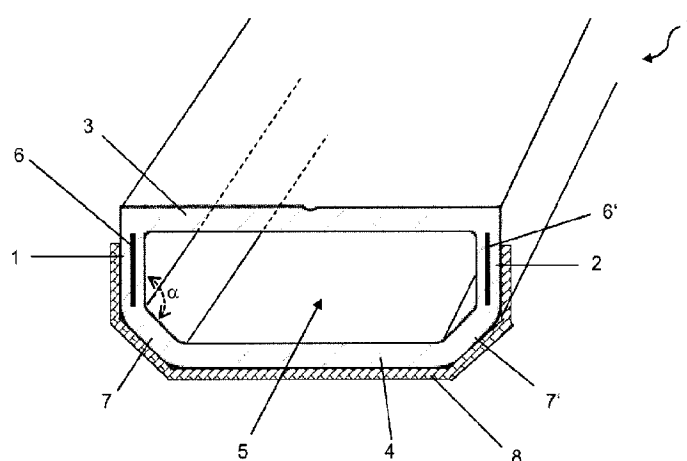




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(54) Titre : ECARTEUR RENFORCE PAR DES FIBRES DE VERRE POUR UN VITRAGE ISOLANT  
(54) Title: GLASS-FIBER-REINFORCED SPACER FOR INSULATING GLAZING UNIT



(57) **Abrégé/Abstract:**

The present invention relates to a spacer for an insulating glazing unit, at least comprising a polymeric main body, at least comprising two parallel side walls that are connected to one another by an inner wall and an outer wall, wherein the side walls, the inner wall, and the outer wall surround a hollow chamber, wherein the main body

- has a glass fiber content of 0 wt.-% to 40 wt.-%, and
- has, due to hollow spaces, a weight reduction of 10 wt.-% to 20 wt.-%.

## **Abstract**

The present invention relates to a spacer for an insulating glazing unit, at least comprising a polymeric main body, at least comprising two parallel side walls that are connected to one another by an inner wall and an outer wall, wherein the side walls, the inner wall, and the outer wall surround a hollow chamber,

wherein the main body

- has a glass fiber content of 0 wt.-% to 40 wt.-%, and
- has, due to hollow spaces, a weight reduction of 10 wt.-% to 20 wt.-%.

## Glass-Fiber-Reinforced Spacer for Insulating Glazing Unit

The invention relates to a glass-fiber-reinforced spacer for an insulating glazing unit, a method for its production, and its use.

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In the window and façade region of buildings, insulating glazing units are used almost exclusively nowadays. Insulating glazing units consist for the most part of two glass panes, which are arranged at a defined distance from each other by means of a spacer. The spacer is arranged peripherally in the edge region of the glazing unit. An intermediate space, which is usually filled with an inert gas, is thus formed between the panes. The flow of heat between the interior space delimited by the glazing unit and the external environment can be significantly reduced by the insulating glazing unit compared to a simple glazing.

The spacer has a non-negligible influence on the thermal properties of the pane. Conventional spacers are made of a light metal, customarily aluminum. These can be easily processed. The spacer is typically produced as a straight endless profile, which is cut to the necessary size and then brought by bending into the rectangular shape necessary for use in the insulating glazing unit. Due to the good thermal conductivity of the aluminum, the insulating effect of the glazing unit is, however, significantly reduced in the edge region (cold edge effect).

In order to improve the thermal properties, so-called "warm edge" solutions for spacers are known. These spacers are made in particular of plastic and, consequently, have significantly reduced thermal conductivity. Plastic spacers are known, for example, from DE 27 52 542 C2 or DE 19 625 845 A1.

WO 2013/104507 A1 discloses a spacer with a polymeric main body and an insulation film. The insulation film contains a polymeric film and at least two metallic or ceramic layers that are arranged alternately with at least one polymeric layer, with the outer layers preferably being polymeric layers. The metallic layers have a thickness of less than 1 µm and have to be protected by polymeric layers. Otherwise, damage to the metallic layers readily occurs during automated processing of the spacer during assembly of the insulating glazing units.

EP 0 852 280 A1 discloses a spacer for multipane insulating glazing units. The spacer includes a metal foil with a thickness of less than 0.1 mm on the adhesive surface and glass fiber content in the plastic of the main body. During further processing in the insulating

glazing unit, the outer metal foil is exposed to high mechanical stresses. In particular, when spacers are further processed on automated production lines, damage to the metal foil and, thus, degradation of the barrier action readily occur.

- 5 There exists a need for spacers for insulating glazing units, which ensure minimal thermal conductivity and are nevertheless simple to process. In particular, there is a need for spacers with which the retention of the mechanical properties can be further improved and which can be produced with reduced costs.
- 10 The object of the present invention is to provide such a spacer for insulating glazing production. A further object of the present invention is to provide a method for producing such a spacer for insulating glazing production. Yet another object of the present invention is to provide a use of such a spacer for insulating glazing production.
- 15 The object of the present invention is accomplished by a spacer for insulating glazing production that comprises a polymeric main body that has at least two parallel side walls, which are connected to one another by an inner wall and an outer wall, wherein the side walls, the inner wall, and the outer wall surround a hollow chamber, wherein the main body has a glass fiber content of 0 wt.-% to 40 wt.-% and has a weight reduction of 10 wt.-% to
- 20 20 wt.-% due to enclosed gas-filled hollow spaces.

