

(19) World Intellectual Property Organization  
International Bureau



(43) International Publication Date  
3 September 2009 (03.09.2009)

(10) International Publication Number  
**WO 2009/108889 A2**

(51) International Patent Classification:  
**G01V 1/52** (2006.01) **E21B 47/12** (2006.01)  
**E21B 47/08** (2006.01)

77077 (US). **ACHANTA, Anjani, R.** [IN/US]; 2416 Yorktown #472, Houston, TX 77056 (US).

(21) International Application Number:  
PCT/US2009/035536

(74) Agents: **CARSON, Matt, W.** et al.; Baker Hughes Incorporated, P.O. Box 4740, Houston, TX 77210-4740 (US).

(22) International Filing Date:  
27 February 2009 (27.02.2009)

(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BR, BW, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RS, RU, SC, SD, SE, SG, SK, SL, SM, ST, SV, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:  
61/032,007 27 February 2008 (27.02.2008) US  
12/392,487 25 February 2009 (25.02.2009) US

(71) Applicant (for all designated States except US): **BAKER HUGHES INCORPORATED** [US/US]; P.O. Box 4740, Houston, TX 77210-4740 (US).

(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, SE, SI, SK, TR),

(72) Inventors; and  
(75) Inventors/Applicants (for US only): **STEINSIEK, Roger, R.** [US/US]; 3131 Summerwind Ct., Pearland, TX 77584 (US). **PATTERSON, Douglas, J.** [US/US]; 8219 Northbridge Drive, Spring, TX 77379 (US). **REDDING, Charles, E.** [US/US]; 1228 Martin Road, Houston, TX

[Continued on next page]

(54) Title: COMPOSITE TRANSDUCER FOR DOWNHOLE ULTRASONIC IMAGING AND CALIPER MEASUREMENT

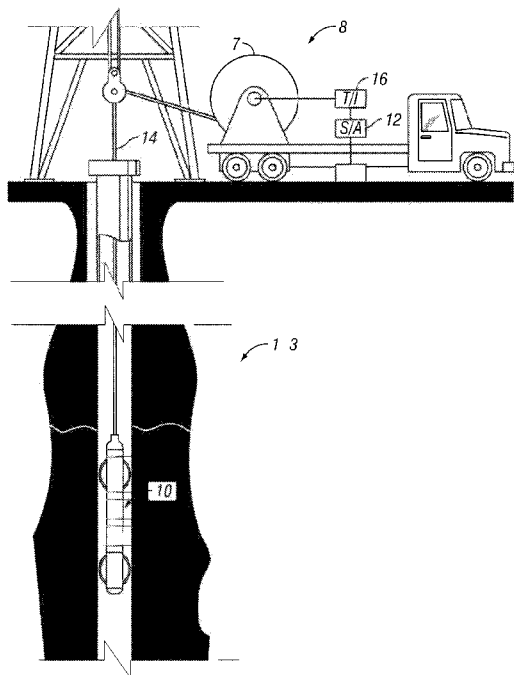


FIG. 1

(57) Abstract: A transducer assembly for downhole imaging includes a 1 -3 Piezoelectric composite transducer of high Q ceramic rods in a polymer matrix. The assembly also includes a Teflon® window, a fluid-filled cavity adjacent to the window, and impedance matching material between the composite transducer and the fluid. The transducer is positioned to reduce the reverberation time.

WO 2009/108889 A2



OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML,  
MR, NE, SN, TD, TG).

— *as to the applicant's entitlement to claim the priority of  
the earlier application (Rule 4.17(iii))*

**Declarations under Rule 4.17:**

— *as to applicant's entitlement to apply for and be granted  
a patent (Rule 4.17(ii))*

**Published:**

— *without international search report and to be republished  
upon receipt of that report (Rule 48.2(g))*

## COMPOSITE TRANSDUCER FOR DOWNHOLE ULTRASONIC IMAGING AND CALIPER MEASUREMENT

**Inventors:** STEINSIEK, Roger R., PATTERSON, Douglas J.,  
REDDING, Charles E.

### FIELD OF THE PRESENT DISCLOSURE

[0001] A downhole acoustic logging tool is provided for imaging the texture and structure of the borehole sidewall. The level of the acoustic signals reflected from the wall is enhanced by using a composite transducer in a borehole with highly attenuating borehole fluids.

