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<b>(21) International Application Number:</b> PCT/US93/07823 <b>(22) International Filing Date:</b> 25 August 1993 (25.08.93)  <b>(30) Priority data:</b> 07/937,037                      31 August 1992 (31.08.92)                      US  <b>(71) Applicant:</b> E.I. DU PONT DE NEMOURS AND COMPANY [US/US]; 1007 Market Street, Wilmington, DE 19898 (US).  <b>(72) Inventors:</b> RODINI, David, Joseph ; 1401 Lady Ashley Court, Midlothian, VA 23113 (US). HOFFMAN, Donald, Edmund ; 2 Alton Court, Newark, DE 19711-7602 (US).  <b>(74) Agents:</b> SCHWARTZ, Sol et al.; E.I. du Pont de Nemours and Company, Legal/Patent Records Center, 1007 Market Street, Wilmington, DE 19898 (US).		<b>(81) Designated States:</b> AU, JP, KR, RU, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE).  <b>Published</b> <i>With international search report. Before the expiration of the time limit for amending the claims and to be republished in the event of the receipt of amendments.</i>
<b>(54) Title:</b> PROCESS FOR MAKING SPUN YARN  <b>(57) Abstract</b>  Spun yarns are made at high speeds of up to 220 meters per minute, using spinning techniques in which air is used to twist the fibers of a three component blend, one component of which consists of staple fibers made from electrically conductive filaments having a denier no greater than 2.5 times the denier of the filaments of the other components.		

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## Title

Process for Making Spun YarnBackground of the Invention

The field of art to which this invention  
5 pertains is spun yarn. The invention is more specifically  
directed to a process for making such yarn from a  
three-component blend of staple fibers using high speed,  
air spinning techniques with spinning speeds in excess of  
70 meters per minute. In a preferred embodiment these  
10 speeds can range from 150 to 220 meters per minute.

The fiber blend used in the process is formed  
from a plurality of selected filaments. One component of  
the blend comprises staple fibers made from filaments  
having an electrically conductive carbon black core and a  
15 sheath of non-conductive polymer. The other two  
components, which are heat-resistant, are preferably  
formed from filaments of poly(m-phenylene isophthalamide)  
and of poly(p-phenylene terephthalamide).

The deniers of the electrically conductive  
20 sheath core filaments are preferably no greater than 2.5  
times the deniers of the other filaments. This helps  
prevent or lessens their migration to the surface of the  
spun yarn during the spinning operation and thereby  
improves the appearance of the yarn and of the fabrics  
25 woven from such yarn.

Summary of the Invention

In a preferred process of this invention, staple  
fibers formed from electrically conductive first component  
30 filaments having a carbon black core are blended with  
heat-resistant staple fibers, prior to spinning, to impart  
desired antistatic properties to a fabric or garment made  
from such fibers.

In this process, the blend is first formed into  
35 a sliver which is processed into a spun yarn using high  
speed spinning techniques in which a fluid is used to  
twist the fibers. The most convenient fluid is air,  
however, other fluids, such as nitrogen could be used.

The appearance of the fabric made from these spun yarns is improved provided the denier per filament of the electrically conductive filaments is no greater than about 2.5 times the denier per filament of the filaments used to form the heat-resistant fibers.

Preferably the blend consists of at least two other components, in addition to the first component, electrically conductive fibers. Preferably these components are heat-resistant fibers formed from filaments of poly(m-phenylene isophthalamide) and poly(p-phenylene terephthalamide).

In a preferred embodiment, the denier per filament of the first component filaments used to form electrically conductive staple fibers is about 3.0. The denier per filament of the second component filaments of the poly(p-phenylene terephthalamide) is about 1.5; and, the denier per filament of the third component filaments of poly(m-phenylene isophthalamide) is about 1.7.

The sliver formed from the three-component blend is spun at high speeds in excess of 70 meters per minute, and, preferably, is spun at speeds from 150 to 220 meters per minute. The preferred air spinning technique used to twist the fibers is air-jet spinning.

