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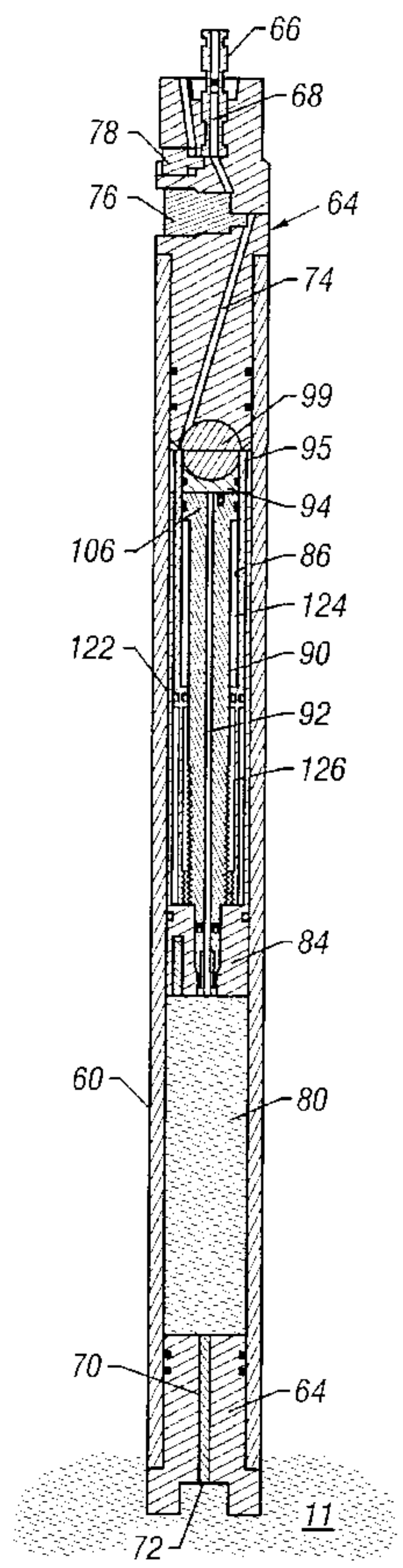
(54) Titre : APPAREIL ET PROCEDE PERMETTANT DE CONTROLER LA PRESSION D'UN ECHANTILLON DE FLUIDE DE PUITS
(54) Title: APPARATUS AND METHOD FOR CONTROLLING WELL FLUID SAMPLE PRESSURE



(57) Abrégé/Abstract:
An apparatus and method for maintaining the pressure of a well fluid sample as the sample is transported to the well surface from a downhole wellbore location. The invention collects a formation fluid sample under pressure. The fluid sample is further

(57) **Abrégé(suite)/Abstract(continued):**
pressurized with a traveling piston powered by the hydrostatic wellbore pressure. The pressurized formation fluid sample is contained under high pressure within a fixed volume chamber for retrieval to the well surface. Multiple collection tanks can be lowered into the wellbore during the same run to sample different zones with minimal rig time. The tanks can be emptied at the well surface with an evacuation pressure so that the fluid sample pressure is maintained above a selected pressure at all times.

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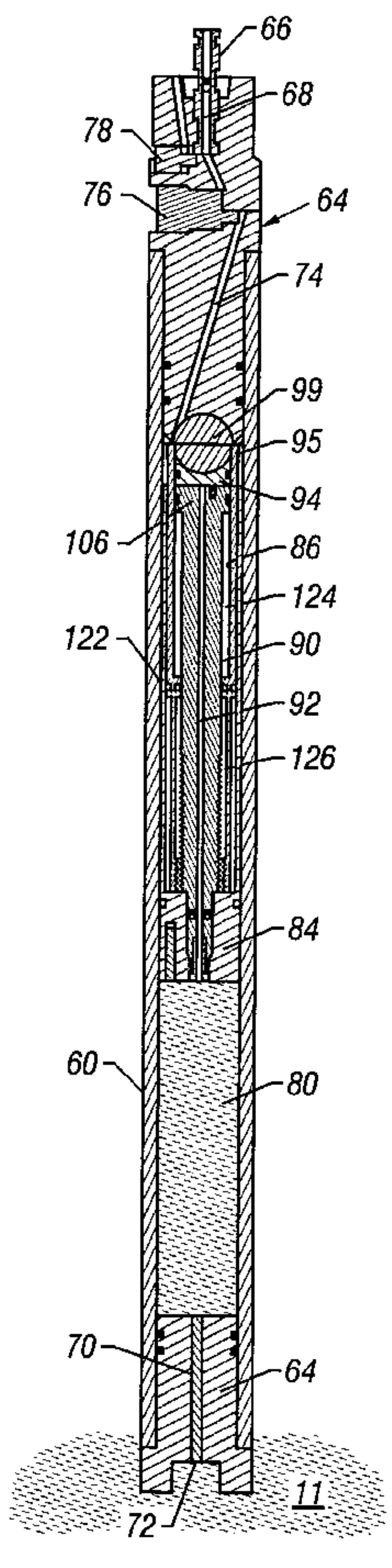

(57) Abstract: An apparatus and method for maintaining the pressure of a well fluid sample as the sample is transported to the well surface from a downhole wellbore location. The invention collects a formation fluid sample under pressure. The fluid sample is further pressurized with a traveling piston powered by the hydrostatic wellbore pressure. The pressurized formation fluid sample is contained under high pressure within a fixed volume chamber for retrieval to the well surface. Multiple collection tanks can be lowered into the wellbore during the same run to sample different zones with minimal rig time. The tanks can be emptied at the well surface with an evacuation pressure so that the fluid sample pressure is maintained above a selected pressure at all times.

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Title: APPARATUS AND METHOD FOR CONTROLLING WELL FLUID SAMPLE PRESSURE

BACKGROUND OF THE INVENTION

FIELD OF THE INVENTION

The present invention relates to the art of earth boring and the collection of formation fluid samples from a wellbore. More particularly, the invention relates to methods and apparatus for collecting a deep well formation sample and preserving the in situ constituency of the sample upon surface retrieval.

DESCRIPTION OF RELATED ART

Earth formation fluids in a hydrocarbon producing well typically comprise a mixture of oil, gas, and water. The pressure, temperature and volume of formation fluids control the phase relation of these constituents. In a subsurface formation, high well fluid pressures often entrain gas within the oil above the bubble point pressure. When the pressure is reduced, the entrained or dissolved gaseous compounds separate from the liquid phase sample. The accurate measure of pressure, temperature, and formation fluid composition from a particular well affects the commercial interest in producing fluids available from the well. The data also provides information regarding procedures for maximizing the completion and production of the respective hydrocarbon reservoir.

Certain techniques analyze the well fluids downhole in the wellbore. United States Patent No. 5,361,839 to Griffith et al. (1993) disclosed a transducer for generating an output representative of fluid sample characteristics downhole in a wellbore. United States Patent No. 5,329,811 to Schultz et al. (I 994) disclosed an apparatus and method for assessing pressure and volume data for a downhole well fluid sample.

Other techniques capture a well fluid sample for retrieval to the surface. United States Patent No. 4,5 83,595 to Czenichow et al. (1986) disclosed a piston actuated mechanism for capturing a well fluid sample. United States

Patent No. 4,721,157 to Berzin (1988) disclosed a shifting valve sleeve for capturing a well fluid sample in a chamber. United States Patent No. 4,766,955 to Petermann (1988) disclosed a piston engaged with a control valve for capturing a well fluid sample, and United States Patent No. 4,903,765 to Zunkel (1990) disclosed a time delayed well fluid sampler. United States Patent No. 5,009,100 to Gruber et al. (1991) disclosed a wireline sampler for collecting a well fluid sample from a selected wellbore depth, United States Patent No. 5,240,072 to Schultz et al. (1993) disclosed a multiple sample annulus pressure responsive sampler for permitting well fluid sample collection at different time and depth intervals, and United States Patent No. 5,322,120 to Be et al. (1994) disclosed an electrically actuated hydraulic system for collecting well fluid samples deep in a wellbore.

Temperature downhole in a deep wellbore often exceed 300 degrees F. When a hot formation fluid sample is retrieved to the surface at 70 degrees F, the resulting drop in temperature causes the formation fluid sample to contract. If the volume of the sample is unchanged, such contraction substantially reduces the sample pressure. A pressure drop changes in the situ formation fluid parameters, and can permit phase separation between liquids and gases entrained within the formation fluid sample. Phase separation significantly changes the formation fluid characteristics, and reduces the ability to evaluate the actual properties of the formation fluid.

To overcome this limitation, various techniques have been developed to maintain pressure of the formation fluid sample. United States Patent No. 5,337,822 to Massie et al. (1994) pressurized a formation fluid sample with a hydraulically driven piston powered by a high pressure gas. Similarly, United States Patent No. 5,662,166 to Shammai (1997) used a pressurized gas to charge the formation fluid sample. United States Patent Nos. 5,303,775 (1994) and 5,377,755 (1995) to Michaels et al. disclosed a bi-directional, positive displacement pump for increasing the formation fluid sample pressure above the bubble point so that subsequent cooling did not reduce the fluid pressure below the bubble point.

Existing techniques for maintaining the sample formation pressure are limited by many factors. Pretension or compression springs are not suitable because the required compression forces require extremely large springs. Shear mechanisms are inflexible and do not easily permit multiple sample gathering at different locations within the wellbore. Gas charges can lead to explosive decompression of seals and sample contamination. Gas pressurization systems require complicated systems including tanks, valves and regulators which are expensive, occupy space in the narrow confines of a wellbore, and require maintenance and repair. Electrical or hydraulic pumps require surface control and have similar limitations.

Accordingly, there is a need for an improved system capable of compensating for hydrostatic wellbore pressure loss so that a formation fluid sample can be retrieved to the well surface at substantially the original formation pressure. The system should be reliable and should be capable of collecting the samples from the different locations within a wellbore.

SUMMARY OF THE INVENTION

The present invention provides an apparatus and method for controlling the pressure of a pressurized wellbore fluid sample collected downhole in an earth boring. The apparatus comprises a housing having a hollow interior. A compound piston within the housing interior defines a fluid sample chamber wherein the piston is moveable within the housing interior to selectively change the fluid sample chamber volume. The compound piston comprises an outer sleeve and an inner sleeve moveable relative to the outer sleeve. However, movement of the inner sleeve relative to the outer sleeve is unidirectional. An external pump extracts formation fluid for delivery under pressure into the fluid sample chamber. A positioned opened valve permits pressurized wellbore fluid to move said piston for pressurizing the fluid sample within the fluid sample chamber so that the fluid sample remains pressurized when the fluid sample is moved to the well surface.

The method of the invention is practiced by lowering a housing into a wellbore. The compound piston is displaced within the sample chamber by formation fluid delivered by the external pump. When the sample chamber has filled, a valve is opened to introduce wellbore fluid at hydrostatic wellbore pressure against the piston to move the piston for pressurizing the well fluid sample within the fluid sample chamber. By means of piston area differential, force on a inner sleeve of the compound piston is unbalanced to compress the fluid sample by a volumetric reduction. The reduced volume is secured by mechanically securing the relative positions of the compound piston against the sample chamber.

