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(54) **A METHOD OF IMPROVING DEWATERING EFFICIENCY, INCREASING SHEET WET WEB STRENGTH, INCREASING SHEET WET STRENGTH AND ENHANCING FILLER RETENTION IN PAPERMAKING**

VERFAHREN ZUR VERBESSERUNG DER ENTWÄSSERUNGSEFFIZIENZ, ERHÖHUNG DER NASSFESTIGKEIT VON BAHNMATERIAL, ERHÖHUNG DER NASSFESTIGKEIT VON BLATTMATERIAL UND VERBESSERUNG DER FÜLLSTOFFRETENTION BEI DER PAPIERHERSTELLUNG

PROCÉDÉ POUR AMÉLIORER L'EFFICACITÉ DE DÉSHYDRATATION, AUGMENTER LA RÉSISTANCE D'UNE BANDE HUMIDE DE FEUILLE, AUGMENTER LA RÉSISTANCE À L'ÉTAT HUMIDE DE FEUILLES ET AMÉLIORER LA RÉTENTION DE CHARGE DANS LA FABRICATION DU PAPIER

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Remarks:

The file contains technical information submitted after the application was filed and not included in this specification

Description

Background of the Invention

[0001] This invention relates to a method of improving dewatering efficiency, increasing sheet wet web strength, increasing sheet wet strength and enhancing filler retention in a papermaking process. Typically in a papermaking process chemicals are added in the wet end to assist in the dewatering of the slurry, increasing retention and improving wet or dry sheet strength. The wet end of the papermaking process refers to the stage in the papermaking process where the fiber is dispersed in the water in the slurry form. The fiber-water slurry then goes through drainage and dewatering process to form a wet web. The solid content after this wet formation process is about 50%. The wet web is further dried and forms a dry sheet of paper mat. Paper mat comprises water and solids and is commonly 4 to 8% water. The solid portion of the paper mat includes fibers (typically cellulose based fibers) and also fillers.

[0002] Fillers are mineral particles that are added to paper mat during the papermaking process to enhance the resulting paper's opacity and light reflecting properties. Some examples of fillers are described in US Patent Number 7,211,608. Fillers include inorganic and organic particle or pigments used to increase the opacity or brightness, reduce the porosity, or reduce the cost of the paper or paperboard sheet. Some examples of fillers include one or more of: kaolin clay, talc, titanium dioxide, alumina trihydrate, barium sulfate, magnesium hydroxide, pigments such as calcium carbonate, and the like.

[0003] Calcium carbonate filler comes in two forms, GCC (ground calcium carbonate) and PCC (precipitated calcium carbonate). GCC is naturally occurring calcium carbonate rock and PCC is synthetically produced calcium carbonate. Because it has a greater specific surface area, PCC has greater light scattering abilities and provides better optical properties to the resulting paper. For the same reason however, PCC filled paper mat produces paper which is weaker than GCC filled paper in dry strength, wet strength and wet web strength.

[0004] Filler is generally much smaller than fiber, therefore, filler has much larger specific surface area than fiber. One of the challenges people found to increase filler content in the sheet is that high filler content decreases the efficiency of wet end chemicals, such as dewatering aids, wet web strength aids and wet strength aids. This invention is to provide novel filler pretreatment, so that it reduced the adsorption of wet end chemicals onto filler surface, therefore, increased the efficiency of wet end chemicals such as dewatering aids, wet web strength aids and wet strength aids.

[0005] Paper wet web strength is very critical for paper producers because increased paper wet web strength would increase machine runnability and reduce sheet breaks and machine down time. Paper wet web strength is a function of the number and the strength of the bonds

formed between interwoven fibers of the paper mat. Filler particles with greater surface area are more likely to become engaged to those fibers and interfere with the number and strength of those bonds. Because of its greater surface area, PCC filler interferes with those bonds more than GCC.

[0006] WO 2012/125235 relates to a method of improving dewatering efficiency, increasing sheet wet web strength, increasing sheet wet strength and enhancing filler retention in a papermaking process. The method improves the efficiency of drainage aids or wet web strength aids or wet strength aid by coating at least some of the filler particles with a material that prevents the filler materials from adhering to those additives. The drainage additive or wet web strength additive or wet strength aid holds the cellulose fibers together tightly and is not wasted on the filler particles.

[0007] US 2010/126684 provides a method of producing paper with a higher proportion of mineral filler particles than is otherwise be possible without the expected loss in paper strength. The method allows for the use of the greater amount of filler particles by coating at least some of the filler particles with a material that prevents the filler materials from adhering to a strength additive. The strength additive holds the cellulose fibers together tightly and is not wasted on the filler particles. The method is particularly effective when the filler particles are a PCC-GCC blend and when the GCC particles are coated with the adherence preventing coating.

[0008] Paper dewatering efficiency is also very critical for paper producers because decreased dewatering efficiency in wet web would increase steam demand for drying operation, reduce machine speed and production efficiency. Dewatering aids are widely used to improve dewatering efficiency for reducing energy consumption, increasing machine speed and production efficiency.

Brief Summary of the Invention

[0009] To satisfy the long-felt but unsolved needs identified above, at least one embodiment of the invention is directed towards a method of papermaking comprising filler, the method comprising the steps of: providing a blend of filler particles, at least one drainage additive or wet web strength additive or wet strength aid selected from the list of: glyoxylated Acrylamide/DADMAC copolymer, poly-vinylamine, poly-vinylamide, poly-diallylamine, and any combination thereof, and cellulose fiber stock,

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treating the filler particles with a composition of matter in the absence of cellulose fiber stock, the composition of matter being a coagulant, wherein at least some of the composition of matter is added to the filler with a rotating admixing apparatus, the apparatus having a distribution head, which is rotated by a drive with a rotational speed of 1,000 to 2,500 revolution/min, is arranged in a con-

tainer containing a slurry of the filler particles, and is associated with a rotational plane, and the distribution head has, along a circumference thereof, which surrounds a rotational axis, distributed outlets from which the composition is passed into the slurry and mixing blades,

wherein the outlets are formed as openings and the mixing blades are formed as strips extending transverse to the rotational plane and having a length equal at least half of an inner diameter of the slurry pipe;

and delivering the composition to the distribution head for admixing the composition to the filler slurry; combining the filler particles with the cellulose fiber stock,

treating the combination with the at least one wet strength aid or wet web strength additive or drainage additive, and

forming a paper mat by removing some of the water from the combination,

wherein at least 10% of the filler particles are precipitated calcium carbonate and at least 10% of the filler particles are ground calcium carbonate, the cellulose fiber stock comprises a plurality of cellulose fibers and water, and the composition of matter enhances the performance of the wet strength aid or wet web strength additive or drainage additive in the paper mat.

[0010] Additional features and advantages are described herein, and will be apparent from, the following Detailed Description.

Brief Description of the Drawings

[0011] A detailed description of the invention is hereinafter described with specific reference being made to the drawings in which:

FIG. 1 is a cross sectional illustration of a device used to feed the invention to a slurry of filler particles.

FIG. 2 is an exploded view of a cross sectional view of a device used to feed the invention to slurry of filler particles.

[0012] For the purposes of this disclosure, like reference numerals in the figures shall refer to like features unless otherwise indicated. The drawings are only an exemplification of the principles of the invention and are not intended to limit the invention to the particular embodiments illustrated.