The present object is achieved by a spacer for the insulating glazing unit according to the invention that is produced by the foaming of the plastic during the extrusion process. The spacer according to the invention has an improvement of the thermal properties while retaining

25 the mechanical properties with reduced production costs.

In the spacer according to the invention, due to foaming during the extrusion, the walls of the hollow profile are no longer implemented as solid material but are, instead, permeated by gas bubbles, i.e., hollow spaces. In this manner, depending on the case, up to 10 wt.-% to

30 20 wt.-%, preferably from 11 wt.-% to 14 wt.-% of the material can be saved.

The spacer according to the invention has substantially higher strength and fracture resistance. The spacer according to the invention has substantially higher elasticity.

With the spacer according to the invention, a glass-fiber-reinforced plastic is improved in its thermal properties by slight foaming during extrusion, without degrading its mechanical properties. For the thermal properties, an improvement of as much as 45% has been measured. The thermal properties are greatly improved by the gases entrapped in the hollow spaces. The inactive gases entrapped in the hollow spaces act as a very good insulator.

A preferred embodiment of the present invention is a spacer, wherein the enclosed gas-filled hollow spaces are obtained by addition of at least one foaming agent. Preferably, this is chemical foaming. A blowing agent, in most cases in the form of a so-called masterbatch granulate is added to the plastic granulate. By addition of heat, a volatile component, usually carbon dioxide, separates from the blowing agent, resulting in the foaming of the molten material.

A preferred embodiment of the present invention is a spacer, wherein the amount of the foaming agent added is 0.5 wt.-% to 1.5 wt.-%. The foaming agent is added in granulate form to the polymer before the melting in the extruder.

A preferred embodiment of the present invention is a spacer, wherein the amount of the foaming agent added is 0.7 wt.-% to 1.0 wt.-%. In this range, particularly good results are obtained with the foaming agent.

A preferred embodiment of the present invention is a spacer, wherein the main body contains 1.0 wt.-% to 4.0 wt.-%, preferably 1.3 wt.-% to 2.0 wt.-% color masterbatch. In this range, particularly good coloring action is obtained. In the context of the invention, "color masterbatch" means a plastic additive in the form of a granulate that contains a colorant.

A preferred embodiment of the present invention is a spacer, wherein the main body (I) is fracture-resistant up to an applied force of 1800 N to 2500 N. The high fracture resistance is very advantageous for the spacer.

A preferred embodiment of the present invention is a spacer, wherein the main body (I) contains at least, polyethylene (PE), polycarbonates (PC), polystyrene, polybutadiene, polynitriles, polyesters, polyurethanes, polymethylmethacrylates, polyacrylates, polyamides, polyethylene terephthalate (PET), polybutylene terephthalate (PBT), preferably

polypropylene (PP), acrylonitrile butadiene styrene (ABS), acrylonitrile styrene acrylester (ASA), acrylonitrile butadiene styrene/polycarbonate (ABS/PC), styrene acrylonitrile (SAN), polyethylene terephthalate/polycarbonate (PET/PC), polybutylene terephthalate/polycarbonate (PBT/PC) or copolymers or derivatives or mixtures thereof.

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A particularly preferred embodiment of the present invention is a spacer, wherein the main body (I) contains at least, styrene acrylonitrile (SAN) or polypropylene (PP), or copolymers or derivatives or mixtures thereof. With these polymers, in particular with foaming, very good results are obtained in terms of thermal properties as well as fracture resistance and elasticity.

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A preferred embodiment of the present invention is a spacer, wherein the spacer has, at least on the outer wall, an insulation film that contains a polymeric carrier film and at least one metallic or ceramic layer; the thickness of the polymeric carrier film of the insulation film is from 10  $\mu\text{m}$  to 100  $\mu\text{m}$  and the thickness of the metallic or ceramic layer of the insulation film is from 10 nm to 1500 nm, and wherein the installation film contains at least one more polymeric layer with a thickness of 5  $\mu\text{m}$  to 100  $\mu\text{m}$  and the metallic or ceramic layer of the insulation film contains at least iron, aluminum, silver, copper, gold, chromium, silicon oxide, silicon nitride, or alloys or mixtures or oxides thereof, and wherein the polymeric carrier film of the insulation film contains at least polyethylene terephthalate, ethylene vinyl alcohol, polyvinylidene chloride, polyamides, polyethylene, polypropylene, silicones, acrylonitriles, polymethyl acrylates, or copolymers or mixtures.

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A preferred embodiment of the present invention is a spacer, wherein, in each side wall, a reinforcing strip is embedded, which contains at least a metal or a metallic alloy, preferably steel, and has a thickness of 0.05 mm to 1 mm, and a width of 1 mm to 5 mm. By means of the embedded reinforcing strip, the spacer obtains unexpected stability.

