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INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification 6:
H01Q 19/00, 19/28

A1
(11) International Publication Number: WO 98/44591
(43) International Publication Date: 8 October 1998 (08.10.98)

(21) International Application Number: PCT/US98/06349

(22) International Filing Date: 31 March 1998 (31.03.98)

(30) Priority Data:

08/828,579

31 March 1997 (31.03.97) US

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(81) Designated States: European patent (AT, BE, CH, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).

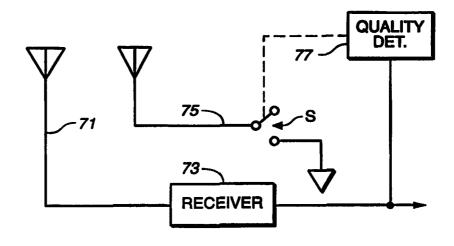
Published

With international search report.

(54) Title: ADJUSTABLE ARRAY ANTENNA

(57) Abstract

A passive reflective antenna (75) located near an active receiving antenna (71) is used to change the energy at the receiving antenna (71). The change in energy may be such as to remove a null created by multipath or to provide directionality, or both. The receiving antenna (71) is permanently connected to a single receiver When the receiver's output signal degrades below an acceptable level of quality, the reflective phase of the passive antenna's load is changed to change the phase of the reflected energy and



achieve a desired effect (remove a null, change directionality, etc.) at the receiving antenna (71). In the simplest embodiment, the termination of the passive antenna (75) is switched from an open circuit to a short circuit, or vice versa, to invert the phase of the reflected energy.

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ADJUSTABLE ARRAY ANTENNA

BACKGROUND OF THE INVENTION

Field of the Invention

The present invention relates to array antennae for communications systems, 5 particularly RF microcell personal communications systems.

State of the Art

Wireless personal communications systems are known as exemplified by published International Application WO 96-41498 entitled Hearing Aid With Wireless Remote Processor, incorporated herein by reference. As described therein, a hearing aid system consists of an earpiece that can be hidden in the ear canal, and which communicates wirelessly with a remote processor unit (RPU). The RPU may be a belt pack, wallet or purse-based unit. Sounds from the environment are picked up by a microphone in the earpiece and sent with other information over a primary two-way wireless link to the RPU, where the audio signals are enhanced according to the user's needs. Signal processing is performed in the RPU rather than the earpiece to take advantage of relaxed size and power constraints. The enhanced audio signals may be combined with other information and transmitted from the RPU over the primary wireless link to the earpiece, where they are converted by a speaker to sounds that can only be heard by the user.

In an exemplary embodiment, communications between the RPU and the earpiece follow an interrogate/reply cycle. The reply portion of the primary wireless link (from the earpiece to the RPU) may use a reflective backscatter technique in which the RPU radiates a carrier signal and the earpiece uses a switch to change between a high backscatter antenna state and a low backscatter antenna state. An additional, optional secondary two-way wireless link can be used for communication between the RPU and a cellular telephone system or other source of

information. Furthermore, an RPU keyboard, or voice recognition capabilities in the RPU, can be used to control hearing aid parameters and telephone dialing functions. Two earpieces and an RPU can be used in a binaural wireless system that provides hearing protection and noise cancellation simultaneous with hearing aid 5 functions.

Although the system of WO 96-41498 arises out of the field of hearing health care, as may be appreciated from the foregoing description, the system is more broadly applicable to personal communications in general. Recently, attention has been drawn to the application of wireless personal communications systems to 10 telecommunications and computing. At "ACM97: The Next 50 Years of Computing", for example, the prediction was made that in the future, personal computers will be wrist-sized, accompanied by a pair of reading glasses that present high-resolution images at a comfortable distance. A small, fitted earpiece and a "finger mouse" will be linked to other devices with low-power radio signals. Such a 15 future is not far off.

One of the challenges presented in personal communications systems is to allow multiple such systems to function in close proximity to one another with no performance degradation (or graceful degradation) due to interference. An unofficial benchmark developed by the present assignee to test for robustness of communications in the presence of interference has been the "ten-person hug." That is, ten persons each with a personal communications system of the type described should be able to form a group hug without experiencing significant performance degradation of their respective personal communications systems.

In a personal communications system as described, the RPU requires an antenna diversity system to mitigate against signal drop out due to signal nulls encountered in any real-world situation. Basically, the signal emanating from the earpiece antenna may reach the RPU's receiving antenna via numerous paths, due to

multiple reflections from environmental objects. These reflections result in "multipath" problems.

