(54) Title: METHOD OF SEPARATING SUPERABSORBENT POLYMER PARTICLES FROM A SOLIDIFIED THERMOPLASTIC COMPOSITION COMPRISING POLYMERS

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METHOD OF SEPARATING SUPERABSORBENT POLYMER PARTICLES FROM A SOLIDIFIED THERMOPLASTIC COMPOSITION COMPRISING POLYMERS

FIELD OF THE INVENTION

The present invention relates to a method for re-mobilizing superabsorbent polymer particles which have previously been immobilized by a solidified thermoplastic composition comprising at least 30 weight-% of a thermoplastic polymer. The superabsorbent polymer particles are separated from the solidified thermoplastic composition by using a supercritical fluid comprising carbon dioxide, propane or mixtures thereof. Separation may be further improved by the use of a co-solvent.

BACKGROUND OF THE INVENTION

In the course of manufacturing disposable absorbent articles, such as diapers and sanitary napkins, it is common to detect defect or imperfect articles and discard them from the production process. Though not suitable for sale, these waste products may contain materials, which are too valuable to be thrown away. Instead, it may be desirable to retrieve certain materials from the defect product. Especially, it is desirable to regain the superabsorbent polymer particles typically comprised in disposable absorbent articles.

Today, most disposable diapers use absorbent cores with superabsorbent polymer particles intermingled with pulp fibers (so-called "airfelt"), such as cellulose fibers. In these diapers, the superabsorbent polymer particles are largely held in place by the surrounding pulp fibers. The superabsorbent polymer (SAP) particles may therefore be retrieved by shredding the articles and shaking the SAP particles out e.g. via vibration, freeing the particles from the surrounding pulp fibers.

However, moving to absorbent articles wherein the absorbent cores are free from airfelt or wherein the absorbent cores contain only small amounts of airfelt, the SAP particles have to be immobilized by different means, as they can no longer be held in place by surrounding pulp fibers. One way to immobilize the SAP particles within the absorbent core is by using adhesives. These adhesives, though used in small amounts relative to the amount of SAP particles, closely adhere to the SAP particles. Apart from attaching the SAP particles to each other, the adhesives also adhere the SAP particles to a carrier substrate, such as a nonwoven web. Thereby, the particles cannot simply be shaken out to recycle them.
Thus, it would be desirable to have a method for separating SAP particles from the adhesives in order to regain the SAP particles. The particles can then be re-used for the manufacture of disposable absorbent articles.

SUMMARY OF THE INVENTION

The invention relates to a method for separating superabsorbent polymer particles from a solidified thermoplastic composition comprising at least 30 weight-% of a thermoplastic polymer based on the weight of the solidified thermoplastic composition. The method comprises the steps of:

a) providing agglomerates of the superabsorbent polymer particles and the solidified thermoplastic composition, wherein at least a part of the superabsorbent polymer particles are adhered to at least a part of the solidified thermoplastic composition,

b) subjecting the agglomerates to a supercritical fluid comprising carbon dioxide, propane or mixtures thereof.

BRIEF DESCRIPTION OF THE DRAWINGS

These and other features, aspects and advantages of the present invention will become better understood with regard to the following description, appended claims, and accompanying drawings where:

Fig. 1 is a plan view of a diaper comprising the fibrous structure made by the process of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

Definitions

"Absorbent article" refers to devices that absorb and contain body exudates, and, more specifically, refers to devices that are placed against or in proximity to the body of the wearer to absorb and contain the various exudates discharged from the body. Absorbent articles may include diapers, pants, training pants, adult incontinence undergarments, sanitary napkin, and the like. As used herein, the term "body fluids" or "body exudates" includes, but is not limited to, urine, blood, vaginal discharges, breast milk, sweat and fecal matter. Preferred absorbent articles of the present invention are diapers, pants, training pants and/or sanitary napkins.
"Absorbent core" means a structure typically disposed between a topsheet and a backsheet of an absorbent article for absorbing and containing liquid received by the absorbent article. The absorbent core typically comprises absorbent material such as airfelt (comprising cellulose fibers), SAP particles and possibly nonwoven webs. In one embodiment, the absorbent core may comprise less than 10% of cellulose fibers or may even be substantially cellulose free (i.e. less than 1% cellulose) and may comprise one or more substrates, SAP particles disposed on the one or more substrates, and a solidified thermoplastic composition. The solidified thermoplastic composition is applied on the SAP particles and at least a portion of the one or more substrates for immobilizing the absorbent particulate polymer material on the one or more substrates. The one or more substrates may comprise or consist of nonwoven webs. The nonwoven webs will at least partially surround the SAP particles and the solidified thermoplastic composition and these nonwovens are therefore often referred to as core wrap or core cover. The core wrap or core cover may consist of an upper layer towards the body-facing surface of the absorbent article and of a lower layer towards the garment-facing side of the absorbent article. The two layers may be continuously or intermittently bonded to each other around their perimeters. The upper and lower layer may be made of the same nonwoven webs or may be made of different nonwoven webs, i.e. the upper layer may be fluid pervious whereas the lower layer may be fluid impervious. The core wrap / core cover may also consist of a single nonwoven web, which envelops the SAP particles and the solidified thermoplastic composition. In a multilayer absorbent core, one or more layers of a substrate (e.g. a nonwoven web) may additionally be placed within the absorbent core to at least partially separate and segment the SAP particles.

In the present invention, the absorbent cores will typically comprises more than 80% of SAP particles by weight of absorbent material (i.e. excluding any substrate layers), more preferably more than 90%. The absorbent core may even be free of airfelt. The absorbent material of the absorbent core may also consist solely of SAP particles.

