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(54) Title: COLLOIDAL PARTICLES OF SOLID FLAME RETARDANT AND SMOKE SUPPRESSANT COMPOUNDS AND METHODS FOR MAKING THEM		
(57) Abstract The present invention concerns finely divided particles of compounds that provide flame retardancy and/or smoke suppressant properties to fibers, textiles, polymeric articles, paper, paint, coating and insulation. More particularly, the present invention concerns colloidal-sized particles of hydrated salts, organic phosphates, metal borates, polyamides, solid halogenated flame retardants with a melting point greater than 250 °C, molybdenum compounds, metallocenes, antimony compounds, zinc compounds, bismuth compounds and other solid chemicals which act as flame retardants or smoke suppressants. The present invention also concerns various milling processes to reduce these materials to colloidal sizes and to disperse them in water, organic liquids and meltable solids.		

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**COLLOIDAL PARTICLES OF SOLID FLAME RETARDANT AND SMOKE
SUPPRESSANT COMPOUNDS AND METHODS FOR MAKING THEM**

FIELD OF THE INVENTION

The present invention concerns finely divided particles of compounds that provide flame retardancy and/or smoke suppressant properties to fibers, textiles, polymeric articles, paper, paint, coatings and insulation. More particularly, the present invention concerns colloidal-sized particles of hydrated salts, organic phosphates, metal borates, polyamides, solid halogenated flame retardants with a melting point greater than 250°C, molybdenum compounds, metallocenes, antimony compounds, zinc compounds, bismuth compounds and other solid chemicals which act as flame retardants or smoke suppressants. The present invention also concerns various milling processes to reduce these materials to colloidal sizes and to disperse them in water, organic liquids and meltable solids.

BACKGROUND OF THE INVENTION

The ability of various solids to act as flame retardants and/or smoke suppressants is known in the art. Such solids act by various mechanisms to provide flame retardancy including the following:

- a) Release of Water and/or Carbon Dioxide -
Hydrated salts (such as magnesium sulfate

pentahydrate, aluminum trihydrate, magnesium hydroxide, hydrated magnesium carbonate and so forth) decompose at high temperatures, and release water and or carbon dioxide in an endothermic reaction to quench a fire.

b) Char Formation - When exposed to high temperatures, char formers, which include organic phosphates, zinc compounds, nitrogen compounds (such as melamine esters and polyamides) and metal borates, form char barriers which insulate the combustible materials from the fire.

c) Free Radical Capture/Oxygen Deprivation - Halogen compounds alone or in combination with antimony will prevent combustion. The primary mechanism is believed to be the formation of a dense gas layer above the burning substance that inhibits or prevents oxygen from reaching the combustible material. There is also evidence in support of the ability of antimony halides to scavenge free radicals in the flame, stopping the reaction.

d) Smoke Suppression - Smoke suppressants work by aiding the complete oxidation of carbonaceous materials formed in the flame and/or the formation of char or glasses. They are usually catalysts for oxidation reactions and/or char or glass formers. Typical smoke suppressants are molybdenum oxide and ferrocene or other metallocenes.

All of the above listed solids are used commercially to provide either flame retardancy or low smoke generation to plastics, carpets, fabrics, paper, paints, coatings, adhesives, wood composites and so forth. Unfortunately, the use of such solids often

imparts other undesirable properties to the item to which they are added. Typical undesirable properties that result from adding solid particles of flame retardant or smoke suppressant compounds include:

5 pigmentation (e.g., addition of unwanted colors), opacity (e.g., loss of light transmission), stiffness (e.g., loss of hand in textiles), lowered impact strength (resulting, e.g., an increase in crack propagation), and setting of solids (in, e.g., paints,

10 coatings and adhesives). Such undesirable properties can be reduced or eliminated by reducing average particle size and eliminating substantially all particles above about 1 micron.

