

(12) NACH DEM VERTRAG ÜBER DIE INTERNATIONALE ZUSAMMENARBEIT AUF DEM GEBIET DES
PATENTWESENS (PCT) VERÖFFENTLICHTE INTERNATIONALE ANMELDUNG

(19) Weltorganisation für geistiges Eigentum
Internationales Büro



(43) Internationales Veröffentlichungsdatum
29. November 2007 (29.11.2007)

PCT

(10) Internationale Veröffentlichungsnummer
WO 2007/135092 A1

(51) Internationale Patentklassifikation:

B05D 7/24 (2006.01) *C23C 14/16* (2006.01)
B05D 7/14 (2006.01) *C23C 28/02* (2006.01)

(81) Bestimmungsstaaten (soweit nicht anders angegeben, für jede verfügbare nationale Schutzrechtsart): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BH, BR, BW, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RS, RU, SC, SD, SE, SG, SK, SL, SM, SV, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

(21) Internationales Aktenzeichen: PCT/EP2007/054825

(22) Internationales Anmeldedatum:

18. Mai 2007 (18.05.2007)

(25) Einreichungssprache: Deutsch

(26) Veröffentlichungssprache: Deutsch

(30) Angaben zur Priorität:

10 2006 023 230.5 18. Mai 2006 (18.05.2006) DE
10 2006 047 060.5 4. Oktober 2006 (04.10.2006) DE

(84) Bestimmungsstaaten (soweit nicht anders angegeben, für jede verfügbare regionale Schutzrechtsart): ARIPO (BW, GH, GM, KE, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), eurasisches (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), europäisches (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IS, IT, LT, LU, LV, MC, MT, NL, PL, PT, RO, SE, SI, SK, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

(71) Anmelder (für alle Bestimmungsstaaten mit Ausnahme von US): ThyssenKrupp Steel AG [DE/DE]; Kaiser-Wilhelm-Str. 100, 47166 Duisburg (DE).

(72) Erfinder; und

(75) Erfinder/Anmelder (nur für US): NIKOLOV, Krasimir [DE/DE]; Aussigring 12, 44225 Dortmund (DE). SÄMANN, Nicole [DE/DE]; Im Ostholtz 64, 44879 Bochum (DE). SCHUHMACHER, Bernd [DE/DE]; An der Fillekuhle 14 a, 44227 Dortmund (DE).

(74) Anwalt: COHAUSZ & FLORACK; Bleichstrasse 14, 40211 Düsseldorf (DE).

Veröffentlicht:

— mit internationalem Recherchenbericht

Zur Erklärung der Zweibuchstaben-Codes und der anderen Abkürzungen wird auf die Erklärungen ("Guidance Notes on Codes and Abbreviations") am Anfang jeder regulären Ausgabe der PCT-Gazette verwiesen.

(54) Title: SHEET STEEL PROVIDED WITH A CORROSION PROTECTION SYSTEM AND METHOD FOR COATING SHEET STEEL WITH SUCH A CORROSION PROTECTION SYSTEM

(54) Bezeichnung: MIT EINEM KORROSIONSSCHUTZSYSTEM VERSEHENES STAHLBLECH UND VERFAHREN ZUM BESCHICHTEN EINES STAHLBLECHS MIT EINEM SOLCHEN KORROSIONSSCHUTZSYSTEM

(57) Abstract: The invention relates to a flat steel product provided with a coating system, which has optimized corrosion resistance and weldability in coated condition. According to the invention, the steel product includes a base layer made from steel and a corrosion protection system applied to the base layer, which has a metallic coating of less than 3.5 µm thickness, which is formed from a first metallic layer applied to the base layer and a second metallic layer applied to the first metallic layer, with the second metallic layer having formed a metallic alloy with the first metallic layer, and a plasma polymer layer superimposed on the metallic coating.