Detailed Description of the Invention

[0013] In at least one embodiment of the invention is a method of making paper which comprises filler. In at least one embodiment of the invention the method of papermaking comprises the steps of: creating a filler blend

of PCC and GCC in which PCC comprises at least 10% by mass of the filler and GCC comprises at least 10% of the filler mass, pre-treating at least some of the filler particles with a coating that decreases the adhesion between a wet web strength additive or drainage aid or wet strength aid and the filler particles, and adding both the filler blend and the wet web strength additive or drainage aid or wet strength aid to the paper mat.

[0014] It has been known for some time that adding wet web strength additives or drainage aid or wet strength aid to paper mat increases the wet web strength of the resulting paper or enhances drainage or improves machine speed and runnability or enhance sheet wet strength. Some examples of wet strength aids, wet web strength additives and drainage aids are described in US Patents 7,125,469, 7,615,135 and 7,641,776.

[0015] Unfortunately it is not practical to add large amounts of wet strength aids or wet web strength additives or drainage aids to compensate for the weakness due to large amounts of filler in paper mat. One reason is because those additives are expensive and using large amounts of additives would result in production costs that are commercially non-viable. In addition, adding too much additive negatively affects the process of papermaking and inhibits the operability of various forms of papermaking equipment. Furthermore cellulose fibers can only adsorb a limited amount of wet strength aid or wet web strength additive or drainage aid. This imposes a limit on how much additive can be used. One reason why this is so is because wet strength aid or wet web strength additive or drainage aid tend to neutralize the anionic fiber/ filler charges and when these charges are neutralized further adsorption of those additives is inhibited.

[0016] Adding filler to the paper mat also reduces the effectiveness of the wet strength aid or wet web strength additive or drainage aid. Those additives have a tendency to coat the filler particles. The more filler particles present, the more additive coats the filler particles, and therefore there is less wet strength aid or wet web strength additive or drainage available to bind the cellulose fibers together. Because there is a maximum amount of wet strength aid or wet web strength additive or drainage that can be added, more filler has always meant less effective strength additive. This effect is more acute with PCC than GCC because PCC's higher surface area becomes more coated with the additives than GCC.

[0017] In at least one embodiment of the invention at least some of the filler particles are pre-treated with a composition of matter to at least partially prevent the adherence of wet strength aid or wet web strength additive or drainage aid to the filler particles. The pre-treatment contemplates entirely coating some or all of one or more filler particles with the composition of matter. In the alternative, the pre-treatment contemplates applying the composition of matter to only a portion of one or more of the filler particles, or completely coating some filler particles and applying the composition of matter to only a

portion of some other particles. In at least one embodiment the pre-treatment is performed with at least some of the compositions of matter described in US Patent Number 5,221,435 and in particular the cationic charge-biasing species described therein. In at least one embodiment the pre-treatment is performed with a diallyl-N,N-disubstituted ammonium halide-acrylamide copolymer described in US Patent Number 6,592,718.

[0018] While pre-treating filler particles is known in the art, prior art methods of pre-treating filler particles are not directed towards affecting the adhesion of the wet strength aid or wet web strength additive or drainage aid to the filler particles. In fact, many prior art pre-treatments increase the adhesion of the strength additive to the filler particles. For example, US Patent Number 7,211,608 describes a method of pre-treating filler particles with hydrophobic polymers. This pre-treatment however does nothing to the adhesion between the strength additive and the filler particles and merely repels water to counterbalance an excess of water absorbed by the strength additive. In contrast, the invention decreases the interactions between the wet strength aid or wet web strength additive or drainage aid and the filler particles and results in an unexpectedly huge increase in paper strength, sheet dewatering and machine runnability.

[0019] When comparing wet tensile strength of a given paper versus the percentage of filler relative to the total solid portion of the paper mat used to produce the given paper, the results clearly illustrates that sheet had very weak wet strength without addition of wet strength aid 63700 (temporary wet strength aid). Velox could significantly increase sheet wet strength. Filler pretreatment alone did not increase sheet wet strength. However, filler pretreatment further enhance Velox performance which resulted in higher sheet wet strength.

[0020] When comparing wet web tensile strength of a given paper versus the percentage of filler relative to the total solid portion of the paper mat used to produce the given paper, the relationship between increasing filler content and decreasing paper wet web strength is a linear relationship. Without the addition of Nalco dewatering aid (wet web strength aid) 63700, paper sheet had very poor wet web strength. Sheet wet web strength could be significantly improved by the using of Nalco dewatering aid 63700. Filler pretreatment alone had negligible effect on paper wet web strength. However, filler pretreatment could further boost the performance of Nalco dewatering aid 63700, and additional 20% wet strength improvement was achieved by the filler pretreatment at the lower ash content. As for the higher ash content, the performance of 63700 was boosted even higher than 20%. This is because the reduced effectiveness of the strength additive trapped against the filler particles was released by the filler pretreatment.

[0021] At least some of the fillers encompassed by this invention are well known and commercially available. They include any inorganic or organic particle or pigment used to increase the opacity or brightness, reduce the

porosity, or reduce the cost of the paper or paperboard sheet. The most common fillers are calcium carbonate and clay. However, talc, titanium dioxide, alumina trihydrate, barium sulfate, and magnesium hydroxide are also suitable fillers. Calcium carbonate includes ground calcium carbonate (GCC) in a dry or dispersed slurry form, chalk, precipitated calcium carbonate (PCC) of any morphology, and precipitated calcium carbonate in a dispersed slurry form. The dispersed slurry forms of GCC or PCC are typically produced using polyacrylic acid polymer dispersants or sodium polyphosphate dispersants. Each of these dispersants imparts a significant anionic charge to the calcium carbonate particles. Kaolin clay slurries also are dispersed using polyacrylic acid polymers or sodium polyphosphate.

[0022] In at least one embodiment, the treating composition of matter is any one of or combination of the compositions of matter described in US Patent 6,592,718. In particular, any of the AcAm/DADMAC copolymer compositions described in detail therein are suitable as the treating composition of matter. An example of an AcAm/DADMAC copolymer composition is product# Nalco -4690 from Nalco Company of Naperville, Illinois (hereinafter referred to as 4690).

[0023] The treating composition of matter is a coagulant. The coagulants encompassed in this invention are well known and commercially available. They may be inorganic or organic. Representative inorganic coagulants include alum, sodium aluminate, polyaluminum chlorides or PACs (which are also known as aluminum chlorohydroxide, aluminum hydroxide chloride, and poly-aluminum hydroxychloride), sulfated polyaluminum chlorides, polyaluminum silica sulfate, ferric sulfate, ferric chloride, and the like and blends thereof.

[0024] Some organic coagulants suitable as a treating composition of matter are formed by condensation polymerization. Examples of polymers of this type include epichlorohydrin-dimethylamine (EPI-DMA), and EPI-DMA ammonia crosslinked polymers.

[0025] Additional coagulants suitable as a treating composition of matter include polymers of ethylene dichloride and ammonia, or ethylene dichloride and dimethylamine, with or without the addition of ammonia, condensation polymers of multifunctional amines such as diethylenetriamine, tetraethylenepentamine, hexamethylenediamine and the like with ethylenedichloride and polymers made by condensation reactions such as melamine formaldehyde resins.