15 SUMMARY OF THE INVENTION

Accordingly, it is an object of this invention to provide colloidal particles (particles having a size ranging from 10^{-9} to 10^{-6} m) of solid flame retardant and/or smoke suppressant compounds, including hydrated

20 salts (such as aluminum trihydrate, magnesium sulphate pentahydrate, magnesium hydroxide and hydrated magnesium carbonate), ammonium polyphosphate, organic phosphates (such as melamine pyrophosphate), metal borates (such as zinc borate and barium metaborate), polyamides,

25 melamine, solid halogenated flame retardants with a melting point greater than 250°C (such as brominated polymers, decabromodiphenyloxide, ethylene bis-tetrabromophthalamide, decabromodiphenylethane, and dodecachlorododecahydrodimethanodibenzocyclooctene),

30 molybdenum compounds (such as molybdenum oxide and ammonium octamolybdate), metallocenes (such as ferrocene), antimony compounds (such as antimony metal, antimony trioxide, antimony pentoxide and sodium antimonate), zinc compounds (such as mixed metal oxide

35 of zinc and magnesium, or zinc sulfide) and bismuth compounds (such as bismuth subcarbonate), as well as a process for producing them.

It is also an object of the present invention to provide stable dispersions of these materials in water, organic liquids or meltable solids, and to provide a method for producing the same.

5 Colloidal particles of insoluble, solid flame retardant and/or smoke suppressant compounds are advantageous for use as external flame retardant coatings on textiles or as internal flame retardant additives to systems such as coatings, plastic, textiles
10 and rubber.

Dispersions of such particles are convenient, because they allow the particles to be transported, while simultaneously inhibiting the particles from coalescing into larger agglomerates.

15 These and other objects and advantages have been achieved by the present invention, wherein colloidal-sized particles of insoluble solid flame retardant and/or smoke suppressant compounds are provided by means of a high energy mill, such as a media
20 mill, even though commercial suppliers of such milling equipment do not suggest that such particle sizes can be achieved.

According to an embodiment of the present invention, an agitated media mill loaded with
25 comminuting media is provided with a slurry comprising a fluid vehicle and particles of a solid compound having flame retardant or smoke suppressant properties. The slurry is processed in the agitated media mill until the particles are reduced in size by at least 10%, more
30 preferably 50 to 90%, and even more preferably 10 to 99%. Moreover, the particles have a volumetric average particle size of less than 0.5 micron, preferably 0.01 to 0.5 micron, more preferably 0.01 to 0.25 micron, and even more preferably 0.01 to 0.1 micron. It is
35 preferred that at least 99% of said particles have sizes less than 1 micron. More preferably at least 99.9% of the particles should have sizes less than 1 micron. It

is also preferred that the slurry further comprise a dispersion agent.

Other objects and advantages of the invention and alternative embodiments will readily become apparent to those skilled in the art, particularly after reading the detailed description, and examples set forth below.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

Wet media milling is the preferred process for making the finely divided particles of the present invention. In general, the ultimate characteristics of material comminuted in a wet media mill, particularly the particle size, is determined by several processing variables.

For example, the type of mill can affect the ultimate characteristics of the comminuted materials. The mill type can also determine how quickly a particular result may be achieved.

Other factors also determine the ultimate characteristics of the comminuted material, as well as the time and energy it takes to achieve them. Examples of such factors include the following:

(1) In wet media milling, smaller media are more efficient in producing finer particles within times of 10 minutes and less.

(2) More dense media and higher tip speeds are desired to impart more energy to the particles being comminuted.

(3) Lower fluid viscosities are beneficial in comminuting particles.

(4) As the particles are reduced in diameter, exposed surface areas increase, and a dispersion agent is generally used to keep small particles from agglomerating. In some cases dilution alone can help achieve a particular ultimate particle size, but a dispersion agent is generally used to achieve long-term stability against agglomeration.

The above and other factors that influence comminuting performance is discussed in the paragraphs that follow.

As used herein "particle size" refers to a volumetric average particle size as measured by conventional particle size measuring techniques such as sedimentation, photon correlation spectroscopy, field flow fractionation, disk centrifugation, transmission electron microscopy, and dynamic light scattering. A dynamic light scattering device such as a Horiba LA-900 Laser Scattering particle size analyzer (Horiba Instruments, Irvine, California) is preferred by the present inventors, because it has advantages of easy sample preparation and speed. The volumetric distribution of the sample relates to the weight distribution.