BRIEF DESCRIPTION OF THE DRAWINGS

The advantages and further aspects of the invention will be readily appreciated by those of ordinary skill in the art as the same becomes better understood by reference to the following detailed description when considered in conjunction with the accompanying drawings in which:

FIG. 1 is a schematic earth section illustrating the invention operating environment;

FIG. 2 is a schematic of the invention in operative assembly with cooperatively supporting tools;

FIG. 3 is a schematic of a representative formation fluid extraction and delivery system;

FIG. 4 is an isometric view of a sampling tank magazine;

FIG. 5 is an isometric view of the present invention;

FIG. 6 is an axially sectioned isometric view of the invention;

FIG. 7 is a sectioned detail of the sample inlet end of the invention;

FIG. 8 is a sectioned detail of the sample chamber portion of the invention assembly;

FIG. 9 is a sectioned detail of the hydrostatic wellbore pressure end of the compound piston;

FIG. 10 is an axially sectioned isometric view of the invention in the course of receiving a sample of formation fluid;

FIG. 11 is a sectioned detail of the compound piston position for wellbore fluid entry;

FIG. 12 is a sectioned detail of relative axial displacement between the elements of the compound piston;

FIG. 13 is an axially sectioned view of the invention in the course of sample extraction; and,

FIG. 14 is an orthographic axial section of the invention.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

FIG. 1 schematically represents a cross-section of earth **10** along the length of a wellbore penetration **11**. Usually, the wellbore will be at least partially filled with a mixture of liquids including water, drilling fluid, and formation fluids that are indigenous to the earth formations penetrated by the wellbore. Hereinafter, such fluid mixtures are referred to as "wellbore fluids". The term "formation fluid" hereinafter refers to a specific formation fluid exclusive of any substantial mixture or contamination by fluids not naturally present in the specific formation.

Suspended within the wellbore **11** at the bottom end of a wireline **12** is a formation fluid sampling tool **20**. The wireline **12** is often carried over a pulley **13** supported by a derrick **14**. Wireline deployment and retrieval is performed by a powered winch carried by a service truck **15**, for example.

Pursuant to the present invention, a preferred embodiment of a sampling tool **20** is schematically illustrated by **FIG. 2**. Preferably, such sampling tools are a serial assembly of several tool segments that are joined end-to-end by the threaded sleeves of mutual compression unions **23**. An assembly of tool segments appropriate for the present invention may include a hydraulic power unit **21** and a formation fluid extractor **23**. Below the extractor **23**, a large displacement volume motor/pump unit **24** is provided for line purging. Below the large volume pump is a similar motor/pump unit **25** having a smaller displacement volume that is quantitatively monitored as described more expansively with respect to **FIG. 3**. Ordinarily, one or more tank magazine sections **26** are assembled below the small volume pump. Each magazine section **26** may have three or more fluid sample tanks **30**.

The formation fluid extractor **22** comprises an extensible suction probe **27** that is opposed by borewall feet **28**. Both, the suction probe **27** and the opposing feet **28** are hydraulically extensible to firmly engage the wellbore walls. Construction and operational details of the fluid extraction tool **22** are more expansively described by U.S. Patent No. 5,303,775, the specification of which is incorporated herewith.

Operation of the tool is fundamentally powered by electricity delivered from the service truck **15** along the wireline **12** to the hydraulic power supply unit **21**. With respect to **FIG. 3**, the constituency of the hydraulic power supply unit **21** comprises an A.C. motor **32** coupled to drive a positive displacement, hydraulic power pump **34**. The hydraulic power pump energizes a closed loop hydraulic circuit **36**. The hydraulic circuit is controlled, by a solenoid actuated 4-way valve **47**, for example, to drive the motor section **42** of an integrated, positive displacement, pump/motor unit **25**. The pump portion **44** of the pump/motor unit **25** is monitored by means such as a rod position sensor **46**, for example, to report the pump displacement volume. Formation fluid drawn through the suction probe **27**, is directed by a solenoid controlled valve **48** to alternate chambers of the pump **44** and to a tank distributor **49**. By this route, sample volumes of selected formation fluid is extracted directly from respective in situ formations and delivered to designated sample chambers among the several sample tank tools **30**.

As sub-steps in the formation fluid extraction procedure of the present invention, the large volume motor/pump unit **27** is employed to purge the formation fluid flow lines between the suction probe **27** and the small volume pump **25**. Since these sub-steps do not require accurate volumetric data, measurement of the pump displacement volume is not required. Otherwise, the motor/pump unit **24** may be substantially the same as motor/pump unit **25** except for the preference that the pump of unit **24** have a greater displacement volume capacity.

A representative magazine section **26** is illustrated by **FIG. 4** to include a fluted cylinder **50**. Preferably, the cylinder **50** is fabricated to accommodate three or four tanks **30**. Each tank **30** is operatively loaded into a respective alcove **52** with a bayonet-stab fit. Two or more cylinders **50** are joined by an internally threaded sleeve **23** that is axially secured to one end of one cylinder but freely rotatable about the cylinder axis. The sleeve **23** is turned upon the external threads of a mating joint boss **52** to draw the boss into a compression sealed juncture therebetween whereby the fluid flow conduits **54** drilled into the end of each boss **52** are continuously sealed across the joint .

FIGs. 5, **6** and **7** illustrate each tank **30** as comprising a cylindrical pressure housing **60** that is delineated at opposite ends by cylinder headwalls. The bottom-end headwall comprises a valve sub-assembly **62** having a socket boss **63** and a fluid conduit nipple **66** projecting axially therefrom. A conduit **68** within the nipple **66** is selectively connected by a respective conduit **54** to the tank distributor **49** and, ultimately, to the suction probe **22** of the formation fluid extractor **27**. Fluid flow within the conduit **68** is rectified by a check valve **69**. Within the valve sub-assembly **62** is a formation fluid flow path **74** between the conduit **68** and a formation fluid reservoir internally of the pressure housing **60**. A solenoid actuated shut-off valve **76** is disposed to selectively open and close the channel of flow path **74**. As best seen from the isometric detail of **FIG. 7**, a bleed valve **78** selectively closes a shunt conduit **79** that junctions with the flow path **74**.

Referring again to the axial half-section of **FIG. 6**, the pressure housing top-end headwall comprises a sub **64** having a fluid inlet conduit **70** that connects the interior bore **80** of the pressure housing **60** with a threaded tubing nipple socket **72**. The conduit **70** is a normally open fluid flow path between the interior bore **80** and the in situ wellbore environment. Within the interior bore **80** of the pressure housing **60** is a traveling trap sub-assembly **82** that comprises the coaxial assembly of an inner traveling/locking sleeve **86** within an outer traveling sleeve **84** as shown by **FIG.8**. Unitized with the outer traveling sleeve **84** by a retaining bolt **88** as shown by **FIG. 9**, is a locking piston rod **90**. A fluid channel **92** along the length of the rod 90 openly communicates the inner face **96** of a floating piston **94** with the open well bore conduit **70**. The floating piston **94** is axially confined within the inner bore of the inner traveling/locking sleeve

86 by a retaining ring **98**. A mixing ball **99** is placed within the sample (formation fluid) receiving chamber **95** that is geometrically defined as that variable volume within the interior bore **80** of pressure housing 60 between the valve sub-assembly **62** and the end area of the traveling trap sub-assembly **82**.

A body lock ring **100** having internal barb rings **102** and external barb rings **104** selectively connects the rod **90** to the inner traveling/locking sleeve **86**. The selective connection of the barbed lock ring **100** permits the sleeve 86 to move coaxially along the rod **90** from the piston **84** but prohibits any reversal of that movement.

Another construction detail of the inner traveling/locking sleeve **86** is the sealed partition **122** between the opposite ends of the sleeve **86**. The chamber **124** created between the partition **122** and the piston head **106** of the rod **90** is sealed to the atmospheric pressure present in the chamber at the time of assembly.

The body lock ring **100** between the locking piston rod **90** and the inner bore wall of the inner traveling/locking sleeve **86** above the partition **122** does not provide a fluid pressure barrier. Consequently, the chamber **126** between the partition **122** and the body lock ring **100** functions at the same fluid pressure as the wellbore fluid flood chamber **120** when the flood valve **110** is opened..

Still with respect to **FIG.9**, the base of the floating piston/sleeve **84** includes a flood valve **110** having a pintle **112** biased by a spring **114** against a seal seat **116**. The pintle includes a stem **118** that projects beyond the end plane of the floating piston /sleeve **84**. When the end plane of the floating piston/sleeve **84** is pressed against the inner face of the top sub **64** (**FIG. 11**), the pintle **112** is displaced from engagement with the seal seat **116** to admit wellbore fluid into the flood chamber **120** as is illustrated by **FIGs. 11** and **12**. *The flood chamber* ***120*** *is geometrically defined as the variable volume bounded* by the annular space between the outer perimeter of the rod **90** and the inner bore **85** of the outer traveling sleeve **84**.

OPERATION

Preparation of the sample tanks **30** prior to downhole deployment includes the closure of bleed valve **78** and the opening of shut-off valve **76**. Under the power and control of instrumentation carried by the service truck **15**, the sampling tool is located downhole at the desired sample acquisition location. When located, the hydraulic power unit **21** is engaged by remote control from the service truck **15**. Hydraulic power from the unit **21** is directed to the formation fluid extractor unit **22** for borewall engagement of the formation fluid suction probe **27** and the borewall feet **28**. The suction probe **27** provides an isolated, direct fluid flow channel for substantially pure formation fluid. Such formation fluid flow into the suction probe **27** is first induced by the suction of large volume pump **24** which is driven by the hydraulic power unit **21**. The large volume pump **24** is operated for a predetermined period of time to flush the sample distribution conduits of contaminated wellbore fluids with formation fluid drawn through suction probe **27**. When the predetermined line flushing interval has concluded, hydraulic power is switched from the large volume pump **24** to the small volume piston pump **25**. Referring to **FIG. 3**, formation fluid drawn from the suction probe **27** by the pump **25** is shuttled by 4-way valve **48** into successively opposite chambers **44**. Simultaneously, the valve **48** directs discharge from the chambers to a multiple port rotary valve **49**, for example, which further directs the formation fluid on to the desired sample tank 30.

Formation fluid enters the tank **30** through the nipple conduit **68** and is routed past the check valve **69** and along the flow path **74** into the sample receiving chamber **95**. The tank shut-off valve **76** was opened before the tank was lowered into the wellbore. Pressure of the pumped formation fluid in the receiving chamber **95** displaces both, the outer traveling sleeve **84** and the inner traveling/locking sleeve **86**, against the standing wellbore pressure in the interior bore **80** of pressure housing **60** as shown by **FIG. 10.** When the pressure of the formation fluid sample within the formation fluid sample chamber **95** reaches the boost pressure limit of pump **25**, high pressure check valve closes to trap the sample of formation fluid within the sample chamber **30** and passage **32**.