[0026] Additional coagulants suitable as a treating composition of matter include cationically charged vinyl addition polymers such as polymers, copolymers, and terpolymers of (meth)acrylamide, diallyl-N,N-disubstituted ammonium halide, dimethylaminoethyl methacrylate and its quaternary ammonium salts, dimethylaminoethyl acrylate and its quaternary ammonium salts, methacrylamidopropyltrimethylammonium chloride, diallylmethyl(beta-propionamido)ammonium chloride, (beta-methacryloyloxyethyl)trimethyl ammonium methylsul-

fate, quaternized polyvinylactam, vinylamine, and acrylamide or methacrylamide that has been reacted to produce the Mannich or quaternary Mannich derivatives. Preferable quaternary ammonium salts may be produced using methyl chloride, dimethyl sulfate, or benzyl chloride. The terpolymers may include anionic monomers such as acrylic acid or 2-acrylamido 2-methylpropane sulfonic acid as long as the overall charge on the polymer is cationic. The molecular weights of these polymers, both vinyl addition and condensation, range from as low as several hundred to as high as several million. Preferably, the molecular weight range should be from about 20,000 to about 1,000,000. In at least one embodiment, the pre-treatment is performed by a combination of one, some, or all of any of the compositions of matter described as suitable compositions of matter for pre-treating the filler particles.

[0027] In at least one embodiment, the wet strength aid or wet web strength additive or drainage aids carries the same charge as the composition of matter suitable for treating the filler particles. When the two carry the same charge, the filler additive is less likely to adsorb wet strength aid, wet web strength additive or drainage aid on its surface. Wet strength aids, wet web strength additives or drainage aids encompassed by the invention include any one of the compositions of matter described in US Patent 4,605,702 and US Patent Application 2005/0161181 A1 and in particular the various glyoxylated Acrylamide/DADMAC copolymer compositions described therein. An example of a glyoxylated Acrylamide/DADMAC copolymer composition is product# Nalco 63700 (made by Nalco Company, Naperville, Illinois). Another example of is amine-containing polymers including allylamine/acrylamide copolymers and polyvinylamines; one more example is Polyamide-Polyamine-Epichlorohydrin (PAE)

[0028] In at least one embodiment, the fillers used are PCC, GCC, and/or kaolin clay. In at least one embodiment, the fillers used are PCC, GCC, and/or kaolin clay with polyacrylic acid polymer dispersants or their blends. The ratio of wet strength additive or wet web strength aid or drainage additive relative to solid paper mat can be 3kg of additive per ton of paper mat.

[0029] In at least one embodiment of the invention at least some of the filler particles are pre-treated using a rotating admixing apparatus. A rotating admixing apparatus comprises a distribution head which is constructed and arranged to rotate as it disperses the treating chemicals to the filler particles. In at least one embodiment the rotating admixing apparatus is the device described in US Patent 5,993,670. The apparatus can admix flocculant liquid(s) to a process stream, in which a distribution head, which is rotated by a drive, is arranged in a pipe/conduit, through which a slurry of filler particles flows, and is associated with a rotational plane, and the distribution head has, along a circumference thereof, which surrounds a rotational axis, distributed flocculant outlets and mixing blades, and is connected with a flo-

culant liquid delivery conduit.

[0030] In at least one embodiment the invention also relates to the use of the apparatus of admixing the flocculant liquid, which is formed by a mixture of an active agent and water and of which n parts are added to 100 parts of the filler slurry, with the flocculant liquid added to the 100 parts of the slurry containing a necessary amount a of the active agent.

[0031] There exist cases, when an apparatus for admixing is located, in the direction of the filler slurry flow, downstream of a delivery pump or a centrifuge and which mixes a flocculant liquid and the filler with each other with good results. However, there exists a noticeable number of cases when this is not the case and when the admixing apparatus fails to effect a satisfactory mixing of the flocculant liquid and the filler. In a known apparatus of the above-mentioned type (DE-05 40 29 824), the flocculant outlets are formed as holes or nozzles, and each mixing blade is formed as a journal-like projection, with the dimensions of the mixing blade and the outlet in a direction transverse to the rotational plane being very small in comparison with the width of the filler slurry stream. In some cases the admixture of the flocculant liquid to the slurry, which is obtained with this apparatus is insufficient, i.e., the added flocculant liquid is not sufficiently uniformly distributed in the slurry stream behind the apparatus and is not contained in the slurry in the quantity necessary for a satisfactory flocculation.

[0032] Therefore, an object of the invention is an apparatus of the above-described type with which a better admixing of the flocculant liquid to the slurry is achieved. The apparatus, which achieves this object, is characterized in that the flocculant outlets are formed as slots and the mixing blades are formed as strips, which extend transverse to the rotational plane and have a length equal at least a half of the width of the slurry stream.

[0033] In at least one embodiment only one, some, or all of the chemicals added in the pre-treatment process are added with the rotating apparatus.

[0034] In at least one embodiment the construction of the distribution head of the apparatus permits to achieve an improved admixture and distribution of the flocculant liquid in the slurry. The flocculant liquid exits from every slot in a form of a broad strip into which a following mixing blade is inserted in a direction opposite to the rotational direction and which pulls the flocculant liquid along its edge as a foggy strip through the slurry. The flocculant liquid is delivered through the slots as an interrupted torrent into the slurry, and the slots and strips are arranged one after another in the rotational direction. The dimensioning of the length of the slots and the blades is effected in accordance with the diameter of the stream or of the distribution head.

[0035] In at least one embodiment, the flocculant slots and the strip-shaped blades can extend both in the direction of the slurry stream and substantially perpendicular to the slurry stream. Another embodiment of the invention is possible in which the rotational axis of the mix-

ing head extends at an angle to the slurry stream. As a rule, however, the rotational plane of the mixing head extends substantially in the direction of the slurry stream. **[0036]** Each slot is formed, e.g., of two or more slot sections arranged in a row. It is, however, particularly effective and advantageous when each slot is continuous along its entire length. This prevents clogging and an undesirable high exit velocity of the flocculant liquid.

[0037] Each strip-shaped mixing blade is divided, e.g., along its length, with radial incisions in a comb-like fashion. However, it is particularly effective and advantageous when each strip-shaped mixing blade is continuous over its length. This improves the rigidity of the strip-shaped mixing blades and improves the mixing action.

[0038] The cross-section of each outlet slot can be changed along its length for controlling the amount of the emerging flocculant liquid. It is particularly effective and advantageous when the cross-section of each outlet slot is increased, when viewed along its length, toward the middle. This shape of the outlet slots is used when the slots extend transverse to the stream direction, as in the middle of the slurry pipe, there is more slurry than at the sides. With a uniform slot width, a uniform delivery of the flocculant into the slurry is achieved.

[0039] In at least one embodiment the slots, which form an outlet for the flocculant liquid, have, e.g., a width of 7-9 mm. The greater is the amount of the flocculant liquid to be delivered in a unit of time, the wider the slots are, and the smaller is the amount of the flocculant liquid to be delivered in a unit of time, the narrower they are.

[0040] It is particularly effective and advantageous when the edge of each strip-shaped mixing blade extend approximately parallel to the inner contour of the slurry pipe, forming a clearance therebetween. The elongate strip-shaped mixing blades extending in a radial direction improve the admixing action. However, a clearance should remain between the mixing blade and the slurry conduit, with the clearance being sufficiently large to permit passing of stone pieces present in the slurry.

[0041] This clearance is particularly important and is large when the strip-shaped mixing blades extend transverse to the stream. When the strip-shaped mixing blades extend transverse to the stream, the clearance preferably is smaller in the direction of the rotational axis than in the direction transverse to the rotational axis.

[0042] A particularly effective and advantageous embodiment of the invention is obtained, when the direction of rotation of the distribution head drive can be changed. In the apparatus, the mixing blade is relatively large or protrudes with respect to the slurry pipe cross-section, so that a danger of clogging with hard pieces and of accumulation of fibers or threads exists if the distribution head rotates in the same direction for a long time. The rotation in opposite directions prevents such clogging and accumulation.