Classical antenna diversity systems employ more than one antenna and either a) when the signal quality is measured to be below a predetermined threshold, the 5 receiver input is switched to a different receiving antenna (with, hopefully, a better quality signal) or b) each antenna has its own receiver and the best quality received signal is utilized as the output signal. Any of various different measures of signal quality may be employed, such as signal strength, bit-error rate (BER), signal distortion, etc. Typically the antennae are spaced physically apart so that if one is in a null, the other or others are unlikely to also be in a null. A conventional diversity antenna system in accordance with the former technique is shown in Figure 1. A conventional diversity antenna system in accordance with the latter technique is shown in Figure 2.

In the first case a) active switching circuitry must be located in the antenna's signal path where signals are small and weak and subject to degradation by the switch. Furthermore, data transmission or reception must be interrupted periodically to perform a comparison of the signals received by the different antennae. Based on this comparison, one of the signals is selected. Such comparison, or "hunting," uses bandwidth that might otherwise be used for data transmission or reception. In the second case b) multiple receivers are required with the increase in size, weight, power, complexity, and, of course, cost.

In diversity antenna systems, multiple antennae function independently, usually without significant RF interaction. Apart from diversity antenna systems, directional antenna systems are also known. In directional antenna systems, also known as "beam steering" or "beam forming" antenna systems, the RF interaction between multiple antennae is controlled to realize the equivalent of a single antenna having a desired directionality. Directional antenna systems are most commonly

used in radar applications, but are also being increasingly used in cellular communications, for example.

In some instances, passive reflector elements have been used to generate directionality. Referring to Figure 3, for example, a linear antenna 31 forming a 5 driven element has positioned adjacent to it a thin reflector element 33. With respect to the driven element, the reflector dipole is shorted out to cause the reflection of energy and is mistuned to a lower frequency (by using a longer element) to provide a phase delay that compensates for the reflective-to-active-element spacing d, thereby causing maximum radiation in the desired direction.

10 Such a configuration is not adaptive and cannot be used to improve reception in a rapidly-changing RF environment.

A limited measure of adaptivity is attained using a conventional phased array antenna system of a type shown in Figure 4. Multiple antennae 41 are coupled together using transmission lines (l_1 -, l_2 , l_3). The transmission lines function as 15 delay lines, the lengths of the transmission lines being chosen to exhibit the desired delay. Two different sets of transmission lines are provided, the transmission lines in each set having length chosen appropriately to achieve a desired directionality. RF switches 43 are used to switch between the two different sets of transmissions lines. When the RF switches are in one state, for example, the antenna system 20 might be optimized for "broadside" reception. When the RF switches are in the other state, the system might be optimized for 45° reception. The limited degree of adaptivity of the system of Figure 4 comes at the expense of increased size and cost.

Other conventional phased array antenna systems are fully adaptive.

Referring to Figure 5, for example, multiple antenna elements 51 are each coupled to individual phase shifters 53 and antenuators 55, the outputs of which are coupled to a common line feed 57. Referring to Figure 6, a conventional phased array antenna system is shown using continuously adjustable RF phase shifters 61 and

separate receivers (63, 65) for each element. (The separate receivers are provided with a common frequency reference f_0 , element 64.) Using RF signal processing techniques, the signals from the two different elements (67, 69) can be summed (block 68) in any desired phase relationship.

None of the foregoing techniques is suitable for a compact, low-power, low-cost personal communications system. What is needed, then, is an antenna system that provides the benefits of known diversity and/or directional antenna systems but that is small, power efficient, and low-cost. The present invention addresses this need.

SUMMARY OF THE INVENTION

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A passive reflective antenna located near an active receiving antenna is used to change the energy at the receiving antenna. The change in energy may be such as to remove a null created by multipath or to provide directionality, or both. The receiving antenna is permanently connected to a single receiver. When the 15 receiver's output signal degrades below an acceptable level of quality, the reflective phase of the passive antenna's load is changed to change the phase of the reflected energy and achieve a desired effect (remove a null, change directionality, etc.) at the receiving antenna. In the simplest embodiment, the termination of the passive antenna is switched from an open circuit to a short circuit, or vice versa, to invert 20 the phase of the reflected energy.

The use of reflective elements in antenna designs, usually to achieve directionality, is well known (see the common Yagi or corner reflector antenna designs, for example), but these use passive reflector elements. The present invention, in contrast, employs active control of the reflective element. The term 25 "reflective element" is used to mean an element that re-radiates RF energy. The position of a reflective element relative to the active receiving antenna (whether the reflective element receives RF energy from a waveform and before or after the

active receiving antenna) is unimportant, so long as a portion of the re-radiated energy is picked up by the active receiving antenna and the phase with which the re-radiated energy is received is controllable. By actively controlling the load impedance, the phase of the reflected signal can be controlled, giving an added 5 measure of flexibility and usefulness. For example, a single, omni directional, active antenna surrounded by numerous passive reflective elements can be configured to produce a steered beam system where the reflective elements are the only elements to be controlled. Unlike other steered beam systems which are either mechanically steered or phased-array steered, the present method is more reliable, 10 simpler, less costly, smaller, and more power efficient.