(57) Zusammenfassung: Die Erfindung betrifft ein mit einem Überzugssystem versehenes Stahlflachprodukt, das im beschichteten Zustand eine optimierte Kombination von Korrosionsbeständigkeit und Verschweißbarkeit besitzt. Erfindungsgemäß weist dazu das Stahlprodukt eine aus einem Stahl gebildete Grundschicht und ein auf die Grundschicht aufgebrachtes Korrosionsschutzsystem auf, das einen weniger als 3,5 µm dicken metallischen Überzug, der aus einer ersten auf die Grundschicht aufgetragenen metallischen Schicht und einer zweiten auf die erste metallische Schicht aufgebrachten zweiten metallischen Schicht gebildet ist, wobei die zweite metallische Schicht mit der ersten metallischen Schicht eine metallische Legierung gebildet hat, und eine auf den metallischen Überzug aufgebrachte Plasmapolymerschicht umfasst.

WO 2007/135092 A1

TRANSLATOR'S CERTIFICATE

I, the undersigned, being familiar both with the German and English language, certify that the attached English translation is a true and exact translation of all the parts of the International patent application PCT/EP2007/054825.



Horst Vissel

Düsseldorf, November 24, 2008

SI/cs 060234WOX
18 May 2007

**STEEL SHEET PROVIDED WITH A CORROSION PROTECTION SYSTEM AND
A METHOD FOR THE COATING OF A STEEL SHEET WITH SUCH A
CORROSION PROTECTION SYSTEM**

The invention relates to a flat steel product provided with a multi-layered corrosion protection system, such as sheet or strip, and a method for coating a flat steel product with a multi-layered protection system.

In order to improve resistance against corrosion, metallic coatings are applied in particular on steel sheets, which in the majority of cases consist of zinc or zinc alloys. Such zinc or zinc alloy coatings, due to their barrier and cathodic protective effect, provide good protection against corrosion for the appropriately coated steel sheet when in practical application.

The thicker the coating, the greater the protective effect of the zinc coating becomes. High zinc coating thicknesses which guarantee a particularly good resistance to corrosion are offset, however, by the decreasing weldability with increasing coating thickness of the sheets to which the zinc coating has been applied. Accordingly, in practice, for example, problems then arise with processing if, by means of laser welding, through-welding of the parts to be connected to one another is to be produced at high welding speeds. Therefore, the requirements placed on the processing capacity of the sheets coated in the conventional manner with a zinc coating 5 - 15 µm thick, which today is used for example in the area of vehicle body

construction or in the manufacture of domestic appliances, are frequently not fulfilled.

The corrosion resistance of zinc-coated sheets can indeed be further improved, with the thickness of the coating adjusted to average values of 7.5 μm , by the application of what is referred to as a "corrosion protection primer". The application of such an additional coating, however, leads to a drastic reduction in the laser welding capacity. This possibility has therefore also not proved its worth for large-scale technical processing.

Against the background of problems with the weldability of conventional Zn-coated sheets, new highly corrosion-resistant Zn-Mg and Zn-Mg-Al coating systems have been developed, which with a perceptibly reduced coating thickness offer corrosion protection comparable to a conventional 7.5 μm thick zinc coating, but which lead to a significant improvement in suitability for laser welding.

One possibility of manufacturing hot-dip galvanized steel sheets of such a nature with increased corrosion resistance with simultaneously reduced coating weight is described in EP 0 038 904 B1. According to this prior art, by means of hot-dip coating a zinc coating containing 0.2% by weight Al and 0.5% by weight Mg is applied onto a steel substrate. The sheet coated in this manner has a better welding capacity with excellent resistance to rust formation.

Despite the reduction in the coating weight made possible by the method known, for example, from EP 0 038 904 B1, with simultaneous good corrosion resistance, the steel sheets coated in this manner still do not fulfil the

requirements imposed for example in the area of motor vehicle body construction on the weldability of sheet metal parts, which in practical use are subjected to high loadings.

Taking the prior art as set out heretofore as a starting point, the invention is based on the object of providing a flat steel product provided with a coating system which in the coated state has a combination of corrosion resistance and weldability optimised to such a degree that it is also capable of meeting the further increasing demands of processors of such sheets. In addition to this, a method for the manufacture of such sheets is to be described.

