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(54) Titre : STRUCTURE COMPOSITE POURVUE DE CONTREFICHES A NOYAU CERAMIQUE ET PROCEDE DE FABRICATION

(54) Title: COMPOSITE STRUCTURE HAVING CERAMIC TRUSS CORE AND METHOD FOR MAKING THE SAME

(57) Abrégé/Abstract:

A CMC sandwich used to fabricate CMC structures includes facesheets bonded to a core reinforced with a ceramic truss comprising an array of CMC pins. The binder matrix in the ends of the pins is removed, leaving exposed, flexible ceramic fibers. The exposed ceramic fibers are bent so as to extend parallel to the facesheets, and are bonded to one or more plies of the facesheets. The binder matrix in the ends of the ceramic pins may be removed by mechanical or chemical processes.

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ABSTRACT OF THE DISCLOSURE

A CMC sandwich used to fabricate CMC structures includes facesheets bonded to a core reinforced with a ceramic truss comprising an array of CMC pins. The binder matrix in the ends of the pins is removed, leaving exposed, flexible ceramic fibers. The exposed ceramic fibers are bent so as to extend parallel to the facesheets, and are bonded to one or more plies of the facesheets. The binder matrix in the ends of the ceramic pins may be removed by mechanical or chemical processes.

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COMPOSITE STRUCTURE HAVING CERAMIC
TRUSS CORE AND METHOD FOR MAKING THE SAME

Technical Field

This disclosure generally relates to ceramic composite structures, and deals more particularly with a composite sandwich construction having a ceramic truss core, and a method of making the same.

Background

Ceramic matrix composite (CMC) structures may be used in aerospace and other applications because of their ability to withstand relatively high operating temperatures. For example, CMC structures may be used to fabricate parts subjected to high temperature exhaust gases in aircraft applications. One type of CMC structure employs a sandwich construction in which two CMC facesheets are bonded to a core. In one sandwich construction, the core may be reinforced by a truss-like array of CMC pins which extend through the thickness of the core and penetrate the facesheets. These pins provide load paths along which compressive, tensile and/or shear loads are transferred between the facesheets. The load carrying ability of this prior pin truss construction is limited however, due to the

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limited bond strength between the ends of the pins and the plies of the facesheets, especially where the facesheets are relatively thin.

The bond strength between the CMC pins and the facesheets may be increased if the ends of the pins could be bent so as to extend parallel to the facesheets, providing a greater bond area. This solution has not been feasible however, because the CMC pins are relatively brittle and may break if attempts are made to bend the ends of the CMC pins.

Accordingly there is a need for a CMC structure having a ceramic truss core exhibiting improved bonding properties between the core and the facesheets. Embodiments of the disclosure are intended to satisfy this need.

SUMMARY

A CMC structure includes a sandwich construction having a ceramic truss reinforced core. Superior bonding between the core and facesheets is achieved by bending the outer ends of CMC pins forming the truss. By bending the ends of the CMC pins, a greater bond area is provided between the pins and the facesheets, thereby improving the load transmitting ability of the core. The ends of the CMC pins may be bent by removing the matrix material from the

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pin ends which binds the ceramic fibers. With the matrix material removed, the remaining ceramic fibers are relatively flexible, allowing them to be bent so that they extend parallel to and may be bonded with the planar surfaces of the facesheets.

According to one disclosed method embodiment, a ceramic composite structure may be fabricated by the steps comprising: forming a core including a ceramic truss having a plurality of pins formed from ceramic fibers held in a rigid binder; removing the binder from the ends of the pins to expose the ceramic fibers; bending the ends of the pins; and, bonding a facesheet to the ends of the pins. The ceramic truss may be formed by inserting the pins into a carrier such that the ends of the pins protrude from the carrier. The binder in the ends of the pins is then removed by etching, pulverizing or ablative processes. Plies of the facesheets may be applied to the core, penetrating the ends of the pins before the binder material is removed from the ends of the pins. Following removal of binder material, the exposed ceramic fibers in the ends of the pins may be bonded to or between plies of the facesheets.

According to another method embodiment, a ceramic truss core used in a ceramic composite structure may be

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fabricated by a process comprising the steps of: forming a ceramic truss using a plurality of composite ceramic pins, wherein the composite ceramic pins comprise ceramic fibers held in a matrix; and, removing the matrix from the ends of the pins to expose the ceramic fibers. The truss may be formed by partially inserting the pins into a carrier foam such that the ends of the ceramic pins remain exposed. The matrix is removed from the ends of the pins so that only flexible ceramic fibers remain. The flexible ceramic fibers may be bent to conform to the surface of facesheets to which the core may be bonded. The matrix binder may be removed from the ends of the CMC pins by any of several processes, including etching, pulverizing or ablation. A layer of protective material may be applied over the carrier in order to protect the carrier during the matrix binder removal process.

According to a further method embodiment, a ceramic composite structure may be made by the steps comprising: fabricating a core, and bonding a facesheet to the core by bonding the facesheet to exposed, bent ends of ceramic fibers forming a part of the core. The core may be made by: forming an array of composite ceramic pins within a carrier, each of the pins comprising ceramic fibers held in a matrix and protruding from the carrier; removing the matrix from

the protruding ends of the pins to expose portions of the ceramic fibers; and, bending the exposed portions of the ceramic fibers so that they may be bonded to the facesheet.

According to another embodiment, a composite ceramic structure comprises: a pair of generally parallel composite ceramic facesheets; and, a core including a truss disposed between and bonded to the facesheets, the truss including a plurality of composite ceramic pins, each of the pins including medial portions extending generally transverse to the facesheets, and distal portions extending generally parallel and bonded to the facesheets. At least one of the facesheets may include multiple plies, and the distal portions of the pins may be sandwiched between these plies. Alternatively, the distal portions of the pins may be bonded to an inside face of the facesheets.

In accordance with one aspect of the invention there is provided a method of making a ceramic composite structure. The method involves the steps of (A) forming a core including a ceramic truss having a plurality of pins formed from ceramic fibers held in a rigid binder, (B) removing the binder from the ends of the pins to expose the ceramic fibers, (C) bending the ends of the pins, and (D) bonding a facesheet to the ends of the pins.

Step (A) may include inserting a length of pin stock into a carrier, and cutting the length of pin stock such that ends of the pins may be exposed.

The pin stock may be inserted into a layer of foam.

The method may further involve protecting a portion of the core during the removal of the binder in step (B) by applying a protective coating to the core portion.

Step (B) may be performed by etching the ends of the pins.

