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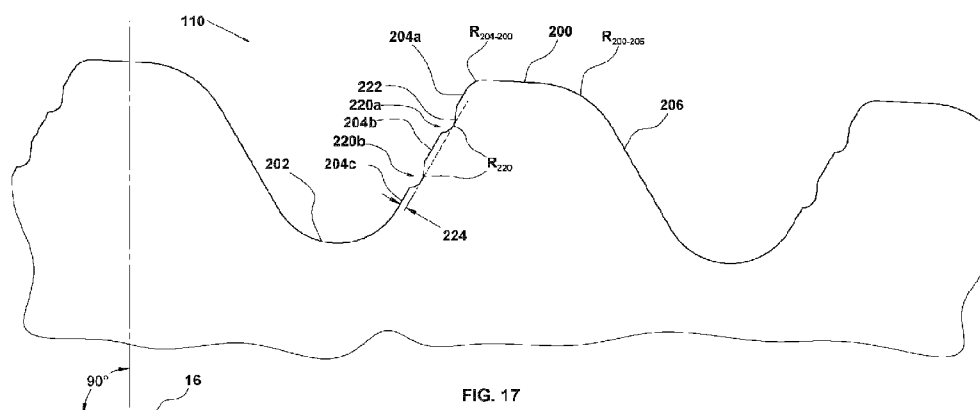


FIG. 17

(57) Abstract: A tubular member having a first connector provided on a first end thereof, this first connector being adapted to receive a corresponding connector provided on another tubular member, forming a tubular connection comprising: a pin connector, a box connector, an outer diameter, an inner diameter, and a longitudinal axis. The pin connector threads or box connector threads feature a threadform having at least one load flank reduction zone such that when the pin connector is threadably engaged with the box connector, the resulting tubular connection radial bearing strength is desirably reduced. More specifically in the preferred embodiment, the at least one load flank reduction zone is preferably configured such that the tubular connection radial bearing strength is between 100% to 110% of the cross sectional connection strength when the box connector is threadably engaged with a pin connector. A method for forming connectors on a tubular member comprising threads which have at least one load flank reduction zone described herein is also provided.

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HIGH TORQUE CONNECTION WITH ENHANCED BREAK IN PERFORMANCE

CROSS REFERENCE TO PRIOR APPLICATIONS

[0001] The present application claims priority under the Paris Convention to U.S. Application No. 63/264,001, filed on November 12, 2021. The entire contents of such prior application are incorporated herein by reference as if set forth herein.

FIELD OF THE DISCLOSURE

[0002] The present application relates generally to tubular members having threaded connections. More specifically this application relates to tubular members having high strength double shoulder threaded connections utilized in downhole drilling operations such as drill pipe, drill collars, tool joints and downhole tools.

BACKGROUND

[0003] This section provides background information to facilitate a better understanding of the various aspects of the invention. It should be understood that the statements in this section of this document are to be read in this light, and not as admissions of prior art.

[0004] In oil and gas drilling a drill bit is threadably attached to the end of a drill string comprised of a variety of sub-assemblies and tubular members. The drill bit is traditionally attached to the Bottom Hole Assembly (BHA) at the bottom of the drill string which may include a variety of downhole tools and tubulars such as a rotary steerable tool, a mud motor, Measurement-While-Drilling (MWD) tools, Logging-While-Drilling (LWD) tools, a configuration of stabilizers, reamers, jars, shocks, agitators, and multiple drill collars among other modern drilling technologies. Connected to the BHA is a configuration of other tubular members typically including a plurality of Heavy Weight Drill Pipe (HWDP) and drill pipe which couple the drill bit and BHA back to the surface completing the drill string and affording for surface rotation, torque, compression, and tension to be applied to the drill string and thus the drill bit in efforts to further advance the borehole. Further, the assembled drill string also functions as a conduit for pumping drilling fluid through the sufficiently hollow inside diameter to clean the borehole, provide hydraulic power to downhole tools and cool the heat generated by the drill bit and downhole friction. It is common that all of these drill string tubular members are threadably attached to one another by tubular connections such that as the borehole is advanced further the drill string can be sequentially assembled or

1 disassembled through the threading or unthreading of tubular members at surface. The most
2 common tubular connections for use in a drill string are rotary shouldered connections, with
3 most modern variants introducing a secondary torque bearing shoulder on the nose of the
4 pin connector which contacts the rear of the box connector when the pin connector is
5 threadably engaged with the box connector.