[0043] One, two, and/or more flocculant outlets can be provided, e.g., between two mixing blades. However, it is particularly effective and advantageous when outlet

slots and strip-shaped mixing blades alternate in the rotational direction. This also improves the admixing process. Over the distribution head, in the rotational direction, there are provided two or more outlet slots and two or more strip-shaped mixing blades.

[0044] It is further particularly effective and advantageous when the inner cross-section of the slurry pipe, in the region of the distribution head, is similar to the further inner cross-section of the slurry pipe. The apparatus thus eliminates the narrowing of the slurry pipe and an associated with it increase of the flow velocity of the slurry. The distribution head already forms a greater narrowing of the cross-section available for the slurry.

[0045] It is particularly effective and advantageous when the distribution head is formed as a cylindrical tubular section and/or when the outer diameter of the distribution head is equal at least to 0.4 of the inner diameter of the slurry pipe. This simplifies the construction and improves the rigidity of the distribution head, with the shape of the outlet slots and the strip-shaped mixing blades presenting an increased demand to the rigidity of the distribution head.

[0046] A particularly effective and advantageous embodiment is formed when the distribution head passes into a rotatably supported connection tube which extends away from the slurry pipe and which is connected to the drive and with a flocculant liquid delivery conduit, and is further provided with inlet openings and is rotatably supported in a connection chamber into which the flocculant liquid delivery conduit opens. This manner of delivery of the flocculant liquid to a rotatable distribution head permits to insure an increased rigidity of the connection tube and its support with simple means. This becomes possible in the apparatus due to the "stone crushing" cooperation of the strip-shaped mixing blades and the slurry pipe.

[0047] For a satisfactory delivery of the flocculant liquid(s) through the outlet slots, the flow cross-section, which is available for the flocculant liquid(s), is very important. In one embodiment, all of the outlet slots together have a cross-section which is smaller than the preceding flow cross-section of the flocculant liquid. The entire cross-section of the inlet opening is not smaller than the flow cross-section in the delivery conduit and in the connection tube. The flow cross-section in the distribution head and in the connection tube are similar. The arrangement of the connection tube in a sealed connection chamber enables to optimize the flow cross-section of the flocculant liquid.

[0048] It is particularly effective and advantageous when a check valve is arranged in the flocculant liquid delivery conduit when the flocculant liquid in front of the check valve is not under pressure, e.g., when the flocculant liquid pump does not operate, the slurry can penetrate into the outlet slots. The sealings and the bearings in the connection chamber remain lubricated with the flocculant liquid when the flocculant liquid from the flocculant liquid pump is not under pressure any more.

[0049] A particular effective and advantageous embodiment is obtained when the distribution head is driven with a rotational speed of 1,000-2,000 revolution/min. According to the invention, the apparatus has a distribution head, which is rotated by a drive with a rotational speed of 1,000 to 2,000 revolution/min. At this relatively high rotational speed, a desired improved admixing and distribution of the flocculant liquid in the slurry takes place. At the too low rotational speed, below 500 revolution/min, the strip or the stream of the flocculant liquid break off. However, a big speed requires too high expenses in order to achieve the desired effect. In a known apparatus (DE-05 4029824) of the above-described type, the flocculant is available which is stored in a reservoir. It is further known (DE-05 39 01 292) to add fresh water to a flocculant available in a liquid or powder form to obtain about 1% of a flocculant parent solution. The flocculant parent solution is then mixed, at a filling station, with 4-10 volume parts of make-up water to obtain a flocculant in a form of a so-called commercial solution. This flocculant is added in the amount of 18-20% of the amount of the filler slurry is added to the slurry, i.e., about 20 parts of the flocculant liquid in a form of flocculant agent is added to 100 parts of filler particles. At that, the flocculant-containing slurry, i.e., the conditioned filler, contains 1/6 of liquid added by admixing of the additionally added flocculant liquid.

[0050] In a known application, for the additional processing of the flocculant agent a large amount of water is used, which is expensive. For processing, in addition to the apparatus for obtaining the parent solution, an apparatus for obtaining the commercial solution is needed, which results in additional expenses associated with the apparatus and in additional expenses associated with the driving of the apparatus. The flocculant and its water are delivered until they mix up with the slurry, and the delivery require energy, which is costly. The water component of the flocculant must be delivered, together with the slurry, to filter presses, pass through the filter presses and, finally, purified again. Thus, in a known application, additional increased expenses are associated with the water contained in the flocculant liquid.

[0051] Therefore, an object of the invention is to so improve the process described above that the expenses associated with the use of the flocculant liquid or increase of its water content, are eliminated. This object is achieved according to the invention by so designing the above-described apparatus that maximum 3t of the flocculant liquid need be provided for 100t of filler slurry.

[0052] It was found out, that the use of the distribution head of the apparatus permits to eliminate the water component of the flocculant liquid without the elimination of the effectiveness of the flocculant liquid admixed to the slurry. Whereas in the know application in order to achieve a predetermined effect with a predetermined amount of the additive, a large amount of the water component is necessary, this is not necessary when the apparatus is used. The water component of the flocculant liquid can be reduced to a very large extent, so that the

expenses associated with this water content are correspondingly eliminated. As less water is necessary, less water need be pumped, and less water need be purified.

[0053] The improved effectiveness achieved by the invention can be explained, without claiming that the explanation is correct, as follows: The particular shape of the mixing blade of the apparatus breaks the filler slurry particles of the slurry to a great extent, and the resulting broken pieces form open fissures. The particular shape of the flocculant outlets insures that the flocculant liquid takes a shape of a large surface veil which cover the freshly opened fissures so that the mixing of the filler and the flocculant intensifies. The flocculant liquid in accordance with the invention is already admixed in a finely distributed state so that it is not necessary the additive to further dilute in a large amount of water, i.e., to increase the water component of the flocculant liquid. Thus, according to a particular effective and advantageous embodiment of the invention, the flocculant liquid is used as a parent solution, with the additive being mixed with water in a single step. With this embodiment, additional stations for further mixing with water are eliminated.

[0054] Referring now to FIG.s 1 and 2 it is shown in at least one embodiment that the apparatus may be mounted on a filler slurry carrying conduit/pipe 1 through which a filler slurry flows in a direction of arrow 2. The apparatus may be mounted on the slurry pipe 1 by means of an elongate flange 3 and includes a connection chamber 4 projecting from the flange 3. From the connection chamber 4, a distribution head 6 extends into the slurry pipe 1 and is rotated by a drive 7 provided at the opposite end of the chamber 4 and formed as an electromotor. A flocculant liquid conduit 8 opens into the chamber 4, and a check valve 9 is located in the conduit 8. The distribution head 6 forms outlet slots 10 and carries mixing strip shaped blades (11).

[0055] A sleeve 14 supports a connection tube 15 in a shaft extension 12 which extends from the drive 7, and in the end wall of the connection chamber 4, there is provided an axial face seal 16 through which the shaft extension 13 extends. The connection tube 15 has a plurality of elongate entrance openings 17 through which flocculant flows into the connection tube from the connection chamber. The connection tube 15 projects into connection chamber 4 through a plain bearing sleeve 5 provided in the flange 3, with the tubular-shaped distribution head 6 forming an integral part of the tube 15. The distribution head 6 is associated with a rotational plane 18 designated with a dash line. Each mixing blade 11 forms an arcuate edge 19 which, in a corresponding position of the blade, limits a slot 20 with respect to the slurry pipe 1, which has a circular cross-section.

