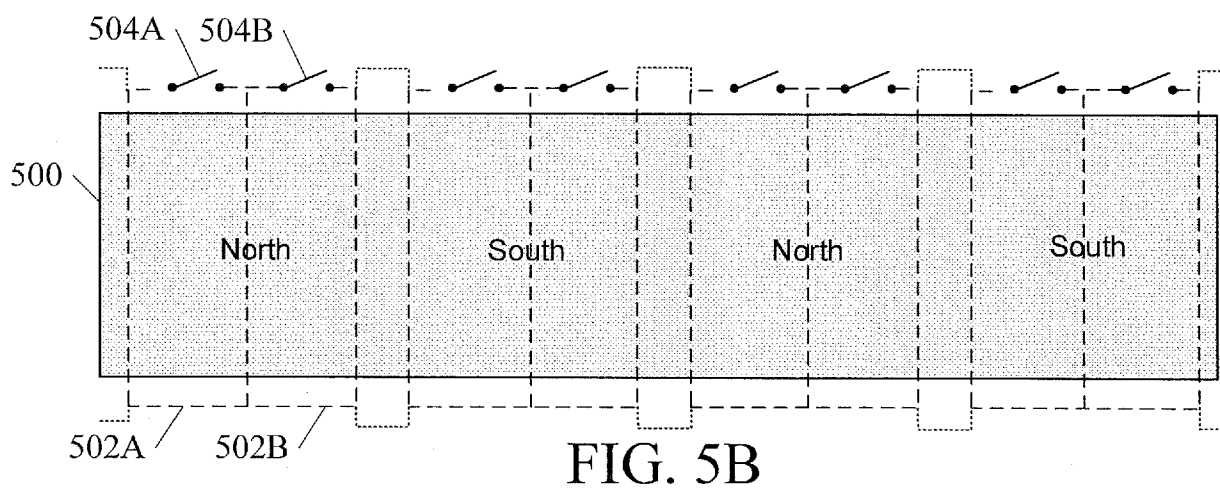
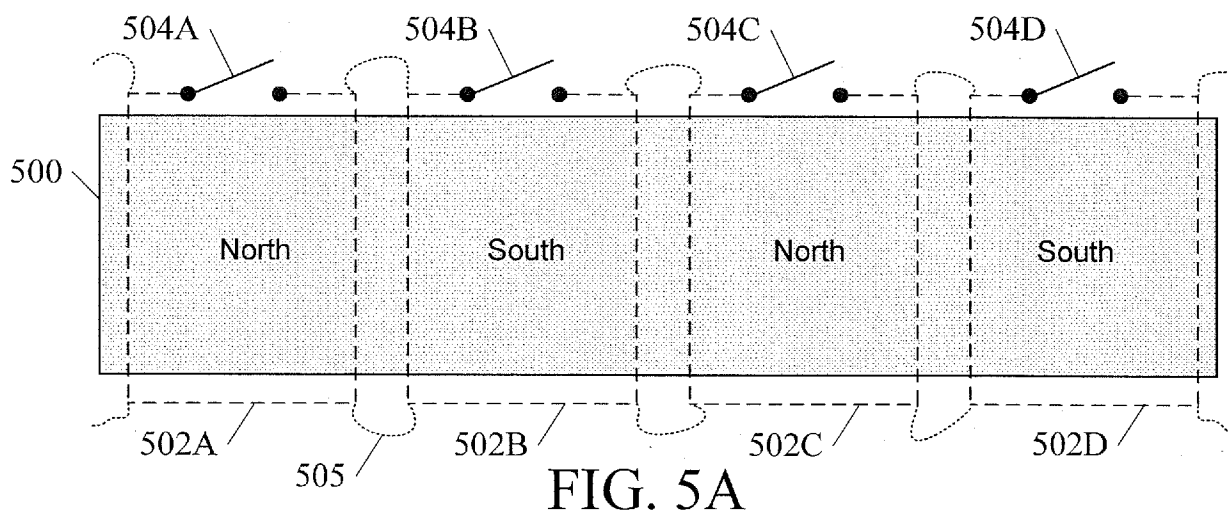


