



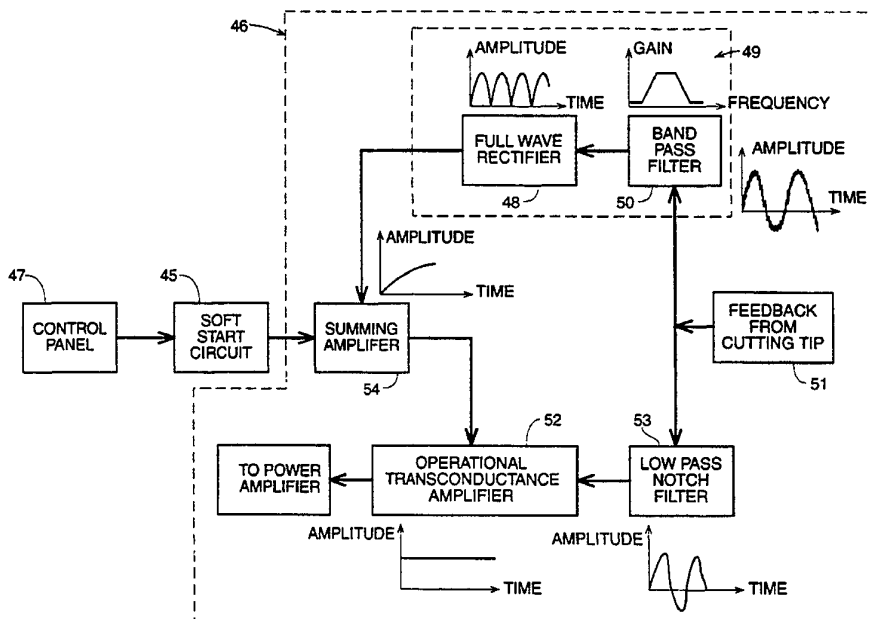
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(54) Title: AN ULTRASONIC SURGICAL HANDPIECE AND AN ENERGY INITIATOR TO MAINTAIN THE VIBRATION AND LINEAR DYNAMICS

(57) Abstract

An ultrasonic oscillator (46) drives a tool at a set frequency. An amplitude control runs the oscillator (46) to set the vibration level. A frequency regulator joins the amplitude and the oscillator (46). A control feedback loop (49), in the frequency regulator, keeps handpiece linear dynamics. An operational transconductance amplifier (52), in the oscillator (46), governs gain of the loop (49). A circuit (55) connects to the control to retard the rate of current application over time to the amplifier (52). The circuit (55) has switching to either retard the rate or reset for start up. The amplifier (54) is a current output device with current directly proportional to the bias current and input voltage with bias as gain change for the loop (49). The circuit (55) limits the bias to the amplifier (54) to modify frequency response and output current. A capacitor delays application of the bias to the amplifier (54). Replaceable tools of various lengths or shapes positioned along an axis vibrate for surgery at the frequency and a wave length. Tools longer than one wavelength and of configurations tuned to oscillate around the frequency resonate as a function of their material, length and configuration. A flue (17) surrounds the tool and has a hollow elongate semi rigid central body (28) about an axis with a funnel (29), at one end thereof and a nozzle (30), at the other to direct annular irrigant/coolant flow therethrough. The funnel (29) and nozzle (30) are resilient. Reinforcing ridges (32), inside the nozzle (30), act to maintain concentricity between the flue (17) and nozzle tip and channel irrigant thereabout.



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AN ULTRASONIC SURGICAL HANDPIECE AND
AN ENERGY INITIATOR TO
MAINTAIN THE VIBRATION AND LINEAR DYNAMICS

5 1. Field of the Invention This invention relates to an ultrasonic surgical handpiece and an energy initiator to maintain the vibration and linear dynamics during start up and under loads. In addition, a flue construction and an elongate tapered pipe tool structures as part of the ultrasonic surgical handpiece are driven by a vibrating driver powered by a circuit including the energy initiator.

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 2. Background of the Disclosure Described herein are an ultrasonic surgical handpiece with the energy initiator circuit to begin and maintain the vibrations and linear dynamics of the elongate tapered pipe tool. The flue is coaxially about the tool.

15 U. S. Patent 4,223,676 discloses an ultrasonic surgical handpiece having a longitudinally vibrating cutting tool ending in a tip with a flue to surround the vibrating tool. The disclosure of '676 is incorporated herein by reference and made a part of this disclosure since the surgical instrument therein is substantially refined and improved by that disclosed and claimed herein. Handpieces made in accordance with the teachings
20 of the '676 patent have tools that were less than four inches long and even with extenders less than seven inches long. Heretofore the need for a tool that was greater than seven inches was unsatisfied and the flue and oscillating electronics needed to serve with such an elongate tool were undeveloped.

25 U.S. Patent Number 4,747,820 owned by the assignee in this present disclosure has a rigid plastic flue constructed so that the body thereof may be rotated relative to a flue adapter, i.e., the piece that attaches to the distal end of the handpiece. The body and adapter are two separately made rigid plastic parts for allowing the relative rotary motion therebetween so that alignment may be achieved particularly where there is a
30 curve in the flue body to accommodate a curved tool. An alternate flue of flexible polymer with supporting ribs is shown and described as received on a rigid adapter with an appropriate conjugating configuration.

While it might seem logical that an elongate tool requires a longer flue to supply irrigation and cooling fluid to the preaspiration holes near the tip of the elongate tool, many unsolved technicalities need resolutions which go beyond the mere extension of the length of the components. With increase in length the structure of the flue needs
5 improvement to have the requisite strength and to provide the needed cooling flow to cover all of the increased size of the elongate tool. The flue disclosed herein is preferably of a soft polymer so that it will not injure the patient and in order to seal to the hand piece in a gasket like easily used way. Soft polymers such as silicon rubber have very little beam or bending strength and consequently, sag without support from the elongate
10 tool or even with the elongate tool disposed coaxially therewithin the flue could lean under the force of gravity so as to be against the elongate tool, thus damping the tool vibrations. Circumferential or surround coolant is thus hampered by any off center disposition of the flue and the need to maintain concentricity between the flue and the elongate tool remains an unresolved problem.

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In addition the dispersion of the irrigation fluid so as to equally access all side and areas of the elongate tool is a problem relative to length. The fluid flow tends to be influenced by gravity as well as the flue deflection. That is, the distance from the support or supply to the distal end increases the problem. Uniform circumferential distribution is
20 difficult with a long flue.

To initiate the vibration in an elongate tip the electronic oscillating circuitry requires particular attention to avoid start up transient overshoots causing the electromechanical oscillating system to equilibrate (or lock up) on an unwanted adjacent resonance. Said
25 adjacent unwanted resonances are present, in particular, due to a long mechanical vibrator in that it has a lower fundamental resonance. The harmonics are integral multiples of the fundamental resulting in a closer spacing, in the frequency domain (of harmonics, or poles), as a function of vibrator length. For example, U.S. patent number 4,587,958 has a starting impulse reducing circuit to prevent transient current from over
30 driving the power amplifier by maintaining the waveform at a predetermined flat amount instead of an initiating spike or overshoot resulting during start up transient conditions. While it is recognized that peak current waveform suppression is useful to prevent spikes that can be two or more times greater than required, a circuit to control the rate of power application to an operational transconductance amplifier is not disclosed. It is now

appreciated that the peak initiating current is not the only factor affecting amplifier performance. For consistent operating characteristics after starting and under loads the rate at which power is supplied to the amplifier in an oscillating circuit must be specifically controlled in a manner not disclosed in '958. Normal variations in the response
5 characteristics of amplifiers can greatly influence the manner in which any specific amplifier of a particular type will respond to input power. Reduction of such variations and the uniform responses are desired.