Step (B) may be performed by pulverizing the ends of the pins.

Step (B) may be performed by ablation.

Step (C) may be performed by bringing the facesheet into contact with the exposed ceramic fibers, and bending the exposed ceramic fibers using the facesheet.

Step (C) may include bonding the exposed ceramic fibers between plies of ceramic prepreg.

The method may involve specifying and designing an aircraft subassembly including the composite structure.

The method may involve procuring the material used to manufacture the composite structure.

In accordance with another aspect of the invention there is provided a composite ceramic structure. The structure includes a pair of generally parallel composite ceramic facesheets, and, a core disposed between and bonded to the facesheets. The core includes a ceramic truss and the truss includes a plurality of composite ceramic pins. Each of the pins includes medial portions extending generally transverse to the facesheets, and

distal portions extending generally parallel and bonded to the facesheets.

At least one of the facesheets may include multiple plies and, the distal portions of the pins may be sandwiched between the plies.

The media portion of at least certain of the pins may form an angle of approximately 30 degrees relative to the planes of the facesheets.

The distal portions of the pins may be bonded to interior opposing surfaces of the facesheets.

The core further may include structural foam surrounding the ceramic truss.

Other features, benefits and advantages of the disclosed embodiments will become apparent from the following description of embodiments, when viewed in accordance with the attached drawings and appended claims.

BRIEF DESCRIPTION OF THE ILLUSTRATIONS

FIG. 1 is an isometric illustration of a prior art CMC sandwich construction employing a ceramic truss core,

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the carrier not shown and portions of the facesheets having been broken away to better show the straight ends of CMC pins.

FIG. 2 is a cross sectional illustration of a portion of a CMC sandwich construction having a ceramic truss core according to an embodiment of the disclosure.

FIG. 3 is a cross sectional view illustrating one step of a method for making the CMC sandwich construction.

FIG. 4 is a cross sectional view illustrating another step in the method.

FIG. 5 is a view similar to FIG. 4 but showing the bent ends of the CMC pins having been bonded between plies of a facesheet.

FIG. 6 is a cross sectional view illustrating an alternate embodiment of a CMC sandwich construction.

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FIG. 7 is a simplified flow diagram illustrating the basic steps of a process used to fabricate a CMC sandwich having a ceramic truss core

FIG. 8 is a simplified flow diagram illustrating alternative steps for fabricating the ceramic pin stock.

FIG. 9 is a flow diagram of an aircraft production and service methodology.

FIG. 10 is a block diagram of an aircraft.

DETAILED DESCRIPTION

Referring first to FIG. 1, a typical prior art CMC sandwich construction comprises a pair of parallel, CMC facesheets 14, 16 bonded to a core that includes an array of ceramic pins 18. The pins 18 are arranged in "X" patterns and function to reinforce a core that may include a structural foam (not shown). Each of the pins 18 is straight, and has outer ends extending through and bonded to facesheets 14, 16. The bond area between the pins 18 and the facesheets 14, 16 is limited to the depth of penetration of the ends of the pins 18 into the facesheets 14, 16.

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Referring now to FIGS. 2 and 6, a CMC sandwich construction 20 broadly comprises a pair of generally parallel CMC facesheets 24, 26 bonded to a core 22. Core 22 may comprise a CMC truss 25 held within a layer 30 of structural or semi-structural foam. The truss 25 reinforces the core 22 and may function to transmit compressive, tensile and/or shear loads between the facesheets 24, 26. In the illustrated example, the facesheets 24, 26 are flat and extend substantially parallel to each other; however other geometries are possible, including without limitation, non-parallel curvilinear and combinations of curvilinear and rectilinear.

Each of the facesheets 24, 26 may comprise multiple layers or plies of ceramic cloth fibers dipped in a ceramic slurry. As used herein, the term "ceramic fiber" refers to the conventionally known and commercially available ceramic materials that are fabricated in fiber form. The ceramic fibers may include, but are not limited to, silicon carbide, silica, TYRANNO[®], alumina, alumino-silicate aluminoborosilicate, silicon nitride, silicon boride, silicon boronitride, and similar materials. The truss structure 25 defines load paths that reinforce the sandwich construction 20 allowing CMC structures to be fabricated

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that are both self supporting and load carrying, if desired. The CMC sandwich 20 is particularly well suited to high temperature applications since all the constituents used in the sandwich 20 are ceramic-based.

Layer 30 forms a carrier for holding the truss 25 in place during fabrication, and may add structural rigidity to the sandwich 20, depending upon the materials used. The carrier layer 30 may comprise any of a variety of materials including for example, without limitation, organic fugitive foam, a lightweight, closed cell polynethacrylimide (PMI) foam, tile, rigidized batting, or other ceramic material. Further examples of ceramic materials that may be used as the carrier layer 30 include, without limitation, ceramic felt, other fibrous ceramic insulation (soft or rigid), monolithic ceramics, etc. One particular rigid foam suitable for use as the carrier layer 30 is disclosed in U.S. Patent No. 6,716,782 issued April 6, 2002 and assigned to The Boeing Company. The rigid foam insulation described in this prior patent is a combination of ceramic fibers that are sintered together to form a low density, highly porous material with low thermal conductivity. This foam exhibits high tensile strength and good dimensional stability. As used herein, "high temperature" material is generally

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intended to refer to temperatures above which polymeric materials exhibit diminished capacity.

The truss structure 25 comprises an array of CMC pins 28 extending through the thickness of the carrier layer 30, generally transverse to the facesheets 24, 26. The pins 28 are formed from pin stock comprising ceramic fibers held in a rigid ceramic binder or matrix. The pins 28 may be fabricated with materials that allow the matrix material to be etched away, for purposes which will be described below. The diameter of the individual fibers in the pins 28 is relative small compared to the overall pin 28; for example, in one satisfactory embodiment, the fibers may each have a diameter of approximately 11 micrometers, where the pin has an overall diameter of approximately 700 micrometers.

The pins 28 may be arranged in groups forming a geometric truss network, such as a tetragonal geometry, for example. Each of the pins 28 include straight, medial portions 28a, and opposite distal portions 28b which are sandwiched between and bonded to adjacent plies 24a, 24b and 26a, 26b of the respective facesheets 24, 26. In one embodiment, the pins 28 may form an angle of approximately 30 degrees relative to an axis extending normal to the

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facesheets **24**, **26**, as best seen in FIG. **2**. The distal portions **28b** of each of the pins **28** are bent, so as to extend generally parallel to the plane of the facesheets **24**, **26**. The length of the distal portions **28b** will depend on the particular application; in one embodiment, a length approximately equal to **4** to **5** times the diameter of the pin **28** provided satisfactory results.