FIG. 4B



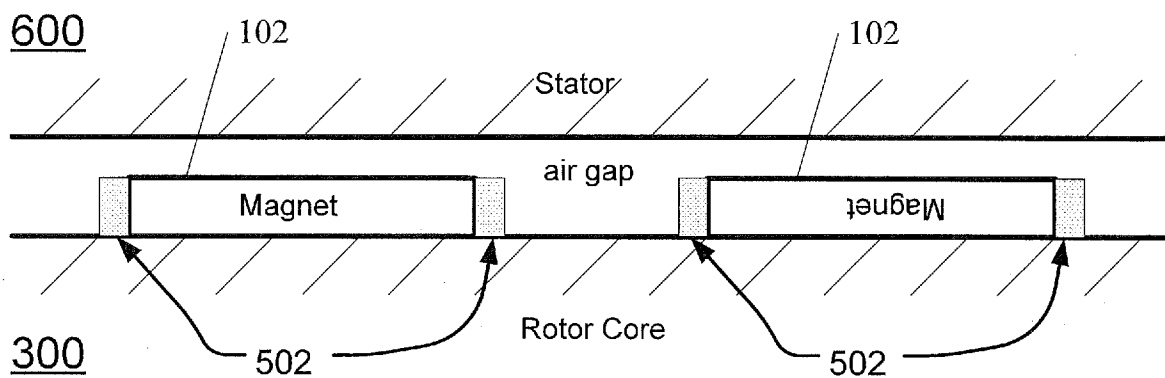


FIG. 6

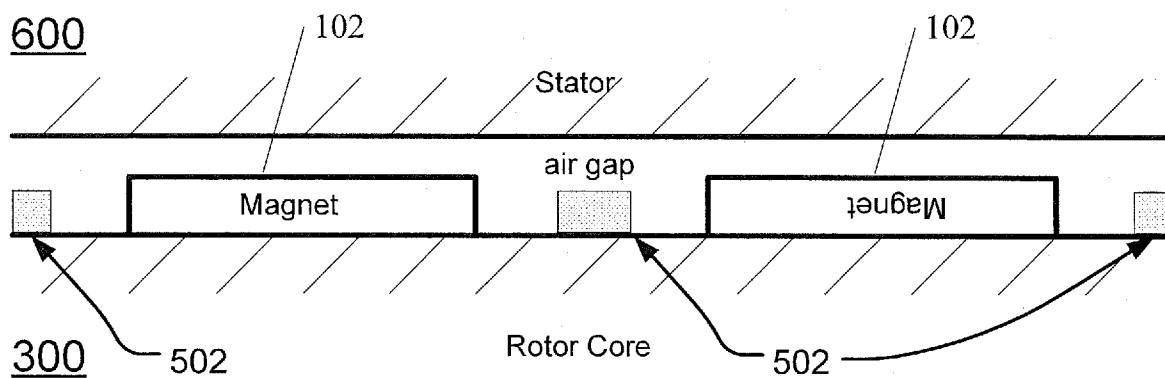