### BACKGROUND OF THE PRESENT DISCLOSURE

[0002] Typical acoustic logging tools may include, by way of example, a circumferential televiewer which comprises a rotating ultrasonic acoustic transducer that operates in a frequency range on the order of 100 kHz or more. Higher acoustic frequencies are preferred in order to achieve better resolution in the confined space of a borehole. In operation, the televiewer rotates at a desired rate such as 5 to 16 rotations per second to continuously scan the borehole sidewall as the televiewer is drawn up the borehole at a rate that is typically 3/16 to 3/8 inch per scan. A beam of acoustic pulses is launched along the normal to the borehole sidewall as the transducer scans the interior surface of the borehole. The pulse rate depends upon the desired spatial resolution such as 1500 pulses per second or 128 to 256 pulses per scan. The insonified borehole sidewall returns pulses reflected therefrom, back to the transducer on a time-multiplexed basis. The reflected acoustic signals are detected, amplified and displayed to provide a continuous picture of the texture and structure of the borehole sidewall. Other application include determination of the goodness of a cement bond to a steel casing as well as monitoring the integrity of the casing itself.

[0003] The diameter of a borehole logger is on the order of 2<sup>7</sup>/<sub>8</sub> in (7.3 cm), so that it can be run into relatively small boreholes. However many borehole diameters are on the order of 10 – 14” (25.4- 35.6cm) or more such that the length of the acoustic-pulse trajectory from the transducer, through the borehole fluid to the borehole sidewall, may be up to 10” (25.4 cm). In the normal course of events, the borehole

fluid is contaminated by drill cuttings, air bubbles and foreign matter which severely attenuate the acoustic energy by scattering because the physical dimensions of the contaminants are comparable to the wavelength of the wavefields emitted by the transducer.

- 5 [0004] What is even more troublesome, however, is the complication that the acoustic attenuation coefficient in certain types of drilling fluid such as heavily-weighted oil-based muds is very high, on the order of 5 dB/cm. Since the reflected acoustic signals must propagate over a two-way travel path, the maximum path length through the highly-attenuating drilling fluid should normally be kept well  
10 under 4 cm. Even that short path length may result in an attenuation of 20 dB. Although it is true that the coefficient of attenuation diminishes with decreasing acoustic frequency, space considerations and resolution requirements do not permit the use of large, low-frequency transducers. US Patent No. 5,541,889 to *Priest* having the same assignee as the present disclosure teaches an apparatus in which  
15 televiewer signals from a rotary sidewall acoustic-beam scanner is improved by replacing the volume of borehole drill fluid that lies in the path of the acoustic beam with a solid medium characterized by a lower coefficient of attenuation than that of the drill fluid. A mud excluder assembly is used for the purpose. The excluder assembly includes a solid shroud of polymethylacrylate, polycarbonate  
20 polymethylflouroethylene, polyphenylsulfide or polymethylpentane or any other solid medium that has an acceptably low coefficient of acoustic attenuation. An added constraint of the shroud is that its acoustic impedance should match as closely as possible the acoustic impedance of the fluid inside the enclosure as well as the fluid bathing the exterior of the shroud.
- 25 [0005] It would be desirable to have an apparatus and method with a simpler structure that is able to make acoustic measurements of a borehole wall when the borehole includes a highly attenuating fluid. The present disclosure addresses this need.

#### SUMMARY OF THE PRESENT DISCLOSURE

- 30 [0006] One embodiment of the disclosure is an apparatus configured to evaluate an earth formation. The apparatus includes a rotatable transducer assembly, a

composite transducer on the rotatable transducer assembly configured to propagate an acoustic signal through an acoustically transparent window into a borehole and receive a reflection from a wall of the borehole, and at least one processor configured to use the reflection obtained at a plurality of orientations of the transducer during rotation of the transducer assembly to provide an image of the earth formation.

[0007] Another embodiment of the disclosure is a method of evaluating an earth formation. The method includes conveying a rotatable transducer assembly into a borehole, using a composite transducer on the rotatable transducer assembly configured to propagate an acoustic signal through an acoustically transparent window into the borehole and receive a reflection from a wall of the borehole, and using the reflection obtained at a plurality of orientations of the transducer during rotation of the transducer assembly to provide an image of the earth formation.

[0008] Another embodiment of the present disclosure is a computer-readable medium accessible to at least one processor, the computer-readable medium including instructions which enable the at least one processor to use a reflected signal from a borehole wall resulting from generation of an acoustic signal by a composite transducer on a rotatable transducer assembly in the borehole and transmission of the generated acoustic signal through an acoustically transparent window on the transducer assembly into the borehole.

#### **BRIEF DESCRIPTION OF THE DRAWINGS**

[0009] The present disclosure is best understood with reference to the accompanying figures in which like numerals refer to like elements and in which:

**FIG. 1** shows an imaging well logging instrument disposed in a wellbore drilled through earth formations.

**FIG. 2A** shows the rotator assembly;

**FIG. 2B** shows the transducer assembly;

**FIGS. 3A** and **3B** show some details of the transducer assembly;

**FIG. 4** shows the structure of the transducer;

**FIGS. 5A, 5B, and 5C** illustrate how the composite transducer of **FIG. 4** may be built;

**FIG. 6** illustrates a cross-section of the transducer assembly; and  
**FIGS. 7A** and **7B** illustrate exemplary signals for two different distances of the transducer from the Teflon window.