As previously noted, in the embodiment illustrated in FIGS. **2** and **5**, the distal portions **28b** are sandwiched between and bonded to adjacent plies **24a**, **24b**, and **26a**, **26b** of the corresponding facesheets **24**, **26**. The strength of the bond between each of the pins **28** and the facesheets **24**, **26** may be determined in part by the length over which the distal portion **28b** is bonded to the facesheets **24**, **26**. In the final, cured sandwich construction **20**, the use of applied adhesives along with ceramic matrix material derived from the plies **24a**, **24b**, **26a**, **26b** function to bond the distal portions **28b** of the pins **28** to the facesheets **24**, **26**.

An alternate embodiment **20a** of the sandwich construction is shown in FIG. **6**. In this embodiment, the distal portions **28b** of the pins **28** are bonded directly to the inside, opposing faces of the facesheets **24**, **26** through

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a layer **40** of adhesive which may comprise a film adhesive applied during the fabrication process and/or matrix material derived from the facesheets **24**, **26**.

Attention is now directed to FIGS. **3**, **4**, **5**, **7** and **8** which disclose a method for fabricating the CMC sandwich structure **20** described above. Beginning with step **42** (FIG. **7**), material for forming the pins **28** is fabricated using for example, without limitation, a poltrusion process which is known in the art. Fabrication of the pins **28** may be tailored to facilitate the process that is later used to remove the matrix material from the ends of the pins to expose the ceramic fibers.

Referring particularly to FIG. **8**, a continuous length of pin stock may be fabricated by poltrusion in which ceramic fibers are poltruded, as shown at step **60**. Next, any of three processes designated as "A", "B", and "C" may be used to form a pin construction using materials and processes that render the pin more amenable to subsequent processes used to remove the matrix from the ends of the pins. Thus, using process "A", the protruded ceramic fibers are undercoated at step **62** with a low temperature coating such as epoxy at a set interval. Next, at step **64**, the undercoated fibers are overcoated with a ceramic slurry, and

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then baked at step 66. The alternative process "B" begins at step 68 in which the ceramic fibers are coated with a material to tailor the strength and brittleness of the pins. Similarly, a varying temperature baking schedule may be used at step 70 to better enable removal of the matrix with mechanical, thermal or chemical means. The alternative process "C" begins with undercoating the fibers with an epoxy or similar coating at step 72, following which, at step 74, the undercoated fibers are overcoated with a ceramic slurry. Then, at step 76, the coated fibers are baked at an intermediate temperature.

Returning now to FIG. 7, the pin stock having been fabricated at step 42, a suitable carrier 30 is fabricated at step 44, which may comprise forming a layer of light weight, low density foam or ceramic material as previously described. Depending upon the process used to remove the matrix binder from the pins 28 in a later step, a protective coating 32 may be optionally applied to the carrier 30 at step 46 in order to protect the carrier 30 against erosion or other damage during the matrix removal procedure.

At step 48, the individual pins 28 are inserted into the carrier 30. The pin insertion process may be carried

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out using known equipment designs that insert the pin stock into the carrier 30 at predetermined angles and then cuts the pin stock to the desired final length of the pin 28. This pin insertion process is performed such that the outer ends of the pins remain exposed, protruding from the carrier 30.

\Next, at step 50, one or two plies of prepreg may be optionally applied over the surface of the truss core, with the ends of the pins 28 passing through the prepreg layers in order to better bind and lock the pins 28 in the facesheets 24, 26. At step 52, the ends of the pins 28 are then flayed by removing the matrix binder in the distal portions 28b using any of several processes. Removal of the rigid matrix binder exposes the ceramic fibers 34 in the distal portions 28b, as shown in FIGS. 4 and 5. The exposed, individual ceramic fibers in the ends of the pins 28 are relatively flexible, due to their relatively small diameter, thus allowing the distal portions 28b to be bent or flayed so as to lie parallel to the facesheets 24, 26.

The matrix binder may be removed from the distal portions 28b of the pins 28 by chemical etching, pulverizing, or other forms of mechanical or ablative

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processes which may include, but are not limited to, erosion, evaporation, melting and vaporization. For example, the ends of the truss core may be immersed in a chemical etchant so as to subject the distal portions 28b to chemical etching which removes the matrix binder. During this process, the coating 32 protects the medial portions 28a of the truss core from damage. One mechanical process for removing the matrix binder from the ends of the pins may comprise crushing the pin ends between two platens or similar mechanical apparatus. Other chemical processes may be used to remove the matrix binder from the pin ends which are particularly formulated to remove the undercoating and/or overcoating applied to the ceramic fibers as previously described with reference to FIG. 8.

In those applications in which the protective coating 32 is applied to the carrier 30, step 54 may be optionally performed, consisting of the removal of the protective coating 32 by any of several suitable processes, including incineration (burning).

At step 56, the lay-up sandwich is placed on a tool, following which, at step 58, the lay-up is cured and sintered in order to bond the prepreg to the core and create a fully cured sandwiched construction. Mechanical pressure

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may be applied in the direction of the arrow 36 (FIG. 4) in order to compact the plies and force the exposed fibers 34 to lie flat, parallel to plies 24a, 24b.

Referring now to FIGS. 9 and 10, embodiments of the disclosure may be used in the context of an aircraft manufacturing and service method 78 as shown in FIG. 9 and an aircraft 94 as shown in FIG. 10. During pre-production, exemplary method 78 may include specification and design 80 of the aircraft 94 and material procurement 82. During production, component and subassembly manufacturing 84 and system integration 86 of the aircraft 94 takes place. Thereafter, the aircraft 94 may go through certification and delivery 88 in order to be placed in service 90. While in service by a customer, the aircraft 94 is scheduled for routine maintenance and service 90 (which may also include modification, reconfiguration, refurbishment, and so on).

Each of the processes of method 78 may be performed or carried out by a system integrator, a third party, and/or an operator (e.g., a customer). For the purposes of this description, a system integrator may include without limitation any number of aircraft manufacturers and major-system subcontractors; a third party may include without

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limitation any number of vendors, subcontractors, and suppliers; and an operator may be an airline, leasing company, military entity, service organization, and so on.

As shown in FIG. 10, the aircraft 94 produced by exemplary method 78 may include an airframe 98 with a plurality of systems 96 and an interior 100. Examples of high-level systems 96 include one or more of a propulsion system 102, an electrical system 104, a hydraulic system 106, and an environmental system 108. Any number of other systems may be included. Although an aerospace example is shown, the principles of the invention may be applied to other industries, such as the automotive industry.