BRIEF DESCRIPTION OF THE DRAWING

The present invention may be further understood from the following description in conjunction with the appended drawing. In the drawing:

Figure 1 through Figure 3 are block diagrams of conventional diversity antenna systems;

Figure 3 through Figure 6 are block diagrams of conventional directional antenna systems;

Figure 7 is a block diagram of a multiple-antenna diversity system in accordance with one embodiment of the present invention;

Figure 8a through 8g are block diagrams illustrating various means of creating controllable phase shifts of the reflected energy from a reflective antenna element;

Figure 9 is a block diagram of a multiple-antenna system in accordance with another embodiment of the invention;

Figure 10a is a diagram illustrating a plane wave being reflected from an array of reflective elements so as to focus reflected energy on an active element;

Figure 10b is a diagram like that of Figure 10a, illustrating how a change in the reflected phase can redirect the angle of greatest sensitivity for a reflective phased array.

Figure 11 is a representation of a multiple-antenna system in which one active element is placed in a field of phased reflectors;

Figure 12 is a diagram of a multiple-antenna system in which more than one active element is placed in a field of phased reflectors;

Figure 13 is a diagram illustrating the use of reflected energy from one or more reflective elements to fill in the null in a multipath situation; and

Figure 14 is a block diagram of a multiple antenna system in accordance with a further embodiment of the invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

- The present invention will be described with particular reference to a personal communications system of the type previously described. In such a system, receiver diversity at the RPU is a real-world requirement. Directionality may also be used to advantage in such a system to minimize interference and power consumption. Because of the bi-directional (fully reversible) nature of antennas, directionality in one mode (transmit or receive) may be continued during the other mode if desired. Although described in relation to a personal communications system, the present invention is applicable to RF systems generally, particularly to antenna systems for radar, cellular, PCS and wireless microphone systems, among others.
- Referring now to Figure 7, a block diagram is shown of a multiple-antenna system in accordance with one embodiment of the present invention. A primary antenna 71 is permanently connected to a receiver 73. A secondary, passive antenna 75 is positioned in proximity to the primary antenna 71. The secondary antenna 75 is terminated through a switch S to ground. A signal quality determination block 77 is coupled to an output of the receiver 73.

Depending on the quality of reception, the switch S is placed in the open state, as shown, or the closed state. That is, to achieve control, the reflective

element (secondary antenna 75) can simply be shorted or open-circuited to produce 0° or 180° phase switching.

Alternatively, an electronic load (not shown) which shifts the phase of the reflected energy by other angles can either be switched in or kept connected while 5 the reflected phase is controlled electronically. The reflected phase may be controlled continuously if desired, i.e., the resulting directionality or other desirable trait can be continuously, or smoothly, changed (steered) in an "analog" way, stopping wherever is desired, and moved when decided.

Modification of the phase of the reflected signal can be accomplished by

switching or continuous control. Switches can be electronic, mechanical, manual or
any other method (even thermal). The simplest method (Figure 7) involves using a
switch to either short or open the reflective element to produce a 180° shift in the
phase of the reflected signal. By switching between an open and a shorted
transmission line (delay line) the phase shift, instead of 180°, can be made any

value. By continuously controlling the phase shift of a permanently connected delay
line or phase shifter, the phase of the reflected signal can be controlled smoothly
and continuously or in steps.

The effect of a multiple-antenna system such as that of Figure 7 in a multipath situation is illustrated in Figure 13. The multiple-antenna system includes 20 a primary antenna 1302, a receiver 1301, a secondary, passive antenna 1303 terminated by a controllable load 1305 (such as a switch), and a control signal 1307. The receiver 1301 is assumed to incorporate means for determining the desired measure of signal quality and for producing the control signal 1307 in response to that measure.