A difficulty with merely applying power to the electronic circuitry that drives a
10 mechanical reverberating system results from the tuning of the resonance frequency of the mechanical structure designed to vibrate in harmony with the spring constant of the system. An electrical driving circuit is inherently flexible and can oscillate at several frequencies more readily than any mechanical system. Consequently, the driving impetus of the electronic circuit can excite the mechanical structure at different frequencies than
15 the intended resonance frequency. There are many mechanical resonant modes of acoustic vibrators that are independant of drive afforded by the electronics. When that occurs, the mechanical system will vibrate in a manner that does not produce useful displacement and the energy output from the electrical oscillator is wasted. Filtering can be used to assure that the driving frequency is identical with the harmonic of the
20 mechanical system but that requires a complicated circuit design and can not be retrofitted to an existing oscillating circuit. A way to control the initiation and maintenance of the oscillation so that the operating frequency is at the preferred resonant frequency of the mechanical system is required.

25

SUMMARY OF THE INVENTION

The energy initiator includes an electronic oscillator for driving an ultrasonic surgical handpiece preferably operating at a predetermined frequency of about 23 kilohertz. An amplitude control may operate the electronic oscillator permitting the setting
30 of the level of ultrasonic vibration. It is preferred that a frequency regulator be connected between the amplitude control and the electronic oscillator. A frequency control feedback loop may be part of the frequency regulator to maintain the linear dynamics of the ultrasonic surgical handpiece about the predetermined preferred frequency.

An operational transconductance amplifier may be included as part of the electronic oscillator for controlling gain of the frequency control feedback loop. A circuit is preferably connected to the amplitude control for retarding the rate of current application per unit of time to the operational transconductance amplifier thereby
5 ameliorating the effects of transients on the ultrasonic instrument during start up and otherwise. The circuit may include switching systems to in one direction retard the rate of current application and in the other direction of current flow reset the circuit. The operational transconductance amplifier is preferably a current output device with its output current directly proportional to the bias current and input voltage thereto. During
10 operation the bias current may act as the gain or amplitude adjustment for the frequency control feedback loop. The circuit provides a soft start that may also limit the bias current applied to the operational transconductance amplifier thereby modifying the frequency response and output current therefrom during start up and/or limiting the peak bias current applied thereto. The soft starting circuit may include a resistance/capacitance
15 network for setting the delay of the application of the full bias current to the operational transconductance amplifier.

The ultrasonic surgical handpiece may include replaceable ultrasonic tools of various lengths or configurations. A housing gripped proximally controls the handpiece
20 during use. A transducer may be within the housing and positioned along an axis thereof. The transducer is selected or designed to have its primary resonance for oscillating around the preferred frequency and at a length along the axis with motion sufficient for surgery. A connecting member is fitted to the transducer and preferably extends distally from the transducer along the axis but within the housing. Pipe tools are
25 replaceably attachable to the connecting member so that each pipe tool may be of a different length and/or configuration tuned so that the assembly of tool, connecting member and transducer oscillate around the preferred frequency and/or wave length. Wave length equals the speed of sound in material divided by frequency of operation. The soft starting or energy initiator circuit may be used in connection with an electronic
30 oscillator for vibrating the replaceable tools. The length of the replaceable attachable tools may be a function of the material that the pipe tool is made, and its configuration whereby they are tuned to resonate at the preferred predetermined frequency, i.e., 23 kilohertz. The pipe tools are most preferably longer than one wave length or at least five-quarter wave lengths or seven-quarter wave lengths.

A flue for directing coolant to the pipe tool of the ultrasonic surgical handpiece may include a central body that is hollow, elongate and semi-rigid for extending concentrically about and coaxially to an axis passing centrally therethrough and through the pipe tool. A funnel is most preferably at one end of the central body and is proximally
5 positioned to first receive the pipe tool vibrating tip when inserted therewithin and therethrough. A nozzle is opposite the funnel and attached to the central body. The nozzle tapers toward the distal vibrating tip of the ultrasonic surgical handpiece for directing annular flow of fluid from an annular space between the pipe tool and the central body. The funnel and nozzle are preferably made of a resilient material having a
10 durometer which is softer than that of the central body. The central body is preferably of a higher durometer. The modulus of elasticity of the central body is most preferably greater than the modulus of the elasticity of either the funnel or the nozzle. The central body may be made of a separate piece that is preferably extruded transparent polymer such as polysulfone tubing. The nozzle and funnel may be made of molded silicone
15 rubber and connected to one another by a recess or reduced diameter therebetween such that the recess may be surrounded by the extruded transparent tube for support.

The central body may separately, preferably and alternately be made of a molded
20 construction of silicone rubber having a durometer higher than the funnel which may be bonded to the proximal portion of the central body. The nozzle may be more flexible than the central body although molded of the same silicone rubber because of its lesser cross sectional area.

25 The funnel may, on either flue construction, include a shouldered opening for receiving a tube for supplying cooling and preaspiration fluid. Reinforcing ridges may, on either connection, extend longitudinally inside the nozzle to act as a concentric support to coaxially position the nozzle relative to the vibrating tip whereby fluid passing in the annular space may preferably be channelled between the ridges.

30

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a perspective view of an ultrasonic surgical handpiece with part of the housing thereof removed so as to show the inside and the components therein.

Figure 2 is a side view of a flue in cross section and an elongate tapered pipe tool therein and has their relative coaxial disposition as would be seen if the cross section were taken along line 2-2 in Figure 1.

5 Figure 3 is a view in cross section of the flue and the elongate tapered pipe tool of Figure 2 as would be seen if the cross section were taken along line 3-3 in Figure 2.

Figure 4 is an illustration of the pipe tool juxtaposed to plots showing the amplitudes of stress and displacement which occur along its length wherein a pipe tool
10 is elongate to a $7/4$ wavelength.

Figure 5 is an illustration of the pipe tool juxtaposed to plots showing the amplitudes of stress and displacement which occur along its length wherein the pipe tool is elongate to a $5/4$ wavelength.

15

Figure 6 is a schematic block diagram of the electronic components that drive the ultrasonic surgical handpiece of Figure 1 at 23 kilohertz.

Figure 7 is a schematic block diagram of the soft start or energy initiator circuit
20 shown as a block in Figure 6 with the details of a preferred energy initiator having a ramp circuit controlled by the charging rate of a capacitor.