#### DETAILED DESCRIPTION OF ILLUSTRATIVE EMBODIMENTS

5 [0010] Referring to **FIG. 1**, a well logging instrument **10** is shown being lowered into a wellbore **2** penetrating earth formations **13**. The instrument **10** can be lowered into the wellbore **2** and withdrawn therefrom by an armored electrical cable **14**. The cable **14** can be spooled by a winch **7** or similar device known in the art. The cable **14** is electrically connected to a surface recording system **8** of a type  
10 known in the art which can include a signal decoding and interpretation unit **16** and a recording unit **12**. Signals transmitted by the logging instrument **10** along the cable **14** can be decoded, interpreted, recorded and processed by the respective units in the surface system **8**.

[0011] **FIG. 2A** shows mandrel section **201** of the imager instrument with a  
15 Teflon® window **203**. Shown in **FIG. 2B** is the rotating platform **205** with the ultrasonic transducer assembly **209**. The rotating platform is also provided with a magnetometer **211** to make measurements of the orientation of the platform and the ultrasonic transducer. The platform is provided with coils **207** that are the secondary coils of a transformer that are used for communicating signals from the  
20 transducer and the magnetometer to the non-rotating part of the tool. The transducer **209** is discussed further below.

[0012] **FIG. 3A** shows the transducer assembly while **FIG. 3B** shows some details of the transducer assembly. This includes the actual transducer **301**, the backing **303**, and a polymer material **305**. The transducer is mounted in a brass frame  
25 indicated by **307**.

[0013] **FIG. 4** shows an exemplary transducer. The transducer is a composite transducer that includes a plurality of Piezoelectric transducer (PZT) rods **401** set in a polymer matrix **403**. The PZT rods may be made of ceramic with a high quality factor (Q). As discussed by *Fleury et al*:

30 The properties of these materials imply a certain number of specific characteristics as: - acoustical impedance : located between the one of the

polymer material and the one of the ceramic material. In practice, it is adjusted between 8 and 12 MRayleigh, which allows a good transfer of energy in a large frequency band when the impedance of the coupling medium is low, which is always the case for immersion testing.

- 5
- ***coupling coefficient*** : its high value also contributes to the increase of energy transfer and to the widening of the bandwidth. These materials, thanks to the double effect of a low acoustical impedance and a high coupling coefficient, make possible a quite important improvement of the ratio sensitivity/bandwidth compared to the
- 10
- ***electrical impedance*** : the judicious choice of the constituents and their respective proportions allow to adjust the electrical impedance and to favour, in that way, the matching of the transducer to its electrical environment.
- 15
- ***shaping*** : it is linked to the thermal and mechanical properties of the polymer phase.
  - ***lateral modes*** : they are strongly attenuated with this type of material and associated parasitic effects are consequently reduced.
  - ***cross coupling*** : this parameter is very important for the design of
- 20
- multielements transducers. The anisotropy of these materials on the mechanical, dielectrical and piezo-electric aspects allows, thanks to a simple deposit of electrodes having the required geometry, to surround the active zones which have a low interaction with the adjacent zones.
- 25
- In the context of the present disclosure, the strong attenuation of the lateral modes and the lack of cross-coupling enables the use of PZT rods that have a higher Q than with prior art transducers. As would be known to those versed in the art, traveltime measurements commonly rely on picking of first arrivals, and attenuation estimates are based on measuring the frequency dispersion of signals. The high Q
- 30
- PZT generate much greater transmission and reception amplitudes than the low Q

prior art transducers. The higher amplitudes extend the operating range of the instrument in heavily attenuating borehole fluids.

[0014] FIGS. 5A-5C schematically show how the composite transducer of FIG. 4 may be constructed. FIG. 5A shows a solid block of a PZT that has been diced to remove portions of the PZT while still retaining its integral structure. The removed portions are infilled with polymer (FIG. 5B). Finally, the base of the PZT structure is removed, leaving behind a plurality of PZT rods in a polymer matrix (FIG. 5C). It is possible to have the rods arranged in any geometric configuration, though the simple geometry shown is the easiest to fabricate.

10 [0015] Turning now to FIG. 6, a cross section of a transducer assembly is shown. Depicted therein is the Teflon® window 601. One transducer is depicted by 607. The assembly may include a second transducer on the opposite side (not shown). The front portion of the transducer is in contact with an impedance matching material 605 that is used to match the impedance of the transducer with that of oil in the space 605 between the transducer and the Teflon® window. It should be noted that the use of Teflon® is not to be construed as a limitation and any other material with the necessary abrasion resistance and acoustic properties could be used.