[0056] The foregoing may be better understood by reference to the following example, which is presented for purposes of illustration and is not intended to limit the scope of the invention.

Comparative Example 1

1(i) Filler pre-treatment:

[0057] A blend of filler particles was obtained from a paper mill. The blend filler was a mixture of 50% PCC and 50% GCC. The filler blend was diluted to 20% solid content with tap water. 200 mL of the diluted filler blend was placed in a 500 mL glass beaker. Stirring was conducted for at least 30 seconds prior to the addition of coagulant. The stirrer was a EUROSTAR Digital overhead mixer with a R1342, 50 mm, four-blade propeller (both from IKA Works, Inc., Wilmington, North Carolina). A coagulant solution was slowly added after the initial 30 seconds of mixing under stirring with 800rpm. The coagulant solution used was 4690. The dose of coagulant was 1kg/ton based on dry filler weight. Stirring continued at 800 rpm until all the coagulant was added. Then the stirring speed increased to 1500 rpm for one minute.

1(ii) Use of filler:

[0058] Furnish was prepared by disintegrating commercial bleached hardwood dry lap. The mixture of 50% PCC and 50% GCC was added to pulp furnish to achieve different filler content in the sheet. 200ppm Nalco 61067 was used as retention aid. For the pretreatment evaluation, filler mixture was pretreated using Nalco coagulant 4690 before filler was added into the furnish. During the handsheet preparation, 3kg/ton Nalco 63700 was added to improve the sheet wet web strength. We tried to evaluate the effect of filler pretreatment on the press dewatering performance of 63700 by measuring sheet wet web strength. Handsheets were pressed to a certain solid content (50%) by controlling the same pressure level at 60 degree C, and the time required to completely break up wet sheet in water under the shear force of 1000RPM was recorded to compare sheet wet web strength, which was expected to indirectly reflect press dewatering. The results indicate that sheet wet web strength could be significantly improved by the addition of 63700. Filler pretreatment could further boost sheet wet web strength by additional 20% at the lower ash content. As for the higher ash content, the performance of 63700 was even higher than 20%.

Comparative Example 2

[0059] A machine trial was run in which a papermaking machine made GAB300 with machine speed of 900m/min. A composition was provided whose cellulose fibers were 14% MXW; 3% coated broke; 17% SOW; 12% Uncoated Broke, 44% DIP and 10% ONP. The furnish also contained GCC. During the trial, all the wet end additives including 15/ton Nalco press dewatering aid 63700, retention aids, sizing agents, and cationic starches were kept constant.

1) Filler retention enhancement:

4690 was gradually increased from 0.5kg/ton to 2kg/ton based on filler. It was found that online ash content was increased gradually with the addition of 4690 to the filler pipe. Obviously, 0.7 ash point increase from 15.6% to 16.3% was obtained through filler pre-treatment. Historically, for the same grade production, recorded ash content of DCS was about 12% without using Nalco 63700. It should be pointed out that the ash content improvement was only contributed by filler ply. Therefore, ash content increase in filler ply was supposed to be about 1.4% because filler ply accounted for half basis weight of the final product. FPAR was increased from 70% to 75%, which could explain why final ash content was significantly enhanced.

2) Steam pressure reduction:

It was also found that steam pressure of the pre-dryer was reduced through filler treatment. Steam pressure was gradually decreased from 215 kPa to 200 kPa (2.15 to 2) bar from 10:30am to 2:00pm. Even though press pressure of the first press section and press pressure of the second press section were reduced from 550 to 470 and 600 to 580 respectively, the steam pressure only went back to 205 kPa (2.05 bar).

[0060] During the trial, the ash content increased from around 15.6% to 16.3% about 1 hour after the filler was pretreated, then was kept at the same level for several hours. On the other hand, the steam pressure kept decreasing for several hours until the press load was reduced. This seems to indicate that the steam reduction was not only from ash content increase. Moreover, the steam demand reduction of this trial was only from filler ply since 4690 was only applied for this ply, thus the total steam reduction caused by ash content increase alone should be less. Therefore, the results illustrated that filler pre-treatment could enhance 63700 performance as press dewatering agent or wet web strength aid.

[0061] A person of ordinary skill in the art will recognize that all of the previously described methods are also applicable to paper mat comprising other non-cellulose based fibrous materials, paper mats comprising a mixture of cellulose based and non-cellulose based fibrous materials, and/or synthetic fibrous based materials.

Claims

1. A method of papermaking comprising filler, the method comprising the steps of:
providing a blend of filler particles, at least one drainage additive or wet web strength additive or wet strength aid selected from the list of: glyoxylated Acrylamide/DADMAC copolymer, poly-vinylamine, poly-vinylamide, poly-dial-

lylamine, and any combination thereof, and cellulose fiber stock,
treating the filler particles with a composition of matter in the absence of cellulose fiber stock, the composition of matter being a coagulant,

wherein at least some of the composition of matter is added to the filler with a rotating admixing apparatus, the apparatus having a distribution head, which is rotated by a drive with a rotational speed of 1,000 to 2,500 revolution/min, is arranged in a container containing a slurry of the filler particles, and is associated with a rotational plane, and the distribution head has, along a circumference thereof, which surrounds a rotational axis, distributed outlets from which the composition is passed into the slurry and mixing blades,
wherein the outlets are formed as openings and the mixing blades are formed as strips extending transverse to the rotational plane and having a length equal at least half of an inner diameter of the slurry pipe;
and delivering the composition to the distribution head for admixing the composition to the filler slurry;

combining the filler particles with the cellulose fiber stock, treating the combination with the at least one wet strength aid or wet web strength additive or drainage additive, and forming a paper mat by removing some of the water from the combination, wherein at least 10% of the filler particles are precipitated calcium carbonate and at least 10% of the filler particles are ground calcium carbonate, the cellulose fiber stock comprises a plurality of cellulose fibers and water, and the composition of matter enhances the performance of the wet strength aid or wet web strength additive or drainage additive in the paper mat.

2. The method of claim 1 in which at least some of the calcium carbonate is in one form selected from the list consisting of: undispersed calcium carbonate, dispersed slurry calcium carbonate, chalk, and any combination thereof.
3. The method of claim 1 in which at least a portion of the calcium carbonate is in a dispersed slurry calcium carbonate form, the dispersed slurry calcium carbonate further comprising at least one item selected from: polyacrylic acid polymer dispersants, sodium polyphosphate dispersants, Kaolin clay slurry, and any combination thereof.
4. The method of claim 1 in which the blend of filler

particles is 50% ground calcium carbonate and 50% precipitated calcium carbonate.