In one embodiment, the absorbent core, in addition to the SAP particles, comprises an odor control compound. The odor control compound may be provided in the form of odor control particles. The odor control particles may be distributed homogeneously throughout the absorbent core or may, alternatively, be provided only in distinct areas, while other areas are free from odor control particles. For example, the odor control particles may be provided in the form of one or more distinct layers within the absorbent core. The odor control particles may have a particle size similar to the particle size of the SAP particles. In one embodiment, the odor control compound,
e.g. the odor control particles, comprise tetra acetyl ethylene diamine and percarbonate. The odor control particles comprising percarbonate and tetra acetyl ethylene diamine may be comprised in an amount from 200 mg to 400 mg per absorbent core, preferably from 250 mg to 350 mg. Typically the weight of the SAP particles in the absorbent core will be from 30 times to 50 times the weight of the odor control compounds, preferably the weight of the SAP particles in the absorbent core will be from 35 times to 45 times the weight of the odor control compounds.

It is understood that for the present invention the solidified thermoplastic composition -as well as the odor control compound, if present- will not be considered to be a comprised by the absorbent material, as the solidified thermoplastic composition does not have absorbing properties. Further, for the present invention, the absorbent core does not include the topsheet, the backsheet and (if present) the acquisition system of the absorbent article.

"Superabsorbent polymer particles" as used herein refer to cross linked polymeric materials that can absorb at least 5 times their weight of an aqueous 0.9% saline solution as measured using the Centrifuge Retention Capacity test (Edana 441.2-01). The SAP particles are in particulate form so as to be flowable in the dry state. Preferred SAP particles of the present invention are made of poly(meth)acrylic acid polymers. However, e.g. starch-based SAP particles are also comprised within the scope of the present invention.

"Contaminated SAP particles" as used herein refers to SAP particles to which the solidified thermoplastic composition of the present invention is adhered.

"Airfelt" is used herein to refer to comminuted wood pulp, which is a form of cellulose fibers.

"Comprise," "comprising," and "comprises" are open ended terms, each specifies the presence of what follows, e.g., a component, but does not preclude the presence of other features, e.g., elements, steps, components known in the art, or disclosed herein.

"Consisting essentially of is used herein to limit the scope of subject matter, such as that in a claim, to the specified materials or steps and those that do not materially affect the basic and novel characteristics of the subject matter.

"Disposable" is used in its ordinary sense to mean an article that is disposed or discarded after a limited number of usage events over varying lengths of time, for example, less than about 20
events, less than about 10 events, less than about 5 events, or less than about 2 events. A disposable absorbent article is most often disposed after single use.

"Diaper" refers to an absorbent article generally worn by infants and incontinent persons about the lower torso so as to encircle the waist and legs of the wearer and that is specifically adapted to receive and contain urinary and fecal waste. As used herein, the term "diaper" also includes "pants" which is defined below.

"Pant" or "training pant", as used herein, refer to disposable garments having a waist opening and leg openings designed for infant or adult wearers. A pant may be placed in position on the wearer by inserting the wearer's legs into the leg openings and sliding the pant into position about a wearer's lower torso. A pant may be preformed by any suitable technique including, but not limited to, joining together portions of the article using refastenable and/or non-refastenable bonds (e.g., seam, weld, adhesive, cohesive bond, fastener, etc.). A pant may be preformed anywhere along the circumference of the article (e.g., side fastened, front waist fastened). While the terms "pant" or "pants" are used herein, pants are also commonly referred to as "closed diapers," "prefastened diapers," "pull-on diapers," "training pants," and "diaper-pants".

A "nonwoven web" is a manufactured sheet, web or batt of directionally or randomly orientated fibers, bonded by friction, and/or cohesion and/or adhesion, excluding paper and products which are woven, knitted, tufted, stitch-bonded incorporating binding yarns or filaments, or felted by wet-milling, whether or not additionally needled. The fibers may be of natural or man-made origin and may be staple or continuous filaments or be formed in situ. Commercially available fibers have diameters ranging from less than about 0.001 mm to more than about 0.2 mm and they come in several different forms such as short fibers (known as staple, or chopped), continuous single fibers (filaments or monofilaments), untwisted bundles of continuous filaments (tow), and twisted bundles of continuous filaments (yarn). Nonwoven webs can be formed by many processes such as meltblowing, spunbonding, solvent spinning, electrospinning, carding and airlaying. The basis weight of nonwoven webs is usually expressed in grams per square meter (gsm).
Absorbent articles comprising the fibrous structure

In the following, a disposable diaper will be described as one example of an absorbent article of the present invention. It is however understood, that the other disposable absorbent articles are also encompassed by the present invention, such as pants, training pants and sanitary napkins.

Fig. 1 is a plan view of a diaper 210 according to a certain embodiment of the present invention. The diaper 210 is shown in its flat out, uncontracted state (i.e. without elastic induced contraction) and portions of the diaper 210 are cut away to more clearly show the underlying structure of the diaper 210. A portion of the diaper 210 that contacts a wearer is facing the viewer in Fig. 1. The diaper 210 generally may comprise a chassis 212 and an absorbent core 214 disposed in the chassis.

The chassis 212 of the diaper 210 in Fig. 1 comprises the main body of the diaper 210. The chassis 212 may comprise an outer covering 216 including a topsheet 218, which may be liquid pervious, and/or a backsheet 220, which may be liquid impervious. The absorbent core 214 may be encased between the topsheet 218 and the backsheet 220. The chassis 212 may also include side panels 222, elasticized leg cuffs 224, and an elastic waist feature 226.

The leg cuffs 224 and the elastic waist feature 226 may each typically comprise elastic members 228. One end portion of the diaper 210 is configured as a first waist region 230 of the diaper 210. An opposite end portion of the diaper 210 is configured as a second waist region 232 of the diaper 210. An intermediate portion of the diaper 210 is configured as a crotch region 234, which extends longitudinally between the first and second waist regions 230 and 232. The waist regions 230 and 232 may include elastic elements such that they gather about the waist of the wearer to provide improved fit and containment (elastic waist feature 226). The crotch region 234 is that portion of the diaper 210 which, when the diaper 210 is worn, is generally positioned between the wearer's legs.