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The reinforcing strips give the spacer the necessary bendability to be processed even with conventional industrial systems. The spacer can be bent into its final shape without having to be previously heated. By means of the reinforcing strips, the shape remains durably stable. In addition, the reinforcing strip increases the stability of the spacer. The reinforcing strips do not, however, act as a thermal bridge such that the properties of the spacer in terms of thermal conduction are not substantially adversely affected. There are, in particular, two reasons for this: (a) the reinforcing strips are embedded in the polymeric main body, thus have no contact with the environment; (b) the reinforcing strips are arranged in the side walls

and not, for example, in the outer wall or the inner wall, via which the heat exchange between the interpane space and the external environment occurs. The simultaneous realization of bendability and optimum thermal properties as well as the increased fracture resistance and elasticity are key advantages of this preferred embodiment.

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The object of the present invention is further accomplished by a method for producing a spacer for an insulating glazing unit, wherein

- a) a mixture of at least one polymer, color masterbatch, and foaming agent is prepared,
- b) the mixture is melted in an extruder at a temperature of 170 °C to 230 °C,
- 10 c) the foaming agent is decomposed and volatile components foam the molten material,
- d) the molten material is pressed by a mold and a main body it is obtained,
- e) the main body is stabilized, and
- f) the main body is cooled.

15 A preferred embodiment of the present invention is a method, wherein a granulate mixture at least containing 95.0 wt.-% to 99.0 wt.-% polymer with 30.0 wt.-% to 40.0 wt.-% glass fibers, 1.0 wt.-% to 4.0 wt.-% color masterbatch, and 0.5 wt.-% to 1.5 wt.-% foaming agent is provided. This mixing ratio is particularly advantageous for producing a foamed spacer.

20 A preferred embodiment of the present invention is a method, wherein the mixture is melted in an extruder at a temperature of 215 °C to 220 °C. With these melting temperatures, very good results are obtained with the foamed spacer.

The invention further includes the use of the spacer according to the invention in multiple  
25 glazing units, preferably in insulating glazing units. The insulating glazing units are preferably used as window glazings or façade glazings of buildings.

In the following, the invention is explained in detail with reference to drawings and exemplary  
30 embodiments. The drawings are a schematic representation and not true to scale. The drawings in no way restrict the invention.

They depict:

- Fig. 1 a perspective cross-section through an embodiment of the spacer according to the invention,
- 35 Fig. 2 a cross-section through an embodiment of the insulating glazing unit according to the invention with the spacer according to the invention,

Fig. 3 a flowchart of an embodiment of the method according to the invention,

Fig. 4 a microscopic photograph of the cross-section of the foamed hollow profile.

Fig. 1 depicts a cross-section through a spacer according to the invention for an insulating  
 5 glazing unit. The spacer comprises a polymeric main body I, made, for example, of polypropylene (PP) or of styrene acrylonitrile (SAN). The polymer has a glass fiber content of 0 wt.-% to 40 wt.-%.

The main body I comprises two parallel side walls 1, 2 that are intended to be brought into  
 10 contact with the panes of the insulating glazing. In each case, between one end of each side wall 1, 2, runs an inner wall 3 that is intended to face the interpane space of the insulating glazing. At the other ends of the side walls 1, 2, a connection section 7, 7' is connected in each case. Via the connecting sections 7, 7', the side walls 1, 2 are connected to an outer wall 4 that is implemented parallel to the inner wall 3. The angle  $\alpha$  between the connecting  
 15 sections 7 (or 7') and the side wall 3 (or 4) is roughly 45°. The result of this is that the angle between the outer wall 4 and the connecting sections 7, 7' is also roughly 45°. The main body I surrounds a hollow chamber 5.

The material thickness (thickness) of the side walls 1, 2, of the inner wall 3, of the outer wall  
 20 4, and of the connecting section 7, 7' is roughly the same and is, for example, 1 mm. The main body has, for example, a height of 6.5 mm and a width of 15 mm.

A reinforcing strip 6 is preferably embedded in each side wall 1, 2. The reinforcing strips 6, 6'  
 are made of steel, which is not stainless steel, and they have a thickness (material  
 25 thickness) of, for example, 0.3 mm and a width of, for example, 3 mm. The length of the reinforcing strips 6, 6' corresponds to the length of the main body I.

The reinforcing strips give the basic body I sufficient bendability and stability to be bent  
 without prior heating and to durably retain the desired shape. In contrast to other solutions  
 30 according to the prior art, the spacer here has very low thermal conductivity since the metallic reinforcing strips 6, 6' are embedded only in the side walls 1, 2, via which only a very small part of the heat exchange between the pane interior and the external environment occurs. The reinforcing strips 6, 6' do not act as thermal bridges. These are major advantages of the present invention.

An insulation film 8 is preferably arranged on the outer surface of the outer wall 4 and of the connection sections 7, 7' as well as a section of the outer surface of each of the side walls 1, 2. The insulation film 8 reduces diffusion through the spacer. Thus, the entry of moisture into the interpane space of an insulating glazing unit or the loss of the inert gas filling of the interpane space can be reduced. Moreover, the insulation film 8 improves the thermal properties of the spacer, thus reduces thermal conductivity.