Milling Equipment

The milling equipment preferred for the practice of the invention are generally known as a wet agitated media mills, wherein comminuting media are agitated in a milling chamber. The preferred method of agitation is by means of an agitator comprising a rotating shaft, such as those found in attritor mills. The shaft may be provided with disks, arms, pins, or other attachments. The portion of the attachment that is radially the most remote from the shaft is referred to herein as the "tip". The mills may be batch or continuous, vertical or horizontal. A ball mill is an example of a rudimentary agitated media mill.

A horizontal continuous media mill equipped with an internal screen having hole sizes that are $1/2$ to $1/3$ the media diameter is preferred as an efficient media mill for the practice of the present invention. High loadings of media are possible (e.g., loadings of 92%).

An increase in the amount of comminuting media in the chamber will increase comminuting efficiency by decreasing the distances between individual comminuting

media particles and increasing the number of surfaces available to shear the material to be comminuted. The volume of comminuting media can be increased until the comminuting media constitutes up to about 92% of the mill chamber bulk volume (dead space between particles is excluded). At levels substantially above this point, the media locks up.

Starting Materials

10 By the present invention, flame retardants or smoke suppressants can be wet milled to levels that are currently not achievable with dry milling techniques.

Within reason, the size of the feed material that is to be comminuted is not critical. For example, 15 antimony trioxide can be reduced to a 0.10 micron average particle size with an agitated media mill using the process of the present invention, whether starting from particles that have an average particle size of 4.3 microns, 2.0 microns, or 0.6 micron. However, in 20 generally, the feed material should not be more than 10% of the size of the comminuting media. Other flame retardants such as decabromodiphenyl oxide and zinc borate can be similarly reduced to 0.25 and 0.14 micron or less, respectively, in short comminuting times.

25 Faster milling times can be achieved, if smaller starting materials are used. Thus, it is preferable to start with particles that are as small as is economically feasible, to reduce milling time. For example, 0.5 micron antimony trioxide feed material (as 30 measured by Transmission Electron Microscopy) can be comminuted to a desired size (e.g., .1 micron) in a shorter time than can a 4.3 micron material. For this reason, antimony trioxide having a 0.5 micron average particle size is preferred to material having a larger 35 particle size. When such material is used, a tight particle distribution can be achieved, as well as a short milling time.

Comminuting Media

Acceptable comminuting media for the practice of the present invention include sand, glass beads, metals, and ceramics. Preferred glass beads include barium titanite (leaded), soda lime (unleaded), and borosilicate. Preferred metals include carbon steel, stainless steel and tungsten carbide. Preferred ceramics include yttrium stabilized zirconium oxide, zirconium silicate, and alumina. The most preferred comminuting media for the purpose of the invention is yttrium stabilized zirconium oxide.

Each type of media has its own advantages. For example, metals have high specific gravities, which increase comminuting efficiency due to increased impact. Metal costs range from low to high, and contamination may be an issue. Glasses are advantageous from the standpoint of low cost and the availability of small sizes as low as .004 mm. Such small sizes make possible a finer ultimate particle size. The specific gravity of glasses, however, is lower than other media and more milling time is required. Finally, ceramics are advantageous from the standpoint of low wear, low porosity and ease of cleaning.

The comminuting media used for particle size reduction are preferably spherical. As noted previously, smaller comminuting media sizes result in smaller ultimate particle sizes. The comminuting media for the practice of the present invention preferably have an average size ranging from 0.004 to 1.2mm, more preferably 0.012 to 0.2mm. By using properly selected comminuting media, the milling process of the present invention actually comminutes particles, rather than deagglomerating clumps of particles--a task for which media mills are normally used.

Fluid Vehicles

Fluid vehicles in which the particles may be comminuted and dispersed include water, organic liquids (such as dimethylacetamide or ethylene glycol),
5 polyvinyl chloride plasticizers (such as diisodecylphthalate) and low melting solids such as waxes or fats wherein the milling is conducted at temperatures greater than the melting point of the waxes or fats. In general, as long as the fluid vehicle used
10 has a reasonable viscosity and does not adversely affect the chemical or physical characteristics of the particles, the choice of fluid vehicle is optional. Water is ordinarily preferred.