The diaper 210 is depicted in Fig. 1 with its longitudinal axis 236 and its transverse axis 238. The periphery 240 of the diaper 210 is defined by the outer edges of the diaper 210 in which the longitudinal edges 242 run generally parallel to the longitudinal axis 236 of the diaper 210 and the end edges 244 run between the longitudinal edges 242 generally parallel to the transverse axis 238 of the diaper 210. The diaper 220 may also include such other features as are known in the art including front and rear ear panels, waist cap features, elastics and the like to provide
better fit, containment and aesthetic characteristics. Such additional features are well known in
the art and are e.g., described in U.S. Pat. No. 3,860,003 and U.S. Pat. No. 5,151,092.

In order to keep the diaper 210 in place about the wearer, at least a portion of the first waist
region 230 may be attached by the fastening member 246 to at least a portion of the second waist
region 232 to form leg opening(s) and an article waist. According to certain embodiments, the
diaper 210 may be provided with a re-closable fastening system or may alternatively be provided
in the form of a pant-type diaper. When the absorbent article is a diaper, it may comprise a re-
closable fastening system joined to the chassis for securing the diaper to a wearer. The fastening
system may include at least one fastening member 246 and at least one landing zone 248. When
the absorbent article is a pant-type diaper, the article may comprise at least two side panels
joined to the chassis along their longitudinal edges facing towards the longitudinal axis 236 and
joined to each other along their longitudinal edges facing away from the longitudinal axis 236 to
form a pant.

Taking a cross section of Fig. 1 along the sectional line 2-2 of Fig. 1 and starting from the wearer
facing side, the diaper 210 may comprise the topsheet 218, the components of the absorbent core
214, and the backsheet 220. Diaper 210 also comprises an acquisition system 250 disposed
between the liquid permeable topsheet 218 and the wearer facing side of the absorbent core 214.
The acquisition system 250 may be in direct contact with the absorbent core.

The acquisition system 250 may comprise a single layer or multiple layers, such as an upper
acquisition layer 252 facing towards the wearer and a lower acquisition 254 layer facing the
garment of the wearer. According to a certain embodiment, the acquisition system 250 may
function to receive a surge of liquid, such as a gush of urine. In other words, the acquisition
system 250 may serve as a temporary reservoir for liquid until the absorbent core 214 can absorb
the liquid.

In a certain embodiment, the acquisition system 250 may comprise chemically cross-linked
cellulose fibers and/or nonwoven webs.

**Supercritical Fluids**

When a gas is compressed to a sufficiently high pressure, it becomes liquid. If, on the other hand,
the gas is heated beyond a specific temperature, it can no longer be transferred to the liquid state
by compression. This temperature is called the critical temperature and the corresponding vapor
pressure is called the critical pressure. These values of temperature and pressure define a critical point, which is unique to a given substance. The state of the substance is called supercritical state when both the temperature and pressure exceed the critical point values as shown in the diagram below. Critical temperature and pressure values for carbon dioxide are 31.1°C and 73.8 bar. For propane, the critical temperature and pressure values are 38.8°C and 42.5 bar.

This supercritical fluid (SCF) takes on many of the properties of both gas and liquid. In the supercritical state, increasing the solvent capacity and varying the solvent properties can be achieved with relatively small changes in temperature and pressure. Due to its favorable diffusivity, viscosity, surface tension and other physical properties, SCFs are especially suitable as solvents for extraction. For example SC carbon dioxide has much higher diffusion rates and considerably higher viscosity compared to typical liquid solvents, such as ethanole, isopropanole or n-hexane.

Its low viscosity and low surface tension enable SCFs to penetrate a solid substance from which an active component is to be extracted.

Furthermore, in SCF extraction with CO₂, there is no solvent residue in the extract. For the present invention, CO₂ purity should be at least 99.95%. Also, its near ambient critical temperature makes it ideally suitable for thermo labile products. Due to its very low latent heat
of vaporization, relatively low energy input is required for the extract separation. Furthermore, the energy required for attaining the supercritical state of CO₂ is often less than the energy associated with distillation of conventional organic solvents. CO₂ required for the supercritical fluid extraction process is readily available, as it is e.g. obtained as a by-product from the fermentation process or fertilizer industry. So its use as an extractant does not cause any further increase in the amount of CO₂ present in the atmosphere. There is no additional "Green House effect" from using CO₂ as the SCF solvent. Moreover, CO₂ is readily available at low cost.

The method of the present invention

The system used for carrying out the method of the present invention comprises at least one extractor, one precipitator and tubes connecting the extractor and the precipitator. Furthermore, the system should comprise a device, such as a pump, which maintains constant flow-rate and pressure of the supercritical fluid within the system. All components need to be combined in a closed system. The SCF passes through the extractor, leaves the extractor through at least one outlet (of the extractor) into the tubes and moves on to the precipitator through at least one inlet (of the precipitator). Upon expansion in the precipitator, the expanded gas (former SCF) leaves the precipitator through at least one outlet (of the precipitator) and passes back to the extractor through tubes. Before entering the extractor again through at least one inlet (of the extractor), the gas needs to be compressed to transfer it back into its supercritical state. Valves may serve to enable decoupling of the different components (e.g. extractor, precipitator) such that the extractor and/or precipitator can be isolated from the closed system to allow opening of these components without subjecting the complete system to ambient conditions. Optionally, the system may further comprise coolers (e.g. to cool the precipitator and/or to cool the gas within the tubes before it is transformed back to its supercritical state). The system may also comprise a heating device to maintain the supercritical fluid at the desired temperature.

To recycle the SAP particles, the SAP particles are placed in an appropriate container, herein called an extractor. At least a part of the SAP particles placed in the extractor are closely adhered to a solidified thermoplastic composition comprising at least 30 weight-% of a thermoplastic polymer based on the weight of the solidified thermoplastic composition. In most embodiments, the majority (i.e. more than 50%) of the SAP particles will be closely adhered to the solidified thermoplastic composition. However, more than 50%, e.g. more than 70% or more than 80% may be closely adhered to the solidified thermoplastic composition, or even more than 95%. To be closely adhered, it is sufficient that a relatively small part of the surface of the SAP particles
has the solidified thermoplastic composition adhered to it while the remaining surface is free of the solidified thermoplastic composition. For the present invention such SAP particles will already regarded as being contaminated with the solidified thermoplastic composition. Typically, the SAP particles will be immobilized within a fibrous network of the solidified thermoplastic composition.