FIG. 7

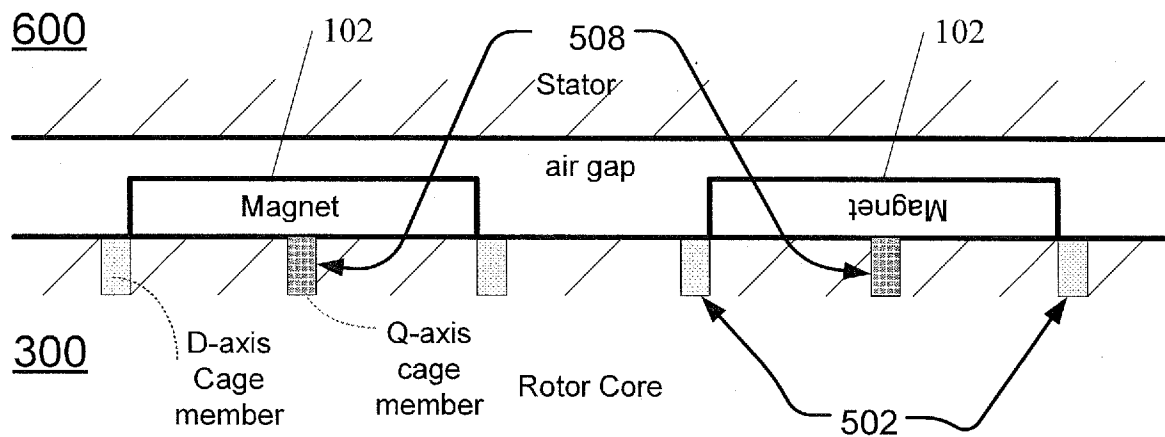


FIG. 8

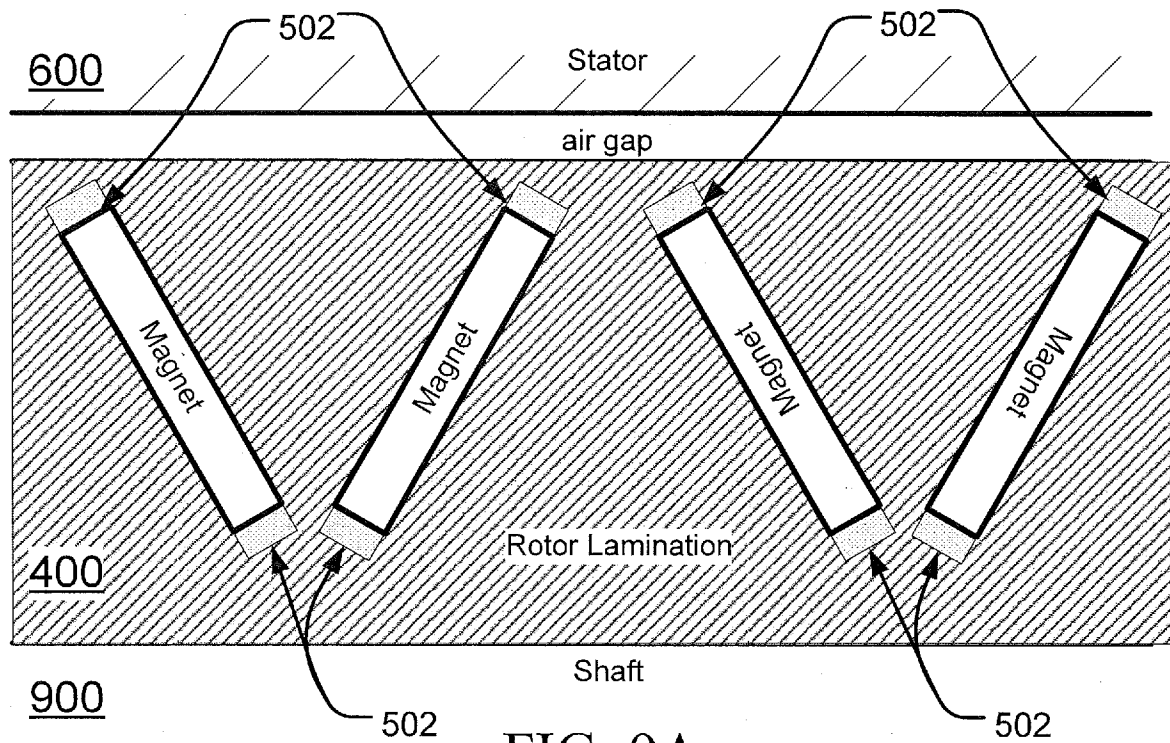