The apparatus embodied herein may be employed during any one or more of the stages of the production and service method 78. For example, components or subassemblies corresponding to production process 84 may be fabricated or manufactured in a manner similar to components or subassemblies produced while the aircraft 94 is in service. Also, one or more apparatus embodiments may be utilized during the production stages 84 and 86, for example, by substantially expediting assembly of or reducing the cost of an aircraft 94. Similarly, one or more apparatus embodiments may be utilized while the aircraft 94 is in

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service, for example and without limitation, to maintenance and service **92**.

Although the embodiments of this disclosure have been described with respect to certain exemplary embodiments, it is to be understood that the specific embodiments are for purposes of illustration and not limitation, as other variations will occur to those of skill in the art.

THE EMBODIMENTS OF THE INVENTION IN WHICH AN EXCLUSIVE
PROPERTY OR PRIVILEGE IS CLAIMED ARE DEFINED AS FOLLOWS:

1. A method of making a ceramic composite structure,
5 comprising the steps of:

(A) forming a core including a ceramic truss
having a plurality of pins formed from ceramic
fibers held in a rigid binder;

(B) removing the binder from the ends of the
pins to expose the ceramic fibers;

(C) bending the ends of the pins; and

(D) bonding a facesheet to the ends of the
pins.

2. The method of claim 1, wherein step (A) includes:

inserting a length of pin stock into a carrier;
and

cutting the length of pin stock such that ends
of the pins are exposed.

3. The method of claim 2, wherein the pin stock is
inserted into a layer of foam.

4. The method of claim 1, further comprising the step
of:

(E) protecting a portion of the core during the removal of the binder in step (B) by applying a protective coating to the core portion.

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5. The method of claim 1, wherein step (B) is performed by etching the ends of the pins.

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6. The method of claim 1, wherein step (B) is performed by pulverizing the ends of the pins.

7. The method of claim 1, wherein step (B) is performed by ablation.

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8. The method of claim 1, wherein step (C) is performed by:

bringing the facesheet into contact with the exposed ceramic fibers; and

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bending the exposed ceramic fibers using the facesheet.

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9. The method of claim 1, wherein step (C) includes bonding the exposed ceramic fibers between plies of ceramic prepreg.

10. The method of claim 1, further comprising the step of:

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(F) specifying and designing an aircraft subassembly including the composite structure.

11. The method of claim 1, further comprising the step of:

5 (F) procuring the material used to manufacture the composite structure.

12. A composite ceramic structure, comprising:

10 a pair of generally parallel composite ceramic facesheets; and

a core disposed between and bonded to the facesheets, the core including a ceramic truss,
15 the truss including a plurality of composite ceramic pins, each of the pins including medial portions extending generally transverse to the facesheets, and distal portions extending generally parallel and bonded to the
20 facesheets.

13. The composite ceramic structure of claim 12, wherein:

25 at least one of the facesheets includes multiple plies; and

the distal portions of the pins are sandwiched between the plies.

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14. The composite ceramic structure of claim 12, wherein the medial portion of at least certain of the pins

form an angle of approximately 30 degrees relative to the planes of the facesheets.

- 5 **15.** The composite ceramic structure of claim **12**, wherein the distal portions of the pins are bonded to interior, opposing surfaces of the facesheets.
- 10 **16.** The composite ceramic structure of claim **12**, wherein the core further includes structural foam surrounding the ceramic truss.