The insulation film 8 comprises the following layer sequence: a polymeric carrier film (made of LLDPE (linear low density polyethylene), thickness: 24  $\mu\text{m}$ ) /a metallic layer (made of aluminum, thickness: 50 nm) /a polymeric layer (PET, 12  $\mu\text{m}$ ) /a metallic layer (Al, 50 nm) /a polymeric layer (PET, 12  $\mu\text{m}$ ). The layer stack on the carrier film thus includes two polymeric layers and two metallic layers, with the polymeric layers and the metallic layers arranged alternately. The layer stack can also include other metallic layers and/or polymeric layers, with metallic and polymeric layers likewise preferably arranged alternately such that a polymeric layer is arranged between two adjacent metallic layers in each case and a polymeric layer is arranged above the uppermost metallic layer.

By means of the assembly comprising a polymeric main body I, the reinforcing strips 6,6', and the insulation film 8, the spacer according to the invention has advantageous properties with regard to stiffness, leakproofness, and thermal conductivity. Consequently, it is especially suitable for use in insulating glazings, in particular in the window or façade region of buildings.

Fig. 2 depicts a cross-section through an insulating glazing according to the invention in the region of the spacer. The insulating glazing is made of two glass panes 10, 11 of soda lime glass with a thickness of, for example, 3 mm, which are connected to each other via a spacer according to the invention arranged in the edge region. The spacer is the spacer of Fig. 1 with the reinforcing strips 6,6' and the insulation film 8.

The side walls 1, 2 of the spacer are bonded to the glass panes 10, 11 via, in each case, a sealing layer 13. The sealing layer 13 is made, for example, of butyl. In the edge space of the insulating glazing between the glass panes 10, 11 and the spacer, an outer sealing compound 9 is arranged peripherally. The sealing compound 9 is, for example, a silicone rubber.

The hollow chamber 5 of the main body I is preferably filled with a desiccant 12. The desiccant 12 is, for example, a molecular sieve. The desiccant 12 absorbs residual moisture present between the glass panes and the spacer and thus prevents fogging of the panes 10, 11 in the interpane space. The action of the desiccant 12 is promoted by holes (not shown) in the inner wall 3 of the main body I.

Fig. 3 depicts a flowchart of an exemplary embodiment of the method according to the invention for producing a spacer for an insulating glasings.

Fig. 4 shows a microscopic photograph of the foamed hollow profile. The polymer styrene acrylonitrile (SAN) is seen. The dark-colored hollow spaces are clearly visible. The walls between the individual cells, the hollow spaces, are completely closed. The hollow spaces are obtained by chemical foaming. A blowing agent is added to the plastic granulate, usually in the form of a so-called masterbatch granulate. By addition of heat, a volatile component of the blowing agent separates out, resulting in the foaming of the molten material.

### Comparative Example

#### Method for producing a foamed spacer

A mixture of:

98.5 wt.-% styrene acrylonitrile (SAN) with 35 wt.-% glass fibers (A. Schulmann) and  
1.5 wt.-% color masterbatch Sicoversal® Black (BASF)

was added as granulate into an extruder and melted in the extruder at a temperature of 218 °C. Using a melt pump, the molten material was shaped by a mold into a hollow profile (spacer). The still soft hollow profile with a temperature of roughly 170 °C was stabilized in a vacuum calibrator. This ensured the geometry of the hollow profile. Thereafter, the hollow profile was guided through a cooling bath and finally reached room temperature.

The hollow profile had a wall thickness of  $1.0 \text{ mm} \pm 0.1 \text{ mm}$ .

The total width of the hollow profile was  $15.5 \text{ mm} \pm 0.1 \text{ mm}$ .

The total height of the hollow profile was  $6.5 \text{ mm} - 0.05 \text{ mm} + 0.25$ .

The weight of the hollow profile was 52 g/m.

The mechanical strength of the hollow profile was  $>600$  N/cm.

#### Example

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Method for producing a foamed spacer

A mixture of:

- 97.7 wt.-% styrene acrylonitrile (SAN) with 35 wt.-% glass fibers (A. Schulmann)  
10 1.5 wt.-% color masterbatch Sicoversal® Black (BASF), and  
0.8 wt.-% foaming agent Polybatch 8850 E (A. Schulmann)  
was added as granulate into an extruder and melted in the extruder at a temperature of  
218 °C. At this time, the decomposition of the foaming agent with release of CO<sub>2</sub> occurred.  
Using a melt pump, the molten material was shaped by a mold into a hollow profile (spacer).  
15 The still soft hollow profile with a temperature of roughly 170 °C was stabilized in a vacuum  
calibrator. This ensured the geometry of the hollow profile. Thereafter, the hollow profile was  
guided through a cooling bath and finally reached room temperature.

20

The hollow profile had a wall thickness of  $1.0 \text{ mm} \pm 0.1 \text{ mm}$ .

The total width of the hollow profile was  $15.5 \text{ mm} \pm 0.1 \text{ mm}$ .

The total height of the hollow profile was  $6.5 \text{ mm} - 0.05 \text{ mm} + 0.25$ .

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The weight of the hollow profile was 45 g/m.

The mechanical strength of the hollow profile is  $> 600$  N/cm.

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A comparison between the non-foamed hollow profile of Comparative Example 1 and the  
foamed hollow profile according to the invention of Example 1 is found in Table 1.