FIG. 9A

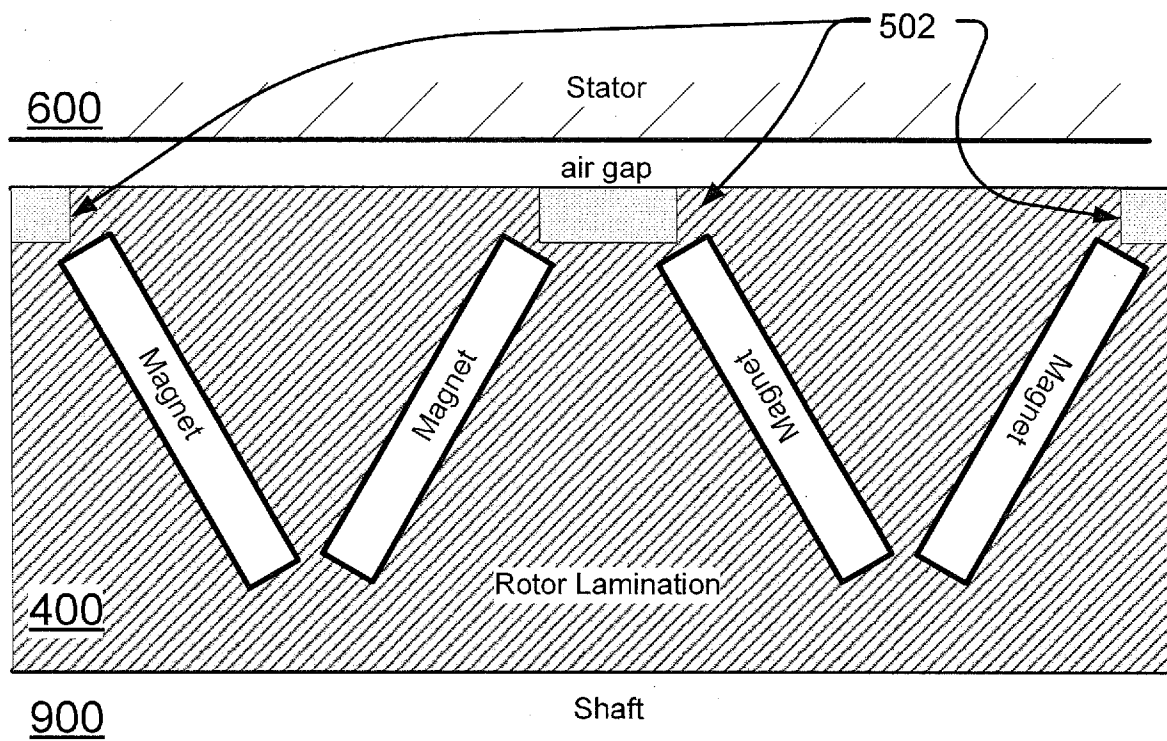


FIG. 9B