[0016] Still referring to FIG. 6, the transducer assembly also includes a backing material 609. In one embodiment, the backing material is a 0-3 composite of tungsten particles in high temperature rubber. In another embodiment, liquid Viton®  
20 ®, a synthetic rubber may be used. The backing material absorbs acoustic signals propagating from the transducer away from the borehole wall and reduces reflections from the interface between the transducer and the backing material. Also shown in FIG. 6 are the leads 611 from the transducer that go to transformer coils 207.

[0017] An important aspect of the disclosure is the reduction of reverberations within the transducer assembly, specifically between the transducer and the Teflon® window. FIG. 7A shows an exemplary signal recorded with a relatively longer spacing between the transducer and window. For this particular spacing, the reverberation time was approximately 75  $\mu$ s. As a result of this, reverberations can still be seen, as indicated by 701. The signal 703 is the desired reflection from the  
30

borehole wall. The distance between transducer and the window may be adjustable. One advantage of having the adjustable distance is to reduce the reverberations. Shown in **FIG. 7B** is a signal recorded with a short of spacing (6.8 mm) between the transducer and window. The reverberation time is reduced to 42  $\mu$ s.

- 5 Consequently, at the time **705** corresponding to **701** in **FIG. 7A**, the reverberations have decayed significantly in **FIG. 7B** compared to **FIG. 7A**. Another advantage of having the distance adjustable is to provide improved acoustic transmission. Specifically, by having the distance substantially equal to a quarter wavelength to provide improved energy transfer between the oil in the cavity and the Teflon<sup>®</sup>
- 10 window. The Teflon<sup>®</sup> window also has an advantage over alternate designs in which the window is not used but the rotating transducer is exposed to abrasive and highly viscous borehole fluids that can interfere with rotation of the transducer.
- [0018] Once the data have been acquired, standard processing methods are used to provide an image of the borehole wall. This image may be based on the reflectance
- 15 amplitude or on the travel time. See, for example, U.S. Patent No. 5,502,686 to *Dory et al.*, having the same assignee as the present disclosure.
- [0019] The processing of the data may be done by a downhole processor and/or a surface processor to give corrected measurements substantially in real time. Implicit
- 20 in the control and processing of the data is the use of a computer program on a suitable machine readable medium that enables the processor to perform the control and processing. The machine readable medium may include ROMs, EPROMs, EEPROMs, Flash Memories and Optical disks. Such media may also be used to store results of the processing discussed above.

**CLAIMS**

What is claimed is:

- 1 1. An apparatus configured to evaluate an earth formation, the apparatus  
2 comprising:  
3 a rotatable transducer assembly;  
4 a composite transducer on the rotatable transducer assembly  
5 configured to propagate an acoustic signal through an acoustically  
6 transparent window into a borehole and receive a reflection from a wall of  
7 the borehole; and  
8 at least one processor configured to use the reflection obtained at a  
9 plurality of orientations of the transducer during rotation of the transducer  
10 assembly to provide an image of the earth formation.
- 1 2. The apparatus of claim 1 wherein the composite transducer further  
2 comprises piezoelectric transducer (PZT) rods in a polymer matrix.
- 1 3. The apparatus of claim 1 wherein the rotatable transducer assembly further  
2 comprises:  
3 (i) a fluid in a cavity adjacent to the acoustically transparent window,  
4 and  
5 (ii) an impedance matching material disposed between the composite  
6 transducer and the fluid.
- 1 4. The apparatus of claim 1 wherein a distance between the composite  
2 transducer and the acoustically transparent window is selected to at least one  
3 of: (i) reduce a reverberation time of a reverberation therebetween, and (ii)  
4 improve acoustic coupling with the acoustically transparent window.
- 1 5. The apparatus of claim 1 further comprising a backing material on a side of  
2 the transducer opposite to the acoustically transparent window configured  
3 to absorb acoustic signals.
- 1 6. The apparatus of claim 1 wherein the image produced by the at least one  
2 processor is selected from: (i) a traveltime image, and (ii) a reflectance  
3 image.

- 1 7. The apparatus of claim 1 wherein the rotatable transducer assembly is part  
2 of a logging string conveyed into the borehole on a wireline.
- 1 8. The apparatus of claim 1 wherein the PZT further comprises a ceramic  
2 having a high quality factor.
- 1 9. A method of evaluating an earth formation, the method comprising:  
2 conveying a rotatable transducer assembly into a borehole;  
3 using a composite transducer on the rotatable transducer assembly  
4 configured to propagate an acoustic signal through an acoustically  
5 transparent window into the borehole and receive a reflection from a wall of  
6 the borehole; and  
7 using the reflection obtained at a plurality of orientations of the  
8 transducer during rotation of the transducer assembly to provide an image of  
9 the earth formation.
- 1 10. The method of claim 9 further comprising using, as the composite  
2 transducer,  
3 a piezoelectric transducer (PZT) rods in a polymer matrix.
- 1 11. The method of claim 9 further providing in the transducer assembly:  
2 (i) a fluid in a cavity adjacent to the acoustically transparent window,  
3 and  
4 (ii) an impedance matching material disposed between the composite  
5 transducer and the fluid.
- 1 12. The method of claim 9 further comprising selecting a distance between the  
2 composite transducer and the acoustically transparent window to at least one  
3 of: (i) reduce a reverberation time of a reverberation therebetween, and (ii)  
4 improve acoustic coupling with the acoustically transparent window.
- 1 13. The method of claim 9 further comprising providing a backing material on a  
2 side of the transducer opposite to the acoustically transparent window  
3 configured to absorb acoustic signals.
- 1 14. The method of claim 9 wherein the produced image produced is selected  
2 from: (i) a traveltime image, and (ii) a reflectance image.