With regard to the product, this object is resolved by a flat steel product which, according to the invention, has a base layer formed from a steel and a corrosion protection system applied onto the base layer, which comprises a metallic coating less than 3.5 μm thick, formed from a first metallic layer applied onto the base layer and a second metallic layer applied onto the first metallic layer, wherein the second metallic layer has formed a metallic alloy with the first metallic layer, and comprises a plasma polymer layer applied onto the metallic coating.

With regard to the method for the manufacture of a corrosion-resistant and readily weldable flat steel product, the object referred to above is resolved in the appropriate manner according to the invention in that a first metallic layer is applied onto a steel substrate forming the base layer of the flat steel product and a second metallic layer is applied onto the first metallic layer, which, as a consequence of heat treatment, becomes

an alloy with the first metallic layer, wherein the total thickness of the metallic coating formed from the first and second metallic layers amounts to less than 3.5 μm , and in that a plasma polymer layer is applied onto the coating formed from the first and second metallic layers.

The thickness of the plasma polymer layer applied according to the invention onto the metallic coating is preferably restricted to a maximum of 2500 μm . It has surprisingly transpired that, in particular with lesser thicknesses of the plasma polymer layer, especially good properties of the steel sheet according to the invention can be guaranteed. As a result, the thickness of the plasma polymer layer is advantageously restricted to 100 - 1000 nm, in particular 200 - 500 nm.

With a steel strip or sheet according to the invention, having a multi-layer, thin corrosion protection system, an optimum combination of the advantages of the different corrosion protection properties of the different layers is achieved. Accordingly, a flat steel product according to the invention has a high resistance to corrosion both in the bare state and in combination with organic coatings. This high corrosion stability proves its worth in particular with regard to flanges and cavities. Tests on flange samples prepared in accordance with SEP 1160 and manufactured from steel sheets coated in accordance with the invention have shown that in the corrosion cyclic test in accordance with VDA test specification 621-415 a corrosion stability of more than 10 cycles without red rust is guaranteed.

A further surprising property possessed by a flat steel product according to the invention is demonstrated when such a sheet or strip is painted directly (without phosphating and passivation) by means of cathodic immersion painting. In a bend test carried out on the basis of DIN EN ISO 6860 for steel sheets or strips in accordance with the invention, an excellent paint adherence capacity resulted. No paint flaking and also no flaking of the coating from the base material was in evidence.

In addition to a high resistance to corrosion and an excellent paint adherence capacity, sheets according to the invention have good resistance to stone impact.

Accordingly, in the stone impact tests carried out in accordance with DIN 55996-1B, it was proved that, with steel sheets according to the invention, no flaking of the coating from the base material is caused by stone impact.

In addition to a high resistance to corrosion, an excellent paint adherence capacity and good resistance to stone impact, sheets according to the invention have very good laser welding properties. This is demonstrated by the fact that hole-free laser seams could be achieved without or with only a very small proportion of pores and/or discharge craters, with a technical joint gap of 0 mm and welding speeds of up to 5 m/min. In addition to this, good spot welding could be demonstrated in the test carried out in accordance with ISO 14327.

The good corrosion resistance of the steel sheets or strips coated in accordance with the invention, in combination also with their inherently excellent paint adherence capacity, their good resistance to stone impact and their

good spot-welding and laser-welding ability, make flat steel products according to the invention especially well-suited for use as materials for motor vehicle body construction or for the manufacture of domestic appliances.

With a metal sheet or strip coated in accordance with the invention, the thin, multi-layer corrosion protection system is formed from at least one layer, which guarantees electrochemical protection of the steel substrate forming the base layer, a layer lying on top of this which is capable of forming an alloy coating with the first layer and so leads to a perceptible improvement in the corrosion protection by means of additional electrochemical protection mechanisms of the metal sheet or strip, as well as from a further layer - the plasma polymer layer - which in its capacity as a barrier and/or passive layer leads to a further improvement in the corrosion protection.

