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Lundquist et al.

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(54) **OPTICAL AMPLIFIER FOR MICROWAVE BURSTS**

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(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 10 days.

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(22) Filed: **Jan. 27, 2012**

(65) **Prior Publication Data**

US 2012/0213236 A1 Aug. 23, 2012

Related U.S. Application Data

(60) Provisional application No. 61/436,875, filed on Jan. 27, 2011.

(51) **Int. Cl.**
H01S 3/10 (2006.01)

(52) **U.S. Cl.**
USPC **372/25**; 372/29.02; 372/30; 372/99;
372/101

(58) **Field of Classification Search**
USPC 359/347, 348; 372/25, 29.02, 30, 99
See application file for complete search history.

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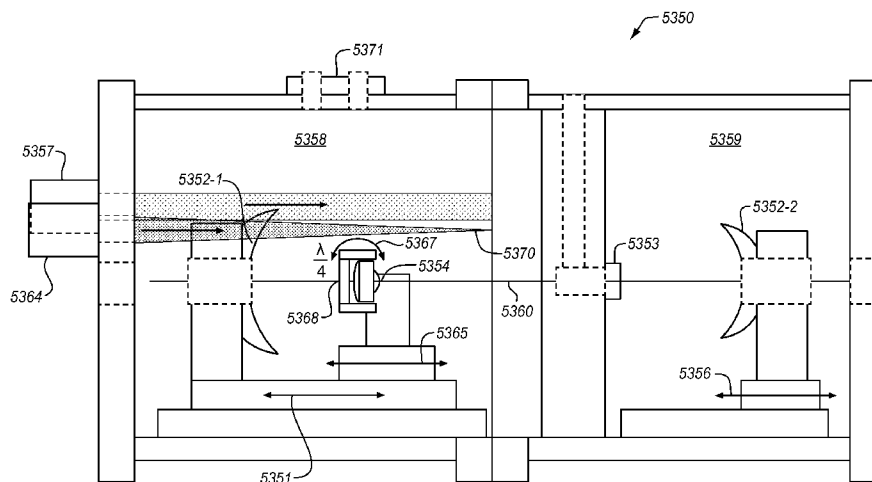
Primary Examiner — Dung Nguyen

(74) *Attorney, Agent, or Firm* — Duft Bornsen & Fettig LLP;
Gregory T. Fettig

(57) **ABSTRACT**

The various laser architectures described herein provide increased gain of optical energy as well as compensation of optical phase distortions in a thin disk gain medium. An optical amplifier presented herein provides for scalable high energy extraction and gains based on a number of passes of the signal beam through a gain medium. Multiple, spatially separate, optical paths may also be passed through the same gain region to provide gain clearing by splitting off a small percentage of an output pulse and sending it back through the amplifier along a slightly different path. By clearing out the residual gain, uniform signal amplitudes can be obtained.

20 Claims, 58 Drawing Sheets



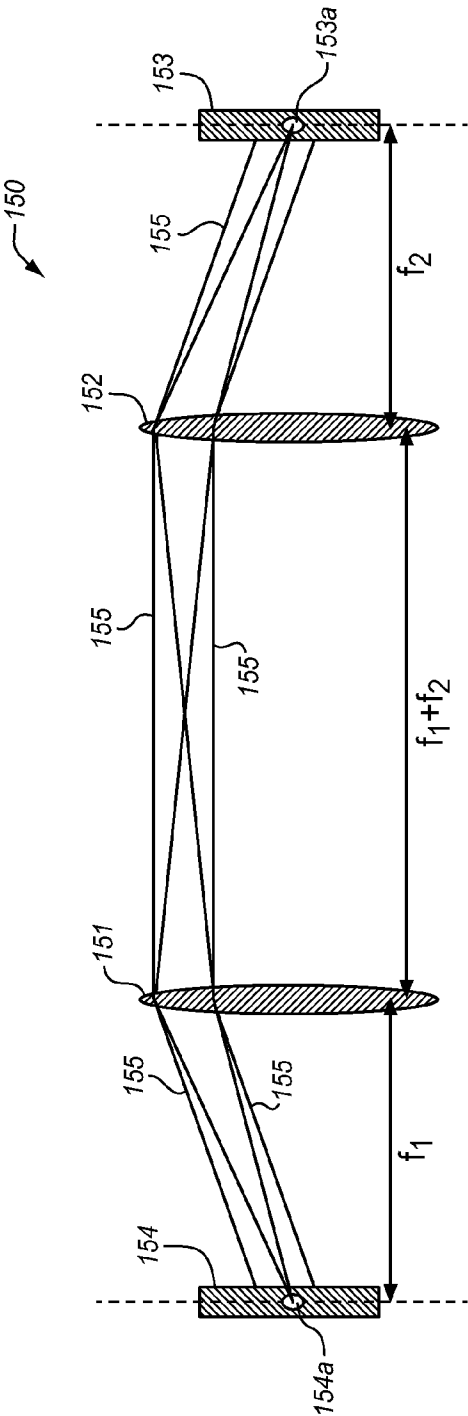


FIG. 1A

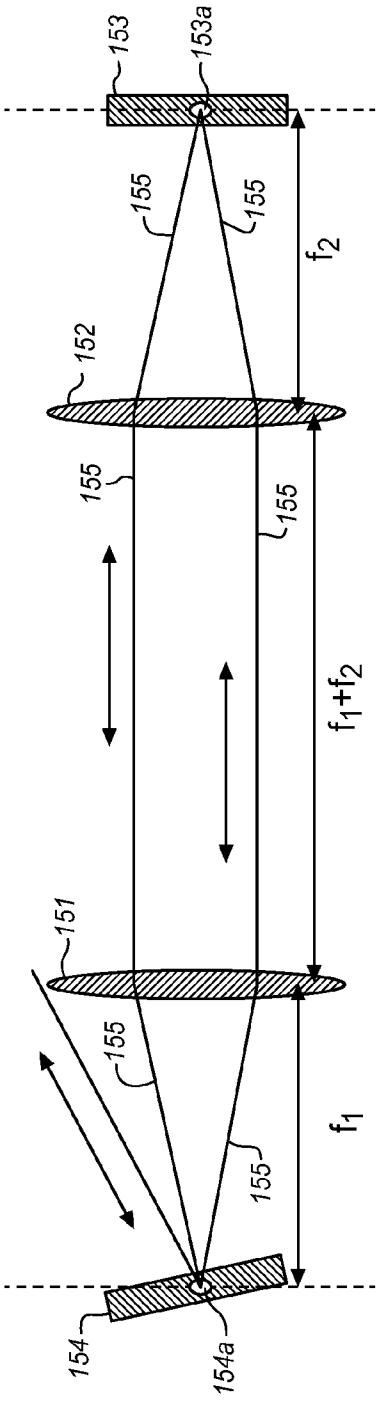


FIG. 1B

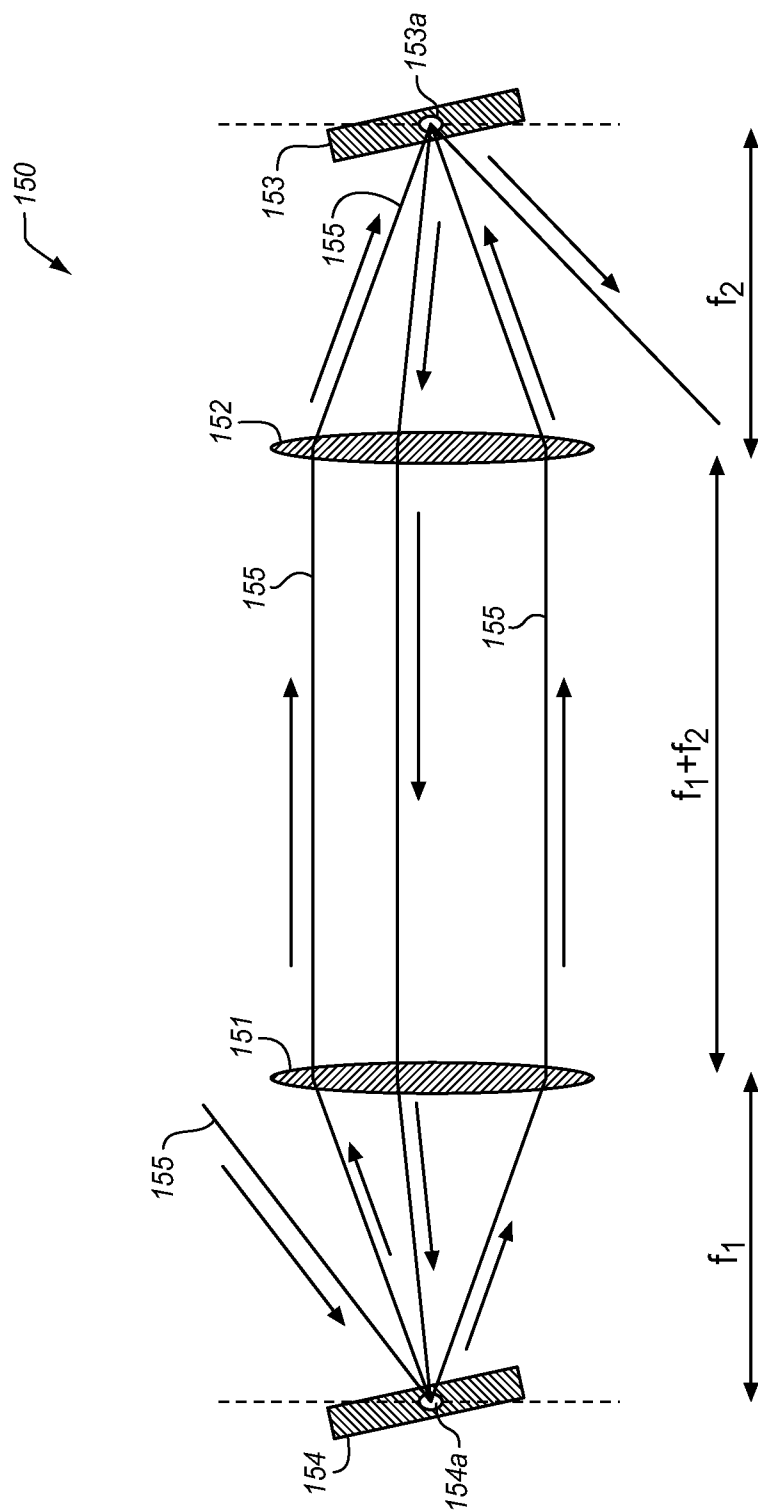


FIG. 2

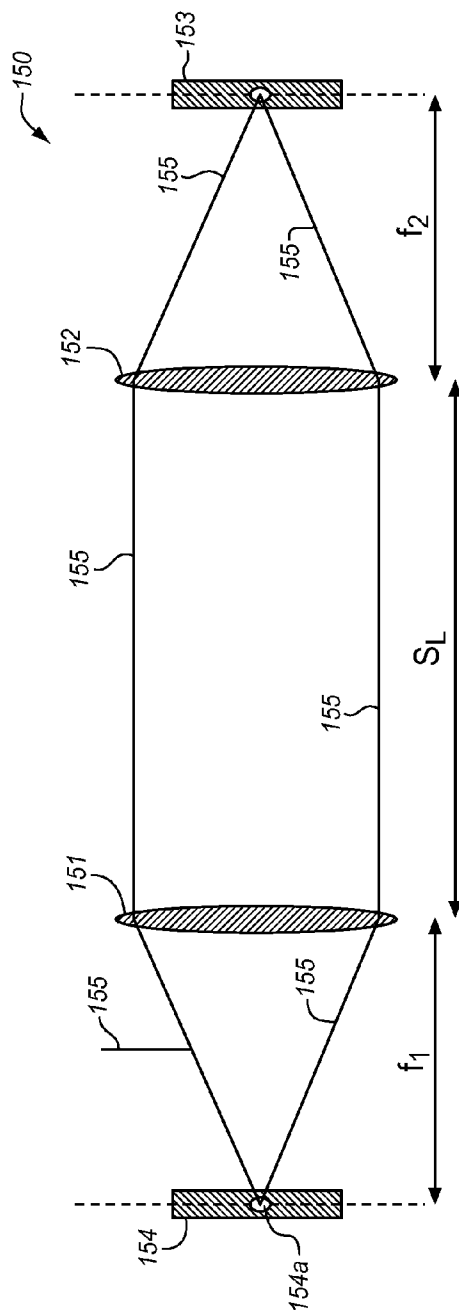


FIG. 3A

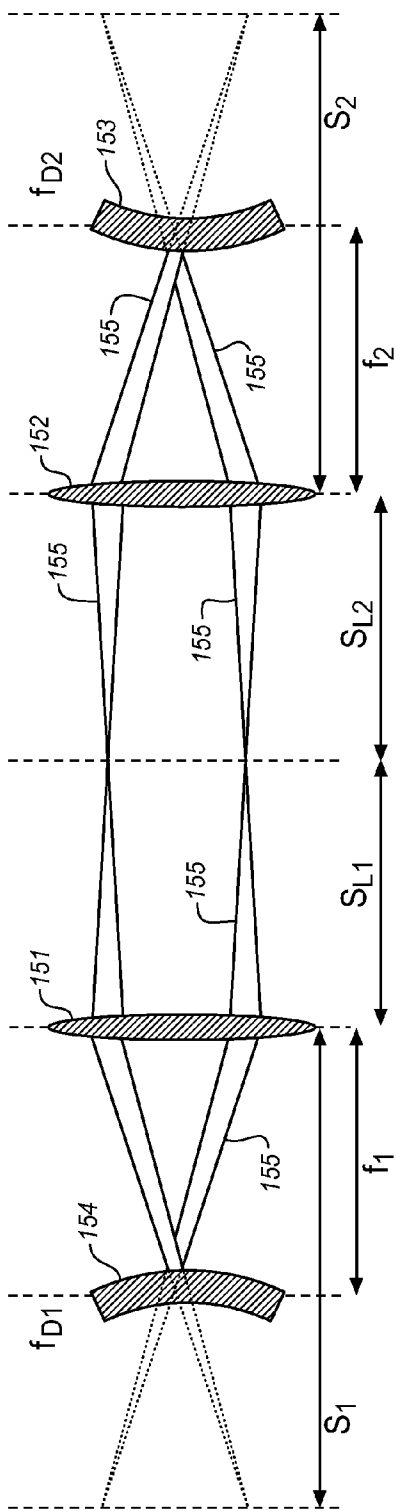


FIG. 3B

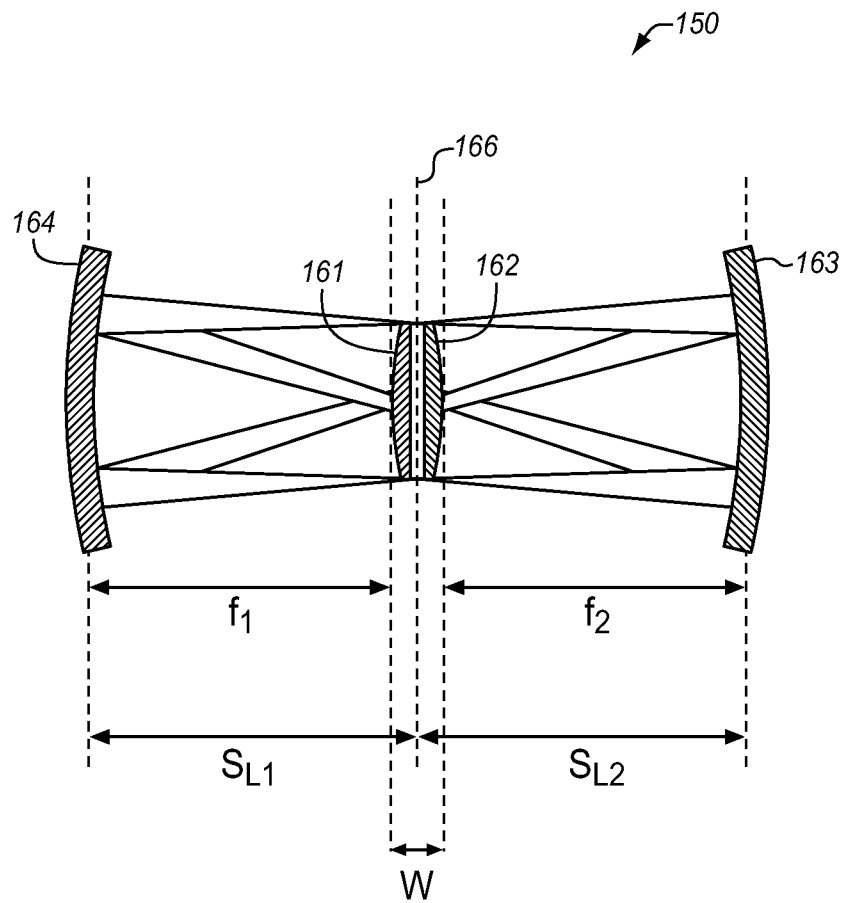


FIG. 4A

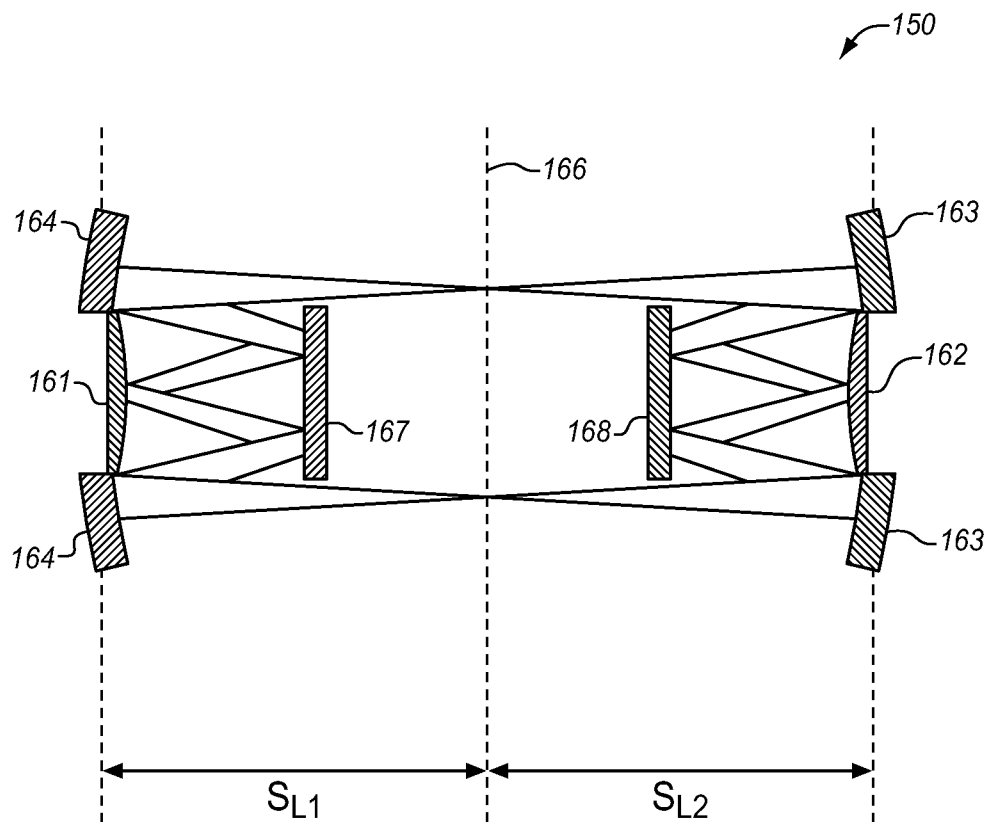


FIG. 4B

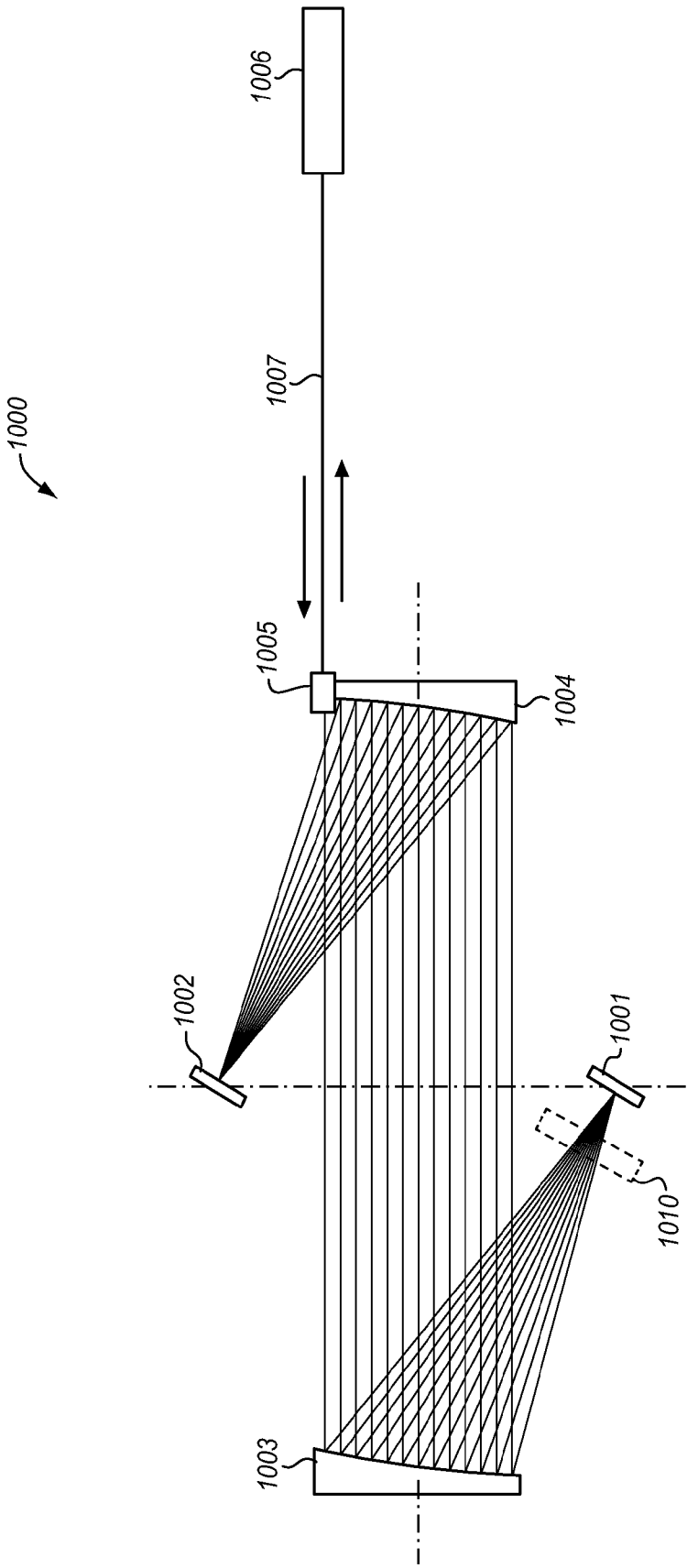


FIG. 5

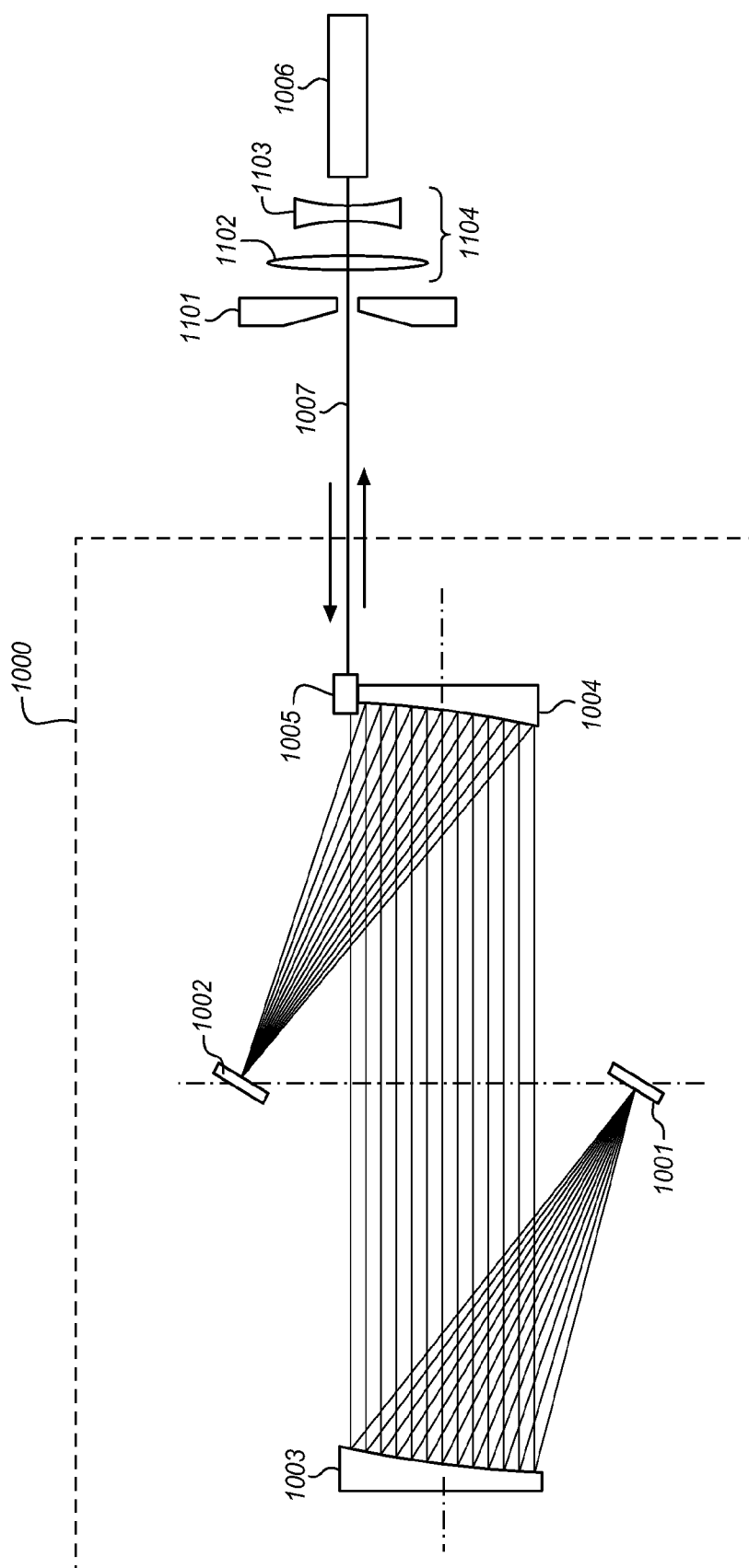


FIG. 6

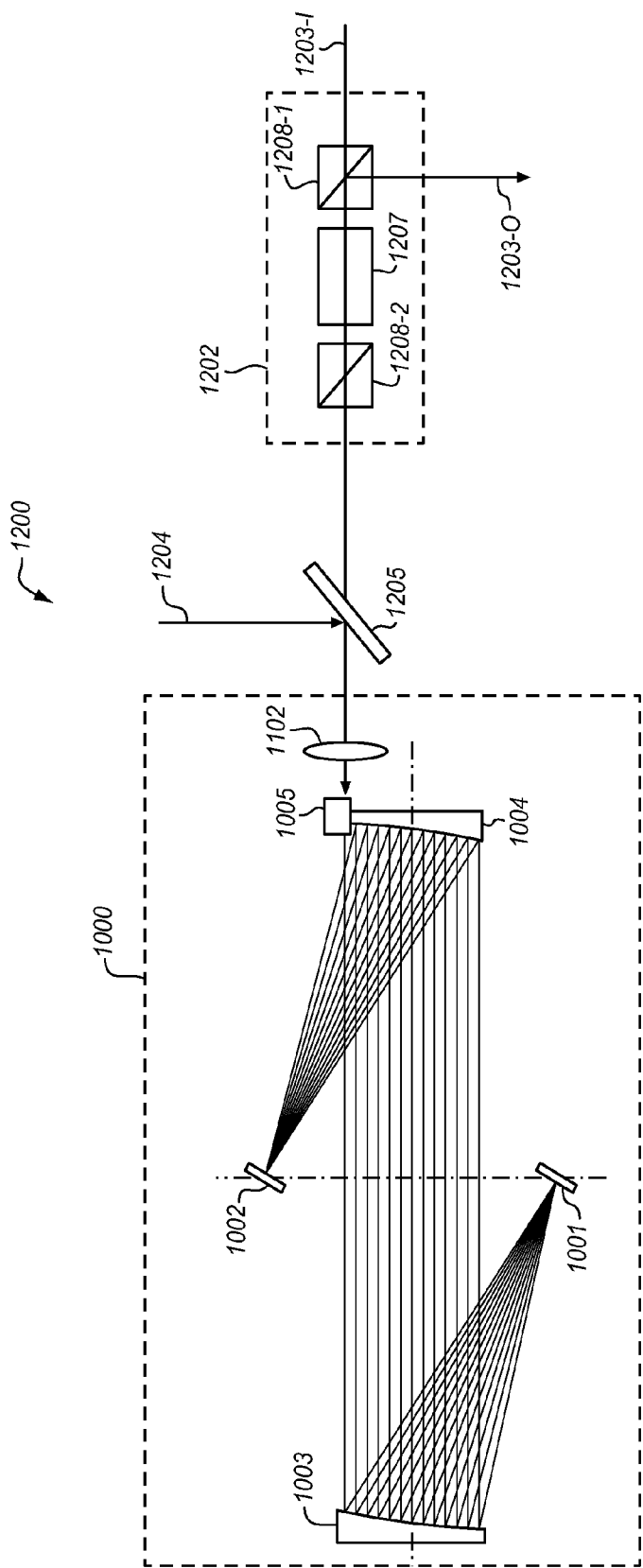


FIG. 7

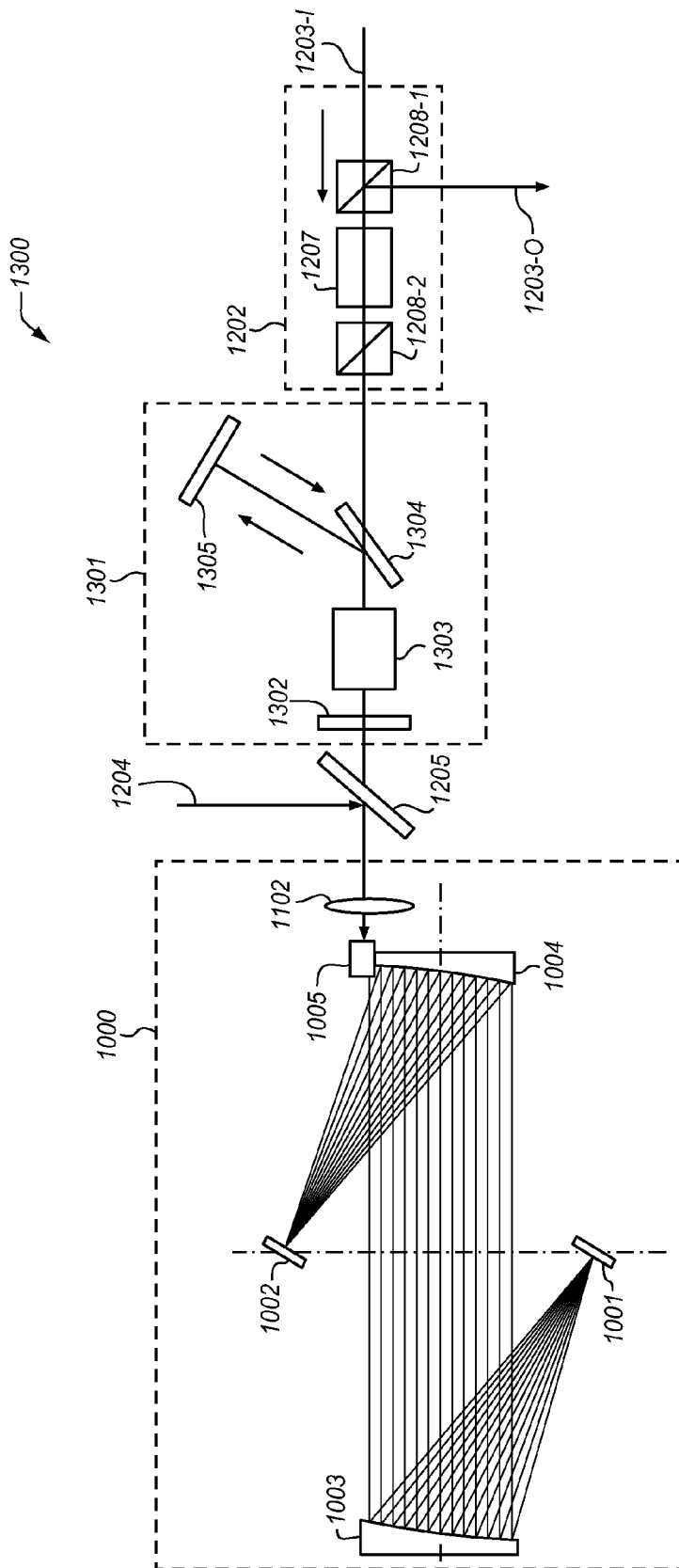


FIG. 8

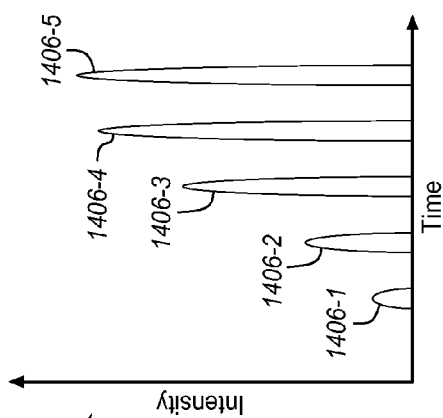


FIG. 9B

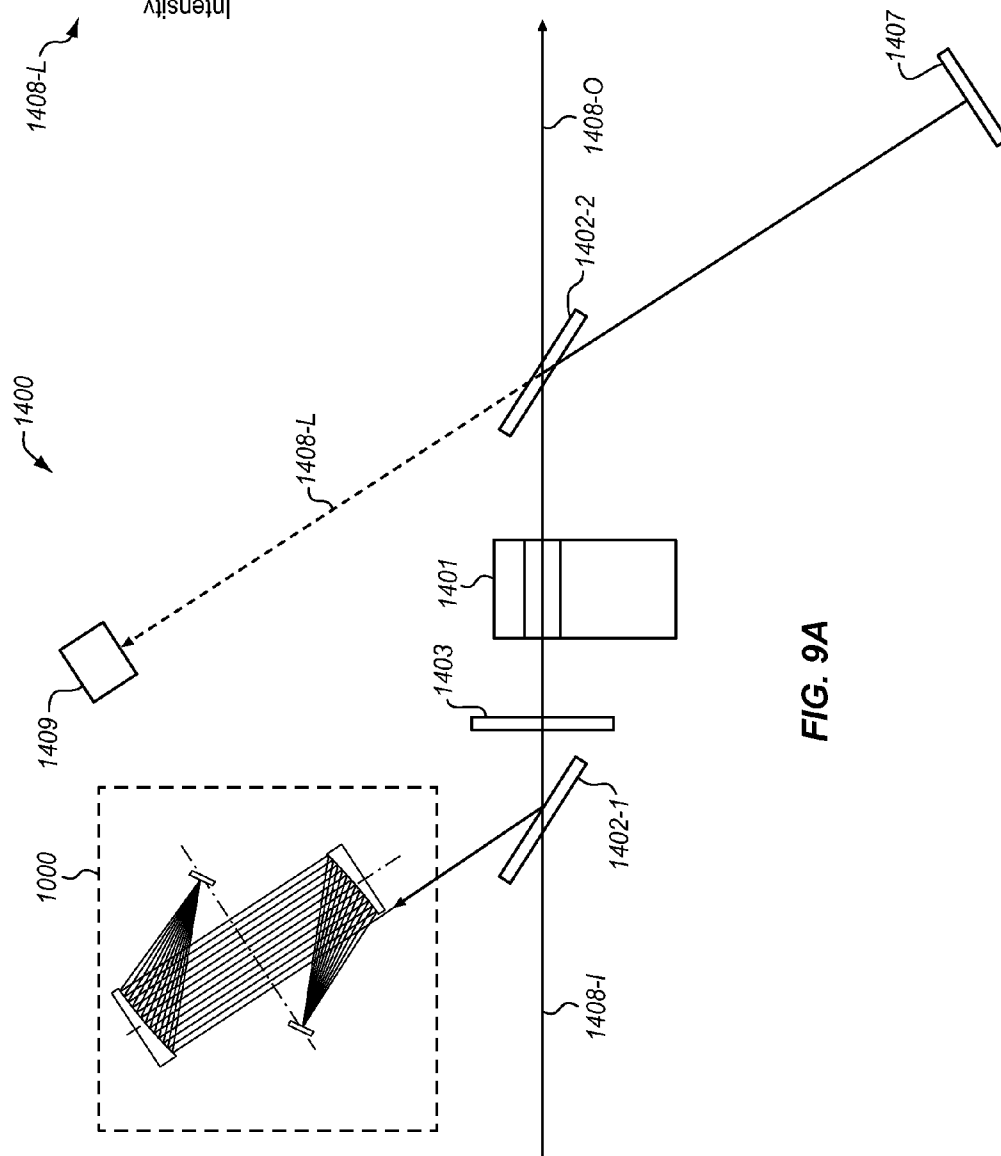


FIG. 9A

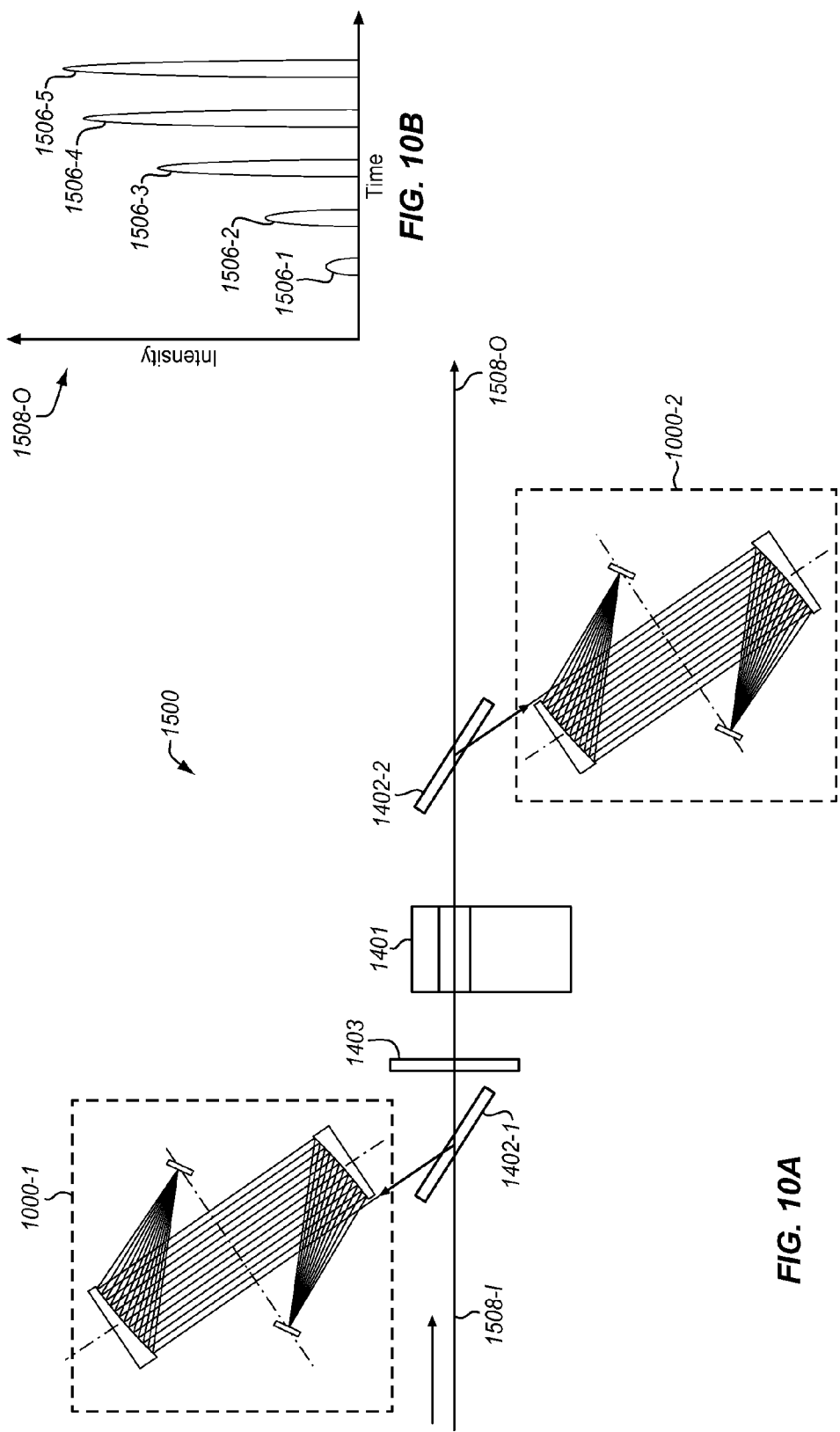
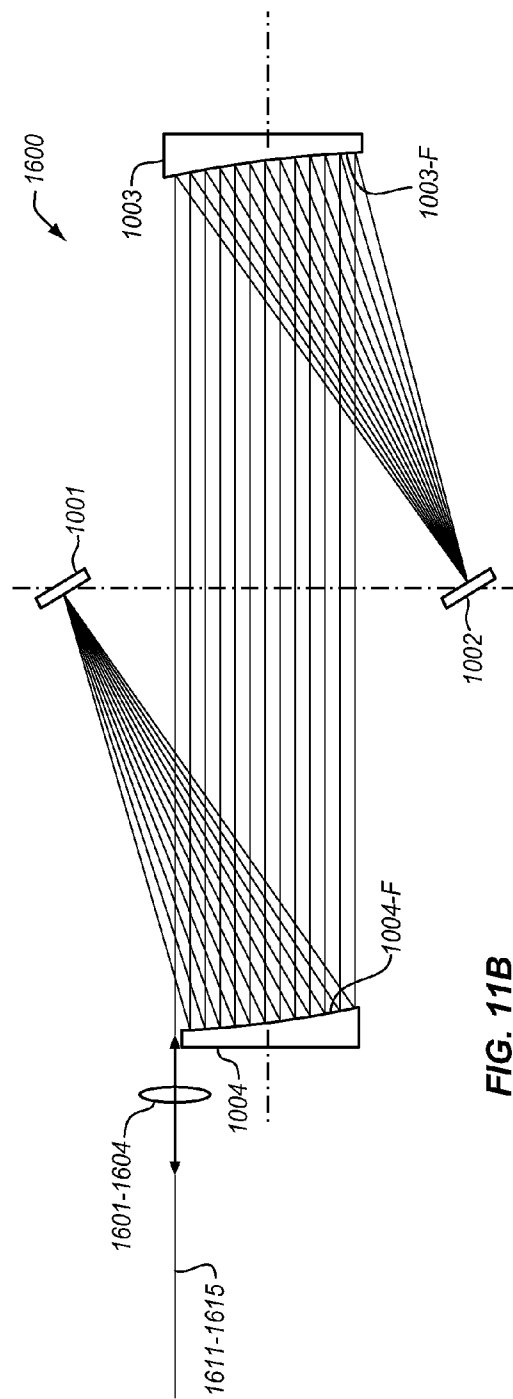
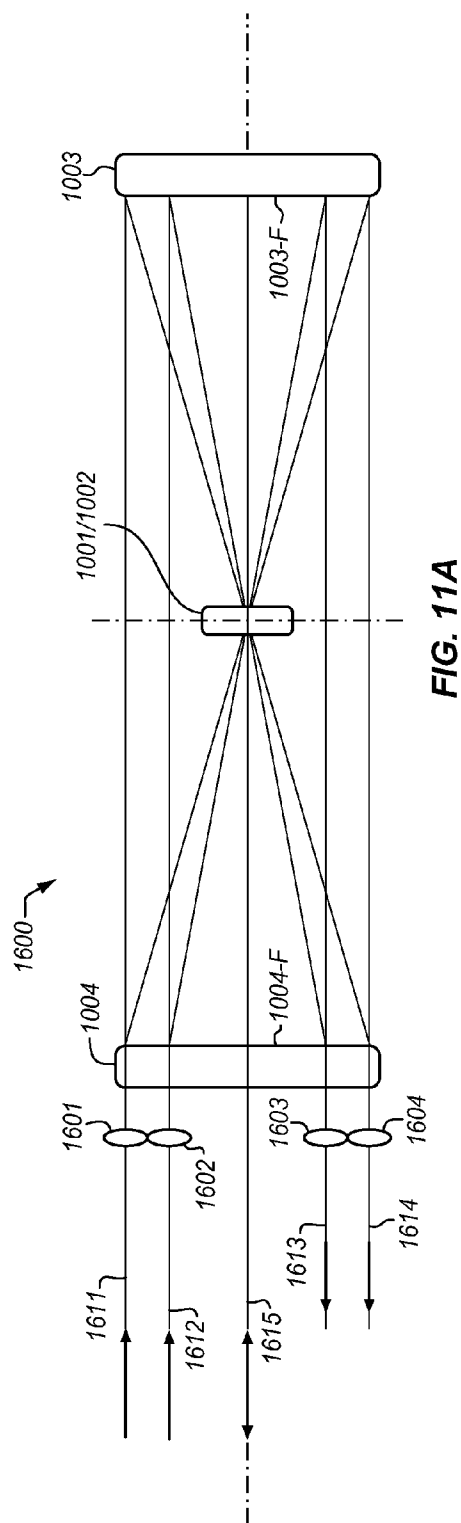