DETAILED DESCRIPTION OF THE INVENTION

The claims are not limited to the structure for an ultrasonic surgical handpiece, a flue or an energy initiator to maintain the vibration and linear dynamics described and illustrated by way of example and specifically explained. The claims are to be considered in view of the existing knowledge of skilled artisans in the Field prior to the inventions defined by the language of the claims herein, as amended or considered in view of knowledge of skilled artisans prior to these inventions. As used throughout this disclosure proximal or posterior has the meaning near the user and distal or anterior is near the patient. The reference numbers as seen in the several figures are identical wherein the components are the same.

Figure 1 is a perspective view partially in section showing an ultrasonic surgical handpiece 10, including a housing 11 that encloses a transducer 12, an electric coil 13 and a connecting member 14 extending axial therethrough along an axis A which represents the longitude for the ultrasonic surgical handpiece 10. In front of the housing 11 there is a nose cone 15 tapered from the housing 11 to a distal end 16 thereof to which mounts a nose cone extending flue 17 thereabout to coaxially surround an axially vibrating metal fragmenting or cutting pipe tool 24. The axially vibrating cutting pipe tool 24 is preferably metal, but might be otherwise, and tip 18 of pipe tool 24 extends longitudinally along axis A beyond the flue 17. A CUSA System 200 made by Valleylab, 5920 Longbow Drive, Boulder, Colorado, has been used to drive the altered components disclosed herein.

A manifold assembly 19 composed of two tubes 20 and 21 for irrigation and suction, respectively lies atop and along the housing 11 to reside parallel to axis A. Tube 20 connects to the flue 17 near distal end 16 so as to feed sterile irrigation and cooling fluid down through the flue 17 for flow toward the tip 18. The vibration introduced into the tip 18 by means of the connecting member 14 generates an acoustic wave or stress resulting in the transformation of some energy into heat. The suction tube 21 draws fluid through at least one preaspiration hole 18a (small of size and shown only in Figures 2, 4 and 5, as will be described hereinafter that provides a portal between the flue 17 and a bore 22, see figure 3). The bore 22 of the pipe tool 24 extends between the tip 18 and a connection 23 for tube 21.

In Figure 2 there is an enlarged side view in cross section of the flue 17 as would be seen along line 2-2 of Figure 1. In Figures 1 and 2, the flue 17 is shown shortened with a section missing as the preferred full length of the flue 17 would not fit on the page without reducing the cross section of the ultrasonic surgical handpiece 10 to an extent such that detail would be lost or to a degree so that the diameter to length relationship would be distorted and any appreciation of the relative lengths of the handpiece 10, flue 17 and cutting tip 18 could not be understood.

In operation the tip 18 is the working end of an elongate tapered hollow metal pipe tool 24, preferably made of titanium alloy tubing of one quarter inch, or 6.3 millimeters, outside diameter and an inside diameter of about .078 inch, or 2 millimeters, for high strength, lightweight lower density than the connecting member, and biologically inert. The pipe tool 24, when part of the acoustic vibrator, is designed to vibrate at a preferred frequency of 23,000 cycles per second so that the tip 18 reciprocates longitudinally along axis A with an excursion or peak to peak stroke of about 200 micrometers (.008 inches) for the preferred embodiment. The irrigation flow through tube 20 passes within an annular space between the flue 17 and the elongate pipe tool 24 picking up heat therefrom.

The irrigation fluid is sucked through the preaspiration hole 18a shown in Figures 2, 4 and 5 near the tip 18 and returned through connection 23 to tube 21 near the nose cone 15. Thus, irrigant flows and can while cooling aid the movement of debris, such as cut tissue and blood up from the surgical site through bore 22 for removal. Longitudinal ultrasonic vibrations of tip 18 fragment tissue which it contacts. The excursion or amplitude and frequency of the vibrations are electronically maintained and to some extent are adjustable as will be explained herein so that the vibrations are in accord with the gaussian or harmonic design of elongate pipe tool 24 and the requirements of the surgical procedure being practiced. The operational parameters of the design of the pipe tool 24 for a preferred resonant frequency and tip excursion is shown in Figures 4 and 5 which illustrate the $7/4$ wavelength and the $5/4$ wavelength elongated pipe tools, respectively. The ultrasonic motion of the vibrating tip 18 relates to the configuration and length of the pipe tool 24 and as shown in Figures 4 and 5 the displacement at the free end of the vibrating tip 18 is at a maximum. To avoid failure, a portion of the vibrating pipe tool 24 is shaped with a Gaussian curved profile which results in an essentially flat

stress notwithstanding the increased displacement of the free end. In a pipe tool made of titanium alloy with the stated preferred dimensions, the axial span of each wavelength at the frequency of 23 kilohertz is about 8.7 inches. The overall length of the pipe tool 24 is thus about 12 inches for $5/4$ wavelength and 16 inches for $7/4$ wavelength.

5

Numerous shapes, as well as combinations thereof, have been theoretically treated and used as mechanical resonators. There have been attempts by suitable shaping to extend the zone of maximum elastic stress in the axial direction and thereby make greater amplitudes possible, see U.S. Patent No. 2,984,154. Since the specific
10 technical application constrained four quantities of the resonance element, namely input, node and output cross section and the transmission ratio, the solution of the resulting problem in variation leads to a function that is Gaussian in profile for the tapered part of the vibrating pipe tool 24.

15 Tubes 25 and 26 provide circulating coolant to the ultrasonic surgical handpiece 10 as shown by arrows in Figure 1. As explained acoustic vibration of the transducer 12 converts electrical energy to mechanical longitudinal vibrating motion along axis A and through pipe tool 24 to its vibrating tip 18. The preferred transducer 12 is an acoustic vibrator having a laminated nickel alloy structure which is excited by a magnetic field
20 creating oscillating currents passing through the electrical coil winding 13. Coil winding 13 is excited at 23,000 cycles per second (23 kilohertz) alternating current. The resulting longitudinal oscillating motion of the preferred laminated nickel alloy structure is amplified by a preferred tapered titanium alloy pipe tool 24 which extends from the distal end of the nose cone 15 to the distal end of the vibrating tip 18. The pipe tool 24 attaches with
25 threads 27 to the transducer 12 by way of the connecting member 14 interposed therebetween. The taper and wall of the extending titanium pipe tool 24 is designed to be a mechanical structure such that it vibrates at 23,000 cycles per second.

An embodiment of flue 17 shown in Figure 2, is composed of two composite
30 pieces which may preferably be made of different polymeric materials since the extremities of the flue 17 should preferably be soft and flexible. There is a central body 28 which is hollow, elongate and semi rigid for extending with and coaxial about the axis A passing longitudinally and centrally therethrough. Central body 28 terminates in a funnel 29 which is proximal and a nozzle 30 which is distal. The flue 17 is primarily and

preferably made of silicone rubber that has a relatively resilient quality whereby the funnel 29 fits tightly over the nose cone 15 of the ultrasonic surgical handpiece 10 forming a fluid tight gasket like seal 31 due to the rubbery resilient nature of the silicone rubber used.