As the name already indicates, the extractor, wherein the contaminated SAP particles are placed, serves as an extraction vessel. The extractor may e.g. be an autoclave. The extractor needs to be hermetically sealable against ambient air to allow the appropriate pressure and temperature to build up.

The material placed in the extractor may be only the SAP particles to which solidified thermoplastic composition is adhered. However, it has been surprisingly found that the method of the present invention can also be carried out when the SAP particles with the closely adhered solidified thermoplastic composition are comprised within an absorbent core of an absorbent article while being subjected to the method of the present invention. The absorbent core may further to the contaminated SAP particles comprise nonwoven webs, airfelt and/or other liquid absorbing materials, such as absorbent foams. In one embodiment, the absorbent core comprises the contaminated SAP particles and one or more nonwoven webs.

In one embodiment, the absorbent core subjected to the method of the present invention will comprise at least 75 weight-% of SAP particles based on the total weight of the absorbent core.

In another embodiment, the absorbent core will comprise at least 80 weight-% of SAP particles based on the total weight of the absorbent core. In still another embodiment, the absorbent core will comprise at least 90 weight-% of SAP particles based on the total weight of the absorbent core.

Further, in one embodiment, the absorbent core subjected to the method of the present invention will comprise less than 8 weight-% of the solidified thermoplastic composition based on the total weight of the absorbent core. In another embodiment, the absorbent core will comprise less than 6 weight-% of the solidified thermoplastic composition based on the total weight of the absorbent core. In still another embodiment, the absorbent core will comprise less than 5 weight-% of the solidified thermoplastic composition based on the total weight of the absorbent core.
Alternatively, the material subjected to the method of the present invention comprises further to the absorbent cores with the contaminated SAP particles also other components of an absorbent article, such as the acquisition system.

Moreover, the inventors of the present invention have found that complete absorbent articles, e.g. complete diapers, can be subjected to the method of the present invention. This eliminates the need to retrieve the absorbent cores from the absorbent articles before subjecting them to the method of the present invention. Thus, in a still further embodiment, complete absorbent articles, such as disposable diapers, training pants or sanitary napkins, are subjected to the method of the present invention. These absorbent articles comprise the SAP particles to which the solidified thermoplastic composition is adhered. The SAP particles are comprised inside the absorbent articles, i.e. the SAP particles with the adhered solidified thermoplastic composition are surrounded by other materials, such as nonwoven webs, films and/or airfelt. The complete absorbent articles may also comprise inks which have been used to provide a print on portions of the absorbent article (e.g. on the backsheet or the landing zone).

In one embodiment, the disposable absorbent article subjected to the method of the present invention comprises at least 25 weight-% of SAP particles based on the total weight of the disposable absorbent article. In another embodiment, the disposable absorbent article comprises at least 30 weight-% of SAP particles based on the total weight of the disposable absorbent article.

Further, in one embodiment, the disposable absorbent article subjected to the method of the present invention will comprise less than 3 weight-% of the solidified thermoplastic composition based on the total weight of the disposable absorbent article. In another embodiment, the disposable absorbent article will comprise less than 2.5 weight-% of the solidified thermoplastic composition based on the total weight of the disposable absorbent article.

After the SAP particles with the adhered solidified thermoplastic composition have been placed in the extractor, at least one inlet and at least one outlet is connected to the extractor and the extractor is hermetically sealed against ambient air.

Supercritical fluid, such as supercritical carbon dioxide, is fed into the system and enters the extractor through the at least one inlet line. While passing through the extractor, the supercritical fluid also passes through the material comprised in the extractor.
Due to its low viscosity and high diffusion coefficient, the supercritical fluid can easily penetrate the material placed in the extractor, thus coming into close contact with the SAP particles to which the solidified thermoplastic composition is adhered, even if the SAP particles are comprised in an absorbent article. Passing though the material, the supercritical fluid extracts the solidified thermoplastic composition, which thereby is removed from the SAP particles little by little.

The supercritical fluid together with the extracted solidified thermoplastic composition leaves the extractor through the at least one outlet and passes through tubes into the precipitator. In the precipitator the supercritical fluid is allowed to expand to conditions below the supercritical temperature and pressure, e.g. supercritical carbon dioxide and/or propane is/are transferred back to the gaseous state. Upon expansion of the supercritical fluid, the extracted solidified thermoplastic composition precipitates in the precipitation vessel, as the gaseous carbon dioxide and/or propane can no longer serve as an extraction medium.

However, the chemical configuration of the solidified thermoplastic composition will most likely not be the same as the chemical configuration, which the solidified thermoplastic composition had while it was adhered to the SAP particles. For example, if the solidified thermoplastic composition is not a pure chemical compound but rather a mixture of different components, the different components may have at least partly been separated from each other upon extraction, possibly resulting in part of the formerly solidified thermoplastic composition being now in a liquid state (e.g. oil, if present).

Upon precipitation of the extracted material in the precipitator, the carbon dioxide and/or propane is regenerated, i.e. not "loaded" with the extracted material any longer. The carbon dioxide and/or propane leave the precipitator through at least one outlet and enter into the pipe leads it back to the precipitator. At its way back, the gas is compressed again until it has reached its supercritical state. Thereupon, the supercritical fluid can again enter the extractor wherein the SAP particles with the adhered solidified thermoplastic composition have been placed.

As has been explained, the method of the present invention can be carried out in a closed system, where the carbon dioxide and/or the propane can be at least partially recycled and be re-used for many cycles, passing through the extractor with the contaminated SAP particles again and again.