FIG. 10A

FIG. 10B



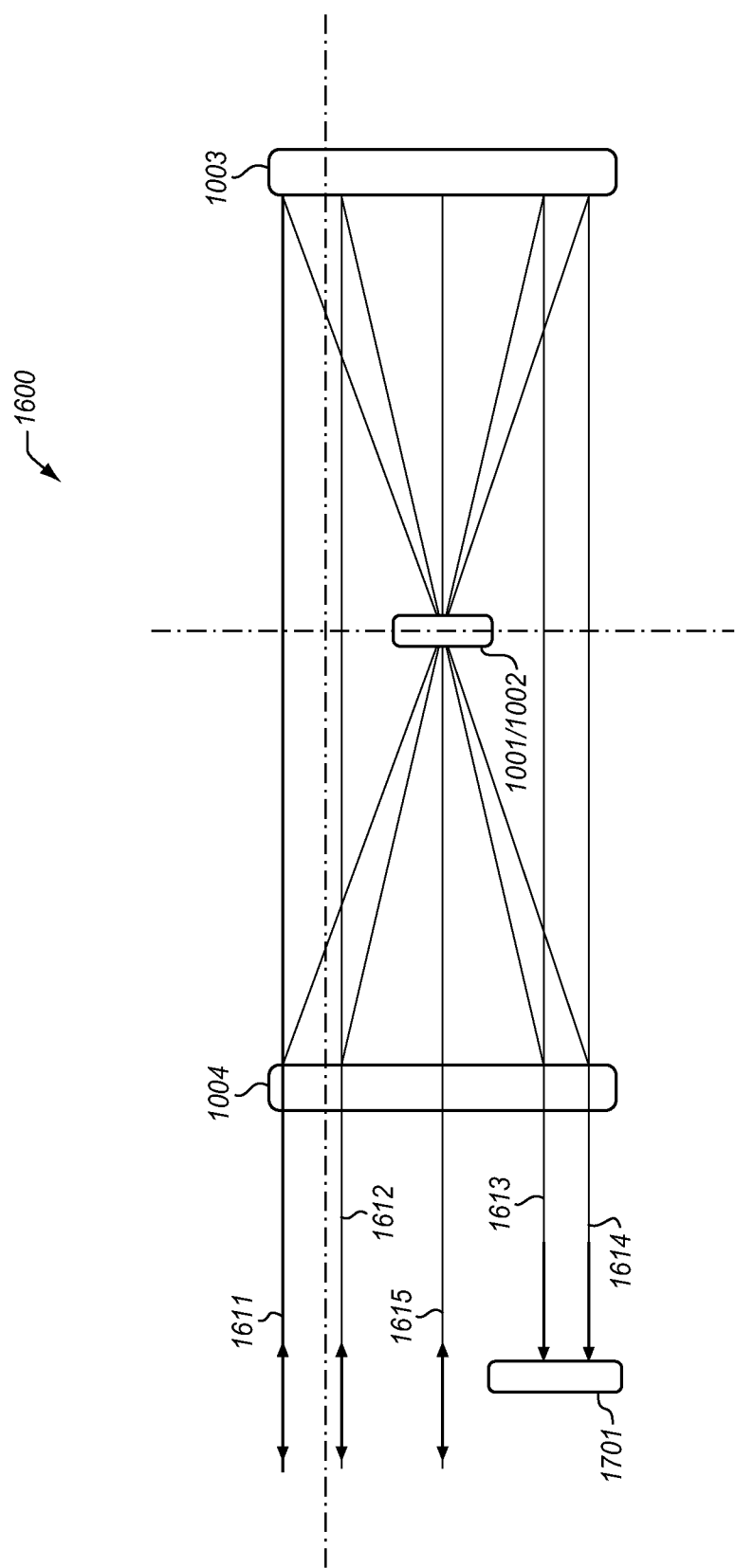


FIG. 12

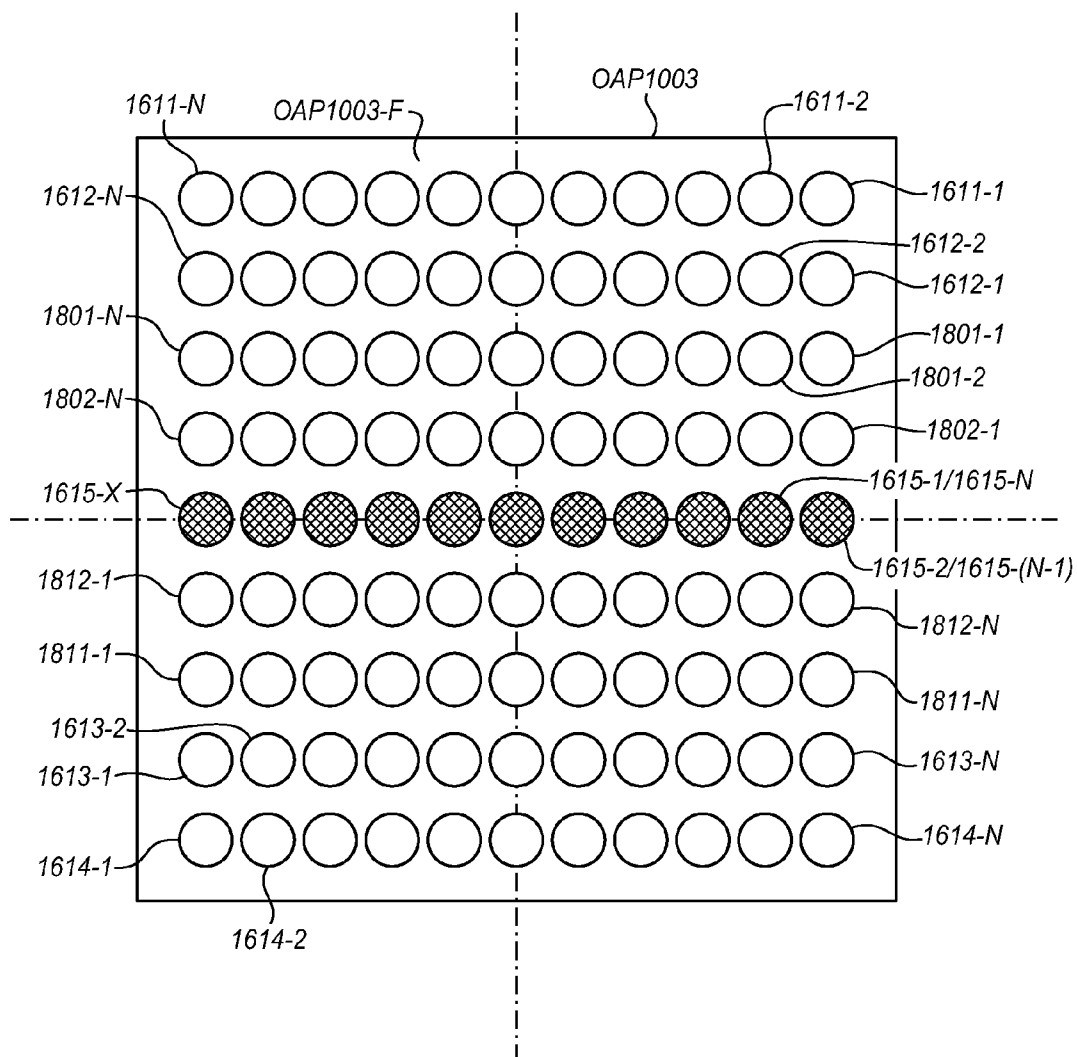


FIG. 13

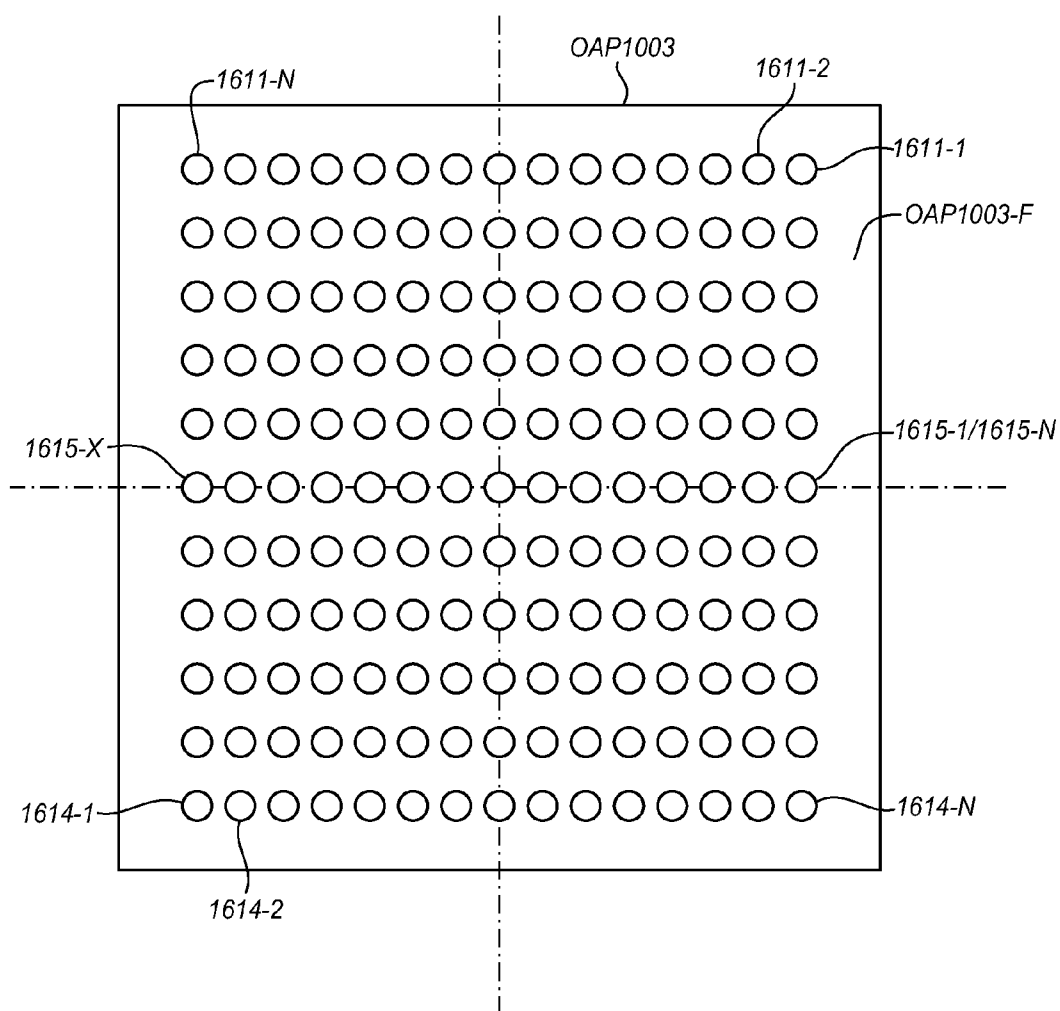


FIG. 14

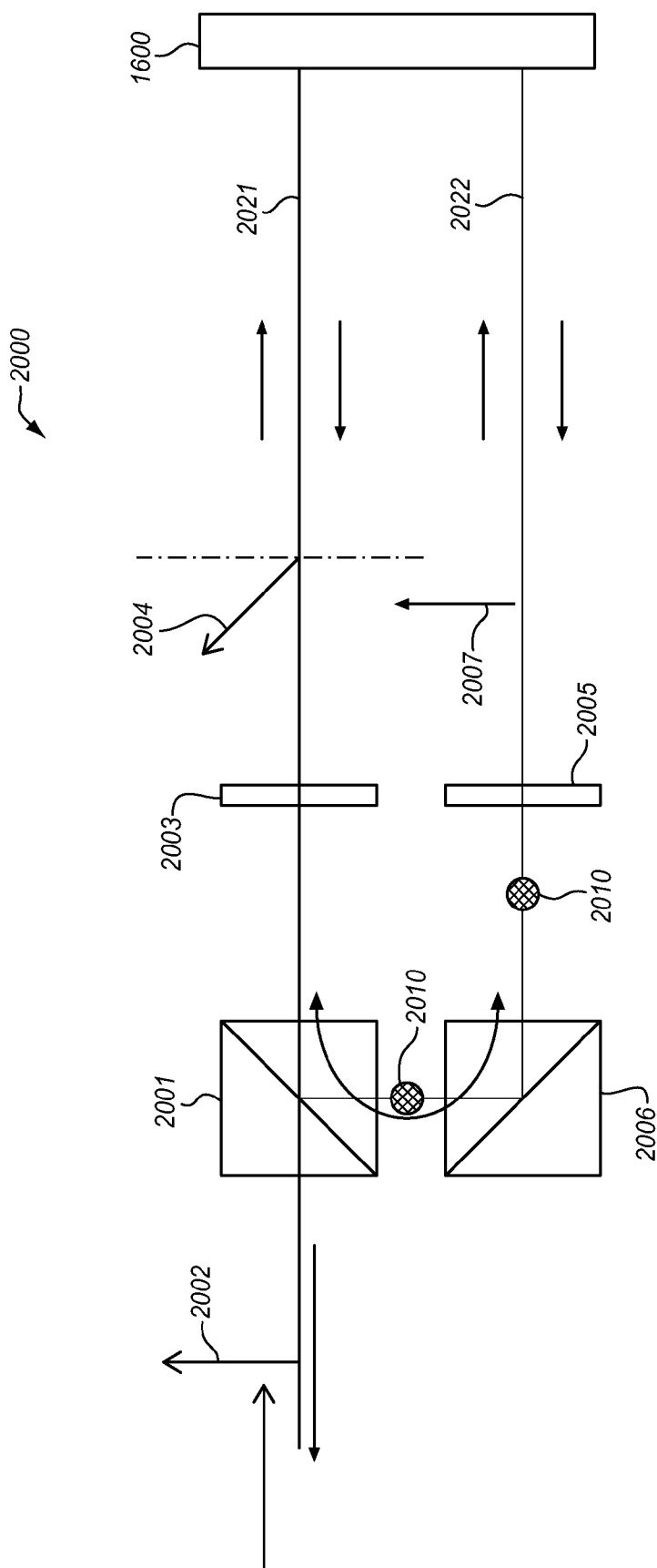


FIG. 15

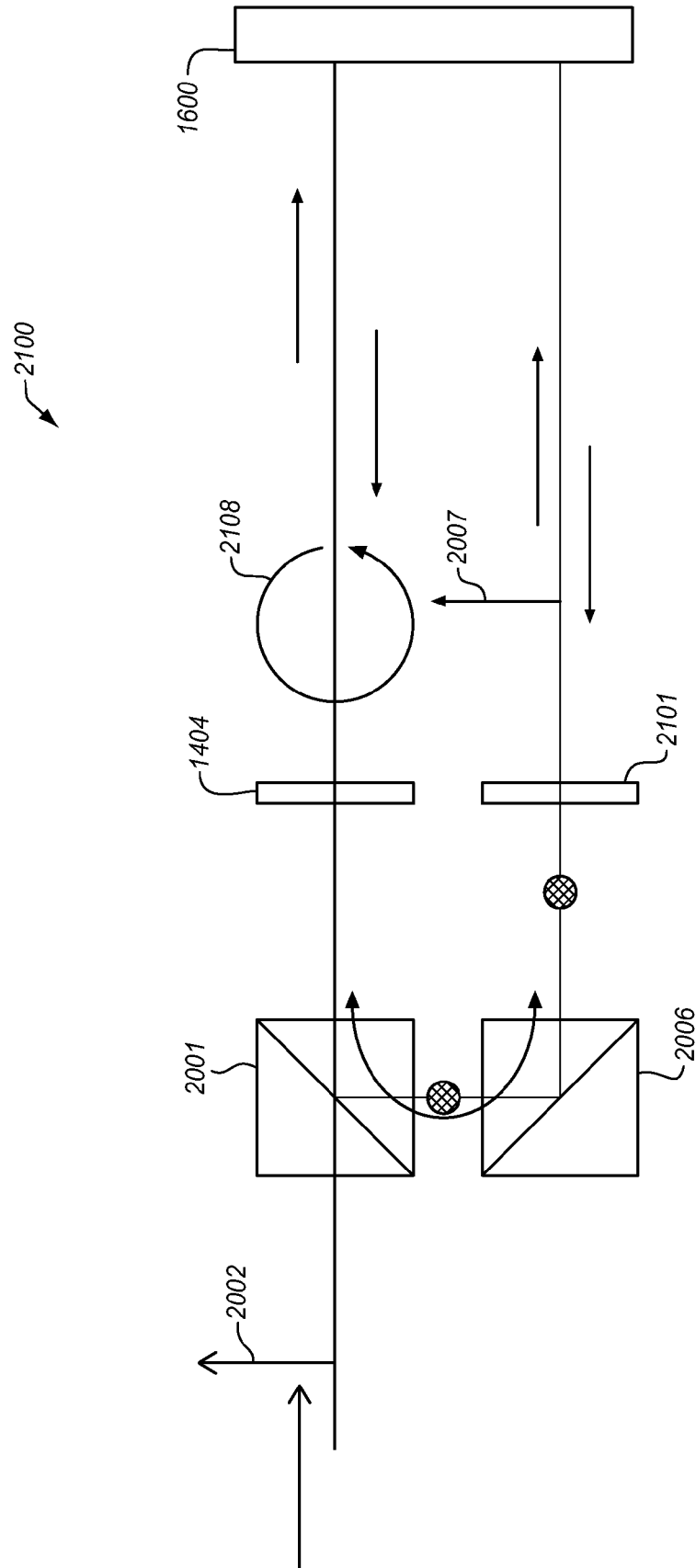


FIG. 16

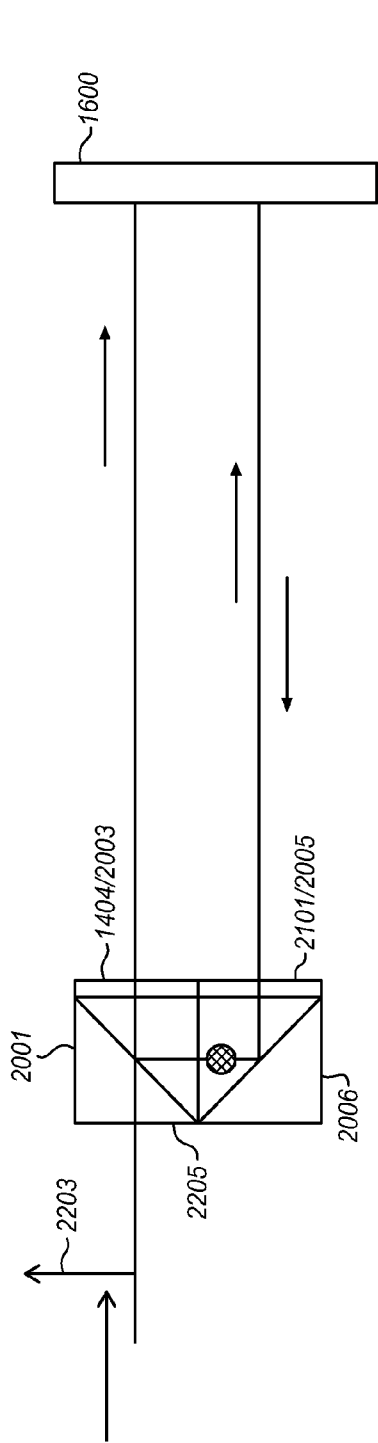


FIG. 17

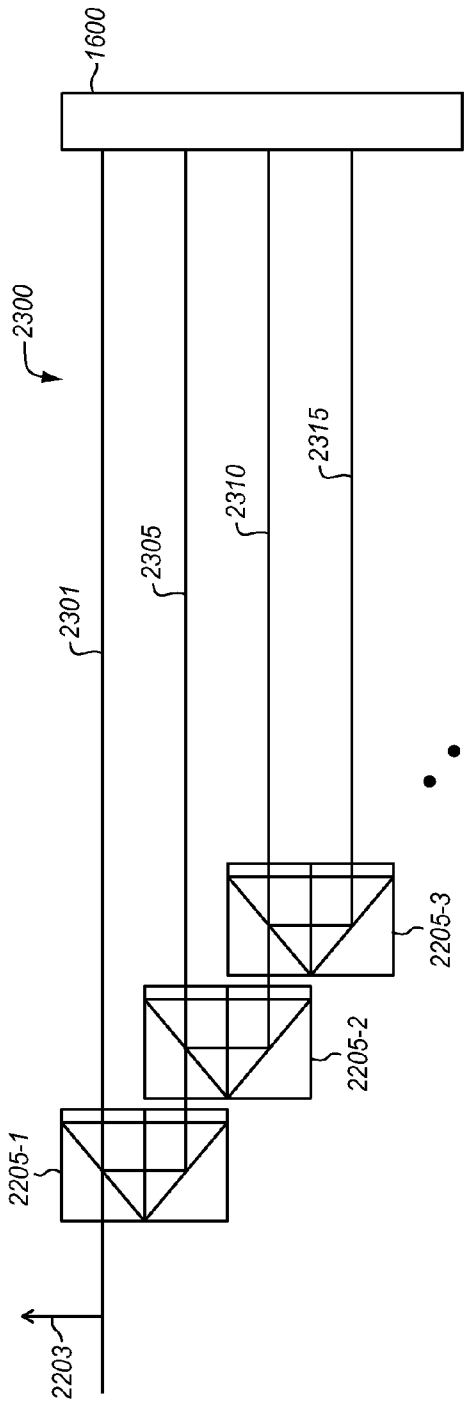


FIG. 18

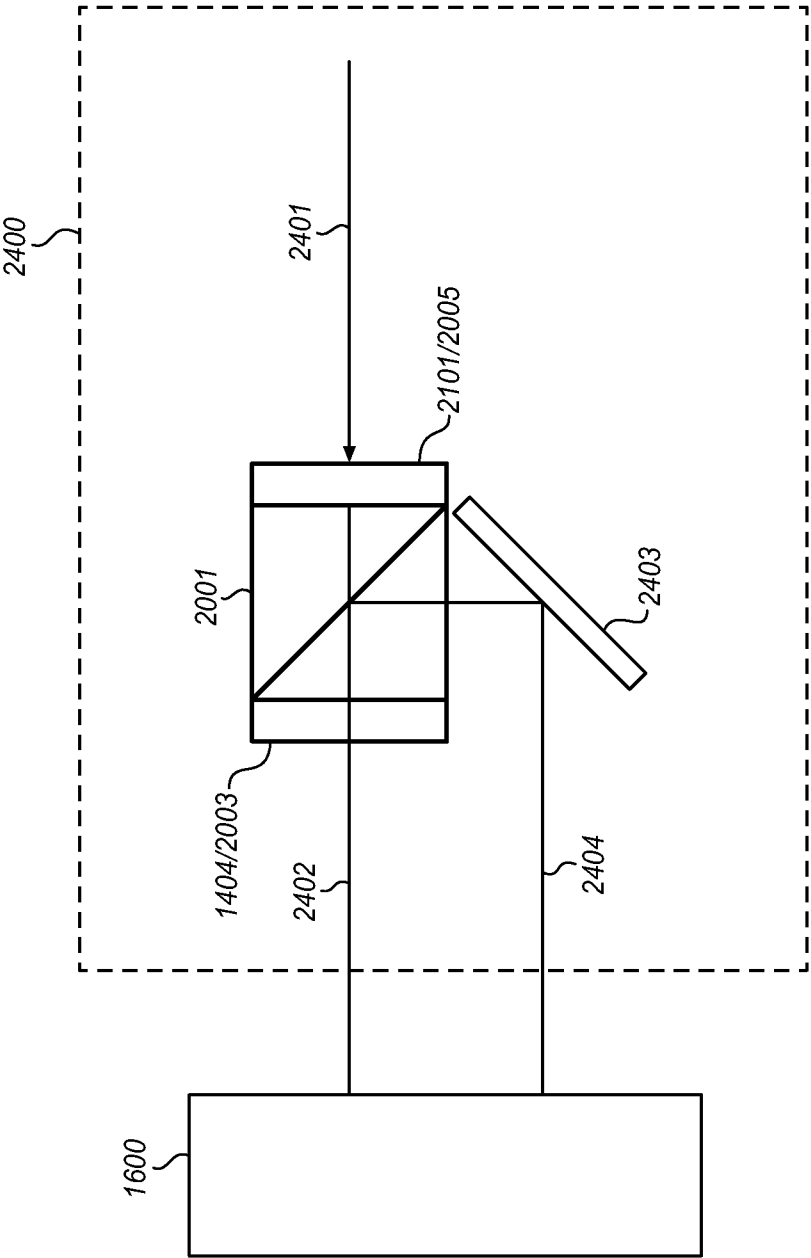
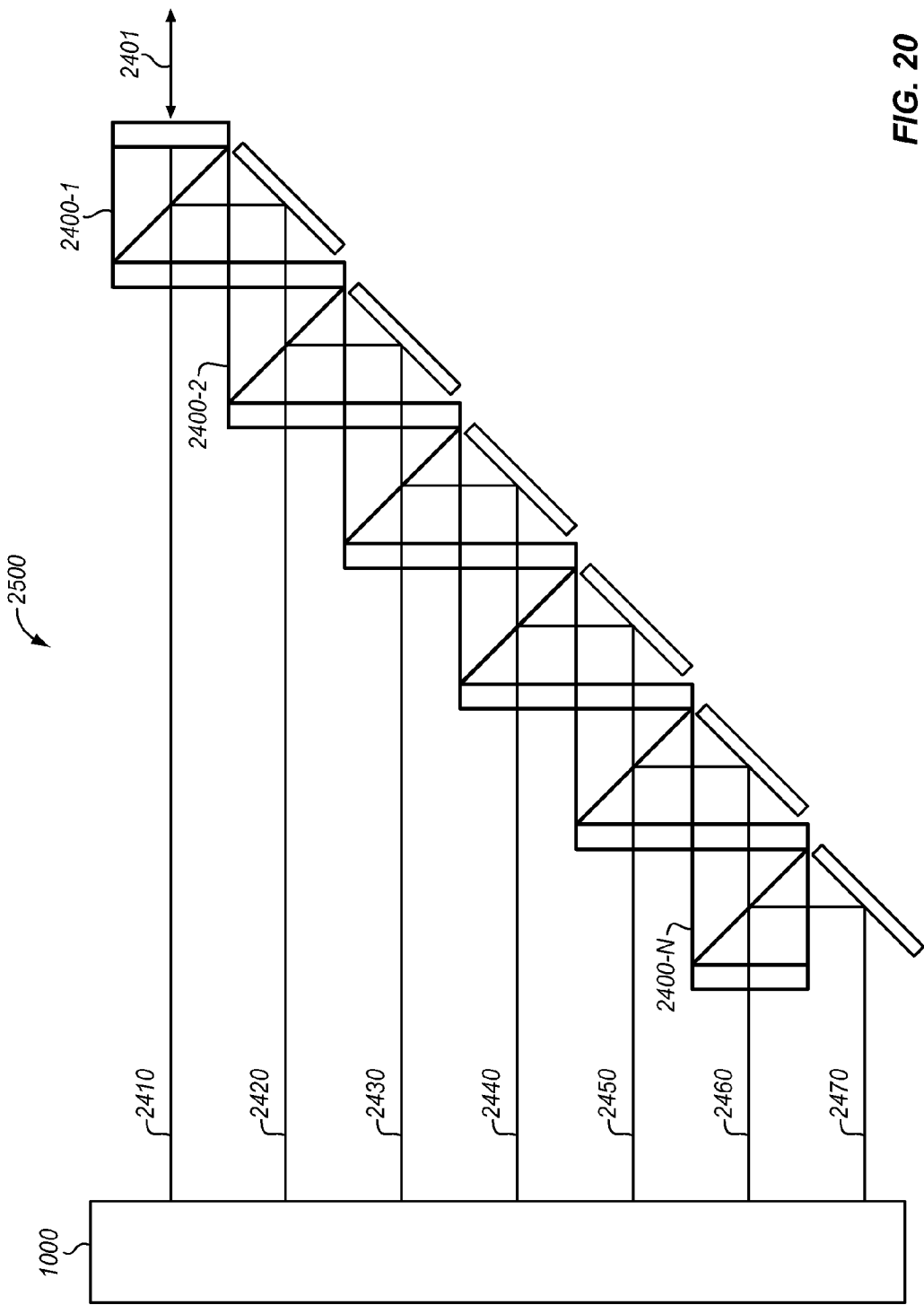


FIG. 19



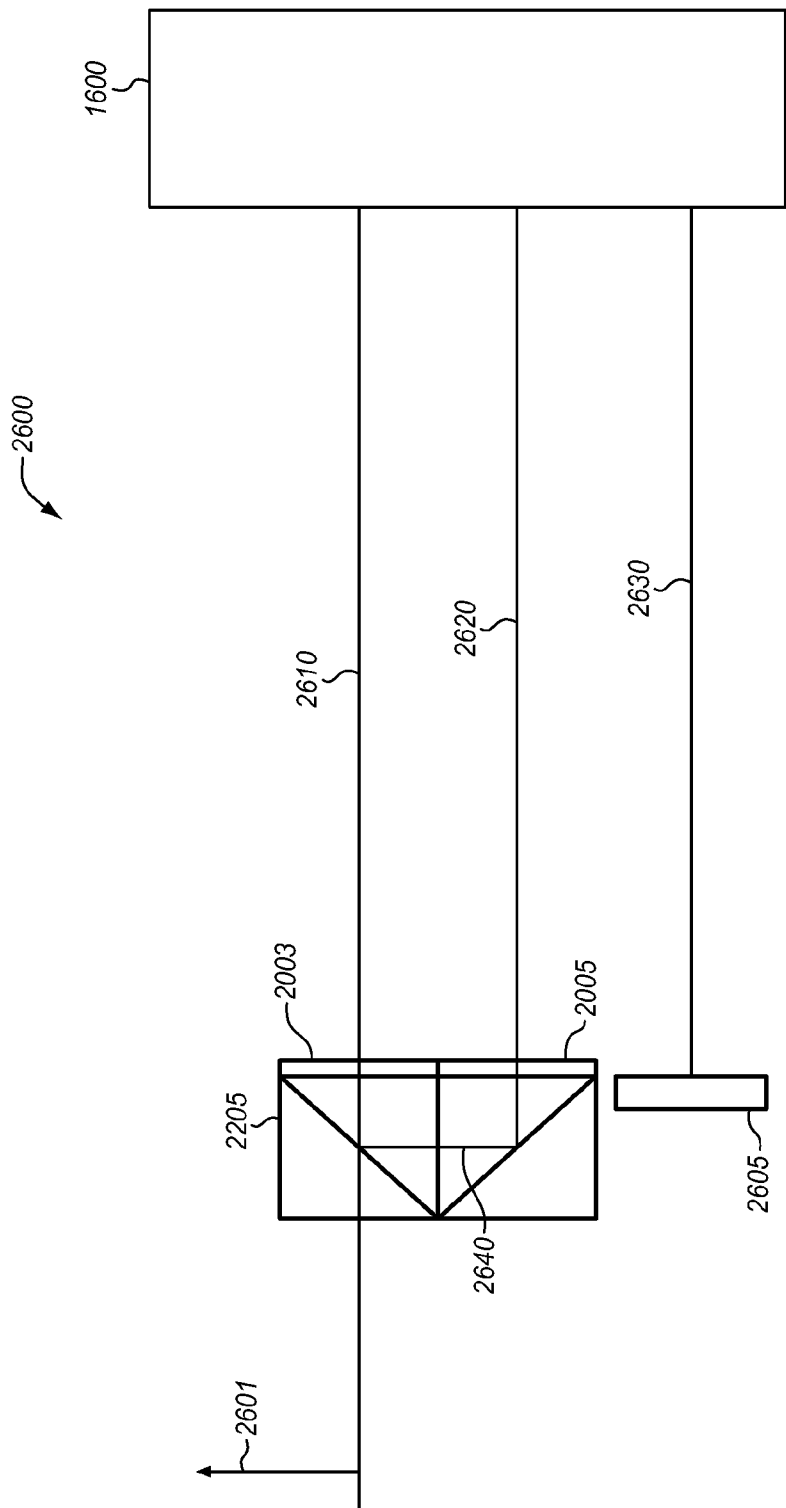
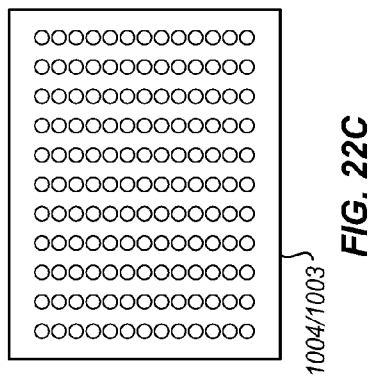
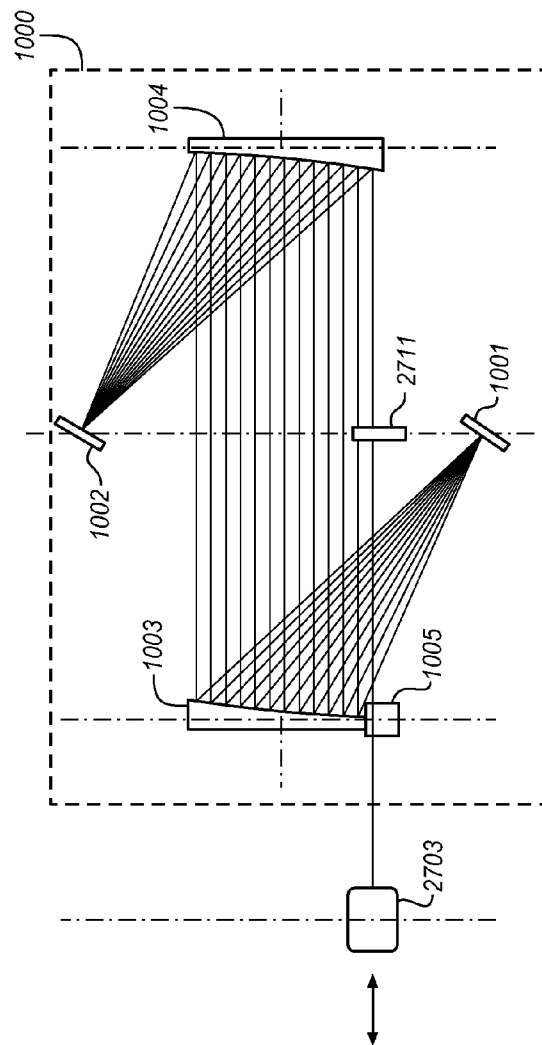
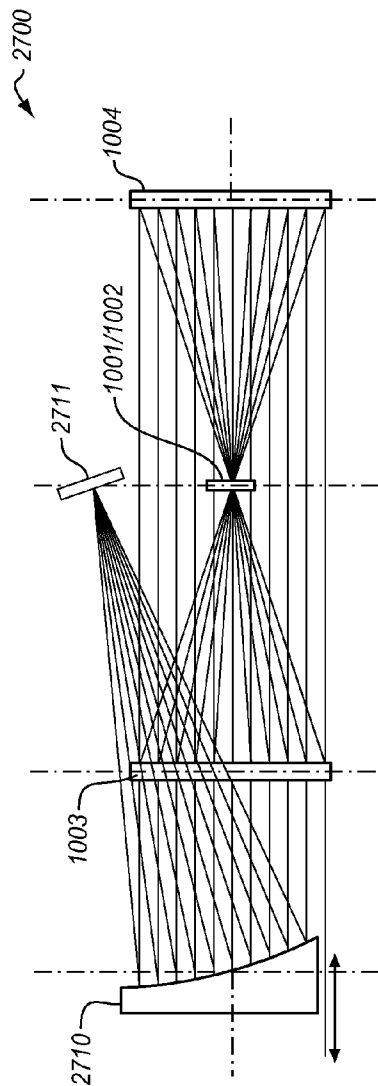
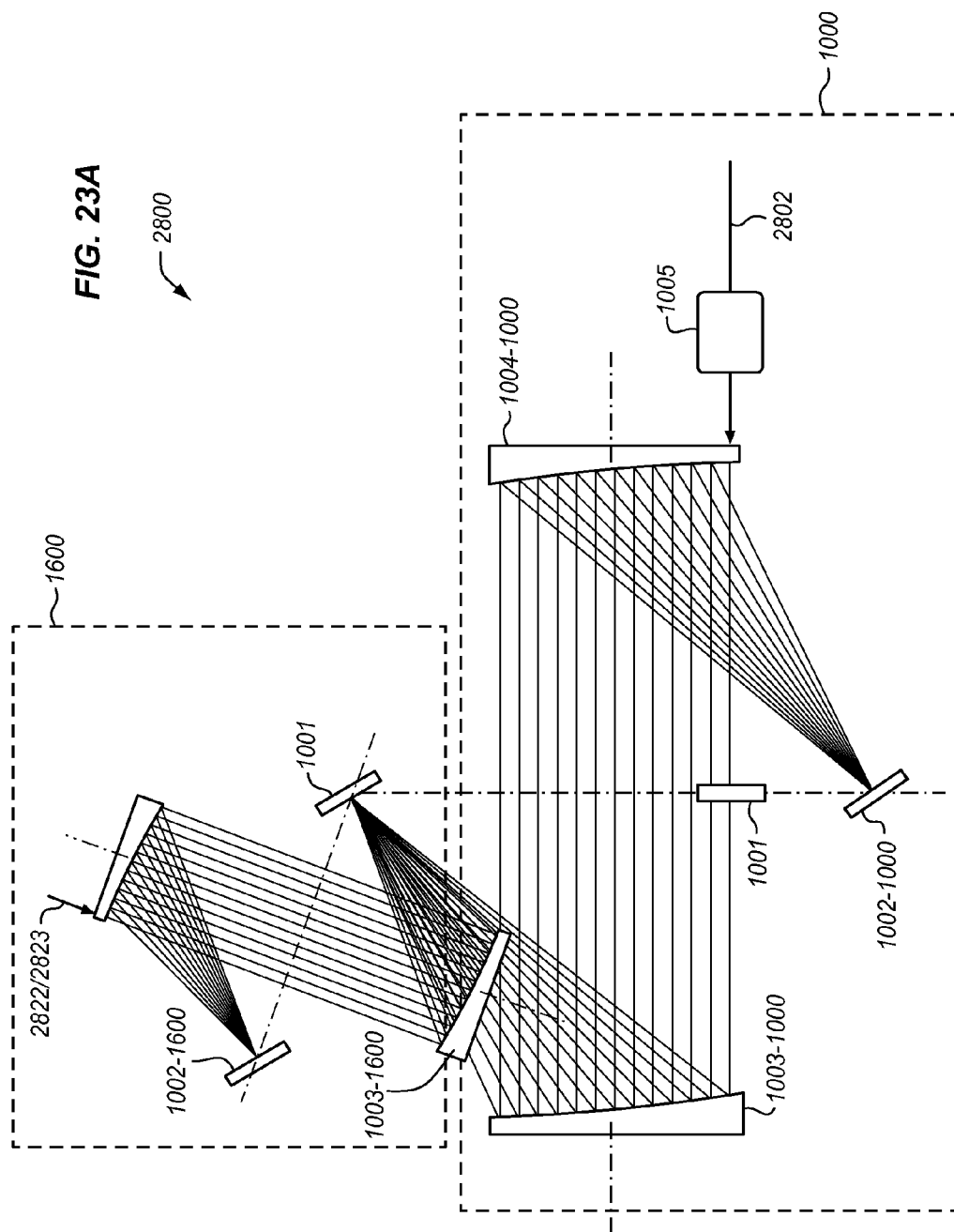