5. The method of claim 1 in which the coagulant is selected from the list consisting of: inorganic coagulants, organic coagulants, condensation polymerization coagulants, and any combination thereof.
6. The method of claim 1 in which the coagulant has a molecular weight range of between 200 and 1,000,000.
7. The method of claim 1 in which the coagulant is selected from the list consisting of: alum, sodium aluminate, polyaluminum chlorides, aluminum chlorohydroxide, aluminum hydroxide chloride, polyaluminum hydroxychloride, sulfated polyaluminum chlorides, polyaluminum silica sulfate, ferric sulfate, ferric chloride, epichlorohydrin-dimethylamine (EPI-DMA), EPI-DMA ammonia crosslinked polymers, polymers of ethylene dichloride and ammonia, polymers of ethylene dichloride, polymers of dimethylamine, condensation polymers of multifunctional diethylenetriamine, condensation polymers of multifunctional tetraethylenepentamine, condensation polymers of multifunctional hexamethylenediamine condensation polymers of multifunctional ethylenedichloride, melamine polymers, formaldehyde resin polymers, cationically charged vinyl addition polymers, and any combination thereof.
8. The method of claim 1 in which the coagulant is an AcAm/DADMAC copolymer.
9. The method of claim 1 in which the ratio of drainage additive or wet web strength additive or wet strength aid relative to the solid portion of the paper mat is 0.3 to 5 kg of strength additive per ton of paper mat.
10. The method of claim 1 in which at least some of the GCC particles are treated with the composition of matter.
11. The method of claim 1 in which none of the PCC particles are treated with the composition of matter.
12. The method of claim 1 in which the paper mat has a solid portion and the filler particles in the paper mat comprise more than 50% of the combined mass of the solid portion of the paper mat.
13. The method of claim 1 in which the drainage additive or wet web strength additive or wet strength aid and the composition of matter carry the same charge.
14. The method of claim 1 in which the blend of filler particles further comprises one item selected from the list consisting of: organic pigment, inorganic pig-

ment, clay, talc, titanium dioxide, alumina trihydrate, barium sulfate, magnesium hydroxide, and any combination thereof.

Patentansprüche

1. Verfahren zur Papierherstellung, das Füllstoffe umfasst, wobei das Verfahren die folgenden Schritte umfasst:

Bereitstellen einer Mischung aus Füllstoffpartikeln, wenigstens einem Entwässerungsadditiv oder Nassbahnfestigkeitsadditiv oder Nassfestigkeitshilfsmittel, ausgewählt aus der folgenden Liste:

glyoxyliertes Acrylamid/DADMAC-Copolymer, Polyvinylamin, Polyvinylamid, Polydiallylamin und eine beliebige Kombination davon und Cellulosefaserrohrstoff,

Behandeln der Füllstoffpartikel mit einer Stoffzusammensetzung in der Abwesenheit von Cellulosefaserrohrstoff, wobei die Stoffzusammensetzung ein Koagulans ist, wobei wenigstens ein Anteil der Stoffzusammensetzung dem Füllstoff mit einer sich drehenden Beimischeinrichtung zugesetzt wird, wobei die Einrichtung, die einen Verteilerkopf aufweist, der durch einen Antrieb mit einer Drehzahl von 1.000 bis 2.500 Umdrehungen pro Minute gedreht wird, in einem Behälter eingerichtet ist, der eine Aufschämmung der Füllstoffpartikel enthält, und einer Drehebene zugehörig ist, und der Verteilerkopf entlang eines Umfangs davon, der eine Drehachse umgibt, verteilte Auslässe, aus denen die Zusammensetzung in die Aufschämmung geführt wird, und Mischblätter aufweist, wobei die Auslässe als Öffnungen ausgebildet sind und die Mischblätter als Streifen ausgebildet sind, die sich quer zu der Drehebene erstrecken und eine Länge aufweisen, die gleich wenigstens der Hälfte eines Innendurchmessers des Aufschämmungsrohrs ist; und Zuführen der Zusammensetzung zu dem Verteilerkopf zum Beimischen der Zusammensetzung zu der Füllstoffaufschämmung; Kombinieren der Füllstoffpartikel mit dem Cellulosefaserrohrstoff, Behandeln der Kombination mit dem wenigstens einen Nassfestigkeitshilfsmittel oder Nassgewebefestigkeitsadditiv oder Entwässerungsadditiv und Ausbilden eines Papiervlies durch Entfernen eines Anteils des Wassers aus der Kombination, wobei wenigstens 10 % der Füllstoffpartikel ausgefälltes Calciumcarbonat sind und wenigstens 10 % der Füllstoffpartikel gemahnelenes Calciumcarbonat sind, wobei der Cellulosefaserrohrstoff mehrere Cellulosefasern und Wasser umfasst und die Stoffzusammensetzung die Leistung

des Nassfestigkeitshilfsmittels oder des Nassgewebefestigkeitsadditivs oder des Entwässerungsadditivs in dem Papiervlies verbessert.

- 5 2. Verfahren nach Anspruch 1, wobei wenigstens ein Anteil des Calciumcarbonats in einer Form vorliegt, die aus der Liste ausgewählt ist, die aus Folgendem besteht: nicht dispergiertes Calciumcarbonat, dispergiertes Aufschämmungscalciumcarbonat, Kalk und einer beliebigen Kombination davon.
- 10 3. Verfahren nach Anspruch 1, wobei wenigstens ein Anteil des Calciumcarbonats in einer dispergierten Aufschämmungscalciumcarbonatform vorliegt, wobei das dispergierte Aufschämmungscalciumcarbonat ferner wenigstens ein Element umfasst, das aus Folgendem ausgewählt ist: Polyacrylsäurepolymerdispersanten, Natriumpolyphosphatdispersanten, einer Kaolintonaufschämmung und einer beliebigen Kombination davon.
- 15 4. Verfahren nach Anspruch 1, wobei die Mischung aus Füllstoffpartikeln 50 % gemahnelenes Calciumcarbonat und 50 % ausgefälltes Calciumcarbonat ist.
- 20 5. Verfahren nach Anspruch 1, wobei das Koagulans aus der Liste ausgewählt ist, die aus Folgendem besteht: anorganischen Koagulantien, organischen Koagulantien, Kondensationspolymerisationskoagulantien und einer beliebigen Kombination davon.
- 25 6. Verfahren nach Anspruch 1, wobei das Koagulans einen Molekularmassebereich zwischen 200 und 1.000.000 aufweist.
- 30 7. Verfahren nach Anspruch 1, wobei das Koagulans aus der Liste ausgewählt ist, die aus Folgendem besteht: Alau, Natriumaluminat, Polyaluminiumchloriden, Aluminiumchlorhydroxid, Aluminiumhydroxidchlorid, Polyaluminiumhydroxychlorid, sulfatierten Polyaluminiumchloriden, Polyaluminumsiliciumdioxidsulfat, Eisensulfat, Eisenchlorid, Epichlorhydrin-dimethylamin (EPI-DMA), mit EPI-DMA ammoniakvernetzten Polymeren, Polymeren von Ethylendichlorid und Ammoniak, Polymeren von Ethylendichlorid, Polymeren von Dimethylamin, Kondensationspolymeren von multifunktionellem Diethylentriamin, Kondensationspolymeren von multifunktionellem Tetraethylpentamin, Kondensationspolymeren von multifunktionellen Hexamethylendiamin-Kondensationspolymeren von multifunktionellem Ethylenchlorid, Melaminpolymeren, Formaldehydharzpolymeren, kationisch geladenen Vinyladditionspolymeren und einer beliebigen Kombination davon.
- 35 8. Verfahren nach Anspruch 1, wobei das Koagulans ein AcAm/DADMAC-Copolymer ist.
- 40
- 45
- 50
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9. Verfahren nach Anspruch 1, wobei das Verhältnis von Entwässerungssadditiv oder Nassgewebefestigkeitsadditiv oder Nassfestigkeitshilfsmittel relativ zu dem festen Abschnitt des Papiervlies 0,3 bis 5 kg Festigkeitsadditiv pro Tonne Papiervlies beträgt. 5
10. Verfahren nach Anspruch 1, wobei wenigstens ein Anteil der GCC-Partikel mit der Stoffzusammensetzung behandelt wird. 10
11. Verfahren nach Anspruch 1, wobei keines der PCC-Partikel mit der Stoffzusammensetzung behandelt wird. 15
12. Verfahren nach Anspruch 1, wobei das Papiervlies einen festen Abschnitt aufweist und die Füllstoffpartikel in dem Papiervlies mehr als 50 % der kombinierten Masse des festen Abschnitts des Papiervlies umfassen. 20
13. Verfahren nach Anspruch 1, wobei das Entwässerungssadditiv oder das Nassbahnenfestigkeitsadditiv oder das Nassfestigkeitshilfsmittel und die Stoffzusammensetzung dieselbe Ladung tragen. 25
14. Verfahren nach Anspruch 1, wobei die Mischung aus Füllstoffpartikeln ferner ein Element umfasst, das aus der Liste ausgewählt ist, die aus Folgendem besteht: einem organischen Pigment, einem anorganischen Pigment, Ton, Talk, Titanoxid, Aluminiumtrihydroxid, Bariumsulfat, Magnesiumhydroxid und einer beliebigen Kombination davon. 30