Also, when the sample receiving chamber **95** is full, the base plane of the outer traveling sleeve **84** will engage the inside face of the top sub **64**. Thereby, the stem **118** is axially displaced to open the flood valve **110**. Internal conduits within the outer traveling sleeve **84** direct wellbore fluid into the flood chamber **120**. The wellbore pressure in the flood chamber **120** bears against the inner traveling/locking sleeve **84** over the cross-sectional area of the flood chamber **120** annulus.

Opposing the flood chamber force on the traveling/locking sleeve **86** are two pressure sources. One source is the formation fluid pressure in the sample chamber **95** bearing on the annular end section of the traveling/locking sleeve **86** as was provided by the small volume pump unit **25**. The other pressure opposing the flood chamber pressure is the closed atmosphere chamber **124** acting on the area of the annular partition **122**. Initially, the force balance on the traveling/locking sleeve **86** favors the flood chamber side to press the annular end of the sleeve **86** into the sample chamber **95**. Since the liquid formation fluid is substantially incompressible, intrusion of the solid structure of the sleeve **86** annulus into the sample chamber volume exponentially increases the pressure in the sample chamber until a final force equilibrium is achieved. Nevertheless, at the pressures of this environment, measurable liquid compression may be achieved.

This axial movement of the inner traveling/locking sleeve **86** relative to the outer sleeve **84** also translates to the piston rod 90 which is secured to the outer sleeve **84** via the retaining bolt **88**. Consequently, the sleeve **86** partition **122** is displaced toward the piston head **106** to compress the gaseous atmosphere of chamber 124 thereby adding to the equilibrium forces.

Due to the internal and external barb rings 102 and 104 respective to the body lock ring 100, movement of the piston 90 relative to the inner traveling sleeve **86** is rectified to maintain this volumetric invasion of the structure **86** into the sample chamber volume.

By compressing the volume of the formation fluid sample, the fluid sample pressure is greatly above the wellbore pressure. Although this greatly increased in situ pressure declines when the confined formation sample is removed from the wellbore, the operative components may be designed so that when the collected formation sample is removed from the well, the sample pressure does not decline below the bubble point of entrained or dissolved gas. Movement of the inner traveling/locking sleeve **86** further compresses the collected formation fluid sample above the boost capability of the pump **25**. Such compression continues until the desired boost ratio is accomplished.

For example, a down hole fluid sample can have a hydrostatic wellbore pressure of 10,000 psi. The typical compressibility for such a fluid is $5X10^{-6}$ so that a volume decrease of only eight percent would raise the fluid sample pressure by 16,000 psi to 26,000 psi, for a boost ratio os 2.6 to 1.0. When the magazine section **26** and the collected formation fluid sample is raised to the surface of wellbore **11**, the formation fluid sample temperature will cool, thereby returning the formation fluid sample pressure toward the original pressure of 10,000 psi. If the downhole fluid temperature is 270°F and the wellbore **11** surface temperature is 70°F, the resulting 200° drop in temperature will lower the fluid sample pressure by approximately 15,300 psi in a fixed volume, thereby resulting in a surface fluid sample pressure of approximately 10,700 psi.

To hold the volume of fluid sample chamber **95** constant as the magazine **26** is removed from the wellbore **11**, inner traveling/locking sleeve **86** is fixed relative to outer traveling sleeve **84** during retrieval of the magazine **26**. The invention accomplishes the fixed relationship by means of the body lock ring **100**. This mechanism permits additional boost to be added to the formation fluid sample pressure within the sample chamber **95** as a proportionality of the in situ wellbore pressure. For example, the magazine section **26** may subsequently be lowered to additional depths within a wellbore **11** where the hydrostatic pressure is greater than a prior sample extraction. The hydrostatic wellbore pressure increase is transmitted through flood valve **112** into flood chamber **120** to further move the inner traveling/locking sleeve **86** and to further compress the formation fluid sample within the sample chamber **95** to a greater pressure. Such pressure boost con be accomplished quickly and magazine **26** removed to the surface of wellbore **11** before a significant amount of heat from the additional wellbore depth is transferred to the previously collected formation fluid sample.

At the surface of wellbore **11**, tank shut-off valve **76** is closed to trap the formation fluid sample. Thereafter, bleed valve **78** may be opened to relieve the fluid pressure in the flow passage between tank shut-off valve **76** and the high pressure check valve **69**. This pressure release provides a positive indication of fluid pressure and facilitates removal of a tank **30** from a magazine **26**.

Fig. 13 illustrates one technique for removing the formation fluid sample under pressure from within fluid sample chamber **95**. Tank **30** is connected to a pressure source **130** engaged with aperture **132** through top sub **64**. Pressure from the pressure source **130** is introduced until the inverse of the boost ratio times the expected pressure within fluid sample chamber **95** is reached. For a fluid sample pressure of 10,000 psi, the extraction pressure required would be:

$$1/2.6 \ \text{X} \ 10{,}000 = 3{,}850 \text{ psi}$$

After the inverse boost ratio is reached, shut-off valve **76** is cracked open and the formation fluid sample is permitted to pass through passage **74** into an attached receiver line **140**. The reverse boost pressure can be increased to displace the collected formation fluid sample until the sleeve edge of the inner traveling/locking sleeve **86** bottoms out against the valve sub **62**. Continued extraction fluid from the pressure source **130** displaces the outer traveling sleeve **84** relative to the inner sleeve **86**. Hence, the piston head **106** engages the floating piston **94** to sweep most of the formation fluid sample from the chamber **95**. The only volume within the chamber **95** not removed by the extraction pressure is found in an annular space between the outer traveling sleeve **84** and the valve sub **62**. The components of tank **30** can be dissembled and reset for another use.

In summary, the invention permits multiple tanks **30** to be lowered in the same operation so that different zones within wellbore **11** can be sampled. Each tank can be selectively operated to collect different samples at different pressures and to compress each sample to different rates exceeding the bubble point for gas within the sample. Operating costs are significantly reduced because less rig time is required to sample multiple zones. The invention prevents the pressure within each fluid sample from being reduced below the bubble point therefore delivering each fluid sample to the wellbore surface in substantially the same pressure state as the downhole sampling state. The invention accomplishes this function without requiring expanding gases, large springs and complicated mechanical systems. The fluid sample is collected under pressure and additional pressure is added with a force exerted by the downhole hydrostatic pressure.

Although the invention has been described in terms of certain preferred embodiments, it will become apparent to those of ordinary skill in the art that modifications and improvements can be made to the inventive concepts herein without departing form the scope of the invention. The embodiments shown herein are merely illustrative of the inventive concepts and should not be interpreted as limiting the scope of the invention.

CLAIMS

1. An apparatus for controlling the pressure of a pressurized wellbore fluid sample collected downhole in a well, comprising:

a housing having a hollow interior;

a piston within said housing interior for defining a fluid sample chamber, wherein said piston is moveable within said housing interior to selectively change said fluid sample chamber volume;

a pump for introducing a fluid sample under pressure into said fluid sample chamber; and

a valve for permitting pressurized wellbore fluid to move said piston, wherein said piston movement pressurizes the fluid sample within said fluid sample chamber so that the fluid sample remains pressurized when the fluid sample is moved to the well surface.

2. An apparatus as recited in Claim 1, further comprising a check valve engaged between said pump and said fluid sample chamber for preventing said piston from forcing the fluid sample toward said pump.

3. An apparatus as recited in Claim 1, wherein said valve is attached to said piston.

4. An apparatus as recited in Claim 1, further comprising a tank shut-off valve engaged between said pump and said fluid sample chamber for selectively permitting said fluid sample chamber to be pressure isolated from said pump

5. An apparatus as recited in Claim 1, further comprising a lock for retaining said piston fixed relative to said housing to maintain the volume of said fluid sample chamber.

6. An apparatus as recited in Claim 1, wherein said piston includes an outer sleeve and an inner sleeve moveable relative to said outer sleeve, and wherein said valve is capable of permitting the pressurized wellbore fluid to contact said inner sleeve for moving said inner sleeve relative to said outer sleeve to pressurized the fluid sample.

7. An apparatus as recited in Claim 6, further comprising a lock for retaining said inner sleeve fixed relative to said outer sleeve to maintain the volume of said fluid sample chamber.

8. An apparatus as recited in Claim 6, further comprising a flood chamber between said inner sleeve and said outer sleeve for receiving the pressurized wellbore fluid so that the fluid exerts a differential pressure against said inner sleeve to move said inner sleeve relative to said outer sleeve.

9. An apparatus as recited in Claim 8, further comprising an atmospheric chamber between said inner sleeve and said outer sleeve which initially has a pressure lower than the hydrostatic pressure and which is reduced in volume as said inner sleeve moves relative to said outer sleeve.

10. An apparatus as recited in Claim 1, further comprising a second piston engaged with said housing to define a second fluid sample chamber and engaged with said pump and said valve for selectively pressurizing a fluid sample to a different pressure than the fluid pressure within the other fluid sample chamber.

11. An apparatus for controlling the pressure of a pressurized wellbore fluid sample collected downhole in a well, comprising:

a housing having a hollow interior;

a piston within said housing interior for defining a fluid sample chamber, wherein said piston is moveable within said housing interior to selectively change said fluid sample chamber volume, and wherein said piston comprises an outer sleeve and an inner sleeve moveable relative to said outer sleeve;

a pump for introducing a fluid sample under pressure into said fluid sample chamber;

retainer means for retaining said piston outer sleeve relative to said housing; and

a valve for selectively permitting pressurized wellbore fluid to move said piston inner sleeve relative to said piston outer sleeve so that fluid in said fluid sample chamber is compressed.

12. An apparatus as recited in Claim 11, further comprising a valve for selectively blocking fluid communication between said pump and said fluid sample chamber.

13. An apparatus as recited in Claim 12, wherein said valve comprises a check valve.

14. An apparatus as recited in Claim 11, further comprising a lock for retaining said piston inner sleeve stationary relative to said housing.

15. A method for controlling the pressure of a pressurized well fluid sample from a wellbore, comprising :

lowering a housing into the wellbore, wherein said housing has a piston within a hollow interior of said housing which is moveable to define a fluid sample chamber;

pumping well fluid into said fluid sample chamber to collect a well fluid sample;

operating a valve to introduce well fluid at a downhole hydrostatic pressure into contact with said piston to move said piston for pressurizing the well fluid sample within said fluid sample chamber;

retaining the well fluid sample within said fluid sample chamber as said piston moves to compress the well fluid sample within said fluid sample chamber;

locking said piston relative to said housing to fix the volume of well fluid sample within said fluid sample chamber when the well fluid reaches a selected pressure above the downhole hydrostatic pressure; and,

withdrawing said housing to the well surface.

16. A method as recited in Claim 15, further comprising the step of removing the well fluid sample from said fluid sample chamber while maintaining the pressure of the well fluid sample above a selected pressure.

17. A method as recited in Claim 15, further comprising the step of moving said housing to another location within the wellbore after said piston is locked relative to said housing, and further comprising the steps of pumping a second well fluid sample into a second well fluid chamber, of operating said valve to move a second piston to compress the second fluid sample, and of locking said piston relative to the said housing to fix the volume of the second fluid sample.