- 1 15. The method of claim 1 further comprising conveying the rotatable  
2 transducer into the borehole on a wireline.
- 1 16. The method of claim 1 further comprising using for the PZT a ceramic  
2 having a high quality factor.
- 1 17. A computer-readable medium accessible to at least one processor, the  
2 computer-readable medium including instructions which enable the at least  
3 one processor to use a reflected signal from a borehole wall resulting from  
4 generation of an acoustic signal by a composite transducer on a rotatable  
5 transducer assembly in the borehole and transmission of the generated  
6 acoustic signal through an acoustically transparent window on the  
7 transducer assembly into the borehole.
- 1 18. The computer-readable medium of claim 17 further comprising at least one  
2 of: (i) a ROM, (ii) an EPROM, (iii) an EEPROM, (iv) a flash memory, and  
3 (v) an optical disk.

1/6

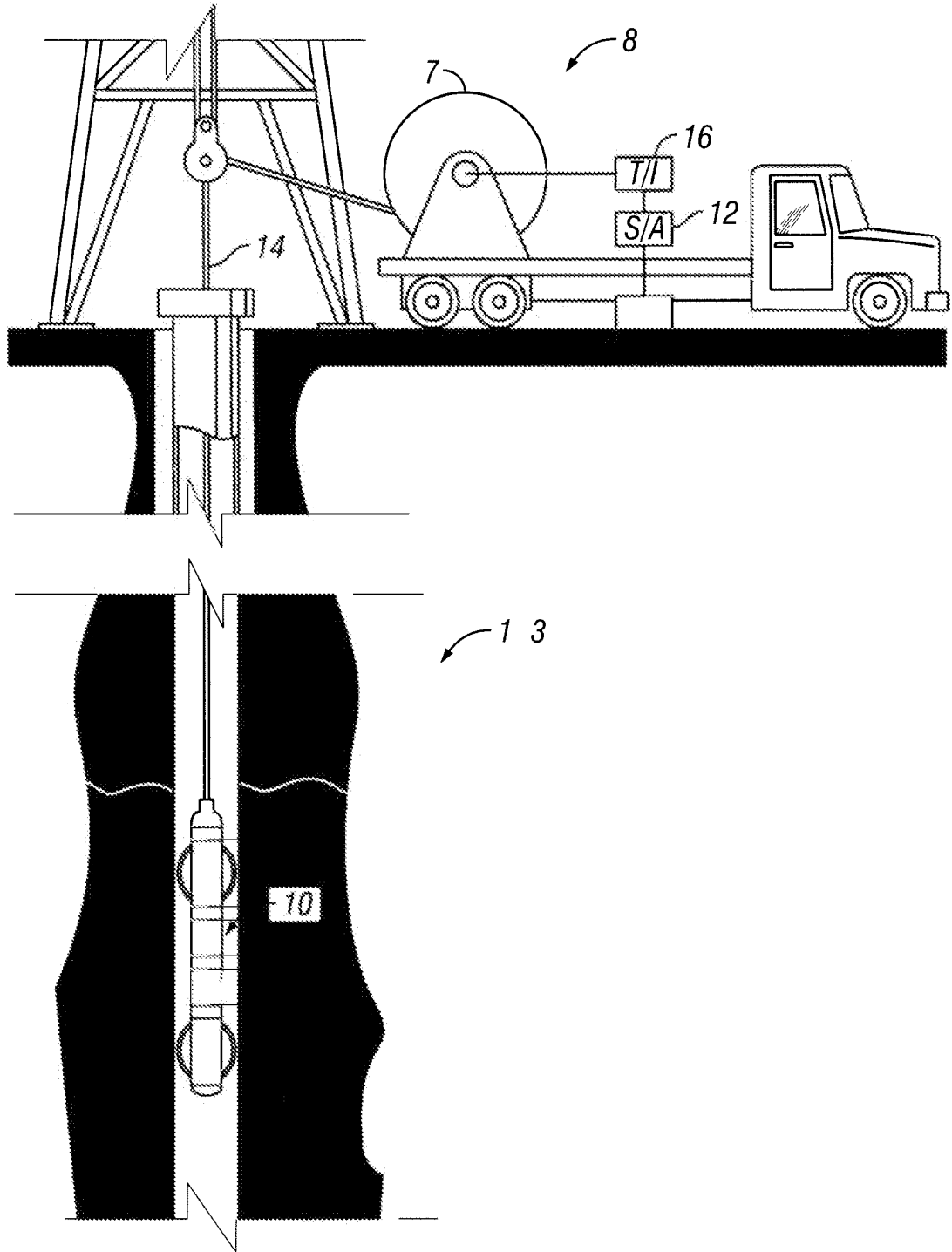


FIG. 1

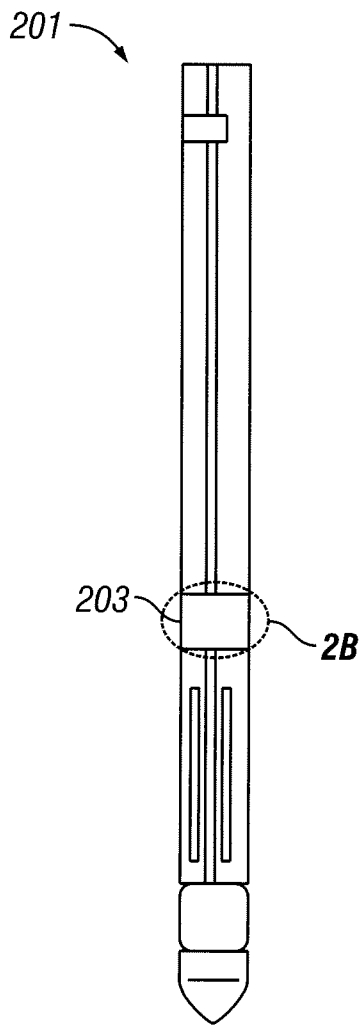


FIG. 2A

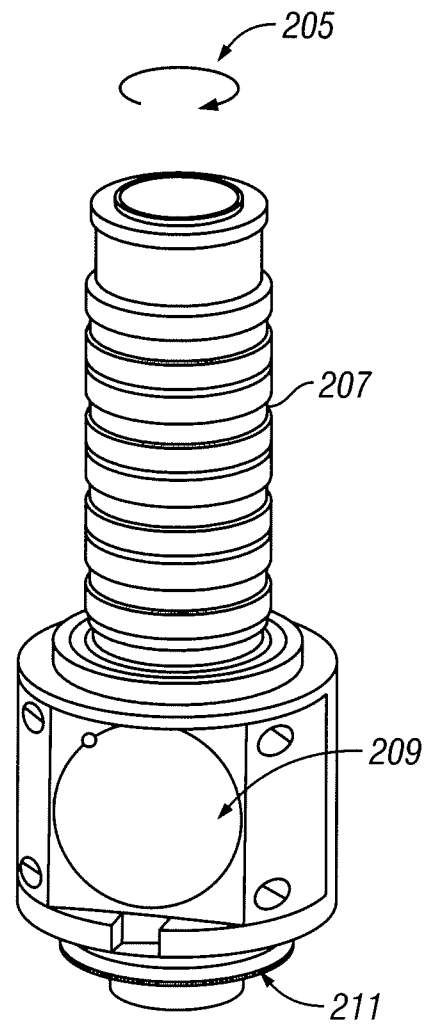


FIG. 2B

3/6

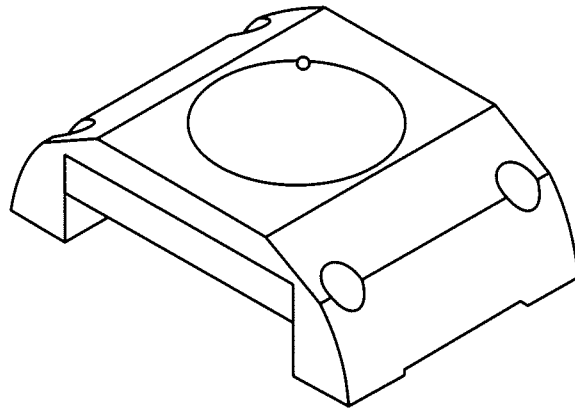


FIG. 3A

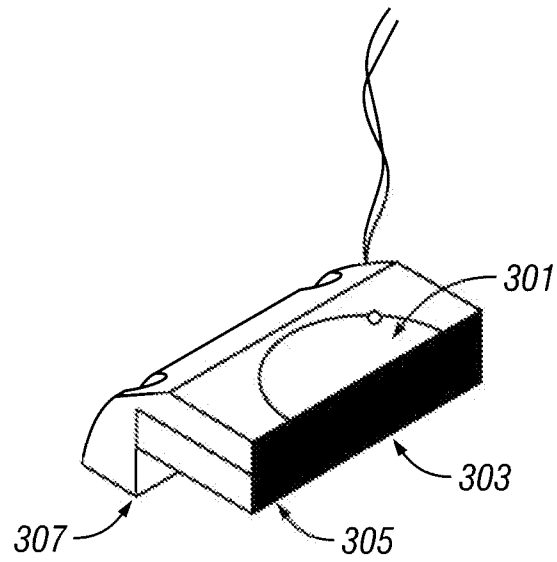