5

In Figures 1 and 2, the flue 17 is shown less than its preferred length which is about 11 1/2 inches or 29 centimeters. The diameter at the funnel 29 is such that the flue 17 tapers generally toward its nozzle 30. The central body 28 is hollow throughout. Reinforcing ridges 32 extend longitudinally inside the nozzle 30. A recess 34 may
10 circumscribe the exterior of central body 28 and extend proximally from the funnel 30 to the taper of the nozzle 30. The recess 34 is designed to receive a hollow support surrounding cylinder 35 thereabout for reinforcement thereof in the embodiment shown. The hollow support surrounding cylinder 35 is preferably an extruded polysulfone tubular configuration sized to sit within the recess 34 for reinforcement against bending of central
15 body 28. Alternately, the central body 28 can be made of a stiffer construction, i. e. thicker wall or of a coextruded material having a greater modulus since the cross sectional appearance of such a stiffer molded material would not be apparent, that integral construction is not specifically shown in the Figures. Skilled artisans would appreciate how that could be accomplished.

20

Funnel 29 which is generally enlarged diametrically relative to axis A and the rest of the central body 28. The funnel 29 includes a fluid communication port 36 between its inside and outside. The port 36 is arranged to pass fluid from tube 20 which seats within a shouldered opening 37 therein and extends distally from a proximal face 38
25 thereof. Fluid may pass from the tube 20 through the port 36 into flue 17 and more particularly, the annular space 33 between the flue 17 and the pipe tool 24. The reinforcing ridges 32 support the nozzle 30 (that has a smaller cross sectional area than the funnel 29 or central body 28) maintaining concentricity relative to the tapered titanium vibrating pipe tool 24 near vibrating tip 18 which passes coaxially therethrough, see
30 Figure 2 and 3. More importantly, ridges 32 do not clamp the pipe tool 24 or the vibrating tip 18 but still separate the flow of irrigation and coolant so that it passes in laminar fashion along the pipe tool 24 and to the tip 18. Consequently, the coolant is channelled so the flow is between the ridges 32.

In particular and as best seen in Figures 2, 4 and 5 the elongate tapered pipe tool 24 has the vibrating tip 18 at its patient contacting extreme (for fragmenting) and a threaded fitting 39 at its proximal extreme (for attachment). Threads 27 allow removable connection of the elongate tapered pipe tool 24 to the connecting member 14 as shown 5 in Figure 1. The elongate tapered pipe tool 24 is preferably made of an extender 41 having the threads 27 and a straight pipe of about six inches or 15 centimeters length with a diameter of one quarter inch or about seven millimeters. The extender 41 is hollow having an inside diameter of .078 inch or 2 millimeters. Threaded connections, shown in partial section in Figure 5 on the distal end of the extender 41 (away from the threads 10 27), cooperate with the posterior 42 of the vibrating tip 18 of the tool 24. That is to say that, the tool 24 is composed of the vibrating tip 18 which tapers to a diameter at its anterior of .100 inch or 2.5 millimeters. The posterior diameter is seven thirty seconds inches or six millimeters and the length of the tip 18 is three and one half inches or nine centimeters. A slight shoulder 43 defines the beginning of a hollow cylinder 44 that is two 15 and one eighth inches or five and one half centimeters and one quarter inch or about seven millimeters in diameter. The hollow cylinder 44 is held to the extender 41 by the threaded connection so the overall length of the elongate tapered pipe tool 24 is about twelve inches or thirty centimeters for the 5/4 wavelength length pipe tool 24. The 7/4 wavelength is a 1/2 wave length longer or about 4.3 inches longer or about nine and one 20 half centimeters. The added length is due to a hollow spacer 42 shown in Figure 4 added between the distal end of extender 41 and the hollow cylinder 44. The hollow spacer 42 is also the same diameter inside and out as the hollow cylinder 44.

The ultrasonic surgical handpiece 10 is driven by an energy initiator 45, also 25 referred to herein as the soft start or circuit 45 for a frequency regulator. Circuit 45 is schematically depicted in the block diagram of Figure 6 and more specifically shown in Figure 7. The energy initiator 45 for frequency regulation maintains a preset vibrational mode and the linear dynamics of the vibrating tip 18 as driven by the ultrasonic surgical handpiece 10 capable of operation at resonance characteristics and under varying loads. 30 An electronic oscillator 46 drives the ultrasonic surgical handpiece 10 at a predetermined frequency, preferably 23 kilohertz. An amplitude control on the control panel 47 in Figure 6 is connected to the electronic oscillator 46. The control panel 47 amplitude control permits manual setting of the level of the ultrasonic vibration. A frequency regulator preferably in the form of a full wave rectifier 48 connects between the control panel 47

amplitude control and the electronic oscillator 46. A frequency control feedback loop 49 includes the frequency regulator and is designated by a dashed line forming a block about the full wave rectifier 48 and the band pass filter 50. The frequency control feedback loop 49 maintains the linear dynamics of the ultrasonic surgical handpiece 10 and vibrating pipe tool 24 about the predetermined frequency during use. Feedback 51 from the cutting pipe tool 24 is delivered to the frequency control feedback loop 49 through the band pass filter 50 therein.

An operational transconductance amplifier 52, included as part of the electronic oscillator 46, controls gain for the frequency control feedback loop 49. Specifically, feedback from the cutting tip 51 is delivered to the operational transconductance amplifier 52 through a low pass notch filter 53. Pulse wave diagrams are shown throughout Figure 6 to illustrate the effect of the circuit components (shown as blocks therein) and to define the operation of a preferred embodiment of the electronic oscillator 46.

15

The soft start circuit 45 connected to the control panel 47 amplitude control retards the rate of the current application per unit of time to the operational transconductance amplifier 52 to ameliorate the effects of transients on the ultrasonic surgical handpiece 10 vibrating pipe tool 24. The soft start circuit 45 shown in Figure 7 energizes the circuit 45 in one direction for retarding the rate of current application per unit of time and upon deenergization resets the circuit to ready it for retarding the rate of the current application per unit of time to the operational transconductance amplifier. When the ultrasonic surgical instrument 10 is subject to the effects of transients during restarting or loading, the circuit 45 is ready to retard input to the operational tranconductance. The preferred switching system may be a amplifier transistor which is used to charge and discharge a capacitor in accord with initiation and shut off of the electronic oscillator 46. The effect of this is shown in the pulse wave diagram above, a summing amplifier 54 in Figure 6.

30 Figure 7 has the soft start circuit 45 shown as a dashed line block including a ramp circuit 55 in parallel with a bypass buffer 56. Power flow from the control panel 47 as authorized by a foot switch 57 or otherwise sends current to the ramp circuit 55 if the electronic oscillator 46 is not operating and soft start circuit 45 is set to begin. A capacitor in the ramp circuit 55 is charged thus providing a rate dependent start.

The operational transconductance amplifier 52 is a current output device wherein the output current therefrom is directly proportional to its bias current and input voltage so that under steady state operation the bias current acts as the gain or amplitude adjustment for the frequency control feedback loop 49. The soft start circuit 45 connects
5 to the amplitude control for retarding the rate of the bias current application per unit of time to the operational transconductance amplifier 52 thereby limiting the bias current applied to the operational transconductance amplifier 52 during start up and thereby modifies the frequency response and output current therefrom.