In operation, multiple transmission paths can create spatial signal nulls at reception locations; for example the direct path and reflected path energy can sum at

the receive antenna 1302 so as to produce a local spatial null 1306. Changing the phase of a portion of the reflected energy from the reflective element (secondary antenna) can change the summed energy at the receiving antenna 1302 so as to fill in the null. More particularly, a signal of interest follows a direct path to the primary antenna 1302 and also follows one or more reflected paths. At the primary antenna 1302, the direct signal and the reflected signal interfere destructively, causing a local spatial null at the primary antenna 1302. The signal of interest follows a direct path to the secondary antenna 1303 and is wholly or partially reflected with the reflected wave having a phase determined by the controllable load 1305 in response 10 to the control signal 1307. The receiver adjusts the control signal 1307 to produce constructive interference between the reflected wave and the weak signal in the region of the local null to thereby increase the signal level.

Various means may be used to create different controllable phase shifts of the reflected energy from a reflective antenna as shown in Figure 8a through Figure 8g. Referring to Figure 8a, the simplest arrangement is a switch that may be controlled so as to terminate the reflective antenna in either a short circuit or an open circuit, producing a phase shift of 180°. A phase shift of other than 180° may be produced using a switch and a delay element such as a transmission line as in Figure 8b. A similar arrangement, shown in Figure 8d, uses a phase shifter instead of a delay element. Referring to Figure 8c, a switch may be used to connect the reflective antenna through any one of multiple delay elements. A similar arrangement, shown in Figure 8e, uses phase shifters instead of delay elements. A single continuously-adjustable delay element or phase shifter may be used as shown in Figure 8g and Figure 8f, respectively. Other combinations of the foregoing 25 elements will be readily apparent.

Note that the specific nature of the reflective antenna termination in Figures 8a through Figure 8g (whether short circuit, open circuit, etc.) is unimportant. The only requirement is that the reflection condition be established and that the reflection

condition be controllable in some manner so as to control the phase of the reflected energy. Furthermore, although at least two distinct control states are required, any number of control states equal to or greater than two, including an infinite number of control states, may be used.

As with conventional phased array antennas, multiple reflective antennae may be used within a single antenna system. Such a system is shown in Figure 9. A primary antenna 901 is coupled to a receiver 903. Multiple secondary antennae 905-1 through 905-N are arrayed near the primary antenna 901. The respective secondary antennae are terminated with phase shifters 907-1 through 907-N 10 (continuous or discrete), controlled by respective phase control signals.

Such an array of secondary antennae may be used to reflect a plane wave so as to focus reflected energy on the active element, primary antenna 901. This result is shown in Figure 10a. Algorithms for determining the appropriate phase shifts are known in the art and do not form part of the present invention.

Just as a conventional phased array antenna can be used to steer a null or a peak, similarly, an array of reflective antennae as in Figure 9 can be used to redirect the angle of greatest sensitivity by changing the phase shifts of the respective reflective antennae appropriately. This result is shown in Figure 10b.

In Figure 9, the reflective antennae are arrayed in a line. As shown in 20 Figure 11, the reflective antennae may also be arrayed in a 2D or 3D field. One or multiple active elements may be positioned in such a field. In the example of Figure 11, a single primary antenna 1101 is positioned within a field of reflective antennae 1103. The primary antenna is connected to a receiver 1105. In the example of Figure 12, two primary antennae (1201, 1203) are positioned within a field of reflective antennae 1205. Signals from the primary antennae are summed using a summer 1207 and input to a single receiver 1209. Alternatively, multiple

independent receivers may be provided if desired, with the independent received signals being combined as in conventional diversity techniques or directional techniques.

Using reflective antennae arrayed in a 2D or 3D field, the benefits of 5 diversity and directionality may be simultaneously obtained. For example, in Figure 14, four reflective antennae 1401-1 through 1401-4 and a single active antenna 1403 may be arranged in a geometry in which the four reflective antennae are placed at the corners of a square and the single active antenna is placed in the middle of the square as shown in Figure 14, the single active antenna being connected to a 10 receiver 1405. The reflective antennae are connected to respective loads 1407-1 through 1407-4, shown in exploded view as including a switch S, a matching impedance load, and a phase-controllable load 1413. A computer 1409 produces control signals for the switches and the phase-controllable loads of each of the reflective antennae. The magnitude and phase of the load of one of the three 15 reflective antennae might be controlled to minimize reflections from it. In this instance, three of the four reflective antennae will therefore be operative such that one of four different sets of three reflective antennae may be selected. The three operative reflective antenna may be controlled to achieve a desired directionality. As required by reception conditions, the system may switch to a different set of 20 three reflective antenna but with reflective phases which still direct the beam in the same direction, thereby achieving diversity.

As compared to conventional multiple-antenna systems, which are typically bulky and costly, the described techniques provide for a multiple-antenna system 25 that is small, low-power and low-cost, ideally suited for personal communications devices. The described techniques are characteristically simple, but allow for most or all of the advantages of sophisticated diversity antenna systems and of phased array antenna systems to be realized.