FIG. 21





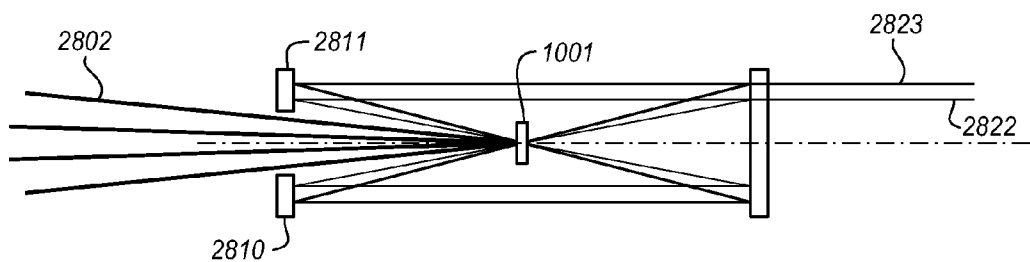


FIG. 23B

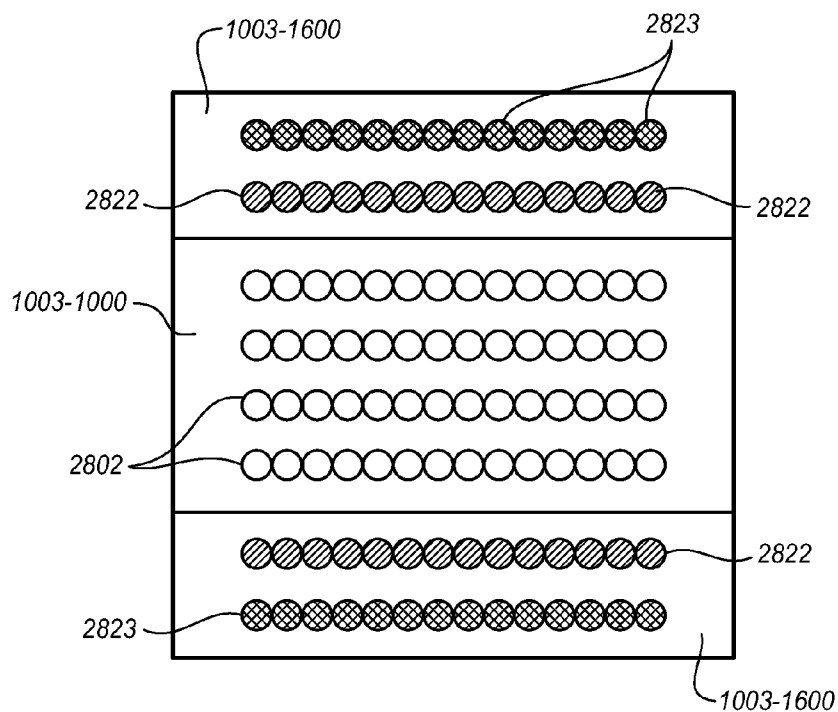


FIG. 23C

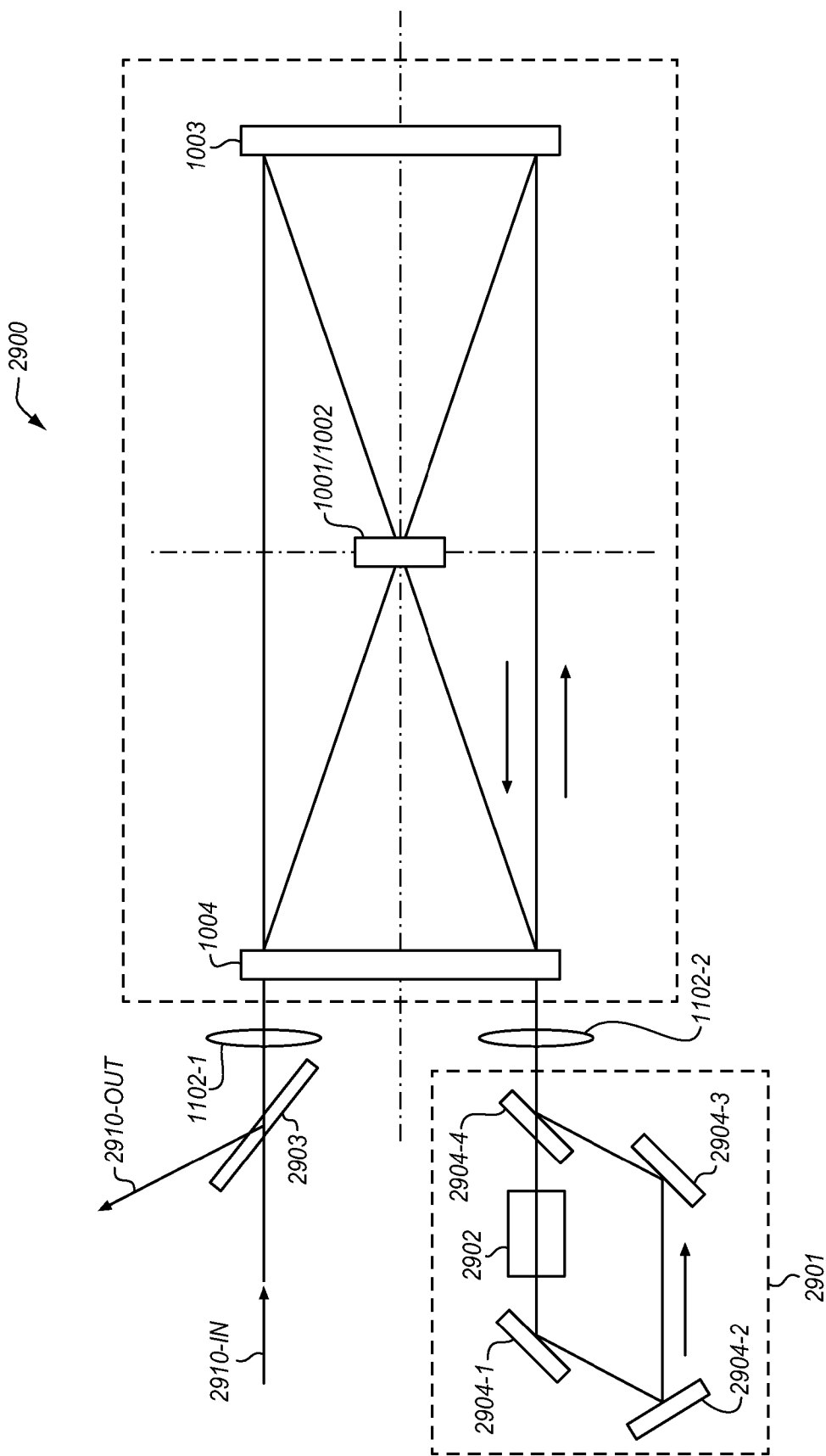


FIG. 24

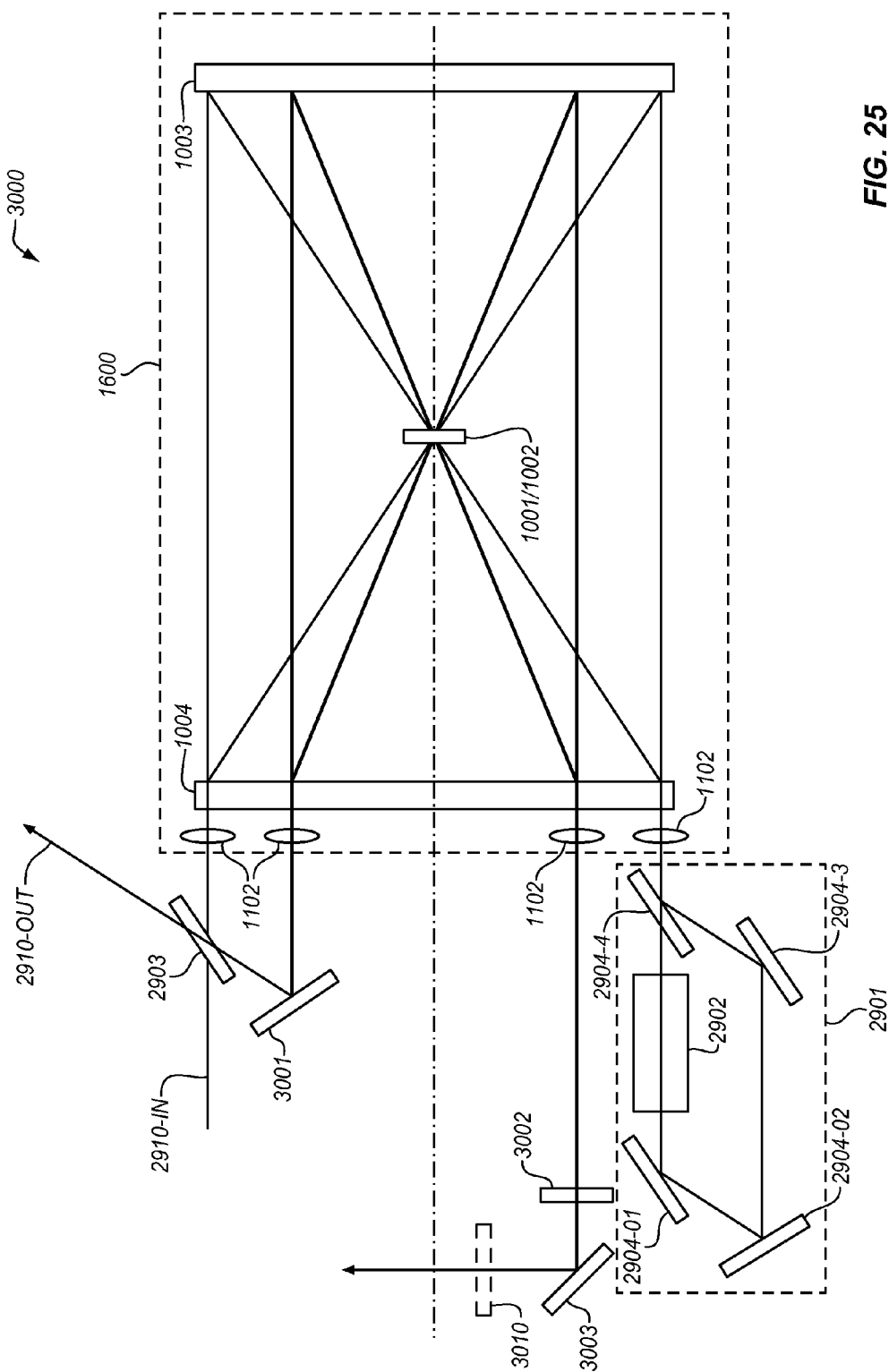


FIG. 25

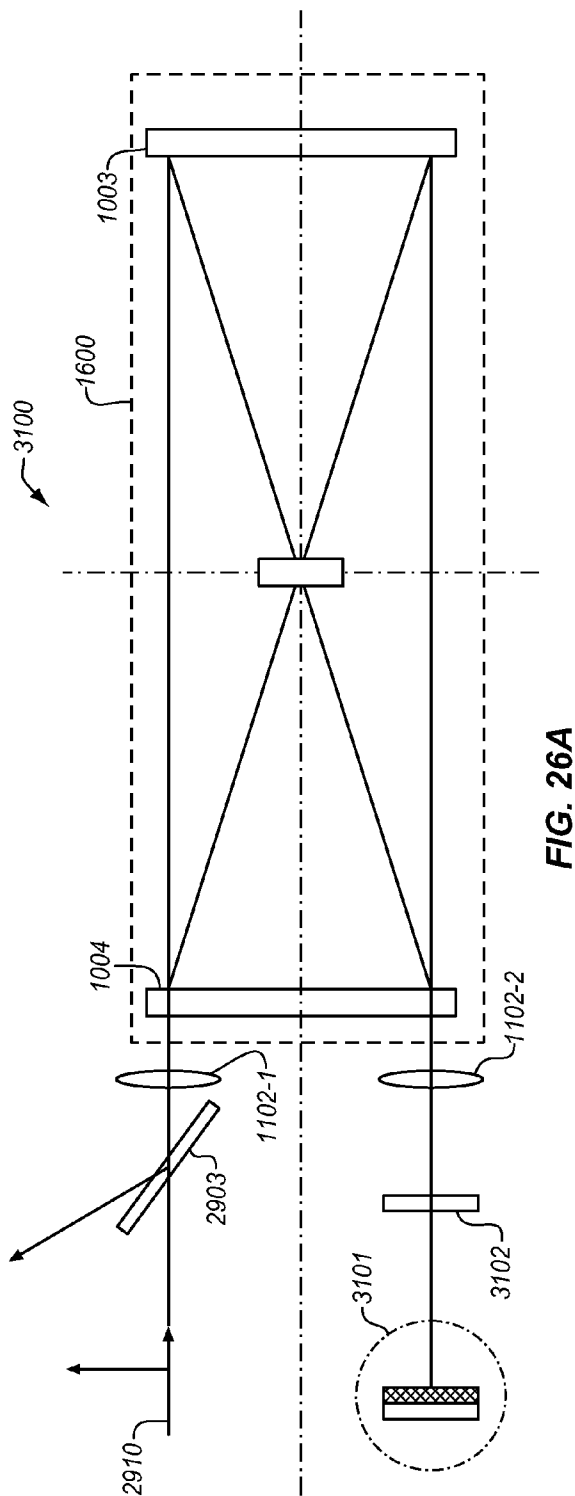


FIG. 26A

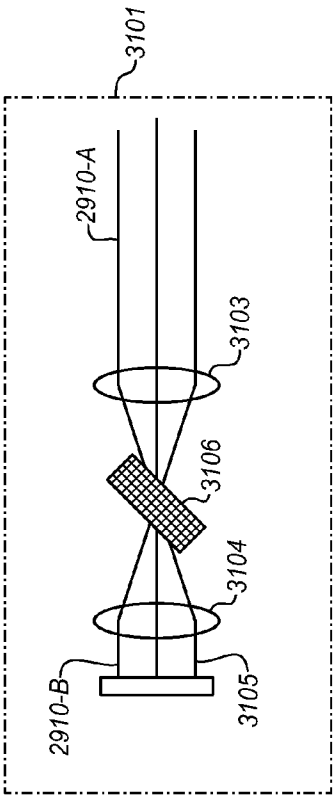


FIG. 26B

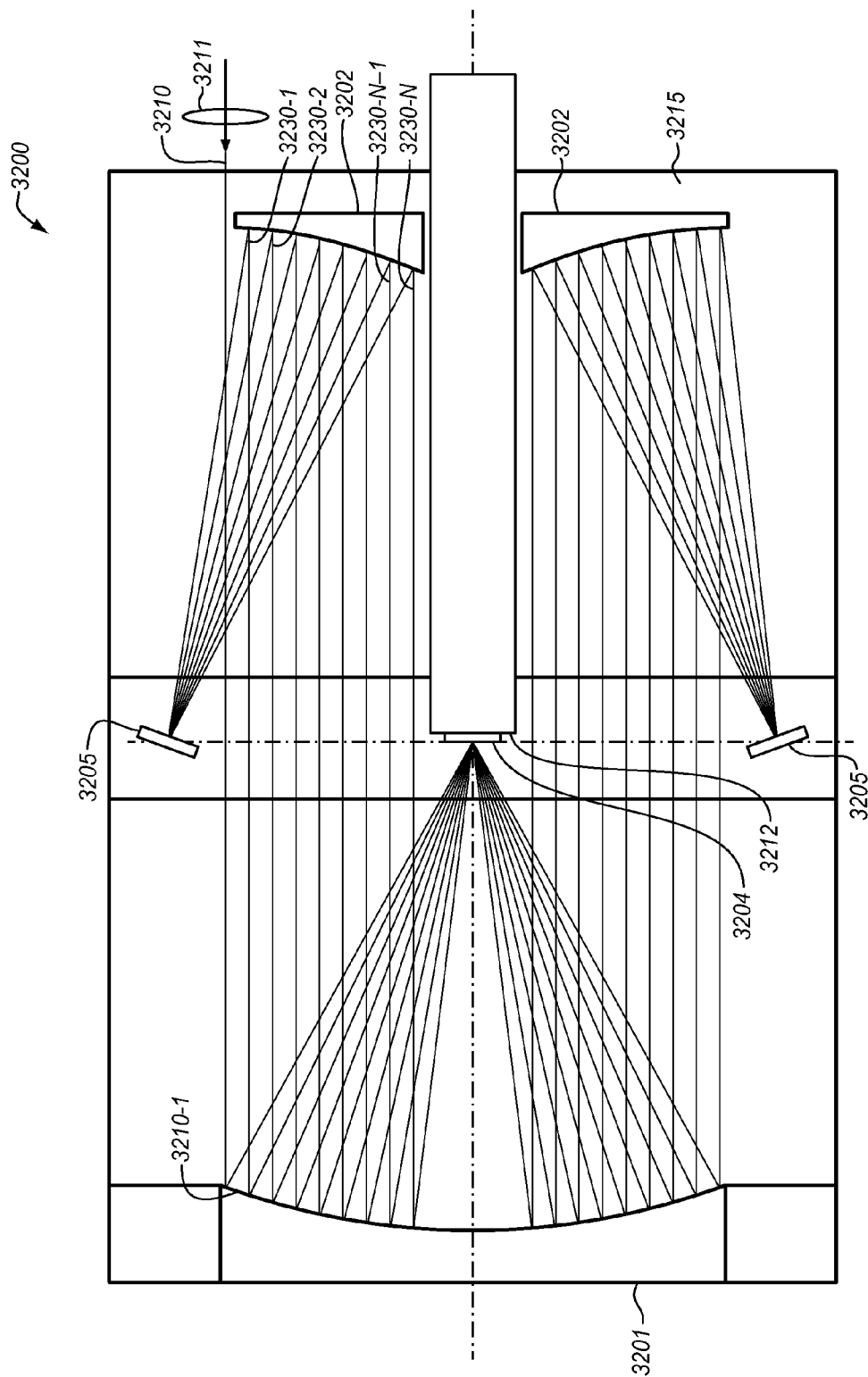


FIG. 27

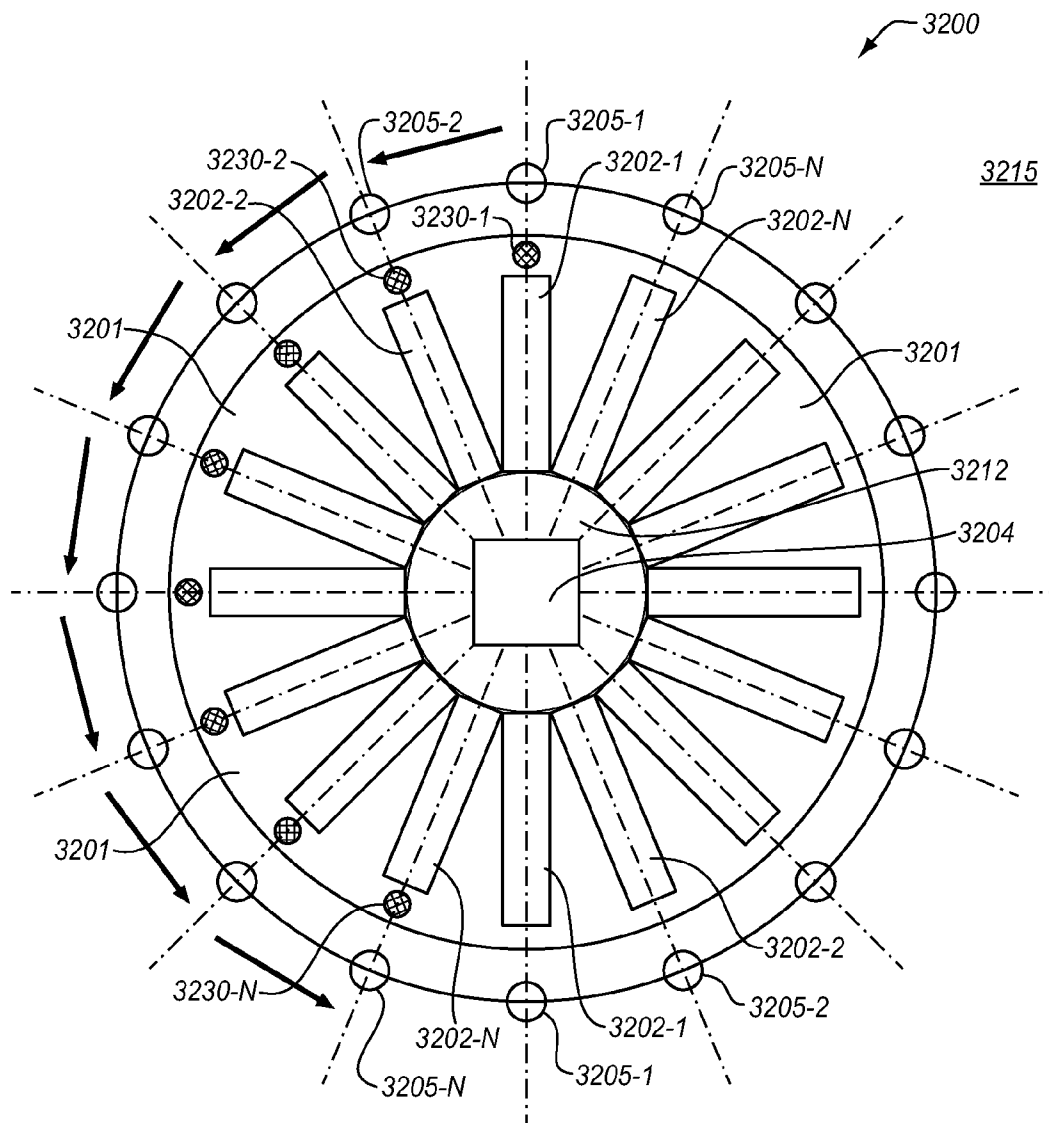


FIG. 28

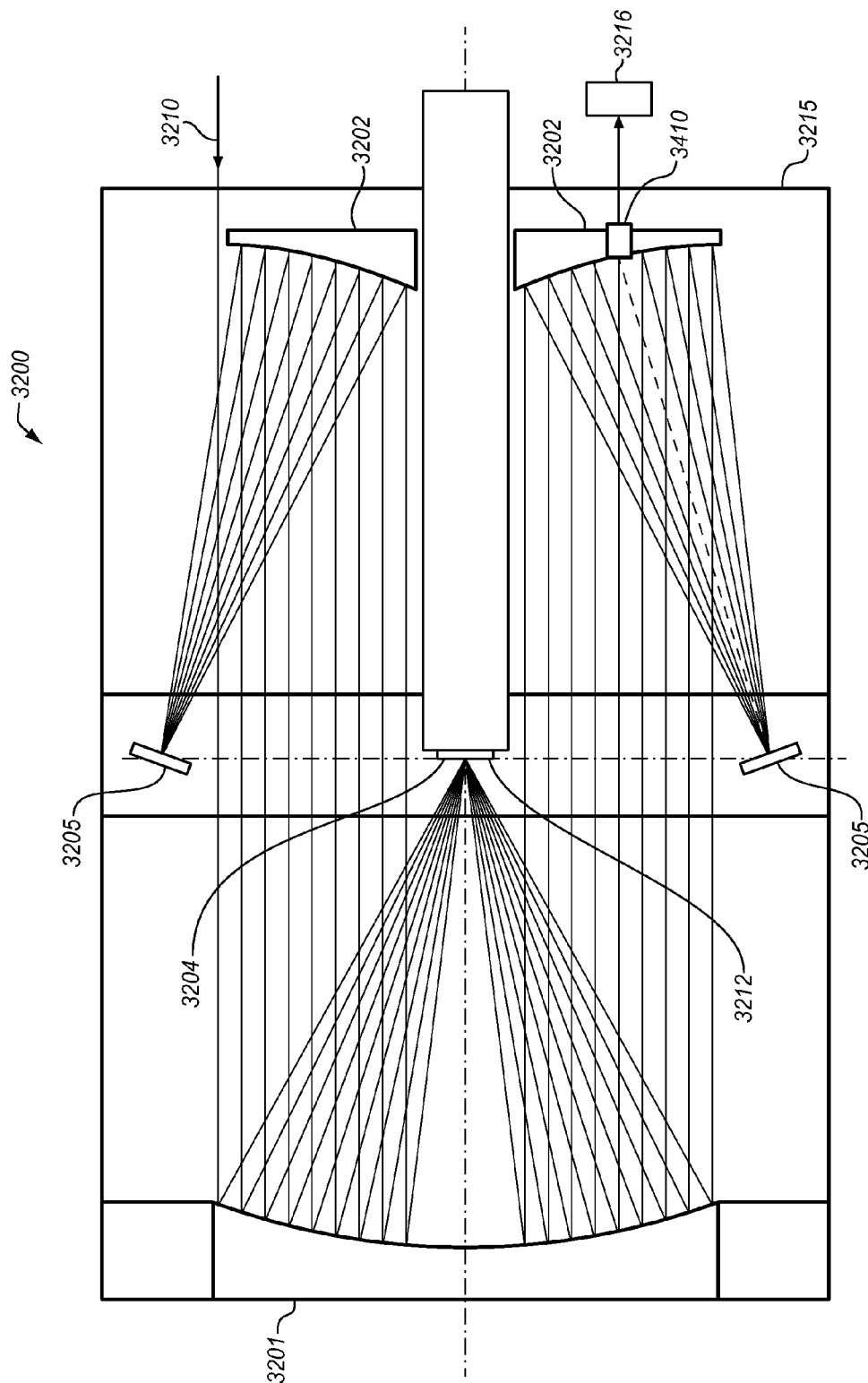


FIG. 29

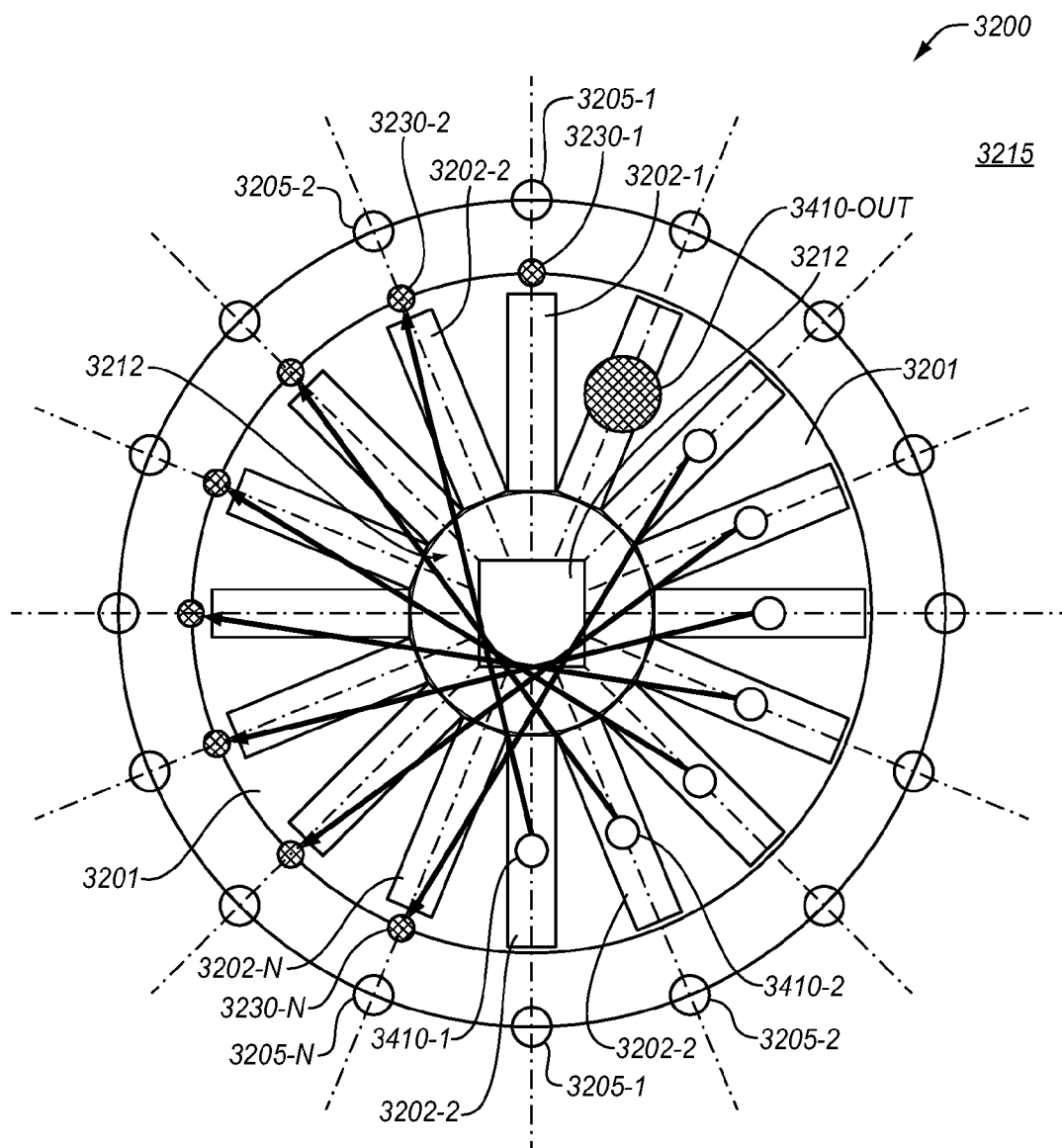


FIG. 30

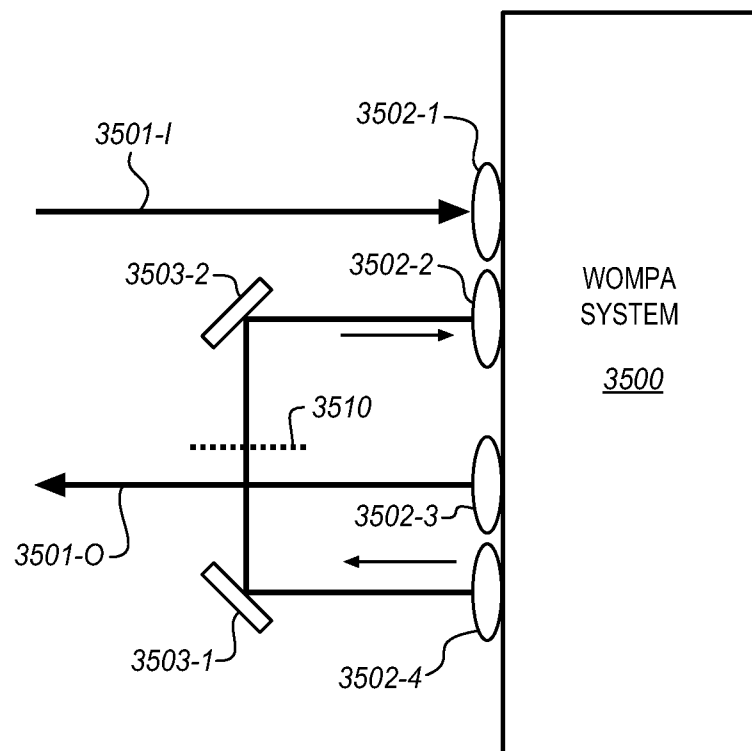


FIG. 31

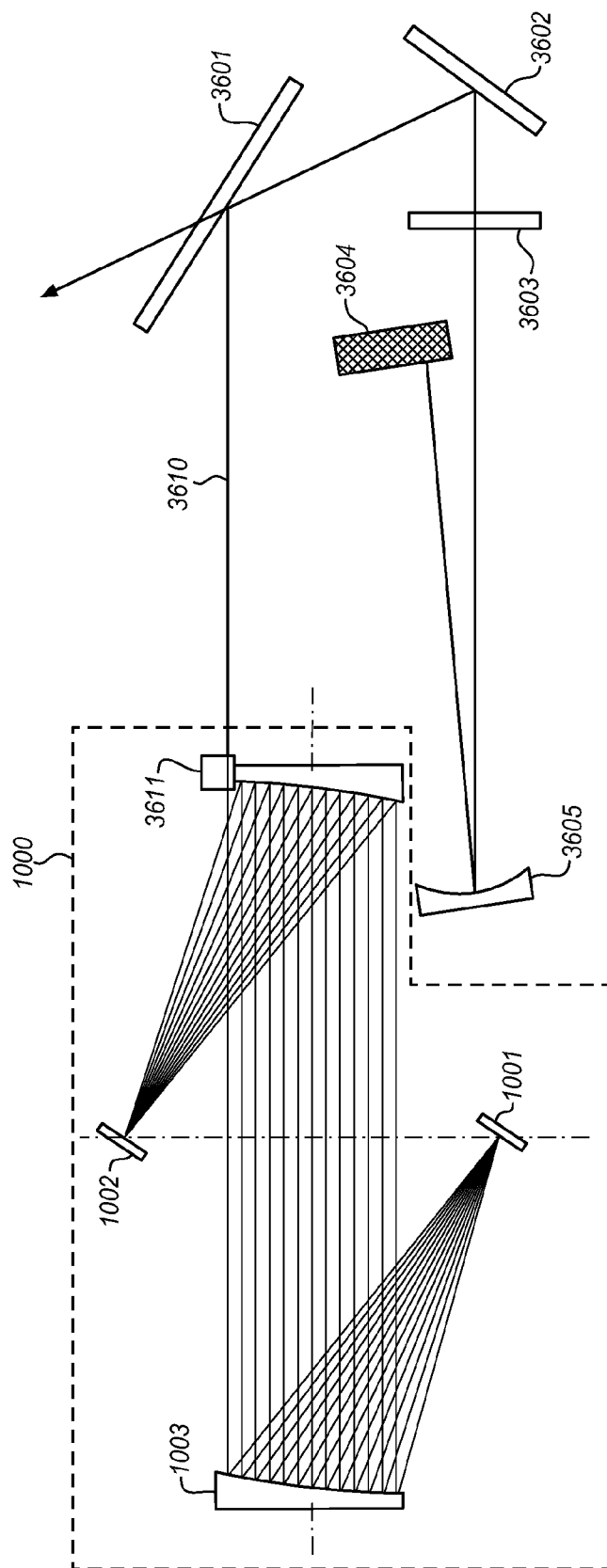
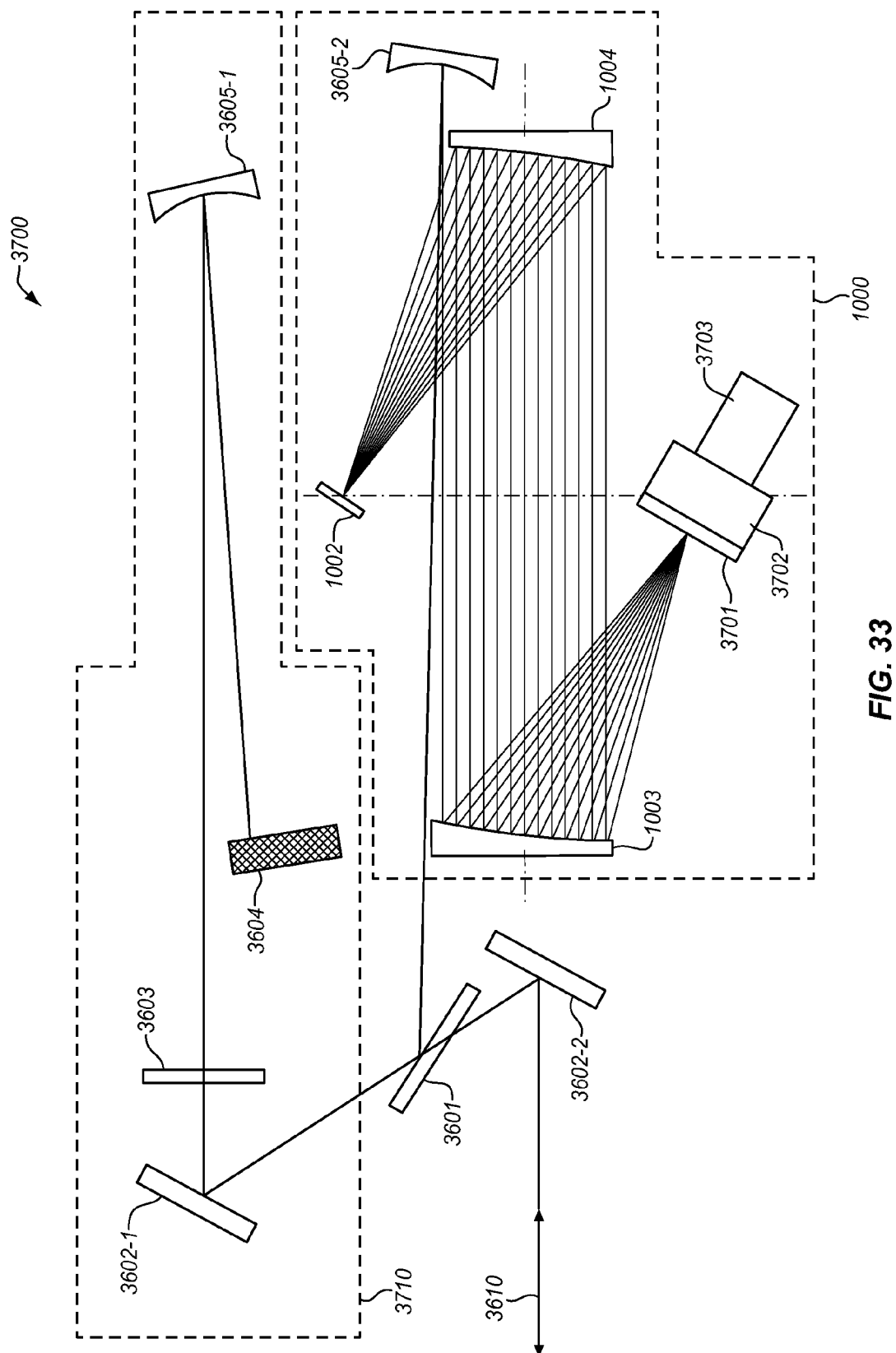
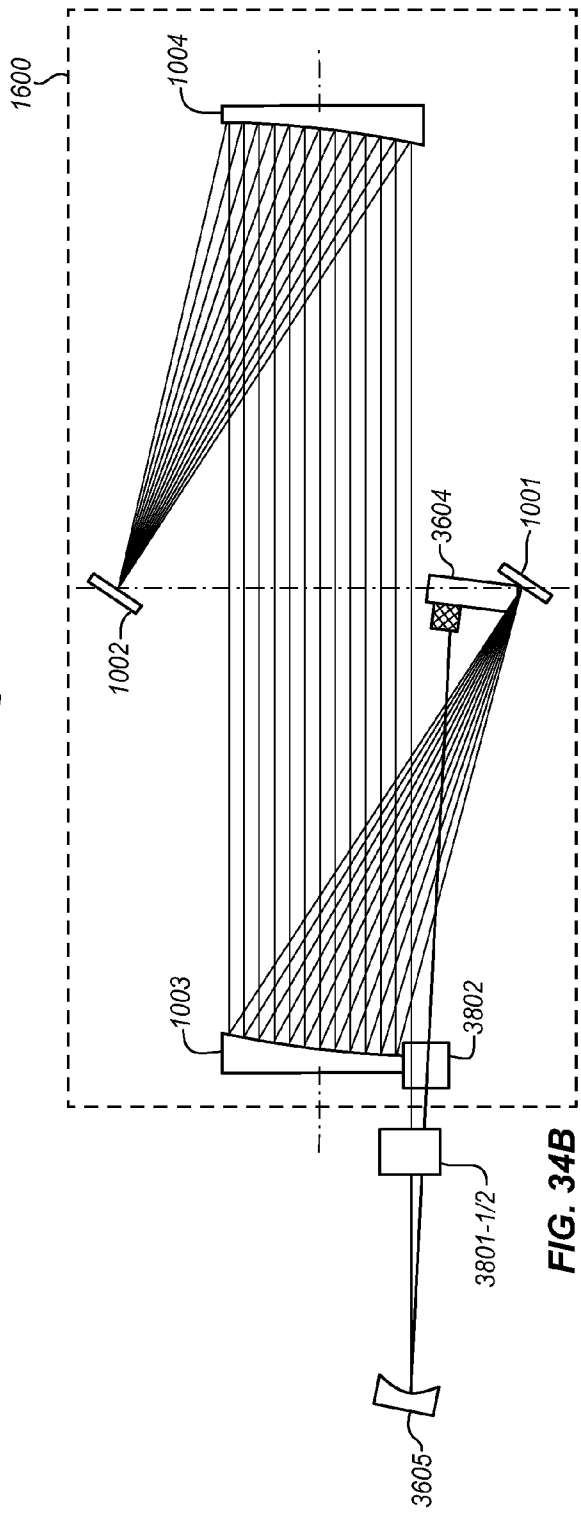
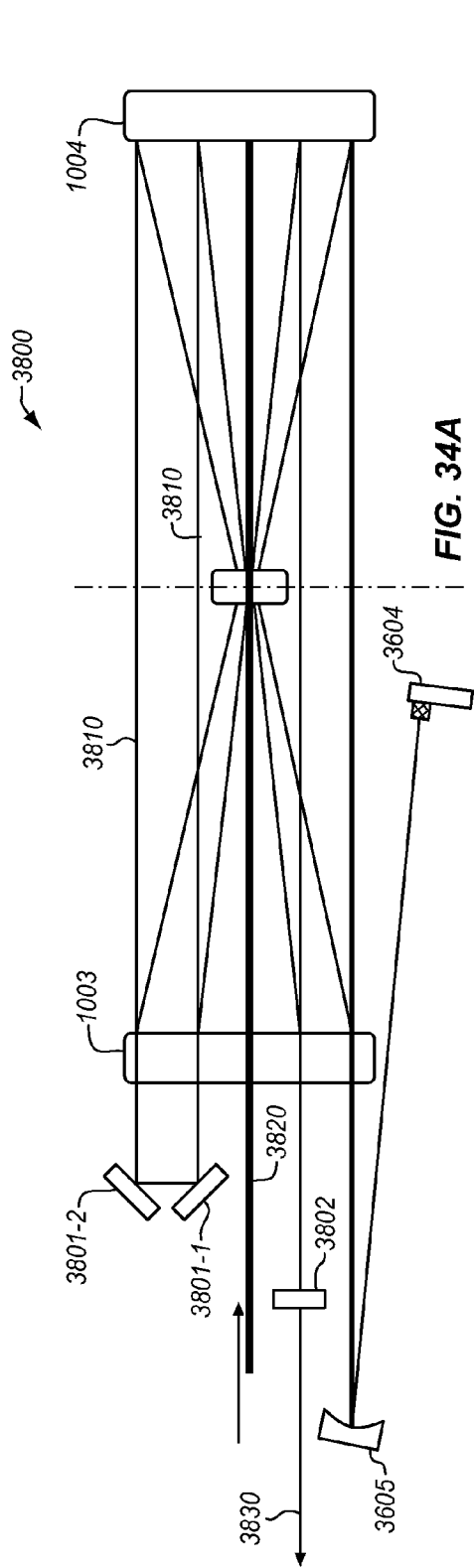


FIG. 32





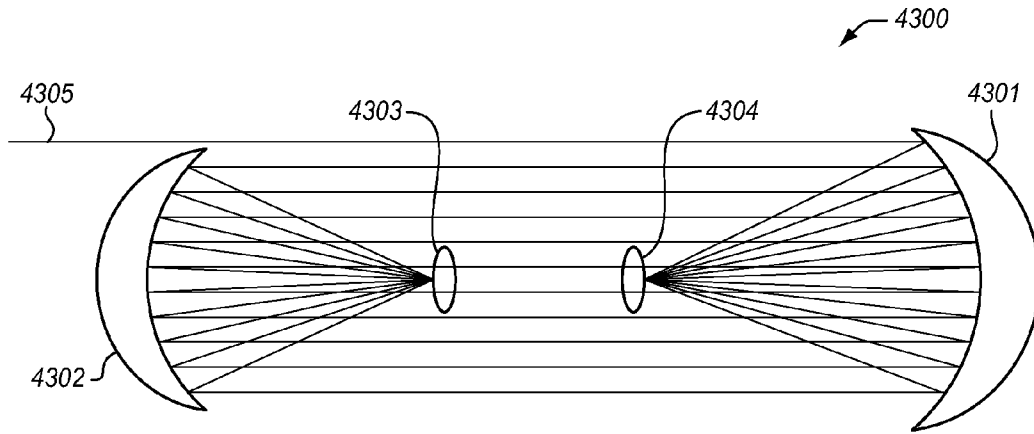


FIG. 35A

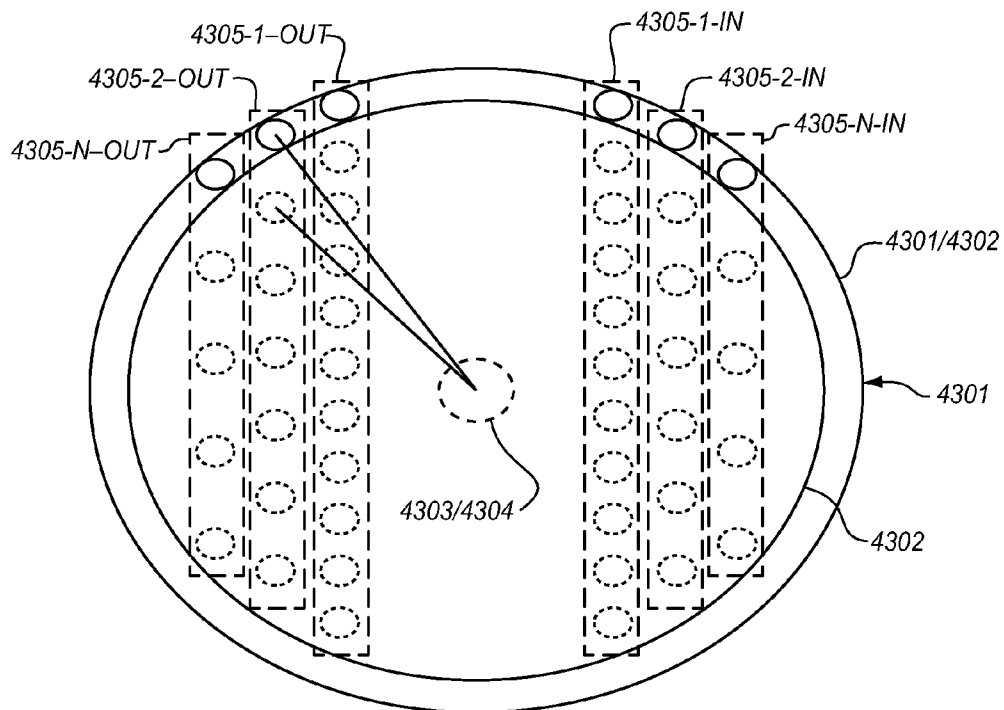


FIG. 35B

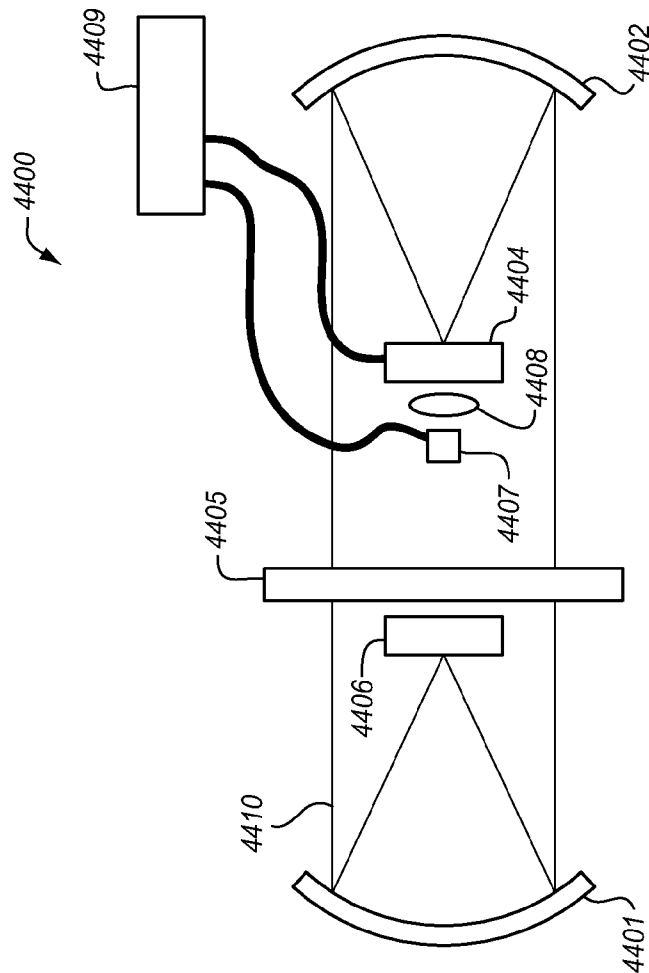


FIG. 36A

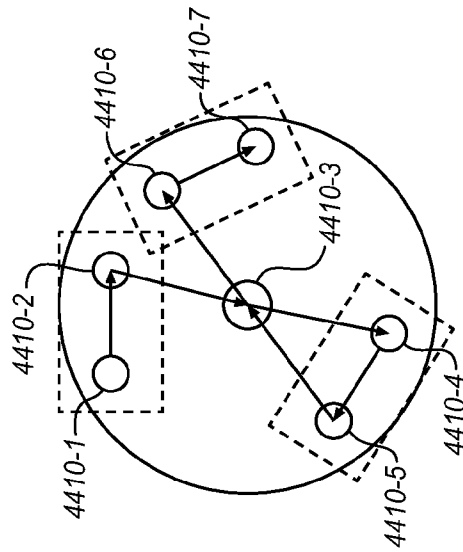


FIG. 36B

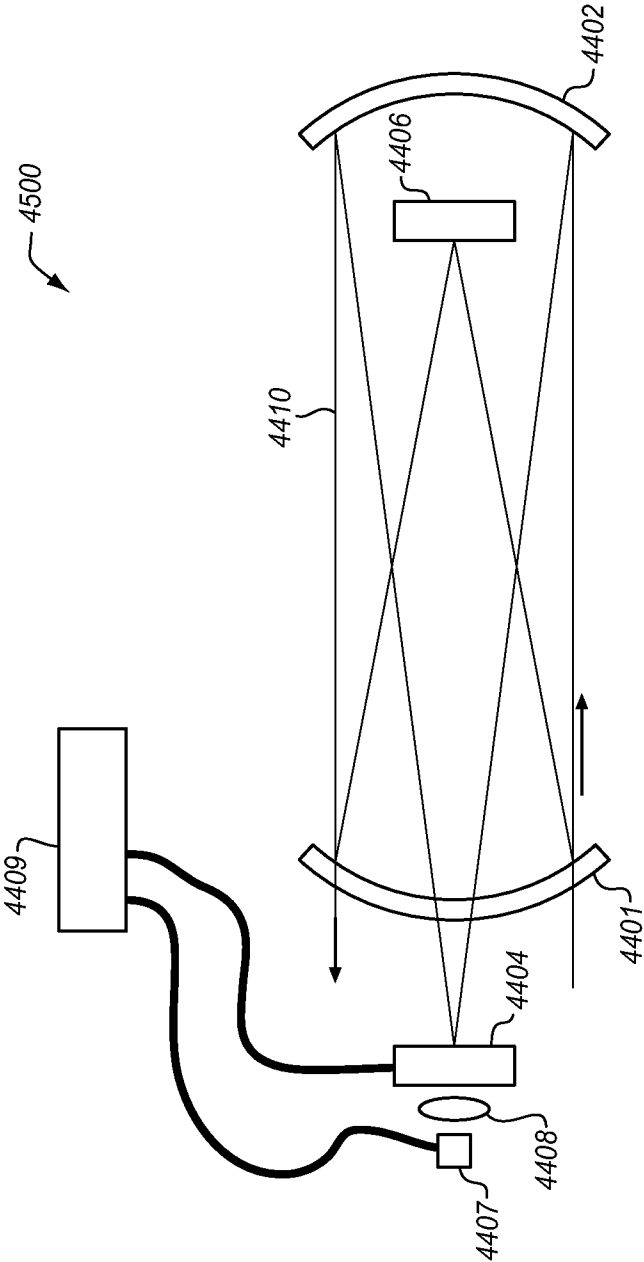
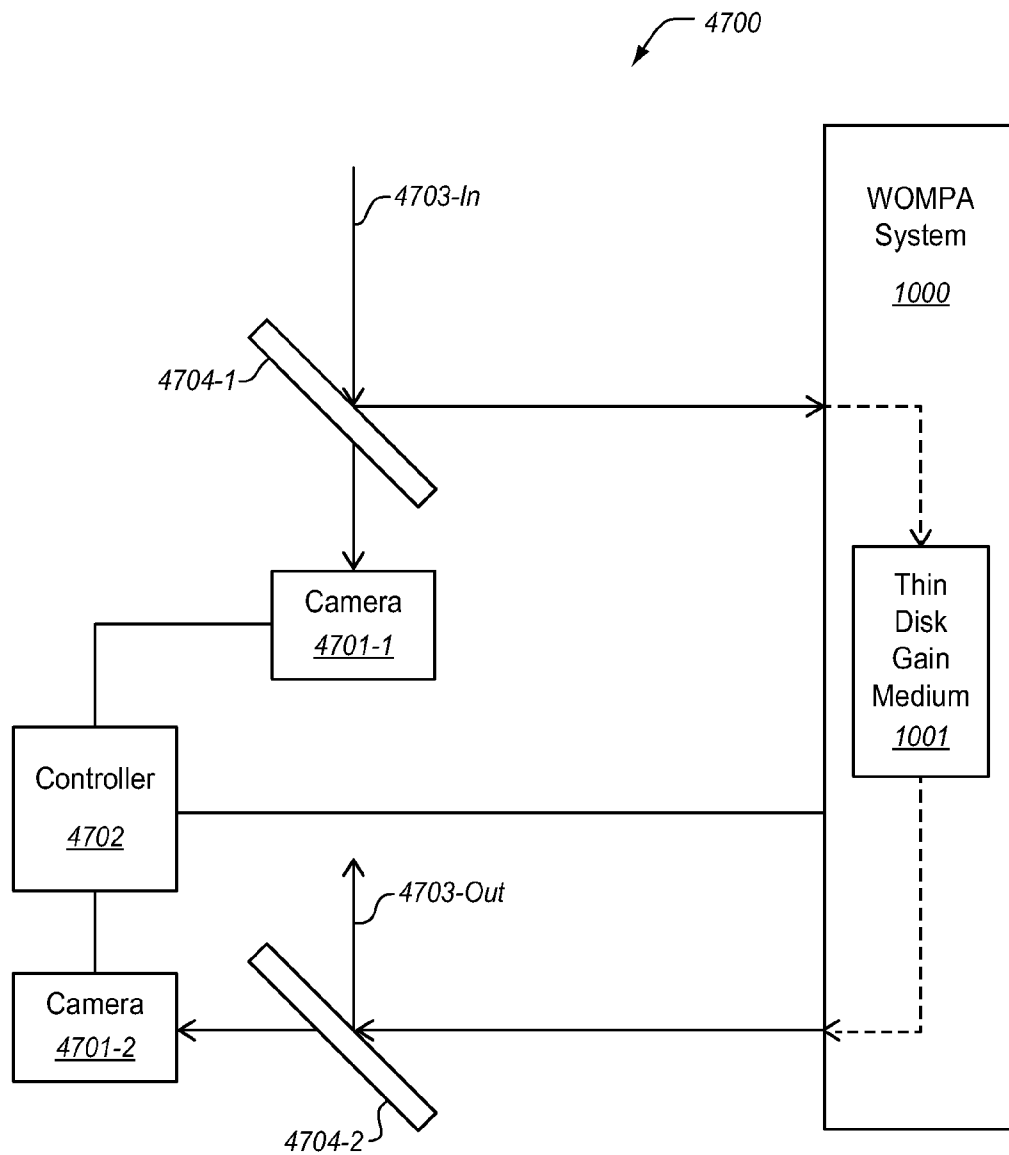


FIG. 37

FIG. 38

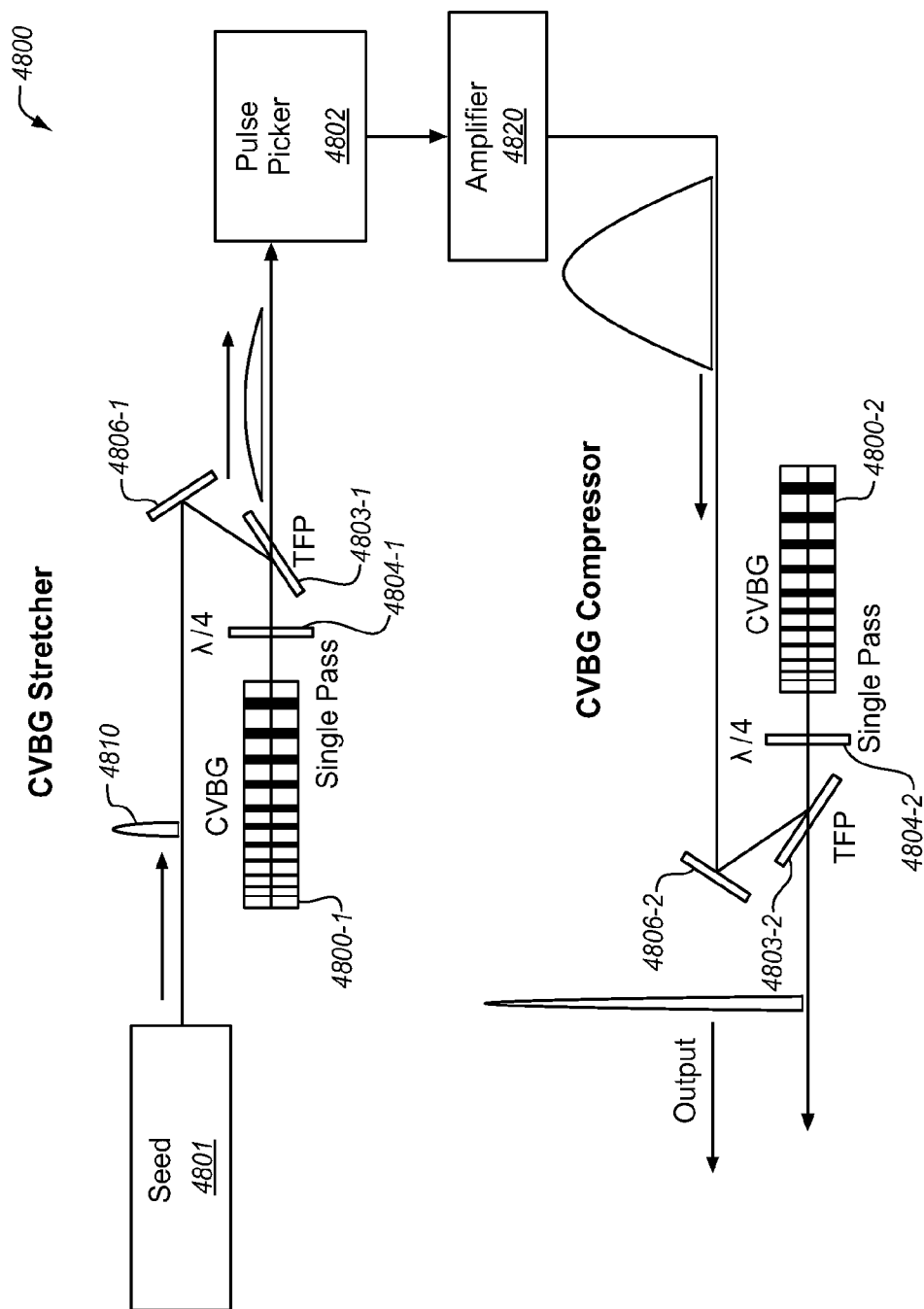


FIG. 39

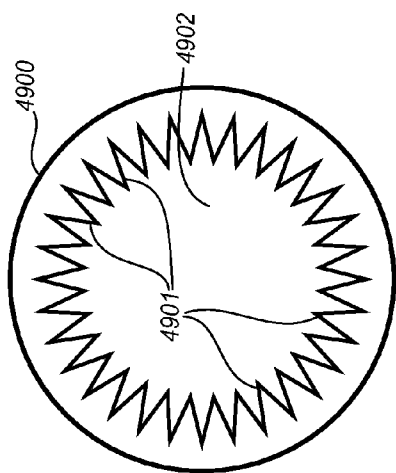


FIG. 40

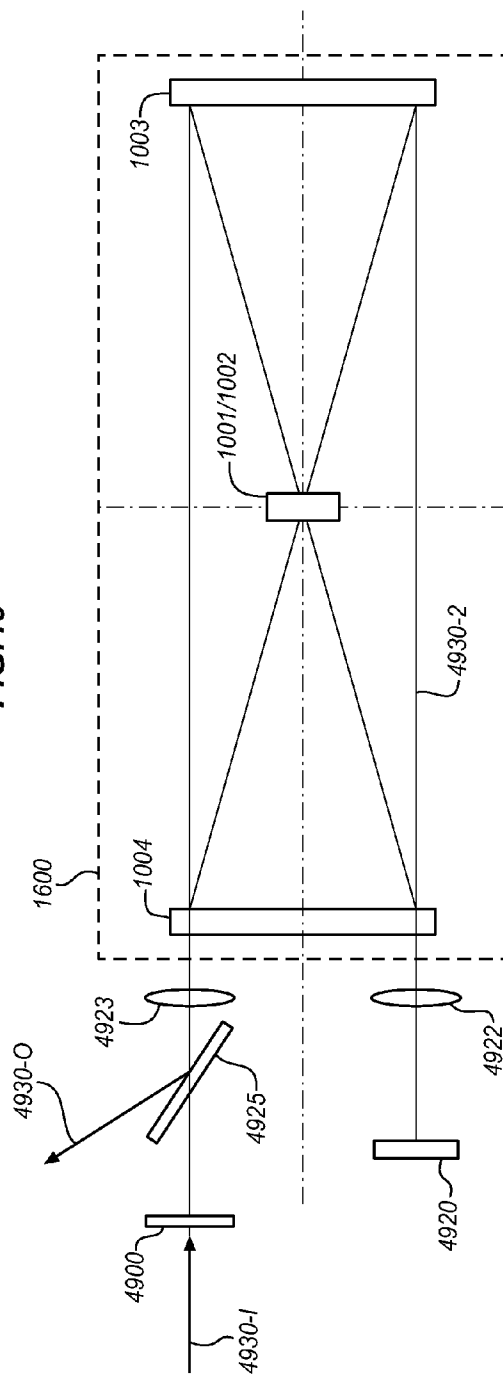
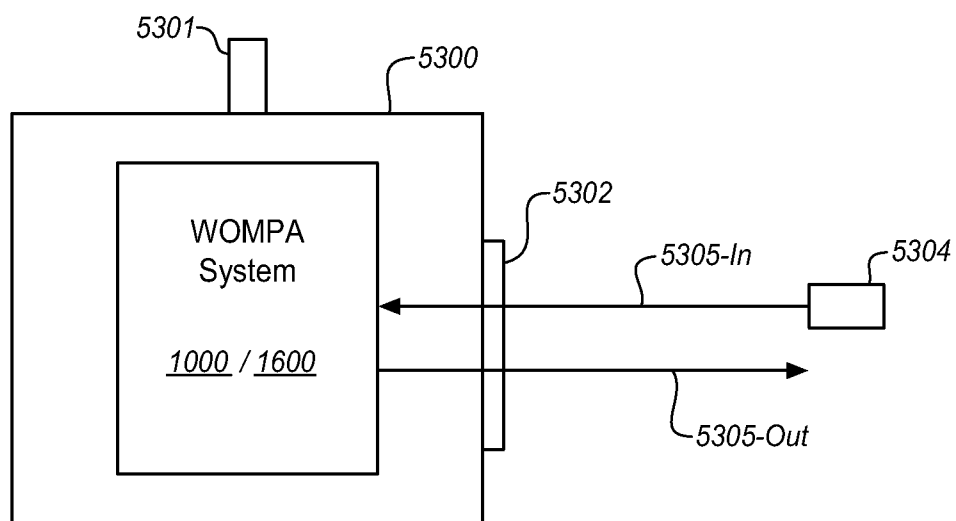