\textit{Pressure and temperature:}
As higher pressures are more difficult to facilitate, relatively low pressures are desirable from a process engineering and cost standpoint. However, it has been found that a relatively high pressure may make the method of the invention more efficient, possibly leading to a shorter time, during which the contaminated SAP particles have to be subjected to the supercritical fluid in order to remobilize SAP particles and free them from the solidified thermoplastic composition. Higher pressure means that more molecules of the supercritical fluid are present per given volume, thus enabling faster extraction. In the method of the present invention, the supercritical fluid may be under a pressure of from 100 bar to 600 bar, or from 150 bar to 400 bar or from 200 bar to 350 bar.

As carbon dioxide reaches its supercritical state at a pressure of 73.8 bar and at a temperature of 31.1°C, the temperature of the supercritical fluid should be at least 40°C. Temperatures below 40°C may result in areas within the system having a temperature which is at least temporarily below the supercritical temperature of 31.1°C. Thus, to ensure process stability, the temperature should be at least 40°C. However, if propane is used as supercritical fluid (or a mixture which predominantly consists of propane), it may be desirable to have a temperature of at least 45°C due to the slightly higher critical temperature of propane compared to carbon dioxide. Generally, it is desirable that the temperature of the supercritical fluid is from 40°C to 100°C, preferably from 40°C to 75°C and more preferably from 40°C to 60°C. Temperatures above 100°C do not only increase the cost for running the system, but they may also have an adverse effect on the SAP particles, e.g. yellowing of the SAP particles.

If the contaminated SAP particles subjected to the method of the invention comprise odour control compounds, such as odour control particles comprising percarbonate and tetra acetyl ethylene diamine, the odour control compound may deteriorate at elevated temperatures. For example, percarbonate may decompose, setting free hydrogen peroxide. However, for the present invention it is not critical whether the odor control compound decomposes and is inactivated upon being subjected to the present invention, as long as the SAP particles are not adversely affected.

If it is desired to maintain activity of the odor control compounds, the temperature, upon which the odor control compounds are deactivated can be determined and the temperature, at which the contaminated SAP particles comprising the odor control compounds, are subjected to supercritical fluid, can be chosen accordingly to avoid deactivation (as long as no temperature
below 40°C is required - in these embodiments the activity of the odor control compound cannot
be maintained). For example, percarbonate should not be subjected to temperatures above 60°C
in order to avoid decomposition and liberation of hydrogen peroxide.

Amount of supercritical fluid and time:

The supercritical fluid is provided to the extractor comprising the contaminated SAP particles as
a continuous stream. The stream enters the extractor through the at least one inlet and leaves the
extractor through the at least one outlet.

Generally, it is desirable that the amount of supercritical fluid is many times the amount of
solidified thermoplastic composition, which is to be extracted in order to separate the solidified
thermoplastic composition from the SAP particles.

The amount which is actually needed *inter alia* depends on whether or not co-solvents are
applied besides the carbon dioxide and/or propane. If co-solvents are used, lower amounts of
supercritical fluid may be sufficient. If pure carbon dioxide is used, the amount of supercritical
fluid to flow through the extractor is desirable from 50 time to 500 times (by weight), more
preferably from 70 times to 150 times (by weight) the amount of the solidified thermoplastic
composition.

If pure propane or a mixture of (only) carbon dioxide and propane (i.e. with no additional co-
 solvent) is used, the amount of supercritical fluid to flow through the extractor is desirable from
40 time to 300 times (by weight), more preferably from 50 times to 100 times (by weight) the
amount of the solidified thermoplastic composition. If a mixture of carbon dioxide and propane
is used, it is preferred that the mixture consists of from 60 weight-% to 95 weight-% of carbon
dioxide and from 5 weight-% to 40 weight-% of propane based on the total weight of
supercritical fluid, more preferably of from 75 weight-% to 95 weight-% of carbon dioxide and
from 5 weight-% to 25 weight-% of propane.

If co-solvents are used, it may be sufficient to use from 20 times to 120 times (by weight) the
amount of supercritical fluid to flow through the extractor compared to the amount of solidified
thermoplastic composition, preferably from 20 times to 80 times (by weight) and more
preferably from 20 times to 60 times.
The time, for which the contaminated SAP particles have to be subjected to the supercritical fluid treatment in order to separate the SAP particles from the solidified thermoplastic composition will inter alia depend on the pressure of the supercritical fluid, on the flow rate and on which supercritical fluid is used.

The contaminated SAP particles may generally be subjected to the supercritical fluid for from 15 minutes to 180 minutes, or from 30 minutes to 90 minutes.

The method of the present invention may be carried out in a batch process or in a quasi-continuous process. A "batch process" as used herein means that a given amount of SAP particles with adhered solidified thermoplastic composition is placed in the extractor and treated with supercritical fluid until the SAP particles have been completely separated from the solidified thermoplastic composition. Thereafter, the SAP particles (and other parts of the disposable absorbent articles / complete absorbent articles, if present) are taken out of the extractor and a new amount of SAP particles with adhere solidified thermoplastic composition (i.e. a new batch) is placed in the extractor. Also, it may be necessary to empty the precipitator, if there is too much precipitated material resulting from extraction of the solidified thermoplastic composition. However, the present invention also encompasses methods wherein the SAP particles are treated in a quasi-continuous process. "Quasi-continuous" as used herein means that more than one extractor is comprised by the system. The system is set up appropriately to allow one or more extractors to be disengaged from the system such that they can be opened while leaving the remaining system -with the other extractor(s)- unaffected.

*Supercritical fluid used in the method of the present invention:*

For the present invention, the supercritical fluid will comprise carbon dioxide, propane or mixtures thereof. Both, carbon dioxide and propane are non-polar solvents.

In general the extractability of the compounds with a SCF depends on the occurrence of the individual functional groups in these compounds, their molecular weights and polarity.

Many non-polar organic solvents (such as carbon dioxide or propane) are able to dissolve polar substances. When comparing a polar and non-polar molecule with similar molar masses, the polar molecule generally has a higher boiling point, because of the dipole-dipole interaction
between polar molecules. The most common form of such polar interaction is the hydrogen bond, which is also known as the H-bond.