It will be apparent to those of ordinary skill in the art that the invention can be embodied in other specific forms without departing from the spirit or essential character thereof. The foregoing description is therefore considered in all respects to be illustrative and not restrictive. The scope of the invention is indicated by the appended claims rather than the foregoing description, and all changes which come within the meaning and range of equivalents thereof are intended to be embraced therein.

WHAT IS CLAIMED IS:

1. A method of enhancing an RF signal using an RF section having a primary antenna and at least one secondary antenna in the vicinity of the primary antenna, comprising the steps of:

5 producing an RF signal the secondary antenna reflecting energy from the RF signal; and

changing the phase of RF energy reflected by the secondary antenna in the vicinity of the primary antenna to enhance the RF signal.

- 2. The method of Claim 1, wherein the RF section has multiple 10 secondary antennae, comprising the further step of controlling the secondary antennae to focus reflected RF energy in relation to the primary antenna.
 - 3. The method of Claim 1, wherein electronically changing the phase comprises changing an electronic switch from one of an open state and a closed state to the other of the open state and closed state.
- 15 4. The method of Claim 1, wherein the RF section comprises a variable delay line coupled to the secondary antenna, and wherein electronically changing the phase comprises applying a control signal to the variable analog delay line.
- 5. The method of Claim 1, wherein the RF section comprises a variable phase shifter, and wherein electronically changing the phase comprises applying a20 control signal to the variable phase shifter.
 - 6. The method of Claim 1, comprising the further step of:
 determining signal quality with respect to the primary antenna;
 wherein if said signal quality is below a predetermined threshold, the
 phase of RF energy reflected from the secondary antenna is changed.

7. The method of Claim 1, wherein the RF section has multiple secondary antennae, comprising the further step of controlling the secondary antennae to achieve a desired directionality of the antenna system.

8. The method of Claim 1, wherein the RF section has multiple 5 secondary antennae, comprising the further steps of:

selecting a first subset of secondary antennae;

controlling the secondary antennae to achieve a desired directionality of the primary antenna;

determining signal quality with respect to the primary antenna; and if said signal quality is below a predetermined threshold, selecting a second subset of secondary antennae.

9. An RF section comprising:

an RF amplifier;

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a primary antenna coupled to the RF amplifier;

a secondary antenna in the vicinity of the primary antenna; and means for changing the phase of RF energy reflected by the secondary antenna to enhance one of RF reception and RF transmission.

- 10. The apparatus of Claim 9, wherein the means for changing comprises an electronically controlled switch.
- 20 11. The apparatus of Claim 10, wherein the electronically controlled switch is coupled between the secondary antenna and ground.
 - 12. The apparatus of Claim 11, wherein the electronically controlled switch is controlled so as to present at one time a substantially open circuit and at another time a substantially short circuit.

13. The apparatus of Claim 9, wherein the means for electronically changing comprises a variable delay line.

- 14. The apparatus of Claim 9, wherein the means for electronically changing comprises a variable phase shifter.
- 5 15. The apparatus of Claim 9, further comprising multiple secondary antenna.
 - 16. The apparatus of Claim 15, wherein multiple secondary antenna are positioned and/or phase controlled so as to form an RF beam or beams.
- 17. The apparatus of Claim 16, wherein multiple secondary antenna are 10 arrayed in a two-dimensional array.
 - 18. The apparatus of Claim 16, wherein multiple secondary antenna are arrayed in a three-dimensional array.
 - 19. The apparatus of Claim 15, Claim 16, Claim 17 or Claim 18, further comprising multiple primary antennae.
- The apparatus of Claim 9, further comprising:
 means for determining signal quality with respect to the primary
 antenna;

wherein if said signal quality is below a predetermined threshold, the phase of RF energy reflected from the secondary antenna is changed.

20 21. The apparatus of Claim 9, further comprising: multiple secondary antennae; and

means for controlling the secondary antennae to achieve a desired directionality of the antenna array.