More specifically, this invention is a process for making a three-component spun yarn comprising the steps of:

forming a first tow from a plurality of heat-resistant filaments;

forming a second tow from a plurality of heat-resistant filaments and a plurality of filaments composed of an electrically conductive carbon black core with a sheath of a non-conductive polymer;

and wherein the denier of the filaments in the tow having the electrically conductive filaments is no greater than 2.5 times the denier of the heat-resistant filaments from either tow;

crimping these tows separately, wherein each tow has between 3 and 6 crimps per centimeter (7.6 to 15.2 crimps per inch);

combining the two crimped tows and cutting the tows to form a three-component blend of staple fibers;

carding and forming a sliver of the three-component blend of staple fibers;

spinning the sliver into a spun yarn with spinning techniques which use air or other fluids to twist the fibers.

In another embodiment, this invention is a process for making spun yarn including the steps of:

forming a plurality of first component filaments each having an electrically conductive carbon black core and a sheath of a non-conductive polymer into a first component yarn;

forming a plurality of second component filaments of non-conductive poly(p-phenylene terephthalamide) into a second component yarn;

forming a plurality of third component filaments of poly(m-phenylene isophthalamide) into a third component yarn;

and wherein the denier of the filaments of the first component yarn is no greater than about 2.5 times the denier of the filaments of the second and third yarns;

combining the first and second component yarns into a first tow;

crimping the first tow, wherein such tow has between 3 and 6 crimps per centimeter (7.6 to 15.2 crimps per inch);

forming the third component yarn into a second tow;

crimping the second tow, wherein such tow has between 3 and 6 crimps per centimeter (7.6 to 15.2 crimps per inch);

combining the crimped first and second tows; cutting the combined tows to form a three-component blend of staple fibers;

forming the blend of staple fibers into a  
sliver;

spinning the sliver using air spinning  
techniques to twist the fibers to form a spun yarn  
5 suitable for use in making permanently antistatic fabrics.

In this process the first component yarn prior  
to processing, comprises from about 1 to 5% of the spun  
yarn by weight;

the second component yarn from about 1 to 25% of  
10 the spun yarn by weight; and

the third component yarn comprises at least  
about 70% of the spun yarn by weight.

#### Description of the Preferred Embodiments

15 The three-component blend of staple fibers of  
this invention may be spun at high speeds into spun yarns,  
which can then be made into fabrics having permanent  
antistatic properties. Such properties are imparted to  
the fabric by the sheath-core fibers.

20 Briefly described, in the process of this  
invention, a tow of spin-oriented electrically conductive  
sheath-core filaments and non-conductive poly(p-phenylene  
terephthalamide) (PPD-T) filaments are crimped together  
and cutter blended with a separately crimped tow of non-  
25 conductive poly(m-phenylene isophthalamide) (MPD-I)  
filaments using a process as described in U. S. patents  
5,001,813 and 5,026,603 both to Rodini, the teachings of  
which are incorporated by reference herein. The blend is  
then cut into staple and processed into a sliver suitable  
30 for use in high speed spinning devices to form spun yarn.

The spinning process is preferably accomplished  
by an air-jet process similar to that generally shown and  
described in U. S. patent 4,497,167 to Nakahara et al.,  
and a teaching of the production of multiply yarns using  
35 this method is generally shown and described in U. S.  
patent 5,107,671 to Morihashi et al. The teachings of  
both of these patents are incorporated by reference  
herein.

The crimping is preferably accomplished in a stuffer box crimper of the type described in U. S. patent 2,747,233 to Hitt, the teachings of which are incorporated herein by reference.

5           The PPD-T filaments and MPD-I filaments are heat resistant, that is, they have, either by their inherent nature or by some chemical or other treatment, a limiting oxygen index (L.O.I) of at least 26.5.

          The electrically conductive sheath-core  
10 filaments which play such a significant role in this invention can be made by the process described in detail, in U. S. patent 4,612,150 to De Howitt, the teachings of which are incorporated herein by reference.