Application number / numéro de demande: 2635305

Figures: 1, 2,

Pages: 1

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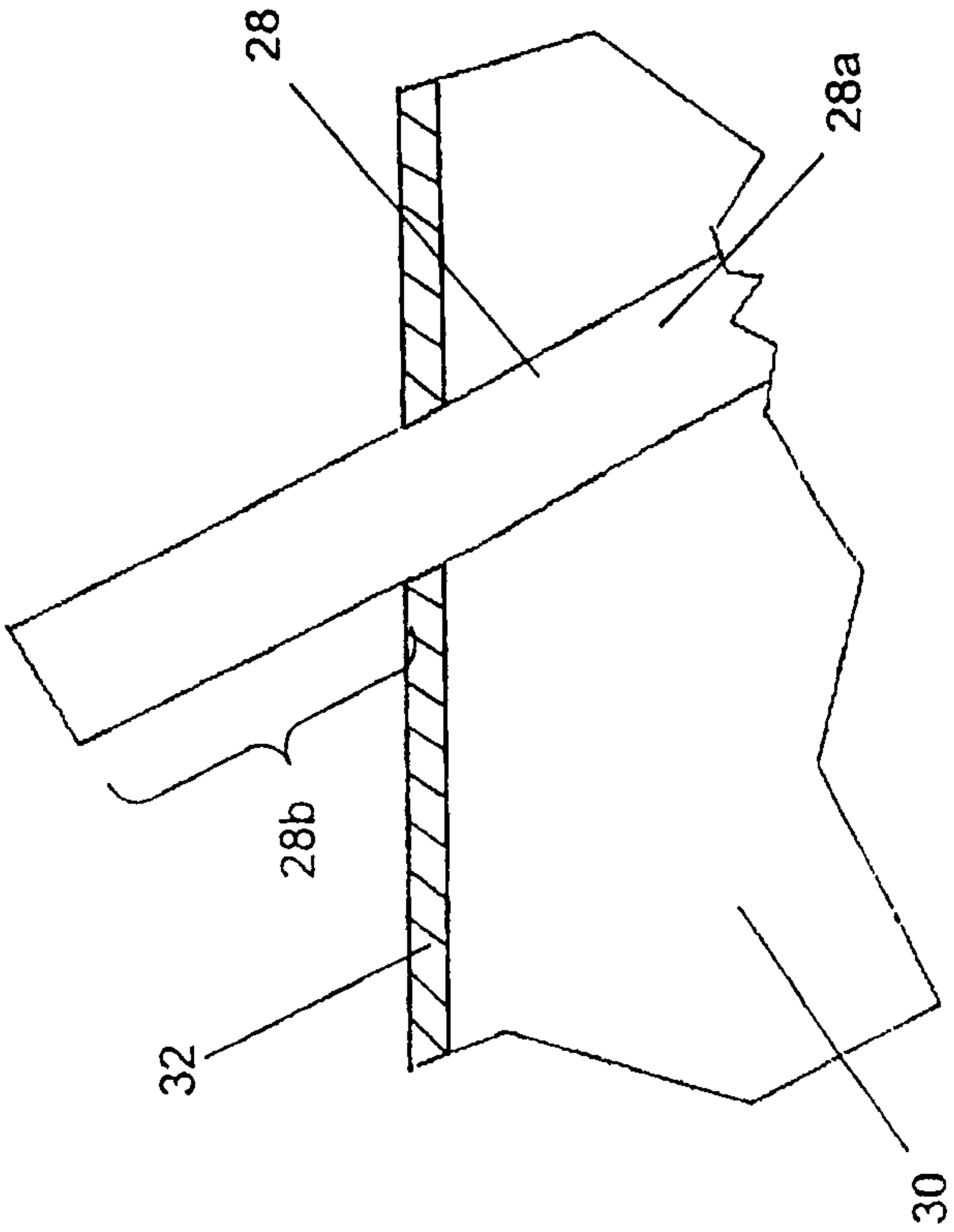