6 **[0005]** During drilling operations, it is desirable that all of the aforementioned tubular
7 connections between adjacent drill string tubular members possess sufficient mechanical
8 and metallurgical capabilities to withstand the loads placed on them during drilling operations
9 (e.g., torsional, tensile, compressive loads, and so forth). Generally, the mechanical behavior
10 of standard materials utilized in constructing tubular connectors (for example steel,
11 aluminum, titanium) reflects the relationship between the material's deformation response to
12 externally applied loads and forces. It will be appreciated that the stress-strain behavior of
13 materials, in particular the metals used in constructing tubular members, are a large
14 influence on the performance of a tubular connection. Further, as it will be appreciated by
15 those skilled in the art it is desirable to exploit stress-strain characteristics of both the macro
16 and microscopic behavior of a material's deformation mechanisms to strengthen and
17 improve designs, including tubular connections. In this way, the mechanical behavior of the
18 tubular connection under high loads may be enhanced to become desirably stronger and
19 more predictable, while mitigating undesirable deformation, damage and fracture.

20 **[0006]** Without being limited to this or any other technique or theory, as it will be appreciated
21 the mechanical behavior of a given material may be ascertained by a stress-strain test. In
22 this way, stress may be defined through the relationship of a load applied perpendicular to a
23 known test specimen cross section, and strain may be defined as the ratio of the change in
24 length of said test specimen with reference to the original length of the specimen. Broadly
25 speaking elastic deformation is a nonpermanent deformation where when an applied load is
26 removed the loaded specimen returns to its original size and shape, and plastic deformation
27 is a permanent deformation where when an applied load is removed the loaded specimen
28 does not return to its original size and shape. More specifically, macroscopic elastic
29 deformation is an indication of small changes in interatomic spacing and the stretching of
30 interatomic bonds, while plastic deformation indicates the breaking of interatomic bonds and
31 the forming of new interatomic bonds where large numbers of atoms or molecules
32 permanently move relative to one another.

1 **[0007]** Further, it is known in the art that crystalline materials such as metals do not possess
2 perfect order on an atomic scale, but instead contain large numbers of various imperfections
3 and deviations from crystalline perfection. Particularly, many of the metallurgical and
4 mechanical properties of materials are profoundly sensitive to deviations from the perfectly
5 ordered crystalline structure. The influence of these defects is not always adverse, and often
6 specific mechanical characteristics are tailored and fashioned by the deliberate introduction
7 of controlled amounts of desirable imperfections. More particularly as discussed above,
8 plastic deformation is a permanent change to a material, and on a microscopic scale
9 corresponds to the net movement of large numbers of atoms in response to applied stress.
10 During this process, interatomic bonds must be ruptured and then reformed around a
11 dislocation; a linear defect around which some of the atoms are misaligned. Macroscopically,
12 plastic deformation corresponds to the motion of large numbers of dislocations and the
13 overall capability of a metal to plastically deform depends on the ability of dislocations to
14 move.