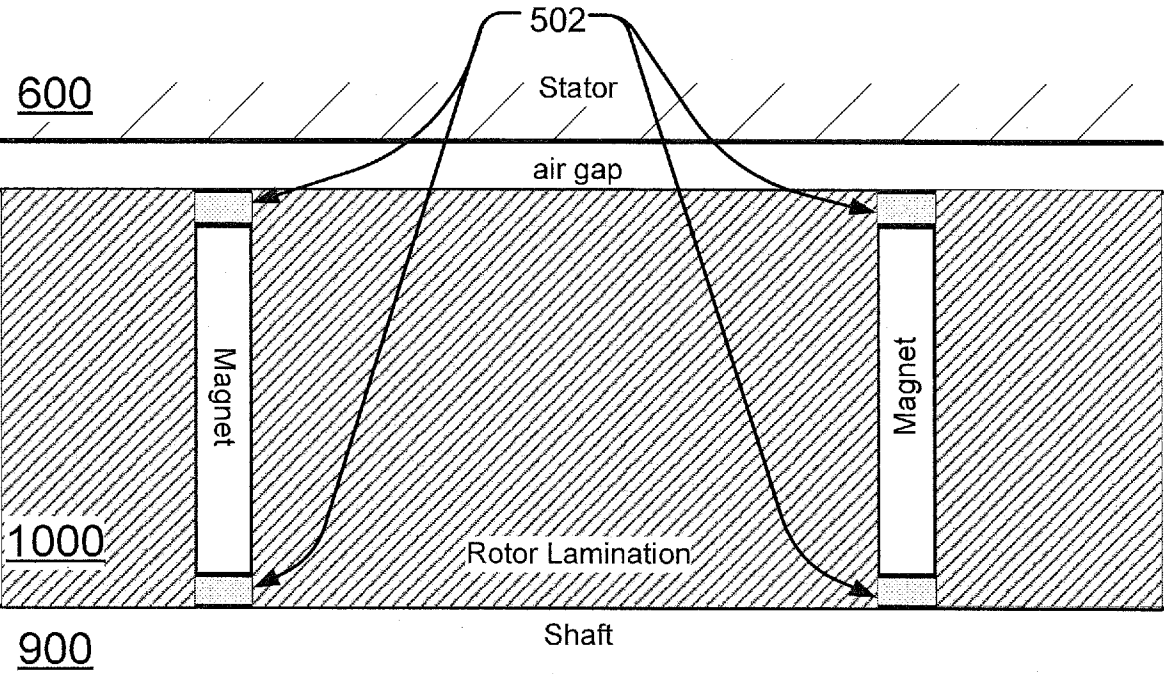


FIG. 10A

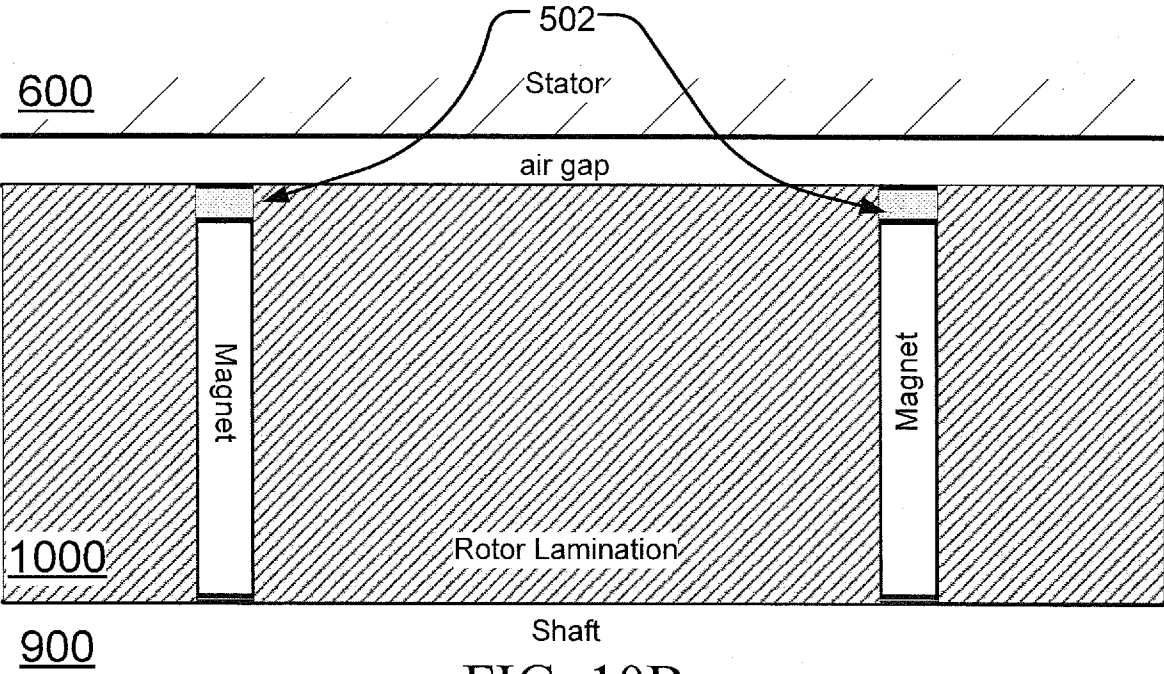


FIG. 10B