10 The soft start circuit 45 connects to the control panel 47 amplitude control for retarding the rate of the bias current application per unit of time to the operational transconductance amplifier 52. The soft start circuit is similarly capable of limiting the rate of peak bias current application to the operational transconductance amplifier 52 preventing overdriving bias current during start up. The soft start circuit 45 may include
15 a resistance/capacitance network for delaying the application of the fully bias current to the operational transconductance amplifier 52 so already explored.

What is claimed is:

1. An energy initiator 45 for a frequency regulator to maintain a preset vibrational mode and the linear dynamics of an ultrasonic surgical instrument capable of operation at resonance characteristics and under varying loads comprising:
- 5 an electronic oscillator 46 for driving the ultrasonic instrument at a predetermined frequency;
- an amplitude control connected to the electronic oscillator 46 permitting setting of the level of the ultrasonic vibration;
- 10 a frequency regulator between the amplitude control and the electronic oscillator 46;
- a frequency control feedback loop 49 in the frequency regulator for maintaining the linear dynamics of the ultrasonic surgical instrument about the predetermined frequency;
- 15 an operational transconductance amplifier 52 included as part of the electronic oscillator 46 for gain control for the frequency control feedback loop 49, and
- a circuit 55 connected to the amplitude control for retarding the rate of the current application per unit of time to the operational transconductance amplifier 52 to ameliorate the effects of transients on the ultrasonic surgical instrument.
- 20
2. The energy initiator 45 of Claim 1 wherein the circuit 55 includes switching systems added to energize the circuit 55 in one direction for retarding the rate of current application per unit of time and upon deenergization reset the circuit 55 to ready it for retarding the rate of the current application per unit of time to the operational
- 25 transconductance amplifier 52 when the ultrasonic surgical instrument is subject to the effects of transients during starting or loading.
3. The energy initiator 45 of Claim 1 wherein the operational transconductance amplifier 52 is a current output device wherein the output current
- 30 therefrom is directly proportional to the bias current and input voltage so that under steady state operation the bias current acts as the gain or amplitude adjustment for the frequency control feedback loop 49.

4. The energy initiator 45 of Claim 3 wherein the circuit 55 connected to the amplitude control for retarding the rate of the bias current application per unit of time to the operational transconductance amplifier 52 limits the bias current applied to the operational transconductance amplifier 52 during start up and so modifies the frequency response and output current therefrom.

5. The energy initiator 45 of Claim 4 wherein the circuit 55 connected to the amplitude control for retarding the rate of the bias current application per unit of time to the operational transconductance amplifier 52 limits the peak bias current applied to the operational transconductance amplifier 52 preventing overdriving bias current during start up.

6. The energy initiator 45 of Claim 5 wherein the circuit 55 include a resistance/capacitance network for delaying the application of the full bias current to the operational transconductance amplifier 52.

7. A handpiece for replaceable ultrasonic surgical tools of various different lengths and/or configurations, comprising:

- a housing 11 for holding the handpiece, the housing 11 held proximally during use;
- a transducer 12 within the housing 11, the transducer 12 positioned along an axis and selected for oscillating along the axis with motion sufficient for surgery and at around at least one preferred frequency and wavelength,
- a connecting member fitted to the transducer 12 and extending distally from the transducer 12 along the axis within the housing 11;
- pipe tools 24 attachable to the connecting member so that each pipe tool 24 may be of different lengths and/or configurations tuned to oscillate around at least one preferred frequency and wavelength, and
- an energy initiator 45 for a frequency regulator to maintain a preset vibrational mode and the linear dynamics of an ultrasonic surgical instrument capable of operation at resonance characteristics and under varying loads comprising:
 - an electronic oscillator 46 for driving the transducer 12;
 - an amplitude control connected to the electronic oscillator 46 permitting setting of the level of the ultrasonic vibration;

a frequency regulator between the amplitude control and the electronic oscillator 46;

a frequency control feedback loop 49 in the frequency regulator for maintaining the linear dynamics of the ultrasonic surgical instrument about the preferred
5 frequency;

an operational transconductance amplifier 52 included as part of the electronic oscillator 46 for gain control for the frequency control feedback loop 49, and

a circuit 55 connected to the amplitude control for retarding the rate of the current application per unit of time to the operational transconductance amplifier 52 to
10 ameliorate the effects of the attachable pipe tool 24 of different lengths and/or configurations fitted to the ultrasonic surgical instrument.

8. The pipe tools 24 attachable to the connecting member of Claim 7 wherein each pipe tool 24 may be of different lengths and/or configurations tuned to oscillate
15 around at least one preferred frequency of about 23 kilohertz when part of the acoustic structure of the handpiece.

9. The pipe tools 24 attachable to the connecting member of Claim 8 wherein the excursion length is a function of each pipe tool 24 material, length and configuration
20 tuned to oscillate around the preferred frequency of about 23 kilohertz.

10. The pipe tools 24 attachable to the connecting member of Claim 9 wherein the each pipe tool 24 length is greater than one wavelength and at least $5/4$ wavelengths or $7/4$ wavelengths.

25

11. A flue 17 for an ultrasonic surgical handpiece having an elongate pipe tool 24 that vibrates, the flue 17 forming an annular space surrounding the pipe tool 24 and extending from the handpiece to a vibrating tip 18 on the pipe tool 24 comprising:

a central body 28 which is hollow elongate and semi-rigid for extending
30 with and coaxially about an axis passing centrally therethrough and through the pipe tool 24;

a funnel 29 at one end of the central body 28 for as a proximal portion thereof to first receive the pipe tool 24 vibrating tip 18 when inserted therewithin; and

a nozzle 30 opposite the funnel 29 on the central and body and tapered toward the distal vibrating tip 18 of the ultrasonic surgical handpiece for directing annular flow of fluid from the annular space.

5 12. The flue 17 for an ultrasonic handpiece of Claim 11 wherein at least the funnel 29 and the nozzle 30 are made of a resilient material having a durometer of about thirty.

 13. The flue 17 for an ultrasonic handpiece of Claim 11 wherein the central
10 body 28 is made of a material having a durometer higher than that of the nozzle 30 or the funnel 29.

 14. The flue 17 for an ultrasonic handpiece of Claim 11 wherein the modulus of elasticity of the central body 28 is greater than the modulus of elasticity of either the
15 nozzle 30 or the funnel 29.

 15. The flue 17 for an ultrasonic handpiece of Claim 11 wherein the central body 28 is made of a material having a higher durometer than that of the nozzle 30 or the funnel 29 and the funnel 29 has a mouth to seal 31 about the handpiece.
20

 16. The flue 17 for an ultrasonic handpiece of Claim 15 wherein the central body 28 is an extruded transparent polysulfone tube.

 17. The flue 17 for an ultrasonic handpiece of Claim 16 wherein the nozzle 30
25 and funnel 29 are molded of a silicone rubber and connected to one another by a recess 34 of reduced diameter and the recess 34 being surrounded by the extruded transparent polysulfone tube.