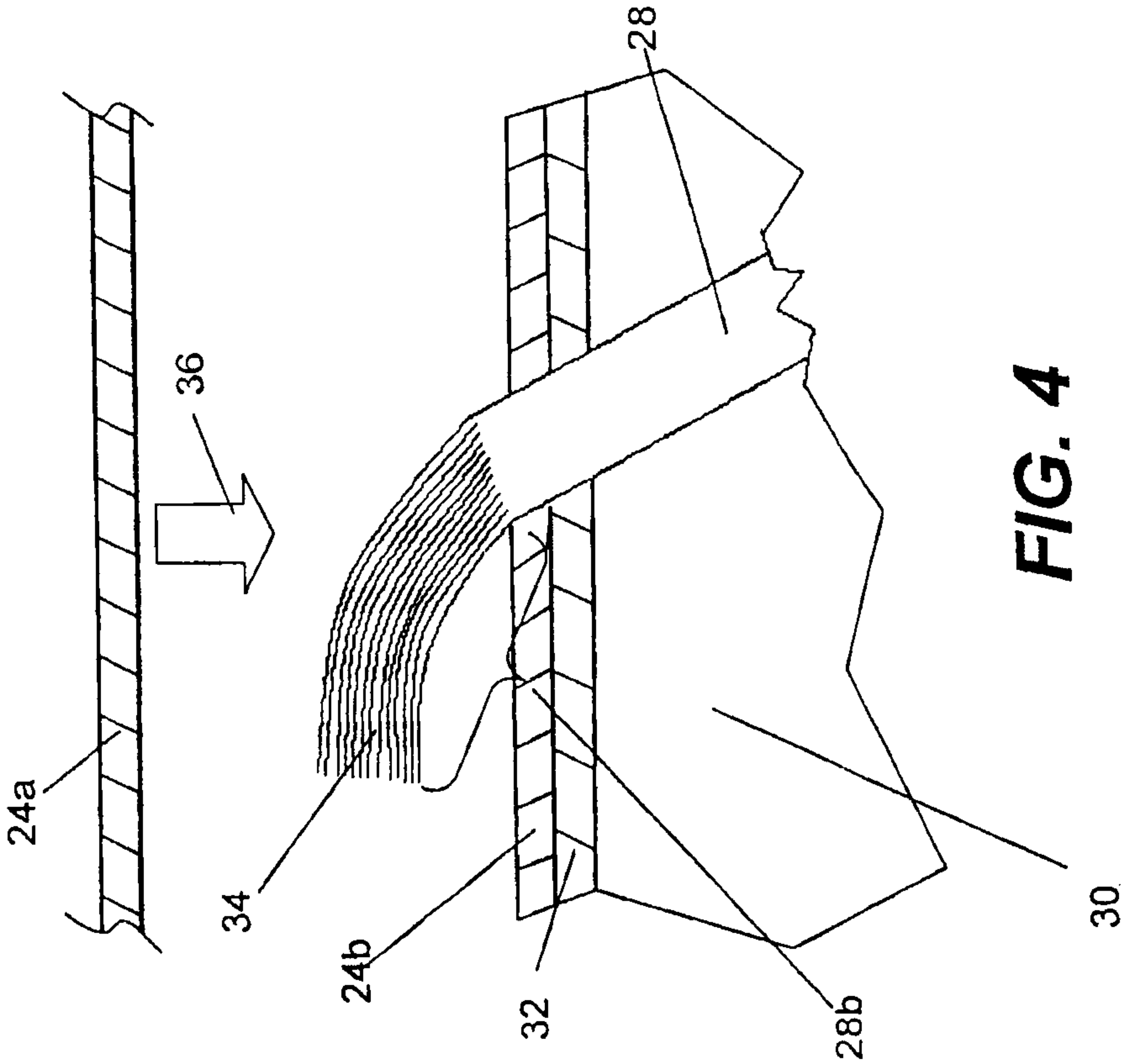
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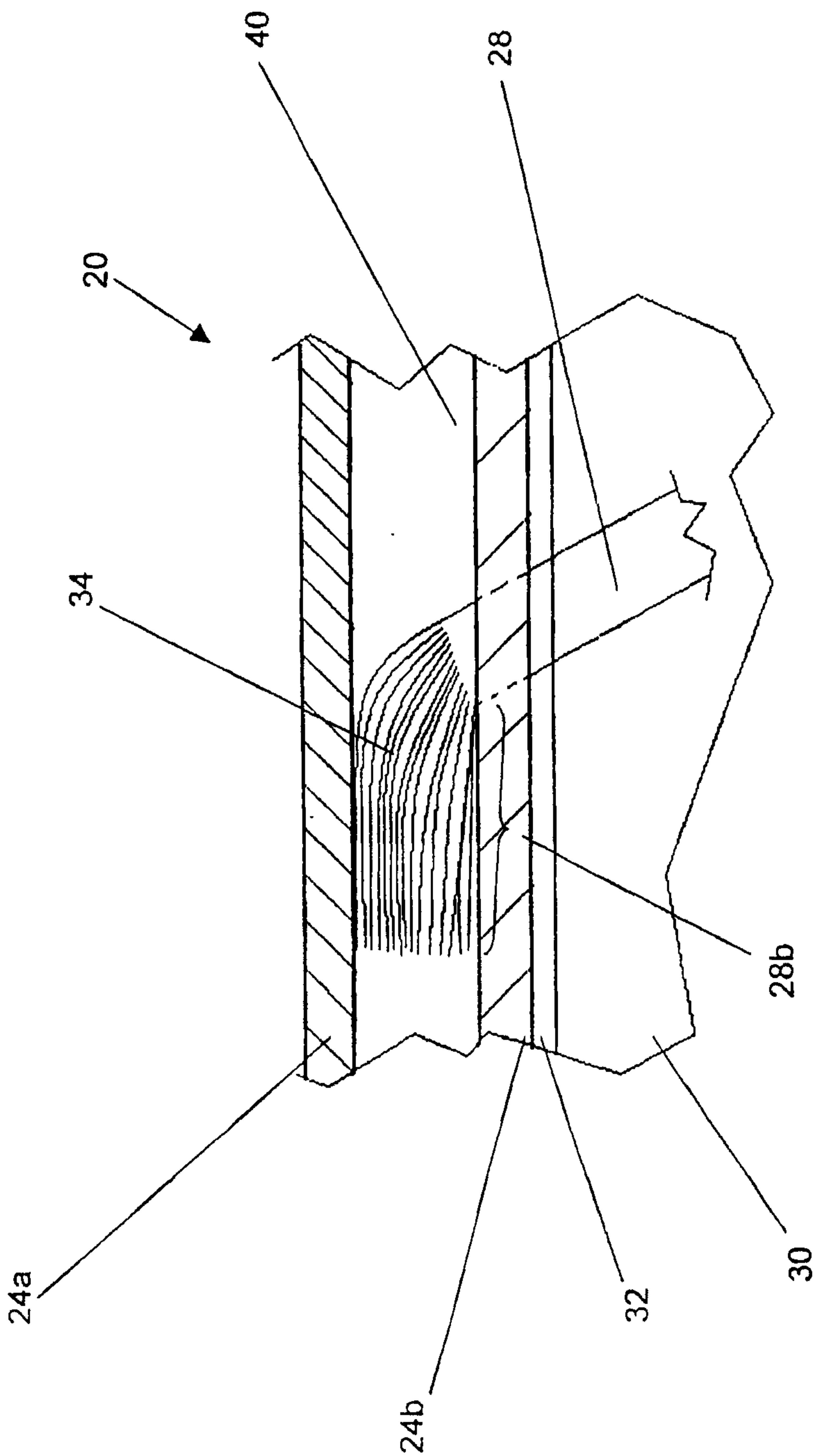
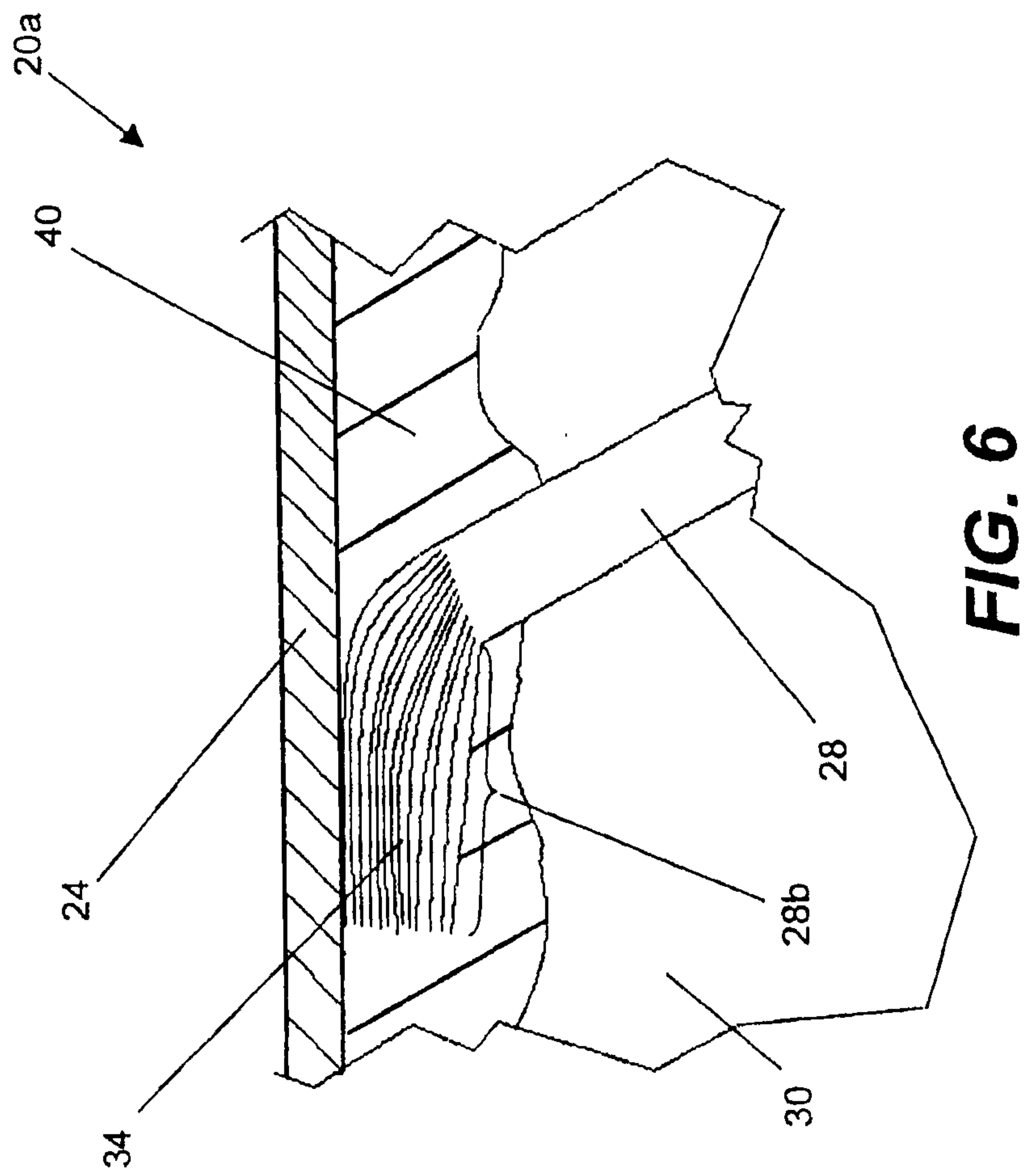