18. A method as recited in Claim 17, wherein said second pressure compresses the second fluid sample to a pressure greater gm the pressure of the other fluid sample.

19. A method as recited in Claim 15, further comprising the step of lowing said housing within the wellbore so that a greater hydrostatic fluid pressure moves said piston to further compress the well fluid sample before said housing is withdrawn to the well surface.

20. A method as recited in Claim 15, wherein said piston compresses the well fluid sample to a pressure so that the well fluid sample does not change phase when said housing is withdrawn to the well surface.

21. A process for transferring a sample of earth formation fluid from a downhole production depth to a wellbore surface, said process comprising:

(a) lowering a unitized assembly of downhole tools into a wellbore, said assembly including a formation fluid extraction tool, a formation fluid sample retrieval tank and a surface controlled pump for selectively charging said sample retrieval tank with formation fluid;

(b) positioning said fluid extraction tool at a first wellbore depth;

(c) extracting formation fluid at said first wellbore depth;

(d) charging a first sample volume in said sample retrieval tank with a corresponding volume of the first depth formation fluid;

(e) applying in situ wellbore pressure to an element of said sample retrieval tank to reduce the first sample volume of said first sample tank to a second sample volume less that said first sample volume without displacement of fluid from said sample retrieval tank whereby the first sample volume of first depth formation fluid is compressed to a pressure substantially greater than said in situ wellbore pressure;

(f) structurally securing said second sample volume; and,

(g) retrieving the downhole tool assembly to the wellbore surface.

22. A process as described by claim 21 wherein said downhole tool assembly includes a second sample retrieval tank and said process further comprises:

(a) repositioning said formation extraction tool to a second wellbore depth prior to surface retrieval of said tool assembly;

(b) extracting formation fluid at said second wellbore depth;

(c) charging a first sample volume of said second sample retrieval tank with second depth formation fluid;

(d) applying said second in situ wellbore pressure to an element of said second sample retrieval tank to reduce the first sample volume thereof to a second sample volume less than said first sample volume without displacement of fluid from said second sample retrieval tank whereby the first sample volume of second depth formation fluid is compressed to a pressure substantially greater than said second in situ wellbore pressure; and,

(e) structurally securing said second enclosed volume of said second sample retrieval tank.

23. A process as described by claim 21 wherein said structural component of said sample retrieval tank is provided less effective pressure area within said first enclosed volume than effective pressure area receiving said wellbore pressure.

24. A process for extracting a sample of earth formation fluid comprising:

(a) preparing a sample retrieval tank with a variable volume sample chamber;

(b) placing said sample retrieval tank in a wellbore;

(c) filling, in situ, a first volume of said sample chamber with a first volume of formation fluid;

(d) applying in situ wellbore pressure against a structural component of said sample retrieval tank to reduce said sample chamber to a second volume less than said first volume without displacement of fluid from said sample chamber whereby said formation fluid therein is compressed to a pressure substantially greater than said in situ wellbore pressure;

(e) securing the second volume position of said structural component; and,

(f) removing said sample retrieval tank from said wellbore.

25. A process as described by claim 24 wherein said structural component is a moveable partition between in situ wellbore fluid and formation fluid within said sample chamber.

26. A process as described by claim 24 wherein the in situ wellbore pressure applied against said structural component displaces said component into said sample chamber to reduce the chamber volume thereof.

27. A process as described by claim 26 wherein said in situ wellbore fluid bears upon a greater area of said structural component than formation fluid within said sample chamber.

28. An apparatus for retrieving a sample of earth formation fluid from a wellbore comprising:

(a) a cylinder having a moveable piston therein to define a variable volume sample chamber, said piston having relatively moveable first and second pressure bearing elements, each of said pressure bearing elements having respective sample chamber pressure bearing areas and wellbore pressure bearing areas wherein the wellbore pressure bearing area of said second pressure bearing element is greater than the sample chamber pressure bearing area of said second pressure bearing element;

(b) a pump for extracting fluid from an earth formation and for discharge of said fluid through a transfer conduit into said sample chamber;

(c) a first valve in said transfer conduit for preventing fluid flow reversal from said sample chamber;

(d) a second valve for admitting wellbore fluid against the wellbore pressure area of said second pressure bearing element, said second valve being positioned on said first pressure bearing element and operable by arrival of said first pressure bearing element at a position corresponding to a maximum sample chamber volume.

29. An apparatus as described by claim 28 wherein said first and second pressure bearing elements include coaxially moveable first and second sleeve members, respectively, the second sleeve member being moveable within the first sleeve member.

30. An apparatus as described by claim 29 wherein said first and second sleeve members have mutually engaged barb members to rectify relative displacement between said sleeve members.

31. An apparatus as described by claim 30 wherein the wellbore pressure bearing area of said first pressure bearing element comprises a substantially continuous piston face across one end of said first sleeve member, said valve being disposed within said piston face.

32. An apparatus as described by claim 29 wherein said cylinder is terminated at opposite ends by respective end walls whereby said variable volume sample chamber is expanded by displacement of said piston along said cylinder toward a first end wall.

33. An apparatus as described by claim 32 wherein said second valve is positioned on said first sleeve member to be opened by proximity of said piston with said first cylinder end wall.

34. An apparatus as described by claim 33 wherein said second valve admits wellbore fluid between said first and second sleeve members to axially displace said second sleeve member relative to said first sleeve member.

35. An apparatus as described by claim 34 wherein said first and second sleeve members include a cooperative displacement rectifier whereby the displacement of said second sleeve member relative to said first sleeve member is unidirectional.

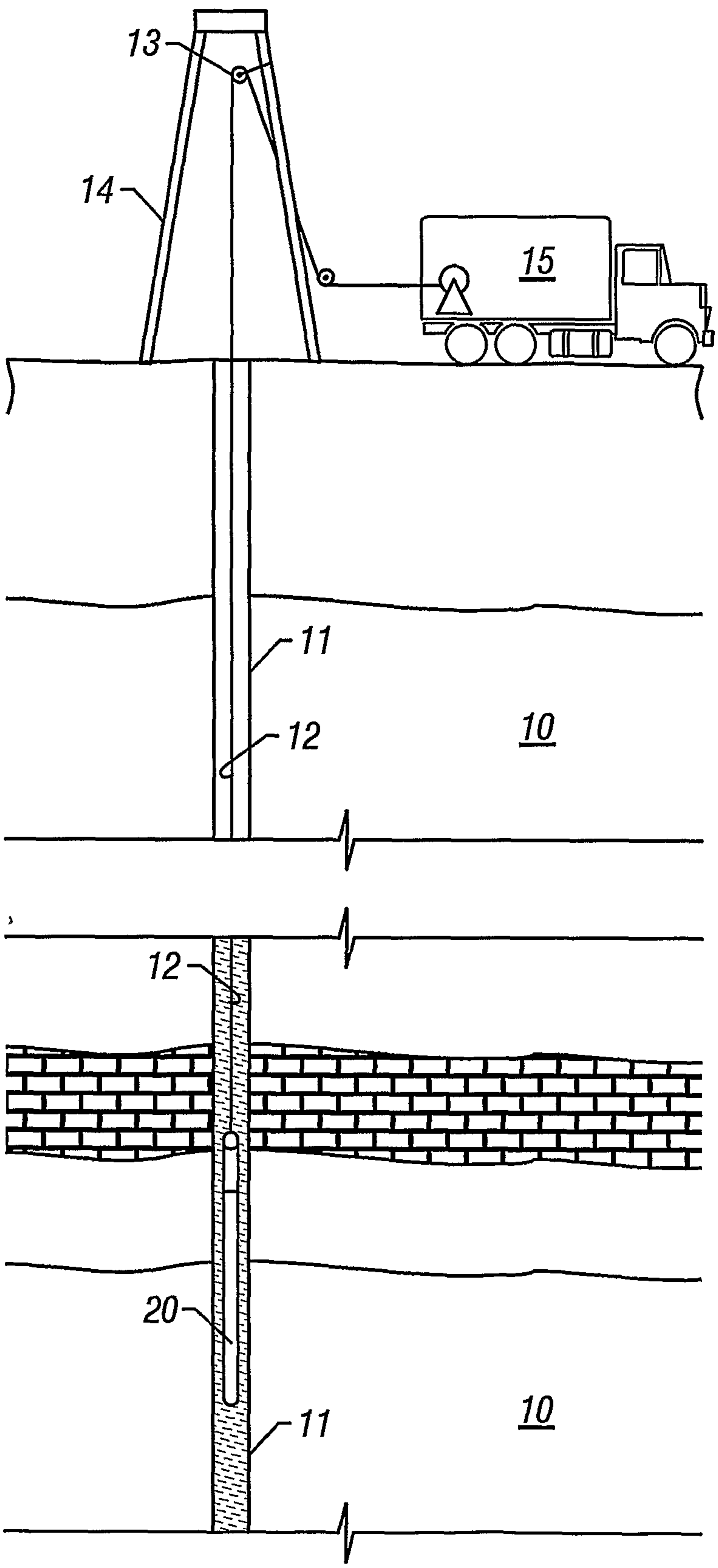

FIG. 1

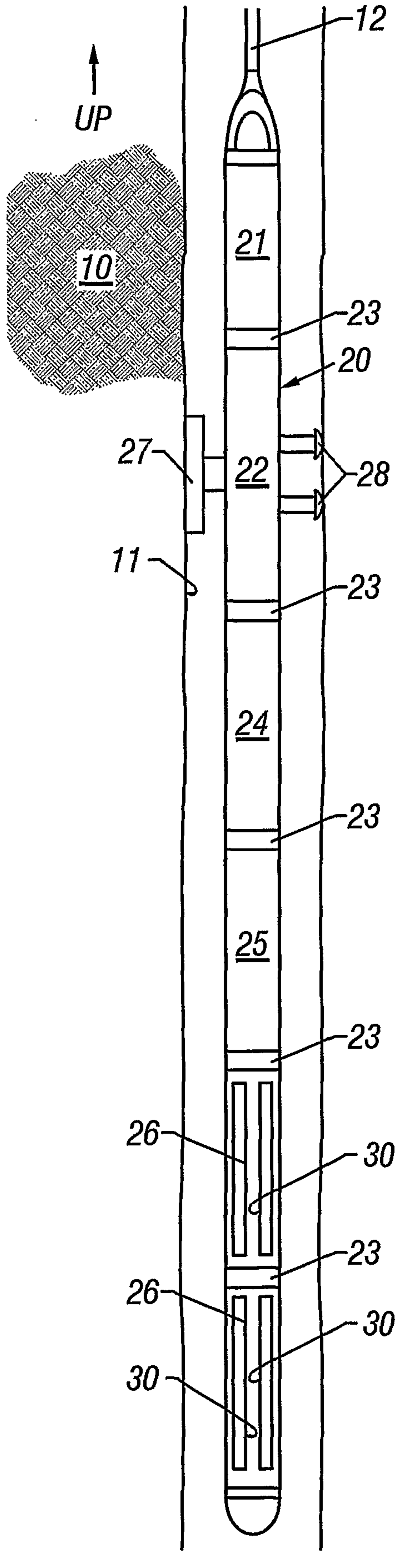
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FIG. 2