35

Table 1

|                                      | Comparative Example 1   | Example 1               |
|--------------------------------------|-------------------------|-------------------------|
| Wall thickness of the hollow profile | 1.0 mm $\pm$ 0.1 mm     | 1.0 mm $\pm$ 0.1 mm     |
| Width of the hollow profile          | 15.5 mm $\pm$ 0.1 m     | 15.5 mm $\pm$ 0.1 mm    |
| Height of the hollow profile         | 6.5 mm - 0.05 mm + 0.25 | 6.5 mm - 0.05 mm + 0.25 |
| Mechanical strength                  | > 600 N/cm              | > 600 N/cm              |
| Weight of the hollow profile         | 52 g/m                  | 45 g/m                  |

With the hollow profile according to the invention, a material savings of 7 grams per meter was achieved with the same mechanical strength. This means a material savings of 13.46% based on 52 grams per meter.

A further comparison between the non-foamed hollow profile of Comparative Example 1 and the foamed hollow profile according to the invention of Example 1 is found in Table 2. For this, 12 specimens each of non-foamed and foamed hollow profiles were measured. Force/strain measurements were performed. For this, the maximum force  $F_{\max}$  (N) was applied to the specimen until the specimen breaks. Difference length, DL (mm) at  $F_{\max}$  (N) is the path that two test jaws must travel at maximum force before the hollow body breaks. In the table, X represents the mean; S, the scattering; and V, the standard deviation.

Table 2

| Series | Un-Foamed Hollow Profile |                              | Foamed Hollow Profile |                              |
|--------|--------------------------|------------------------------|-----------------------|------------------------------|
| N = 12 | $F_{\max}$ (N)           | DL (mm)<br>at $F_{\max}$ (N) | $F_{\max}$ (N)        | DL (mm)<br>at $F_{\max}$ (N) |
| X      | 1150                     | 0.4                          | 2290                  | 0.7                          |
| S      | 141                      | 0.1                          | 730                   | 0.2                          |

From the comparison of the measured  $F_{\max}$  (N) value of the un-foamed hollow profile of 1150 N with that of the foamed hollow profile at 2290 N, it is clear that the foamed hollow profile according to the invention has substantially higher stress and fracture resistance.

The comparison between the measured DL at  $F_{\max}$  (N) value of the un-foamed hollow profile at 0.4 mm with that of the foamed hollow profile at 0.7 mm shows that the foamed hollow profile has substantially higher elasticity.

The advantages of the foamed hollow profile according to the invention were unexpected and very surprising.

- 5 For the thermal properties of the hollow profile, an improvement of up to 45% was measured. The thermal properties are greatly improved by the gas entrapped in the hollow spaces. The in active gas entrapped in the hollow spaces acts as a very good insulator.

**List of Reference Characters:**

|    |          |                                                         |
|----|----------|---------------------------------------------------------|
|    | (I)      | polymeric main body                                     |
| 5  | (1)      | side wall                                               |
|    | (2)      | side wall                                               |
|    | (3)      | inner wall                                              |
|    | (4)      | outer wall                                              |
|    | (5)      | hollow chamber                                          |
| 10 | (6,6')   | reinforcing strip                                       |
|    | (7,7')   | connecting section                                      |
|    | (8)      | insulation film                                         |
|    | (9)      | outer sealing compound                                  |
|    | (10)     | glass pane                                              |
| 15 | (11)     | glass pane                                              |
|    | (12)     | desiccant                                               |
|    | (13)     | sealing layer                                           |
| 20 | $\alpha$ | angle between side wall 1,2 and connecting section 7,7' |

### Claims

1. Spacer for an insulating glazing unit, at least comprising:  
a polymeric main body, at least comprising two parallel side walls that are connected to one another by an inner wall and an outer wall, wherein the side walls, the inner wall, and the outer wall surround a hollow chamber,  
wherein the main body
  - has a glass fiber content of 0 wt.-% to 40 wt.-% and
  - has, due to hollow spaces, a weight reduction of 10 wt.-% to 20 wt.-% and wherein
  - the hollow spaces are obtained by addition of at least one foaming agent and
  - the amount of the foaming agent added is 0.5 wt.-% to 1.5 wt.-%.
2. Spacer according to claim 1, wherein the weight reduction is from 11 wt.-% to 14 wt.-%.
3. Spacer according to claim 1 or 2, wherein the amount of the foaming agent added is 0.7 wt.-% to 1.0 wt.-%.
4. Spacer according to any one of claims 1 through 3, wherein the main body contains 1.0 wt.-% to 4.0 wt.-% color masterbatch.
5. Spacer according to claim 4, wherein the main body contains 1.3 wt.-% to 2.0 wt.-% color masterbatch.
6. Spacer according to any one of claims 1 through 5, wherein the main body is fracture-resistant up to an applied force of 1800 N to 2500 N.
7. Spacer according to any one of claims 1 through 6, wherein the main body contains at least polyethylene (PE), polycarbonates (PC), polystyrene, polybutadiene, polynitriles, polyesters, polyurethanes, polymethylmethacrylates, polyacrylates, polyamides, polyethylene terephthalate (PET), polybutylene terephthalate (PBT) or copolymers or derivatives or mixtures thereof.
8. Spacer according to claim 7, wherein the main body contains polypropylene (PP), acrylonitrile butadiene styrene (ABS), acrylonitrile styrene acrylate (ASA), acrylonitrile

butadiene styrene/polycarbonate (ABS/PC), styrene acrylonitrile (SAN), polyethylene terephthalate/polycarbonate (PET/PC), polybutylene terephthalate/polycarbonate (PBT/PC).