22. The apparatus of Claim 9, further comprising multiple secondary antennae;

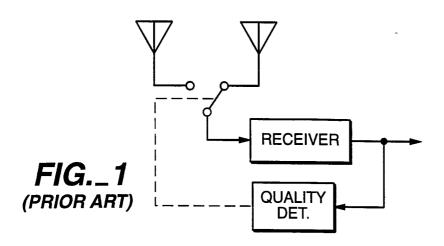
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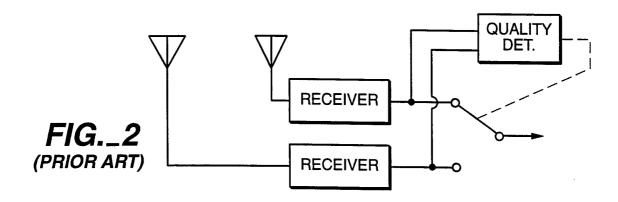
means for selecting a first subset of secondary antennae;

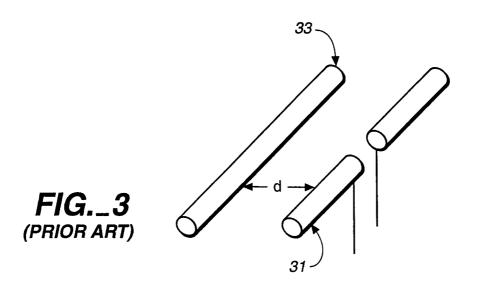
means for controlling the secondary antennae to achieve a desired directionality of the primary antenna;

means for determining signal quality with respect to the primary antenna; and

means for if said signal quality is below a predetermined threshold, selecting a second subset of secondary antenna.









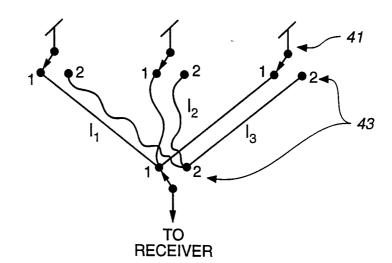
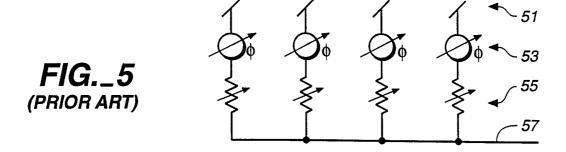
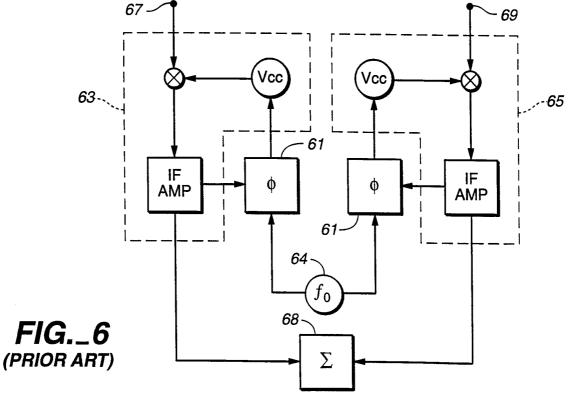
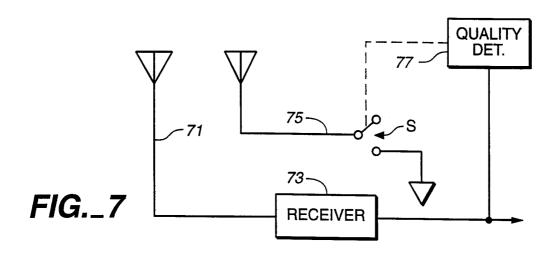


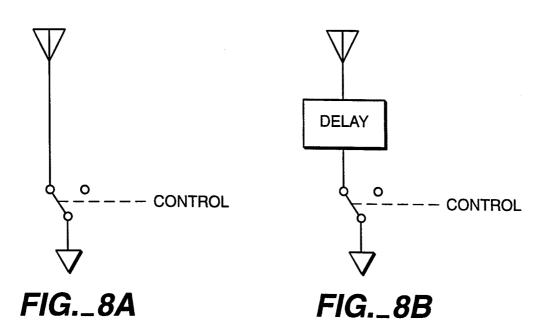
FIG._4
(PRIOR ART)



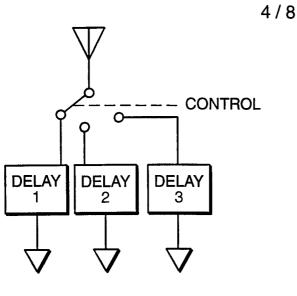


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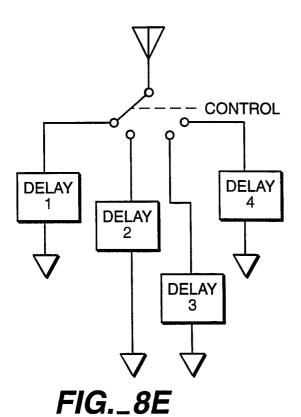