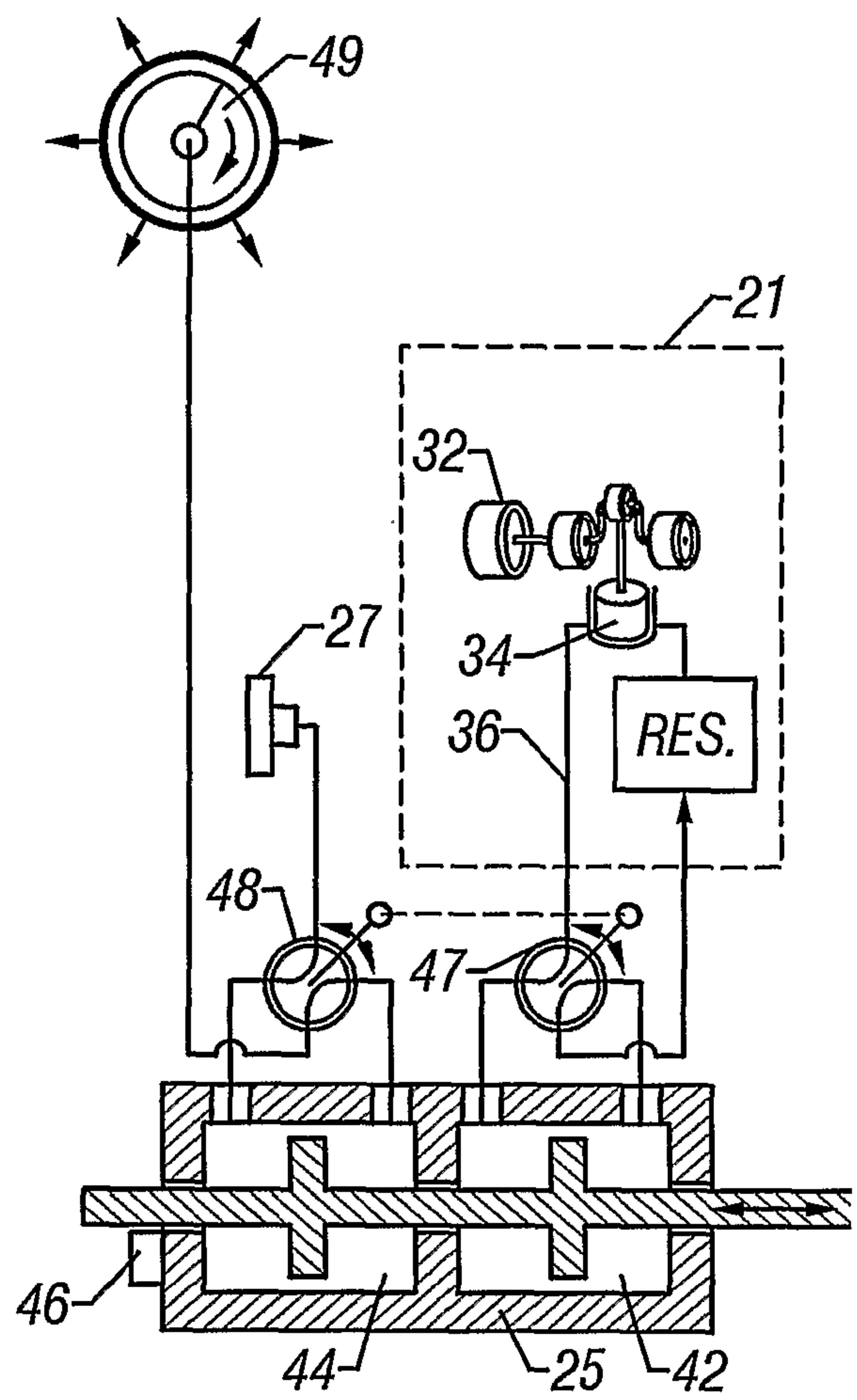
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FIG. 3

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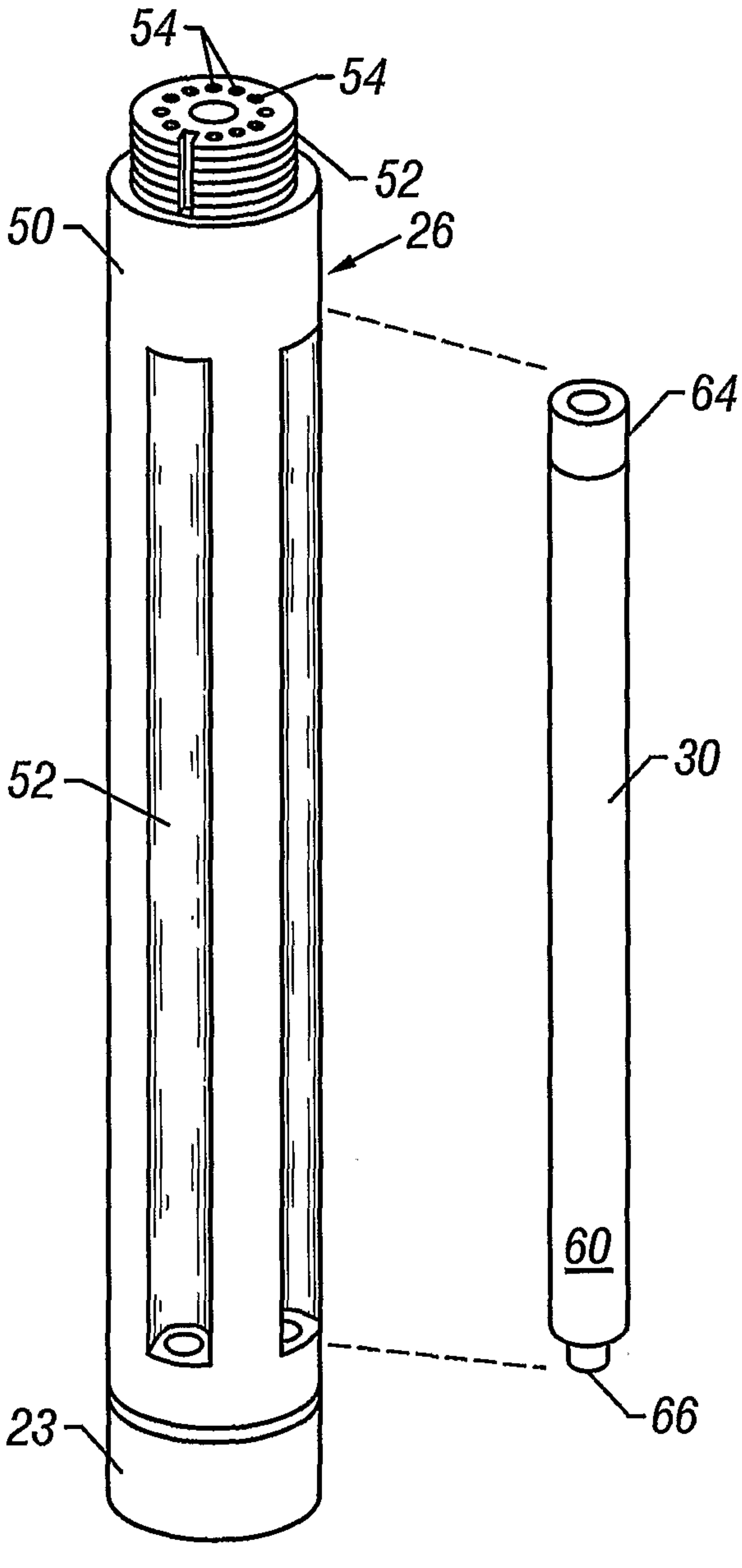