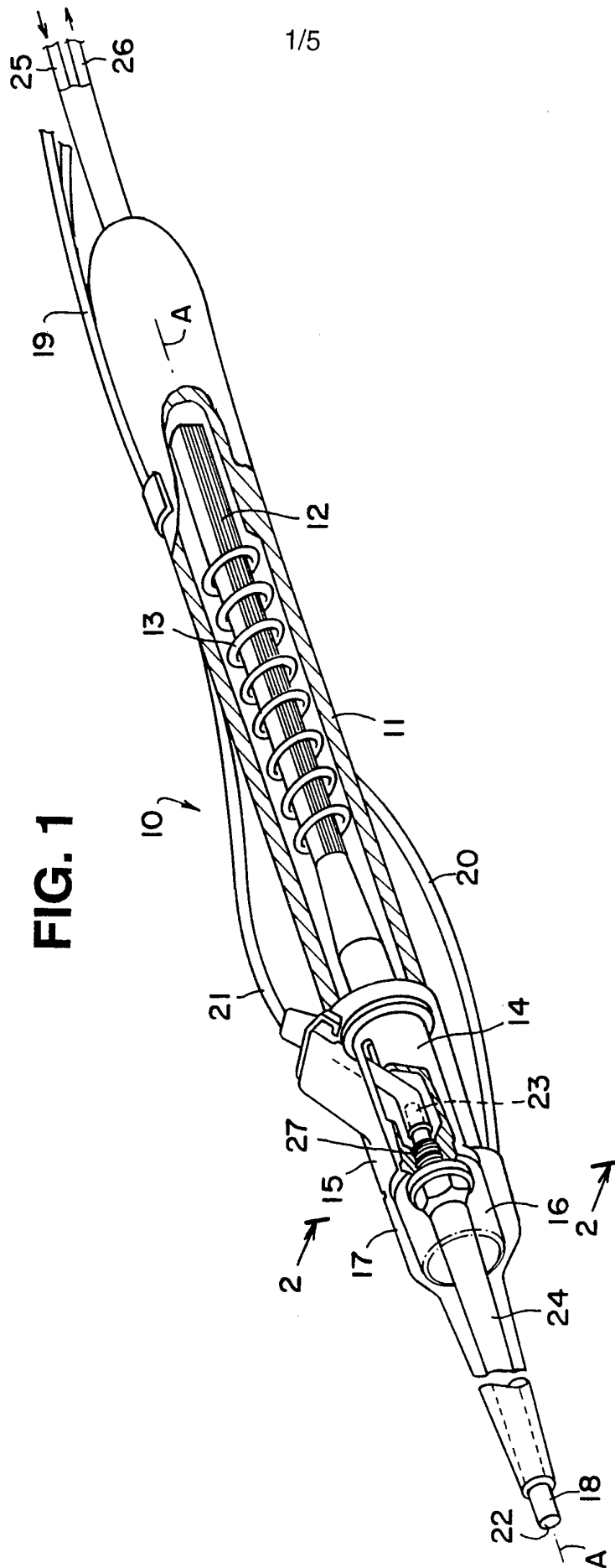
 18. The flue 17 for an ultrasonic handpiece of Claim 11 wherein the nozzle 30
30 and central body 28 are a molded construction of a silicone rubber having a durometer higher than the funnel 29 which is bonded to the proximal portion of the central body 28.

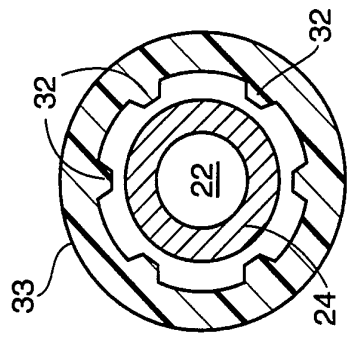
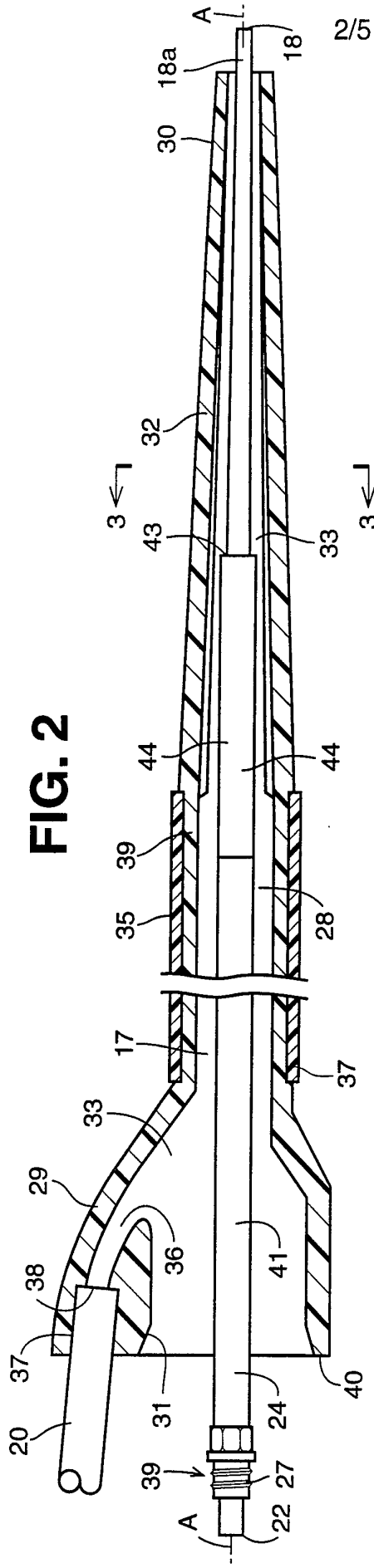
 19. The flue 17 for an ultrasonic handpiece of Claim 18 wherein the funnel 29 is molded of silicone rubber and is of a durometer of about twenty.

20. The flue 17 for an ultrasonic handpiece of Claim 11 wherein the funnel 29 includes a shouldered opening 37 for receiving a tube for supplying cooling and preaspiration fluid.

5 21. The nozzle 30 for an ultrasonic handpiece of Claim 11 wherein reinforcing ridges 32 extending longitudinally inside the nozzle 30 act to concentrically support and coaxially position the nozzle 30 relative to the vibrating tip 18 of the ultrasonic handpiece so fluid passing in the annular space between the flue 17 and the ultrasonic vibrating tip 18 maintains concentricity between the flue and nozzle tip so as to channel irrigant.