15 Dispersion Agents

Dispersion agents preferably act to wet newly exposed surfaces that result when particles are broken open. Dispersion agents also preferably stabilize the resulting slurry of milled particles by providing either
20 (1) a positive or negative electric charge on the milled particles or (2) steric blocking through the use of a large bulking molecule. An electric charge is preferably introduced by means of anionic and cationic surfactants, while steric blocking is preferably
25 performed by absorbed polymers with charges on the particle which repel each other. Zwitterionic surfactants can have both anionic and cationic surfactant characteristics on the same molecule.

Preferred dispersion agents for the practice of the
30 invention include wetting agents (such as Triton X-100 and Triton CF-10, sold by Union Carbide, Danbury, Connecticut, and Neodol 91-6, sold by Shell Chemical); anionic surfactants (such as Tamol 731, Tamol 931 and Tamol-SN, sold by Rohm & Haas, Philadelphia,
35 Pennsylvania, and Colloid 226/35, sold by Rhone Poulenc); cationic surfactants (such as Disperbyke 182 sold by Byke Chemie, Wellingford, Connecticut);

amphoteric surfactants (such as Crosultain T-30 and Incrosoft T-90, sold by Croda, Inc., Parsippany, New Jersey); and non-ionic surfactants (such as Disperse-Ayd W-22 sold by Daniel Products Co., Jersey City, New Jersey). Most preferred dispersion agents are anionic surfactants such as Tamol-SN.

Other Milling Parameters

The relative proportions of particles to be comminuted, fluid vehicles, comminuting media and dispersion agents may be optimized for the practice of the present invention.

Preferably, the final slurry exiting the mill comprises the following: (1) 5 to 60 wt%, more preferably 15 to 45 wt% of the particle to be comminuted (2) 40 to 95 wt%, more preferably 55 to 85 wt% of the fluid vehicle; and (3) 2 to 15 wt%, more preferably 6 to 10 wt% of the dispersion agent.

Preferably the comminuting media loading as a percent of the mill chamber volume is 80 to 92%, more preferably 85 to 90%.

The agitator speed controls the amount of energy that is put into the mill. The higher the agitator speed, the more kinetic energy is put into the mill. Higher kinetic energy results in greater comminuting efficiency, due to higher shear and impact. Thus, an increase in agitator RPM results in an increase in comminuting efficiency. Although generally desirable, it is understood by those skilled in the art that an increase in comminuting efficiency will be accompanied by a concurrent increase in chamber temperature, chamber pressure, and wear rate.

The tip speed of the agitator represents the maximum velocity (and, thus, kinetic energy) experienced by the particles to be milled. Thus, larger diameter mills can impart media velocities equal to those of smaller mills at a lower RPM.

Residence time (referred to cumulatively as retention time) is the amount of time that the material spends in the comminuting chamber while being exposed to the comminuting media. Residence time is calculated by simply determining the comminuting volume that is available for the mill and dividing this figure by the rate of flow through the mill (throughput rate). In general, a certain residence time will be required to achieve the ultimate product characteristics desired (e.g., final product size). If this residence time can be reduced, a higher throughput rate can be achieved, minimizing capital costs. For the practice of the present invention, the residence time can vary, but is preferably less than 15 minutes, and more preferably less than 10 minutes.

It is often desirable to stage two or more mills in series, particularly when dramatic reductions in particle size are necessary to optimize comminution efficiency. Maximum particle size reduction within a given milling step typically ranges from about 10:1 to as high as about 40:1 and is to some extent dependent upon media size. As a result, the number of milling steps increases as the overall size reduction requirement increases. Effects similar to that of staged mills can also be achieved using a single mill by collecting the output and repeatedly feeding the output through the mill. However, residence time may be longer to achieve similar ultimate particle size.

30 EXAMPLES

The following examples, as well as the foregoing description of the invention and its various embodiments, are not intended to be limiting of the invention but rather are illustrative thereof. Those skilled in the art can formulate further embodiments encompassed within the scope of the present invention.