FIG. 4

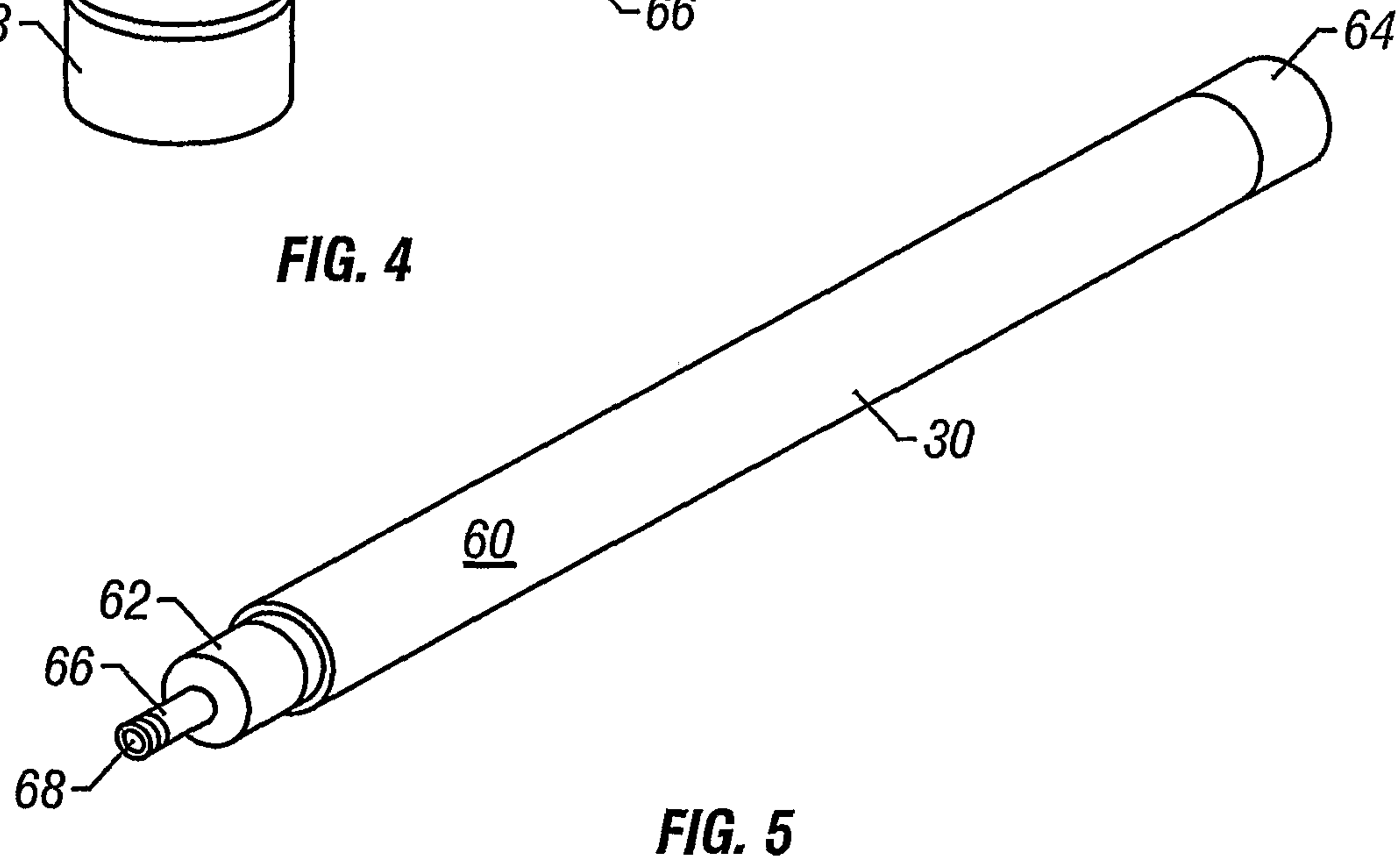

FIG. 5

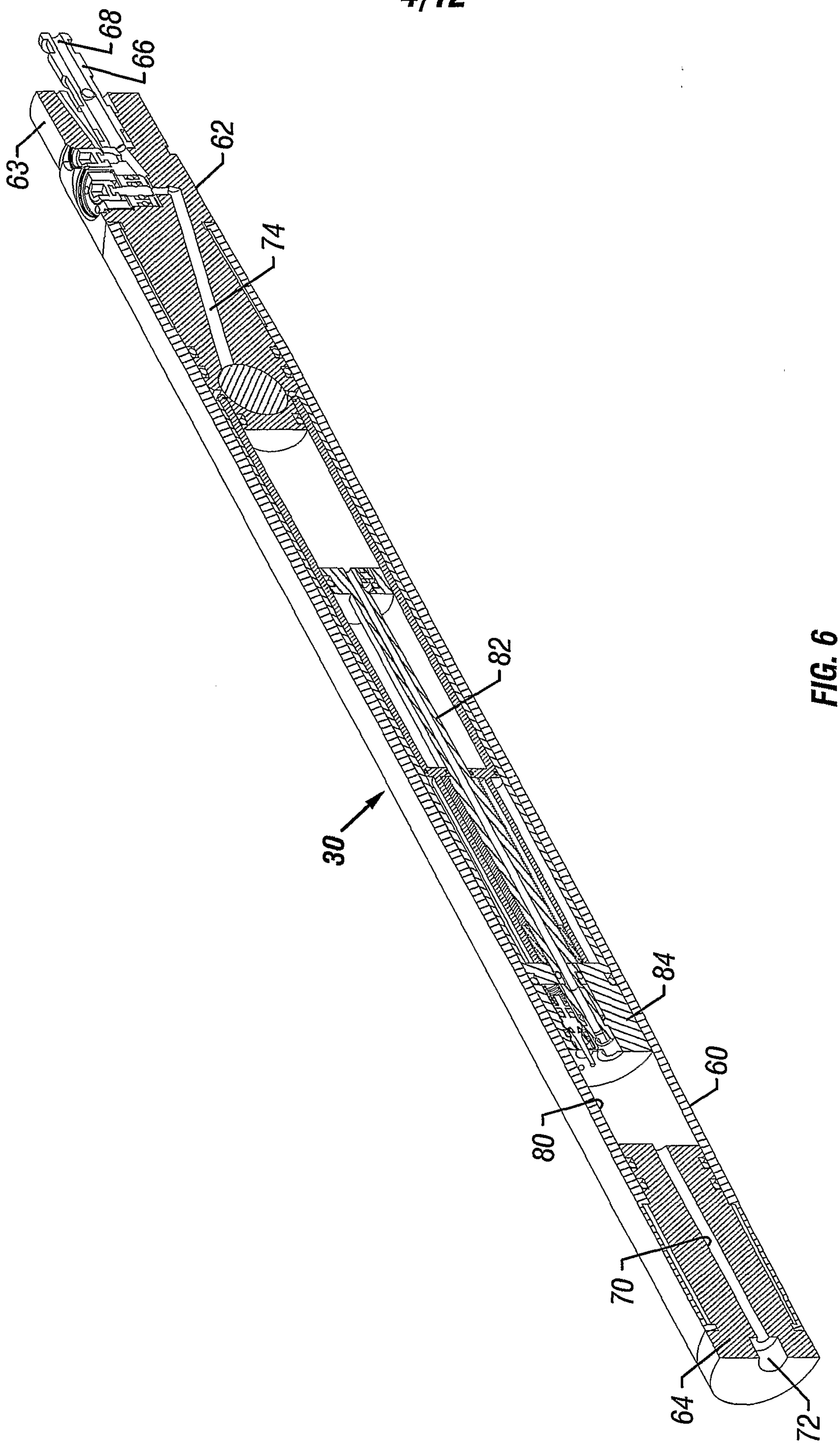

FIG. 6

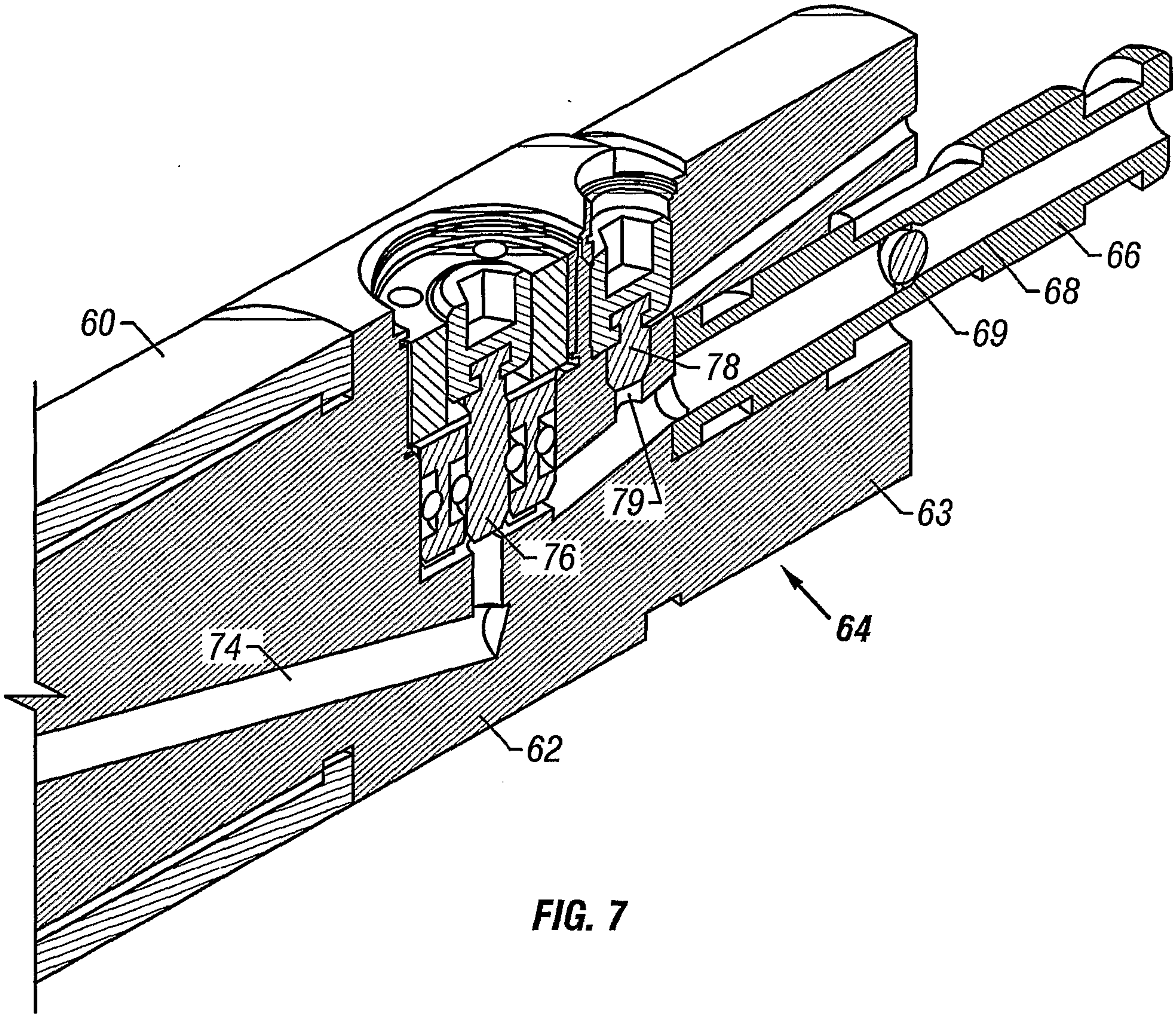

FIG. 7

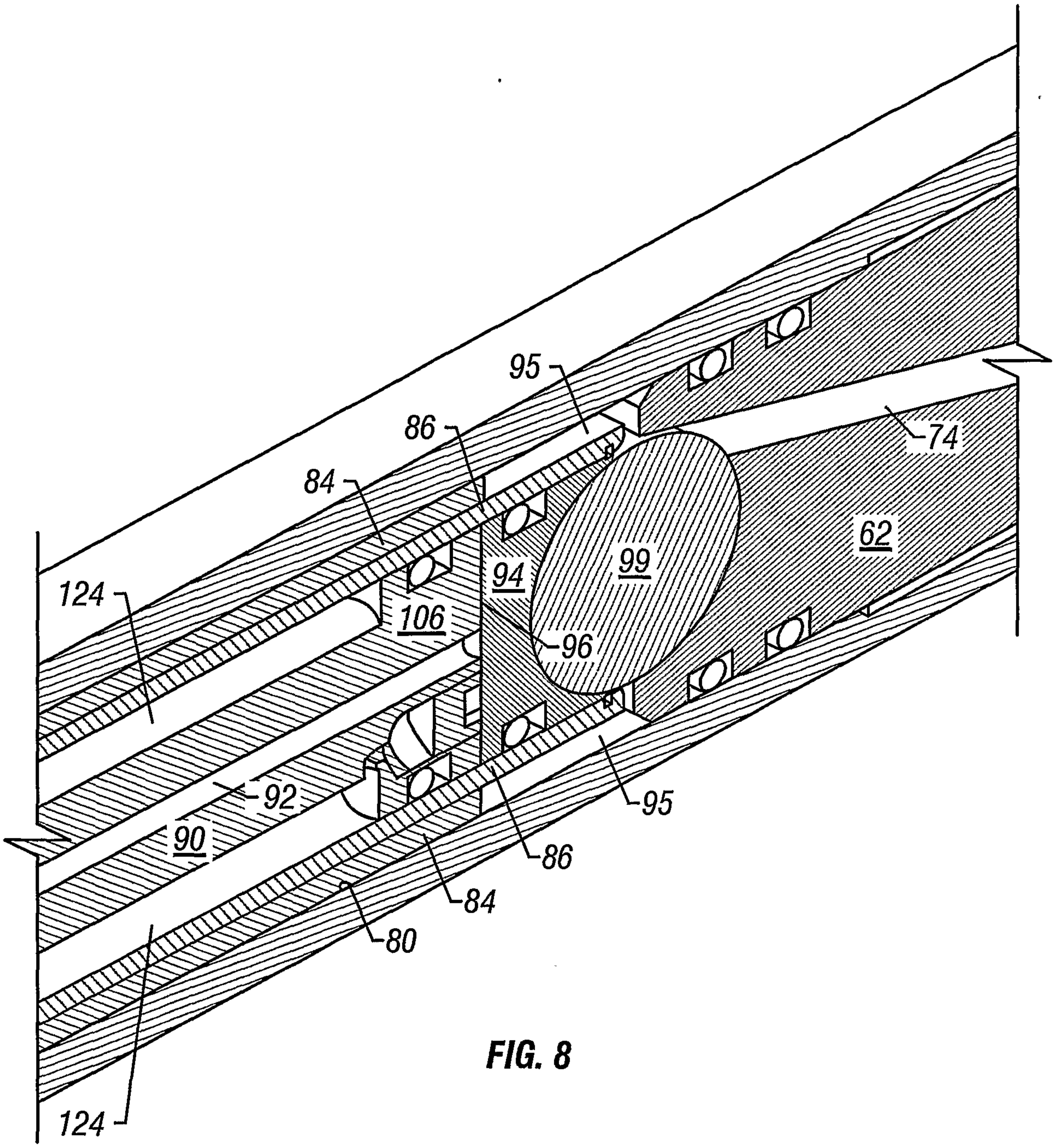

FIG. 8