FIG. 41

FIG. 42

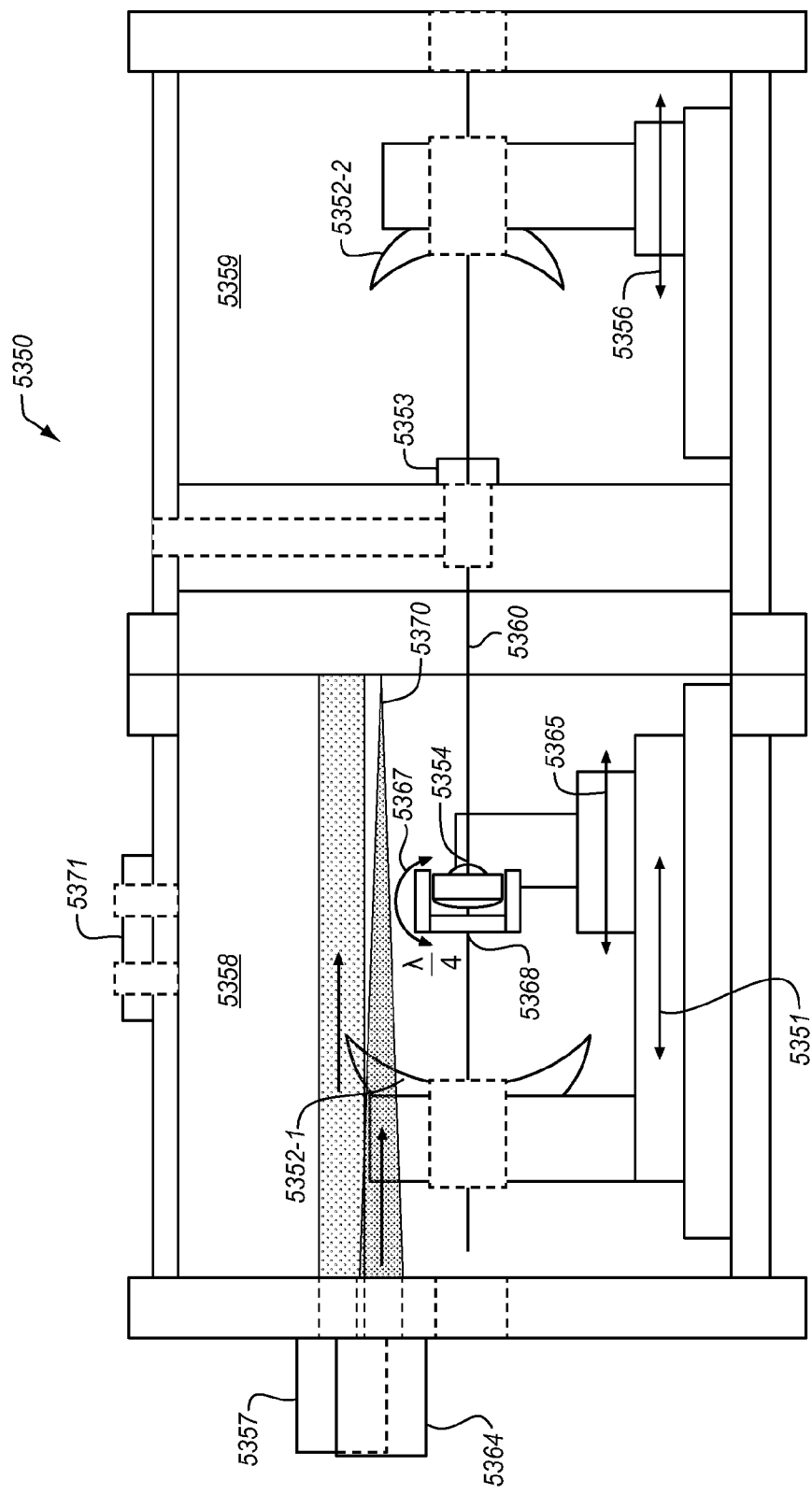


FIG. 43

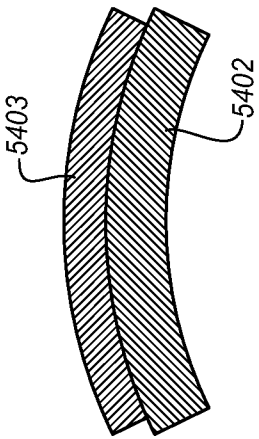
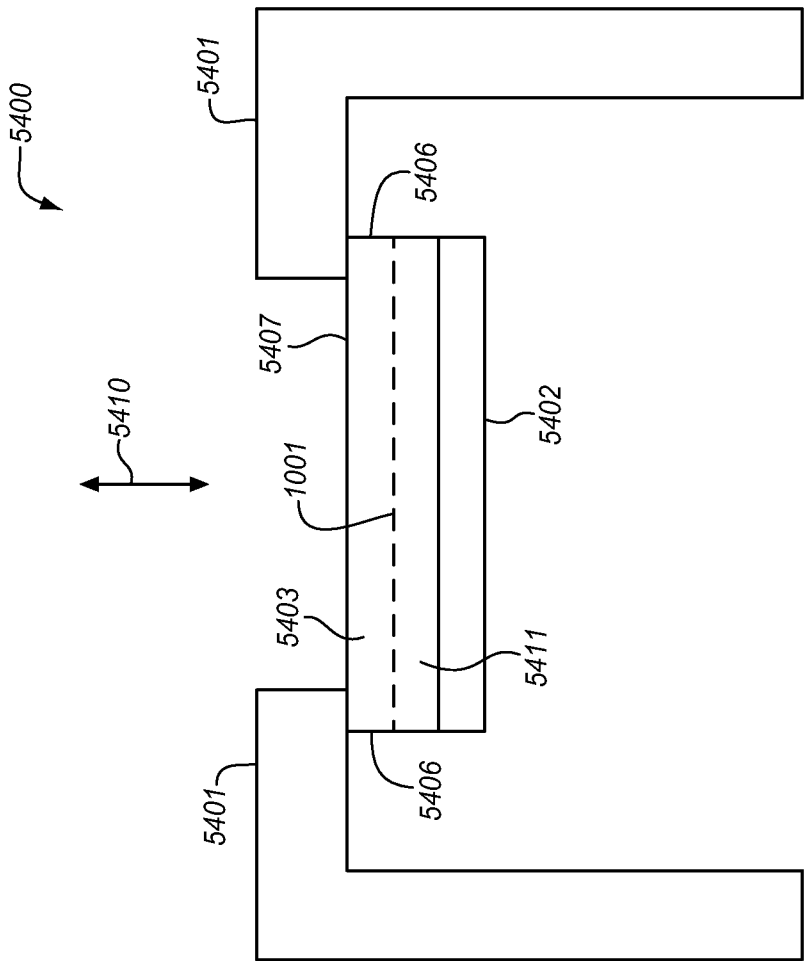


FIG. 44B

FIG. 44A

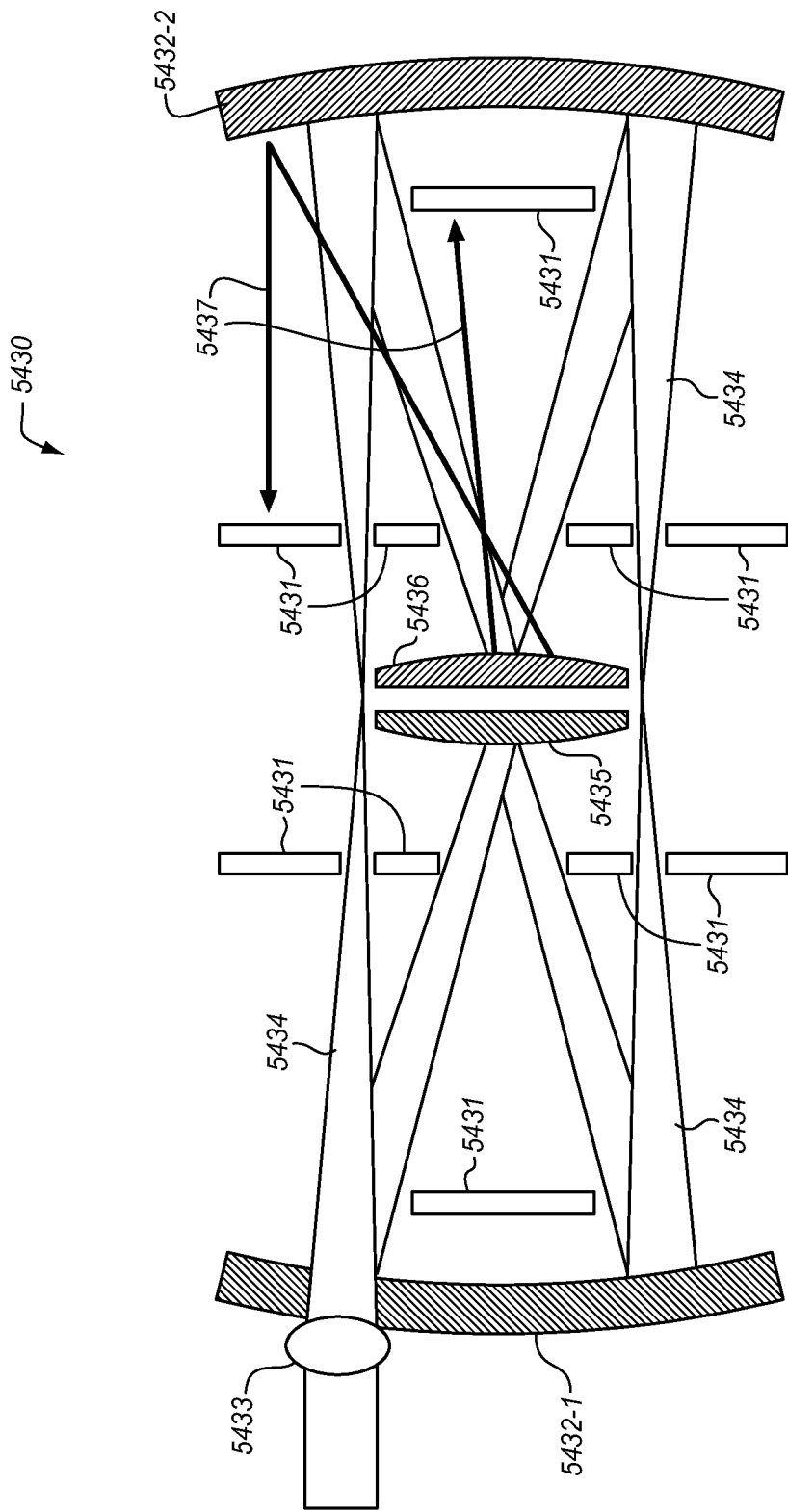


FIG. 45

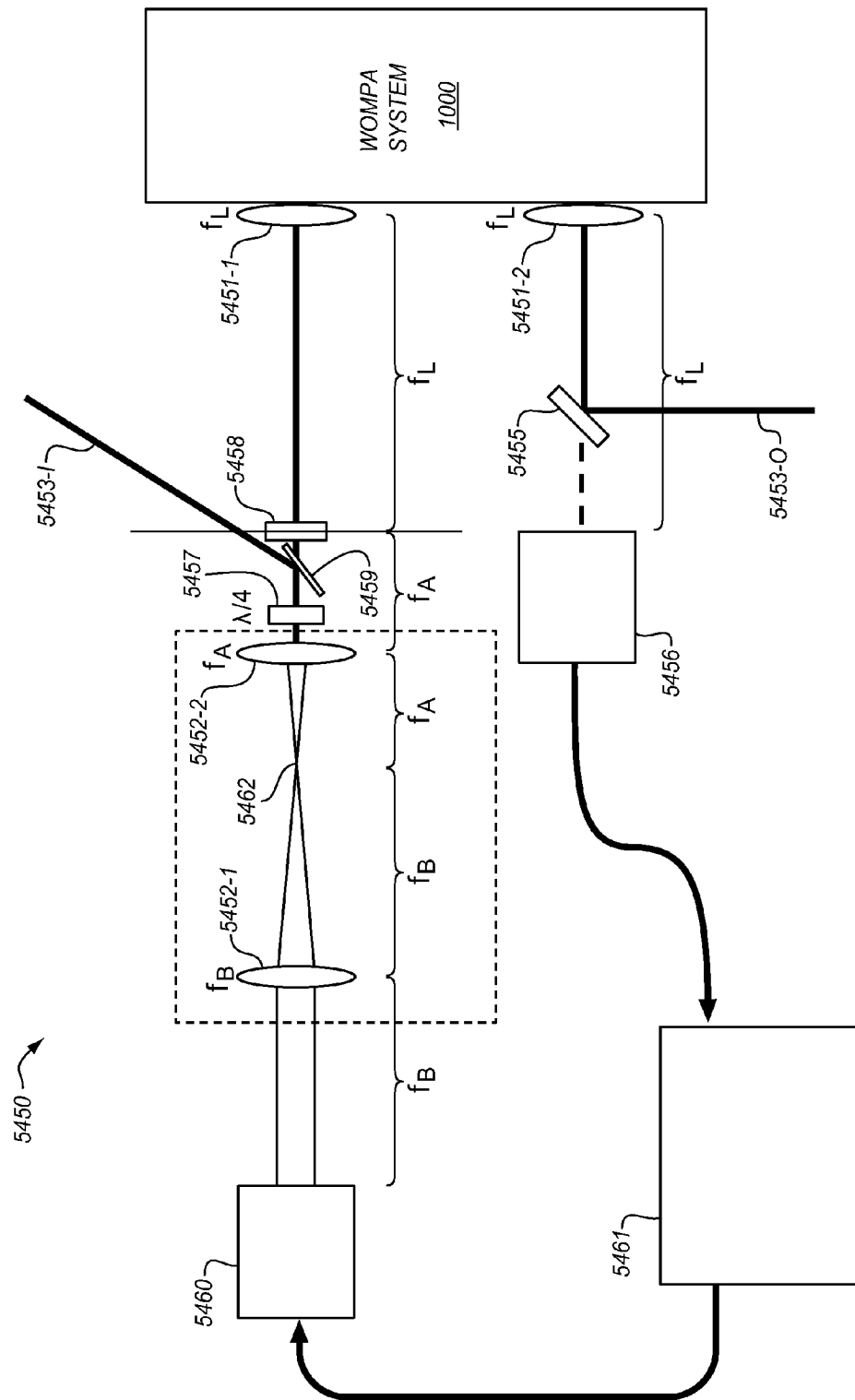


FIG. 46

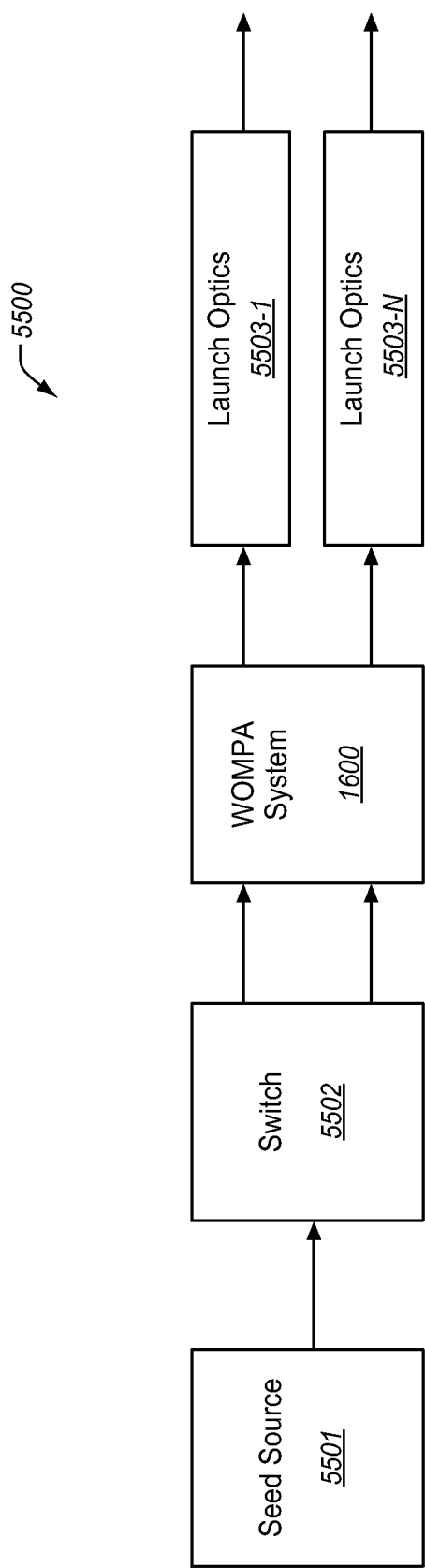


FIG. 47

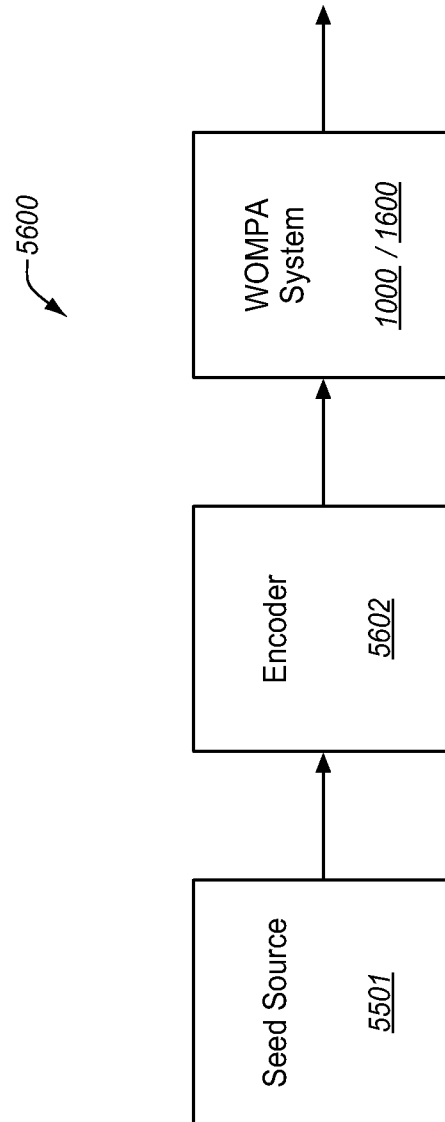


FIG. 48

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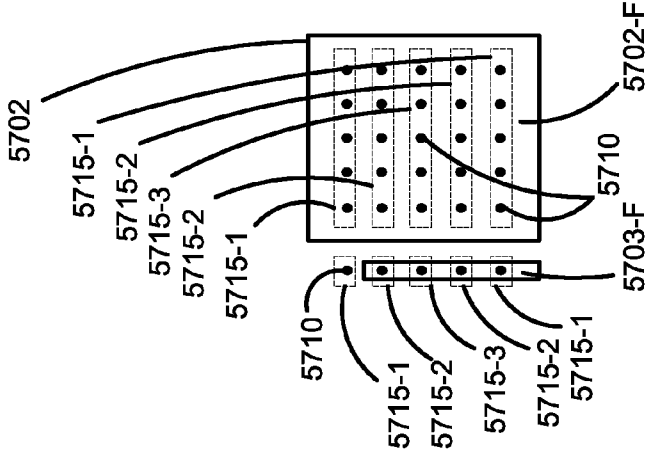


FIG. 49A

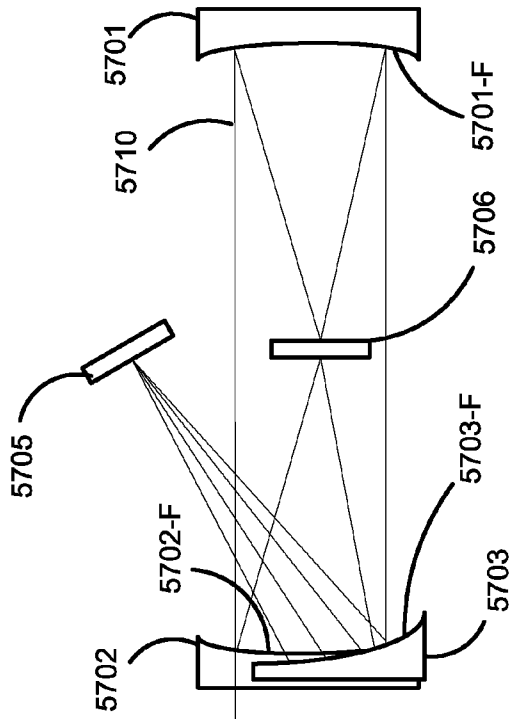


FIG. 49B

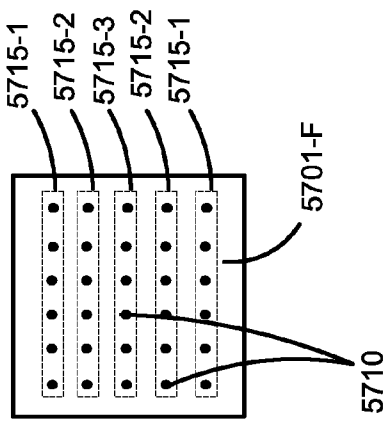


FIG. 49C

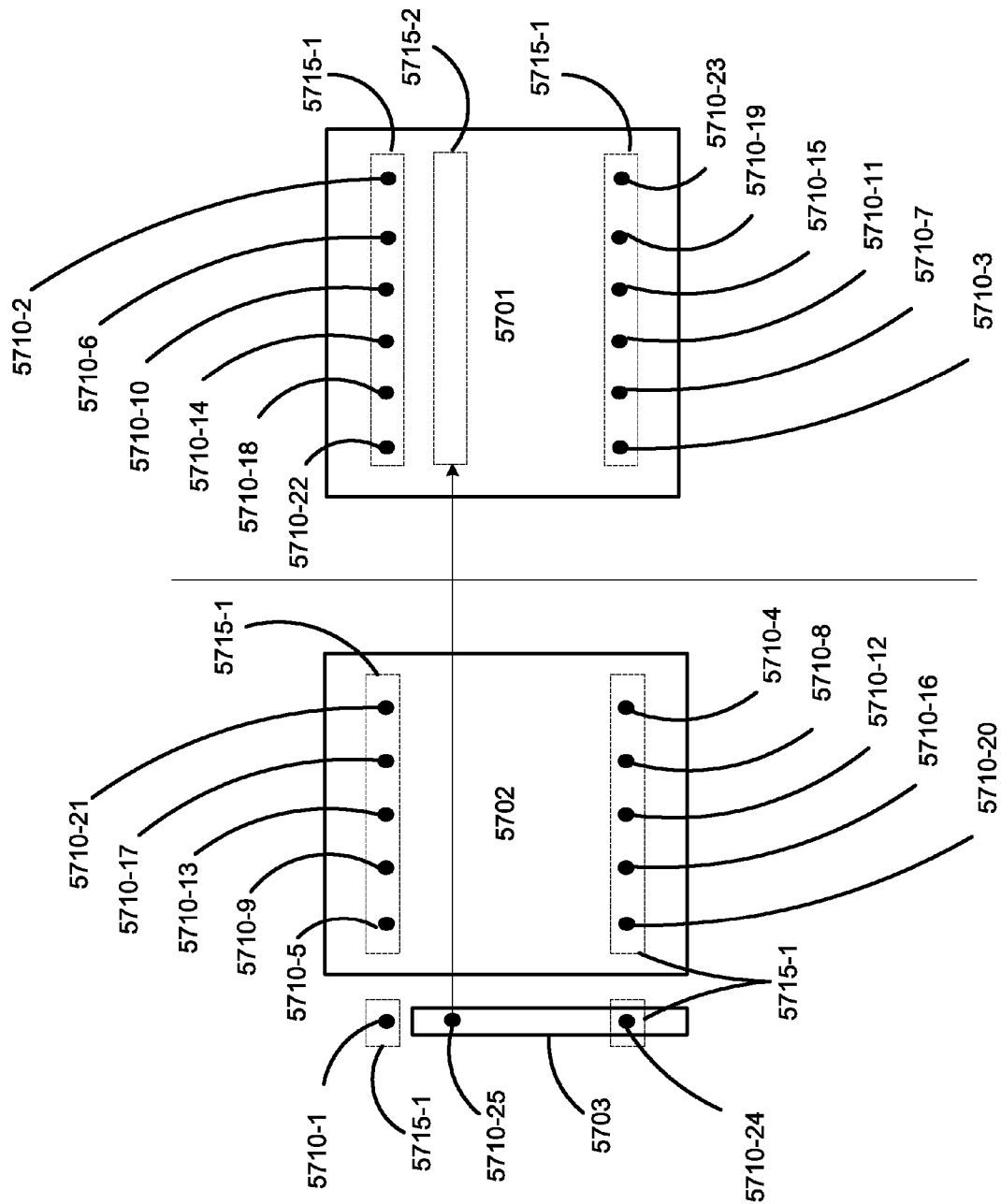
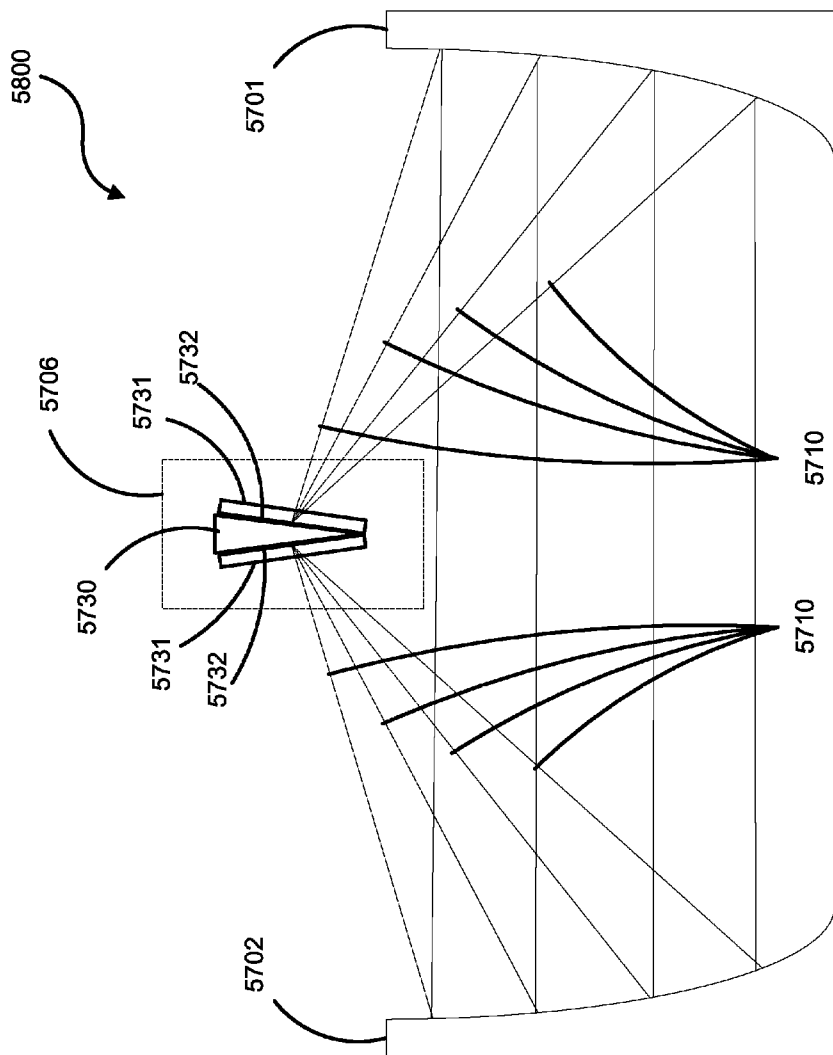


FIG. 50



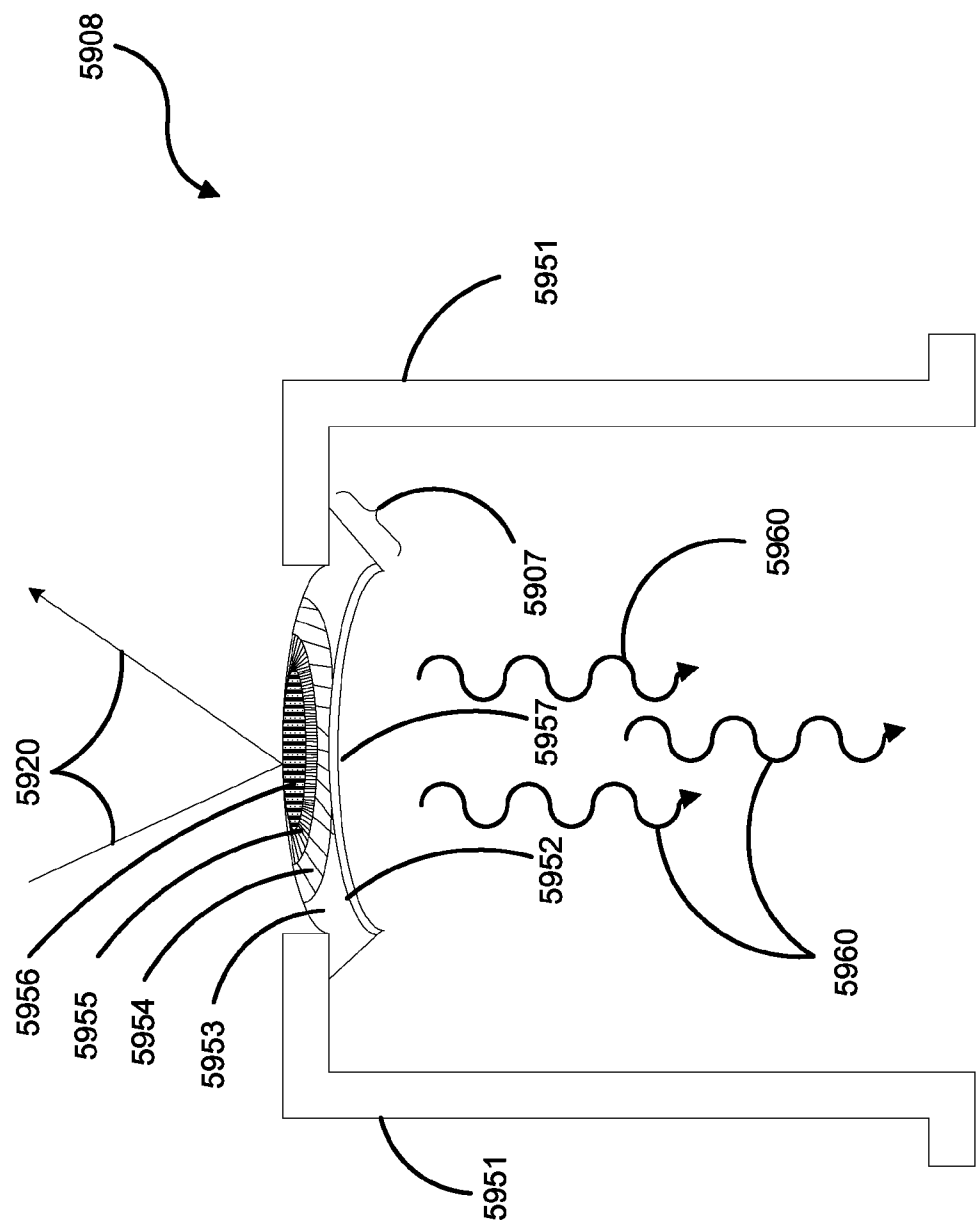


FIG. 52

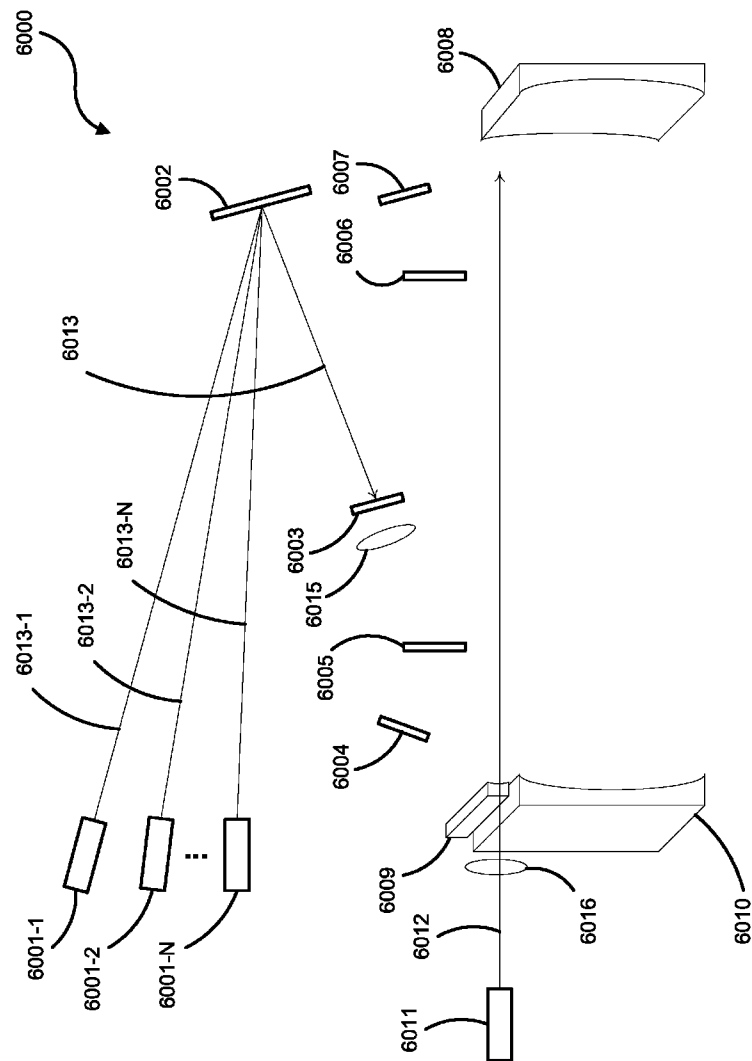


FIG. 53

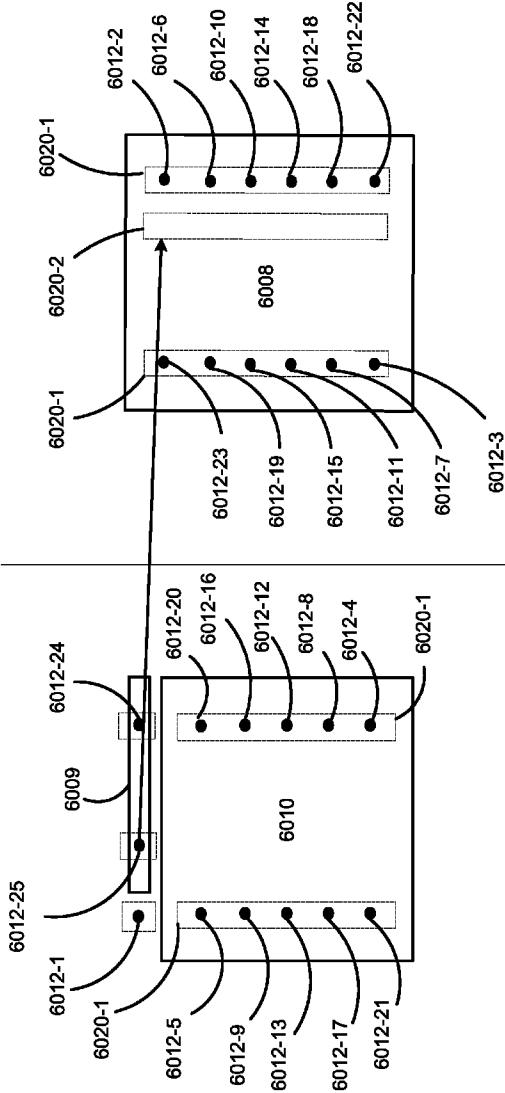


FIG. 54

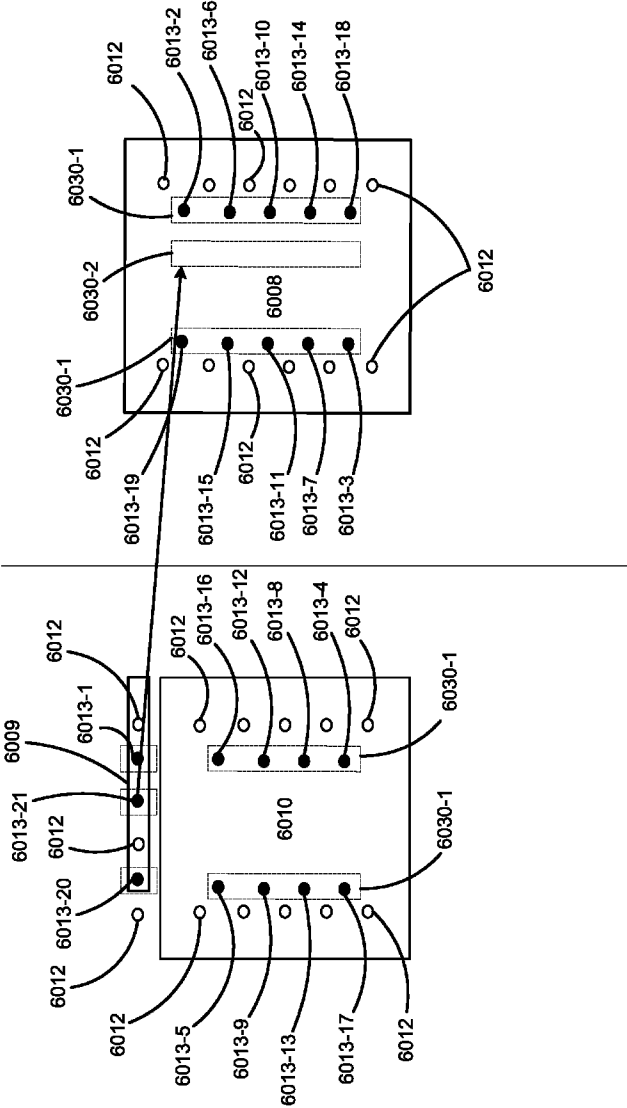


FIG. 55

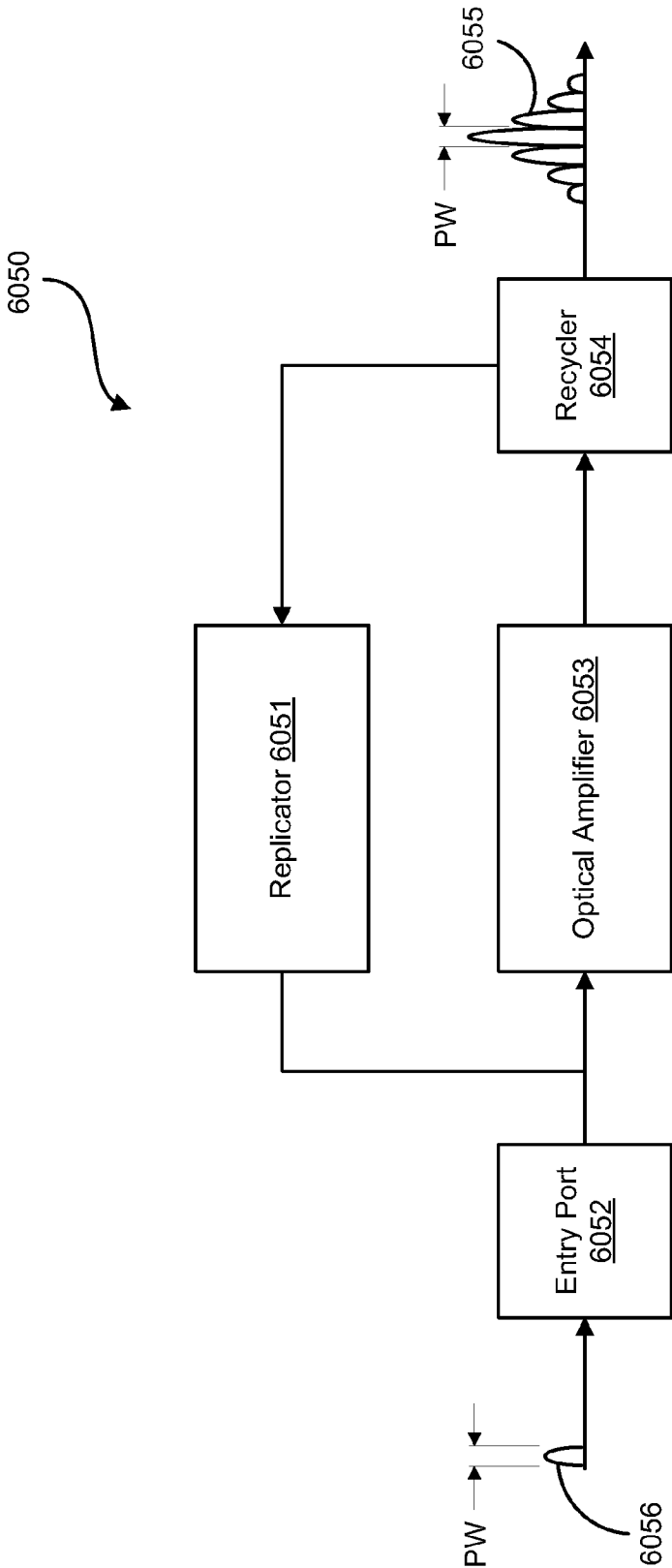


FIG. 56

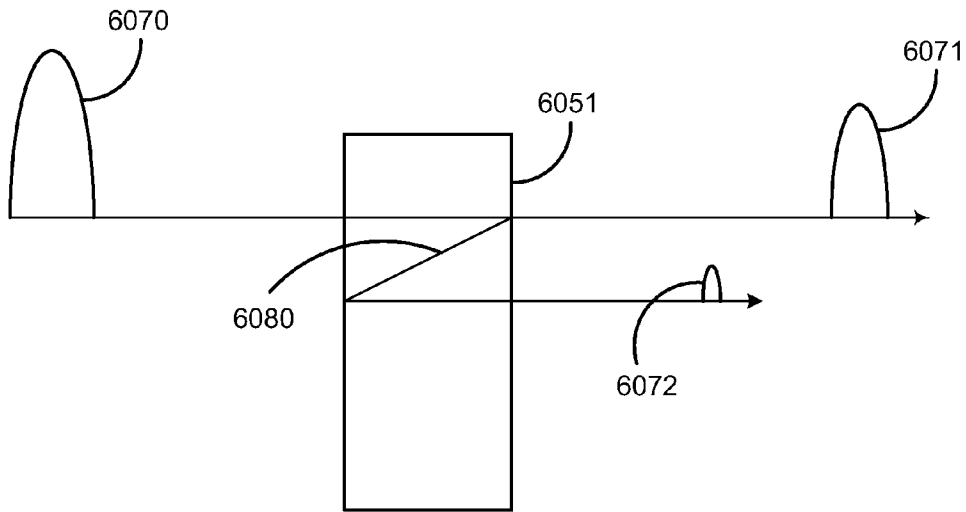


FIG. 57

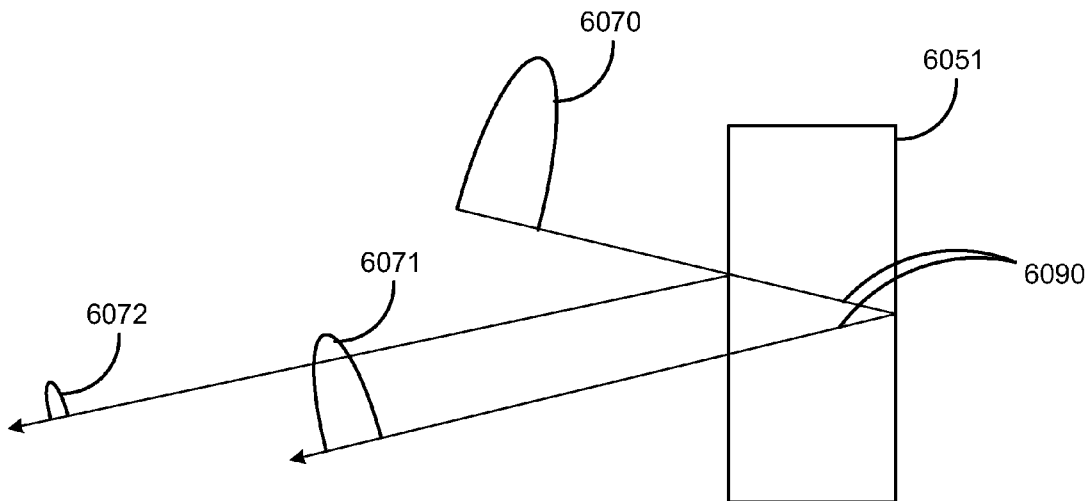


FIG. 58

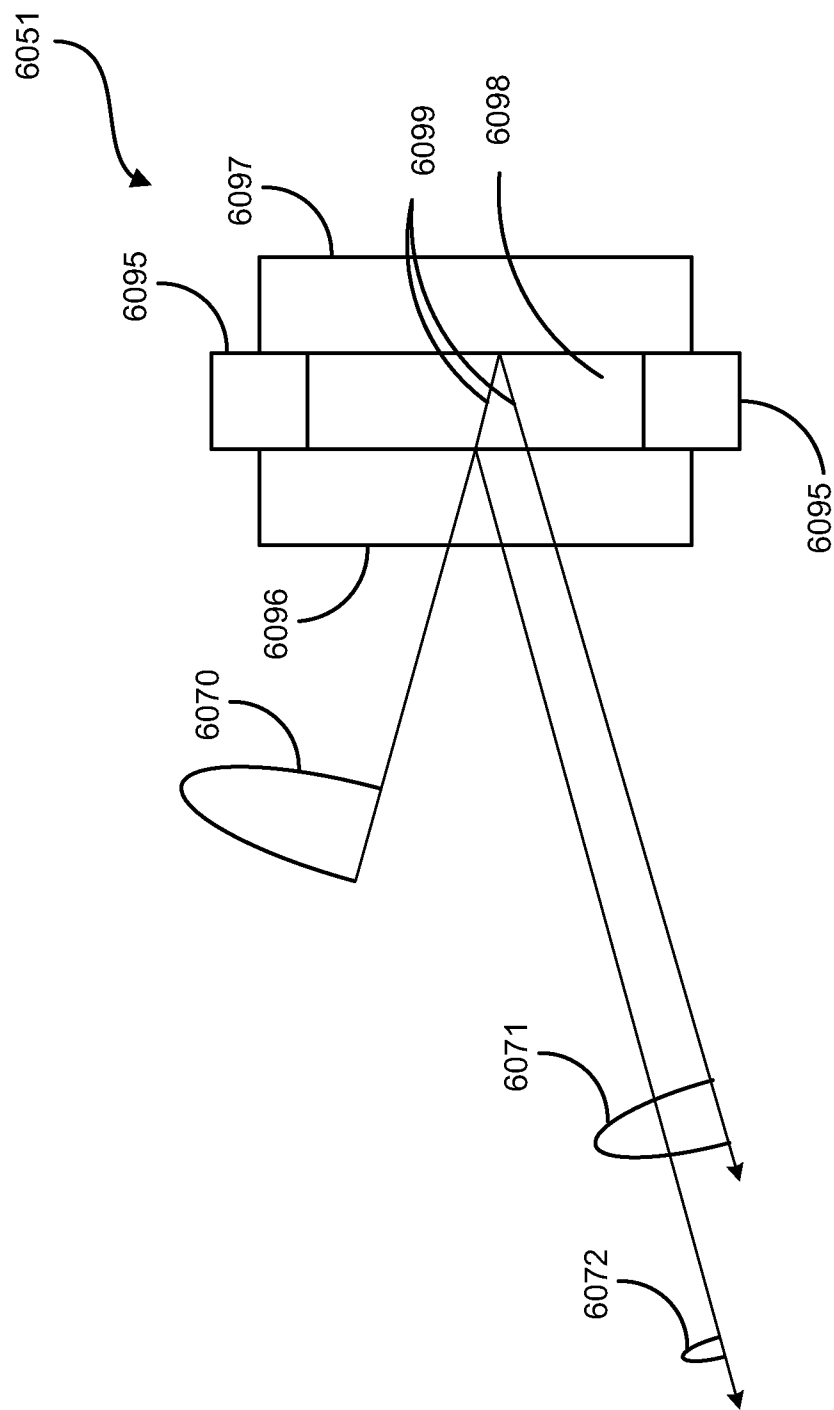


FIG. 59

OPTICAL AMPLIFIER FOR MICROWAVE BURSTS

CROSS-REFERENCE TO RELATED APPLICATIONS

This patent application is a non provisional patent application claiming priority to, and thus the benefit of an earlier filing date from, U.S. Provisional Patent Application No. 61/436,875 (filed Jan. 27, 2011), the entire contents of which are incorporated by reference.