Example 1

A 10 liter horizontal continuous media mill (Netzsch, Inc., Exton, Pennsylvania) was 90% filled with YTZ (yttrium stabilized zirconium oxide) media with an average diameter of 0.2mm and a specific gravity of 5.95 (Tosoh Corp., Bound Brook, New Jersey). A 0.1 mm screen was installed inside the mill at the outlet. Forty-five pounds of antimony trioxide with an average starting particle size of 2.0 microns (Cookson Specialty Additives, Anzon Division, Philadelphia, Pennsylvania) were slurried in 55 pounds of water and 4.5 pounds of Tamol-SN.

The mill was operated at a tip speed that averaged 2856 feet per minute. After 7.5 minutes of retention time (5 passes through the mill) the average particle size, by volume, was reduced to 0.102 micron and 99.9% of the particles had sizes less than 0.345 micron.

Example 2

The same mill, media and loading as in Example 1 were used. This time, antimony trioxide feed having a 0.6 micron average particle size (Cookson Specialty Additives, Anzon Division, Philadelphia, Pennsylvania) was used. Thirty pounds of the antimony trioxide were slurried with 70 pounds of water and 1.8 pounds of Tamol-SN and 0.9 pounds of Triton CF-10.

The tip speed during the run averaged 2878 feet per minute. After 4.8 minutes of retention time in the mill (4 passes), the volume average particle size was 0.11 micron and 99.9% of the particles had sizes less than 0.31 micron.

Example 3

The same mill, media, antimony trioxide and loading as in Example 1 were used. This time no surfactants were used.

Twenty-eight pounds of the antimony trioxide were slurried with 100 pounds of water. Tip speed was 3023 feet per minute. After 2.4 minutes of retention time (2 passes). The average particle was 0.13 micron with
5 99.9% of the particles having sizes less than 1.06 micron.

Since the viscosity of the product was high, 35 additional pounds of water were added. After 1.8 minutes of additional retention time (2 extra passes),
10 the average particle size was further reduced to 0.10 micron, with 99.9% of the particles having sizes less than 0.32 micron.

Example 4

15 The same mill, media, and loading as in Example 1 were used. Thirty pounds of 4 micron antimony trioxide feed material (Cookson Specialty Additives, Anzon Division) were slurried with 70 pounds of water and 2.8 pounds of Tamol-SN. Tip speed was 2860 feet per minute.
20 After 7 minutes of retention time (5 passes), the average particle size was 0.10 micron with 99.9% of the particles having sizes less than 1.2 micron.

Example 5

25 Using the same mill, media and loading of Example 1, 80 pounds of a brominated organic flame retardant (decabromodiphenyl oxide) (Arblemarle, Inc. Baton Rouge, Louisiana; Great Lakes, Lafayette, Indiana; Ameribrom, Inc., New York, New York) were slurried with 55 pounds
30 of water. The starting particle size averaged 2.7 microns with some particles as large as 10 microns. After 10.4 minutes of retention time (6 passes), the average particle size was 0.25 micron, with 99.9% of the particles having a size less than 2.70 micron.

Example 6

The 10 liter horizontal media mill of Example 1 was 90% filled with 4-6mm electrofused zirconia/silica ceramic beads having a specific gravity of 3.85 (SEPR, Mountainside, New Jersey). The same .1 mm screen of Example 1 was used inside the mill.

50 pounds of 2 micron antimony trioxide feed were mixed with 11 pounds of water and 5 pounds of Tamol-SN. After 7.8 minutes of retention time, the average particle size was 0.20 micron, with 99.9% of the particles having sizes below 0.46 micron.

Example 7

A 10 liter horizontal media mill of Example 1 was 90% loaded with borosilicate glass beads having a .093mm mean diameter and a specific gravity of 2.6 sold by Potters Industries. A .025mm screen was used in the mill.

Fifty pounds of 0.6 micron antimony trioxide were slurried with 61 pounds of water and 5 pounds of Tamol-SN. The tip speed was 3420 feet per minute. Mill amperage was only 67% of similar runs using the 5.95 specific gravity media. The resulting antimony trioxide product had a 0.09 micron average particle size, with 100% of the particles having sizes less than .30 micron.