          These conductive filaments have sheaths which  
15 can contain additives such as titanium dioxide; the resultant staple fibers are generally light gray in color and are difficult to dye. Such filaments, after further processing, are capable of imparting the desired anti-static properties sought in the garment. This capability  
20 would be lost or substantially reduced if these conductive filaments in tow form were crimped alone in a stuffer box crimper prior to being processed into staple fibers. By co-crimping them with the non-conductive filaments, that capability is maintained. As so crimped, the co-crimped  
25 tow has a crimp frequency of 3 to 6 uniform crimps per centimeter. This range effectively holds the conductive and non-conductive filaments together in the stuffer box crimper and in the cutter and in subsequent processing without damaging the core of the conductive filaments.

30           It is important in the practice of the process of this invention that the deniers of the filaments be substantially of the same order. More specifically, the denier of the first component electrically conductive filaments should be no greater than about 2.5 times the  
35 deniers of the filaments of the second and third component heat-resistant filaments.

          In a preferred embodiment, the denier per filament (dpf) of the poly(p-phenylene terephthalamide)

filaments used in the instant process is about 1.5; the dpf of the poly(m-phenylene isophthalamide) filaments is about 1.7; and the dpf of the electrically conductive sheath-core filaments is about 3.0.

5           Further, preferably, the electrically conductive first yarn made from these filaments comprises from about 1 to 5% of the spun yarn. The non-conductive second component yarn comprises from about 1 to 25% of such spun yarn, and the non-conductive third component yarn  
10 comprises at least about 70% of the spun yarn.

          The deniers of the filaments is significant because filaments of different sizes and weights tend to behave differently when using the high speed air spinning techniques which play such a key role in the practice of  
15 this invention. It has been observed, for example, that in those instances where the deniers of the electrically conductive filaments are over 2.5 times the deniers of the other filaments that some of these heavier filaments are not spun in and tend to rest on the surface of any fabric  
20 made from the spun yarn. This detracts from the overall aesthetics or quality of the fabric and tends to give it a hairy or lint-like appearance or look. Further, these electrically conductive filaments, as processed, are difficult to dye, so even a subsequent dyeing operation  
25 would in most cases fail to noticeably improve the appearance of the fabric spun from such yarn.

          This appearance problem is most frequently evident when high speed air spinning techniques are used to spin the yarn. If slower, ring spinning techniques are  
30 used the deniers of the filaments is not important since the electrically conductive filaments, even those having a denier well over 2.5 times the denier of the other filaments, are effectively spun into the yarn (e.g., at ring spinning speeds from about 20 to 30 meters per  
35 minute) and do not tend to rest on the surface.

          The high speed air spinning techniques used to spin yarns in accordance with this invention are well known to the art.



Preferably, the spinning technique used is a jet spinning technique, and, more specifically, a Murata-type spinning technique is utilized. An air jet may also be used or a vortex formed to twist the yarn.

5 "Jet spinning" is a type of air spinning in which a core of generally parallel staple fibers are bound together by surface wrapping fibers which usually constitute a minor portion of the population of fibers.

"Jet spinning" processes are also sometimes  
10 referred to as "open end" spinning even though all of the fibers are not detached from the drawn sliver at the gap. For example, in Murata jet spinning a portion of the fiber is detached from the drawn sliver and then reassembled and wrapped around the undetached fibers using at least one  
15 vortex formed by air jets to form the spun yarn.

Other types of "open end" spinning include rotor spinning, which utilizes a rotor in the gap to help collect the fibers; air can be used to convey and twist the fibers while they are in the gap.

20 In air jet spinning, speeds from about 150 to 220 meter per minute are obtainable in producing acceptable spun yarns in accordance with this invention. Other air spinning techniques operating at speeds in excess of 70 meters per minute are also usable in  
25 obtaining quality yarn having good visual aesthetics.