BACKGROUND

In recent years, there have been significant advances in laser technology including solid state laser technology. This technology is being used in numerous applications including scientific research, manufacturing, medicine, security, communications, and many others. Many laser applications require reliable high power outputs and numerous mechanisms have been developed to achieve such. Indeed, high power laser amplifiers have been developed in a variety of forms to accommodate a wide variety of applications, but each amplifier generally functions to amplify the power of an input pulse or beam to provide an amplified output pulse or beam.

Design of laser amplifiers may be limited by factors related to optical component tolerances in the amplifier to pulses of high-energy laser light and average power loading. For example, in one large class of amplifier designs, known as regenerative amplifiers, multiple passes through a single gain medium or plural gain media are used for efficient extraction of gain. In these regenerative amplifiers, an optical path is defined around which an input pulse makes a number of passes before being coupled out as an amplified pulse.

Regenerative amplifiers are generally used to provide relatively strong amplification of laser pulses. Multiple passes through the gain medium are achieved by placing the gain medium in an optical resonator, together with an optical switch that may be formed by an electro-optic modulator and one or more polarizers. The number of round trips in the resonator is controlled with the optical switch and, when this number is large, a high overall amplification factor (i.e., gain) can be achieved.

While these regenerative amplifiers provide significant gain, they are often difficult to implement due to their complex cavities. Moreover, switching of the laser pulses within the cavity usually decreases the achievable pulse energies or beam due to nonlinear propagation effects within the switch. Additionally, regenerative amplifiers, under some operating conditions, suffer from chaotic or multi-stable operation. In these operating conditions, the residual gain in the gain medium after energy extraction significantly affects the gain that can be imparted on a subsequent signal pulse. Regenerative amplifiers also generally amplify one pulse at a time. Therefore, the repetition rate of the laser system is less than the reciprocal of the time between the injection and ejection of each amplified pulse.

Another concern in high power laser systems regards heat. High average power laser systems typically produce heat and most laser architectures are designed with this in mind because high temperatures within a gain medium can reduce gain and/or cause thermo-mechanical strains that result in stress-induced birefringence. Temperature distributions in a gain medium can also lead to phase distortions which result in poor laser beam quality. At more extreme temperatures, damage to the gain material or optical coatings can occur. High

temperatures within a laser system can also lead to mechanical movements that result in optical misalignment.

In order to efficiently extract heat from a solid gain medium, the fraction of cooled surface area per heated volume is generally maximized. Two geometries that have been used for high power laser systems include fibers and thin disks. In the case of fibers, two dimensions are minimized and one dimension is maximized so that a large surface area to volume ratio can be obtained for efficient cooling. Additionally, fiber amplifier geometries support very large gain-length products. Fiber amplifiers, however, are not optimal for high-power short pulses because high intensities may result from transmission of laser pulse energy through a very small cross section of an optical fiber. For high pulse powers and small cross-sections, the peak intensity can be extremely high and lead to deleterious nonlinear propagation effects.

One solution for thermal management of pulsed laser operation includes using disk shaped gain media, in which only one dimension is minimized. This geometry also provides large surface areas for heat extraction per gain volume. The thin disk is typically cooled from one side and is accessed optically from the other. A reflective surface is provided between the cooling system and the gain medium. Alternatively, the disk may be cooled from both sides if a thermally conductive medium is used that can also transmit the laser pump and signal beams of energy. Generally, the signal beam is the desired beam of laser energy that is operated on and/or used in a particular application whereas the pump beam may include any type of energy operable to stimulate the gain medium and amplify the signal beam.

Though the thin disk geometry can be efficiently cooled, the pump absorption-length product and signal gain-length product for typical gain media is small. For this reason, thin disk based lasers generally use a multi-pass optical system for optical pumping, and a multi-pass system for the signal beam. After each pass of the pump beam, a portion of the pump beam is absorbed. However, after multiple passes of the pump beam, most of the pump laser light can be absorbed by the crystal. For example, small gains may be achieved each time the signal traverses through a thin disk. Higher amplitude gains thus require multiple traversals of the signal beam through the thin disk so that a larger effective gain-length product can be achieved. Because greater energy extraction can be achieved by using a larger gain volume, a thin disk may utilize a relatively large pump and signal beam spot size. This allows for higher power without exceeding intensity thresholds for deleterious nonlinear propagation effects.

Although heat can be removed from a thin disk, thermal gradients typically lead to phase distortions due to temperature dependent indices of refraction, thermal expansion, and/or strain effects. For thin disk geometries where a reflective surface is included, thermo-mechanical distortions can lead to especially strong phase distortions and each pass of the signal beam can lead to accumulated phase distortions. These phase distortions can also include birefringent effects, such as strain-induced birefringence.

Accumulated phase distortions in a laser system can also lead to "hot spots" or losses that limit the laser powers that can be achieved. For example, if a thin disk imparts focusing phase distortions to a signal beam, the beam may eventually be focused to such a small spot size that it could damage an optical component with extreme intensities or even ionize the air, losing energy in the process. Accordingly, the laser power would be intentionally "dialed down" to avoid these effects. A signal beam that accumulates a divergence with traversals of the disk can also become too large for an optic, aperture, or an amplified region for a subsequent traversal through the gain

medium. Consequently, divergence also results in an energy loss that limits the laser power.

In high power diode pumped laser systems, laser energy from multiple laser diodes may be collected and transmitted to a gain region via fiber. However, such generally requires beam combining mechanisms where multiple diode sources can be independently transmitted to the gain region. This allows for higher pump powers to be used than could be obtained from a single diode source. Additionally, multimode fibers may be used to supply higher average power. In any case, fibers are limited in the amount of power that they can easily transmit. A laser system that provides for simplified beam combining from multiple sources, at the gain medium, would provide a significant benefit.

SUMMARY

The various laser architectures described herein provide increased gain and compensation of optical phase distortions in a thin disk gain medium. In one embodiment, an optical amplifier provides for scalable high energy extraction and gains based on a number of passes of the signal beam through a gain medium. In this regard, new reimaging walk-off multi-pass amplifier architectures are presented herein that are amenable to simpler methods for clearing gain between laser pulses. Because multiple, spatially separate, optical paths can be passed through the same gain region, gain clearing can be achieved by splitting off a small percentage of an output pulse and sending it back through the amplifier along a slightly different path. By clearing out the residual gain, uniform signal amplitudes can be obtained.

For example, by operating in a bi-stable dynamic regime, every other seed pulse can be used to clear out the gain within the gain medium so that energy extraction pulses can experience gain after a uniform gain build up. The amplified back scattered signal can then be sent to a beam dump. By using a back reflection of a small portion of the output beam to clear out the residual gain, it is possible to achieve stable operation at frequencies that would otherwise provide a chaotic or otherwise unstable operation. In this regard, the back reflected portion may simply be a surface glint that is deflected and then redirected along a beam path through the multi-pass amplifier such that the output is separable from the input.

Focusing may be compensated by reimaging the gain medium onto a second surface. For example, focus compensation may be achieved by choosing the optical spacing in the system for the formation of the image at the second surface. Additionally, reimaging reasonably ensures that the spot size is approximately the same size on the gain medium after each pass even if the thin disk is focusing or defocusing. Since the beam is nearly identical on each pass, birefringence can be compensated by introducing a quarter wave plate between each pass.

The signal beam generally undergoes an intermediate focus between the focusing elements. At high power, the system may be placed in a vacuum or filled with a gas that is difficult to ionize. The pump beam may be reimaged through multiple passes of the disk using the same focusing optics that are used to reimage the signal beam. If the pump beam is provided by fiber, it may be desirable to use a collimating optic so that the fiber surface is imaged onto the disk. In this case, the pump beam may not undergo an intermediate focus and the collimating optical focal length may be chosen to provide the desired magnification in the pump beam image on the disk. Alternatively, free space propagation may be used

from the pump laser source and the pump energy may be injected into the laser system in much the same way as the signal beam.

The pump and signal beam may be co-propagated along the same beam path or they may be propagated through the same optics using separate beam paths. Alternatively, a separate multi-pass optical system may be used for the pump. In any case, the pump optical system may reimage the pump beam at the disk or onto a second reflective surface.

Signal beam injection optics may be used for the signal beam, where they may provide an intermediate signal beam focus between the imaging optics. By placing the signal beam waist between the imaging optics, a larger beam footprint can be achieved on the gain medium. Additionally, pump beam injection optics may be used to condition the pump beam prior to injection into the multi-pass laser system. If the pump source is provided through a fiber, the pump beam injection optics may, in conjunction with multi-pass optics, form an image of the pump fiber onto the gain medium with a desired magnification. If the pump beam is a spatially coherent source, the pump injection optics may be used to form an intermediate focus or beam waist between the imaging optics.

Multiple beam paths may be utilized, sharing at least one gain medium. Some of the multiple beam paths may be used to sequentially provide additional passes for the signal beam. Some of the multiple beam paths may be utilized for a separate pump beam propagation path. An optical switch may be utilized to select a subset of the multiple beam paths for the gain extraction, so that switching between the multiple beam paths can occur at lower power. Some of the multiple beam paths may be used for gain clearing to stabilize output pulse operations. This may be performed by clipping some fraction of the output beam and sending it back through the amplifier system to extract residual gain. This may have the effect of providing a consistent gain buildup from pulse to pulse and avoid chaotic or multi-stable operation.

Baffles or masks may be used to suppress Amplified Spontaneous Emission (ASE) within the system. For example, the angle subtended by a refocusing element (e.g. parabolic or off axis parabolic) relative to the gain region may be substantial, in order to operate over the multiple separable beam paths. Consequently a significant fraction of the emitted fluorescence may be redirected to additional passes through the gain medium. However, the signal beam (and possibly the pump beam) typically uses only a fraction of the focusing element. In order to suppress ASE, masks or baffles may be used to eliminate reimaging paths that are not used by the amplifier. Ideally, the mask or baffles would be placed between the focusing elements (e.g. parabolic or off axis parabolic) to eliminate unused optical paths.

Reimaging optics may also be used to reimage the signal and/or the pump spot on more than one conjugate image plane so as to share the same optical axis or have a parallel optical axis. If a parallel optical axis is used, the reimaging optics may be cut to optimize the shape for the multiple beam passes of the design. If reimaging is performed with parabolic surfaces, a pair of off axis parabolas may be used with a parallel optical axis.

The spacing between the reimaging optics may be adjusted to compensate for focusing or defocusing within one or more gain mediums. For example, reflectors (e.g., amplifier disk, mirror, adaptive optics, etc.) may be fixed relative to their respective imaging optics and the distance from one reflector/imaging optic set and the second set may be adjusted. This compensation may be performed actively or even automatically (e.g., via feedback control) so that the system remains compensated (e.g., in the event that the pump power

increases, the system heats up, and/or as other system parameters are adjusted). An image of the spot size on one of the reflectors can be used to provide focus control compensation. The number of passes within the amplifier may be controlled by the tilt of one or more of the optical elements (e.g., one of the reflectors). The number of passes and output alignment can also be actively controlled via the tilt of the optical elements.

In one embodiment, an optical amplifier includes first and second parabolic reflectors, a first reflective element in optical communication with the first parabolic reflector, and a gain module in optical communication with the second parabolic reflector. The gain module has a gain medium and a second reflective element optically coupled to the gain medium. The second parabolic reflector is operable to reflect optical energy to the gain module from different locations on the second parabolic reflector to impart gain on the optical energy. The second parabolic reflector is further operable to reflect the optical energy to the first parabolic reflector from different locations on the second parabolic reflector. The first and second parabolic reflectors have/share a common optical axis. The distance between the first and second parabolic reflectors may be adjustable. For example, the first and second parabolic reflectors may be mounted on movable mounts that allow the reflectors to be moved further apart or closer to one another. This type of adjustment may allow for various corrections (e.g., phase distortion). In one embodiment, the optical amplifier also includes a detector operable to detect the phase deformation in the beam and a controller operable to process the detected phase deformation to change the position of at least one of the first and the second parabolic reflectors.

In another embodiment, an optical amplifier includes first and second parabolic reflectors. Each of the first and second parabolic reflectors has an optical axis that is substantially parallel to the other. The optical amplifier also includes a first reflective element in optical communication with the first parabolic reflector and a gain module in optical communication with the second parabolic reflector. The gain module has a gain medium and a second reflective element optically coupled to the gain medium. The second parabolic reflector is operable to reflect optical energy to the gain module from different locations on the second parabolic reflector to impart gain on the optical energy. The second parabolic reflector is further operable to reflect the optical energy to the first parabolic reflector from different locations on the second parabolic reflector. Since the optical axis of the first parabolic reflector is substantially parallel to the optical axis of the second parabolic reflector, a beam of the optical energy may impinge the gain medium is substantially the same location with each pass (e.g., within the same cross-section on the gain medium). The distance between the first and second parabolic reflectors may be adjustable. The first and second parabolic reflectors may also be mounted on movable mounts that allow the reflectors to be moved farther apart or closer to one another (e.g., to correct phase distortions).

In either embodiment, the gain medium is generally a thin disk gain medium. For example, a relatively thin dopant material may be configured with the second reflective element so as to provide gain to the optical energy each time it reflects off the second reflective element. The thin disk gain medium may be configured from a variety of dopant materials, including ytterbium, erbium, thulium, holmium, chromium, and even various combinations thereof. In one embodiment, a gain medium is alternatively or additionally configured with the first reflective element with the same or different thin disk gain material. For example, the first reflective element may be

configured with a thin disk gain medium having a different dopant material so as to provide different gain effects, such as bandwidth broadening. In any case, the thin disk gain mediums may be configured with host materials selected from a group consisting of: KYW; KGW; Lu₂O₃; and YAG.

The optical amplifier may be configured with a controller that is operable to tilt the gain module and/or the first reflective element to control the gain of the optical energy. For example, the controller may generate a signal that is used to tilt the gain module and/or the first reflective element such that the number of reflections off the parabolic reflectors changes and correspondingly changes a number of reflections off the gain medium, thereby controlling the gain of the optical energy through the tilt of the reflective elements. In any case, a footprint of the optical energy on the gain medium may be substantially similar after each traversal of the optical energy through the optical amplifier.

In one embodiment, a pump energy source is operable to stimulate the gain medium with pump energy and amplify the optical energy. The first parabolic reflector may have an aperture operable to eject the optical energy from the optical amplifier. In this regard, the optical amplifier may also include reflector module (e.g., highly reflective mirrors, partially reflective mirrors, lenses, etc.) operable to redirect the optical energy ejected from the aperture into the optical amplifier to increase the gain of the optical energy. Alternatively or additionally, the second parabolic reflector has an aperture operable to eject the optical energy from the optical amplifier. In this regard, the optical inputs may also include a reflector module operable to redirect the optical energy ejected from the aperture into the optical amplifier to increase the gain of the optical energy.

In one embodiment, the first reflective element is a deformable mirror. For example, the optical amplifier may also include a controller and at least one actuator. The controller may be operable to generate a control signal that directs the actuator to deform the deformable mirror to direct propagation of the optical energy along the second parabolic reflector and/or reduce the phase distortion on the optical energy.

The first reflective element may be operable to provide phase correction to the optical energy (e.g., via positioning and/or focusing effects). The first reflective element may be operable to provide a conjugate image plane to the second reflective element. The first and second parabolic reflectors may have different sizes, the smaller of the first and second parabolic reflectors being operable to input the optical energy to the optical amplifier to initially reflect off the larger parabolic reflector.

The first and second parabolic reflectors may be operable to provide multiple spatially distinct beam paths for reimaging on the gain medium. For example, the multiple beam paths may be sequentially connected for multiple loops through the optical amplifier. Alternatively or additionally, multiple beams of optical energy may be propagated into the optical amplifier along different elevations. For example, one of these beam paths may be utilized to clear gain from the gain medium.

The optical amplifier may also include one or more intermediate focusing elements to increase a beam footprint of the optical energy on the gain medium and increase the gain of the optical energy. In one embodiment, the first and second parabolic reflectors maintain an intermediate focus for the optical amplifier.

In one embodiment, the optical energy is a first signal beam of optical energy and the second parabolic reflector is operable to additionally reflect a second signal beam of optical energy to the gain module from different locations reflector

on the second parabolic reflector. In such a case, the reflection locations on the second parabolic of the first signal beam are different from the reflection locations on the second parabolic of the second signal beam. In this regard, the second signal beam may be operable to clear gain from the thin disk gain medium and lower a population of an upper energy state in the gain medium. Alternatively, the second signal beam may be operable to clear gain from the thin disk gain medium and lower a population of an upper energy state in the gain medium. In another alternative, the optical energy is a signal beam of optical energy and the second parabolic reflector is operable to additionally reflect a beam of pump energy to the gain module from different locations on the second parabolic reflector to stimulate the thin disk gain medium. In such a case, the reflection locations on the second parabolic of the signal beam are different from the reflection locations on the second parabolic of the pump beam.

In another embodiment, the optical amplifier includes third and fourth parabolic reflectors and a third reflective element in optical communication with the third parabolic reflector. The gain module is in optical communication with the fourth parabolic reflector. The fourth parabolic reflector is operable to reflect pump energy to the gain module from different locations on the fourth parabolic reflector to stimulate the gain medium. The fourth parabolic reflector is further operable to reflect the pump energy to the third parabolic reflector from different locations on the fourth parabolic reflector. The third reflective element is positioned between the third and fourth parabolic reflectors.

The optical amplifier may also include a plurality of baffles between the first and second parabolic reflectors operable to block unintentional fluorescence within the optical amplifier. The optical amplifier may also include a saturable absorber operable to reduce amplified spontaneous emission within the optical amplifier. For example, the saturable absorber may be configured with the first reflective element, the second reflective element, the first parabolic reflector, the second parabolic reflector, or a combination thereof.

The optical amplifier may also include a switch and a background suppression module operable to remove amplified spontaneous emission from the optical energy. The switch is operable to synchronize propagation of the optical energy into the optical amplifier and leave the amplified spontaneous emission within the background suppression module. The background suppression module may include a saturable absorber operable to reduce the amplified spontaneous emission.

The optical amplifier may also include a reflective configuration external to the first and second parabolic reflectors. The reflective configuration is operable to provide an optical cavity that oscillates the optical energy through the optical amplifier. For example, the reflective configuration may include a saturable absorber mirror operable to provide a mode locked cavity. Alternatively or additionally, the optical amplifier may include means for injecting the optical energy into the optical cavity to provide a regenerative amplifier.

In one embodiment, the first and second parabolic reflectors, the gain module, and the first reflective element provide a first optical configuration and the optical amplifier includes a second optical configuration. The second optical configuration includes third and fourth parabolic reflectors, a third reflective element in optical communication with the third parabolic reflector, and another gain module in optical communication with the fourth parabolic reflector. The other gain module has a gain medium and a fourth reflective element optically coupled to the gain medium of the other gain module. The fourth parabolic reflector is operable to reflect the

optical energy to the gain module from different locations on the fourth parabolic reflector to impart gain on the optical energy. The fourth parabolic reflector is further operable to reflect the optical energy to the third parabolic reflector from different locations on the fourth parabolic reflector. The second optical configuration is operable to provide sequential amplification of the optical energy from the first optical configuration. The first and second optical configurations may be separated to by two focal lengths (e.g., so as to maintain conjugate image planes).

The optical amplifier may also include a first optical configuration operable to input the optical energy into the optical amplifier and a second optical configuration operable to eject the optical energy from the optical amplifier after amplification. In this regard, the first optical configuration includes a dynamic optic operable to change a wavefront of the optical energy impinging the gain medium and the second optical configuration includes a detector operable to provide feedback to change a focusing aspect of the dynamic optic and change the wavefront of the optical energy.

The optical amplifier may also include a redirection module operable to redirect the optical energy into the optical amplifier for additional amplification. The redirection module includes a pair of reflective elements operable to separate inputs to the optical amplifier by two focal lengths. The redirection module may also include a plurality of lenses operable to, in conjunction with the pair of reflective elements, provide conjugate image planes throughout the optical amplifier.

In another embodiment, an optical system includes first and second parabolic reflectors, a first reflective element in optical communication with the first parabolic reflector, and a second reflective element in optical communication with the second parabolic reflector. The first parabolic reflector is operable to reflect optical energy to the first reflective element from different locations on the first parabolic reflector. The first parabolic reflector is further operable to reflect the optical energy to the second parabolic reflector from different locations on the first parabolic reflector. The second parabolic reflector is operable to reflect the optical energy to the second reflective element from different locations on the second parabolic reflector. The second parabolic reflector is further operable to reflect the optical energy to the first parabolic reflector from different locations on the second parabolic reflector. The first and second parabolic reflectors have a common optical axis. The first reflective element, the second reflective element, or a combination thereof may be configured with a thin disk gain medium that is operable to impart gain on the optical energy.

In another embodiment, an optical amplifier includes a parabolic reflector, a first reflective element in optical communication with the first parabolic reflector, and a gain module in optical communication with the parabolic reflector. The gain module has a gain medium and a second reflective element optically coupled to the gain medium. The parabolic reflector is operable to reflect optical energy to the gain module from different locations on the parabolic reflector to impart gain on the optical energy.

In another embodiment, a method includes propagating optical energy into a multi-pass amplifier. The multi-pass amplifier includes first and second parabolic reflectors having a common optical axis. While in the multi-pass amplifier, the method includes directing the optical energy via the first and second parabolic reflectors to a thin disk gain medium and a reflective element to increase optical gain in the optical energy. The method also includes ejecting the optical energy from the multi-pass amplifier.

In another embodiment, an optical amplifier includes first and second parabolic reflectors, a first reflective element in optical communication with the first parabolic reflector, and a gain module in optical communication with the second parabolic reflector. The gain module has a gain medium and a second reflective element optically coupled to the gain medium. The first and second parabolic reflectors have a common optical axis and are operable to controllably reflect optical energy from different locations to the gain medium.

In another embodiment, an optical amplifier includes a thin disk gain medium operable to impart gain on optical energy and first and second parabolic reflectors. The first parabolic reflector is operable to reflect the optical energy to the thin disk gain medium multiple times. The first and second parabolic reflectors share a common optical axis. That is, each of the first and second parabolic reflectors has an optical axis. Each optical axis of the first and second parabolic reflectors is generally along the same line.

In another embodiment, an optical system includes first and second parabolic reflectors. Each of the first and second parabolic reflectors has an optical axis that is substantially parallel to the other. The optical system also includes a first reflective element in optical communication with the first parabolic reflector and a second reflective element in optical communication with the second parabolic reflector. The first parabolic reflector is operable to reflect optical energy to the first reflective element from different locations on the first parabolic reflector. The first parabolic reflector is further operable to reflect the optical energy to the second parabolic reflector from different locations on the first parabolic reflector. The second parabolic reflector is operable to reflect the optical energy to the second reflective element from different locations on the second parabolic reflector. The second parabolic reflector is further operable to reflect the optical energy to the first parabolic reflector from different locations on the second parabolic reflector. The first and second parabolic reflectors have different sizes. The smaller of the first and second parabolic reflectors is operable to input the optical energy to the optical amplifier to initially reflect off the larger parabolic reflector. The first reflective element, the second reflective element, or a combination thereof may be configured with a thin disk gain medium that is operable to impart gain on the optical energy.

In another embodiment, an optical amplifier is operable to impart gain on optical energy and includes first, second, and third parabolic reflectors. The first parabolic reflector has a larger reflective surface than the second and third parabolic reflectors. The second and third parabolic reflectors are in optical communication with the first parabolic reflector. The optical amplifier also includes a gain module in optical communication with the first parabolic reflector. The gain module has a first reflective element and a gain medium optically coupled to the first reflective element to impart the gain on the optical energy. The optical amplifier also includes a second reflective element in optical communication with the second parabolic reflector. The optical amplifier also includes a third reflective element in optical communication with the third parabolic reflector. The third parabolic reflector may have an aperture operable to eject the optical energy from the optical amplifier. The optical amplifier may also include a reflector module operable to redirect the optical energy ejected from the aperture into the optical amplifier to increase the gain of the optical energy. The second parabolic reflector may have an aperture operable to eject the optical energy from the optical amplifier. The optical amplifier may also include a reflector module operable to redirect the optical energy ejected from the aperture into the optical amplifier to increase

the gain of the optical energy. Each of the first, second, and third parabolic reflectors may include an optical axis. The optical axis of the first, second, and third parabolic reflectors are substantially parallel. Again, this may assist in ensuring that the optical energy impinges again medium at substantially the same location/beam cross-section cross-section.

In another embodiment, a method includes propagating optical energy into a multi-pass amplifier. While in the multi-pass amplifier, the method includes directing the optical energy to a thin disk gain medium multiple times via first and second parabolic reflectors to increase optical gain in the optical energy. Each of the first and second parabolic reflectors has an optical axis that is substantially parallel to the other. The method also includes ejecting the optical energy from the multi-pass amplifier.

In another embodiment, an optical amplifier includes a thin disk gain medium operable to impart gain on optical energy and first and second parabolic reflectors operable to reflect the optical energy to the thin disk gain medium multiple times. Each of the first and second parabolic reflectors has an optical axis that is substantially parallel to the other.

In one embodiment, a laser system includes an optical amplifier that includes a gain medium operable to amplify a laser pulse via multiple passes of the laser pulse through the gain medium. The laser system also includes a replicator optically coupled to the optical amplifier and operable to remove a portion of optical energy from the laser pulse to generate a copy of the laser pulse for input to the optical amplifier. The optical amplifier is may also be operable to amplify the copied laser pulse.

The replicator may also be operable to remove a portion of optical energy from the amplified copied laser pulse to generate another copy of the laser pulse, and wherein the laser system further includes an output that is operable to combine the laser pulses as a burst of laser pulses. For example, the output may be operable to separate the laser pulses in the burst to provide a pulse repetition frequency in the megahertz range. The replicator may also be operable to delay the input of the copied laser pulse into the optical amplifier to clear gain from the gain medium prior to a return pass of the original laser pulse through the gain medium.

The laser system may also include a recycler optically coupled to the optical amplifier and operable to selectively output a first set of laser pulses from the optical amplifier for transmission from the laser system and to selectively input a second set of laser pulses to the replicator for copying. The laser system may also include an entry port operable to select laser pulses at a user defined pulse repetition frequency for input to the optical amplifier. Alternatively, the entry port may be operable to select laser pulses according to a modulation pattern for input to the optical amplifier.

The optical amplifier may be a Walk Off Multi-Pass Amplifier. For example, the optical amplifier may include a gain module, wherein the gain medium is configured within the gain module as a thin disk gain medium disposed on a first reflector, a second reflector that defines an optical cavity for the multi-pass optical amplifier, three parabolic reflectors configured within the optical cavity and operable to cause multiple incidents of the original laser pulse on the gain medium to amplify the original laser pulse, and a multiplexing reflector operable to change beam spot locations of the original laser pulse on the parabolic reflectors. Alternatively, the optical amplifier may include first, second, and third parabolic mirrors, and a multiplexer operable to direct the original laser pulse along multiple paths in or about a first plane between the first and second parabolic mirrors and to direct the original laser pulse along multiple paths in or about a

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second plane to the third parabolic mirror to cause multiple incidents of the original laser pulse on the gain medium to amplify the original laser pulse, wherein the first and second planes are different. In another alternative, the optical amplifier may include a gain module, wherein the gain medium is configured within the gain module as a thin disk gain medium disposed on a first reflector. This optical amplifier may also include a second reflector that defines an optical cavity for the multi-pass optical amplifier, three parabolic reflectors positioned within the optical cavity, wherein a first of the three parabolic reflectors is smaller than a second and a third of the three parabolic reflectors for inputting the original laser pulse into the multi-pass optical amplifier, and a multiplexing reflector operable to change placement of incidence of the original laser pulse within at least one pair of beam spot sets on the parabolic reflectors. The original laser pulse loops through the multi-pass optical amplifier having incidence within a first of the at least one pair of beam spot sets on the first and second parabolic reflectors. The original laser pulse reflects from the third parabolic reflector to the multiplexing reflector after completing a first loop through the multi-pass optical amplifier with incidence of the original laser pulse within the first pair of beam spot sets on the first and second parabolic reflectors. The original laser pulse reflects from the multiplexing reflector to the third parabolic reflector to initiate a second loop through the multi-pass optical amplifier with incidence of the original laser pulse within at least one other beam spot set on the first and second parabolic reflectors that differs from the first pair of beam spot sets on the first and second parabolic reflectors.

The replicator may include a piezoelectric device operable to controllably delay the copied laser pulse with respect to the original laser pulse. Alternatively, the replicator may include a piezoelectric device operable to controllably delay the original laser pulse with respect to the copied laser pulse. Alternatively or additionally, the replicator may include an optic operable to reflect the portion of the optical energy of the laser pulse at least twice to generate the copy of the laser pulse, transmit the remaining portion of the optical energy of the laser pulse, and transmit the copied laser pulse after transmitting the remaining portion of the optical energy of the laser pulse. Alternatively or additionally, the replicator may include an optic operable to reflect the portion of the optical energy of the laser pulse to generate the copy of the laser pulse, reflect the remaining portion of the optical energy of the laser pulse at least twice, and transmit the original laser pulse after transmitting the copied laser pulse.

It should be noted that each of the above concepts may be combined in various ways to provide multi-pass amplification. With each of these concepts in mind, various embodiments of Walk Off Multi-Pass Amplifiers (WOMPAs) are now presented in the following drawings and their descriptions. In some embodiments, Off Axis Parabola (OAP) WOMPAs are presented while in other embodiments Axial Reimaging (ARI) WOMPAs are presented. The details of such are provided to show exemplary WOMPA embodiments and are not intended to limit the invention to any particular architecture.

BRIEF DESCRIPTION OF THE DRAWINGS

Some embodiments of the present invention are now described by way of example and with reference to the accompanying drawings. The same reference number represents the same element or the same type of element on all drawings.

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FIGS. 1-4 illustrate various exemplary focal considerations for a multi-pass laser architecture.

FIG. 5 illustrates an exemplary WOMPA laser architecture.

FIGS. 6-10 illustrate various exemplary optical configurations employing the WOMPA laser architecture.

FIGS. 11 and 12 illustrate other exemplary WOMPA laser architectures.

FIGS. 13 and 14 illustrate exemplary beam spot patterns of an off axis parabolic mirror (OAP) used in the WOMPA laser architecture.

FIGS. 15-37 illustrate various exemplary optical configurations employing a WOMPA laser architecture.

FIG. 38 is a block diagram illustrating exemplary gain detection and gain control of a WOMPA system.

FIG. 39 is a block diagram of an exemplary CVBG-based architecture for stretching and compressing laser pulses.

FIGS. 40-41 illustrate an exemplary serrated aperture for use in a WOMPA system.

FIG. 42 is a block diagram of an exemplary chamber used in preventing optical breakdown within a WOMPA system.

FIG. 43 illustrates another exemplary embodiment in which a WOMPA system is configured within a chamber.

FIGS. 44A and 44B illustrate an exemplary cooling technique of an active mirror of a WOMPA system.

FIG. 45 illustrates a WOMPA system employing a plurality of baffles.

FIG. 46 illustrates an exemplary optical configuration having "closed-loop" control of a deformable mirror for use with a WOMPA system.

FIGS. 47 and 48 are block diagrams of exemplary systems employing a WOMPA system.

FIGS. 49 A-C illustrate a multi-pass optical amplifier in another exemplary embodiment.

FIG. 50 illustrates OAP faces of the multi-pass optical amplifier of FIG. 49 A-C along with exemplary optical propagation.

FIG. 51 is a block diagram of another exemplary multi-pass optical configuration.

FIG. 52 is a block diagram of a mount and a thin disk gain medium/reflective module.

FIG. 53 is a block diagram of a multi-pass optical amplifier in one exemplary embodiment.

FIG. 54 illustrates propagation of a signal beam through the multi-pass optical amplifier of FIG. 53.

FIG. 55 illustrates propagation of a pump beam through the multi-pass optical amplifier of FIG. 53.

FIG. 56 is a block diagram of a laser system that is operable to fire a burst of laser pulses.

FIGS. 57-59 are block diagrams of various replicators for use in the laser system of FIG. 56.

DETAILED DESCRIPTION OF THE DRAWINGS

The figures and the following description illustrate specific exemplary embodiments of the invention. Various arrangements that, although not explicitly described or shown herein, may be devised to embody the principles of the invention and are, therefore, included within the scope of the invention. Furthermore, any examples described herein are intended to aid in understanding the principles of the invention and are to be construed as being without limitation to such specifically recited examples and conditions. As a result, the invention is not to be limited to the specific embodiments or examples described below.

The embodiments shown and described herein are categorized to assist the reader in understanding the various aspects of the invention. The categories are as follows: 1. Design

Choice Considerations; 2. Multi-Pass Amplifier Configurations; 3. Gain Control of a Multi-Pass Amplifier; 4. Components Operable with a Multi-Pass Amplifier; 5. Exemplary Systems Employing Multi-Pass Amplifiers; and 6. Additional Embodiments.

1. Design Choice Considerations

To provide a modular, compact, and efficient high average power/high energy amplifier module with little optical distortion and relatively good beam quality, an appropriate pump absorption and temperature distribution should be maintained. In this regard, low net thermal loading may be achieved by incorporating near-resonant wavelength pumps that are available in certain gain media. Additionally, a large system gain may require a long effective propagation distance through the material of the gain medium. Such may be accomplished via the laser architectures presented herein as they provide a relatively large number of amplification passes through the gain medium.

Thermal management is fundamental to scaling any solid-state laser architecture to high average power. Temperatures need to be maintained at low enough levels to provide sufficient gain. Temperature gradients also need to be minimized to avoid beam deformation effects. Within the laser gain medium, non-uniform thermal distributions with gradients transverse to the laser beam propagation direction modify the index of refraction and lead to optical phase distortions of the laser beam. Elevated temperatures also lead to a reduction in gain due to increased occupancy of lower laser energy levels, especially for a quasi-three level system, such as a Yb:YAG gain medium.

In general, cooling of solid state gain media can be performed in two fundamentally different ways. Cooling may be performed on the surfaces of the gain medium where heat is conducted through the material to the surface where the heat can be extracted through any number of approaches. A second approach is to cool a volume through optical cooling. This type of volumetric cooling utilizes optical energy to extract heat within the gain medium. Volumetric cooling can occur through certain optical processes where fluorescence extracts more power than is deposited into the gain medium. Though optical cooling is generally difficult to achieve, a detailed analysis of fluorescence in a low quantum defect system can provide insights on pumping strategies to minimize a thermal load. For example, antistokes cooling may be performed while pumping the gain medium as heating may occur during amplification of ultrashort pulses. This can be achieved if the pump wavelength is longer than the average fluorescence wavelength. Though, most materials do not prove a sufficiently large absorption cross-section above the average fluorescence wavelength to make this very practical.

In conventional laser systems, cooling is performed through the surface of the gain material. In order to efficiently extract heat from the surface of a solid gain medium, the fraction of cooled surface area per heated volume is maximized. Two geometries that maximize this ratio for high power laser systems are fibers and thin disks. In the case of fibers, two dimensions are minimized and one dimension is maximized so that a large surface area to volume ratio can be obtained for efficient cooling. Additionally, fiber amplifier geometries support very large gain-length products and tend to have negligible thermal gradient effects. Fiber amplifiers, however, are not optimal for high-peak-power short pulses because extreme intensities are produced through very small cross sections of optical fibers. Nonlinear propagation effects generally occur at high intensities and limit the peak power that can be propagated through a fiber amplifier. Additional limitations in fiber amplifiers are related to amplification of spontaneous emission if a pulse repetition rate is too low.

To decrease the peak intensity of an optical pulse, one can imagine the gain volume of fiber being distorted into the shape of a rod. In this case, the same peak power can be propagated through a much larger spatial cross-section at much lower intensities to avoid the onset of nonlinear propagation effects. However, the fraction of surface area to gain volume is lower and the heat generated within a rod gain medium has a further distance to travel prior to exiting through the surface. For this reason, rod geometries tend to have much greater thermally-induced phase distortion issues than fiber geometries.

Alternatively, a reduced thermal load in a low quantum defect system, in combination with surface cooling, may provide certain advantages as one may imagine the rod geometry being shortened until a disk geometry is obtained. This disk geometry has a high surface to volume ratio and the efficiency of surface cooling is much better than a rod. In this case, multiple signal passes are used to achieve a reasonable amplification. Similarly, the pump beam may be repeatedly passed through the disk to achieve efficient absorption. Cooling from a back face of the disk is generally more efficient than cooling around the perimeter of a rod as thermal gradients are generally along the direction of optical propagation. Such may reduce the effects of thermally-induced phase deformations. High peak-power pulses can also be amplified using thin disks because power can be distributed over a larger cross sectional area, maintaining peak intensities and fluence levels well below thresholds for damage and/or deleterious nonlinear propagation effects. Accordingly, thin disks are generally advantageous for high average-power and high peak-power ultrashort laser pulse systems.

Many of the technical challenges with thin disks are related to long optical paths and thermally-induced phase distortions. Although heat can be efficiently removed from a thin disk, thermal gradients, temperature dependent indices of refraction, thermal expansion, and/or strain effects typically lead to phase distortions. For thin disk geometries where a reflective surface is included, thermo-mechanical distortions can lead to especially strong phase distortions. These distortions can also include depolarization effects, such as strain-induced birefringence. Therefore, each pass of the signal beam can lead to large accumulated phase distortions. Because of the optical path length (OPL) between each pass of the signal beam through a thin disk, phase distortions from each pass can lead to focusing or defocusing of the beam on subsequent passes. Without compensation, such may lead to optical damage when a signal beam becomes too small. Moreover, losses may occur if the signal beam "overfills" a pump spot.

Other performance factors may also influence laser design configuration with a multi-pass amplifier. For example, in FIGS. 1A and 1B, a multi-pass laser system 150 is illustrated in an unfolded form with reflectors 153 and 154 on opposite ends of the multi-pass laser amplifier optics to perform reimaging. One or both of the reflectors 153 and 154 may be configured with a gain medium so as to impart gain on optical energy 155 entering the multi-pass laser amplifier optics 150.

In order to configure the multi-pass laser amplifier optics 150 with conjugate image planes on the reflectors 153 and 154, the reflectors 153 and 154 are at the focal planes for their corresponding focusing elements (i.e., with focus f1 and f2). However, even if the two reflectors 153 and 154 are at conjugate image planes, the beam of optical energy 155 that is transmitted from one reflector to the other is approximately collimated at the reflectors 153 and 154 so that the beam of optical energy 155 does not substantially reduce or expand after each round trip. This leads to an additional requirement that focusing elements 151 and 152 be separated by approximately the sum of their two focal lengths. In order to allow the beam to enter and exit the multi-pass laser amplifier optics

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150, a slight tilt can be introduced into one of the reflectors (e.g., reflector 154). FIG. 1A shows a beam emanating from one reflective surface 154, coming to an intermediate focus between focusing elements 151 and 152, and being redirected to a second reflective surface 153. A ray trace overlays the beam to show that a first point 154a on reflective surface element 154 is imaged onto a second point 153a on reflective surface element 153. This optical configuration reimages one reflective surface to the next and maintains approximately the same beam size on each surface.

In FIG. 1B, the beam of optical energy 155 enters the amplifier 150 and is incident upon the tilted reflector 154. After multiple passes, the beam is at normal incidence on the tilted reflector 154 and passes back through the same path in the opposite direction. If the beam of optical energy 155 exits along the same path as the entrance path, it can be separated using a 1/4 wavelength plate. Alternatively, if the beam of optical energy 155 approximately reverses paths, it may be spatially separated from the incident beam at the exit. FIG. 1B shows the central ray for the beam of energy 155, without showing the focusing aspect that was previously shown in FIG. 1A.

Extending this concept, more than one of the reflectors 153 and 154 may be tilted or adjusted for a walk-off beam path as illustrated in FIG. 2. The multi-pass laser amplifier optics 150 may be configured to enter and exit the beam of the optical energy 155 at either end of the multi-pass laser amplifier optics 150. For example, the beam of optical energy 155 may enter the multi-pass laser amplifier optics 150 via the reflective element 154 as illustrated in FIG. 3A. If at least one of the reflective elements 153 and 154 has a focusing or defocusing effect (e.g., via a deformable mirror or thermally induced focusing/defocusing phase deformation), the optical power of the optical energy 155 can be compensated by adjusting the distance between the main focusing elements 151 and 152 as illustrated in FIG. 3B. The convergence/divergence of the beam of optical energy 155 incident on the reflector 154 matches the divergence/convergence of the beam after reflection, as shown by the distances S_{L1} and S_{L2} . Note that the distances (f_1 and f_2) between the reflectors 153 and 154 and a given focusing element (152 and 151, respectively) remains at the total focal length S_L of the focusing elements 151 and 152. The distances and focal lengths can be summarized as follows:

$$\frac{1}{S_1} + \frac{1}{S_{L1}} = \frac{1}{f_1} \quad 1)$$

$$S_1 = -2f_{D1} + f_1 \quad 2)$$

$$\frac{1}{S_{L1}} = \frac{1}{f_1} - \frac{1}{-2f_{D1} + f_1} \quad 3)$$

$$S_{L1} = f_1 - \frac{f_1^2}{2f_{D1}} \quad 4)$$

$$S_{L1} = \frac{f_1(-2f_{D1} + f_1)}{2f_{D1}} = f_1 - \frac{f_1^2}{2f_{D1}} \quad 5)$$

$$S_L = (f_1 + f_2) - \frac{1}{2} \left(\frac{f_1^2}{f_D} + \frac{f_2^2}{f_D} \right) \quad 6)$$

Thus, only the distance between the focusing elements 151 and 152 is adjusted. It should be noted that these distances are merely approximate values and that corrections and/or other adjustments may depend on the distance of the beams of the optical energy 155 from the optical axis and the focusing

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aspects of the focusing elements 151 and 152. Departures for the above derivation may be due to, for example, geometrical factors from non-idealized focusing elements. However, in more detailed simulations, we have shown that most of the effects of typical focusing variations in the reflectors 153 and 154 can be compensated by adjustments in the separation distance between the focusing elements 151 and 152.

Note that the focal lengths of the focusing elements 151 and 152 need not be identical. For example, if the focal lengths are different, the signal spot size on the reflectors 153 may be magnified with respect to the signal spot size on reflector 154. If the reflector 154 is a deformable mirror, the required packing density of actuators or the required damage threshold can be reduced by increasing the size of the signal spots on the reflector. This can be done without changing the signal spot size on the reflector 154 by making focal length f_1 larger than f_2 . The capability for asymmetric imaging, and its application for deformable mirror design freedom, can be applied to the descriptions of WOMPA embodiments described below.

With these concepts in hand, the multi-pass laser amplifier optics 150 may be "folded" by replacing the focusing elements 151 and 152 with reflectors 161 and 162 as illustrated in the multi-pass laser amplifier optics 150 of FIGS. 4A and 4B. In FIG. 4A, the distance between the two reflectors 163 and 164 is now greater than $f_1 + f_2$ in order to have enough room to fit the reflectors 161 and 162. This can be achieved if at least one of the reflectors 161 and 162 has a sufficiently negative focal length so that the distance W is greater than zero. The "walk off" is not discernable from this side view but an intermediate beam focus is illustrated in the middle 166 of the multi-pass laser amplifier optics 150. This optical configuration is advantageous because it can easily be fit into a vacuum chamber with a "tube geometry" so as to prevent optical breakdown at the intermediate beam foci. FIG. 4B illustrates a modification of the embodiment illustrated in FIG. 4A. Additional fold mirrors are inserted between the mirrors and focusing elements. This configuration allows either focusing or defocusing of the reflectors. For example, focusing elements can be mirrors instead of lenses. In this instance, however, the optical distance between the two reflectors 161 and 162 may be greater when positioned between the fold mirrors 167 and 168 the focusing elements 163 and 164. The distance $S_{L1} + S_{L2}$ can therefore be made smaller or even less than $f_1 + f_2$. This provides more flexibility in compensating for focus variations in the reflectors 161 and 162. Additionally, there are several diagnostic advantages in using the fold mirrors 167 and 168. For example, by allowing some leakage through the fold mirrors to cameras or other optical sensors, beam profiles that would also be incident on the focusing elements 163 and 164 or the reflectors 161 and 162 can be obtained. Additionally, if light from fluorescence on a thin disk gain medium leaks through the fold mirrors 167 and 168, a camera may be used to image the pump beam spot on the gain media. Alternatively, pump radiation may be transmitted through a fold mirror to be incident on a thin disk gain medium attached to a reflector.

While each of the figures illustrating the multi-pass laser amplifier optics 150 are shown with respect to the beam of optical energy 155 propagating along center axis of the multi-pass laser amplifier optics 150 in this "axial walk-off multi-pass" configuration, the walk-off multi-pass concepts in the multi-pass laser amplifier optics 150 may be extended into other "off axis walk-off multi-pass" configurations. Examples of axial and off-axis walk off multi-pass configura-

rations are illustrated in the various WOMPA systems shown and described below in the section entitled Multi-Pass Amplifier Configurations.

2. Multi-Pass Amplifier Configurations

Each of the embodiments mentioned herein may be used to implement relatively high power laser systems, such as CPA laser systems. For example, in one embodiment, a Walk-Off Multi-Pass Amplifier (WOMPA) thin disk architecture provides: flexible repetition rate selection; reconfigurable gain selection; disk focus correction for signal beam; and chirped volume Bragg grating (CVBG) stretching and compression. This reimaging WOMPA system may be seeded by a mode-locked oscillator, but may also be seeded by other CW or pulsed optical sources.

One exemplary optical design of the WOMPA laser architecture is depicted in the off axis WOMPA system **1000** of FIG. 5. The WOMPA system **1000** includes a pair of off axis parabolic mirrors (OAPs) **1003** and **1004** and a pair of reflective elements **1001** and **1002** (e.g., highly reflective mirrors). Configured with one of the reflective elements **1001** and **1002** is a thin disk gain medium. For example, the reflective element **1001** may have a thin disk gain medium disposed on the surface of the reflective element **1001** so as to provide optical gain to the signal beam **1007** when the thin disk gain medium is pumped with energy (e.g., optical energy from edged pumping diodes, surface pumping optical energy, or the like). In this regard, the reflective element **1001** is generally referred to herein as the thin disk gain medium. Although, the invention is not intended to be limited to a thin disk gain medium simply affixed to the reflective element **1001**, as other embodiments may implement gain mediums in other manners.

In this embodiment, the optical design of the WOMPA system **1000** is essentially a “4-f” system in which a reflecting thin disk gain medium **1001** and a second reflector **1002** are at conjugate image planes. Multiple passes through the gain medium of the reflective element **1001** are achieved through angular multiplexing. The OAPs **1003** and **1004** shown in the diagram are imaging elements, which provide flexibility for the design. The signal beam **1007** from the laser **1006** propagates through the optical element **1005** (e.g., a lens, filter, beam splitter, or the like) to enter the WOMPA system **1000** and is brought to an intermediate focus between the two OAPs **1003** and **1004** so that the beam is collimated after reflection from the OAP **1003**. After reflection from the thin disk gain medium of the reflective element **1001**, the signal beam is reflected again from the OAP **1003**. Thereafter, the signal beam again passes through an intermediate focus and is incident on the OAP **1004**. The beam is collimated by the OAP **1004** and is incident on the reflective element **1002**. The signal spot on the reflective element **1002** is an image of the signal spot on the thin disk gain medium of the reflective element **1001**. A slight tilt of the reflective element **1002** directs the reflected beam on the OAP **1004**. After multiple passes, the signal beam eventually intercepts the thin disk gain medium of the reflective element **1001** (or the reflective element **1002**) at normal incidence (as viewed from above) and reverses its path (as viewed from above). The total number of bounce passes is selected by the tilt on the mirror **1002**. By inserting polarization rotation optics, thin film polarizers at the input to the system (e.g., the optical element **1005**), the input and output beams can be separated. Additionally, if any depolarization effects are observed, a quarter wave plate **1010** can be inserted in front of the thin disk gain medium or the reflective elements **1001** and **1002** for effective correction.

One advantage of the WOMPA system **1000** is that the gain medium of the reflective element **1001** need not be flat so that it may impart a focusing or defocusing effect on the signal beam **1007**. The reimaging and uniform spot size aspects of the WOMPA **1000** can be recovered by simply changing the distance between the two OAPs **1003** and **1004**, while keeping the distance between the OAPs **1003/1004** and the reflective elements **1001/1002** at their respective focal planes fixed. Adjustment of a translation stage may compensate for thermally induced focus on the disk **1001**, thereby avoiding the daunting challenge of thermal deformation compensation found in many thin disk lasers.

With a few tens of passes, pulse amplification has been experimentally proven to increase by a factor of 10^4 (e.g., 10 nJ to 100 μ J). Additionally, laser amplification may be controlled via the tilting of one or both of the reflective elements **1001** and **1002**. For example, tilting the reflective element **1002** may cause the signal beam to be incident on the OAP **1003** fewer or more times (i.e., depending on the degree of the tilt) causing the signal beam to correspondingly impinge the gain medium. The advantages of the WOMPA system **1000** include increased gain through multiple passes of the thin disk gain medium within a compact yet increased optical path length.

Although shown and described with respect to a thin disk gain medium being configured with the reflective element **1001**, the invention is not intended to be so limited. For example, a gain medium may be configured with either or both of the reflective elements **1001** and **1002**. Alternatively, the WOMPA system **1000** may be configured without a gain medium so as to provide a compact amplifier or laser oscillator with a predetermined or controllable path length (e.g., based on the controlled tilt of the reflective elements **1001** and/or **1002**) and a correspondingly controllable delay for passing through the system. Additionally, this WOMPA system **1000** may be used to provide certain focusing aspects on a beam passing through. Other embodiments of the WOMPA system **1000** and their various implementations in laser systems and optimal configurations are shown and described below.