Revendications

1. Procédé destiné à la fabrication de papier comprenant une charge, le procédé comprenant les étapes consistant à :

fournir un mélange de particules de charge, au moins un additif de drainage ou un additif de résistance à l'état humide de bande ou un auxiliaire de résistance à l'état humide choisi dans la liste constituée par : le copolymère acrylamide/DADMAC glyoxylé, la polyvinylamine, la polyvinylamide, la polydiallylamine, et leurs combinaisons, et une composition de fabrication de fibres cellulosiques, traiter les particules de charge avec une composition de matière en l'absence de composition de fabrication de fibres cellulosiques, la composition de matière étant un coagulant,

au moins une partie de la composition de matière étant ajoutée à la charge avec un appareil de mélange rotatif, l'appareil ayant une tête de distribution, qui est mise en ro-

tation par un entraînement à une vitesse de rotation de 1 000 à 2 500 tours/min, étant disposée dans un récipient contenant une bouillie des particules de charge, et étant associée à un plan de rotation, et la tête de distribution ayant, le long d'une circonférence de celle-ci, qui entoure un axe de rotation, des sorties réparties à partir desquelles la composition est passée dans la bouillie et des lames de mélange, les sorties étant formées en tant qu'ouvertures et les lames de mélange étant formées en tant que languettes s'étendant transversalement au plan de rotation et ayant une longueur égale au moins à la moitié d'un diamètre intérieur du tuyau de bouillie ; et délivrer la composition à la tête de distribution pour mélanger la composition à la bouillie de charge ;

combiner les particules de charge avec la composition de fabrication de fibres cellulosiques, traiter la combinaison avec l'eau au moins un auxiliaire de résistance à l'état humide ou additif de résistance à l'état humide de bande ou additif de drainage, et former une pâte à papier en éliminant une partie de l'eau de la combinaison, au moins 10 % des particules de charge étant du carbonate de calcium précipité et au moins 10 % des particules de charge étant du carbonate de calcium broyé, la composition de fabrication de fibres cellulosiques comprenant une pluralité de fibres cellulosiques et de l'eau, et la composition de matière améliorant les performances de l'auxiliaire de résistance à l'état humide ou de l'additif de résistance à l'état humide de bande ou de l'additif de drainage dans la pâte à papier.

2. Procédé selon la revendication 1, dans lequel au moins une partie du carbonate de calcium est sous une forme choisie dans la liste constituée par : du carbonate de calcium non dispersé, du carbonate de calcium en bouillie dispersée, de la craie, et leurs combinaisons. 45
3. Procédé selon la revendication 1, dans lequel au moins une partie du carbonate de calcium est sous la forme de carbonate de calcium en bouillie dispersée, le carbonate de calcium en bouillie dispersée comprenant en outre au moins un élément choisi parmi : les dispersants de polymère d'acide polycrylique, les dispersants de polyphosphate de sodium, la bouillie d'argile Kaolin, et leurs combinaisons. 50
4. Procédé selon la revendication 1, dans lequel le mé-

- lange de particules de charge est constitué de 50 % de carbonate de calcium broyé et de 50 % de carbonate de calcium précipité.
5. Procédé selon la revendication 1, dans lequel le coagulant est choisi dans la liste constituée par : des coagulants inorganiques, des coagulants organiques, des coagulants de polymérisation par condensation et leurs combinaisons.
6. Procédé selon la revendication 1, dans lequel le coagulant a une plage de poids moléculaire comprise entre 200 et 1 000 000.
7. Procédé selon la revendication 1, dans lequel le coagulant est choisi dans la liste constituée par : l'alun, l'aluminate de sodium, les chlorures de polyaluminium, l'hydroxyde de chlorure d'aluminium, le chlorure d'hydroxyde d'aluminium, le chlorure d'hydroxyde de polyaluminium, les chlorures de polyaluminium sulfatés, le sulfate de silice de polyaluminium, le sulfate ferrique, le chlorure ferrique, l'épichlorhydrine-diméthylamine (EPI-DMA), les polymères réticulés par ammonium EPI-DMA, les polymères de dichlorure d'éthylène et d'ammonium, les polymères de dichlorure d'éthylène, les polymères de diméthylamine, les polymères par condensation de diéthylénetriamine multifonctionnelle, les polymères par condensation de tétraéthylènepentamine multifonctionnelle, les polymères par condensation d'hexaméthylénediamine multifonctionnelle, les polymères par condensation de chlorure d'éthylène multifonctionnel, les polymères de mélamine, les polymères de résine formaldéhyde, les polymères d'addition vinyliques chargés cationiquement et leurs combinaisons.
10. Procédé selon la revendication 1, dans lequel le coagulant a une plage de poids moléculaire comprise entre 200 et 1 000 000.
13. Procédé selon la revendication 1, dans lequel l'additif de drainage ou l'additif de résistance à l'état humide de bande ou l'auxiliaire de résistance à l'état humide et la composition de matière portent la même charge.
14. Procédé selon la revendication 1, dans lequel le mélange de particules de charge comprend en outre un élément choisi dans la liste constituée par : un pigment organique, un pigment inorganique, l'argile, le talc, le dioxyde de titane, le trihydrate d'alumine, le sulfate de baryum, l'hydroxyde de magnésium, et leurs combinaisons.
15. Procédé selon la revendication 1, dans lequel le coagulant est choisi dans la liste constituée par : l'alun, l'aluminate de sodium, les chlorures de polyaluminium, l'hydroxyde de chlorure d'aluminium, le chlorure d'hydroxyde de polyaluminium, les chlorures de polyaluminium sulfatés, le sulfate de silice de polyaluminium, le sulfate ferrique, le chlorure ferrique, l'épichlorhydrine-diméthylamine (EPI-DMA), les polymères réticulés par ammonium EPI-DMA, les polymères de dichlorure d'éthylène et d'ammonium, les polymères de dichlorure d'éthylène, les polymères de diméthylamine, les polymères par condensation de diéthylénetriamine multifonctionnelle, les polymères par condensation de tétraéthylènepentamine multifonctionnelle, les polymères par condensation d'hexaméthylénediamine multifonctionnelle, les polymères par condensation de chlorure d'éthylène multifonctionnel, les polymères de mélamine, les polymères de résine formaldéhyde, les polymères d'addition vinyliques chargés cationiquement et leurs combinaisons.
20. Procédé selon la revendication 1, dans lequel le coagulant a une plage de poids moléculaire comprise entre 200 et 1 000 000.
25. Procédé selon la revendication 1, dans lequel le coagulant a une plage de poids moléculaire comprise entre 200 et 1 000 000.
30. Procédé selon la revendication 1, dans lequel le coagulant a une plage de poids moléculaire comprise entre 200 et 1 000 000.
35. Procédé selon la revendication 1, dans lequel le coagulant a une plage de poids moléculaire comprise entre 200 et 1 000 000.
40. Procédé selon la revendication 1, dans lequel le rapport de l'additif de drainage ou de l'additif de résistance à l'état humide de bande ou de l'auxiliaire de résistance à l'état humide par rapport à la partie solide de la pâte à papier est de 0,3 à 5 kg d'additif de résistance par tonne de pâte à papier.
45. Procédé selon la revendication 1, dans lequel au moins une partie des particules de GCC sont traitées avec la composition de matière.
50. Procédé selon la revendication 1, dans lequel aucune des particules de PCC n'est traitée avec la composition de matière.
55. Procédé selon la revendication 1, dans lequel la pâte à papier a une partie solide et les particules de charge dans la pâte à papier comprennent plus de 50 % de la masse combinée de la partie solide de la pâte à papier.