9. Spacer according to any one of claims 1 through 8, wherein the main body contains at least styrene acrylonitrile (SAN) or polypropylene (PP), or copolymers or derivatives or mixtures thereof.

10. Spacer according to any one of claims 1 through 9, wherein embedded in each side wall is a reinforcing strip that contains at least a metal or a metallic alloy and has a thickness of 0.05 mm to 1 mm, and a width of 1 mm to 5 mm.

11. Spacer according to claim 10, wherein embedded in each side wall is a reinforcing strip that contains steel.

12. Spacer according to any one of claims 1 through 11, wherein the spacer has, at least on the outer wall, an insulation film, which contains a polymeric carrier film and at least one metallic or ceramic layer, the thickness of the polymeric carrier film of the insulation film is from 10  $\mu\text{m}$  to 100  $\mu\text{m}$  and the thickness of the metallic or ceramic layer of the insulation film is from 10 nm to 1500 nm and wherein the insulation film contains at least one more polymeric layer with a thickness of 5  $\mu\text{m}$  to 100  $\mu\text{m}$  and the metallic or ceramic layer of the insulation film contains at least iron, aluminum, silver, copper, gold, chromium, silicon oxide, silicon nitride, or alloys or mixtures or oxides thereof and wherein the polymeric carrier film of the insulation film contains at least polyethylene terephthalate, ethylene vinyl alcohol, polyvinylidene chloride, polyamides, polyethylene, polypropylene, silicones, acrylonitriles, polymethyl acrylates, or copolymers or mixtures.

13. Method for producing a spacer for an insulating glazing unit according to any one of claims 1 through 12, comprising

- a) preparing a mixture of at least one polymer, color masterbatch, and foaming agent,
- b) melting the mixture in an extruder at a temperature of 170 °C to 230 °C,
- c) decomposing the foaming agent foaming the molten material by a gas,
- d) pressing the molten material by a mold, thereby obtaining a main body,
- e) stabilizing the main body, and
- f) cooling the main body.

14. Method according to claim 13, wherein a granulate mixture at least containing 95.0 wt.-% to 99.0 wt.-% polymer with 30.0 wt.-% to 40.0 wt.-% glass fibers, 1.0 wt.-% to 4.0 wt.-% color masterbatch, and 0.5 wt.-% to 1.5 wt.-% foaming agent is provided.
15. Method according to claim 13 or 14, wherein the mixture is melted in an extruder at a temperature of 215 °C to 220 °C.
16. Method according to any one of claims 13 through 15, wherein the molten material is foamed with CO<sub>2</sub>.
17. Use of a spacer according to any one of claims 1 through 12 in multiple glazing units.
18. Use of a spacer according to any one of claims 1 through 12 in insulating glazing units.
19. Use of a spacer according to any one of claims 1 through 12 in window glazing or façade glazing of buildings.