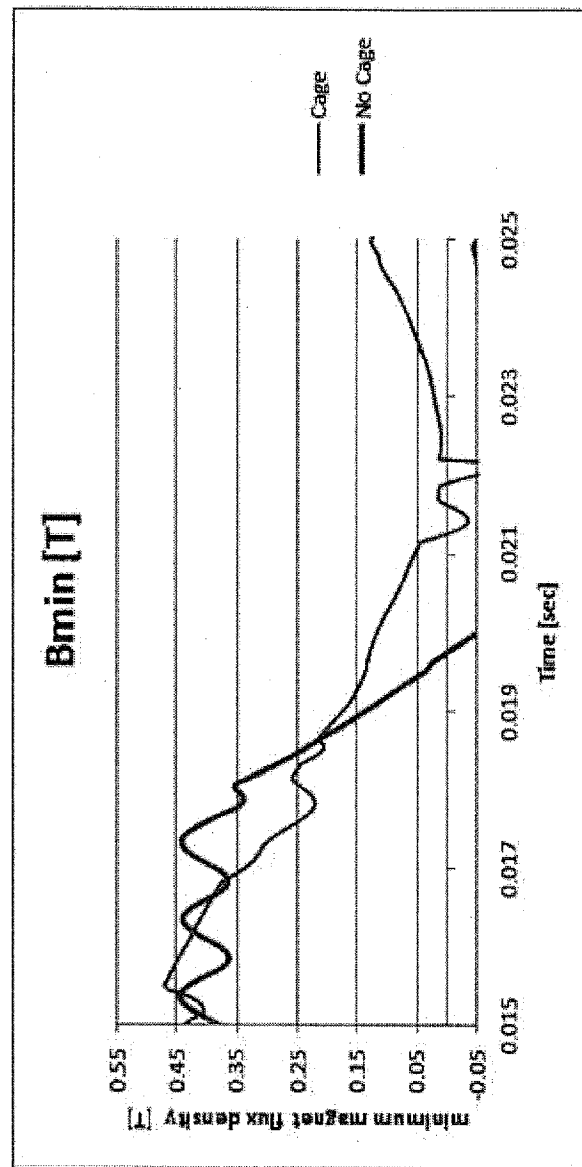


FIG. 11

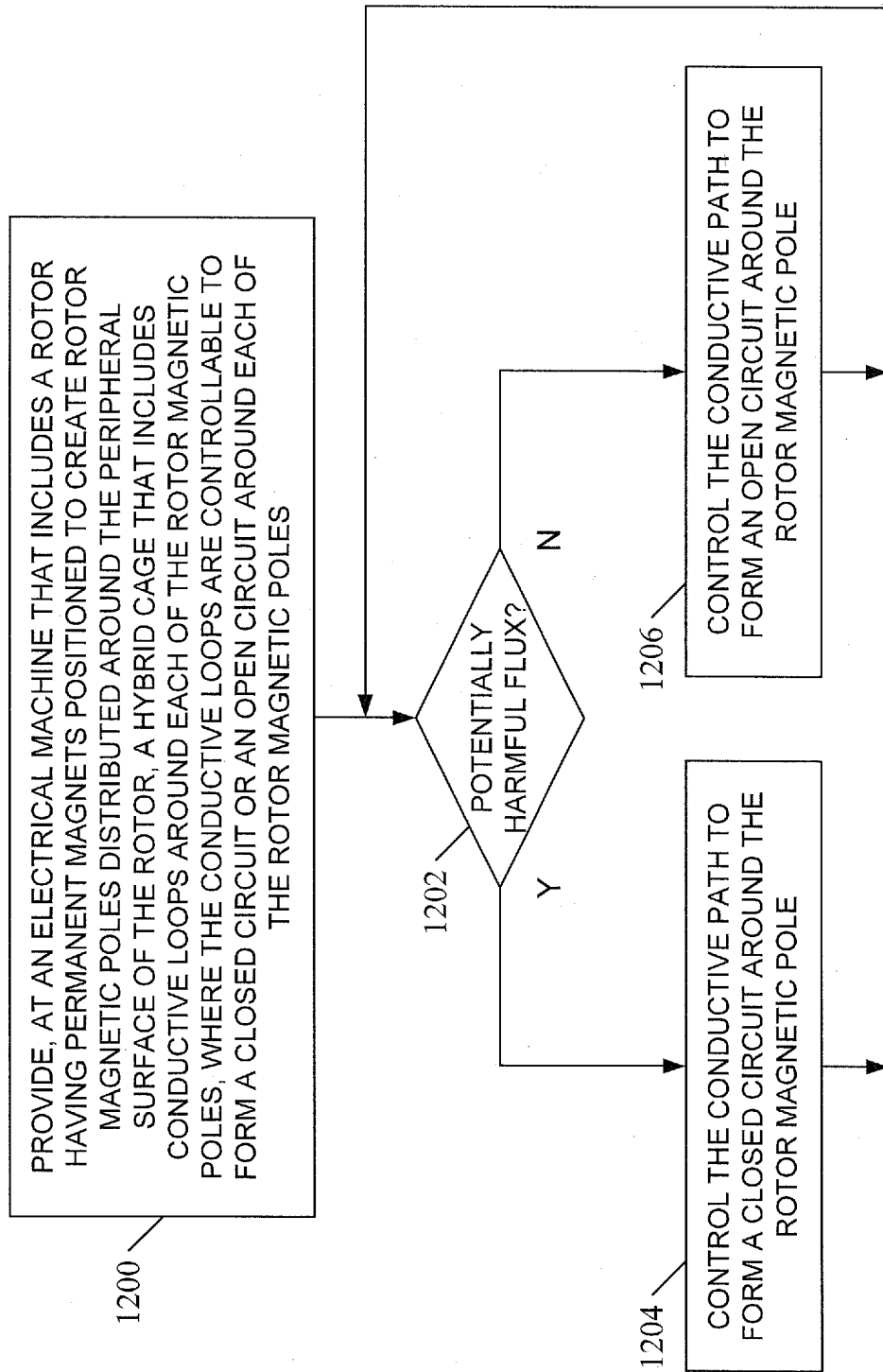


FIG. 12