In order to further improve the solving power of the SCF used in the method of the present invention, one or more co-solvent may be used in addition to the carbon dioxide, propane or carbon dioxide / propane mixture. Thus, in one embodiment of the present invention, the SCF comprises one or more co-solvents in addition to the carbon dioxide, propane or carbon dioxide / propane mixture. Also, in one embodiment of the present invention, the SCF is a mixture of carbon dioxide and one or more co-solvents. In an alternative embodiment of the present invention, the SCF consists of carbon dioxide.

The co-solvents for use in the method of the present invention and comprised by the SCF, which is provided to the extractor may be selected from the group consisting of ethanol, ethyl acetate, butane, butyl acetate, acetone, nitrous oxide, carbon dioxide, nitrogen, water, and mixtures thereof. The amount of the co-solvent (or the total amount of co-solvents, if more than one co-solvent is used) comprised by the SCF which is provided to the extractor may be from 0.1 weight-% to 40 weight-%, preferably from 0.5 weight-% to 30 weight-%, and more preferably from 1 weight-% to 20 weight-% based on the total weight of supercritical fluid. All supercritical fluids are completely miscible with each other so for a mixture a single phase can be guaranteed if the critical point of the mixture is exceeded.

It has been found that it is not only possible to carry out the method of the present invention with complete absorbent cores and even with complete absorbent articles comprising the absorbent cores. Surprisingly, it has been further found that the method may even work better if complete absorbent cores or complete or at least partially assembled absorbent articles are used.

Without wishing to be bound by theory, it is believed that one reason for this improvement is that certain compounds comprised by the absorbent core or absorbent article act as co-solvents. For example, absorbent articles typically comprise adhesives which are used to bond the different webs and materials of the article to each other. Moreover, many absorbent articles have elastic members, which may comprise substances useful as co-solvents. Other compounds, which often find use in absorbent articles, are surfactants (e.g. to render the topsheet hydrophilic). Such surfactants may also work as co-solvents for the method of the invention. It should be understood that for the present invention these "inherent co-solvents" are not taken into consideration when referring to co-solvents, which are used in the supercritical fluid
(especially when determining preferred compounds and amounts of co-solvents). Instead, when referring to co-solvents, only those compounds are referred to, which are consciously and in a controlled manner, mixed into the supercritical fluid.

The SCF does not only penetrate through the contaminated SAP particles but penetrates through the absorbent article as a whole. Thus, not only the solidified thermoplastic composition is extracted, but also other compounds, such as adhesives used in other areas of the article, surfactants, inks and possible elastifiers in elastic elements are affected by extraction. This can be easily demonstrated by the fact, that the absorbent article is -at least to a certain degree- demounted and deconstructed into its individual elements, such as topsheet, backsheet, tapes etc., which have formerly been assembled into the absorbent article.

Thus, as other compounds are extracted, they are set free and are comprised in the stream of SCF, passing with the SCF through the extractor, thereby also coming into contact with the contaminated SAP particles. Contrary to supercritical CO2 and propane, many of these compounds are polar substances, which may support extraction of the solidified thermoplastic composition, especially if the solidified thermoplastic composition comprises substances (i.e. substances additionally to the polymer of the solidified thermoplastic composition), which are rather polar. However, rather non-polar compounds extracted from the absorbent core or absorbent article of course also have the potential of a co-solvent.

**Superabsorbent polymer particles**

The SAP particles may be of numerous shapes. The term "particles" refers to granules, fibers, flakes, spheres, powders, platelets and other shapes and forms known to persons skilled in the art of SAP particles. E.g. the particles can be in the form of granules or beads, having a particle size from about 10 \( \mu \text{m} \) to about 1000 \( \mu \text{m} \), preferably from about 100 \( \mu \text{m} \) to about 1000 \( \mu \text{m} \), even more preferably from about 150 \( \mu \text{m} \) to about 850 \( \mu \text{m} \) and most preferably from about 150 \( \mu \text{m} \) to about 500 \( \mu \text{m} \). In another embodiment, the SAP particles can be in the shape of fibers, i.e. elongated, acicular SAP particles. In those embodiments, the SAP fibers have a minor dimension (i.e. diameter of the fiber) of less than about 1 mm, usually less than about 500 \( \mu \text{m} \), and preferably less than 250 \( \mu \text{m} \) down to 50 \( \mu \text{m} \). The length of the fibers is preferably about 3 mm to about 100 mm. The fibers can also be in the form of a long filament that can be woven.
Preferred SAP particles of the present invention are spherical-like particles. According to the present invention and in contrast to fibers, "spherical-like particles" have a longest and a smallest dimension with a particulate ratio of longest to smallest particle dimension in the range of 1-5, where a value of 1 would equate a perfectly spherical particle and 5 would allow for some deviation from such a spherical particle.

The SAP particles useful in the present invention include a variety of water-insoluble, but water-swellable polymers capable of absorbing large quantities of fluids. Such polymers materials are generally known in the art and include all those well-known polymers used or deemed useful in the context of disposable absorbent article technology.

Preferred polymer materials for use in making SAP particles are slightly network cross linked polymers of partially neutralized polyacrylic acids and starch derivatives thereof. Starch-based SAP particles are also encompassed in the present invention. Preferably, the SAP particles comprise from 25% to 95% by weight, more preferably from 50% to 80% by weight, neutralized, slightly network cross-linked, polyacrylic acid. Network cross-linking renders the polymer substantially water-insoluble and, in part, determines the absorptive capacity and extractable polymer content characteristics of the hydrogel-forming absorbent polymers.

While the SAP is preferably of one type (i.e., homogeneous), mixtures of polymers can also be used in the present invention. The SAP particles can also comprise mixtures with low levels of one or more additives, such as for example powdered silica, surfactants, adhesive, binders, and the like. Furthermore, the SAP particles can comprise a gradient in particle size or can comprise a certain range of particle size.