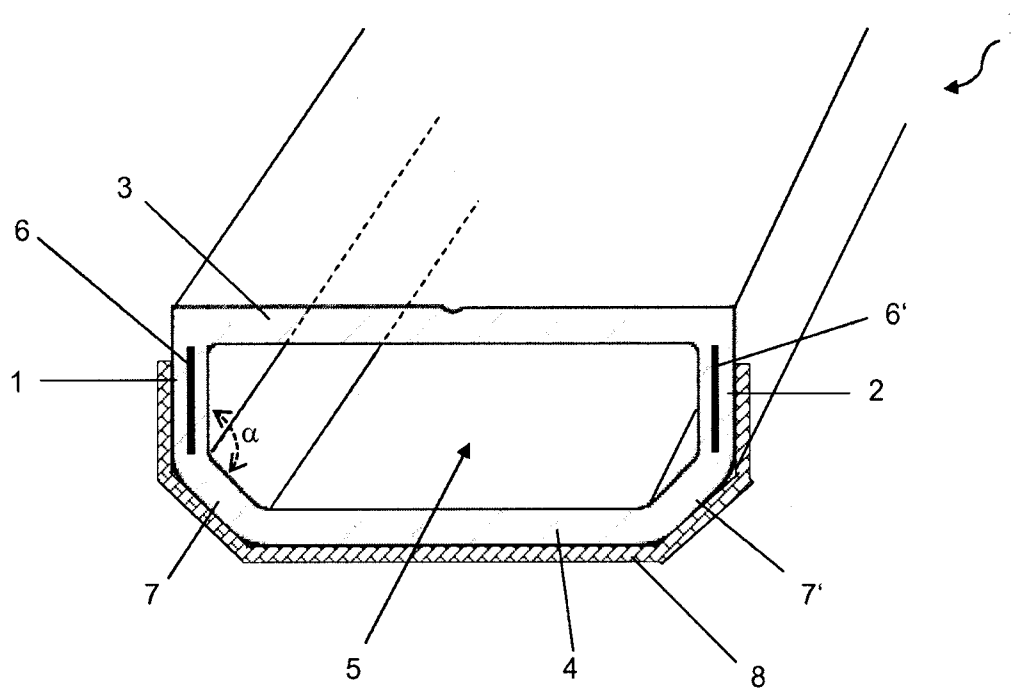


Fig. 1

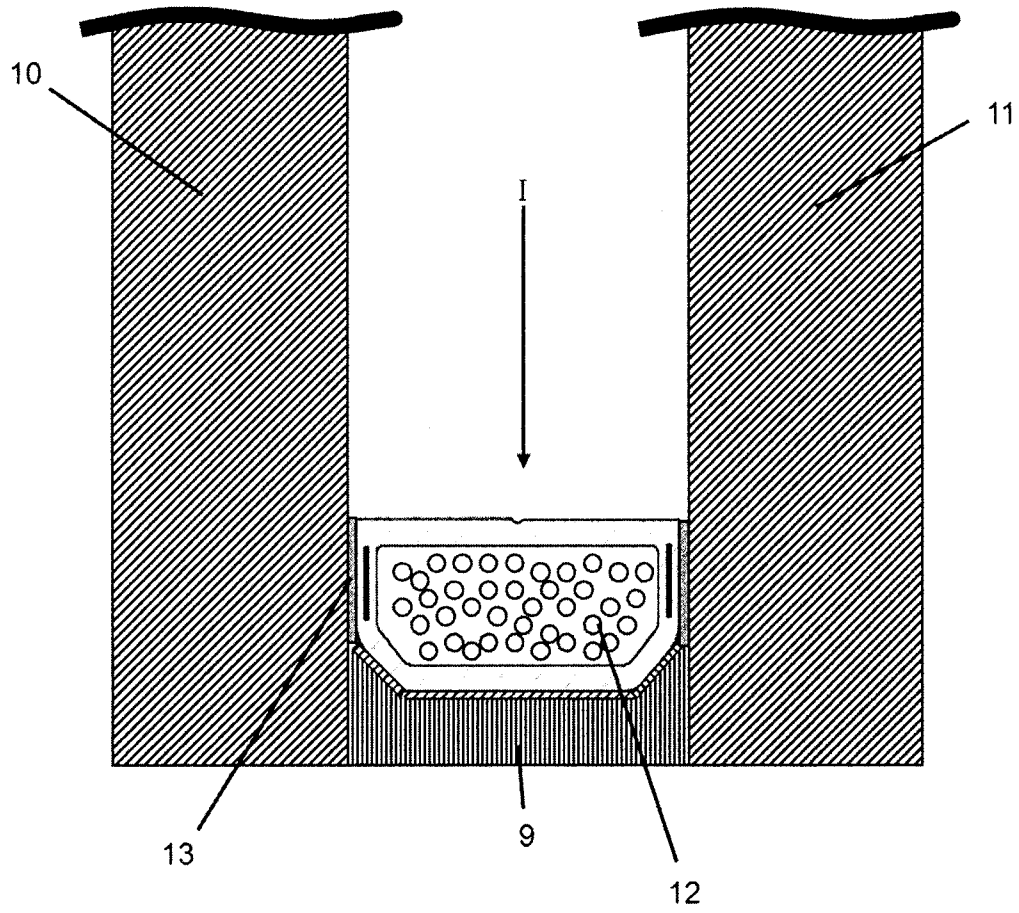


Fig. 2

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