Example 8

The 10 liter continuous horizontal media mill Example 1 was 90% loaded with the YTZ media of Example 1. Fifty pounds of zinc borate having an average particle size of 9.8 microns (Cookson Specialty Additives, Anzon Division, Philadelphia, Pennsylvania) were slurried in 93 pounds of water and 3 pounds of Tamol-SN.

Tip speed was 2788 feet per minute. After 8.9 minutes (4 passes) of retention time, the average

particle size was reduced to .14 micron, with 99.9% of the particles having sizes less than .41 micron.

Example 9

5 An attritor (Union Process, Inc., Akron, Ohio) with
a 750 cc tank volume was loaded with 250 cc of YTZ
powder (Metco, Inc., Westbury, New York) screened to a
size of .053mm. 180 g of the slurry of Example 1 were
added to the attritor. After running the attritor at
10 4000 RPM (3600 ft/min tip speed) for 60 minutes, the
average particle size of the resulting product was 0.07
microns.

CLAIMS

What is claimed is:

1 1. Finely divided particles of a solid chemical
2 compound having flame retardant or smoke suppressant
3 properties, said particles having a volumetric average
4 particle size of less than 0.5 microns, and said
5 particles being produced by comminution.

1 2. The finely divided particles of claim 1,
2 wherein at least 99% of said particles have sizes less
3 than 1 micron.

1 3. The finely divided particles of claim 1,
2 wherein said solid chemical compound is selected from
3 the group consisting of hydrated salts, organic
4 phosphates, metal borates, polyamides, solid halogenated
5 flame retardants with a melting point greater than
6 250°C, molybdenum compounds, metallocenes, antimony
7 compounds, zinc compounds, and bismuth compounds.

1 4. The finely divided particles of claim 1,
2 wherein said solid chemical compound is selected from
3 the group consisting of aluminum trihydrate, magnesium
4 sulphate pentahydrate, magnesium hydroxide, hydrated
5 magnesium carbonate, ammonium polyphosphate, melamine
6 pyrophosphate, barium metaborate, melamine, brominated
7 polymers, ethylene bis-tetrabromophthalamide,
8 decabromodiphenylethane,
9 dodecachlorododecahydrodimethanodibenzocyclooctene,
10 molybdenum oxide, ammonium octamolybdate, ferrocene,
11 antimony metal, antimony pentoxide, sodium antimonate,
12 mixed metal oxide of zinc and magnesium, zinc sulfide
13 and bismuth subcarbonate.

1 5. The finely divided particles of claim 1,
2 wherein said solid chemical compound is zinc borate.

1 6. The finely divided particles of claim 1,
2 wherein said solid chemical compound is
3 decabromodiphenyloxide.

1 7. The finely divided particles of claim 1,
2 wherein said solid chemical compound is antimony
3 trioxide.

1 8. A dispersion comprising a fluid vehicle, a
2 dispersion agent and the particles of claim 1.

1 9. The dispersion of claim 8, wherein said fluid
2 vehicle is selected from the group consisting of organic
3 liquids, polyvinyl chloride plasticizers and low melting
4 point waxes or fats.

1 10. The dispersion of claim 8, wherein said fluid
2 vehicle is selected from the group consisting of
3 dimethylacetamide, ethylene glycol and
4 diisodecylphthalate.

1 11. The dispersion of claim 8, wherein said fluid
2 vehicle is water.

1 12. The dispersion of claim 8, wherein said
2 dispersion agent is selected from the group consisting
3 of cationic surfactants, amphoteric surfactants, and
4 non-ionic surfactants.

1 13. The dispersion of claim 8, wherein said
2 dispersion agent is selected from the group consisting
3 of wetting agents and anionic surfactants.

1 14. A process for producing finely divided
2 particles of a solid compound having flame retardant or
3 smoke suppressant properties comprising:
4 loading an agitated media mill with comminuting
5 media, a fluid vehicle, and particles of a solid
6 compound having flame retardant or smoke suppressant
7 properties; and
8 agitating said comminuting media, fluid vehicle,
9 and particles until said particles are reduced in size
10 by at least 10% and have a volumetric average particle
11 size of less than 0.5 microns, wherein at least 99% of
12 said particles is sized less than 1 micron.