Many of the formerly known SAP particles exhibited gel blocking. "Gel blocking" occurs when particles of the SAP are wetted and the particles swell so as to inhibit fluid transmission to other zones or regions of the absorbent structure. Wetting of these other regions of the absorbent core therefore takes place via a very slow diffusion process. In practical terms, this means acquisition of fluids by the absorbent structure is much slower than the rate at which fluids are discharged, especially in gush situations. Leakage from the absorbent article can take place well before the particles of SAP in the absorbent core are even close to being fully saturated or before the fluid can diffuse or wick past the "blocking" particles into the rest of the absorbent core.
One commonly applied way to reduce gel blocking is to make the particles stiffer, which enables the SAP particles to retain their original shape thus creating or maintaining void spaces between the particles. A well-known method to increase stiffness is to covalently cross-link the carboxyl groups exposed on the surface of the SAP particles. This method is commonly referred to as surface cross-linking.

Solidified thermoplastic composition

The solidified thermoplastic composition of the present invention, which is adhered to the SAP particles, may be an adhesive, preferably a hot melt adhesive. The adhesive may have been initially applied to immobilize the SAP particles. Such immobilization of the SAP particles may generally be required in embodiments, wherein the absorbent core of a disposable absorbent article comprises little (e.g. less than 10% by total weight of the absorbent material) of airfelt or wherein the absorbent core comprises no airfelt at all. Typically, the SAP particles are laid down on a nonwoven carrier web, where they are immobilized to ensure they stay in place during manufacture, storage and use of the absorbent article.

It should be understood that the solidified thermoplastic composition may not be in its solidified state during application onto the SAP particles but the solidified thermoplastic composition may be heated up to a temperature where it is semi-fluid or fluid in order to facilitate application on the SAP particles. Thus, a solidified thermoplastic composition in the present invention refers to a composition which is solidified at room temperature. Generally, the solidified thermoplastic composition in the present invention should also be solid at and slightly above in-use temperatures of absorbent articles, i.e. at a temperature up to about 40°C (even though parts of the absorbent article will have lower in-use temperatures). The solidified thermoplastic composition readily immobilizes the SAP particles and holds them in place.

The solidified thermoplastic composition may at least partly be applied in fibrous form onto the SAP particles (e.g. by spraying) while the solidified thermoplastic composition has been transferred into a semi-fluid or fluid state (upon heating) to form a kind of a fibrous adhesive-network around the SAP particles. If the solidified thermoplastic composition is applied in fibrous form, the fibers will typically have an average thickness of about 1 to about 50 micrometers or about 1 to about 35 micrometers and an average length of about 5 mm to about 50 mm or about 5 mm to about 30 mm.
The solidified thermoplastic composition may comprise a single thermoplastic polymer or a blend of thermoplastic polymers. The thermoplastic polymer(s) may have a softening point, as determined by the ASTM Method D-36-95 "Ring and Ball", in the range between 50 °C and 300 °C, The thermoplastic polymer(s) preferably have a molecular weight (weight average Mw in Dalton) of more than 10,000 and a glass transition temperature (Tg) below room temperature (25 °C) or -6°C < Tg < 16°C. Typical concentrations of the thermoplastic polymer(s) in the solidified thermoplastic composition are in the range of 30 weight-% to about 50 weight-% by weight, preferably 30 weight-% to about 40 weight-% by weight. Preferably, the thermoplastic polymers of the solidified thermoplastic composition are immiscible with water (in amounts above 5 % by weight of the solidified thermoplastic composition).

Exemplary thermoplastic polymers are block copolymers -such as styrenic block copolymers- including A-B-A triblock structures, A-B diblock structures and (A- B)n radial block copolymer structures wherein the A blocks are non-elastomeric polymer blocks, typically comprising polystyrene, and the B blocks are unsaturated conjugated diene or (partly) hydrogenated versions of such. The B block is typically isoprene, butadiene, ethylene/butylene (hydrogenated butadiene), ethylene/propylene (hydrogenated isoprene), and mixtures thereof. Preferably, the polymer in the solidified thermoplastic composition is a styrene-isoprene-styrene (SIS) block copolymer, a styrene-butadiene-styrene (SBS) block copolymer or mixtures thereof. Styrene-block-copolymers are often used in adhesives which find application in absorbent articles. In embodiments of the present invention wherein the solidified thermoplastic composition comprises more than one polymer, the solid composition preferably comprises at least 30 weight-% of a styrene-block-copolymer, such as a styrene isoprene block copolymer, based on the total weight of the solidified thermoplastic composition.

Other suitable thermoplastic polymers that may be employed are metallocene polyolefins, which are ethylene polymers prepared using single-site or metallocene catalysts. Therein, at least one comonomer can be polymerized with ethylene to make a copolymer, terpolymer or higher order polymer. Also applicable are amorphous polyolefins or amorphous polyalphaolefins (APAO) which are homopolymers, copolymers or terpolymers of C2 to C8 alpha olefins. Besides the at least 30 weight-% of the thermoplastic polymer, the solidified thermoplastic composition may further comprise tackifying resins and/or oils. Furthermore, the solidified thermoplastic composition may comprise relatively small amounts of additives, such as antioxidants, fillers (e.g. sand and/or silicates) and/or surfactants.
The amount of tackifying resins, if present in the solidified thermoplastic composition, will typically be from 1 weight-% to 60 weight-%, preferably from 5 weight-% to 40 weight-% and more preferably from 5 weight-% to 30 weight-% based on the weight of the solidified thermoplastic composition. The amount of oils, if present in the solidified thermoplastic composition, will typically be from 1 weight-% to 40 weight-%, preferably from 5 weight-% to 30 weight-%, or from 5 weight-% to 20 weight-% based on the weight of the solidified thermoplastic composition. The solidified thermoplastic composition of the present invention may comprise more than one oil (i.e. different oils) and/or may comprise more than one tackifying resin (i.e. different tackifying resins). The overall amount of additives, if used in the solidified thermoplastic composition, may not more than 15 weight-%, preferably not more than 10 weight-%, more preferably not more than 8 weight-% based on the weight of the solidified thermoplastic composition.