PHASE SHIFT

CONTROL

FIG._8C

FIG._8D



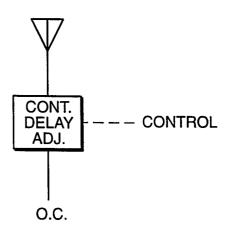


FIG._8F

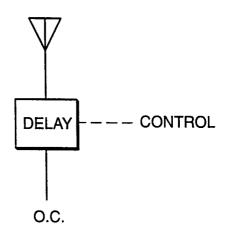


FIG._8G

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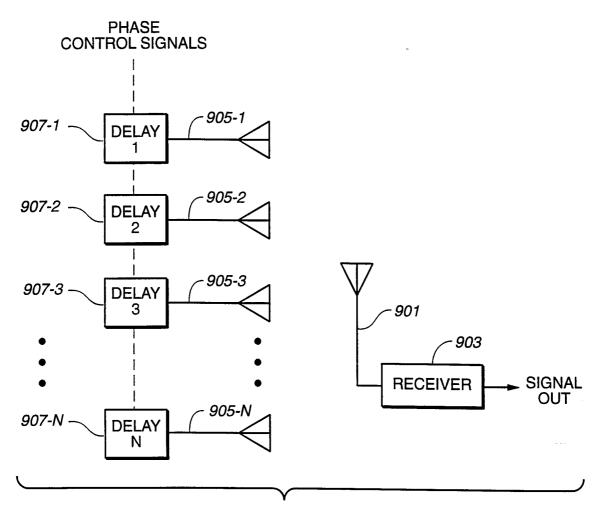
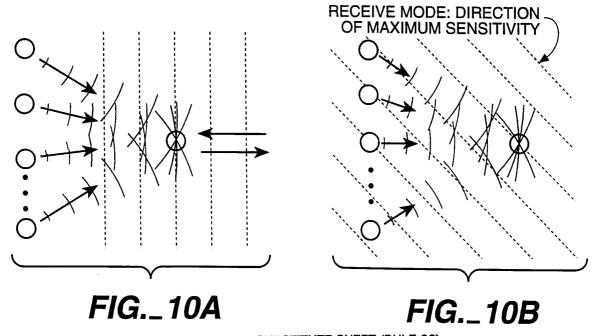


FIG._9



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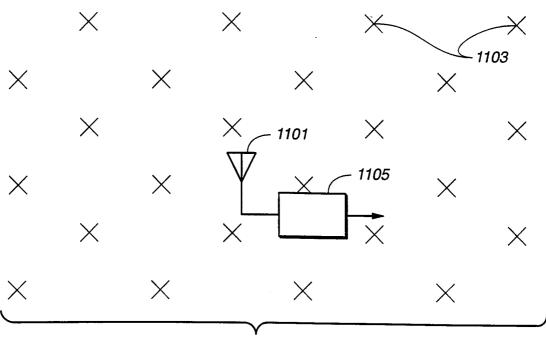