With regard to the capacity for further processing, it is advantageous in this context if the total thickness of the metallic coating according to the invention is less than 3.5 µm and if also the thickness of the plasma polymer layer applied onto the metallic layer is restricted to less than 2500 nm. Surprisingly, it has been demonstrated that, despite the advantageously minimised thickness of the coating according to the invention, the corrosion resistance required by the users of sheets and strips obtained according to the invention is always guaranteed.

The first metallic layer can be, for example, a pure zinc coating, which can be applied onto the steel substrate economically by conventional means by electrolytic galvanizing, hot-dip galvanizing, or vacuum depositing. As

an alternative, the first metallic coating may also consist of Al, a Zn-Ni, a Zn-Fe, or a Zn-Al alloy.

Preferably, the second layer of the coating system according to the invention is a zinc alloy coating (Zn-Y). This zinc alloy coating is formed if a metal is applied onto the first layer which forms a Zn alloy with the first layer containing Zn. For this purpose, the metallic second layer becoming an alloy with the first layer can, for example, be deposited on the first layer by thermal evaporation, preferably carried out in a vacuum. This method is particularly well-suited if the second metallic layer is a fine-structured magnesium layer with a thickness of 100 - 2000 nm, preferably 100 - 1000 nm.

As well as Mg, other metals have proved to be suitable materials for the second metallic layer. Accordingly, for example by using Al, Ti, Cr, Mg, Ni, or their alloys, the demands placed on the second layer in each case can be fulfilled.

The plasma polymer layer applied according to the invention onto the metallic coating can, for example, be formed from organo-silane compounds, hydrocarbon compounds, organo-metallic compounds or their mixtures.

A particularly uniform formation of the plasma polymer layer applied according to the invention onto the metallic coating can be achieved by the plasma polymer layer being deposited by means of hollow cathode glow discharge. With hollow cathode glow discharge, high plasma densities and correspondingly high deposition rates can be achieved. Accordingly, this possibility for producing the plasma

polymer layer is particularly well-suited for large-scale technical application in run-through techniques, and can be integrated into existing run-through coating systems, e.g. electrolytic galvanizing systems or hot-dip coating systems. In this situation, good processing results are achieved if the deposition rate of the hollow cathode glow discharge amounts to 10 - 1000 nm/s. The coating result can be improved further if the deposition rate of the hollow cathode glow discharge is set to 20 - 750 nm/s, wherein an optimum provision of the plasma polymer layer is achieved if the deposition rate of the hollow cathode glow discharge amounts to 50 - 500 nm/s, in particular 50 - 360 nm/s.

The heat treatment carried out according to the invention after the application of the metallic layers of the coating system is preferably carried out at temperatures below 500 °C.

The heat treatment carried out to form alloying between the first and second metallic layers can be applied before or after the application of the plasma polymer layer. Regardless of when it is carried out, it guarantees good binding of the layer and therefore inherently a good corrosion protection effect, with, at the same time, excellent laser welding capacity.

Surprisingly, it has been shown that in a carrying out a process in which, preferably, a subsequent heat treatment is not carried out until after the application of the metallic layers and of the plasma polymer layer, a positive effect on the alloying process between Zn and Mg is achieved. Accordingly, the method according to the invention differs from those methods from the prior art in

which the metallic layer system is produced by means of deposition of a fine-structured magnesium layer, heat-evaporated in a vacuum, with a thickness of 100 ... 2000 nm, in particular 100 - 1000 nm, on a zinc coating deposited by means of electrolytic galvanizing or hot-dip galvanizing or vacuum deposition and subsequent heat treatment, in that the alloying process is carried out before or only after the deposition of the plasma polymer layer by subsequent heat treatment.

The advantage of this procedure lies in the fact that the strip can be coated in series in a vacuum without coming into contact with the atmosphere in the course of carrying out the process.