FIG. 6 illustrates the WOMPA system **1000** in another exemplary embodiment. In this embodiment, the WOMPA system **1000** is configured with optical elements **1101**, **1102**, and **1103** that impart certain optical effects on the signal beam **1007**. More particularly, the lenses **1102** and **1103** form a beam expander module **1104** that expands/compresses the signal beam **1007** through a diaphragm **1101** prior to entering the WOMPA **1100**. By focusing the signal beam **1007** through the diaphragm **1101**, the diameter of the signal beam **1007** can be altered to change the beam spot size on the thin disk **1001** and the mirror **1002**. The diaphragm may be positioned at a plane that is imaged on the reflectors **1001** and **1002**. For example, for a perfect 4-f system where **1005** is a 1-f lens, the diaphragm may be placed a distance of 1-f behind the lens. By imaging the diaphragm **1101** onto the reflectors, a virtual mask is obtained which prohibits light from being incident on the thin disk gain medium outside of a prescribed region. This is particularly useful if higher-order phase distortions outside of a sub-region on the disk result in the down-stream development of “hot-spots”. The placement of the diaphragm substantially reduces or eliminates the possibility of these higher-order phase distortion sub-regions being illuminated even if the input beam is spatially varying. The diaphragm may also be used to decrease the beam spot size on the OAPs **1003** and **1004**, allowing for more round trips of the optical energy through the gain medium so as to increase the gain of the optical energy. That is, by increasing

the number of passes of the signal beam through the WOMPA system **1000** via the multiple impingements of the OAPs **1003** and **1004**, the gain of the signal beam **1007** increases dramatically as each impingement of the signal beam **1007** on an OAP **1003/1004** constitutes a pass of the signal beam **1007** through the material of the thin disk gain medium **1001** that further increases the gain of the signal beam **1007**. Thus, the gain of the signal beam **1007** may be scaled according to the number of passes through the thin disk gain medium **1001** via control of the beam spot size of the signal beam **1007** and/or the change in the number of impingements on the OAPs **1003** and **1004**. It should be noted that the diaphragm **1101** may be a simple optical aperture or may include a more complete beam shaping capability including gradient intensity filters.

FIG. 7 illustrates another exemplary optical configuration **1200** with the off axis WOMPA system **1000**. In this embodiment, the optical configuration **1200** is configured with an optical isolator **1202** in conjunction with the WOMPA system **1000**. The optical isolator **1202** provides separation of input and output signal beams **1203-I** and **1203-O**, respectively. For example, the optical isolator **1202** receives the input signal beam **1203-I** with a polarization beam splitter **1208-1** that filters off any undesired polarizations in the signal beam **1203-I**. The signal beam **1208-I** then passes through the optical element **1207** to change the polarization of the signal beam (e.g., rotate the phase of the signal beam). Additionally, the optical element **1207** may impart certain optical effects on the signal beam **1203-I** (e.g., certain focusing aspects to change the spot size of the signal beam). Thereafter, the signal beam **1203-I** passes through another beam splitter **1208-2** that is subsequently used to filter off any undesirable polarizations on the output beam **1203-O** once it returns from the WOMPA system **1000**.

The laser system **1200** also includes an optical splitter **1205** (e.g. dichroic mirror) that is used to input the pump beam **1204** and the input signal beam **1203-I** to the WOMPA system **1000**. For example, the laser system **1200** may be configured with a pump energy source that is used to stimulate the thin disk gain medium of the reflective element **1001** via multiple passes of the pump beam **1204** through the WOMPA system **1000**. The signal beam **1203-I** entering the WOMPA system **1000** extracts the energy provided by the pump beam **1204**, thereby amplifying the signal beam **1203-I** with each pass through the gain medium in the WOMPA system **1000**. The amplified signal beam **1203-O** then exits the WOMPA system **1000** and passes through the beam splitter **1205** by having a spectrum that is transmissive to the optical splitter **1205**. As mentioned, the amplified signal beam **1203-O** then passes through the optical beam splitter **1208-2** to filter off any undesirable effects imparted on the signal beam **1203-O** during the amplification process. The optical element **1207** rotates the polarization of the signal beam **1203-O** such that it may be reflected off the beam splitter **1208-1** to eject the signal beam from the laser system **1200**.

FIG. 8 illustrates the WOMPA system **1000** in another exemplary optical configuration **1300**. In this embodiment, the optical configuration **1300** is also configured with the optical isolator **1202**, the optical beam splitter **1205**, and the pump energy source **1204**, in conjunction with the WOMPA system **1000**. The optical configuration **1300** also includes an optical module **1301** that provides a double loop regime to further increase amplification of the signal beam **1203**. For example, the optical module **1301** may be used to propagate the signal beam **1203-I** into the WOMPA system **1000** for a single loop amplification by the WOMPA system **1000**, where the term loop refers to propagation in and out of the optical element **1005** and may include many reflections from

the reflectors **1002** and **1001**. Once the amplified signal beam **1203** exits the WOMPA system **1000**, the signal beam **1203** propagates into the optical module **1301** such that it may be reflected back into the WOMPA system **1000** for additional amplifications before exiting the laser system **1300**. In FIG. 8, the lens **1102** is explicitly shown as a separate component from the optical element **1005**.

In this embodiment, the optical module **1301** includes a 45° quartz rotator **1302**, a Faraday rotator **1303**, a thin film polarizer **1304**, and a highly reflective mirror **1305**. The input signal beam **1203-I** passes through the thin film polarizer **1304** and into the Faraday rotator **1303** where it receives a change in polarization. The thin-film polarizer **1304**, like the optical beam splitters **1208** serve to filter off any undesirable polarizations from the signal beam **1203-I**. The Faraday rotator **1303** rotates the polarization of the signal beam **1203-I** by 45° where it passes through the 45° quartz rotator **1302** and the optical beam splitter **1205** to enter the WOMPA system **1000**. On return, the signal beam **1203** passes through the optical beam splitter **1205** and the 45° quartz rotator **1302** into the Faraday rotator **1303**. The Faraday rotator **1303** rotates the signal beam **1203-I** again by 45° such that it reflects off the thin-film polarizer **1304** into the highly reflective mirror **1305**. Thereafter, the signal beam **1203-I** passes through the Faraday rotator **1303** and quartz rotator **1302** to rotate polarization by another 90° such that it again passes into the WOMPA system **1000**. The WOMPA system **1000** then amplifies the signal beam **1203-O** a second time and propagates the signal beam through the optical module **1301** into the optical isolator **1202**. That is, the Faraday rotator **1303** rotates the polarization of the signal beam **1203-O** such that it passes through the thin-film polarizer **1304** and into the optical isolator **1202** for ejection from the optical configuration **1300**.

FIG. 9A illustrates the WOMPA system **1000** in another exemplary embodiment. In this embodiment, the optical configuration **1400** is a multi-loop configuration that allows an input beam **1408-I** to pass through the WOMPA system **1000** multiple times before exiting the optical configuration **1400**. For example, the input beam **1408-I** enters the laser system **1400** where it passes through the thin-film polarizer **1402-1**. The input beam **1408-I** then passes through a half wave plate **1403** ($\lambda/2$, e.g., where the polarization of the input beam is changed from p polarization to s polarization). The input beam **1408-I** then passes through the electro-optic modulator **1401** without additional rotation so that it reflects off the thin-film polarizer **1406-2** and into the highly reflective mirror **1407**. The electro-optic modulator **1401** may then be electronically triggered, so that after the input beam is reflected from the thin film polarizer **1402-2** its polarization is rotated by 90 degrees, first by the electro-optic modulator **1401** and then again by the half-wave plate **1403**, resulting in the input beam **1408-I** reflecting from the thin film polarizer **1402-1** and being injected into the WOMPA system **1000**. After the electro-optic modulator **1401** is configured to rotate the input beam polarization of the input beam **1408-I**, the input beam continually reflects off the thin-film polarizers **1402-1** and **1402-2** and is trapped within a cavity that includes the WOMPA system **100** and the highly reflective mirror **1407**. In this regard, the input beam **1408-I** may continually pass into and out of the WOMPA system **1000** until the electro-optic modulator **1401** is turned off, and no longer rotates the polarization of the input beam **1408-I**, allowing the input beam **1408-I** to pass through the thin-film polarizer **1402-2**. Once the electro-optic modulator **1401** is turned off, the input beam **1408-I** may exit the laser system **1400** as the amplified output beam **1408-O** by propagating through the

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thin-film polarizer **1402-2** as opposed reflecting therefrom. Accordingly, amplification of the input beam **1408-I** may be controllably scaled based on the number of passes through the WOMPA system **1000**. That is, control of the electro-optic modulator **1401** may be based on a predetermined number of passes through the WOMPA system **1000** and a desired level of amplification. A photo-detector **1409** may be configured to detect leakage through thin film polarizer **1402-2**. Leakage pulses from each successive round trip are depicted by pulses **1406-1** through **1406-5** in FIG. 9B. For example, laser pulse intensity increases over time as the input beam **1408-I** makes multiple trips through the WOMPA system **1000**. Such is illustrated in the leakage pulses **1406-1** through **1406-5** detected by the photo-detector **1409** in the beam **1408-L**. After the gain begins to saturate and the leakage pulse energies are maximized, the electro-optic modulator **1401** may be turned off to allow the pulse to exit the cavity through the thin film polarizer **1402-2** along the beam path **1408-O**.

FIG. 10A illustrates WOMPA systems **1000-1** and **1000-2** in another exemplary embodiment of an optical configuration **1500**. In this embodiment, the optical configuration **1500** employs another WOMPA system **1000-2** in place of the highly reflective mirror **1407** illustrated in the laser system **1400** of FIG. 9. In this regard, each pass of the input beam **1508-I** through the WOMPA system **1000-1** constitutes twice the amplification of the input beam as the input beam also passes through the WOMPA system **1000-2**. That is, the WOMPA system **1000-2** may also be configured with a gain medium that also provides gain to the input beam **1508-I** prior to emission from the optical configuration **1500**. The invention, however, is not intended to be limited simply to twice the amplification as the optical configuration **1500** may be implemented in other ways. For example, the optical configuration **1500** may be implemented with additional WOMPA systems **1000** that may be used to further scale the amplification of the input beam **1508-I**. Alternatively, one of the WOMPA systems **1000-1** and **1000-2** may not be configured with a gain medium such that the WOMPA system is used to provide focusing and/or timing affects on the input beam **1508-I**. For example, assuming that the WOMPA system **1000-2** is not configured with a gain medium, the WOMPA system **1000-2** may extend the path of the input beam **1508-I** in a relatively compact manner. Additionally, such a WOMPA system **1000-2** may be used to impart certain focusing effects in the input beam **1508-I** via the OAPs and/or the reflective elements of the WOMPA system **1000-2**. Specifically, the time of traversal for the input beam **1508-I** through the WOMPA system **1000-2** allows for a longer time for the electro-optic modulator **1401** to switch from a passive state to a fully activated polarization rotating state, after the first traversal of the input beam **1508-I** through the electro-optic modulator **1401**. This increased switching time allows greater flexibility in the selection of the electro-optic modulator **1401** and the overall system design.

FIG. 10B illustrates the laser pulse intensity increase over time as the input beam **1508-I** makes multiple trips through the optical configuration **1500** (i.e., and the WOMPA systems **1000-1** and **1000-2**). For example, the laser pulse intensity increases in the output beam **1508-O** be a multiple passes of the laser energy **1508** through the WOMPA systems **1000-1** and **1000-2** as illustrated by the laser pulses **1506-1** through **1506-5**.

FIGS. 11A and 11B illustrate an exemplary multiple input and multiple output WOMPA system **1600**. FIG. 11A is illustrative of a side view of the WOMPA system **1600** whereas FIG. 11B is illustrative of an overhead view of the WOMPA system. The WOMPA system **1600** employs optical elements

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that are similar to the WOMPA system **1000**. For example, the WOMPA system **1600** includes the OAPs **1003** and **1004** and the reflective elements **1001** and **1002**, one or more of which may include a gain medium. In this embodiment, the WOMPA system **1600** has two input beams **1611** and **1612** corresponding to two output beams **1614** and **1613**, respectively. Another beam **1615** is illustrated as an input/output beam. Each of the beams **1611**, **1612**, and **1615** enters the WOMPA system **1600** and impinges the gain medium a certain number of times based on the tilt of the reflective elements **1001/1002** (e.g., 12 times in this example). Each beam, however, exits the WOMPA system **1600** along a different path. For example, the input beam **1611** enters the WOMPA system **1600** through the optical element **1601** (e.g., a lens) and exits the WOMPA system **1600** as the beam **1614** through the optical element **1604** (e.g., a lens). However, the input beam **1612** enters the WOMPA system **1600** through the optical element **1602** and exits the WOMPA system through the optical element **1603** with each input path and output path being different from the input path and output path of the beams **1611** and **1614**. Additionally, the beam **1615** enters and exits the WOMPA system **1600** along the same path. In this regard, the WOMPA system **1600** presents the ability to input different types of beams for different purposes. For example, the beams **1611** and **1612** may be used to pump the gain medium at different wavelengths. This may be useful if multiple gain media are chosen, or if antistokes cooling approaches are used. Alternatively, the beam **1611** and **1612** may be used as scaling pump beams to controllably adjust the pump power to the gain medium and/or serve as a backup in case one of the pump sources fails. In yet another alternative, the WOMPA system **1600** may be used to propagate a plurality of signal beams along different paths. Such may be the case for communication purposes. For example, the gain medium of the reflective element **1001** may be edge pumped such that a plurality of communication signal beams **1611**, **1612**, and **1615** are amplified external to other more sensitive optics.

It should be noted that while the WOMPA system **1600** is shown and described with respect to three input beams and three corresponding output beams, the invention is not intended to be so limited. For example, the WOMPA system **1600** may be configured with as many input and output beams as desired limited in general to the spot sizes of those beams. That is, the spot size of each beam occupies a certain amount of real estate on the OAPs **1003** and **1004**. So long as the individual beams do not overlap (at least not substantially), the number of beams may be simply limited to the spot sizes of the beams and the amount of real estate on the OAPs **1003** and **1004**. Examples of such beam spot sizes on the OAPs are shown and described below in greater detail in FIGS. 13 and 14. It should also be noted that the optical elements **1601-1604** are optional elements that may be used to place beam waists between the OAPs or otherwise change the beam spot sizes (e.g., via focusing) and/or impart other optical effects on the beams.

FIG. 12 illustrates another exemplary embodiment of the multiple input and multiple output WOMPA system **1600** as viewed from the side, as illustrated in FIG. 11A. As with the previous embodiment, the input beams **1611** and **1612** enter the WOMPA system **1600** and exit the WOMPA system as the corresponding output beams **1613** and **1614**. Differing from the previous embodiment is the highly reflective mirror **1701** that is used to reflect the output beams **1613** and **1614** back into the WOMPA system **1600** so as to provide two passes of the beams through the gain medium. For example, once the output beams **1613** and **1614** exit the WOMPA system **1600**

and reflect off the highly reflective mirror **1701**, these output beams become input beams to the WOMPA system **1600** and once again impinge the gain medium configured with the reflective element **1001** (and/or **1002**) and exit the WOMPA system **1600** via the paths of the input beams **1611** and **1612**.

FIGS. **13** and **14** illustrate beam spot sizes on the OAPs **1003** and **1004** in greater detail. Since the OAPs **1003** and **1004** are similar, the discussion will focus on the OAP **1003** for the sake of clarity. In this embodiment, the face **1003-F** of the OAP **1003** of FIGS. **11A** and **11B** is shown with a plurality of beams spots representing the reflections of the beams **1611-1615**. For example, the beam spot **1611-1** represents the first point on the OAP **1003** that the beam **1611** impinges (i.e., reflects off) before propagating to the optical element **1002**. After propagating from the reflective element **1002**, the beam **1611** impinges the face **1003-F** of the OAP **1003** at the beam spot **1614-1** and proceeds to the OAP **1004**. The beam **1614** proceeds to the optical element **1001** to reflect off the face **1004-F** of the OAP **1004** to the face **1003-F** of the OAP **1003** at the beam spot **1611-2**. These reflections continue until the beam **1614** exits the WOMPA system **1600** by reflecting off the face **1003-F** of the OAP **1003** at the beams spot **1614-N** (where N is merely intended to represent an integer greater than one and not necessarily equal to any other N designations described herein). The beam **1612** similarly impinges the face **1003-F** of the OAP **1003** at the beam spot **1612-1** and exits the WOMPA system **1600** from the beam spot **1614-N**. The beam **1615**, due to the point at which the beam **1615** first impinges the face **1003-F** of the OAP **1003**, enters the WOMPA system **1600** at the beam spot **1615-1** and exits at the same location (**1615-N**) after traversing through the WOMPA system **1600** (i.e., via the OAPs **1003/1004** and the reflective elements **1001/1002**). For example, the beam impinges the OAP **1003** at point **1615-1** and traverses to the point **1615-X** (where X is an integer like N merely representing a number greater than one) before traversing back through the WOMPA system **1600** to the point **1615-N** (i.e., **1615-1**) of the OAP **1003** and exiting the system.

Although illustrated with a particular number of beams spots and input/output beams, the invention is not intended to be so limited. For example, input beams **1801** and **1802** may be additional input beams having corresponding output beams **1811** and **1812**. Generally, the number of beams spots, and thus the number of input beams, available to the face **1003-F** of the OAP **1003** depends on the amount of available real estate on the face of the OAP **1003-F** and/or the beam spot size of each impinging beam. As mentioned above, certain optical elements may be configured with the WOMPA system **1600** to change the beam spot sizes. Smaller beam spot sizes mean that more beams can impinge the OAP **1003**. FIG. **14** illustrates such beam spot adjustment via smaller beam spot sizes resulting in more beams spots in the same amount of available real estate than illustrated in FIG. **13**. Physical reductions to practice have shown that a 3 inch square face **1003-F** with a 5 mm spot size can result in 198 passes of optical energy through a gain medium affixed to one of the optical elements **1001/1002**. A 3 mm spot size can result in 330 passes through the gain medium. Note that, while FIG. **13** illustrates the beam spots arranged in a perfect rectilinear grid, the actual spot sizes may be formed on a curvilinear grid due to geometrically based distortions from the OAP or parabolic reflective surfaces. Thus, the invention is not intended to be limited to any particular pattern of beam spots on the OAP.

FIG. **15** illustrates the WOMPA system **1600**, from the side, in another exemplary optical configuration **2000**. In this embodiment, linearly polarized laser energy **2002** enters the optical configuration **2000** through a polarization beam splitter

(or a thin-film polarizer) **2001** to filter off any undesired polarizations. The laser energy **2002** is then rotated in polarization by 45° via a polarization rotator **2003** where it enters the WOMPA system **1600** as the 45° rotated laser energy **2004**. Afterwards, the laser energy **2004** exits the WOMPA system **1600** at another elevation (e.g., into the page of FIG. **15**) and reflects off a mirror (not shown) back into the WOMPA system **1600**. From there, the laser energy **2004** exits the WOMPA system **1600** where it is rotated in phase again by 45° via the rotator **2003**. In this regard, the laser energy **2004** is now horizontally polarized with respect to the laser energy **2002** such that it reflects off the polarization beam splitter **2001** and into the polarization beam splitter (or highly reflective mirror) **2006**. The horizontally polarized laser energy **2010** then propagates through an optional polarization rotator **2005** which rotates the polarization of the laser energy by 90° such that it is again linearly polarized laser energy (**2007**) in the vertical direction. The linearly polarized laser energy **2007** propagates through the WOMPA system **1600** and again exits at another elevation (e.g., into the page of FIG. **15**) and reflects off a mirror (not shown) back into the WOMPA system **1600**. Thereafter, the laser energy exits the WOMPA system **1600** to pass through the optional polarization rotator **2005** where it again becomes the horizontally polarized laser energy **2010**. The horizontally polarized laser energy **2010** reflects off the polarization beam splitters **2006** and **2001** back into the WOMPA system **1600** through the rotator **2003**. The rotator **2003** rotates the polarization of the optical energy **2010** by 45° before and after propagating through the WOMPA system **1600** such that it may exit the optical configuration **2000** as vertically polarized laser energy **2002**. In this regard, the laser energy **2002** is filtered to a single polarization and makes six passes through the WOMPA system **1600**. Depending on the configuration the WOMPA system **1600**, the gain of the laser energy **2002** can be increased dramatically. For example, assuming that the WOMPA system **1600** includes a thin disk gain medium disposed upon one of the reflective elements **1001/1002**, the optical configuration **2000** provides that the laser energy **2002** receives six times as many passes through the gain medium of the WOMPA system **1600**. Depending on the number of beams spots with the OAPs **1003/1004**, the optical configuration **2000** may dramatically increase the total number of passes of the optical energy **2002** through the gain medium. Alternatively, the optical configuration **2000** may be configured with the WOMPA system **1600** of FIG. **14**. For example, the path **2021** may be likened to the path **1611** while the path **2022** may be likened to the path **1612**.

FIG. **16** illustrates the WOMPA system **1600** in another exemplary optical configuration **2100**. In this embodiment, linearly polarized laser energy **2002** again enters the optical configuration **2000** through a polarization beam splitter (or a thin-film polarizer) **2001** to filter off any undesired polarizations. In this configuration, however, the laser energy **2002** propagates through a quarter wave plate ($\lambda/4$) **1404** such that it is circularly polarized before entering the WOMPA system **1600**. With the use of the half wave plate ($\lambda/2$) **2101**, the laser energy **2002** can revert back to linear polarization and exit the optical configuration **2100** with six passes through the WOMPA system **1600** in a manner similar to that shown and described in the optical configuration **2000** of FIG. **15**.

FIG. **17** illustrates the WOMPA system **1600** in another exemplary optical configuration. In this embodiment, the polarization beam splitters **2001** and **2006** are combined with the optical elements **2003** and **2005** of FIG. **17** (or the optical elements **1404** and **2101** of FIG. **16**) to provide a gain scaling module **2205**. The gain scaling module **2205** optically com-

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municates with the WOMPA system 1600 such that the laser energy 2203 makes six passes through the WOMPA system 1600 before exiting the system in the same manner as illustrated in FIGS. 15 and 16. The advantage of the gain scaling module 2205 comes from the ability to combine with other gain scaling modules 2205 to further scale the gain of the laser energy 2203 in a compact manner. An example of such is shown in the optical configuration 2300 of FIG. 18. The optical configuration 2300 includes a plurality of gain scaling modules 2205-1 . . . N that may be configured proximate to one another so as to increase the number of passes through the WOMPA system 1600 by two with each additional gain scaling module 2205. For example, the laser energy 2203 entering the gain scaling module 2205-1 along the path 2301 passes through the gain scaling module into the WOMPA system 1600. The laser energy 2203 then exits the WOMPA system 1600 at another elevation (e.g., into the page of FIG. 17), reflects off a mirror (not shown) back into the WOMPA system 1600, and returns by passing through the gain scaling module 2205-2 along the path 2305. The laser energy 2203 exits the WOMPA system 1600 at another elevation (again into the page of FIG. 17) to reflect off a mirror (not shown) into the WOMPA system 1600. The laser energy 2203 then propagates to the WOMPA system 1600 in a similar manner through the gain scaling module 2205-3 along the path 2310. The laser energy 2203 then traverses from the gain scaling module 2205-3 back to the gain scaling module 2205-1 for a total of fourteen passes through the WOMPA system 1600. However, the invention is not intended to be so limited as the number of gain scaling modules 2205 may be increased or decreased as a matter of design choice.

FIGS. 19 and 20 illustrate another embodiment for scaling the gain of laser energy via the optical configuration 2400. In this embodiment, the laser energy 2401 passes through the quartz 90° rotator 2005 (or half wave plate 2101) where the polarization of the laser energy is rotated by 90° such that it passes through the polarization beam splitter 2001. Thereafter, the laser energy polarization is modified via the 45° polarization rotator 2003 (or quarter wave plate 1404) before it enters the WOMPA system 1600 along the path 2402. The laser energy 2401 exits the WOMPA system 1600 at another elevation (e.g., into the page of FIG. 19), reflects off a mirror (not shown) back into the WOMPA system 1600. Thereafter, the laser energy 2401 exits the WOMPA system 1600 along the path 2402 again passing through the 45° polarization rotator 2003 (or quarter wave plate 1404) such that it reflects off the polarization beam splitter 2001 to the highly reflective mirror 2403. The mirror 2403 reflects the laser energy along the path 2404 into the WOMPA system 1600 and then exits along the same path 2404 (i.e., after another trip through the WOMPA system 1600 at another elevation) to the mirror 2403 for reflection off the polarization beam splitter 2001. The laser energy then undergoes another pass through the WOMPA system 1600 as well as two more polarization modifications via the 45° rotator 2003 (or quarter wave plate 1404). The two additional polarization modifications rotate the polarization of the laser energy 2401 to its original polarization (i.e., when laser energy 2401 initially entered the optical configuration 2400) such that it passes through the polarization beam splitter 2001 and exits the optical configuration along its entering path. With this particular optical configuration 2400, the laser energy 2401 makes a total of six passes through the WOMPA system 1600. Note that if the laser energy 2404 is at the same elevation as the optical axis of the OAPs of the WOMPA system 1600, then the total number of passes would be five.

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The optical configuration 2400 can be extended to increase the number of trips of the laser energy 2401 through the WOMPA system 1600. For example, in FIG. 20, the laser energy 2401 enters the optical scaling configuration 2500 and passes through the optical configuration 2400-1 along the path 2410 to the WOMPA system 1000 for two trips there-through. The laser energy 2401 returns along the path 2410 to the optical configuration 2400-1 where it is reflected to the optical configuration 2400-2 to pass through the WOMPA system 1600 via the path 2420 (i.e., for two trips). The laser energy 2401 returns along the path 2420 to the optical configuration 2400-2 where it is further reflected downstream along the paths 2430, 2440, 2450, and 2460 until it reaches the optical configuration 2400-N. The laser energy 2401 then propagates to the optical configuration 2400-N as described above returning from the WOMPA system 1600 via the path 2470 to pass through the WOMPA system 1600 via the path 2460 again, thus propagating upstream along the paths 2460, 2450, 2440, 2430, 2420, 2410 until the laser energy 2401 exits via the optical configuration 2400-1. The laser energy 2401, in this regard, makes a total of $4N+1$ passes through the WOMPA system 1600 when configured with N optical configurations 2400.

FIG. 21 illustrates another multi-pass optical configuration 2600 employing the WOMPA system 1600. In this embodiment, the optical configuration 2600 is configured with the gain scaling module 2205 to pass the laser energy 2601 multiple times through the WOMPA system 1600. Initially, the laser energy 2601 passes through the gain scaling module 2205 where the phase is rotated after passing through the 45° polarization rotator along the path 2610. The phase rotated laser energy enters the WOMPA system 1600 along the path 2610 and exits the WOMPA system 1600 along the path 2630 where it is reflected by the reflective element 2605.

The reflective element 2605 reflects the laser energy 2601 to the WOMPA system 1600 along the path 2630 where it exits the WOMPA system 1600 along the path 2610. From there, the laser energy 2601 propagates to the gain scaling module 2205 after being rotated in phase by another 45° via the 45° polarization rotator 2003. This rotation causes the laser energy 2601 to reflect along the path 2640 within the gain scaling module 2205. For example, the gain scaling module 2205 may include polarization beam splitters that reflect light at one polarization while passing light at another polarization. In this regard, the gain scaling model 2205 propagates the laser energy 2601 along the path 2620 to the WOMPA system 1600 where it enters the WOMPA system 1600 and exits along the same path 2620. Before entering the WOMPA system 1600, the laser energy 2601 is rotated in phase by 90° via the 90° polarization rotator 2005. The laser energy 2601 is then rotated again by 90° on the return trip along the path 2620 via the 90° polarization rotator 2005. The laser energy 2601 reflects and propagates through the gain scaling module 2205 along the path 2640 where it exits the gain scaling module 2205 along the path 2610 after being rotated by the 45° polarization rotator 2003. The laser energy 2601 then again enters the WOMPA system 1600 along the path 2610, exits along the path 2630, reflects off the reflective element 2605 to enter the WOMPA system 1600, and exit the WOMPA system 1600 along the path 2610. The laser energy 2601 undergoes another 45° phase rotation as it passes through the 45° polarization rotator 2003. This final 45° rotation of the laser energy 2601 causes the laser energy 2601 to pass through the gain scaling module 2205 to exit the optical configuration 2600 after making a total of five passes through the WOMPA system 1600. Thus, the optical configuration 2600 provides a means for multiplying the number of passes

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through a gain medium of the WOMPA system **1600**. For example, assuming that the WOMPA system **1600** provides 30 passes through the thin disk gain medium **1001**, then the optical configuration **2600** provides a means for multiplying that number of passes by a factor of five for a total number of 150 passes through the gain medium **1001**.

It should be noted that the reflective element **2605** may be configured in other ways as a matter of design choice. For example, the reflective element **2605** may be a highly reflective mirror that reflects substantially all of the laser energy impinging the reflective element **2605**. Alternatively, the reflective element **2605** may be configured to pass a certain portion of the optical energy while reflecting the remaining optical energy to the WOMPA system **1600**. Such an embodiment may have advantages in that the optical configuration **2600** may be configured with a controller that is used to control the gain of the optical configuration **2600**. For example, the reflective element **2605** may include a detector that receives the laser energy passing through the reflective element **2605** to determine the gain being imparted on the laser energy **2601** by the WOMPA system **1600**. This information may be passed to the controller such that adjustments may be made to certain reflective elements within the WOMPA system **1600** to adjust the gain of the optical configuration **2600** (e.g., via the tilting of mirrors within the WOMPA system **1600** that change the number of locations where the laser energy **2600** may impinge the OAPs of the WOMPA system). Alternatively or additionally, the reflective element **2605** may be configured with a saturable absorber, such as a SESAM. Such a mirror may be used for the generation of ultrashort pulses by passive mode locking when the optical configuration **2600** exists within a cavity. Additionally, the SESAM may be used to prevent ASE. For example, a SESAM may be used as reflective element **2605** absorb light at certain low intensities while reflecting higher intensity light regardless of the wavelength so as to “filter off” undesirable fluorescence, such as ASE. Each of the SESAMs and saturable absorbers described in the embodiments below may be used for such purposes. In this regard, SESAMs and other saturable absorbers may be configured with the WOMPA systems described herein in a variety of ways as a matter of design choice. In some embodiments, a saturable absorber may even be configured with the thin disk gain medium **1001** to prevent ASE within the WOMPA system **1600**.

In another embodiment, depicted in FIGS. 22A-22C, a WOMPA system **2700** significantly increases the number of round trips through the gain medium **1001**. In implementing such, an OAP **2710** is used in addition to the WOMPA system **1000**. This third OAP **2710** and an additional angular multiplexing mirror **2711** provide angular multiplexing in two directions, allowing for many more round trips. FIGS. 22A and 22B are side and top views, respectively, whereas FIG. 22 provides a footprint view of the any of the OAPs **1003**, **1004**. The top view of FIG. 22B is very similar to the WOMPA system **1000** described in FIG. 5, where horizontal multiplexing mirrors **1001/1002** are used to control the angular multiplexing in the horizontal direction. Since the signal beam is injected below the thin disk gain medium **1001**, after numerous disk “bounces” (i.e., reflections of the gain medium **1001**), the beam **2705** is ejected from the OAP **1003/1004** imaging pair at an elevation that is above the elevation of the thin disk gain medium **1001**. After the signal beam **2705** passes the OAP **1003**, it is reflected off the OAP **2710** and an image of the gain medium **1001** is created at the vertical multiplexer mirror **2711**. The vertical multiplexer mirror **2701** directs the signal beam **2705** back to OAP **2710**, which injects the beam **2705** back into the OAP imaging pair **1003/**

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1004 at a new elevation. In this regard, the WOMPA system **2700** uses both vertical and horizontal angular multiplexing to produce a relatively large number of signal beam **2705** passes to efficiently extract energy from the thin disk gain medium **1001**, even with a relatively low energy seed. This multi-pass system **2700** may also compensate thermal effects from multi-pass pumping, disk geometry, and various round trip losses due to the length of the region. FIGS. 22A and 24B illustrate the case where the optical axis of OAP **2710** is above the optical axis of the OAP **1003** and the OAP **1004**. However it should be understood that the optical axis of OAP **2710** may be along any line approximately parallel to the optical axis of OAP **1003** and/or OAP **1004**.

In one physical reduction to practice, the system **2700** is configured with the parameters listed in the table below:

Parameter	Value
Disk Type	Yb: YAG (5%)
Disk Gain Thickness	225 μm
Pump Power	500 W or 1 kW
Pump Losses (initial)	7%
Pump Losses (R.T.)	0.5%
Pump Round Trips	30
Signal Seed Energy	10 nJ
Signal Rep Rate	1 kHz
Signal/Pump Area Fill Factor	64%
Signal Losses	5%/round trip
Water Temperature	13 degrees
Heat Transfer Coefficient	105 W/m ² /K

The WOMPA system **2700** is operable to substantially increase the output pulse energy for a 10 nJ input pulse and 500 W pump based on the pump spot size and the number of disk bounces. For example, if the WOMPA system **2700** is configured to provide eight rows and eight columns of beam spots on the OAPs **1003**, **1004**, and **2710**, 64 round trips may be achieved with a pump spot size of 4 mm, yielding up to 75 mJ per pulse. With a 1 kW pump source, about 150 mJ may be achieved.

Previously, nanoJoule to milliJoule amplification in an ultrashort pulse laser system called for the use of a regenerative amplifier. Traditionally, a regenerative amplifier is electronically controlled to switch pulses into and out of the region via a Pockels cell or an electro-optic modulator. Such switches, however, are fairly expensive and difficult to operate and align. The switches also require high voltage and are significant sources of loss. Moreover, optical switching technology that is fast enough for a regenerative amplifier application typically can only accommodate a signal beam through a small aperture and requires propagation through a refractive material. Consequently, the pulse energy cannot exceed a certain value at which nonlinear propagation effects cause damage. The optical switch is typically the fundamental constraint on the maximum powers that can be achieved with a traditional regenerative amplifier. For example, amplification to tens of millijoules generally requires a linear amplifier downstream from the regenerative amplifier. The concepts demonstrated in the prototype WOMPA system **2700** and others above may be used to replace the regenerative amplifier and linear amplifier with one device having fewer parts, thereby reducing system complexity and cost.

In another embodiment, a new pumping architecture may be based on similar reimaging concepts for the signal beam as presented herein. In this regard, FIGS. 23A-23C depict an exemplary optical configuration **2800** employing such a pump architecture with the WOMPA system **1600** in combi-

nation with the signal beam architecture of the WOMPA system 1000. FIG. 23A is a top view of the optical configuration 2800. As seen in this figure, the WOMPA system 1000 shares a thin disk gain medium 1001 with the WOMPA system 1600. FIG. 23B illustrates a side view of the optical configuration 2800. The optical configuration 2800, as seen in the side view of FIG. 23B with an aperture 2810, allows the signal beam 2802 to pass along multiple paths to the thin disk gain medium 1001. FIG. 23C thus illustrates the view 2811 of the OAPs 1003-1600 and 1003-1000 from the perspective of the thin disk gain medium 1001.

In this embodiment, two separate pump beams 2822 and 2823 are provided to the WOMPA system 1000 entering at two separate elevations. These elevations are illustrated with the view of the OAP 2811 of the OAP 1003-1600 of FIG. 23C. For example, the input pump beam 2823 impinges the OAP 1003-1600 at a location that is different from the input pump beam 2822. Similarly, the signal beam 2802 impinges the OAP 1003-1000 in the center portion of the view 2811 due to the elevation of the signal beam 2810 after passing through the WOMPA system 1000.

The pumping architecture of the optical configuration 2800 may provide several advantages. For example, this architecture may allow a selection of a much larger number of pump passes. With more pump passes, efficient absorption into even thinner disks may be accomplished, which is advantageous because thinner disk gain mediums enable more effective cooling and reduce thermal focusing and birefringence effects as mentioned above. A selection of the number of pump passes may be determined by adjusting the tilt of the pump horizontal multiplexing mirrors 1001 and/or 1002-1600 of the WOMPA system 1600. Another advantage of this architecture resides in scaling. For example, since the pump beams 2822/2823 are combined with the signal beam 2802 on the thin disk gain medium 1001, multiple diode pump systems may be combined and coupled as a single high power fiber for transmission pump laser. As such, lower power pumps may be used with separate fibers to perform beam combining on the thin disk gain medium 1001. Such provides the capability of relatively high power scaling, since the pump power is not limited by the power that could be transmitted by a single fiber. Moreover, should one or more pumps fail, pumping of the thin disk gain medium 1001 may still occur since there is no single point of failure within the WOMPA system 1000. For example, if a system utilizes 10 separate pump fibers to deliver the pump to the WOMPA system 1000, and if one pump goes fails, 90% of the power may still be delivered to the thin disk gain medium 1001. Such may provide a robust packaging solution suitable for military and industrial applications where complete system failure cannot be tolerated.

Combining pump and signal beams on the disk also provides some flexibility in the multi-pass pump design of the WOMPA system 1000. For example, by using multiple pump delivery fibers, any particular fiber diameter can be reduced for the same total pump power. Various optical design constraints related to the pump spot size on the OAPs 1003/1004, focal lengths of the OAPs 1003/1004, and/or numerical apertures of fibers, also make it easier to image surfaces of smaller diameter fibers onto the thin disk gain medium 1001 with an appropriate magnification factor.

FIG. 24 illustrates another optical configuration 2900 that employs the WOMPA system 1600 of FIG. 11. In this embodiment, laser energy 2910-IN enters WOMPA system 1600 through the optical element 1102-1 (e.g., an optional lens) after passing through a polarization beam splitter 2903 in a particular polarization. The laser energy 2910 experi-

ences multiple passes through the thin disk gain medium 1001 depending on the tilt of the reflective elements (e.g., the reflective element configured with the thin disk gain medium 1001 and/or the reflective element 1002). The laser energy then exits the WOMPA system 1600 into the pulse selection module 2901 through the optical element 1102-2 (e.g., an optional lens).

The pulse selection module 2901 includes a plurality of reflective elements 2904 (e.g., 2904-1 . . . 4) that are operable to direct the laser energy 2910 back into the WOMPA system 1600. The pulse selection module 2901 is operable as a switch, providing a certain optical path length based on the number of reflective elements 2904 within the pulse selection module 2901. For example, the pulse selection module 2901 may be used to block ASE except for a short time window, which is matched to allow the amplified pulse to pass. The pulse selection module 2901 is synchronized with respect to the input pulse to open just in time and let the amplified pulse through, closing shortly thereafter. It is important to note that the pulse selection module 2901 has no requirement for the disposition of the pulse energy 2910 when the pulse selection module 2901 is not configured to pass the pulse energy 2910. Unlike optical configurations for traditional regenerative amplifiers, this pulse selection module 2901 is used to suppress unwanted radiation and allow passage of the amplified pulses. The pulse selection module 2901 does not necessarily need to redirect pulse energy.

The pulse selection module 2901 may include an electro-optic modulator 2902 or other polarization rotator to rotate the polarization of the laser pulses in the laser energy 2910 to a particular polarization. One or more of the reflective elements 2904 may be polarization beam splitters that filter off the undesirable polarizations within the laser energy 2910 to allow the laser pulses of the desired polarization to return to the WOMPA system 1600 for further amplification. In this regard, the reflective element 2904-4 may be a polarization beam splitter that allows the laser energy 2910 to pass into the pulse selection module 2901 just as the polarization beam splitter 2903 allows the laser energy 2910 to enter into the WOMPA system 1600.

After entering the pulse selection module 2901, the electro-optic modulator 2902 rotates the polarization of the laser energy 2910. The laser energy 2910 then propagates through the pulse selection module 2901 according to the reflective elements 2904-1 through 2904-3 until it reaches the reflective element 2904-4. From there, the laser energy 2910, due to its changed polarization, reflects off the reflective element 2904-4 to return into the WOMPA system 1600 through the optical element 1102-2. The laser energy then undergoes multiple passes again through the WOMPA system 1600 to exit the WOMPA system 1600 through the optical element 1102-1 (i.e., the laser energy 2910-OUT). For example, due to its change in polarization, the laser energy 2910 reflects off the polarization beam splitter 2903 and exits the optical configuration 2900. Thus, the optical configuration 2900 has provided a 2x factor of gain via the WOMPA system 1600. In one embodiment, one of the reflective elements 2904 may be partially transmissive so as to allow a portion of the laser energy 2910 to pass and be detected by an optical detector such that the gain of the WOMPA system 1600 may be feedback controlled, as described above. It should be noted that the electro-optic modulator 2902 may be a passive nonlinear device, where nonlinear self-rotation of the polarization is used to self-select the transmission of high intensity pulses.

FIG. 25 illustrates another optical configuration 3000 that employs the WOMPA system 1600 of FIG. 11. In this embodiment, the laser energy 2910-IN enters the WOMPA

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system 1600 by first passing through the polarization beam splitter 2903 and the optional optical element 1102. The laser energy 2910 passes through the thin disk gain medium 1001 multiple times before entering the pulse selection module 2901. Again, the electro-optic module 2902 of the pulse selection module 2901 rotates the polarization of the laser energy 2910 such that it may reenter the WOMPA system 1600. Differing from the optical configuration 2900 illustrated in FIG. 24, however, is the positioning of beam polarization splitter 2903 to reflect the laser energy to the reflective element 3001 such that it reenters the WOMPA system 1600 as opposed to exiting the optical configuration 3000. In this regard, the laser energy propagates along a different path through the WOMPA system 1600 such that it again impinges the thin disk gain medium 1001 multiple times and exits the WOMPA system 1600 (i.e., on a different path). The laser energy then impinges an optical element 3002 such that the polarization of the laser energy 2910 is again modified in polarization (e.g., a quarter wave plate or 45 degree polarization rotator, such that the polarization is rotated by 90 degrees after double passing). In this regard, a portion of the laser energy 2910 may pass through the optical element 3002 and reflect off the reflective element 3003 to exit the system 3000 (e.g., for diagnostic purposes and/or feedback control). For example, a thin-film polarizer may be partially transmissive such that a portion of the laser energy passes through while returning the remaining portion of the laser energy in a rotated polarization to the WOMPA system 1600. After reentering the WOMPA system 1600, the laser energy 2910 propagates through the WOMPA system 1600 multiple times, again impinging the thin disk gain medium 1001 multiple times before finally exiting the WOMPA system 1600 to the reflective element 3001. As the polarization of the laser energy 2910 has been rotated by the optical element 3002, the laser energy then reflects off the optical element 3001 through the beam polarization splitter 2903 to exit the optical configuration 3000. Accordingly, the gain has been increased by a factor of 2x over the embodiment illustrated in FIG. 24 with the relatively simple addition and positioning of a few optical elements (i.e., 2903, 3001, and 3002).

Optionally, the laser energy passing through the optical element 3002 may reflect off the reflective element 3003 and impinge a mirror 3010 to direct a signal beam back through the WOMPA system 1600. If 3002 is a quarter wave plate or 45 degree polarization rotator, then the returned polarization will rotate by 90 degrees and exit the WOMPA system 1600 as 2910-OUT. Without the optical element 3002 and a mirror 3010, the signal beam simply exits after reflecting from the reflective element 3003. Thus, the optical configuration 3000 illustrates two means for ejecting the laser energy 2910.

FIGS. 26A and 26B illustrate another optical configuration 3100 that employs the WOMPA system 1600 of FIG. 11. More specifically, FIG. 26A illustrates the WOMPA system 1600 is configured with a background suppression module 3101. The background suppression module 3101 may consist of a saturable absorber mirror (e.g. a SESAM) to suppress background low level radiation. Alternatively, the background suppression module 3101 may consist of multiple components. FIG. 26B provides a more detailed illustration of one embodiment of the background suppression module 3101.

In this embodiment, the laser energy 2910 enters the WOMPA system 1600 by passing through the polarization beam splitter 2903 and the optical element 1102-1 making multiple passes through the gain medium 1001. The laser energy exits the WOMPA system 1600 through the optical element 1102-2 where it passes through a quarter wave plate

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3102 (or polarization rotator, so that the polarization is rotated by 90 degrees after double passing). The quarter wave plate 3102 rotates the polarization of the laser energy 2910 where it enters the background suppression module 3101.

As illustrated in FIG. 26B, the background suppression module 3101 may be configured of a variety of optical elements so as to suppress background radiation, including a transmissive saturable absorber 3106, lenses 3103 and 3104, and a highly reflective mirror 3105. The lenses 3103 and 3104 are operable to provide high intensities in a smaller spot size within the transmissive saturable absorber 3106. The saturable absorber 3106 operates to allow passage of only high intensity light and block (or less efficiently transmit) less intense light. The laser energy 2910-A passes through the saturable absorber 3106 and is recollimated for reflection from highly reflective mirror 3105. After reflection from the highly reflective mirror 3105, the laser energy 2910-B reverses propagation direction for a second pass through the saturable absorber 3106 and is recollimated for exit from the background suppression module 3101. The background suppression module 3101 is operable to absorb background optical energy and ASE and improve the pulse contrast ratio of the amplified output pulses. Once the laser energy 2910-B exits the background suppression module 3101, it return propagates to the WOMPA system 1600 for multiple return passes through the gain medium 1001. In return propagating to the WOMPA system 1600, the laser energy 2910 passes through the thin film polarizer 3102 for another polarization rotation such that the laser energy 2910 may exit the optical configuration 3100. For example, once the laser energy 2910 exits the WOMPA system 1600 from its return propagation, the laser energy 2910 is rotated in polarization such that it reflects off the beam polarization splitter 2903 to exit the optical configuration 3100.

FIGS. 27 and 28 illustrate an alternative WOMPA system 3200 employing multiple OAPs 3202, and a parabolic reflector 3201. More specifically, FIG. 27 illustrates a side view of the WOMPA system 3200 whereas FIG. 28 illustrates an end in view 3215 of the WOMPA system. In this embodiment, the OAPs 3202 approximately comprise half the parabolic surface of the parabolic reflector 3201. With this configuration, laser energy 3210 enters the WOMPA system 3200 via the optical element 3211 (e.g., an optional lens) at an elevation above the OAP 3202 to propagate to the parabolic reflector 3201. The laser energy 3210 then reflects off the parabolic reflector 3201 at the beam spot location 3210-1 to the thin disk gain medium and reflector 3204 affixed to the mount 3212. The laser energy 3210 reflects back to the parabolic reflector 3201 for reflection to the lower OAP 3202. Once the laser energy 3210 impinges the lower OAP 3202, it propagates to the lower reflective element 3205 and back to the lower OAP 3202 for a return trip. That is, the laser energy 3210 reflects off the lower OAP 3202 to the parabolic reflector 3201, then to the gain medium 3204, then to the parabolic reflector 3201, then to the upper OAP 3202, and then to the upper reflective element 3205 for a single round-trip pass through the WOMPA system 3200. Also illustrated in this embodiment is optical element 3211 (e.g., a lens) that is operable to form an intermediate focus within the WOMPA system 3200.

The WOMPA system 3200 is configured to propagate the laser energy 3210 via such round-trip passes through the system multiple times until the laser energy 3210 exits the WOMPA system 3200 via the point at which it entered at the optical element 3211. For example, the laser energy 3210 may reflect off the upper OAP 3202 at the location 3230-1 during a single round-trip pass through the WOMPA system

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3200. The laser energy 3210 may then reflect off the upper OAP 3202 at the location 3230-N on the next round-trip pass through the WOMPA system 3200 (i.e., where N is simply an integer greater than 1 although not necessarily equal to any other N integer designators referenced herein). On the next round-trip pass, the laser energy reflects off the location 3230-2, and then location 3230-(N-1), and so on. The laser energy 3210 makes a number of round-trip passes through the WOMPA system 3200 until the laser energy 3210 reflects off the OAP 3202 at the location 3230-1 during the last round-trip pass through the WOMPA system 3200 until exiting the WOMPA system 3200 via the optical element 3211.

Although FIG. 27 shows the laser energy 3210 entering and exiting the WOMPA system 3200 along the same path, using concepts previously described in this description, it should be recognized that the laser energy entrance and exit beam paths may be displaced in a direction normal to the page of FIG. 29. In this case, separate lenses 3211, displaced in a direction perpendicular to the page of FIG. 27, may be required to focus the input laser energy 3210 and collimate the output laser energy 3210.

To make the laser energy 3210 exit the WOMPA system 3200, the upper OAP 3202 reflects the laser energy 3210 one less time than the lower OAP 3202. In this embodiment, the laser energy 3210 reflects off the upper OAP 3202 at eight locations 3230. Thus, the lower OAP 3202 includes nine locations at which to reflect the laser energy 3210. In this regard, the laser energy 3210 makes a total of 17 passes through the gain medium 3204 before exiting the WOMPA system 3200.

The number of complete passes of the laser energy 3210 through the gain medium 3204, however, is determined by the tilt of the reflective elements 3205, with consideration being given to the beam spot size of the laser energy 3210 on the OAPs. For example, tilting one or more of the reflective elements 3205 may change the number of times that the laser energy 3210 impinges the OAPs 3202 and 3203, accordingly changing the number of times the laser energy 3210 passes through the gain medium 3204. However, the tilt of the reflective elements 3205 may be such that the beam spots at the locations 3230-1 . . . 3230-N do not overlap as a consequence of aligning the system so that 3230-1 lies entirely on OAP 3202. More specifically the tilt should be sufficient to ensure that the laser energy 3210 impinging on the OAP 3202 at the location 3230-1 does not fall off the edge of the OAP 3202.