FIG._11

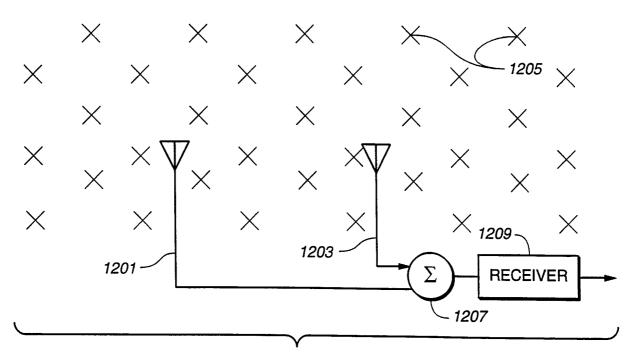
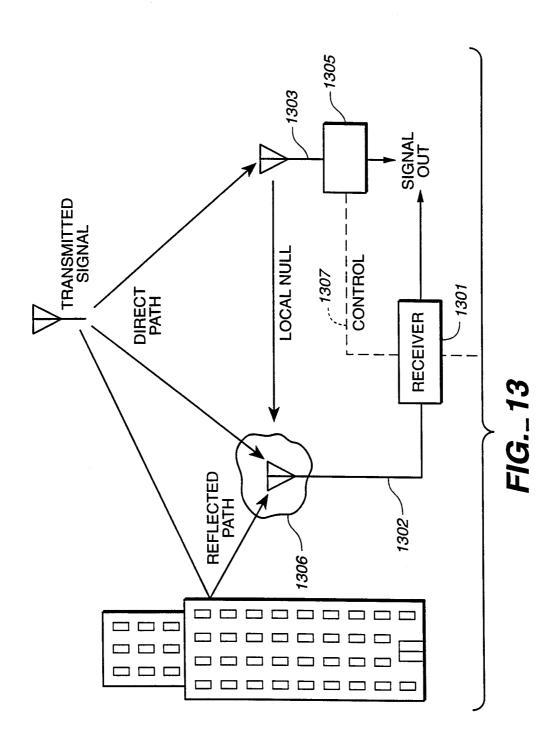
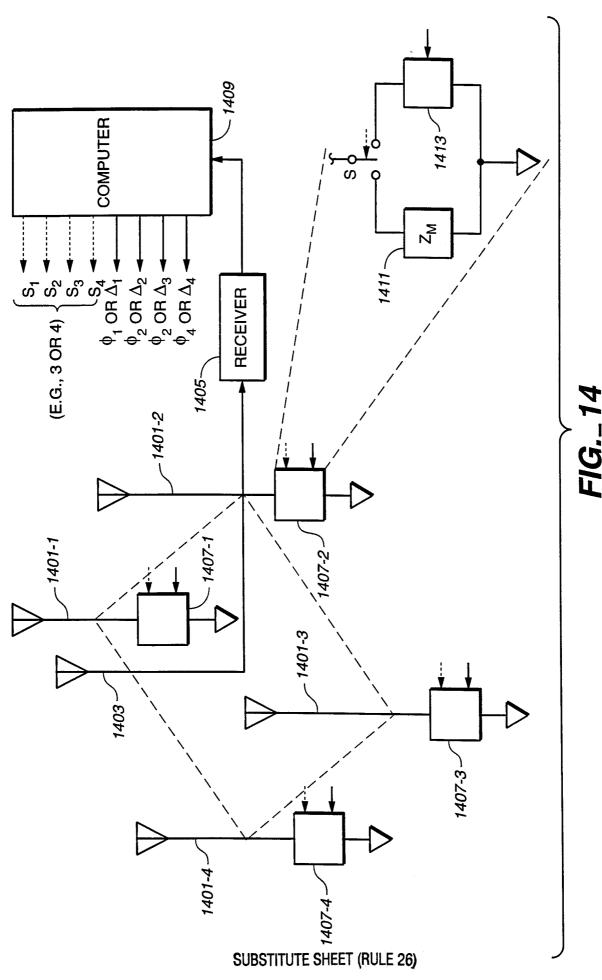


FIG._12





INTERNATIONAL SEARCH REPORT

International application No. PCT/US98/06349

A. CLASSIFICATION OF SUBJECT MATTER								
	:H01Q 19/00, 19/28	-						
US CL :343/834, 835, 836, 817 According to International Patent Classification (IPC) or to both national classification and IPC								
	LDS SEARCHED	national classification and IPC						
Minimum documentation searched (classification system followed by classification symbols)								
U.S. : 343/834, 835, 836, 817, 818, 833, 837, 815, 819								
D								
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched								
Electronic d	Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)							
C. DOCUMENTS CONSIDERED TO BE RELEVANT								
Category*	Citation of document, with indication, where ap	propriate, of the relevant passages Relevant to claim No						
X	US 3,725,938 A (BLACK ET AL.) 03	APRIL 1973 (03/04/73). SEE 1-4, 6-13, 15-22						
	FIGURE 4.	1 1, 6 15, 16 22						
X	US 5,235,343 A (AUDREN ET AL.) 1	0 AUGUST 1993 (10/08/93). 1-4, 6-13, 15-22						
	SEE FIGURE 1.	, , , , , , , , , , , , , , , , , , , ,						
X	US 4,700,197 A (MILNE) 13 OCTO	DBER 1987 (13/10/87). SEE 1-4, 6-13, 15-22						
	FIGURES 2-4.	1 1, 6 15, 15 22						
Y	US 3,199,103 (AUGUSTINE) 03 AU	GUST 1965 (03/08/65). SEE 5 AND 14						
	FIGURE 1.							
Furth	ner documents are listed in the continuation of Box C	. See patent family annex.						
_	ecial categories of cited documents:	"T" later document published after the international filing date or priority						
"A" do to	cument defining the general state of the art which is not considered be of particular relevance	date and not in conflict with the application but cited to understand the principle or theory underlying the invention						
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cit sp	ed to establish the publication date of another citation or other ecial reason (as specified)	"Y" document of particular relevance; the claimed invention cannot be						
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"P" do	cument published prior to the international filing date but later than e priority date claimed	being obvious to a person skilled in the art "&" document member of the same patent family						
Date of the	actual completion of the international search	Date of mailing of the international search report						
19 MAY	1998	1 8 JUN 1998						
37	Y 11 Cd 22 22 2	2 0 0 0 1 1000						
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