The invention is described in greater detail hereinafter on the basis of embodiments.

Example 1

A steel strip for deep-drawing purposes comprises a base layer, manufactured, for example, from a low-alloyed steel, onto which a thin, multi-layered corrosion protection system is applied.

The corrosion protection system in this situation is formed by a zinc coating, applied as a first metallic layer onto the base layer, the thickness of which amounts to approx. 3.4 μm , a second metallic layer applied onto the first metallic layer in the form of a Zn-Mg alloying coating, the thickness of which amounts to less than 1 μm , so that the metallic layers together are less than 3.5 μm thick, and a 340 nm thick plasma polymer layer. The thickness of the

plasma polymer layer was varied. Thus, for example, plasma polymer layers with a thickness of 340 nm and 520 nm were deposited.

The corrosion protection layer built up in this way guarantees, with a plasma polymer layer 340 nm thick, a corrosion stability in flange samples manufactured from the steel strip in accordance with SEP 1160 of at least 10 cycles in the corrosion cycle test in accordance with VDA Test Specification 621-415 without red rust. With steel sheets conventionally coated with a Zn-ZnMg coating system without a plasma polymer layer, examined as a reference, at this point in time more than > 80 - 100 % red rust was present.

With a corrosion protection system built up in an analogous manner and with a plasma polymer layer 520 nm thick, an even higher corrosion resistance could be demonstrated.

Example 2

The manufacture of the thin, multi-layered corrosion protection system represented in Fig. 1 on an IF steel sheet has firstly had a zinc layer deposited on the IF steel substrate forming the base layer by means of electrolytic galvanizing. Next, a fine-structured magnesium coating was applied onto the zinc layer by thermal evaporation in a vacuum. With subsequent heat treatment at 310 °C a Zn-Mg alloying coating was obtained and finally a plasma polymer layer was deposited by means of hollow cathode glow discharge using tetramethyl silane with a deposition rate of 34 nm/s.

The steel sheet obtained in this way had excellent corrosion protection with simultaneously very good laser welding capability.

Example 3

In order to produce the thin, multi-layer corrosion protection system represented in transverse section in Fig. 2 on a fine steel sheet forming the base layer, as a first step a Zn coating was deposited on the base layer as a first metallic layer by means of electrolytic galvanizing. Next, a fine-structured magnesium layer was deposited by thermal evaporation in a vacuum as a second metallic layer on the first metallic layer and a plasma polymer layer was deposited on the second metallic layer by means of hollow cathode glow discharge using tetramethyl silane, with a deposit rate of 34 nm/s. Only after the application of the plasma polymer layer on the second metallic layer was a heat treatment of 10 s at 335 °C carried out to form the Zn-Mg alloying coating.

The steel sheet obtained in this manner also had excellent corrosion protection with simultaneously very good laser welding capability.

With the procedure according to the invention, the corrosion coating can be produced free of interruption in an "in-line process sequence" in a vacuum, so that manufacturing costs are reduced and processing is simplified as a whole.

18 May 2007

CLAIMS

1. Flat steel product with a base layer formed from a steel and a corrosion protection system applied onto the base layer, which comprises a metallic coating less than 3.5 μm thick, formed from a first metallic layer applied onto the base layer and a second metallic layer applied onto the first metallic layer, wherein the second metallic layer has formed a metallic alloy with the first metallic layer, and comprises a plasma polymer layer applied onto the metallic coating.
2. Flat steel product according to Claim 1, characterised in that the plasma polymer layer is a maximum of 2500 μm thick.
3. Flat steel product according to Claim 2, characterised in that the plasma polymer layer is 100 - 1000 nm thick.
4. Flat steel product according to Claim 3, characterised in that the plasma polymer layer is 200 - 500 nm thick.
5. Flat steel product according to any one of the preceding claims, characterised in that the first metallic layer is a Zn, an Al, a Zn-Ni, a Zn-Fe, or a Zn-Al coating.