The number of passes that the laser energy 3210 makes through the gain medium 3204 may be further increased through the rotational propagation of the laser energy through WOMPA system 3200. Such is illustrated in FIG. 28. FIG. 28 illustrates an end view of the WOMPA system 3200. The laser energy 3210 enters the WOMPA system 3200 and impinges the parabolic reflector 3201 at the beam spot 3230-1. The laser energy 3210 then makes several passes through the WOMPA system 3200 via the OAPs 3202-1 (i.e., the first labeled pair of upper and lower OAPs 3202), the reflective elements 3205-1 (i.e., the first labeled pair of upper and lower reflective elements 3205), and the thin disk gain medium/reflective element 3204. That is, the laser energy 3210 enters the WOMPA system 3200 at the beam spot 3230-1 on the parabolic reflector 3201 and makes the plurality of passes through the WOMPA system 3200 based on the tilt of the reflective elements 3205-1 before exiting the WOMPA system 3200 from the OAP 3201 at the beam spot 3230-1.

This exiting laser energy 3210 may be redirected to the WOMPA system 3200 to enter at the beam spot 3230-2 on the parabolic reflector 3201 to again make multiple passes through the WOMPA system 3200. This recirculation of the

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laser energy 3210 through the WOMPA system 3200 may substantially increase the gain of the laser energy 3210. For example, assume that the pair of OAPs 3202-1 is capable of reflecting at a total of 17 non-overlapping locations, as illustrated in FIG. 27. By positioning OAP pairs about a circle, a number of multiple passes through the gain medium 3204 may be increased based on the number of OAP pairs about the circle. In this embodiment, eight pairs of OAPs 3202 about the circular WOMPA system 3200. Accordingly, the WOMPA system 3200 may be configured to propagate the laser energy 3210 through the gain medium 3204 a total of 136 times in this embodiment. However, the invention is not intended to be so limited as the pairs of OAPs 3202 may be operable to reflect at more beam spot locations depending on the size of the beam spot. In some embodiments, a single pair of OAPs 3202 may be operable to propagate the laser energy 3210 through the gain medium 3204 by as much as 205 times or more.

To redirect the laser energy 3210 into the WOMPA system 3200 after the laser energy 3210 exits via the OAP location 3210-1, the WOMPA system 3200 may be configured with additional optical elements. For example, the laser energy 3210 may first pass through a beam thin film polarizer (not shown) and then a polarization modifying element (e.g. a polarization rotator or a quarter waveplate, so that after a return pass the polarization is rotated by 90 degrees). Upon exiting the WOMPA system 3200 at the location 3230-1, the laser energy 3210 may again pass through the polarization modifying element, so that the polarization is rotated by 90 degrees relative to the input polarization and then is reflected from the thin film polarizer to another reflective element (not shown) that directs the laser energy 3210 into the WOMPA system 3200 at the location 3230-2 for interaction with the pair of OAPs 3202-2. This process may continue through the pair of OAPs 3205-N until the laser energy exits the WOMPA system 3200 from the beam spot 3230-N of the parabolic reflector 3201. Alternatively, if an odd number of round trips is used within each pair of the OAPs 3202 and a quarter-wave plate is utilized with one of the pair of reflectors 3205 as illustrated by quarter-wave plate 1010 in FIG. 5, the input and output polarization will be rotated by 90 degrees and can be separated by a thin film polarizer.

The number of pairs of OAPs 3202 is not intended to be limited to the illustrated example. For example, eight pairs of OAPs 3202 are illustrated in FIG. 28. However, the number of OAP pairs 3202 within the WOMPA system 3200 may only be limited by beam spot sizes and corresponding widths of the OAPs 3202. Moreover, the pairs of OAPs 3202 may be cut from a single parabolic reflector similar to that of the parabolic reflector 3201. Additionally, the invention is not intended to be limited to simply a single beam of laser energy 3210 (e.g., a signal beam) entering the WOMPA system 3200. As with other embodiments above, the WOMPA system 3200 may be configured to receive one or more pump beams through the input/output beam spot locations 3210-1-N through a corresponding number of pairs of OAPs 3202. For example, the pairs of OAPs 3202-1 and 3202-2 may be used to pump the gain medium 3204 while one or more of the remaining pairs of OAPs 3202 may be used to induce gain in the signal beam. In yet another embodiment, certain pairs of the OAPs 3202 may be used to pump the gain medium at different wavelengths to provide certain optical effects when a signal beam extracts gain from the gain medium 3204. Accordingly, the inputs of laser energy 3210 to various pairs of OAPs 3202 within the WOMPA system 3200 are not intended to be limited to any particular type of laser energy, as such may be a matter of design choice.

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This embodiment may have certain other advantages in that the multi-pass WOMPA system 3200 may be configured in a relatively compact fashion even though the effective length of the optical region has been increased. Additionally, the mount 3212 for the thin disk gain medium 3204 may be configured along the length of the WOMPA system 3200 as shown so as to provide additional physical space for cooling mechanisms that may be used to cool the thin disk gain medium 3204. For example, the mount 3212 may be configured with a liquid cooling mechanism.

Although shown and described with respect to the thin disk gain medium 3204 being configured with the mount 3212, the invention is not intended to be so limited. For example, thin disk gain mediums may be additionally or alternatively configured with a reflective element 3205. Such may have the effect of providing multiple gain mediums within a single laser system so as to further stimulate gain in the laser energy 3210.

Although FIG. 28 shows the laser energy 3210 entering and exiting the WOMPA system 3200 along the locations 3230-1 through 3230-N, using concepts previously described in this description, it should be recognized that the laser energy entrance and exit beam paths may be displaced for each of the of the locations 3230, so that the input pulse energy 3210 and output pulse energy for each OAP pair, need not overlap. Additionally, it should be noted that the beam paths for each pair of OAPs 3202 may be used for separate laser energies 2010. For example, a pair of OAPs 3202 may be used for the pump beam, one or more beam paths for distinct signal beams, and/or one or more beam paths for distinct beams for gain clearing.

Alternatively, in FIG. 29, the WOMPA system 3200 is configured with apertures 3410 in the lower of the OAP pairs 3202 that are used to provide an output along a separate path from the input for laser energy 3210. The apertures 3410 are operable to output the laser energy 3210 from the WOMPA system 3200 after a certain number of passes through the gain medium 3204 as described above in FIG. 27. The dashed line from the aperture 3410 to the lower reflective element 3205 is approximately perpendicular to the lower reflective element 3205. Thus, after exiting through the aperture 3410-1 of the lower OAP 3202-1, the laser energy is redirected by the optical redirector 3216 into the WOMPA system 3200 through the input beam spot location 3230-2 as illustrated in FIG. 30. The optical redirector 3216 may simply comprise one or more mirrors. The lower OAP 3202 of the pair of OAPs 3202-2 may be similarly configured with an aperture 3410-2 that allows the laser energy 3210 to exit the WOMPA system 3200 for redirection into the WOMPA system 3200 and a return multi-pass trip. This process of redirection of laser energy 3210 into the WOMPA system 3200 may continue until the laser energy 3210 passes through each of the pairs of OAPs 3202, ultimately exiting from the output aperture 3230 of the WOMPA system 3200.

FIG. 31 illustrates a WOMPA system 3500 employing redirection of laser energy 3501 into the WOMPA system. The WOMPA system 3500 may be representative of any of the WOMPA systems described herein in which laser energy is redirected into the WOMPA system. This embodiment of the WOMPA system 3500 illustrates various focal considerations that may be used when redirecting the laser energy 3501 into the WOMPA system. In this regard, slight geometric corrections may be provided when redirecting the laser energy within the WOMPA system 3500 without the use of polarization based or birefringent optics.

In this embodiment, the lenses 3502-1 through 3502-4 have focal lengths of approximately f_L . An input beam of the

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laser energy 3501-I enters the WOMPA system 3500 via the lens 3502-1. The laser energy 3501 exits a first loop of the WOMPA system 3500 and is collimated by the lens 3502-4. The mirrors 3503-1 and 3503-2 redirect the laser energy 3501 into the WOMPA system 3500 through lens 3502-2. The optical path length between the lens 3502-2 and the lens 3502-4 is approximately $2 \cdot f_L$. Thus, the image of the thin disk gain medium (not shown) inside the WOMPA system 3500 from the last bounce in the first loop is imaged at the location 3510, resulting in that image being imaged on the gain medium at the first bounce of the second loop through the WOMPA system 3500. In other words, laser energy 3501 from the lens 3502-1 to the lens 3502-4 is imaged on the position 3510 which is also matched with the image from the lens 3502-2 to the lens 3502-3. Accordingly, consistent conjugate image planes are maintained throughout multiple passes through the WOMPA system 3500. The laser energy 3501 ultimately exits the WOMPA system 3500 as the output beam 3501-O.

The WOMPA system 3500 provides the inherent ability to account for phase distortion in the laser energy 3501. For example, phase corrections and/or phase measurements can be made with relative ease at any of the conjugate image planes of the gain medium before, after, or within any of the WOMPA loops. The beam intensity profile on the gain medium of the WOMPA system 3500 is also more uniform on the subsequent loops through the WOMPA system. Although shown and described with respect to redirection of the laser energy 3501 into the WOMPA system 3500, the invention is not intended to be so limited. For example, the focal considerations described herein may also be employed for redirection of the laser energy 3501 into another WOMPA system. Accordingly, this embodiment merely intends to show that upstream conjugate image planes may be the same as downstream conjugate image planes based on the focal lengths of the WOMPA system 3500.

FIG. 32 illustrates another optical configuration 3600 that employs the WOMPA system 1000 as a gain element within an oscillator cavity. In this case, the laser energy 3610 is initiated from fluorescence within the cavity. After previous round trip passes, the laser energy 3610 enters the WOMPA system 1000 by first passing through optical element 3611, which may be a lens to cause an intermediate focus to be formed in the beam between the two OAPs. On the return trip through the WOMPA system 1000, the laser energy 3610 reflects off the polarization beam splitter (e.g., thin film polarizer) 3601 to the reflective element 3602 (e.g., a highly reflective mirror). After reflecting off the reflective element 3602, the laser energy 3610 passes through a polarization adjusting element (e.g. a wave plate or polarization rotator) 3603, which creates a relatively small polarization component in the plane of the paper. Thereafter, the laser energy 3610 propagates to the focusing element 3605 and to a saturable absorbing mirror (SAM) 3604 (e.g., SESAM, or other device for saturable attenuation and reflection, as similarly illustrated in FIG. 26B) which is operable to configure the optical configuration 3600 as a mode locked system useful in generating ultra short laser pulses. The SAM 3604 may also be used to filter certain undesirable portions of the laser energy 3610 as described above. Optionally, the wave plate or polarization rotator 3603 may also include an electro-optic modulator to allow for cavity dumping operation the oscillator cavity.

Low intensity radiation within laser energy 3610 is attenuated by SAM 3604, whereas high intensity mode locked pulses within laser energy 3610 allowed to circulate with the cavity without attenuation. The laser energy 3610 is reflected back from SAM 3604 to focusing element 3605 and through

polarization adjusting element **3603**, further increasing a polarization component in the plane of the drawing. After reflection from mirror **3602**, laser energy impinges on the thin film polarizer **3601**. The component of the laser energy **3610** (i.e., in the plane of the paper) is transmitted through the thin film polarizer **3601**, whereas the remaining laser energy **3610** is reflected from thin film polarizer **3601** and cycled through a further loop of the WOMPA system **1000**. The laser energy **3610** that cycles through the WOMPA system **1000** consists of mode locked cavity modes. Thin film polarizer **3601** is an output coupling for the laser cavity and transmits a pulse on every round trip of the laser energy **3610**. By adjusting the polarization adjustment element **3603**, the proportion of energy that is transmitted through the thin film polarizer **3601** on each round trip may be controlled. It is important to recognize that focusing element **3605** may be replaced by any number of combinations of transmitting or reflective optics to form an optical laser cavity. It should also be noted that the SAM **3604** may be replaced with other optical elements capable of attenuating low intensity radiation while passing high intensity radiation (e.g. saturable absorbers, nonlinear media and apertures). Additionally, dispersive optical components (e.g. prisms, chirped mirrors, gratings, dispersive transmissive materials) may be added to optimize the round trip dispersion for mode-locking.

The embodiment shown in FIG. **32** has several important features. For example, by adjusting the tilt on the reflective element **1002**, the number of passes through the thin disk gain medium **1001** may be adjusted, thereby modifying the round trip gain within the oscillator and consequently modifying the output pulse energy. Since a modification of the number of round trips in the WOMPA system **1000** changes that total roundtrip time within the oscillator **3600**, adjustments in tilt on the reflective element **1002** also can be used to adjust the repetition rate of oscillator output. It should also be noted that reflective element **1002** may be implemented as a dispersion management mirror or device (e.g., a Gires-Tournois Interferometer or "GTI" Mirror).

It should be noted, however, that the optical configuration **3600** may be configured to receive optical energy along the beam path **3610** from some external source to operate in the same or similar manner described herein. Accordingly, the invention is not intended to be limited to this exemplary embodiment.

FIG. **33** illustrates another optical configuration **3700** that employs the WOMPA system **1000** as a gain element within an oscillator. This embodiment is very similar to configuration **3600**, except that focusing element **3611** is replaced with a focusing mirror **3605-2**. Because this embodiment does not have a refractive lens dispersion within the oscillator, it can be more easily managed in terms of mode-locking.

The WOMPA system **1000**, in this embodiment, is configured slightly different than previous embodiments. Accordingly, the invention is not intended to be limited to any particular embodiment. The reflector **3702** of the WOMPA system **1000** is configured with a saturable absorber **3701** (alternatively the saturable absorber **3701** and the reflector **3702** may be replaced with a SESAM). The reflective element **3702** is configured to pass a certain portion of the laser energy **3610** such that it may be detected by the detector **3703**, which is placed behind the reflective element **3702**, for diagnostic purposes. For example, with each single trip of the laser energy **3610** through the reflector **3702**, the detector **3703** may be operable to determine the amount of gain being imparted on the laser energy **3610** by the WOMPA system **1000**. If a change to that gain is desired, the reflective element **3702** may be tilted so as to change the number of locations

that the laser energy **3610** impinges the OAPs **1003/1004**, accordingly changing the number of times that the laser energy **3610** passes through the gain medium attached to the reflector **1002**. Thus, the gain of the laser energy **3610** may be dynamically controlled.

The detector **3703** may be configured in a variety ways as a matter of design choice. For example, the detector **3703** may be an optical detector that digitally captures optical energy passing through the reflective element **3702**. The detector **3703** may, in turn, generate an electronic signal representative of the detected optical energy such that a controller, processor, or the like may process the electronic signal to determine the gain of the optical energy. This processor may also be coupled to the reflective element **1002** to tilt the reflective element **1002** and correspondingly change that gain imparted on the laser energy **3610**. For example, the reflective element **1002** may be configured with an electromechanical device that is operable to tilt the reflective element **1002** when actuated by a control signal from the processor. Alternatively, the detector **3703** may be configured as a camera (possibly including additional focusing optics) or a detector array so as to independently detect the angularly separated energy and beam size of each pass on the reflective element **3702**. If the detector **3703** is configured as a camera, so as to detect the spot size of each pass of the laser energy **3610** on reflective element **3702**, this information may be used to adjust the distance between the OAPs **1003** and **1004** to better compensate for any focus variations in the reflective element **1002** or the gain element affixed thereto.

FIGS. **34A** and **34B** illustrate an optical configuration **3800** employing the WOMPA system **1600** as an amplifying element within an oscillator. FIG. **34A** is illustrative of a side view of the optical configuration **3800** and the WOMPA system **1600** whereas FIG. **34B** is illustrative of a top view of the optical configuration **3800**. In this embodiment, the WOMPA system **1600** is operable to pump the thin disk gain medium **1001** with the laser energy **3820**. As an oscillator, the signal beam **3210** is generated initially from fluorescence in the gain medium. By tracing the beam path for the signal beam, a signal beam may enter the WOMPA system **1600** to extract energy from the thin disk gain medium **1001** deposited by the pump laser energy **3820**. The signal beam may recirculate through the WOMPA system **1600** as recirculating laser energy **3810**. The recirculating laser energy **3810** reflects off the OAPs **1003/1004** and the reflective element **1002** passing through the thin disk gain medium **1001** multiple times before exiting the WOMPA system **1600** at the reflective element **3801-1**. The reflective element **3801-1** reflects the laser energy **3810** to the reflective element **3801-2** to redirect the laser energy **3810** into the WOMPA system **3800** for another set of passes through the thin disk gain medium **1001**. The laser energy **3810** then exits the WOMPA system **3800** and reflects off the focusing mirror **3605** to the end mirror **3608** (which may be configured as a saturable absorber mirror SAM **3604**). If the end mirror **3604** is configured as a SAM it operates to pass only high intensity mode-locked pulses of the laser energy **3810** during amplification, as described above. The end mirror **3604** reflects the laser energy **3810** to the focusing mirror **3605** to enter the WOMPA system **1600** for subsequent sets of passes through the thin disk gain medium **1001**. The laser energy **3810** continually recirculates through the optical cavity defined by the end mirror **3604** and the output coupler **3802**. On reflection of the circulating signal laser energy **3810** from the end mirror **3802**, a portion of laser energy is transmitted as output laser energy **3830**. If the end mirror **3604** is configured as a saturable absorber and the cavity is configured to generate mode locked pulses, the laser

energy will circulate the cavity as a pulse that will transmit an output pulse through the output coupler **3602** on each round trip. The optical configuration **3800** may also be utilized as a high gain CW cavity, where power is continuously re-circulated through the cavity and transmitted from coupler **3602**. Additionally, the optical configuration **3800** may be utilized as a Q-switched laser cavity if the output coupler **3802** further includes means for switching transmission (e.g., an electro-optic modulator).

Although shown and described with respect to the pump laser energy **3820** being directed towards the center elevation of the WOMPA system **1600**, the invention is not intended to be so limited. For example, additional pump lasers may be configured to stimulate the gain medium **1001** as shown and described above. Additionally, the optical configuration **3800** may be configured in other ways so as to redirect the signal beam laser energy **3810** through the thin disk gain medium **1001** more times than illustrated. Accordingly, this embodiment and those embodiments described above may be combined in a variety of ways to yield other configurations that fall within the scope and spirit of the invention.

FIGS. **35A** and **35B** illustrate an axial WOMPA architecture in the WOMPA system **4300**. More specifically, FIG. **35A** represents a side view of the WOMPA system **4300** whereas FIG. **35B** represents a face of a parabolic mirror **4301/4302** used to reflect the optical energy **4305** within the optical configuration of the WOMPA system **4300**. In this configuration, the optical axes of the parabolic mirrors **4301** and **4302** are substantially the same, whereas the WOMPA systems **1000** and **1600** above utilize corresponding parabolic reflective elements in which the optical axes are parallel, but distinct. Differing from the WOMPA systems **1000** and **1600** above, the WOMPA system **4300** employs the reflective elements **4303** and **4304** within the optical configuration defined by the parabolic mirrors **4301** and **4302**. For example, in the WOMPA systems **1000** and **1600** above, the reflective elements **1001** and **1002** are positioned outside the optical configuration defined by the OAPs **1003** and **1004** to provide an off-axis WOMPA embodiment. In this embodiment, however, the optical energy **4305** propagates within the optical region defined by the parabolic mirrors **4301** and **4302**, while maintaining an intermediate focus as described in FIGS. **4A** and **4B**. Similarly, the parabolic mirrors **4301** and **4302** may be adjusted as described above to compensate for thermally induced focusing/defocusing phase deformation.

The optical energy **4305** enters the WOMPA system **4300** by passing over the parabolic mirror **4302** to reflect off the parabolic mirror **4301**. From there, the optical energy propagates to the mirror **4304** to the parabolic mirror **4301** for reflection to the parabolic mirror **4302**. The optical energy **4305** then reflects off the parabolic mirror **4302** to the reflective element **4303** for reflection to the parabolic mirror **4302**. The parabolic mirror **4302** reflects the optical energy **4305** to the parabolic mirror **4301** for one complete pass through the WOMPA system **4300**. Subsequent passes of the optical energy **4305** through the WOMPA system **4300** propagate at different elevations from previous passes through the WOMPA system **4300**. For example, subsequent passes of the optical energy **4305** impinges the parabolic mirror **4301** at different elevations in a manner similar to that of the other WOMPA systems above. FIG. **35B** illustrates such with the sets of beam spots **4305-1**, **4305-2**, . . . **4305-N**.

FIG. **35B** illustrates an end view looking at the WOMPA system **4300** from the parabolic mirror **4302**. In FIG. **35B**, one beam of optical energy **4305** impinges the parabolic mirror **4301** at the uppermost location on the parabolic mirror **4301** within the set of beam spots **4305-1-IN**. The reflective

element **4304** reflects the optical energy **4305** to the lowermost location on the parabolic mirror **4301** within the set of beam spots **4305-1-OUT**. The parabolic mirror **4301**, in turn, reflects the optical energy **4305** to a corresponding beam spot on the parabolic mirror **4302** (i.e., at the same elevation) within the set of beam spots **4305-1-OUT**. The parabolic mirror **4302** reflects the optical energy **4305** to the reflective element **4303** for reflection to the parabolic mirror **4302** at the next to the uppermost elevation within the set of beam spots **4305-1-IN**. The parabolic mirror **4302** then reflects the optical energy **4305** at the same elevation to the parabolic mirror **4301** for the complete round trip pass through the WOMPA system **4300**. On each subsequent round trip, the beam spots are elevated on the **4305-1-OUT** column and the beam spot within the **4305-1-IN** column is lowered. On the last round trip, the beam exits the WOMPA system **4300** along the uppermost beam spot **4305-1-OUT**, clearing the slightly smaller parabolic mirror **4302** as it passes over the top.

As with the previous embodiments, the WOMPA system **4300** may be configured to provide multiple beam paths to a plurality of different beam inputs or even the same beam inputs. For example, FIG. **35B** also shows the beam spot columns **4305-2-IN** through **4305-N-IN** and the corresponding columns **4305-2-OUT** through **4305-N-OUT**. Either or both of the reflective elements **4303** and **4304** may be configured with a thin disk gain medium that is operable to impart gain on a signal beam as it passes through the WOMPA system **4300**. In this regard, the set of input and output beam spots **4305-1** (labeled-IN and -OUT, respectively) may be representative of a signal beam being amplified by the WOMPA system **4300**. The set of input and output beam spots corresponding to **4305-2** through **4305-N** (also labeled-IN and -OUT, respectively) may be representative of pump laser energy inputs to the WOMPA system **4300** that are used to stimulate the thin disk gain medium such that the gain may be extracted by the signal beam as similarly described above. In this embodiment, each beam path has a separate entrance port over the top and on the right side of element parabolic mirror **4302**, and an exit port over the top and on the left side of parabolic mirror **4302**. FIG. **35B** illustrates the parabolas **4302** and **4301** as circular components, though they may also be configured as square or other shaped elements, so as to optimize the input and output port locations for each of the beam paths.

The invention, however, is not intended to be limited to any particular set of input beams as the WOMPA system **4300** may be configured in a variety of ways subject to design choice. For example, the sets of beam spots **4305-1** through **4305-N** may be representative of any combination of signal beam or pump beam. In some embodiments, either above or herein, multiple signal beams may be used. For example, one signal beam may be amplified by the WOMPA systems presented herein while another signal beam of laser pulses may be used as a gain clearing means to assist in lowering the population of the upper energy states in the gain medium. In some embodiments, one set of beam spots may be representative of the redirection of a particular beam on a return trip through the WOMPA system **4300** as described above. Also, the number of beam spots on any particular parabolic mirror are merely intended as being exemplary. As with the above embodiments, the number of beam spots, and thus the number of trips through a thin disk gain medium, may be determined based on the size of the beam of the optical energy **4305**, the amount of available real estate on the face of a parabolic mirror **4301/4302**, and/or the tilt of one or more of the reflective elements **4303** and **4304**. In this regard, the letter N designating a set of beam spots is again merely intended as an

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integer greater than or equal to 1 and not necessarily equal to any other particular N reference designation described herein.

FIGS. 36A and 36B illustrate another axial WOMPA architecture in the WOMPA system 4400. More specifically, FIG. 36A illustrates a side view of the WOMPA system 4400 whereas FIG. 36B illustrates an end view of the WOMPA system 4400 showing rotational redirection of the laser energy 4410. In this embodiment, the WOMPA system 4400 includes the pair of parabolic reflectors 4401 and 4402, an active mirror 4406 (e.g., a highly reflective mirror configured with a thin disk gain medium), a redirection module 4405, a controller 4409, and a deformable mirror 4404. The deformable mirror 4404 is a reflective element that is operable to change its physical aspects when actuated by the controller 4409. For example, the deformable mirror 4400 may include one or more actuators such as piezoelectric devices or bimorph electrode regions for electronically controlling the curvature of the deformable mirror 4400. When changes in the physical shape of the deformable mirror, in the direction of the propagation the laser energy 4410, and/or in the focusing aspects of the laser energy 4410 are desired, the controller 4409 transfers the appropriate shape changing control signal to the actuator to change the shape of the deformable mirror 4404. The controller may also be used to change the spacing between parabolic reflectors 4401.

In terms of laser energy propagation, the WOMPA system 4400 operates in a similar axial manner as illustrated in the WOMPA system 4300 of FIG. 35. Different, however, is the manner in which the laser energy 4410 is redirected within the WOMPA system 4400, as illustrated in FIG. 36B. In FIG. 36B, the laser energy 4410 enters the WOMPA system 4400 through an aperture or clearance in the parabolic reflector 4401 and is incident on redirector module 4405 where it is reflected from the location 4410-1 to the location 4410-2 and directed to parabolic mirror 4402 at the beam spot in line with 4410-1, which reflects the laser energy to the deformable mirror 4404. This in turn reflects the laser energy 4410 to the lower portion of the parabolic mirror 4402, in line with location 4410-4. From there, the laser energy 4410 is incident at the location 4410-4 on the redirection module 4405, where it is reflected to the location 4410-5 on the redirection module prior to being directed to the parabolic mirror 4401. After being reflected from the parabolic mirror 4401, the laser energy 4410 is incident on the active mirror 4406 and is then reflected back to the parabolic mirror 4401 in line with the location 4410-6. The parabolic mirror reflects the laser energy 4410 to the redirection module 4405 at location 4410-6. The redirection module 4405, reflects the laser energy 4410 to location 4410-7 on the redirection module 4405, prior to directing the laser energy 4410 to the deformable mirror 4401. In this embodiment, the reflective elements (i.e., the active mirror 4406 and the deformable mirror 4404) are not tilted to modify the number of the passes. Rather, the ring of reflectors at the outer circumference of the redirection module 4405 is used for that purpose. The redirection module 4405 serves to provide multiple spatially separated passes on the active mirror.

The active mirror 4406 is imaged onto the deformable mirror 4404 and the deformable mirror 4404 is imaged onto the active mirror 4406, so that the elements are on conjugate image planes. In this regard, the deformable mirror 4404 of the WOMPA system 4400 may be adjusted without a pump laser energy source such that the conjugate image of the beam spot of the active mirror 4406 appears on the deformable mirror 4404. Thus, as power increases, the deformable mirror 4404 may be optimized to maintain maximum beam spot size.

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To assist in this regard, the WOMPA system 4400 may also be configured with a detector 4407 and an optical element 4408 as a sort of feedback control to the controller 4409. For example, the deformable mirror 4404 may provide leakage that is focused by the optical element 4408 to the detector 4407 (e.g., a digital camera). The detector 4407 may detect the optical intensity of the leakage laser energy 4410 to determine the output intensity the WOMPA system 4404 as provided by the active mirror 4406 in a manner similar to that described above. Thus, if the optical energy being obtained is less than desired, the controller 4409 may actuate the deformable mirror 4404 to change the beam spot size of the laser energy 4410 (e.g., by changing the focusing aspects of the deformable mirror 4404).

The WOMPA system 4400 may be configured in a variety of ways as a matter of design choice. For example, the WOMPA system 4400 may be configured with a mount (not shown) that is operable to assist in cooling the active mirror 4406. In this regard, the mount may include liquid cooling mechanisms and/or passive cooling mechanisms, such as heat spreaders. An example of a cooling technique shown and described below in the section entitled "Components Operable with a Multi-Pass Amplifier". Additionally, although shown and described with respect to a particular number of beam spots on the parabolic mirrors 4401 and 4402, the invention is not intended to be so limited. As mentioned, the controller 4409 may be operable to change the direction and/or beam spot size of the laser energy 4410 within the WOMPA system 4400.

FIG. 37 illustrates another axial WOMPA architecture in the WOMPA system 4500. While this embodiment does not use a redirector as was shown in FIG. 36, it is similar to the embodiments shown in FIGS. 4 and 35. However, the reflective elements 4404 and 4406 are positioned away from the center line between the parabolic reflectors 4401 and 4402. This configuration requires a relatively strong focus on at least one of the reflectors 4404 and 4406. In this embodiment, the reflector 4404, may be deformable mirror. The reflector 4404 may be configured outside the region between the parabolic mirrors 4401 and 4402. The reflector 4406 may be an active mirror, including a gain medium. The reflector 4404 may be configured within the region between the parabolic mirrors 4401 and 4402. More fundamentally, the reflectors 4404 and 4406 are positioned to allow passage of laser energy 4410 without impediment. The reflector 4406 is positioned at the focal point of the parabolic mirror 4401. The reflector 4404 is positioned at the focal point of parabolic mirror 4402.

The reflector 4404 is operable to change the number of round trips through tilt variation. If the reflector 4404 is a deformable mirror, it is additionally operable to compensate for any phase deformations and/or distortions induced on the laser energy 4410 by the reflector 4406. Since the deformable mirror is at the conjugate image plane of the reflector 4406, the deformable mirror 4404 may correct phase distortions from the reflector 4406 by inducing the precise opposite distortion on the laser energy 4410. By using a different focal length for the parabolas 4401 and 4402, the size of the image spot from laser energy 4410 may be magnified on the reflector 4404, relative to the reflector 4406. More particularly, the deformable mirror 4404 provides reimaging for the active mirror 4406 of the WOMPA system 4500. That is, the laser energy from the active mirror 4406 is reimaged onto the deformable mirror 4404. This allows for phase error from the active mirror 4406 to be more easily compensated by the deformable mirror 4404.

3. Gain Control of a Multi-Pass Amplifier

As mentioned previously, the WOMPA system 1000 (or its variations such as the WOMPA system 1600) may be config-

ured with a detector to assist in determining gain control. FIG. 38 illustrates one such optical configuration 4700. In this embodiment, the optical configuration 4700 has a pair of partially transmissive mirrors 4704-1 and 4704-2 that respectively direct the laser energy 4703 into and out of the WOMPA system 1000. More specifically, the laser energy 4703 enters the optical configuration 4700 and reflects off the mirror 4704-1 into the WOMPA system 1000 for multi-pass amplification via the thin disk gain medium 1001. The amplified laser energy 4703 exits the WOMPA system 1000 and the optical configuration 4700 via the mirror 4704-2.

A portion of the input laser energy 4703-In passes through the mirror 4704-1 and is detected by the camera 4701-1. The camera 4701-1 generates a digital image of the captured laser energy and transfers that image to the controller 4702 for processing. Similarly, a portion of the output laser energy 4703-Out passes through the mirror 4704-2 and is detected by the camera 4701-2 which also generates a digital image of the captured laser energy for transfer to the controller 4702.

With this configuration, a number of system parameters can be determined. For example, by comparing the digitally captured output laser energy to the digitally captured input laser energy, gain parameters relating to thin disk gain medium 1001 may be used to diagnose the effectiveness of the gain medium and/or control the number of passes through the thin disk gain medium 1001 as discussed above. In this regard, a comparison of the output power to the input power of the laser energy 4703 can be written as follows:

$$\frac{P_{OUT(x)}}{P_{IN(x)}} = e^{-2\alpha(x)nd}, \quad (8)$$

where $P_{OUT(x)}$ is the output power of the laser energy 4703, $P_{IN(x)}$ is the input power of the laser energy 4703, $\alpha(x)$ is the absorption constant of the gain medium 1001, n is the number of passes of the laser energy 4703 through the thin disk gain medium 1001 while within the WOMPA system 1000, and d is the thickness of the thin disk gain medium 1001. To compute the absorption constant of the thin disk gain medium 1001, the input intensity of the laser energy 4703-In detected by the camera 4701-1 may be compared to the output intensity of the laser energy 4703-Out detected by the camera 4701-2 as follows:

$$\ln\left(\frac{I_{OUT(x)}}{I_{IN(x)}}\right) = -2\alpha(x)nd, \quad (9)$$

where the absorption constant is the natural log performed on the output intensity of the laser energy 4703 $I_{OUT(x)}$ divided by the input intensity of the laser energy $I_{IN(x)}$ and then divided by two times the number of passes n and the thickness d . Thus, if a different absorption coefficient of the thin disk gain medium 1001 is desired, the thickness of the gain medium 1001 may be changed or else material of the gain medium 1001 be replaced in its entirety. Similarly, the number of passes through the gain medium 1001 may be used to change the gain of the thin disk gain medium 1001. For example, if additional gain in the output laser energy 4703-Out is desired, the controller 4702 may dynamically compute the input and output laser energies so as to determine the absorption constant $\alpha(x)$ of the gain medium 1001. From there, the controller 4702 may generate a control signal to increase the number of passes n that the input laser energy

4703-In makes through the thin disk gain medium 1001. This control signal may be applied to an actuator (e.g., an electro-mechanical device) that is used to control the tilt of one or more of the reflective elements within the WOMPA system 1000 (e.g., the reflective element 1002 and/or the reflective element 1001 associated with the thin disk gain medium 1001). Thus, to increase the gain of the output laser energy 4703-Out, the controller 4702 may apply a control signal that tilts the reflective element(s) in such a way as to increase the number of passes of the laser energy 4703-In through the WOMPA system 1000 as described above. Similarly, if less gain is desired in the output laser energy 4703-Out, the controller 4702 may tilt the reflective element(s) of the WOMPA system 1000 in the opposite way so as to decrease the number of passes of the laser energy 4703-In through the WOMPA system 1000. It should also be noted that the controller 4702 may tilt the reflective element(s) of the WOMPA system 1000 to stabilize the output "aiming" of the output laser energy 4703. Additionally, the controller 4702 may be configured to adjust other optical elements (e.g., an electro-optic modulator) to reduce variations in output pulse energy. Additionally, the controller 4702 may be configured to control a mirror actuator so as to adjust the round trip cavity length of a WOMPA system 1000 configured as or within an oscillator. Adjustments in the cavity length may be used to synchronize the output repetition rate of a mode-locked optical configuration to an externally controlled frequency.

The cameras 4701-1 and 4701-2 may also be used to detect the relative size of the input beam and output beam. In most configurations, the distances between the parabolic or OAP reflectors may be optimized to ensure that the input and output beam have the same size. Thus, the feedback from the cameras 4701-1 and 4701-2 may be used to drive an electronically controlled translation stage to adjust the distance between the OAP and/or the parabolic reflectors in any of the aforementioned WOMPA systems.

The cameras 4701-2 may also be configured as wavefront sensors (e.g. Shack-Hartmann wavefront sensors) and the controller 4702 may control a deformable mirror within the WOMPA system 1000. In this case, the controller 4702 may be used to select a phase deformation on a deformable mirror so as to optimize the phase distortions observed by the camera 4701-2. As mentioned previously, one of the reflective elements in a WOMPA system may be a deformable mirror to correct phase distortions imposed at any of the other reflective elements that are at a conjugate image plane. Additionally, a deformable mirror may be placed at a conjugate image plane to one of the reflectors, upstream from the to the entire WOMPA system. This allows a direct spatial correspondence of phase error imparted on a reflector, and phase correction imposed at the deformable mirror.

The camera 4701-1 may be placed at a position that is an upstream conjugate image plane to the disk, so that an image profile of the beam as observed by the disk on the first bounce can be detected. Likewise, the camera 4701-2 may be placed at a position that is a downstream conjugate image plane to the disk, so that an image that corresponds to the beam as observed at the last bounce from the disk can be observed.

It should be noted that multiple embodiments have been disclosed in which single parabolic or focusing elements are used to redirect multiple spatially separated optical beam paths. It should be understood that these optical elements used in the WOMPA systems may be cut or implemented as multiple independent optics, though described herein as single elements. For example parabolic reflectors may be

implemented as multiple parabolic and/or off-axis parabolic reflectors whose surfaces conform to a single parabolic optical surface described herein.

4. Components Operable with a Multi-Pass Amplifier

The dramatically high gain capabilities of the WOMPA systems herein present many advantages. For example, an optical communication system may employ a WOMPA system to amplify an optical communication signal external to the generation thereof so as to prevent damage to certain optical components within the optical communication system and/or conserve power. Such an implementation may be particularly advantageous in certain space-based platforms (e.g., satellites) where long-distance optical communications may be desired yet where power management is a constant concern.

As the advantages of the WOMPA systems are many, certain additional components may be useful in controlling the amplified optical energy from the WOMPA systems. For example, the WOMPA systems described above may impart a gain on a signal beam that is so intense that it may damage optics that are downstream from the WOMPA systems. The gain imparted on a signal beam may also increase the likelihood of ASE. In this regard, the components and systems presented herein may increase the advantages and benefits of the WOMPA systems so as to make the gain imparted by the WOMPA systems more manageable.

In one embodiment, one or more Chirped Volume Bragg Gratings (CVBGs) may provide a means for temporarily decreasing the intensity of optical energy through pulse stretching and compression. For very high peak power applications, pulse compression is typically performed with a pair of reflective gratings whereas stretching may be performed with a matched diffraction grating. Diffraction grating-based dispersion management is effective but generally requires large optical components and long optical paths. Accordingly, advantages occur when stretching and compression functions are performed with more compact devices, such as chirped volume Bragg gratings. Recent experimental results suggest that pulse energies up to 10 mJ may be compressed using a CVBG without damage.

FIG. 39 illustrates a block diagram of one exemplary CVBG-based system **4800** or performing laser pulse stretching and compression. In this embodiment, relatively low energy ultrashort pulses may be stretched by providing a wavelength dependent delay across the pulse spectrum using a CVBG **4800-1**. Such generally reduces the peak intensity of a laser pulse without decreasing the total energy of the laser pulse. A WOMPA system **4820**, such as those described above, may then be used to obtain relatively high pulse intensities. After amplification, a compensating wavelength-dependent delay may be introduced by way of a pulse compressor in the form of CVBG **4800-2**, so that the total delay includes negligible wavelength dependence across the pulse bandwidth of the pulse.

The CVBG **4800-1** may be implemented between a mode-locked seed system **4801** and a pulse picker **4802**. A thin film polarizer **4803** may be used to direct the signal (i.e., laser pulse **4810**) by way of the mirror **4806-1** into the CVBG **4800-1** at normal incidence after passing through a quarter-wave plate **4804-1**. The diffracted beam laser pulses may then exit the CVBG **4800-1** and, after traveling through the quarter-wave plate **4804-1** a second time, transmit through the thin film polarizer **4803**. The stretched pulses may then pass through the pulse picker **4802** that is used to select pulses at a

user defined repetition rate or at a desired modulation pattern. The pulses are then amplified with the WOMPA system **4820**. After amplification, the pulses enter and exit the CVBG **4800-2** in the same manner as **4800-1** to compress the laser pulses and reverse the CVBG **4800-1** influence. It should be noted that, although shown separately, the CVBG **4800-1** may also be used as the CVBG **4800-2** so that only one CVBG is needed.

FIGS. 40 and 41 illustrate the use of an optical aperture **4900** in a WOMPA system **1600** so as to keep the input beam **49304** free from a higher order distortion region around the rim of the pump beam spot on the thin disk gain medium **1001**. More specifically, FIG. 40 illustrates the optical element **4900** where a plurality of teeth **4901** about an aperture **4902**. Generally, the optical element **4900** may be a simple aperture without teeth, or may be a serrated aperture having teeth. One advantage of the serrated aperture is suppression of diffraction rings. However, if the diffraction rings fall outside of the pump spot on the gain medium **1001**, then they are generally absorbed and do not affect the output beam. The aperture may reduce the formation of "hot spots" on the OAPs **1003** and **1004**. The aperture **4901** assists in this regard if there are angular or spatial fluctuations of the input beam input beam **49304**, which would otherwise result in fluctuations of the signal beam location on the thin disk gain medium **1001**. As with some previous embodiments and again illustrated in FIG. 41, laser energy **4930** enters the WOMPA system **1600** along the path **4930-1**, through the optical element **4900** and through a polarization beam splitter **4925** and a focusing lens **4923**. Generally, the optical element **4900** is positioned so that it is imaged on to the reflective elements **1001/1002**. After multiple passes through the WOMPA system **1600**, the laser energy **4930** exits the WOMPA system **1600** along the path **4930-2**. The laser energy **4930** passes through the lens **4922** for recollimation. The laser energy **4930** then reflects off the reflective element for another trip through the WOMPA system **1600** to ultimately exit as the amplified laser energy **4930-O**.

FIG. 42 illustrates a WOMPA system **1000/1600** configured within a chamber **5300**. The chamber **5300** may include a port **5301** that is operable to extract gas from the chamber **5300** to create a vacuum. Alternatively, the port **5301** may be operable to fill the chamber **5300** with a gas that is difficult to ionize. In either case, the chamber **5300** assists in preventing optical breakdown from occurring at the intermediate focal points between the OAPs. For example, as the WOMPA system **1000/1600** may be operable to substantially increase the gain of the laser energy **5305**, the amplified laser energy may be intense enough to ionize the air and lead to absorption or distortion of the beam. Accordingly, by configuring the chamber **5300** as a vacuum or filling the chamber **5300** with a gas that is difficult to ionize, the potential for optical breakdown is reduced. Additionally, the use of a vacuum, partial vacuum, or well chosen gas can reduce other deleterious propagation effects (e.g. self-phase-modulation, nonlinear focusing, material dispersion through the air or gas).

In this embodiment, the chamber **5300** is also configured with an optical element **5302** that is operable to propagate the laser energy **5305** into the WOMPA system **1000/1600**. For example, the optical element **5302** may be operable to propagate the laser energy **5305** to and from the WOMPA system **1000/1600** with little or no absorption/focus such that the optical element that **5302** has little effect on the laser energy **5305**. Alternatively, the optical element **5302** may be operable to impart some focusing aspect on the laser energy **5305** as a matter of design choice. In any case, the chamber **5300** is operable to receive the laser energy **5305** from a source **5304**

such that the WOMPA system **1000/1600** may impart gain on the input laser energy **5305**. In this regard, the chamber **5300** may also be operable to transfer the amplified laser energy **5305** out of the chamber **5300** for use as desired.

It should be noted that the chamber **5300** may be operable to include fewer or more optical components than just the WOMPA system **1000/1600**. Similarly, the chamber **5300** may be operable to retain any of the WOMPA systems disclosed herein. In this regard, the WOMPA system designation of **1000/1600** is merely intended to designate any of the various WOMPA systems, their combinations, and variations disclosed herein. Accordingly, the invention is not intended to be limited to merely the exemplary embodiments shown and described above.

FIG. **43** illustrates another exemplary embodiment in which a WOMPA system (e.g., as defined by the parabolic mirrors **5352-1** and **5352-2**, the thin disk gain medium **5353**, the reflective element **5354**, and the ejection optics **5368**) is configured within a chamber **5350**. The chamber **5350** includes a port **5371** that is operable to extract gas from the chamber **5350** to create a vacuum or fill the chamber **5350** with a gas that is difficult to ionize, each of which being operable to prevent optical breakdown from occurring at the intermediate focal points between the parabolic mirrors **5352-1** and **5352-2**. The chamber **5350** may be operable with either an axial WOMPA system or an off-axis WOMPA system. FIG. **43** also illustrates various components used within the chamber **5350** and their relative relationships. For example, the parabolic mirror **5352-1** may be movably mounted in a direction **5351**. The parabolic mirror **5352-2** may be similarly mounted in a direction **5356**. The reflective element **5354** may be movably mounted in a direction **5365** as well as the tilt direction **5367**.

In this embodiment, the chamber **5350** includes two separable regions **5358** and **5359**. The WOMPA system is operable to receive an input beam **5360** for multiple passes through the chamber **5350**. That is, the beam **5360** makes multiple passes through the gain medium **5353** due to the positioning and the shape of the parabolic mirrors **5352-1/5352-2**, the reflective element **5354**, and the reflective element of the gain medium **5853** as described above. The WOMPA system ejects the gain increased beam **5360** from the chamber **5350** via the ejection optics **5368** (e.g., a quarter wave plate or other means for ejecting the beam as described above).

Input pump and signal lenses **5357** and **5367**, respectively, are shown along with the entrance beam path **5360** for the pump and signal beams. The output lens for the signal beam is obscured in this view. As the pump power is increased, the focus of the disk gain medium **5353** changes and the spacing between the two regions **5358** and **5359** generally requires adjustment. This alignment includes the following steps:

1. Separate the regions **5358** and **5359**.
2. The reflective element **5354** is tilted along **5367** and moved along direction **5365** so that the reflective surface is at the focus of parabolic mirror **5352-1** (additional adjustments can be made for the overall centering and a common or parallel optical axis).
3. The parabolic mirror **5352-2** is moved along the direction **5356** so that the thin disk gain medium **5353** is at the focal point of the parabolic mirror **5352-2**.
4. The pump lens **5357** is adjusted so that the pump beam is aligned and prepared for imaging on the thin disk gain medium **5353**.
5. The signal lens **5364** is then adjusted so that the signal focuses at the correct location (i.e., at the location **5370**, the interface to region **5359**).

6. The chamber **5350** is then assembled by configuring regions **5358** and **5359** proximate to one another such that a vacuum can be provided (or non ionizing gas) via the port **5361**.

7. The ejection optics **5368** are tilted to adjust for multi-pass output.

8. The parabolic mirror **5352-1** and the reflective element **5354** may then be moved along the direction **5351** to adjust for appropriate output magnification.

9. The pump power of the pump beam may then be moderately increased and the steps 7-9 may be repeated as needed.

10. The power of the input signal beam may then be moderately increased and the steps 7-10 may be repeated as needed.

FIGS. **44A** and **44B** illustrate a mounting mechanism **5400** for retaining an active mirror **1001**. For example, the reflective element **1001** (e.g., an active mirror) may be a highly reflective mirror configured with a relatively thin gain material **5403** adjacent to a highly reflective material **5411** so as to reflect laser energy **5410** while imparting gain on the laser energy **5410**. In this regard, the thin gain material **5403** may be pumped with pump optical energy such that the laser energy **5410** (e.g., a signal beam) may extract the gain from the gain material **5403**. As mentioned, a thin disk gain medium is particularly useful in implementing the above WOMPA systems. However, due to the substantially thin physical configuration of the gain material **5403**, the thin disk gain medium has the potential for imparting optical distortion on the exiting laser energy **5410** due to the thermo mechanical distortion of the gain material **5403** from the absorption of the entering laser energy **5410**. To compensate for such, the mounting mechanism rigidly retains the reflective element **1001** at the outer edges and disperses heat with a heat spreader **5402**. The heat spreader may be designed to effectively spread heat due to a large thermal conductivity or through other effective thermal transport means (material flow, convection, etc.). The reflective element **1001** may be designed to provide a negative curvature when the heat spreader **5402** is cooled and the upper gain material **5403** is relatively hotter. This thermal distribution may provide a greater expansion within the gain material **5403** than the heat spreader **5402** and lead to a negative curvature, as illustrated FIG. **44B**.

This embodiment also has the advantage of allowing the gain material **5403** to be edged pumped at the sides **5406** of the reflective element **1001** and/or through the surface **5407** of the gain material **5403**. Accordingly, the reflective elements **1001/1002** of the various WOMPA systems disclosed herein may be operable to edge pump and/or surface pump the gain material **5403**. In this regard, the gain material **5403** may be pumped with multiple forms of optical energy. For example, the gain material **5403** may be pumped with a variety of diode sources to provide redundancy and/or scalable power as described above.

It should be also noted that the various WOMPA architectures may include multiple such reflective gain mediums but that the gain materials **5403** need not be necessarily the same. For example, in an embodiment where the reflective elements **1001** and **1002** are configured with gain materials, each reflective element **1001** may include a different gain material so as to provide a broader effective gain spectrum. One specific embodiment may have the reflective element **1001** of the WOMPA system configured with a gain material Yb:YAG while the reflective element **1002** has a gain medium of Yb is configured with a different host material to slightly shift the gain spectrum. Such a WOMPA system may be operated at cryo temperature to provide a narrowing of the gain bandwidth of the Yb:YAG alone and may be compensated by the

composite gain bandwidth of the two separate crystals. However, the invention is not intended to be limited to any particular type of gain material **5403** being configured with the reflective elements **1001/1002** as the gain materials may be selected as a matter of design choice. For example, Ytterbium doped materials are generally a good design choice, although Erbium, Chromium, Thulium, Holmium may be good dopant choices for other wavelengths. The host crystal may be YAG, but there are many other suitable crystal hosts, including KYW, and Lu_2O_3 .