10





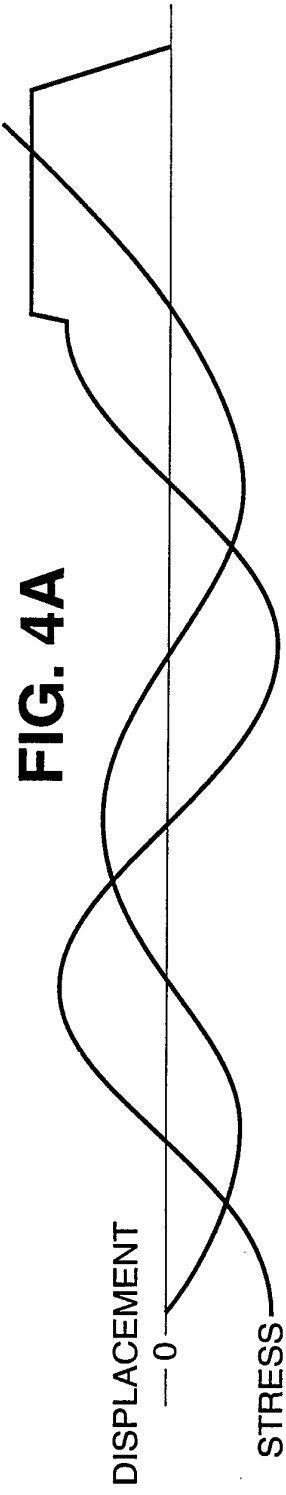


FIG. 4B

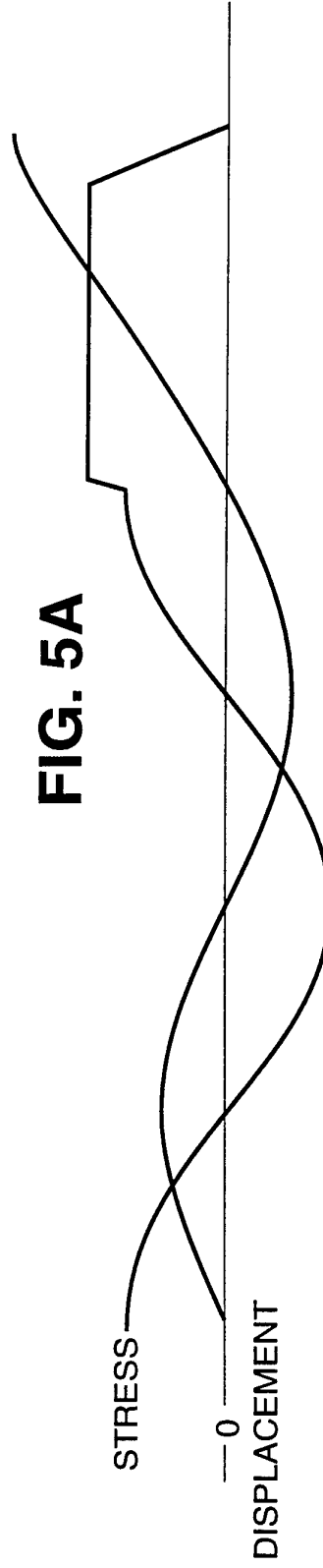
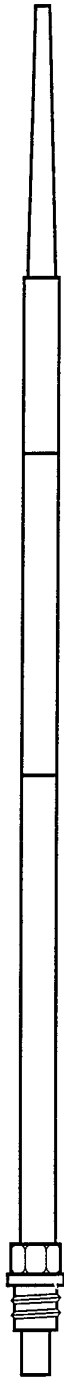
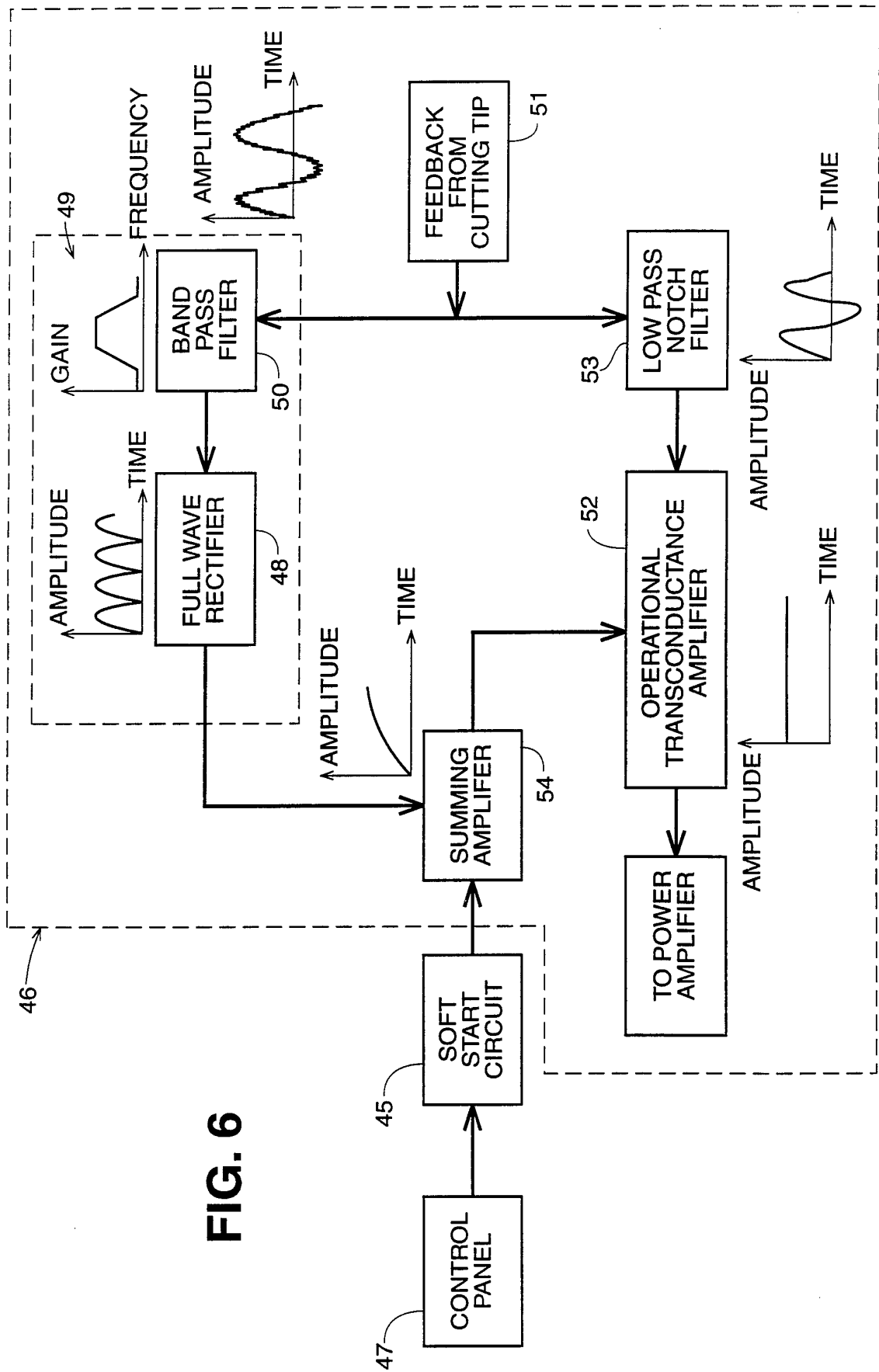