#### Example 1

A blended tow of undrawn, spin-oriented electrically conductive sheath-core filaments and  
30 non-conductive poly(p-phenylene terephthalamide) (PPD-T) filaments were crimped together and cutter blended with a separately crimped tow of non-conductive poly(m-phenylene isophthalamide) (MPD-I) filaments using a process as described in U. S. patents 5,001,813 and 5,026,603, both  
35 to Rodini.

The crimped tows were cut into staple fibers and blended together to form a staple fiber blend consisting of 93% MPD-I filaments, having a 1.7 denier per filament

(1.7 dpf); 5% of PPD-T filaments having a 1.5 denier per filament (1.5 dpf); and 2% electrically conductive sheath-core filaments having a 9.3 denier per filament (9.3 dpf).

The staple blend was spun into 30/2 cotton count staple yarns using a "cotton" system process which included carding the staple blend into sliver(s) using a staple processing card with a stationary top, drawing the fibers, preparation of roving, spinning of the roving into yarn using a ring spinning technique (at a speed of 25 meters per minute), followed by twisting and plying of the spun yarns.

These yarns were woven into a Plain Weave, 4.5 Oz./Sq.Yd. fabric.

The fabric was then dyed with cationic dyes. The resulting fabrics are characterized as having good visual aesthetics, i.e., the fabric does not have a "linty" or "hairy" appearance.

#### Example 2

A staple blend was prepared as in Example 1 and spun into 30/2 cotton count yarns using a No. 881 MTS (Murata Twin Spinner) air jet spinner wherein air is used to twist the fibers and the spun yarns are plied two-for-one. This equipment has the capability to spin yarns directly from a sliver and spin at considerably higher spinning speeds than those used in Example 1 (e.g., from 150 to 220 meters per minute). The speed used to prepare the sample was 190 meters per minute. The fibers, prior to spinning, were also subjected to increased carding speeds using a staple processing card with revolving flats and thus were subjected to greater mechanical action as compared to the carding processing used in Example 1.

These yarns were woven into a Plain Weave, 4.5 Oz./Sq.Yd. fabric. The fabric is then dyed with cationic dyes. The resulting fabrics are characterized as having poor visual aesthetics as characterized as a "hairy" or "linty" appearance. Analysis of the fabrics indicates that the "hairy" or "linty" look is due to the

electrically conductive sheath-core filaments protruding from or resting on the surface of the fabric.

Example 3

5           A staple blend was prepared as in Example 1, except that the electrically conductive sheath-core filaments were drawn from a 9.3 denier per filament (9.3 dpf) to approximately a 3.0 denier per filament (3 dpf).

10           This blend was spun into 30/2 cotton count yarns using the Murata yarn processing equipment and speeds as described in Example 2 and employing the same high speed air jet spinning technique. These yarns were woven into a Plain Weave, 4.5 Oz./Sq.Yd fabric.

15           The fabric is then dyed with cationic dyes. The resulting fabrics are characterized as having good visual aesthetics, that is, the surface of the fabric had little "hairy" or "linty" appearance.

What is claimed is:

1. A process for making spun yarn from a blend of staple fibers formed from a plurality of first, second and third component filaments, wherein the first component  
5 is comprised of staple fibers having an electrically conductive carbon black core and a sheath of a non-conductive polymer and the second and third components are comprised of heat-resistant staple fibers, such process including the steps of:
  - 10 forming the blend of staple fibers into a sliver, and spinning the sliver into a spun yarn using spinning techniques wherein a fluid is used to twist the fibers, the improvement wherein the denier per filament of the first component filaments is no greater than about 2.5  
15 times the denier per filament of the second and third component filaments.
  2. The process of Claim 1 wherein the denier per filament of the first component filament is about 3.0; the denier per filament of the second component filament is  
20 about 1.5; and, the denier per filament of the third component filament is about 1.7.
  3. The process of Claim 1 wherein the spinning technique used to twist the fibers is air-jet spinning.
  4. The process of Claim 1 wherein the sliver is  
25 spun at speeds in excess of 70 meters per minute.
  5. The process of Claim 1 wherein the sliver is spun at speeds from 150 to 220 meters per minute.
  6. The process of Claim 1 wherein the heat-resistant staple fibers are poly(m-phenylene  
30 isophthalamide) and poly(p-phenylene terephthalamide).
  7. A process for making a three-component spun yarn comprising the steps of:
    - forming a first tow from a plurality of heat-resistant filaments;
    - 35 forming a second tow from a plurality of heat-resistant filaments and a plurality of filaments composed of an electrically conductive carbon black core with a sheath of a non-conductive polymer;