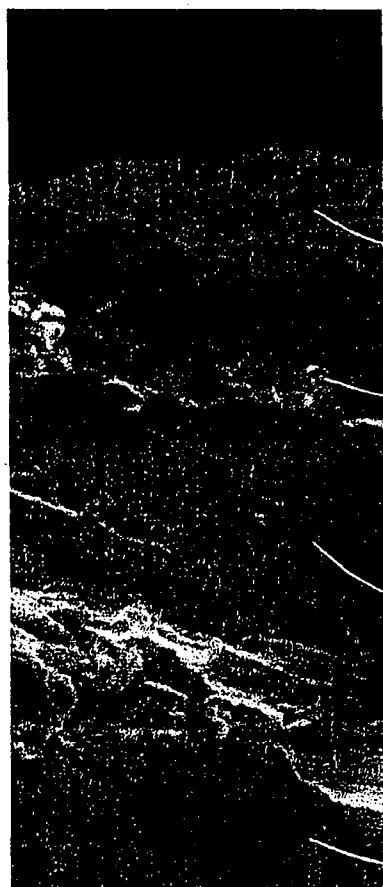
6. Flat steel product according to any one of the preceding claims, characterised in that the second metallic layer is a zinc alloy coating.
7. Flat steel product according to any one of the preceding claims, characterised in that the second metallic layer is formed from at least one of the elements from the group Mg, Al, Ti, Cr, Mn, Ni or their alloys.
8. Flat steel product according to any one of the preceding claims, characterised in that the thickness of the second layer amounts to 100 - 2000 nm.
9. Flat steel product according to Claim 8, characterised in that the thickness of the second layer amounts to 200 - 1000 nm.
10. Flat steel product according to any one of the preceding claims, characterised in that the plasma polymer layer is formed from organo-silane compounds, hydrocarbon compounds, organo-metallic compounds or their mixtures.
11. Method for the manufacture of a flat steel product coated with a corrosion protection system, in which a first metallic layer is applied onto a steel substrate forming the base layer of the flat steel product and a second metallic layer is applied onto the first metallic layer, which, as a consequence of heat treatment, becomes an alloy with the first metallic layer, wherein the total thickness of the metallic coating formed from the first and second metallic

layers amounts to less than 3.5 μm , in which a plasma polymer layer is applied onto the coating formed from the first and second metallic layers.

12. Method according to Claim 11, characterised in that the plasma polymer layer is a maximum of 2500 μm thick.
13. Flat steel product according to Claim 12, characterised in that the plasma polymer layer is 100 - 1000 nm thick.
14. Flat steel product according to Claim 13, characterised in that the plasma polymer layer is 200 - 500 nm thick.
15. Method according to any one of Claims 11 to 14, characterised in that the first layer is a zinc layer, which is applied by electrolytic galvanizing, hot-dip galvanizing, or vacuum evaporation onto the base layer.
16. Method according to any one of Claims 11 to 15, characterised in that the first layer is formed from an Al, a Zn-Ni, a Zn-Fe or a Zn-Al compound.
17. Method according to any one of Claims 11 to 16, characterised in that the second metallic layer is a layer containing magnesium.
18. Method according to any one of Claims 11 to 17, characterised in that the second metallic layer is formed from Al, Ti, Cr, Mn, Ni or their alloys.

19. Method according to any one of Claims 11 to 18, characterised in that the second metallic layer is deposited on the first layer by thermal evaporation.
20. Method according to any one of Claims 11 to 19, characterised in that the plasma polymer layer is deposited by means of hollow cathode glow discharge.
21. Method according to Claim 20, characterised in that the deposition rate of the hollow cathode glow discharge is 10 - 1000 nm/s.
22. Method according to Claim 21, characterised in that the deposition rate of the hollow cathode glow discharge is 20 - 750 nm/s.
23. Method according to Claim 22, characterised in that the deposition rate of the hollow cathode glow discharge is 50 - 500 nm/s.
24. Method according to Claim 23, characterised in that the deposition rate of the hollow cathode glow discharge is 50 - 360 nm/s.
25. Method according to any one of Claims 11 to 24, characterised in that the temperature of the heat treatment is less than 500 °C.
26. Method according to any one of Claims 11 to 25, characterised in that the heat treatment is carried out before the application of the plasma polymer layer.