FIG. **45** illustrates a WOMPA system **5430** employing a plurality of baffles **5431** at various locations within the region between the parabolic mirrors **5432-1** and **5432-2**. The baffles **5431** are generally configured from an opaque material so as to absorb fluorescence **5437** within the WOMPA system **5430**. For example, if the thin disk gain medium **5436** (i.e., configured with a reflective element as described above) fluoresces due to the lack of a signal beam, the fluorescence **5437** may oscillate and reflect virtually everywhere within the WOMPA system **5430**, potentially and undesirably extracting energy from the thin disk gain medium **5436**. The baffles **5434** may prohibit unwanted fluorescence **5437** from being imaged back onto the thin disk gain medium **5436** and extracting energy that could otherwise be used to provide gain to the signal beam.

The baffles **5431** may be positioned at locations within the WOMPA system **5430** so as to allow the laser energy **5434** to propagate through the WOMPA system **5430** as desired. For example, the laser energy **5434** may enter the WOMPA system **5430** through the lens **5433** and reflect off the parabolic mirror **5432-2** to the thin disk gain medium **5436**. The laser energy **5434** may then reflect to the parabolic mirror **5432-2** for reflection to the parabolic mirror **5432-1**. The laser energy **5434** then reflects to the reflective element **5435**, back to the parabolic mirror **5432-1**, returning to the parabolic mirror **5432-2** for a complete trip to the WOMPA system **5430**, as similarly described above, unimpeded by the baffles **5431**. These baffles **5431** may be implemented in any of the WOMPA systems shown and described herein. In this regard, the WOMPA system **5430** may be an axial WOMPA system (i.e., a top view) or an OAP based WOMPA system (i.e., a side view).

FIG. **46** illustrates an exemplary optical configuration **5450** having “closed-loop” control of a deformable mirror **5460** for use with a WOMPA system **1000**. For example, the controller **5461** may adjust the deformable mirror **5460** to reduce or minimize wavefront distortion of the laser energy **5453** detected by a wavefront sensor **5456** as the laser energy **5453** exits from the WOMPA system **1000**. In this embodiment, the optical configuration **5450** is also configured with a pair of focusing elements **5452-1** and **5452-2** (e.g., lenses), a quarter wave polarizer **5457**, a beam splitter **5459**, an aperture **5458**, another pair of focusing elements **5451-1** and **5451-2**, and a partially reflective mirror **5455**. The laser energy **5453** enters the optical configuration **5450** along the beam **5453-I** where it reflects off the beam splitter **5459** through the quarter wave polarizer **5457** and the focusing elements **5452-1** and **5452-2**.

The focusing elements **5452-1** and **5452-2** form a beam expander that provides for less sensitive control of wavefront distortion. For example, with the beam of laser energy **5453** expanded, subtler correction of the wavefront may be imparted on the laser energy via the deformable mirror **5460**. That is, it is more difficult to alter the wavefront of the laser energy **5453** when the beam encompasses a smaller area. In this regard, the beam expander may provide more design options as well as increase damage power thresholds to the deformable mirror **5460**. For example, a larger beam of laser

energy **5453** is less likely to damage the deformable mirror **5460** than a more tightly focused beam of laser energy **5453**.

The focusing element **5452-2** has a focal length of f_d such that the laser energy **5453** has an intermediate focus at the point **5462**. This focal length f_d is also the same distance between the focusing element **5452-2** and the aperture **5458** such that the aperture is imaged onto the thin disk gain medium of the WOMPA system **1000** upstream from the WOMPA system **1000**. The focusing element **5452-1** has a focal length of f_b from the intermediate focus **5462**. In this regard, the deformable mirror **5460** is positioned at the same focal distance f_b from the focusing element **5452-1**. The laser energy **5453** reflects off the deformable mirror **5460**, through the focusing elements **5452-1** and **5452-2** and the quarter wave polarizer **5457** such that the laser energy **5453** passes through the aperture **5458** to enter the WOMPA system **1000** through the focusing element **5451-1**. The WOMPA system **1000** then imparts gain on the laser energy **5453**, as described above, and exits the WOMPA system through the focusing element **5451-2** and a partially reflective mirror **5455** along the output beam path **5453-O**.

A portion of the laser energy **5453** passes through the partially reflective mirror **5455** to the wavefront sensor **5456**, which in turn detects any wavefront distortions imparted on the laser energy **5453** by the WOMPA system **1000**. For example, due to the multiple passes through the WOMPA system **1000** and the various reflective elements therein, the laser energy **5453** may experience wavefront distortions. The wavefront sensor **5456** may detect these distortions such that they may be handled/corrected outside the WOMPA system **1000**. In this regard, the controller **5461** may compute an appropriate correction based on the detected wavefront of the laser energy **5453** passing through the partially reflective mirror **5455** and generate a control signal that is used to actuate (i.e., change the shape of) the deformable mirror **5460**.

In this exemplary configuration **5450**, the upstream image plane is imaged onto the gain medium by the WOMPA system **1000** and the input lens **5451-1**. In this regard, the deformable mirror **5460** is imaged upstream from the WOMPA system **1000**. Additionally, the optical configuration **5450** positions the aperture **5458** upstream from the WOMPA system **1000** such that the aperture **5458** is also imaged on the thin disk gain medium of the WOMPA system **1000**, providing a virtual aperture on the thin disk gain medium. The advantages of such include reducing the risk of damage due to undesirable trajectories of the beam. Less than desirable forms of optical energy may propagate near the beam of the laser energy **5453**. These undesirable forms of optical energy may produce “hotspots” on the reflective elements within the WOMPA system **1000** (or other elements downstream) due to the increasing gain imparted on the laser energy **5453** by the multiple passes through the thin disk gain medium. By placing the aperture **5458** upstream from the WOMPA system **1000**, the aperture is virtually imaged on the thin disk gain medium and thereby removes these undesirable components of optical energy before they impinge downstream optics.

5. Exemplary Systems Employing Multi-Pass Amplifiers

FIG. **47** is a block diagram of an exemplary use of the WOMPA system **1600**. In this embodiment, a system **5500** may employ the WOMPA system **1600** such that multiple beam lines can be switched by an optical switch **5502** at relatively low power upstream from amplification by the WOMPA system **1600**. For example, a seed source **5501** may

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provide a signal beam to the optical switch **5502** which demultiplexes the signal beam into various component beams. The optical switch **5502** may transfer the component beams to the WOMPA system **1600** for amplification. After amplification, the amplified component beams may be directed to separate launch optics **5503-1** . . . **N**. In this regard, scanning operation of the launch optics **5503-1** . . . **N** may be managed according to different spatial regions. Additionally, switching between separate launch optics **5503-1** . . . **N** may be performed at lower power to allow for smaller and faster switching technologies.

FIG. **48** is a block diagram of another exemplary system **5600** employing the WOMPA system **1000/1600**. In this embodiment, the seed source **5501** provides a signal beam to an encoder **5602** for communication purposes. Because signals can be imparted on a signal beam by the encoder **5602** at relatively low power and then downstream amplified to high power, high power optical communications may be possible as damage to the encoder **5602** from a high power signal beam is avoided. Such may be particularly advantageous in long distance free space communications, including satellite communications and deep space missions.

6. Additional Embodiments

FIGS. **49A-C** illustrate a multi-pass optical amplifier **5700** in another exemplary embodiment. More specifically, FIG. **49B** illustrates a side view of the multi-pass optical amplifier **5700** with FIGS. **49A** and **C** illustrating faces of OAPs **5701**, **5702**, and **5703** that are used in the multi-pass optical amplifier **5700**. The multi-pass optical amplifier **5700** is operable to spatially multiplex the optical energy **5710** to increase the number of passes of the optical energy **5710** through a thin disk gain medium. The multi-pass optical amplifier **5700** includes a thin disk gain medium/reflective element **5706**. The thin disk gain medium/reflective element **5706** may be implemented as two components: a first component with a gain medium affixed to a mirror; and a second component that is simply a mirror or another gain medium affixed to a mirror. Although illustrated as a single component **5706**, these two components may be displaced in space with respect to one another. That is, the first component may be projected outward from the page of the drawing (e.g., towards the viewer) whereas second on may be projected into the page of the drawing (e.g., away from the viewer). An alternative embodiment where the components are configured as one is illustrated in FIG. **51**. In any case, the thin disk gain medium/reflective element **5706** defines the optical cavity for multi-pass optical amplifier **5700**.

The multi-pass optical amplifier **5700** also includes a vertical multiplexing mirror **5705** that is operable, in conjunction with the OAP **5703**, to change the elevation of the optical energy **5710** impinging the OAPs **5701** and **5702**. For example, the optical energy **5710** enters the multi-pass optical amplifier **5700** above the OAP **5703** to impinge the OAP **5701** and initiate a first loop along a pair of elevations **5715-1** through the multi-pass optical amplifier **5700**, as illustrated on the OAP faces **5701F-5703F** of FIGS. **49 A** and **C**. In this embodiment, the optical energy **5710** bounces between the OAPs **5701** and **5702** making six round-trip passes through the thin disk gain medium during this loop of the optical energy **5710** through the first pair of elevations **5715-1**, assuming that there is one thin disk gain medium in the multi-pass optical amplifier **5700** configured with the thin disk gain medium/reflective element **5706**.

Upon the final reflection from the OAP **5701** in the first loop through the first pair of elevations **5715-1**, the optical

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energy **5710** is reflected to the OAP **5703** which in turn changes the elevation of the optical energy **5710** to the pair of elevations **5715-2**. For example, the OAP **5703** reflects the optical energy **5710** to the vertical multiplexing mirror **5705**, which in turn **5705** reflects the optical energy **5710** to the OAP **5703** at a different elevation. This initiates a second loop through the multi-pass optical amplifier **5700** along a second pair of elevations **5715-2** on the OAPs **5701** and **5702**. Eventually, the optical energy completes this loop along the pair of elevations **5715-2** followed by a loop along the elevation **5715-3**. The optical energy **5710** then reverses course within the multi-pass optical amplifier **5700** to complete another loop along the pair of elevations **5715-2** followed by another loop along the pair of elevations **5715-1** before exiting the multi-pass optical amplifier **5700**. Thus, the multi-pass optical amplifier **5700** is operable to propagate the optical energy **5710** with thirty round trips through the gain medium before exiting the multi-pass optical amplifier **5700** in this exemplary embodiment, again assuming a single thin disk gain medium. That is, the optical energy **5710** propagates to the gain medium thirty times, each time passing through the gain medium and being reflected back through the gain medium such that the optical energy **5710** has sixty passes through the gain medium. The invention, however, is not intended to be limited to any particular number of passes through the gain medium.

Additional details regarding the propagation along the elevations are illustrated in FIG. **50**. In FIG. **50**, the optical energy **5710** enters the multi-pass optical amplifier **5700** as optical energy **5710-1** above the OAP **5703** to reflect off the OAP **5701** at the beam spot **5710-2** within the first pair of elevations **5715-1**. The OAP **5701** then reflects the optical energy **5710** to the thin disk gain medium/reflective element **5706** which in turn reflects the optical energy back to the OAP **5701** at the beam spot **5710-3**. The OAP **5701** then reflects the optical energy **5710** to the OAP **5702** at the beam spot **5710-4**. The OAP **5702** then reflects the optical energy **5710** to the thin disk gain medium/reflective element **5706** for reflection back to the OAP **5702** at the beam spot **5710-5**. The OAP **5702** reflects the optical energy **5710** to the OAP **5701** at the beam spot **5710-6** (i.e., at a different horizontal location within the first pair of elevations **5715-1**). This reflection between the OAPs **5701** and **5702** along the pair of elevations **5715-1** occurs in the illustrated numerical order (i.e., **5710-1**, **5710-2**, **5710-3**, etc.) and culminates with the final reflection to the OAP **5703** at the beam spot **5710-24**. The OAP **5703** then reflects the optical energy **5710** to the vertical multiplexing mirror **5705**, which in turn reflects the optical energy **5710** back to the OAP **5703** at the beam spot **5710-25** to initiate another loop through the multi-pass optical amplifier **5700** along the second pair of elevations **5715-2**. This process continues for the pair of elevations **5715-2** followed by the elevation **5715-3**. After completing the elevation **5713-3**, the optical energy **5710** reverses course until the optical energy **5710** exits the multi-pass optical amplifier **5700**.

It should be noted that the invention is not intended be limited to any particular number of elevations or beam spots illustrated in the drawings, as such may be a matter of design choice. For example, each of the OAPs **5701**, **5702**, and **5703** may be increased in size to accommodate more beams spots and, thus, more elevations on the OAPs. These larger sizes of the OAPs may therefore accommodate more passes of the optical energy **5710** through the thin disk gain medium of the element **5706**.

As discussed, the thin disk gain medium/reflective element **5706**, in an alternative embodiment, may be configured as a single module with one or more thin disk gain mediums. For

example, the thin disk gain medium/reflective element **5706** may be configured as a two-sided mirror with a thin disk gain medium disposed on either or both sides. In this regard, the layout of the OAPs **5701** and **5702** may be altered such that both OAPs **5701** and **5702** reflect towards the thin disk gain medium/reflective element **5706**. An example of such is illustrated in FIG. **51**.

In FIG. **51**, the multi-pass optical configuration **5800** has a first OAP **5701** and a second OAP **5702** configured to reflect optical energy **5710** to a single thin disk gain medium/reflection module **5706** as well as to each other. In this regard, the thin disk gain medium/reflection module **5706** may be configured as a sort of triangular block with reflective sides **5732** that are operable to reflect to the OAPs **5701** and **5702**. One or both of the reflective sides **5732** may have a thin disk gain material **5731** disposed thereon so as to impart gain on the impinging optical energy **5710** as disclosed herein. Accordingly, the invention is not intended to be limited to any particular optical configuration disclosed herein as such implementations may be a matter of design choice (e.g., based on size constraints, etc.).

FIG. **52** is a block diagram of a mount **5908** and the thin disk gain medium/reflective module **5907**. In this embodiment, the thin disk gain medium/reflective module **5907** includes a gain material **5952** disposed on a reflective element **5957**. In this regard, the thin disk gain medium/reflective module **5907** may be operable to impart gain on an incoming signal beam **5920** as it passes through the gain material **5952**. For example, the signal beam **5920** may pass through the gain material **5952** from the front side of the thin disk gain medium/reflective module **5907** and amplify according to the gain established by the pump beam **5910**. The signal beam **5920** may then reflect off the reflective element **5957** and exit the thin disk gain medium/reflective module **5907** from the front side.

The mount **5908** may be configured with one or more brackets **5951** that are operable to retain the thin disk gain medium/reflective module **5907** about its edges. For example, while FIG. **52** illustrates the mount **5908** as two brackets **5951** retaining the thin disk gain medium/reflective module **5907** at opposite ends, FIG. **52** may be assumed to be a cutaway view with the bracket **5951** actually being circular. In this regard, the thin disk gain medium/reflective module **5907** may also be circular in shape.

The thin disk gain medium/reflective module **5907** may be affixed to the one or more mounting brackets **5951** via an optical glue or other means for rigidly retaining the thin disk gain medium/reflective module **5907**. In this regard, as the thin disk gain medium/reflective module **5907** imparts gain on the signal beam **5920**, some of the energy is transferred to the thin disk gain medium/reflective module **5907** as thermal energy. That is, some optical energy is absorbed by the gain material and then converted to thermal energy. This transfer of thermal energy may tend to "buckle" and alter the wavefront of the signal beam **5920**. For example, the signal beam **5920** may impinge the gain material **5952** and intensely heat a region **5956** of the gain material **5952**. Other regions of the gain material **5952** (e.g., regions **5955**, **5954**, and **5953**) may have lower temperatures. That is, the thin disk gain medium/reflective module **5907** may experience decreasing temperatures further away from the point at which the signal beam **5920** impinges the gain material **5952**. This temperature gradient may cause the thin disk gain medium/reflective module **5907** to physically expand at the inner/hotter temperature regions thereby changing the focusing aspects of the thin disk gain medium/reflection module **5907**.

To compensate for the physical distortion, the back side of the thin disk gain medium/reflective module **5907** (e.g., the reflective element **5957**) may be cooled. For example, the mount **5908** may be hollow at the back side of the thin disk gain medium/reflective module **5907** such that cooling means may be applied to the back side of the thin disk gain medium/reflective module **5907** to extract heat **5960** from the thin disk gain medium/reflective module **5907**. Examples of such cooling means include pumping cooled water to the back of the thin disk gain medium/reflective module **5907** and cryogenic cooling. In one embodiment, the cooling to the back of the thin disk gain medium/reflective module **5907** may be tuned to control the physical distortion of the thin disk gain medium/reflective module **5907**. For example, certain desirable optical effects, such as wavefront shape and beamsizes changes, may be imparted on the signal beam **5920** by changing the shape of the thin disk gain medium/reflective module **5907** in a particular way. By controlling the thermal mechanical distortions of the thin disk gain medium/reflective module **5907** through the controlled tuning of the temperature of the thin disk gain medium/reflective module **5907**, the thin disk gain medium/reflective module **5907** may impart certain desired effects on the signal beam **5920**.

FIG. **53** is a block diagram of a multi-pass optical amplifier **6000** in one exemplary embodiment. In this embodiment, the multi-pass optical amplifier **6000** includes a reflective element **6007**, a gain module **6004**, and OAPs **6008**, **6009**, and **6010**. The reflective element **6007** and the gain module defines the optical cavity for the multi-pass optical amplifier **6000**. The multi-pass optical amplifier **6000** also includes fold mirrors **6005** and **6006** and a horizontal multiplexing mirror **6003**. The gain module **6004** in this embodiment is configured as a thin disk gain medium disposed on a reflective element such as a mirror.

The multi-pass optical amplifier **6000** provides scalable high energy extraction and gains based on the number of passes of a signal beam **6012** through the thin disk gain medium of the gain module **6004**. For example, the number of passes of the signal beam **6012** within the multi-pass optical amplifier **6000** may be controlled by the tilt of one or more of the optical elements therein (e.g., the horizontal multiplexing mirror **6003**, the gain module **6004** and/or the reflective element **6007**). These optical elements may also be tilted to actively control the output alignment of the signal beam **6012**.

Similar to the multi-pass optical amplifier **5700** of FIG. **49**, the horizontal multiplexing mirror **6003** is operable to propagate the signal beam **6012** along multiple spatially distinct paths between the OAP **6008**, **6009**, and **6010**. For example, the multi-pass optical amplifier **5700** may propagate the signal beam **6012** along multiple paths in approximately a first plane between the OAPs **6008** and **6009** as well as along multiple paths in approximately a second plane between the OAPs **6008** and **6010** to cause multiple incidents of the signal beam **6012** on the thin disk gain medium of the gain module **6004** to impart gain on the signal beam **6012**. In this regard, the horizontal multiplexing mirror **6003** may direct propagation of the signal beam **6012** along multiple pairs of beam spot columns between the OAP **6008** and **6009** as well as multiple pairs of beam spot columns between the OAPs **6008** and **6010**. Such propagation is explained in greater detail below.

In addition to multiplexing the signal beam **6012**, the horizontal multiplexing mirror **6003** may be configured as a dichroic mirror that is operable to input one or more beams of pump laser energy **6013-1-N** from pump laser sources **6001-1-N** and cause co-propagation of the pump laser energy **6013-1-N** with the signal beam **6012** within the multi-pass optical amplifier **6000**. That is, the dichroic horizontal multiplexing

mirror **6003** is operable to pass the beams of pump laser energy **6013-1-N** for entrance into the multi-pass optical amplifier **6000**. In doing so, the dichroic mirror may filter the beams of pump laser energy **6013-1-N** such that only certain wavelengths pass into the multi-pass optical amplifier **6000** as a combined beam **6013** of pump laser energy. This combined beam **6013** of pump laser energy enters the multi-pass optical amplifier **6000** and propagates through the multi-pass optical amplifier **6000** in the same manner as the signal beam **6012**, although not necessarily along the same path as the signal beam **6012** on the OAPs **6008**, **6009**, and **6010**.

The pump laser sources **6001-1-N** may propagate the beams of the pump laser energy **6013-1-N** across fiber to the multi-pass optical amplifier **6000**. For example, the pump laser sources **6001-1-N** may be diode lasers that are optically coupled to the multi-pass optical amplifier **6000** via fiber optic cables. In such an instance, multimode fiber may be used to homogenize the pump laser sources **6001-1-N**. For a multimode fiber delivered pump source, the diameter of the fiber facet and numerical aperture generally determine the maximum throughput of the pump laser sources **6001-1-N**. With this throughput in mind, the divergence of the beam **6013** and beam size can be related. For example, by decreasing the diameter of a beam **6013**, its divergence is increased. Accordingly, the beam size the OAP **6008**, can be minimized at the price of increasing the beam size on the OAP **6009**. Once the beam **6013** enters the multi-pass optical amplifier **6000**, the beam **6013** is reimaged onto the thin disk gain medium of the gain module **6004**. Thus, the relatively large footprint of the pump beam **6013** on the OAP **6009** overlaps without deteriorating the signal beam **6012**. The pump beam **6013** may then be injected into the multi-pass optical amplifier **6000** to make multiple passes on the thin disk gain medium of the gain module **6004**.

As mentioned, the divergence and the beam size of the pump beam **6013** determines the size of the image of the fiber facet on the gain medium of the gain module **6004**. With a given fiber numerical aperture, facet size, parabola focal length, and required magnification, the smallest beam size attainable can be calculated. Such may be advantageous to prevent overlap of beam spots of the signal beam **6012** and the pump beam **6013** as illustrated and described in FIGS. **54** and **55**. These parameters may be related to give the minimum beam size of the beam **6013** at the entrance to the multi-pass optical amplifier **6000** on a per loop basis as follows:

$$D_{min} = \frac{2(NA)(D_{fiber})(f)}{D_{image}} = \frac{2(NA)(f)}{M},$$

where D_{min} is the minimum beam diameter passing by the OAP **6009**, NA is the numerical aperture, M is the desired magnification, D_{image} is the desired beam diameter on the OAPs **6008**, **6009**, and **6010**, D_{fiber} is the beam diameter of the fiber, and f is the focal length of the OAPs **6008** and **6009**.

A minimum beam size of the pump beam **6013** may either be virtual or actual depending on the pump optic configuration. Certain advantages exist in placing the minimum spot size of the pump beam **6013** at a single loop entrance port of the multi-pass optical amplifier **6000**. For example, the multiplexing angle is generally constrained by the requirement that after the first round trip of the pump beam **6013** through any pumping loop, the pump beam **6013** should not overlap the entrance of the pump beam **6013** for that loop. By minimizing the spot size of the pump beam **6013** at the OAP **6010** while retaining imaging of the fiber facet on the gain medium

of the gain module **6004**, a smaller multiplexing angle may be used (e.g., based on the tilt of the gain module **6004** and/or the reflective element **6007**). Also, using a smaller multiplexing angle allows for more bounce passes per loop and provides additional energy extraction capability from the thin disk gain medium of the gain module **6004**. A lens at a conjugate image plane to the fiber may alternatively or additionally be used to accomplish such without changing the overall magnification of the multi-pass optical amplifier **6000**.

Additionally, for the beam of pump laser energy **6013** to co-propagate with the signal beam **6012** through the multi-pass optical amplifier **6000**, the beam **6013** should have a small enough footprint on the OAP **6010** such that it does not limit the number of passes for the signal beam **6012**. For example, co-propagation generally means that the signal beam **6012** propagates through the multi-pass optical amplifier **6000** while the pump beam **6013** propagates through the multi-pass optical amplifier **6000**. As mentioned, it may be more advantageous to ensure that the signal beam **6012** and the pump beam **6013** do not propagate along the same path at the same time so as to prevent interference with one another. Accordingly, the beam **6013** may be made small enough so as to ensure that the beam **6013** does not fly along the same path (e.g., by flying the beam **6013** in between or around beams spots of the signal beam **6012** on the OAPs **6008**, **6009**, and **6010**).

If the thin disk gain medium of the gain module **6004** is pumped by a fiber, the fiber may be imaged onto the gain medium of the gain module **6004** in order to obtain an approximate "top hat" pumping profile (e.g., akin to a step function). Based on the properties of the pump fiber, the focal lengths for the OAP **6008** and the OAP **6009** are generally chosen to give a minimum beam size for the pump beam **6013** that is similar or slightly larger than the beam size of the signal beam **6012**. The optics of the pump laser sources **6001-1-N** may be operable to image the fiber facet at the horizontal multiplexing mirror **6003** with a desired magnification. For example, placing a lens **6015** proximate to the horizontal multiplexing mirror **6003** or adding curvature to the back of the horizontal multiplexing mirror **6003** projects the minimum footprint of the pump beam **6013** onto the OAP **6010**. The beam then diverges between the OAP **6008** and the OAP **6010**, requiring that the OAP **6008** be oversized to accommodate the larger beam spot for the beam **6013**. In this arrangement, a single loop may be used for each pump source such that the OAPs **6008**, **6009**, and **6010** are sized according to a desired number of passes of the beam **6013** through the multi-pass optical amplifier **6000**.

If the beams of pump laser energy **6013-1-N** from their respective pump sources **6001-1-N** are not homogenized, the waist of the pump beam **6013** may be propagated between the OAPs **6008** and **6009** along a path that is similar to the signal beam **6012**. Additionally, by increasing the number of passes of the pump beam **6013**, the pump energy can be efficiently absorbed even if the absorption per pass within the multi-pass optical amplifier **6000** is lower. This increased efficiency in pump absorption allows a selection of a pump wavelength with lower material absorption than would be considered for other amplifier configurations. Thus, the requirements for the bandwidth and wavelength drift of the pump laser energy **6013** are less restrictive with this multi-pass configuration.

While increasing gain in the signal beam **6012**, the multi-pass optical amplifier **6000** also reduces undesirable optical phase distortions in the thin disk gain medium. For example, the optical configuration of the multi-pass optical amplifier **6000** is operable to provide conjugate imaging with the gain module **6004** and the reflective element **6007**. This conjugate

imaging substantially reduces any optical phase distortion imparted on the signal beam 6012 during amplification. The multi-pass optical amplifier 6000 also amplifies laser pulses of the signal beam 6012 in a more elegant/uniform fashion than previous optical amplifiers. For example, because multiple, spatially separate, optical paths can be passed through the same gain region, gain clearing can be achieved by splitting off a smaller percentage of an output pulse and recycling that smaller percentage of the output pulse through the multi-pass optical amplifier 6000 along a slightly different path to clear out residual gain in the gain medium of the gain module 6004. And, by operating in a bi-stable dynamic regime, every other seed pulse of the signal beam 6012 can be used to clear out gain within the thin disk gain medium of the gain module 6004 so that energy extraction pulses of the signal beam 6012 can experience gain after a uniform gain build up. This gain clearing causes gain imparted on the signal pulses to be more uniform. The amplified back scattered signal pulses can then be sent to a beam dump. By using a back reflection of a small portion of the output pulse to clear out the residual gain, it is also possible to achieve stable operation at frequencies that would otherwise provide a chaotic or unstable operation. In this regard, the back reflected portion of the output pulse may be as simple as a surface glint that is deflected and then redirected along a beam path through the multi-pass optical amplifier 6000 such that the output is separable from the input. It should be noted that these features may also be available to any of the multi-pass systems described above.

With these concepts in mind, the propagation of the signal beam 6012 and the pump beam 6013 through the multi-pass optical amplifier 6000 may be addressed with respect to the OAPs 6008, 6009, and 6010 illustrated in FIGS. 54 and 55. More specifically, FIG. 54 illustrates the propagation of the signal beam 6012 through the multi-pass optical amplifier 6000 whereas FIG. 55 illustrates an exemplary propagation of the pump beam 6013 through the multi-pass optical amplifier 6000. Beginning with the signal beam 6012 in FIG. 54, the signal beam 6012 enters the multi-pass optical amplifier over the OAP 6010 proximate to the OAP 6009, illustrated as the beam spot 6012-1. The signal beam 6012 impinges the OAP 6008 at the beam spot 6012-2 in a first of a pair of beam spot columns 6020-1 and reflects to the fold mirror 6006 for reflection to the reflective element 6007. The reflective element 6007 reflects the signal beam 6012 to the fold mirror 6006 for reflection to the OAP 6008 at the beam spot 6012-3 in a second of the pair of beam spot columns 6020-1. The OAP 6008 reflects the signal beam 6012 to the OAP 6010 at the beam spot 6012-4 in a first of the beam spot columns 6020-1 for the OAP 6010, which in turn reflects the signal beam 6012 to the fold mirror 6005 for reflection to the gain module 6004. After passing through the thin disk gain medium of the gain module 6004, the signal beam 6012 reflects back through the gain medium to the fold mirror 6005 for reflection to the OAP 6010 at the beam spot 6012-5 in a second of the beam spot columns 6020-1 for the OAP 6010. The OAP 6010 reflects the signal beam 6012 to the OAP 6008 at the beam spot 6012-6 and continues this numerically illustrated propagation (i.e., 6012-1, 6012-2, 6012-3, etc.), ultimately impinging the OAP 6009 at the beam spot 6012-24.

The OAP 6009 based in part on its angular position with respect to the OAP 6010 horizontally multiplexing is the signal beam 6012 to another pair of beam spot columns 6020-2. For example, the OAP 6009 reflects the signal beam 6012 from the beam spot 6012-24 to the horizontal multiplexing mirror 6003 which, in turn reflects the signal beam 6012 back to the OAP 6009 at the beam spot 6012-25. The OAP 6009 then reflects the signal beam 6012 to a first of a second pair of

beam spot columns 6020-2. Like the propagation of the optical energy 5710 in FIGS. 49 and 50, the signal beam 6012 continues propagating through the multi-pass optical amplifier 6000 through the pairs of beam spot columns 6020, ultimately reversing course to exit the multi-pass optical amplifier 6000. That is, once the signal beam 6012 completes propagation through a beam spot column scratch them 6020 at the center of the OAPs 6008 and 6010 (or a center pair of beams spot columns 6020), the signal beam 6012 reverses course and propagates through the multi-pass optical amplifier 6000 in reverse order. For example, in approaching the pairs of beam spot columns 6020-1, the signal beam 6012 propagates to the beam spot 6012-25 on the OAP 6009 for reflection to the horizontal multiplexing mirror 6003. The horizontal multiplexing mirror 6003 reflects the signal beam 6012 to the beam spot 6012-24 on OAP 6009 for reflection to the OAP 6008 at the beam spot 6012-23. The signal beam 6012 then continues along the beam spots in this reverse numerical order (e.g., 6012-25, 6012-24, 6012-23, etc.) until the signal beam 6012 exits the multi-pass optical amplifier 6000.

The exit of the signal beam 6012 may be at or about the beam spot 6012-1 or exit the multi-pass optical amplifier 6000 at a different location. For example, the optical element 6016 may include a polarization beam splitter and a quarter-wave plate to change the polarization of the signal beam 6012 as it enters the multi-pass optical amplifier 6000. Upon exiting the multi-pass optical amplifier 6000, the signal beam 6012 may pass again through the quarter wave plate thereby changing the polarization of the signal beam 6012 such that it reflects off the polarization beam splitter to exit the multi-pass optical amplifier 6000. This configuration could be implemented at various locations within the multi-pass optical amplifier 6000 as a matter design choice (e.g., based on a desired number of passes through the thin disk gain medium, recirculation of the signal beam 6012 through the multi-pass optical amplifier 6000, etc.).

Turning now to the pump beam 6013, the pump beam 6013 enters the multi-pass optical amplifier 6000 through the horizontal multiplexing mirror 6003. After passing through the horizontal multiplexing mirror 6003 to enter the multi-pass optical amplifier 6000, the pump beam 6013 is incident upon the OAP 6009 at the beam spot 6013-1. The OAP 6009 reflects the beam of pump laser energy 6013 to the OAP 6008 at the beam spot 6013-2 in a first pair of beam spot columns 6030-1 on the OAP 6008. The OAP 6008 reflects the pump laser energy 6013 to the fold mirror 6006 for reflection to the reflective element 6007. The reflective element 6007 reflects the pump laser energy 6013 to the fold mirror 6006 for reflection back to the OAP 6008 at the beam spot 6013-3 in a second of the first pair of beam spot columns 6030-1. From there, the OAP reflects the pump beam 6013 to the beam spot 6013-4 on the OAP 6010. The OAP 6010 reflects the pump beam 6013 to the fold mirror 6005 for reflection to the reflective element 6004. The reflective element 604 then reflects the pump beam 6013 back to the fold mirror 6005 for reflection to the OAP 6010 at the beam spot 6013-5. The pump beam 6013 continues this propagation in the illustrated numerical order (e.g., beam spot 6013-1, 6013-2, 6013-3, etc.) until it propagates into another column of beam spots (e.g., one or more beam spot columns 6030-2) on the OAP 6008.

After completing multiple passes through the remaining beam spot columns 6030, the pump beam 6013, like the signal beam 6012, reverses course in the multi-pass optical amplifier 6000 to exit the multi-pass optical amplifier 6000. For example, upon approaching the first pair of beam spot columns 6030 on its reverse trajectory, the pump beam 6013

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propagates to the beam spot **6013-21** for reflection to the fold mirror **6005** and the reflective element **6004**. The reflective element **6004** then reflects the pump beam **6013** to the fold mirror **6005** for reflection to the OAP **6009** at the beam spot **6013-20**, which in turn propagates the pump beam **6013** to the OAP **6008** at the beam spot **6013-19**. This propagation of the pump beam **6013** continues in reverse numerical order until the pump beam **6013** exits the multi-pass optical amplifier **6000**. Generally, this exit of the pump beam **6013** occurs at the point of entry of the pump beam **6013** at the beam spot **6013-1** thereby passing through the horizontal multiplexing mirror **6003**.

In one embodiment, the multi-pass optical amplifier **6000** may be configured with another optical element or combination of optical elements (illustrated as optical element **6015**) that is operable to assist in the exit of any remaining optical energy in the pump beam **6013**. For example, the optical element **6015** may be a birefringent optic that alters the phase of the pump beam **6013**. Thus, upon exiting the multi-pass optical amplifier **6000**, the remaining optical energy in the pump beam **6013** reflects off the optical element **6015** in some desired manner so as to not interfere with the incoming pump beam **6013**. Alternatively or additionally, the optical element **6015** may be used to impart certain focusing effects on the pump beam **6013** and/or the signal beam **6012** so as to assist in maintaining desired beam widths. For example, FIG. **55** shows the beam spots of the pump beam **6013** at locations on the OAPs **6008**, **6009**, and **6010** (illustrated as filled circles) that do not coincide with the beam spots of the signal beam **6012** (illustrated as circles). The optical element **6015** may focus the signal beam **6012** in the pump beam **6013** to ensure that the beam widths of each do not overlap one another on the OAPs.

Although described with the thin disk gain medium being configured with the gain module **6004**, the invention is not intended to be so limited. As described above, the thin disk gain medium may be configured on the gain module **6004** and/or disposed on the reflective elements **6007**. In some embodiments, the gain module **6004** may have a gain medium that is different from the gain medium disposed on the reflective element **6007** so as to alter the intensity profile of the laser pulses. Additionally, the terms elevations and beam spot columns may be used herein interchangeably as such is generally relevant to the physical configuration of the multi-pass optical amplifiers disclosed herein. For example, the term “elevation” as it relates to FIGS. **49 A-C** and **50** describes the propagation of the laser energy as a set of beam spots that is generally aligned to a particular horizontal location on an OAP based in part on the tilt of the thin disk gain medium/reflective element **5706**. The term “column” as it relates to FIGS. **53-55**, on the other hand, describes the propagation of the laser energy as a set of beam spots that is vertically aligned at a particular location based in part on the tilt of the gain module **6004** and/or the reflective element **6007**. Although the two multi-pass optical amplifiers of these figures (i.e., **5700** and **6000**) operate in different manners, changes in their physical configurations may lead to the terms elevations and column being interchanged.

FIG. **56** is a block diagram of a laser system **6050** that is operable to fire a burst of laser pulses **6055** or otherwise increase the pulse repetition frequency (PRF) thereof. For example, the laser system **6050** may receive a laser pulse **6056**, generate a copy of that laser pulse such that two laser pulses then exist, and delay one of those laser pulses at an output of the laser system **6050**. Thus, when viewed at the output of the laser system **6050**, the two laser pulses appear with a PRF based on the delay between the two laser pulses.

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If that delay happens to be the pulse width (PW) of the laser pulse, then the pulses appear as a group with a PRF of $1/PW$. This copying of the laser pulses is implemented in the laser system **6050** via the replicator **6051**.

Since the copying of the laser pulses by the replicator **6051** generally includes the removal of optical energy from an original laser pulse, the laser system **6050** includes an optical amplifier **6053** that is operable to amplify the laser pulses (both copied and original) via multiple passes of the laser pulses through a gain medium within the optical amplifier **6053**. For example, the optical amplifier **6053** may be a multi-pass optical amplifier as disclosed herein or some other multi-pass optical amplifier, such as a regenerative amplifier. One example of a regenerative amplifier includes commonly owned U.S. Pat. No. 7,982,947 (issued Jul. 19, 2011), the contents of which are hereby incorporated by reference.

The replicator **6051** is optically coupled to the optical amplifier to copy the laser pulse **6056** and input the copied laser pulse to the optical amplifier **6053** for amplification. For example, the replicator **6051** may receive an amplified laser pulse from the optical amplifier **6053** and copy the amplified laser pulse by removing a portion of the optical energy from the amplified laser pulse. The replicator **6051** forms the copied laser pulse with about the same pulse width and optical intensity profile of the amplified laser pulse, albeit with less optical intensity. The amplified laser pulse that is output from the replicator **6051** also has a lower optical intensity due to the removal of optical energy therefrom during the laser pulse copying.

The laser system **6050** may also be configured with an entry port **6052** and a recycler **6054**. The entry port **6050** may be a “pulse picker” similar to those disclosed herein and operable to select laser pulses at a user defined PRF or according to a desired modulation pattern. For example, the pulse picker may select pulses of a pulse train from a femtosecond or picosecond laser.

The recycler **6054** is operable to transfer laser pulses from the optical amplifier **6053** back through the optical amplifier **6053** for multiple amplifications prior to exiting the laser system **6050**. In one embodiment, the recycler **6054** is an optical switch, such as an electro-optic modulator or an acousto-optic modulator, that is operable to allow certain laser pulses to exit the laser system **6050** (e.g., those with a desired optical intensity) while returning other laser pulses to the optical amplifier **6050** for additional amplification.

To further illustrate the operation of the laser system **6050**, the following example is provided. The laser pulse **6056** is first fired to the laser system **6050** for entrance via the entry port **6052**. The laser pulse **6056** is amplified by the optical amplifier **6053** and then propagated to the recycler **6054**. The recycler **6054** propagates the amplified laser pulse to the replicator **6051**, which in turn splits off a portion of the amplified laser pulse **6056** to create two laser pulses, one of which is delayed from the other. Both of these laser pulses are then propagated to the optical amplifier **6053** for additional amplification. In the mean time, another laser pulse **6056** may be fired to the laser system **6050** for entrance via the entry port **6052**. Thus, three laser pulses are amplified by the optical amplifier **6053** and output to the recycler **6054**. The recycler **6054** may output these laser pulses as the burst of laser pulses **6055**.

With this continuous firing, recycling, copying, and amplification of laser pulses, bursts of laser pulses may be output from the recycler **6054** at relatively high PRFs, generally only limited by the pulse width of the laser pulse **6056**. For example, the laser system **6050** may be operable to generate bursts of pulses in the microwave region. That is, after many

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passes, a replicated pulse can be amplified until it reaches a magnitude approaching the primary/original pulse. However, during the multiple round trips through the optical amplifier 6053, the amplified delayed pulse can produce additional secondary pulses that are further delayed. If each subsequent pulse is delayed by 65 ps, the PRF is about 15 GHz (i.e., $\frac{1}{65}$ ps). In this regard, as original laser pulses and copied laser pulses are input to the optical amplifier 6053 for amplification, the amplified optical radiation exiting the recycler 6054 generally includes a burst of $n+1$ pulses after n traversals through the replicator 6051. Typically, however, only a fraction of those laser pulses approach the peak intensity of the original pulse, as illustrated with the burst of laser pulses 6055.

The burst of laser pulses 6055 may be used to create and/or re-excite plasma at a specific repetition rate so as to create microwave emissions with an enhanced spectrum at the burst repetition rate. The plasma may be created by the burst of optical pulses itself as it propagates through air or another medium, or as the burst of pulses 6055 is incident on a solid body (e.g., Laser Induced Breakdown Spectroscopy, or "LIBS"). The embodiments herein may also be operable to provide distal microwave emissions using a single signal laser source (i.e., without requiring an additional microwave energy source). For example, the laser pulse interaction may create microwave emissions from a plasma or when incident upon a material. In this regard, a laser beam may move electrons away from positively charged ions through radial pressure or ponderomotive forces, creating a space charge. After each laser pulse passes, relaxation of the induced dipoles correspond to broad band-width emissions in the microwave or terahertz regime. Other processes may also include non-linear optical rectification.

While the above figures illustrate distinct laser pulses, the laser system 6050 is not intended to be limited as such. For example, the laser system 6050 may also be configured to output laser pulses that overlap one another prior to temporal compression. They may then be stretched so as to provide a Chirped Pulse Amplifier laser, or "CPA" laser. Alternatively or additionally, smaller pulses may be used to clear out gain from the gain medium of the optical amplifier 6053. For example, multiple, spatially separate, optical paths may be passed through the same gain region of the optical amplifier 6053 to provide gain clearing via the smaller output pulses of the replicator 6051 (e.g., by sending the smaller pulses back through the optical amplifier 6053 along slightly different paths). By clearing out the residual gain, uniform signal amplitudes can be obtained.

FIGS. 57-59 are block diagrams of various replicators for use in the laser system of FIG. 56. In FIG. 57, the replicator 6051 is configured as a glass optical element where most of a laser pulse 6070 is transmitted as the laser pulse 6071. A slight portion of the incident beam reflects from one surface of the replicator 6051 to the other surface of the replicator 6051. That portion of the beam then transmits through the replicator 6051 as a smaller amplitude laser pulse 6072 thereby creating a delay between the two pulses. This delay is essentially the time it takes for the split off the portion of the beam to pass through the replicator 6051 along the reflection path 6080. In FIG. 58, the opposite occurs. That is, the replicator 6051 in FIG. 58 may be configured as a glass optical element that splits off a smaller portion of the incoming laser pulse 6070 as it is incident upon the replicator 6051 via reflection as the laser pulse 6072. The larger remainder of the laser pulse continues to propagate to the other side of the replicator 6051 for reflection back through the replicator 6051 as the laser pulse 6071. The delay in this instance is

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based on the duration that it takes for the laser pulse 6071 to propagate through the replicator 6051 along the path 6090.

FIG. 59 illustrates a replicator 6051 that may be implemented with a piezoelectric structure 6095 that allows for the modulation of the delay between the two laser pulses 6071 and 6072. For example, two optical elements 6096 and 6097 may be "sandwiched" about the piezoelectric electric structure 6095 (e.g., a ring) the optical element 6096 splits off a portion of the incoming laser pulse 6070 by allowing it to pass through the optical element 6096 and reflecting a smaller portion of that laser pulse 6070 off the back side of the optical element 6096 as the laser pulse 6072. The remaining portion of the laser pulse 6070 passes through the region 6098 between the two optical elements 6096 and 6097 (e.g., air) for reflection off the optical element 6097 back through the optical element 6096 as the laser pulse 6071. The delay that is introduced between the two laser pulses 6071 and 6072 is the time it takes for the laser pulse 6071 to propagate through the region 6098 along the path 6099. To change this delay, a control signal may be applied to the piezoelectric structure to alter the distance that the laser pulse 6071 travels through the region 6098. For example, by controllably shrinking the width between the two optical elements 6096 and 6097, the delay between the two laser pulses 6071 and 6072 may be decreased, and vice versa. Thus, a controller as described herein may be configured to modulate the PRF of the burst of laser pulses 6055 that are output from the laser system 6050.

While the invention has been illustrated and described in detail in the drawings and foregoing description, such illustration and description is to be considered as exemplary and not restrictive in character. Certain embodiments described hereinabove may be combinable with other described embodiments and/or arranged in other ways. Accordingly, it should be understood that only the preferred embodiment and variants thereof have been shown and described and that all changes and modifications that come within the spirit of the invention are desired to be protected.

What is claimed is:

1. A laser system, including:

an optical amplifier that includes a gain medium operable to amplify a laser pulse via multiple passes of the laser pulse through the gain medium; and

a replicator optically coupled to the optical amplifier and operable to remove a portion of optical energy from the laser pulse to generate a copy of the laser pulse for input to the optical amplifier,

wherein the optical amplifier includes:

first, second, and third parabolic mirrors; and

a multiplexer operable to direct the laser pulse along multiple paths in or about a first plane between the first and second parabolic mirrors and to direct the laser pulse along multiple paths in or about a second plane to the third parabolic mirror to cause multiple incidents of the laser pulse on the gain medium to amplify the laser pulse,

wherein the first and second planes are different.

2. The laser system of claim 1, wherein the optical amplifier is further operable to amplify the copied laser pulse.

3. The laser system of claim 2, wherein the replicator is further operable to remove a portion of optical energy from the amplified copied laser pulse to generate another copy of the laser pulse, and wherein the laser system further includes an output that is operable to combine the laser pulses as a burst of laser pulses.

4. The laser system of claim 3, wherein the output is further operable to separate the laser pulses in the burst to provide a pulse repetition frequency in the megahertz range.

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5. The laser system of claim 1, wherein the replicator is further operable to delay the input of the copied laser pulse into the optical amplifier to clear gain from the gain medium prior to a return pass of the original laser pulse through the gain medium.

6. The laser system of claim 1, further including a recycler optically coupled to the optical amplifier and operable to selectively output a first set of laser pulses from the optical amplifier for transmission from the laser system and to selectively input a second set of laser pulses to the replicator for copying.

7. The laser system of claim 1, further including an entry port operable to select laser pulses at a user defined pulse repetition frequency for input to the optical amplifier.

8. The laser system of claim 1, wherein the optical amplifier includes:

a gain module, wherein the gain medium is configured within the gain module as a thin disk gain medium disposed on the first reflector, wherein the second reflector defines an optical cavity for the multi-pass optical amplifier.

9. The laser system of claim 1, wherein the replicator includes a piezoelectric device operable to controllably delay the copied laser pulse with respect to said laser pulse.

10. The laser system of claim 1, wherein the replicator includes a piezoelectric device operable to controllably delay said laser pulse with respect to the copied laser pulse.

11. The laser system of claim 1, wherein the replicator includes an optic operable to reflect the portion of the optical energy of the laser pulse at least twice to generate the copy of the laser pulse, transmit the remaining portion of the optical energy of the laser pulse, and transmit the copied laser pulse after transmitting the remaining portion of the optical energy of the laser pulse.

12. The laser system of claim 1, wherein the replicator includes an optic operable to reflect the portion of the optical energy of the laser pulse to generate the copy of the laser pulse, reflect the remaining portion of the optical energy of the laser pulse at least twice, and transmit the original laser pulse after transmitting the copied laser pulse.

13. A laser system, comprising:

an optical amplifier that includes a gain medium operable to amplify a laser pulse via multiple passes of the laser pulse through the gain medium; and

a replicator optically coupled to the optical amplifier and operable to remove a portion of optical energy from the laser pulse to generate a copy of the laser pulse for input to the optical amplifier,

wherein the optical amplifier includes:

a gain module, wherein the gain medium is configured within the gain module as a thin disk gain medium disposed on a first reflector;

a second reflector that defines an optical cavity for the multi-pass optical amplifier;

three parabolic reflectors positioned within the optical cavity, wherein a first of the three parabolic reflectors is

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smaller than a second and a third of the three parabolic reflectors for inputting the laser pulse into the multi-pass optical amplifier; and

a multiplexing reflector operable to change placement of incidence of the laser pulse within at least one pair of beam spot sets on the parabolic reflectors,

wherein the laser pulse loops through the multi-pass optical amplifier having incidence within a first of the at least one pair of beam spot sets on the first and second parabolic reflectors,

wherein the laser pulse reflects from the third parabolic reflector to the multiplexing reflector after completing a first loop through the multi-pass optical amplifier with incidence of the laser pulse within the first pair of beam spot sets on the first and second parabolic reflectors, and wherein the laser pulse reflects from the multiplexing reflector to the third parabolic reflector to initiate a second loop through the multi-pass optical amplifier with incidence of the laser pulse within at least one other beam spot set on the first and second parabolic reflectors that differs from the first pair of beam spot sets on the first and second parabolic reflectors.

14. The laser system of claim 13, wherein the optical amplifier is further operable to amplify the copied laser pulse, wherein the replicator is further operable to remove a portion of optical energy from the amplified copied laser pulse to generate another copy of the laser pulse, and wherein the laser system further includes an output that is operable to combine the laser pulses as a burst of laser pulses.

15. The laser system of claim 14, wherein the output is further operable to separate the laser pulses in the burst to provide a pulse repetition frequency in the megahertz range.

16. The laser system of claim 13, wherein the replicator is further operable to delay the input of the copied laser pulse into the optical amplifier to clear gain from the gain medium prior to a return pass of the laser pulse through the gain medium.

17. The laser system of claim 13, further including a recycler optically coupled to the optical amplifier and operable to selectively output a first set of laser pulses from the optical amplifier for transmission from the laser system and to selectively input a second set of laser pulses to the replicator for copying.

18. The laser system of claim 13, further including an entry port operable to select laser pulses at a user defined pulse repetition frequency for input to the optical amplifier.

19. The laser system of claim 13, wherein the replicator includes a piezoelectric device operable to controllably delay the copied laser pulse with respect to said laser pulse.

20. The laser system of claim 13, wherein the replicator includes a piezoelectric device operable to controllably delay said laser pulse with respect to the copied laser pulse.

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