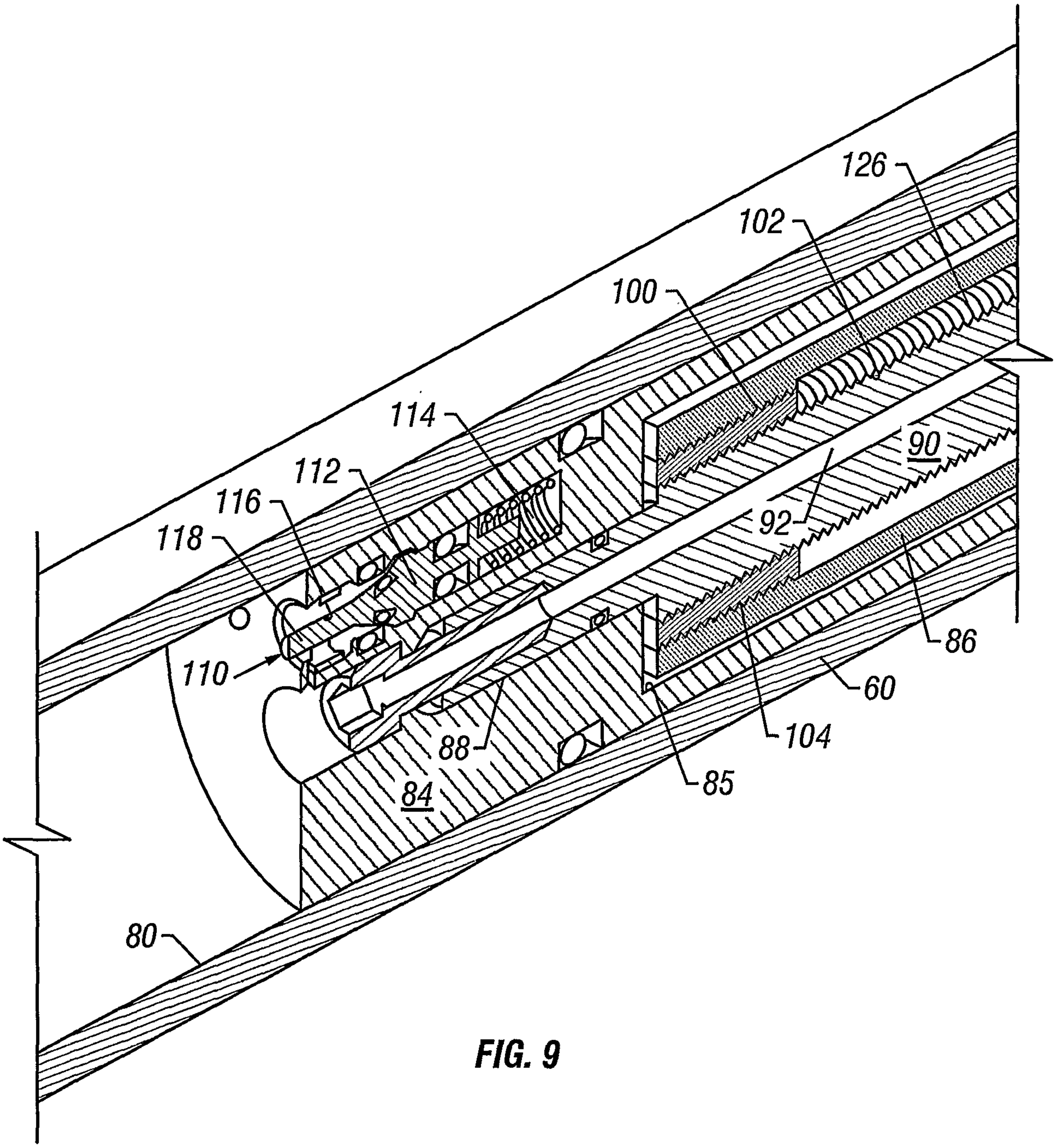

FIG. 9

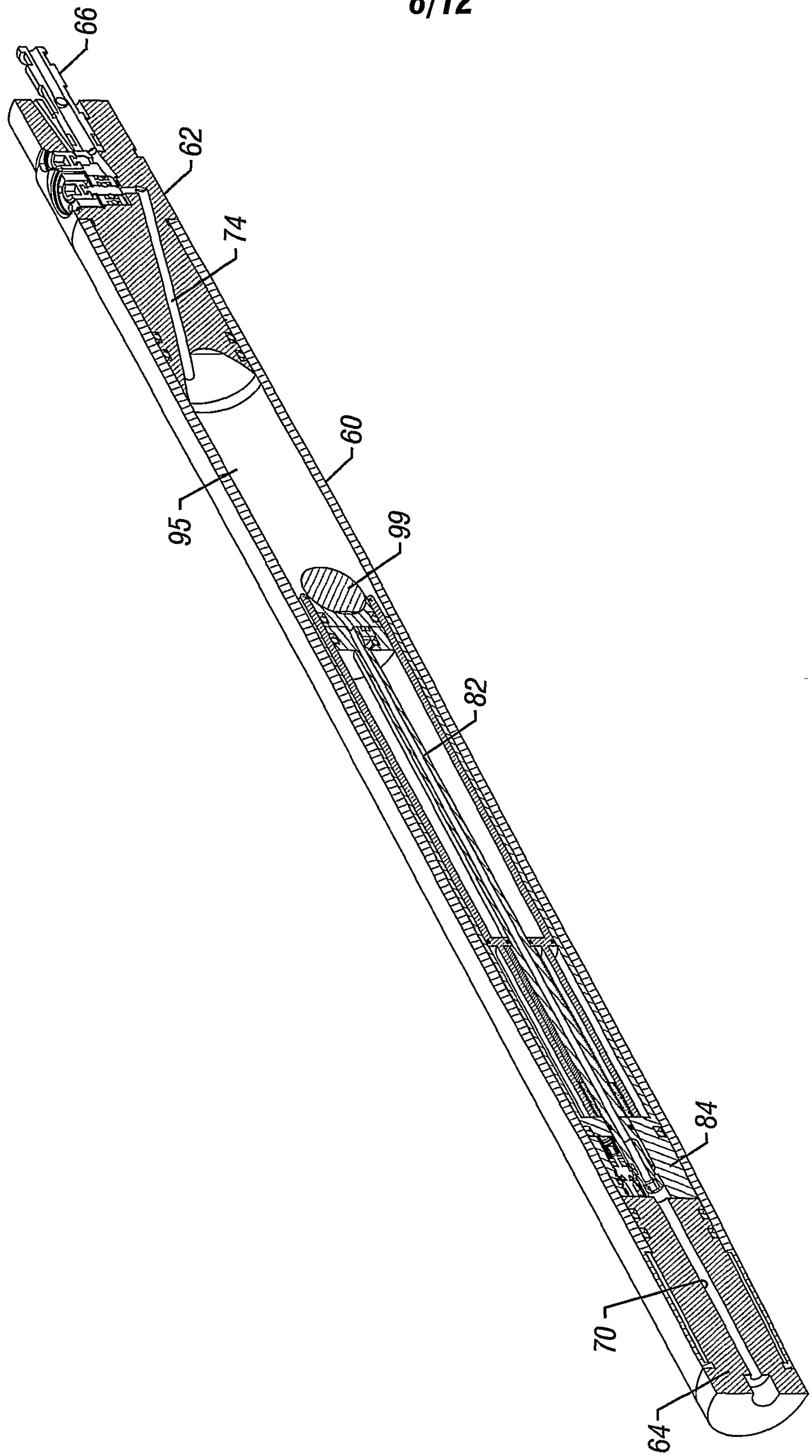

FIG. 10

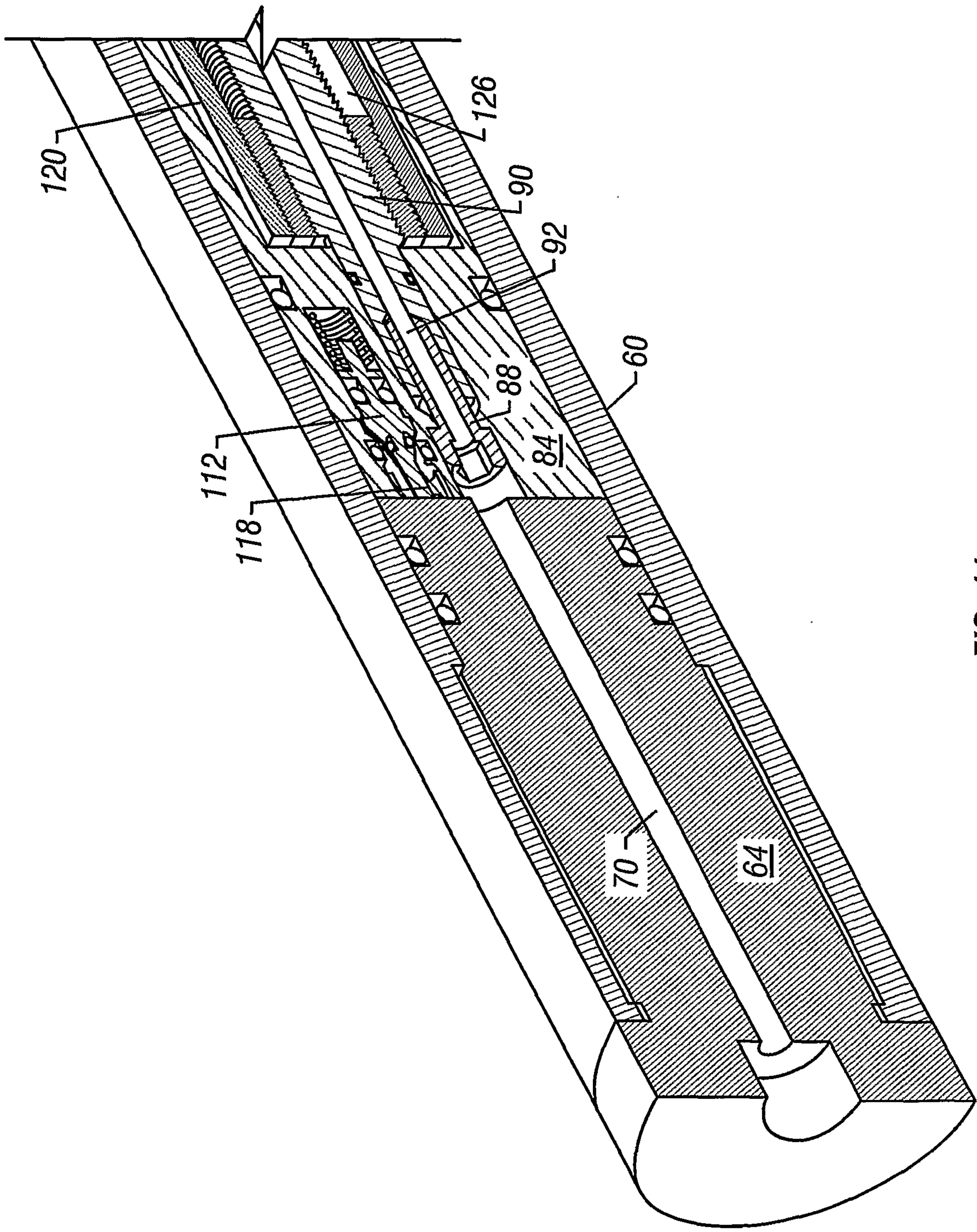

FIG. 11

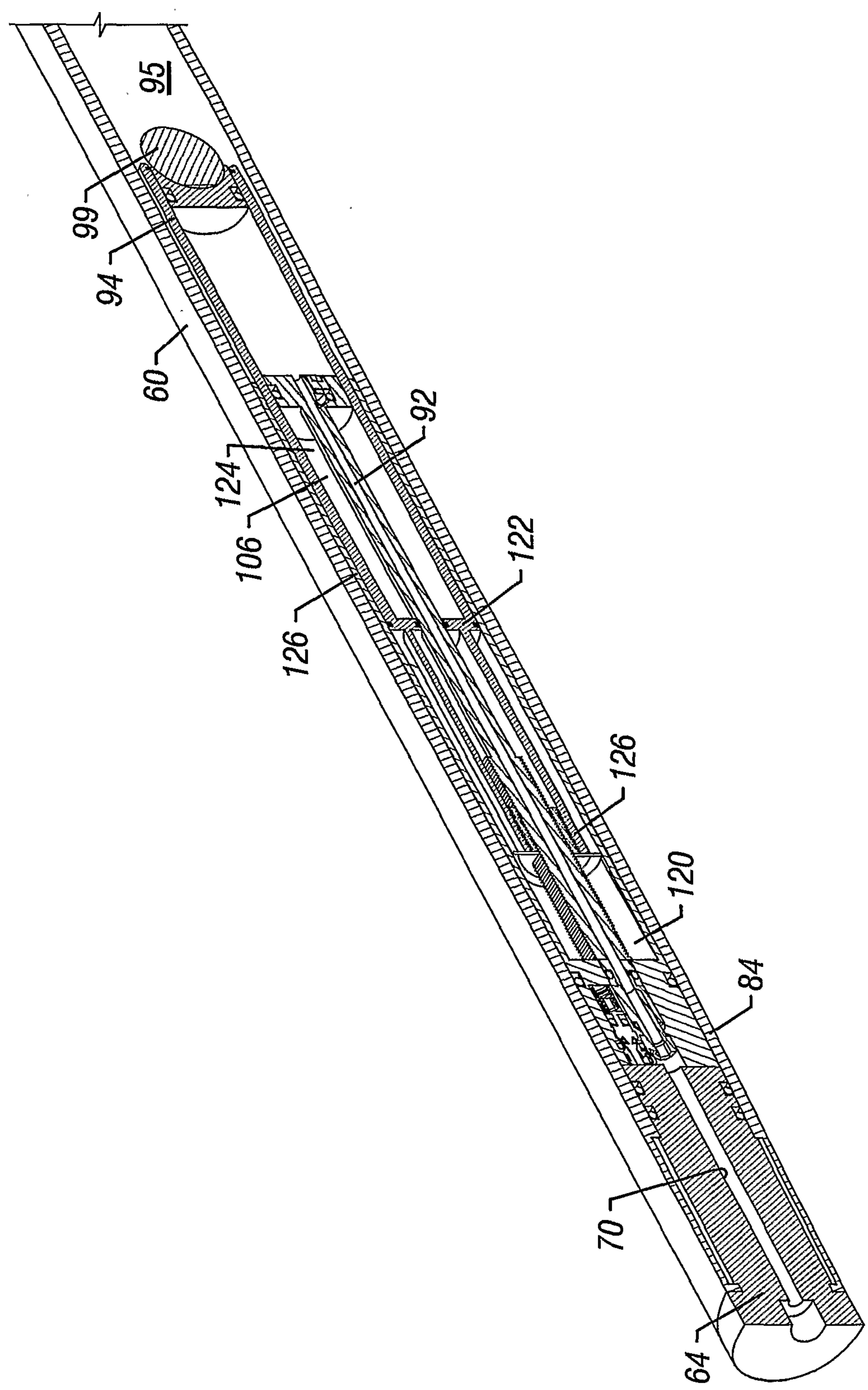

FIG. 12