FIG. 5



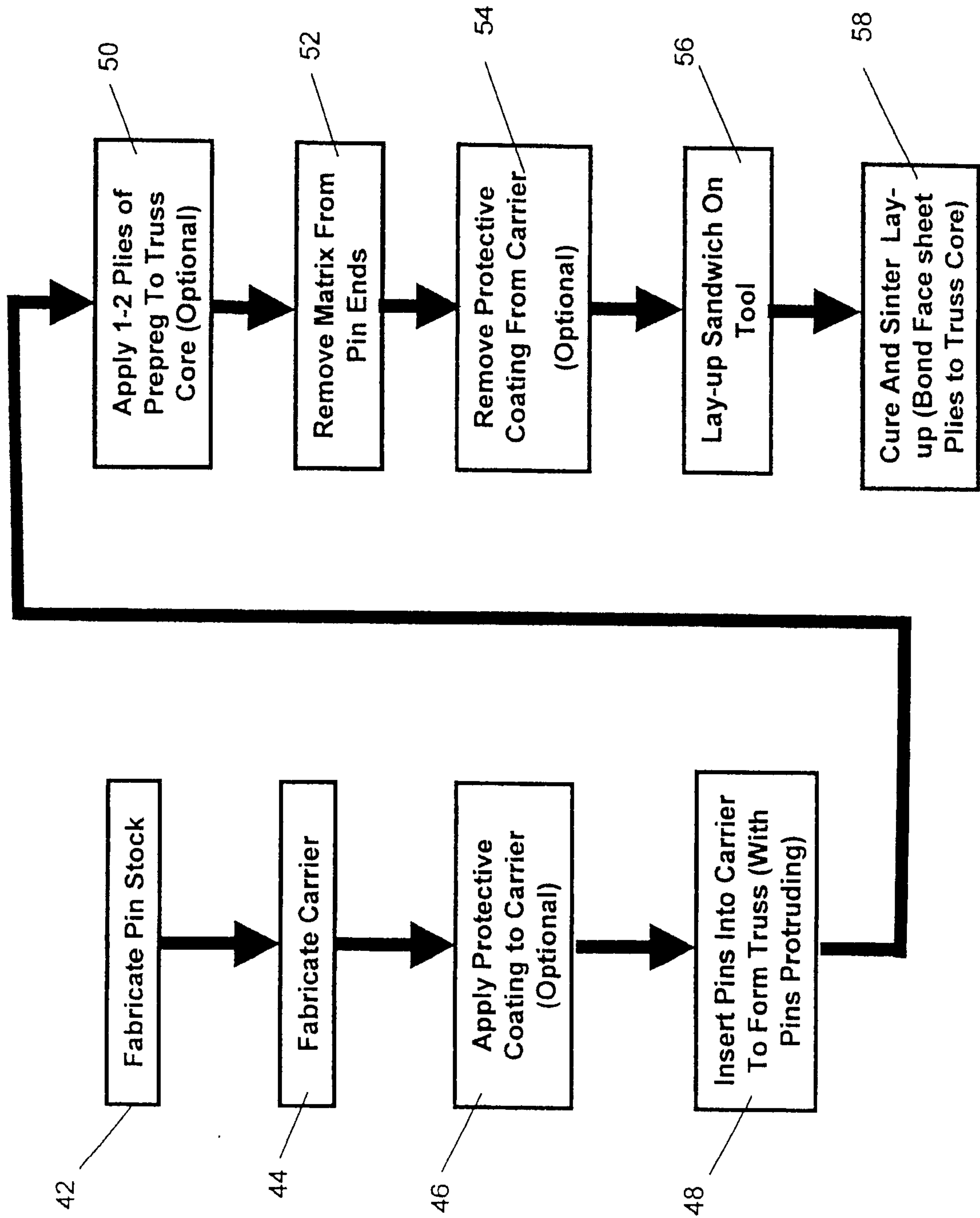


FIG. 7

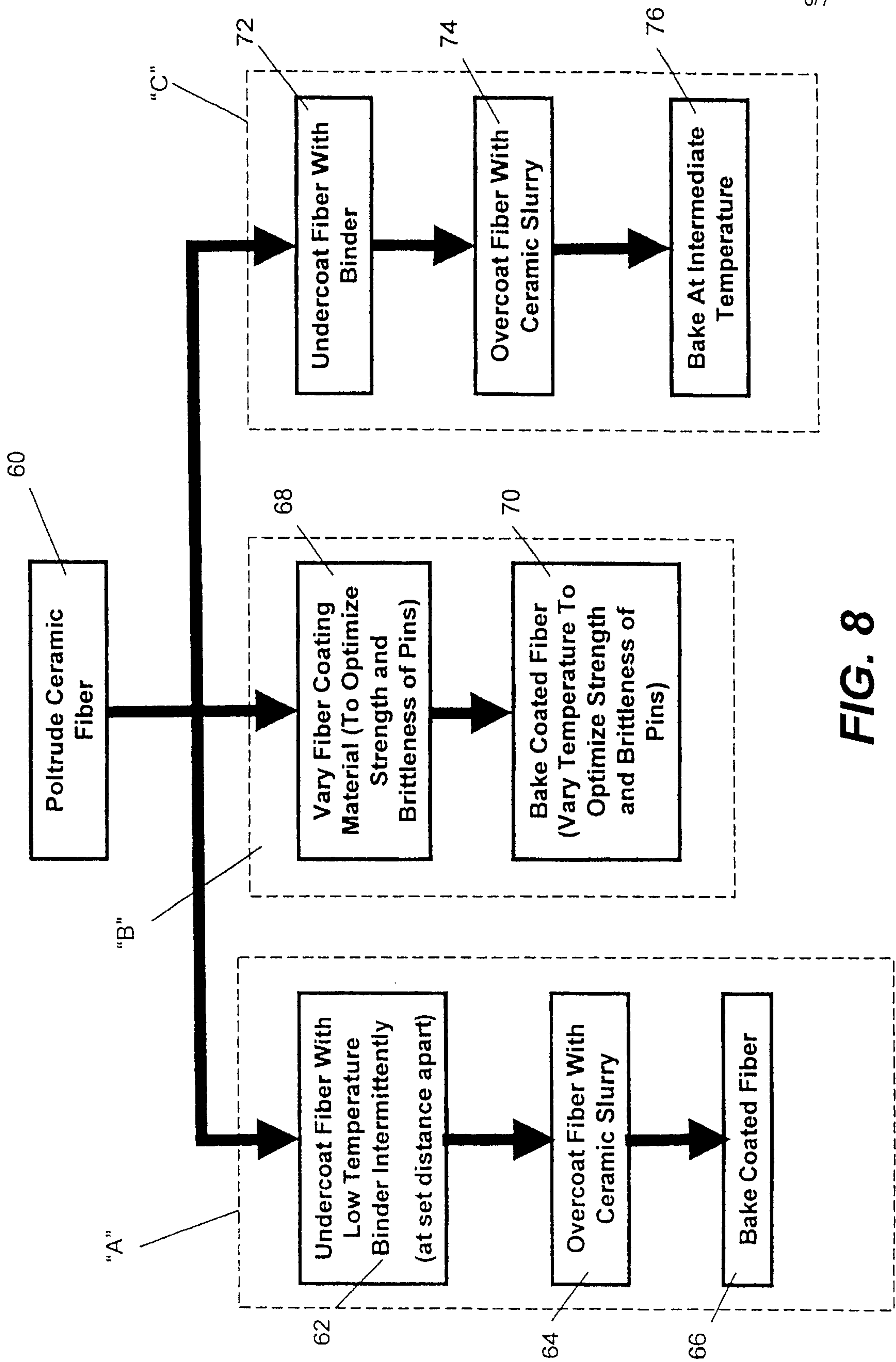


FIG. 8