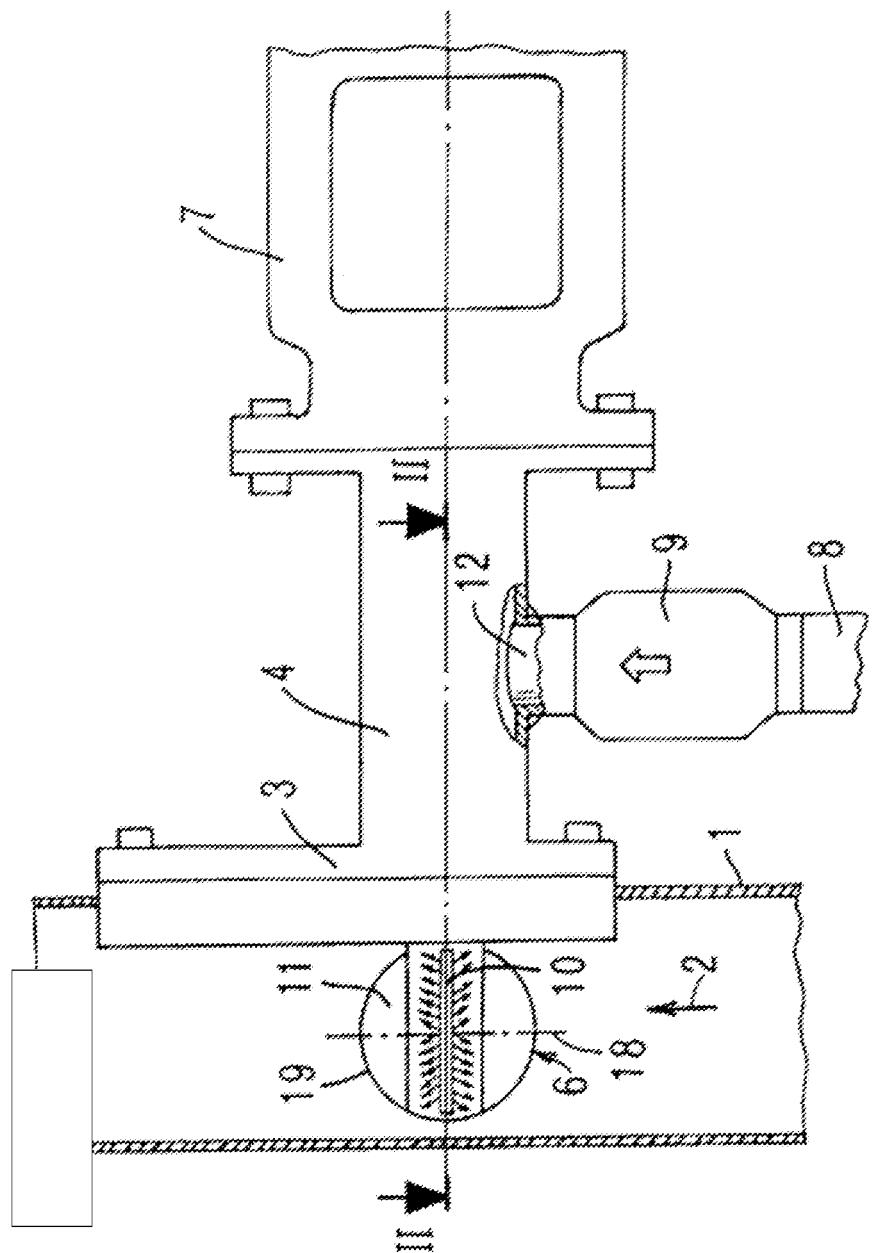


FIG. 1

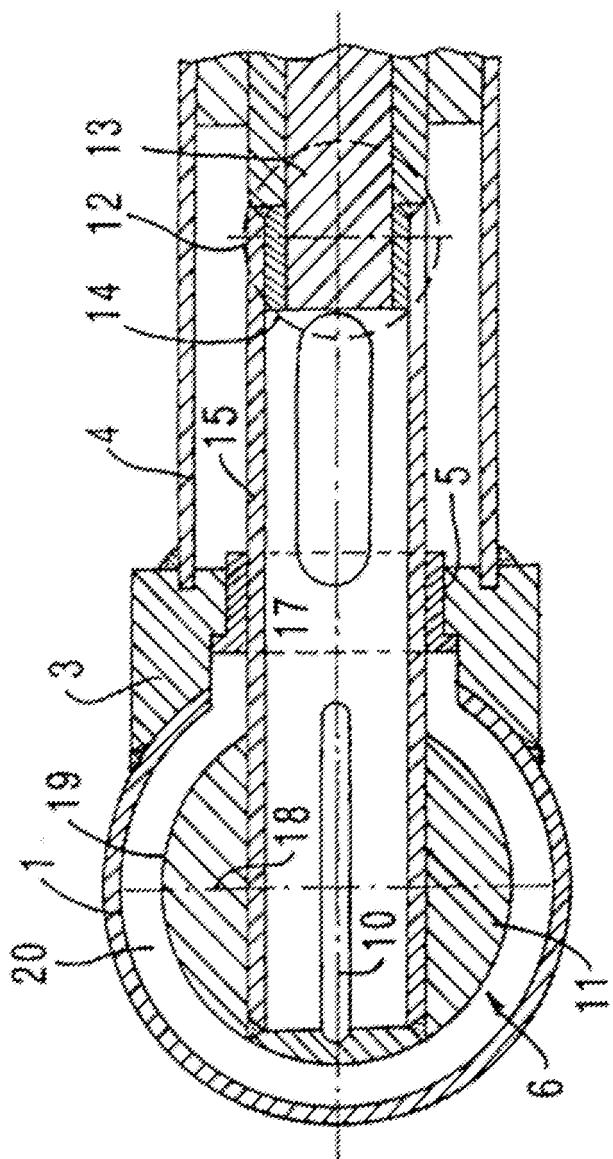


FIG. 2

REFERENCES CITED IN THE DESCRIPTION

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Patent documents cited in the description

- US 7211608 B [0002] [0018]
- WO 2012125235 A [0006]
- US 2010126684 A [0007]
- US 5221435 A [0017]
- US 6592718 B [0017] [0022]
- US 4605702 A [0027]
- US 20050161181 A1 [0027]
- US 5993670 A [0029]
- DE 054029824 [0031] [0049]
- DE 053901292 [0049]