A resin for the present invention is a hydrocarbon secretion of many plants, particularly coniferous trees, e.g. rosin esters (which are often used as tackifiers). The term resin herein is also used for synthetic resins of similar properties. Synthetic resins are materials with similar properties to natural resins—viscous liquids capable of hardening. They are typically manufactured by esterification or soaping of organic compounds. The classic variety is epoxy resin. The tackifying resin of the solidified thermoplastic composition has typically a weight average Mw (in Dalton) below 5,000. The Tg will usually be above room temperature. An oil for the present invention is any substance that is liquid at ambient temperatures and is hydrophobic but soluble in organic solvents. Oils have a high carbon and hydrogen content and are non-polar substances. Oils useful for the solidified thermoplastic composition of the present invention are mineral oils. In one embodiment, the oil is petrolatum oil, for example paraffinic oil, napthenic or mixtures thereof. The oil may have a low weight average Mw (in Dalton) of less than 1,000. The Tg will preferably be below room temperature (25°C).

Examples for solidified thermoplastic compositions of the present invention are the following hot melt adhesives: Bostik Findley H2401, an elastic adhesive; Lunatack D 3155 B Zeropack and D 3166 Zeropack from H.B. Fuller; HL 1358 from H.B. Fuller; Dispomelt (DM526 and DM519 A) sold by National Starch.
One example of an absorbent article comprising an absorbent core with SAP particles, which have been immobilized with a solidified thermoplastic composition of the present invention is Pampers Magic Nicker marketed in India.

All patents and patent applications (including any patents which issue thereon) assigned to the Procter & Gamble Company referred to herein are hereby incorporated by reference to the extent that it is consistent herewith.

The dimensions and values disclosed herein are not to be understood as being strictly limited to the exact numerical values recited. Instead, unless otherwise specified, each such dimension is intended to mean both the recited value and a functionally equivalent range surrounding that value. For example, a dimension disclosed as "40 mm" is intended to mean "about 40 mm."

All documents cited in the Detailed Description of the Invention are, in relevant part, incorporated herein by reference; the citation of any document is not to be construed as an admission that it is prior art with respect to the present invention. To the extent that any meaning or definition of a term in this document conflicts with any meaning or definition of the same term in a document incorporated by reference, the meaning or definition assigned to that term in this document shall govern.

While particular embodiments of the present invention have been illustrated and described, it would be obvious to those skilled in the art that various other changes and modifications can be made without departing from the spirit and scope of the invention. It is therefore intended to cover in the appended claims all such changes and modifications that are within the scope of this invention.
What is claimed is:

1. Method for separating superabsorbent polymer particles from a solidified thermoplastic composition comprising at least 30 weight-% of a thermoplastic polymer based on the weight of the solidified thermoplastic composition, the method comprising the steps of:
   a) providing agglomerates of the superabsorbent polymer particles and the solidified thermoplastic composition, wherein at least a part of the superabsorbent polymer particles are adhered to at least a part of the solidified thermoplastic composition,
   b) subjecting the agglomerates to a supercritical fluid comprising carbon dioxide, propane or mixtures thereof.

2. Method according to claim 1, wherein the supercritical fluid further comprises one or more co-solvents.

3. Method according to claim 2, wherein the co-solvents are selected from the group consisting of ethanol, ethyl acetate, butane, butyl acetate, acetone, nitrous oxide, carbon dioxide, nitrogen, water, and mixtures thereof.

4. Method according to claim 2 or 3, wherein the total amount of the one or more co-solvent is from 0.1 weight-% to 40 weight-%, preferably from 0.5 weight-% to 30 weight-%, and more preferably from 1 weight-% to 20 weight-% based on the total weight of supercritical fluid.

5. Method according to any of the preceding claims, wherein the solidified thermoplastic composition further comprises from 1 weight-% to 60 weight-%, preferably from 5 weight-% to 40 weight-% of resin based on the weight of the solidified thermoplastic composition.

6. Method according to any of the preceding claims, wherein the solidified thermoplastic composition further comprises from 1 weight-% to 30 weight-%, preferably from 5 weight-% to 30 weight-% of oil based on the weight of the solidified thermoplastic composition.

7. Method according to any of the preceding claims, wherein the solidified thermoplastic composition further comprises additives selected from the group of antioxidants, sand, silicone and surfactant, and wherein the overall amount of additives is not more than 15 weight-%, preferably not more than 10 weight-%, more preferably not more than 8 weight-% based on the weight of the solidified thermoplastic composition.
8. Method according to any of the preceding claims, wherein the agglomerates are subjected to a continuous stream of supercritical fluid.

9. Method according to claim 8, wherein the supercritical fluid is recycled after it has been subjected to the agglomerates.

10. Method according to any of the preceding claims, wherein the agglomerates are comprised in complete disposable absorbent articles or parts of absorbent articles, while being subjected to the supercritical fluid.

11. Method according to claim 10, wherein the absorbent articles are diapers, training pants or sanitary napkins.

12. Method according to claim 10 or 11, wherein the parts of the absorbent articles are absorbent cores.

13. Method according to claim 12, wherein the absorbent cores further to the agglomerates comprise one or more nonwoven webs.

14. Use of supercritical fluid for separating superabsorbent polymer particles from a solidified thermoplastic composition comprising at least 30% of a thermoplastic polymer, wherein at least a part of the superabsorbent polymer particles are adhered to at least a part of the composition and wherein the supercritical fluid comprises carbon dioxide, propane or mixtures thereof.

15. Superabsorbent polymer particles obtained by a method according to any of claims 1 to 14.
INTERNATIONAL SEARCH REPORT

A. CLASSIFICATION OF SUBJECT MATTER
INV. B29B17/02
ADD. A61F13/58
According to International Patent Classification (IPC) or both national classification and IPC

B. FIELDS SEARCHED
Minimum documentation searched (classification system followed by classification symbols)
B29B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)
EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

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See patent family annex.

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Kujat, Christian
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