FIG. 5B





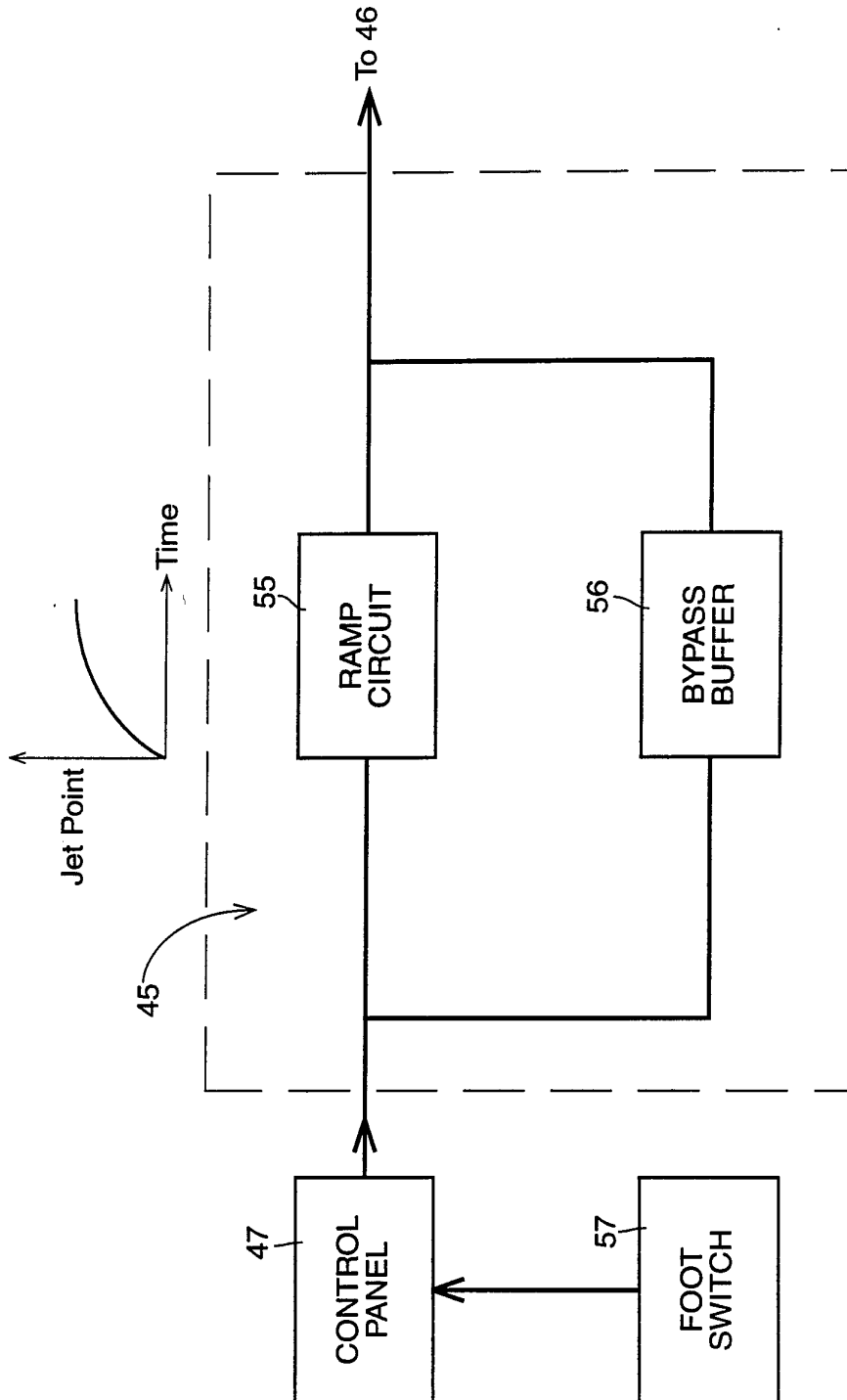


FIG. 7

INTERNATIONAL SEARCH REPORT

International Application No. **PCT/US 93/08614**

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) ⁶		
According to International Patent Classification (IPC) or to both National Classification and IPC: Int.Cl.5 A 61 B 17/32		
II. FIELDS SEARCHED		
Minimum Documentation Searched ⁷		
Classification System	Classification Symbols	
Int.Cl.5	A 61 B	
Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched ⁸		
III. DOCUMENTS CONSIDERED TO BE RELEVANT⁹		
Category ^o	Citation of Document, ¹¹ with indication, where appropriate, of the relevant passages ¹²	Relevant to Claim No. ¹³
A	US,A,5151085 SAKURAI et al. 29 September 1992 29.09.92, figs. 3,6A,6B,9,16; column 5, line 59 - column 7, line 26; column 8, line 53 - column 12, line 59. ---	1,7,8
A	US,A,4587958 NOGUCHI et al. 13 May 1986 13.05.86, figs. 1,2,11; abstract (cited in the application). ---	1,7
A	US,A,4223676 WUCHINICH et al. 23 September 1980 23.09.80, figs. 1,3,4; abstract (cited in the application). -----	1,7,8
<p>^o Special categories of cited documents : ¹⁰</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"&" document member of the same patent family</p>		
IV. CERTIFICATION		
Date of the Actual Completion of the International Search	Date of Mailing of this International Search Report	
07-12-1993	1993	
International Searching Authority	Signature of Authorized Officer	
EUROPEAN PATENT OFFICE	Burghant e.h.	

INTERNATIONAL SEARCH REPORT

International application No.

PCT/US 93/08614

Box I Observations where certain claims were found unsearchable (Continuation of item 1 of first sheet)

This international search report has not been established in respect of certain claims under Article 17(2)(a) for the following reasons:

1. Claims Nos.:
because they relate to subject matter not required to be searched by this Authority, namely:

2. Claims Nos.:
because they relate to parts of the international application that do not comply with the prescribed requirements to such an extent that no meaningful international search can be carried out, specifically:

3. Claims Nos.:
because they are dependent claims and are not drafted in accordance with the second and third sentences of Rule 6.4(a).

Box II Observations where unity of invention is lacking (Continuation of item 2 of first sheet)

This International Searching Authority found multiple inventions in this international application, as follows:

For further information see Form PCT/ISA/206 sent on 20.01.94.

1. As all required additional search fees were timely paid by the applicant, this international search report covers all searchable claims.

2. As all searchable claims could be searched without effort justifying an additional fee, this Authority did not invite payment of any additional fee.

3. As only some of the required additional search fees were timely paid by the applicant, this international search report covers only those claims for which fees were paid, specifically claims Nos.:

4. No required additional search fees were timely paid by the applicant. Consequently, this international search report is restricted to the invention first mentioned in the claims; it is covered by claims Nos.:

1-10

Remark on Protest

- The additional search fees were accompanied by the applicant's protest.
- No protest accompanied the payment of additional search fees.

**ANNEX TO THE INTERNATIONAL SEARCH REPORT
ON INTERNATIONAL PATENT APPLICATION NO.**

US 9308614
SA 79266

This annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the European Patent Office EDP file on 21/02/94. The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US-A- 5151085	29-09-92	JP-A- 2290281 JP-A- 2299646	30-11-90 11-12-90
US-A- 4587958	13-05-86	WO-A- 8403828 EP-A, B 0139753	11-10-84 08-05-85
US-A- 4223676	23-09-80	US-A- 4425115	10-01-84