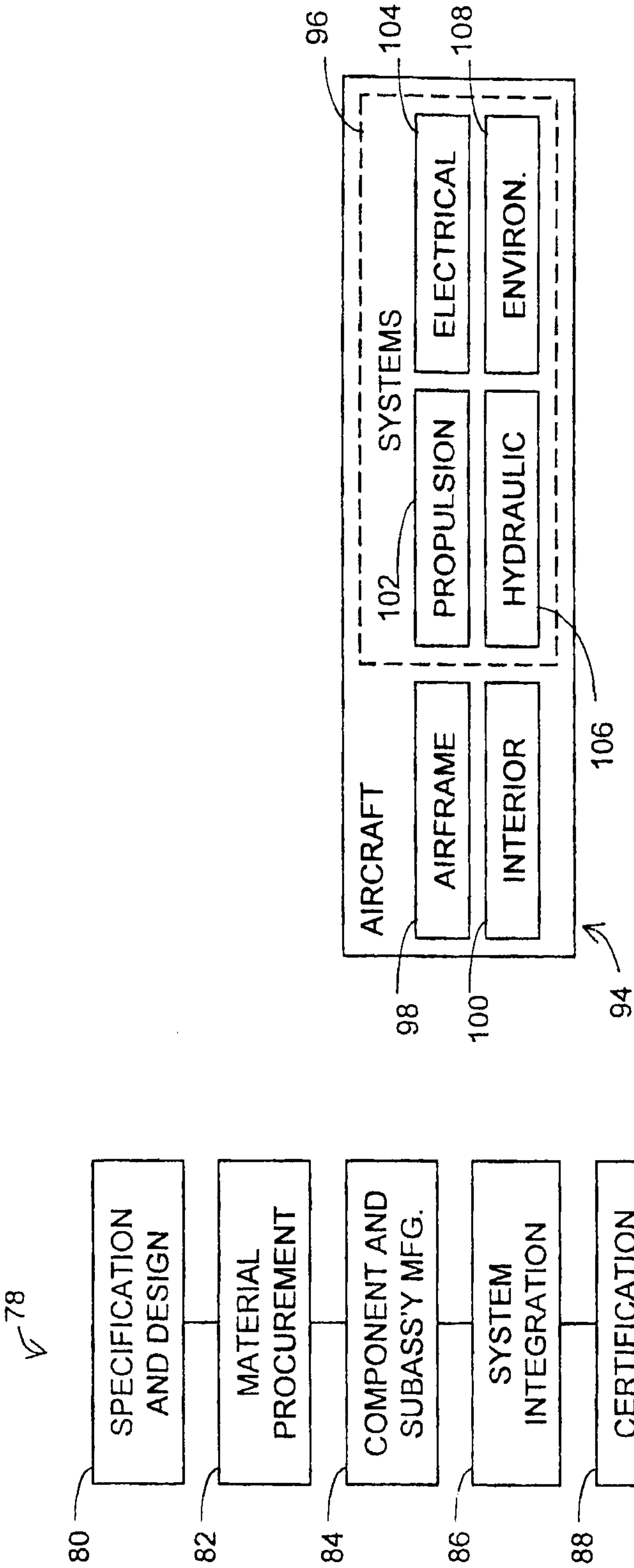


Figure 9

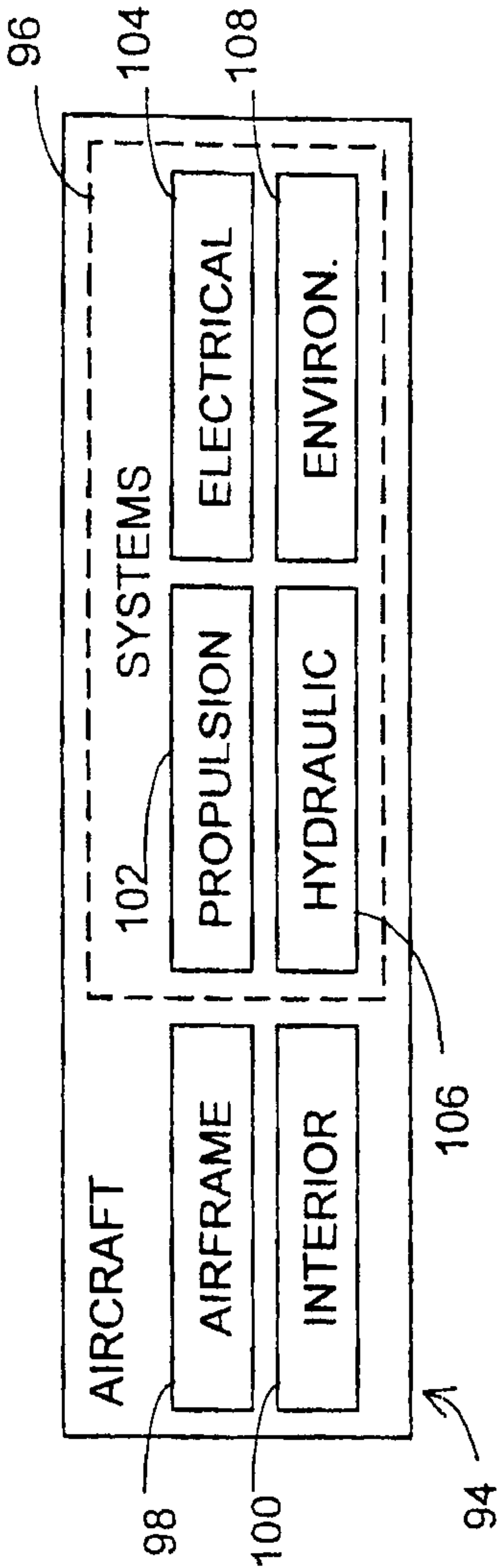


Figure 10