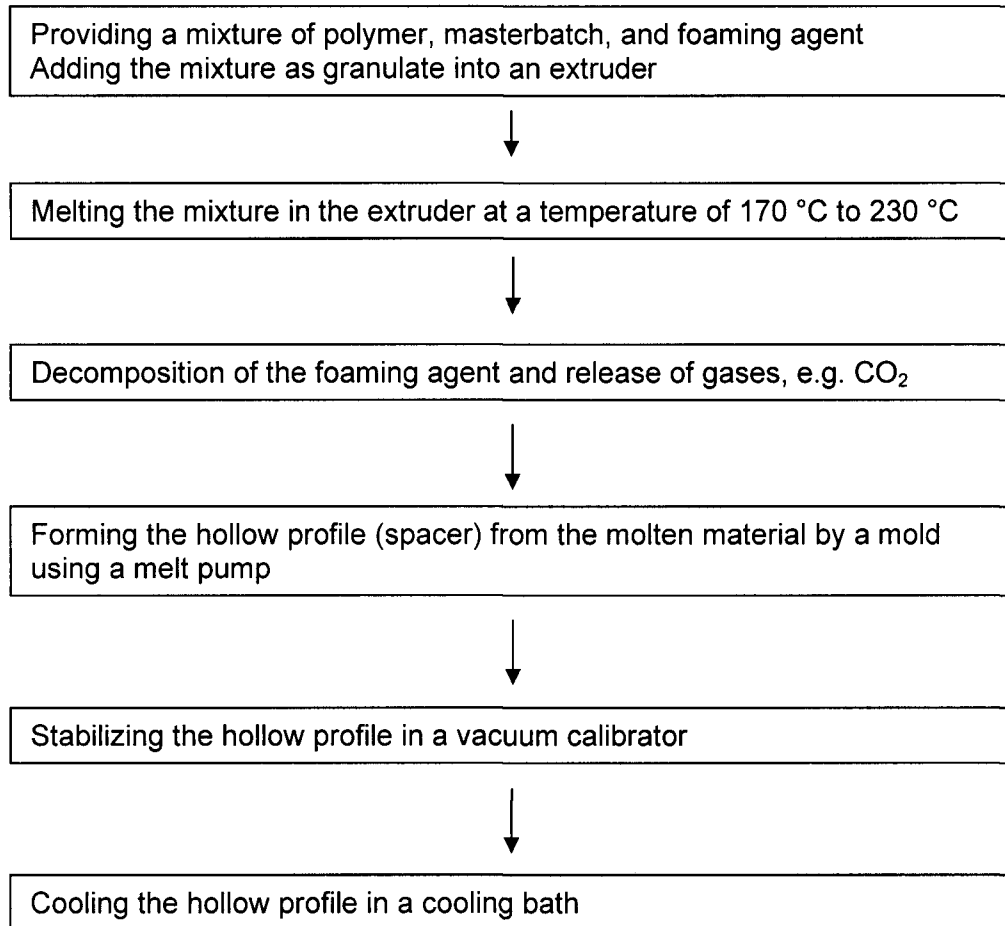
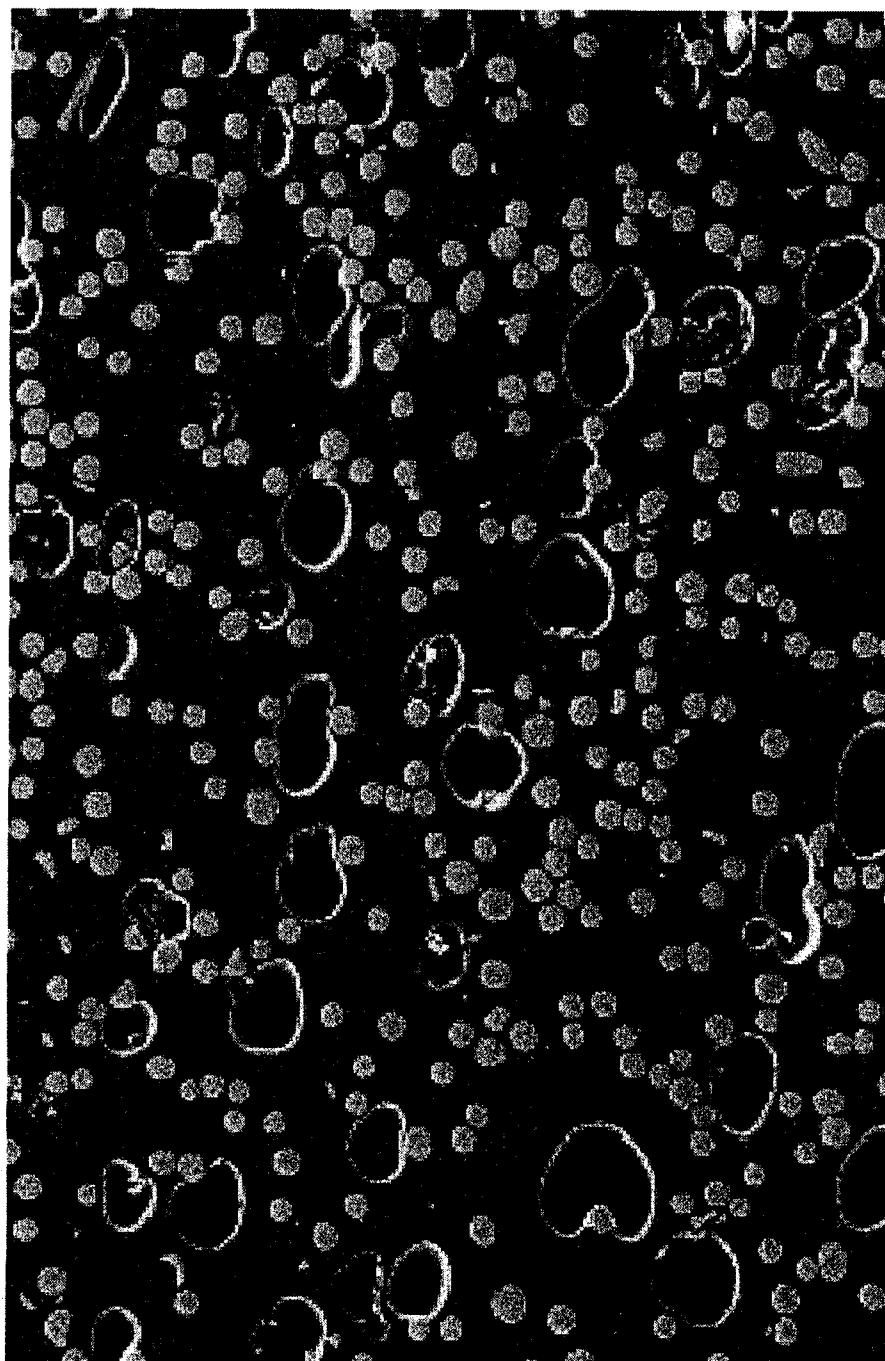


Fig. 3



100  $\mu\text{m}$

Fig. 4