27. Method according to any one of Claims 11 to 26, characterised in that the heat treatment is carried out after the application of the plasma polymer layer.



Plasma polymer coating

Zn-Mg alloy coating

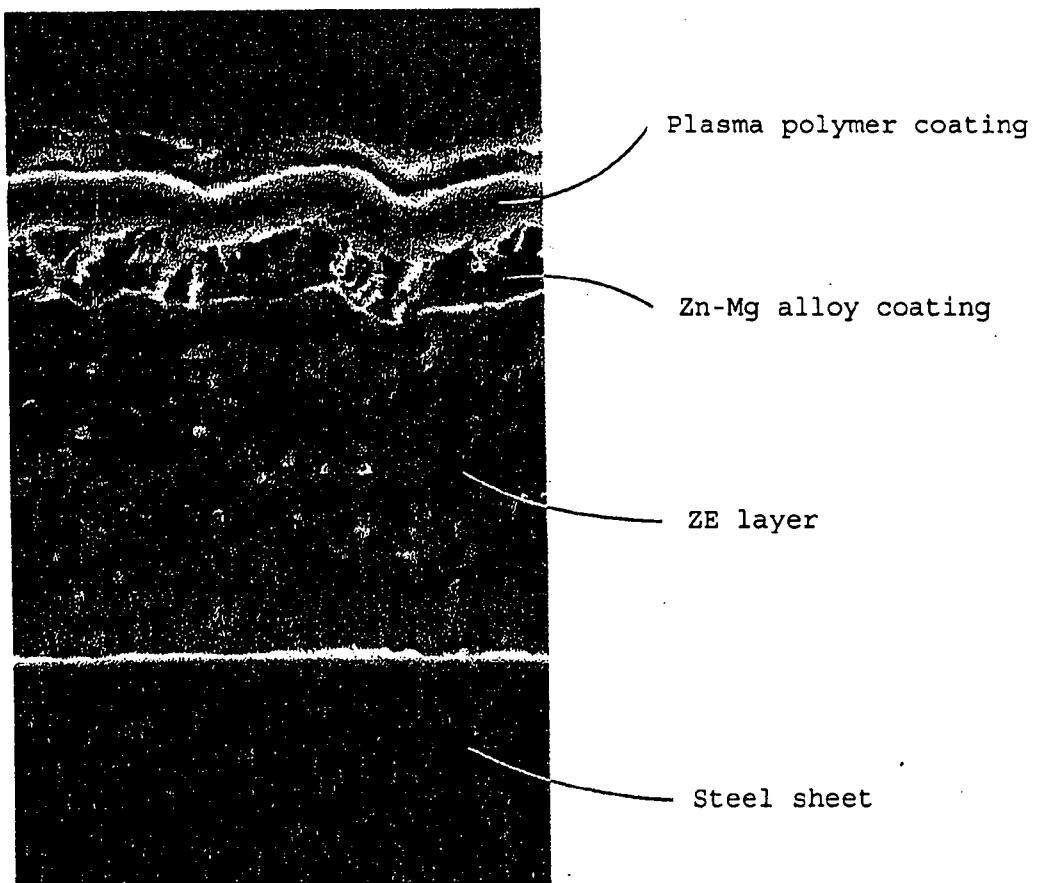
ZE layer

Steel sheet

2 μ m

Fig. 1:

Representation of a multi-layer corrosion protection system according to the invention on the basis of a ZE-ZnMg alloy coating plasma polymer.
FE-SEM image of the cross break through the coating.



2 μm

Fig. 2:

Representation of a multi-layer corrosion protection system according to the invention on the basis of a ZE-ZnMg alloy coating plasma polymer.

Final heat treatment.

FE-SEM image of the cross break through the coating.