and wherein the denier of the filaments having the electrically conductive carbon black core is no greater than 2.5 times the denier of the heat-resistant filaments from either tow;

5                crimping these tows separately, wherein each tow has between 3 and 6 crimps per centimeter (7.6 to 15.2 crimps per inch);

              combining tows and cutting the tows to form a three-component blend of staple fibers;

10              carding and forming a sliver of the three-component blend of staple fibers;

              spinning the sliver into spun yarns with spinning techniques which use a fluid to twist the fibers.

              8. A process for making a three-component spun  
15 yarn including the steps of:

              forming a plurality of first component filaments each having an electrically conductive carbon black core and a sheath of a non-conductive polymer into a first component yarn;

20              forming a plurality of second component filaments of non-conductive poly(p-phenylene terephthalamide) into a second component yarn;

              forming a plurality of third component filaments of poly(m-phenylene isophthalamide) into a third component  
25 yarn;

              and wherein the denier of the filaments of the first component yarn is no greater than about 2.5 times the deniers of the filaments of the second and third yarns;

30              combining the first and second component yarns into a first tow;

              crimping the first tow, wherein such tow has between 3 and 6 crimps per centimeter (7.6 to 15.2 crimps per inch);

35              forming the third component yarn into a second tow;

crimping the second tow, wherein such tow has between 3 and 6 crimps per centimeter (7.6 to 15.2 crimps per inch);

combining the crimped first and second tows;

5 cutting the combined tows to form a three-component blend of staple fibers;

forming the blend of staple fibers into a sliver;

10 spinning the sliver using air spinning techniques to twist the fibers to form a spun yarn suitable for use in making permanently antistatic fabrics.

9. The process of Claim 8 wherein the sliver is spun at speeds in excess of 70 meters per minute.

10. The process of Claim 8 wherein the sliver is  
15 spun at speeds from 150 to 220 meters per minute.

11. The process of Claim 8 wherein the first component yarn comprises from about 1 to 5% of the spun yarn by weight.

12. The process of Claim 8 wherein the second  
20 component yarn comprises from about 1 to 25% of the spun yarn by weight.

13. The process of Claim 8 wherein the third component yarn comprises at least about 70% of the spun yarn by weight.

25 14. The process of Claim 1 wherein the fluid used to twist the fibers is air.

15. The process of Claim 7 wherein the fluid used to twist the fibers is air.

## INTERNATIONAL SEARCH REPORT

International Application No

PCT/US 93/07823

## A. CLASSIFICATION OF SUBJECT MATTER

IPC 5 D02G3/44 D02G3/12 D01H1/115

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 5 D02G D01H

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	EP,A,0 401 739 (E.I. DU POND DE NEMOURS) 12 December 1990 see the whole document & US,A,5 001 813 (RODINI) cited in the application & US,A,5 026 603 (RODINI) cited in the application -----	1,7,8
A	US,A,4 497 167 (NAKAHARA ET AL.) 5 February 1985 cited in the application see the whole document -----	1,3,7,8, 14,15

☐ Further documents are listed in the continuation of box C.☒ Patent family members are listed in annex.

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## INTERNATIONAL SEARCH REPORT

Information on patent family members

International Application No

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Patent document cited in search report	Publication date	Patent family member(s)		Publication date
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