FIG. 3B

4/6

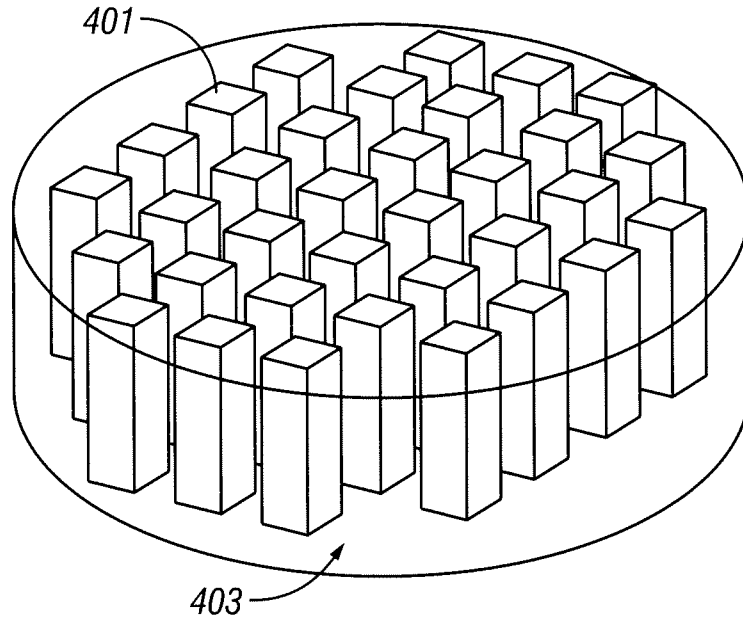


FIG. 4

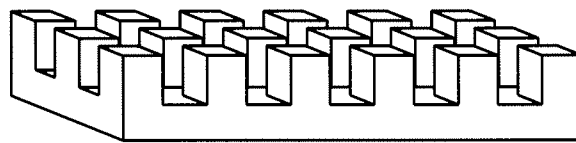


FIG. 5A

DICED PZT

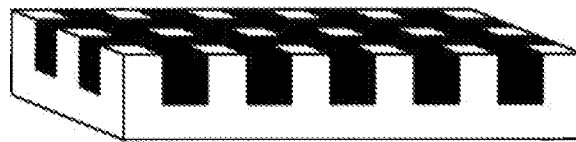


FIG. 5B

EPOXY FILLED PZT



FIG. 5C

PIEZO-COMPOSITE ELEMENT

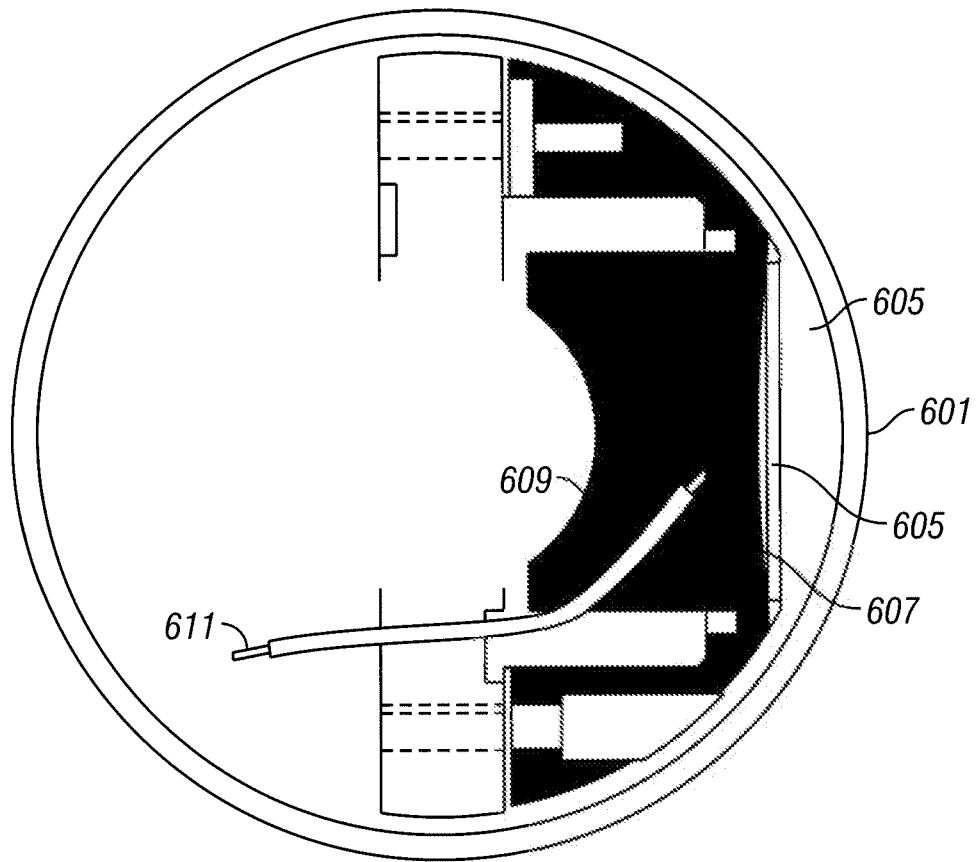


FIG. 6

6/6

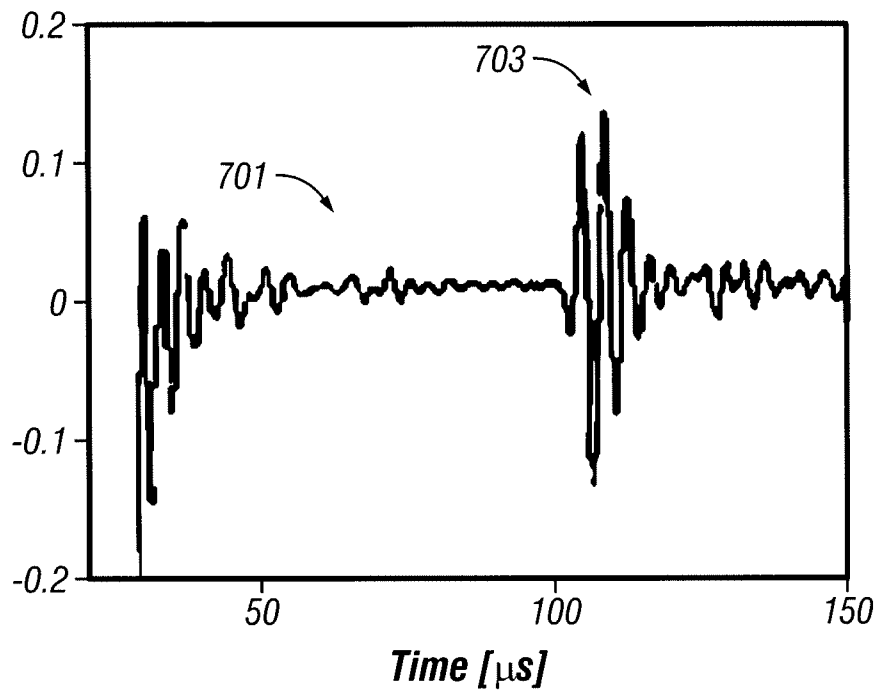


FIG. 7A

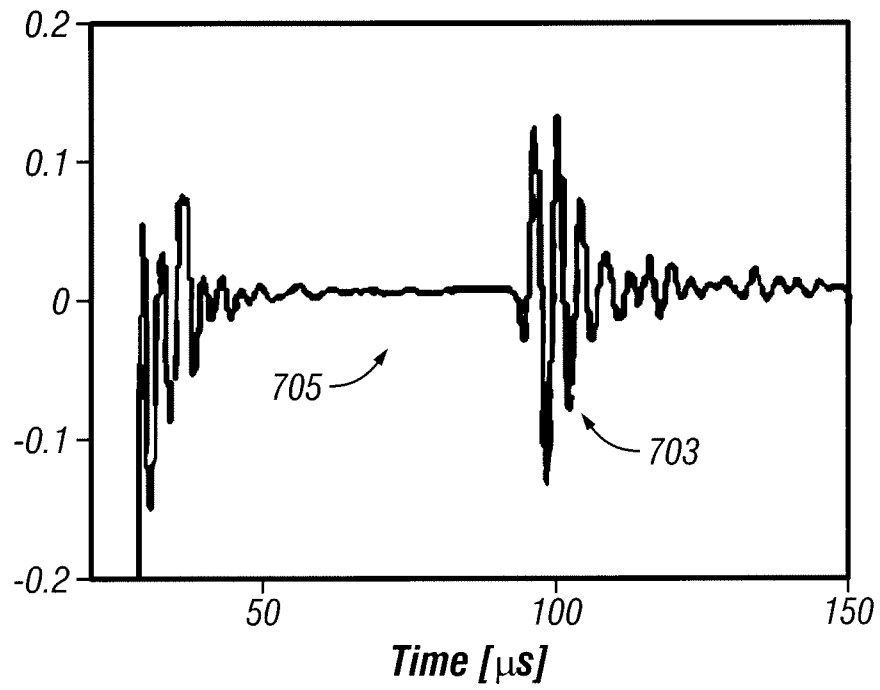


FIG. 7B