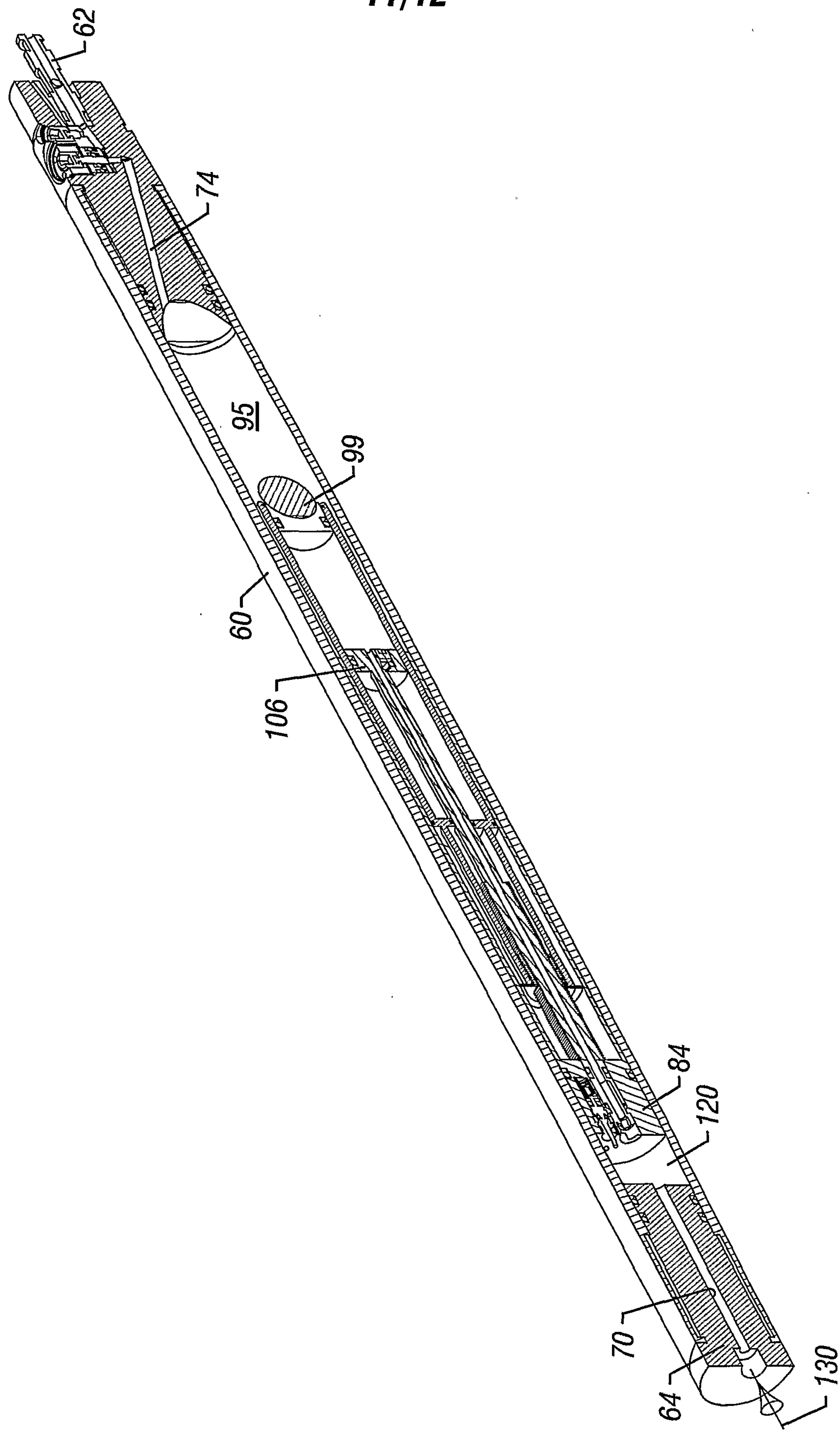

FIG. 13

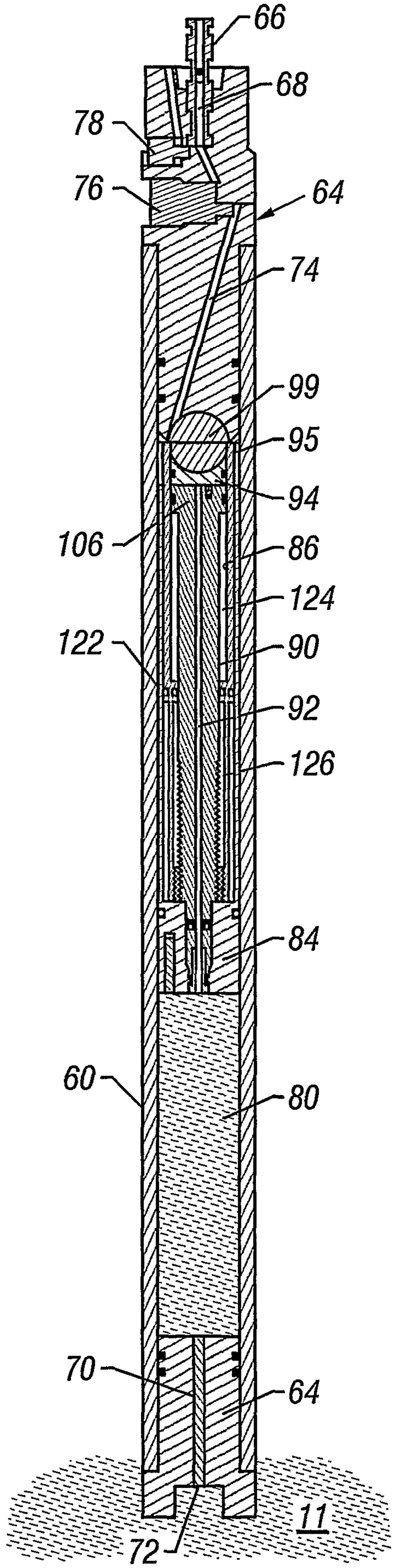
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FIG. 14


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