1 15. The process of claim 14 wherein said slurry
2 further comprises a dispersion agent.

1 16. The process of claim 14, wherein said agitated
2 media mill is operated at a tip speed ranging from 1000
3 to 6000 feet per minute.

1 17. The process of claim 14, wherein said
2 comminuting media are provided in an amount sufficient
3 to fill about 80 to 92% of the bulk volume within said
4 mill.

1 18. The process of claim 14, wherein said
2 comminuting media are selected from the group consisting
3 of sand, glass beads, metals, and ceramics.

1 19. The process of claim 18, wherein said
2 comminuting media are selected from the group consisting
3 of barium titanite, leaded soda lime, borosilicate,
4 carbon steel, stainless steel, tungsten carbide,
5 zirconium silicate, and alumina.

1 20. The process of claim 19, wherein said media is
2 yttrium stabilized zirconium oxide.

1 21. The process of claim 14, wherein said solid
2 chemical compound is selected from the group consisting
3 of hydrated salts, organic phosphates, metal borates,
4 polyamides, solid halogenated flame retardants with a
5 melting point greater than 250°C, molybdenum compounds,
6 metallocenes, antimony compounds, zinc compounds, and
7 bismuth compounds.

1 22. The process of claim 14, wherein said solid
2 chemical compound is selected from the group consisting
3 of zinc borate, decabromodiphenyloxide and antimony
4 trioxide.

1 23. The process of claim 14, wherein said fluid
2 vehicle is selected from the group consisting of organic
3 liquids, polyvinyl chloride plasticizers and low melting
4 point waxes or fats.

1 24. The process of claim 14, wherein said fluid
2 vehicle is selected from the group consisting of
3 dimethylacetamide, ethylene glycol and
4 diisodecylphthalate.

1 25. The process of claim 14, wherein said fluid
2 vehicle is water.

1 26. The process of claim 15, wherein said
2 dispersion agent is selected from the group consisting
3 of cationic surfactants, amphoteric surfactants, and
4 non-ionic surfactants.

1 27. The process of claim 14, wherein said
2 dispersion agent is selected from the group consisting
3 of wetting agents and anionic surfactants.

- 1 28. Finely divided particles of a solid chemical
- 2 compound having flame retardant or smoke suppressant
- 3 properties, produced by the process of claim 14.

INTERNATIONAL SEARCH REPORT

International application No.
PCT/US96/10095

A. CLASSIFICATION OF SUBJECT MATTER

IPC(6) : A62D 1/00; C09K 21/00

US CL : 252/2, 8, 601

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 252/2, 8, 601

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
APS, CAS ONLINE

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X -- Y	US, A, 5,083,712 (ASKEW ET AL) 28 January 1992, see abstract, column 8, lines 24-41.	14-15, 21-22, 25-28 ----- 16-20, 23-24
X	US, A, 4,690,970 (FEINAUER ET AL) 01 September 1987, see abstract, column 6, lines 1-5, column 6, line 57 to column 7, line 53.	1-4, 8-13, 28
X	US, A, 4,120,798 (MISCHTIN) 17 October 1978, column 12, lines 7-31, column 5, line 6 to column 10, line 40.	1-4, 8-13, 28
Y	US, A, 3,951,894 (WHELAN) 20 April 1976, column 1, line 1 to column 2, line 40, column 3 line 66 to column 4, line 23.	5-7

☐ Further documents are listed in the continuation of Box C. ☐ See patent family annex.

* Special categories of cited documents:	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"A" document defining the general state of the art which is not considered to be of particular relevance	"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"E" earlier document published on or after the international filing date	"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"&" document member of the same patent family
"O" document referring to an oral disclosure, use, exhibition or other means	
"P" document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search

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Name and mailing address of the ISA/US
Commissioner of Patents and Trademarks
Box PCT
Washington, D.C. 20231

Facsimile No. (703) 305-3230

Authorized officer

SHEAN C. WU

Telephone No. (703) 308-1235