15 **[0008]** One important source of these new dislocations is existing dislocations which multiply
16 under load, a property known as dislocation density. More specifically, grain boundaries as
17 well as internal defects and surface irregularities such as scratches and nicks may serve as
18 dislocation formation sites where the more unconstrained the dislocation motion, the greater
19 is the facility with which a metal may deform, and the weaker it behaves. Conversely, as
20 strength is related to the ease with which plastic deformation can be made to occur, by
21 deliberately inducing plastic deformation by means of applied compressive force, one
22 constrains and reduces the mobility of dislocations, and in this way the mechanical strength
23 of the material may be enhanced. Put more simply, greater mechanical forces will be
24 required to initiate further plastic deformation, thus the material performance is increased.
25 Generally, this is known in the art as strain hardening, work hardening, or cold working
26 whereby a metal becomes stronger as it is plastically deformed.

27 **[0009]** It will be appreciated that for the materials discussed herein the elastic behavior of a
28 material manifests as a generally proportional relationship between stress and strain, this
29 linear relationship known as Hooke's Law corresponds to the material property known as
30 Young's Modulus. Due to the permanent changes in geometry, and by extension permanent
31 changes to the mechanical performance of a material, it is desirable to ascertain the stress
32 level at which plastic deformation begins. As it is known in the art this property is known as

1 the yield strength of the material, shown as σ_y in FIG. 1 and the overall magnitude of the
2 yield strength for a metal is an indicator of its resistance to plastic deformation. More
3 specifically, without being limited to this theory or any other, it will be appreciated in studying
4 the example engineering stress strain curve in FIG. 1 that a convention has been
5 established wherein a straight line is constructed parallel to the linear elastic portion of the
6 engineering stress-strain curve at some specified strain offset, usually 0.002 (0.2%), wherein
7 the stress corresponding to the intersection of this straight line and the engineering stress-
8 strain curve is commonly defined as the yield strength of the material. It will be understood
9 that this intersection occurs after a small amount of non-linearity occurs within the graph,
10 indicating a very small degree of plastic deformation has occurred. The slope of this line
11 corresponds to Young's Modulus whose magnitude is a measure of the resistance to
12 separation of interatomic bonding forces, indicated as E in FIG. 1.

13 **[0010]** It will be appreciated that should a load be applied to a material to induce stress
14 levels exceeding the yield strength, combined elastic and plastic deformations will occur
15 simultaneously. Upon releasing the applied load, a fraction of the total deformation will be
16 recovered as elastic strain, with the remainder of the deformation being permanent plastic
17 deformation. As shown in FIG. 2, during the unloading cycle the stress-strain curve follows a
18 near straight-line path from the point of unloading, with the slope of the unloading curve
19 being parallel to the initial elastic portion of the curve, and thus virtually identical to Young's
20 Modulus. The magnitude of this elastic strain which is regained during unloading
21 corresponds to strain recovery. If the load is reapplied, the curve will traverse the same
22 linear portion in the direction opposite to the unloading, thus the material, and by extension
23 the mechanical performance of a design, can behave in an elastic fashion despite having a
24 degree of plastic strain induced previously. It will be understood that under this condition a
25 new effective yield strength exists for a material that has residual plastic strain as illustrated
26 in FIG. 2. In this way, it becomes possible to desirably induce plastic strain into a material to
27 enhance the mechanical performance and strength of a design.

28 **[0011]** A known practice of utilizing strain hardening to enhance a tubular connector is
29 through the cold rolling of threads, however this technique does not impart stress on thread
30 flanks. Instead, cold rolling creates residual compressive stress in the thread root in efforts to
31 reduce fatigue cracking of the connector. Shot peening may also be performed on pin and
32 box connectors to impart cold work onto thread flanks and seal surfaces, however this is

1 typically reserved for materials which are not desirably coated with anti-friction coatings (for
2 example non-magnetic steel) as shot peening generally increases costs per-connector
3 without providing a high degree of strain hardening as the size of the shot peening bead,
4 and thus overall intensity of the peening, are limited to the smallest features of the thread
5 form such as the thread root radius.

6 **[0012]** A common form of damage to thread form flanks is observed as a 'tearing' or 'cold
7 welding' of the thread flank material during threading or unthreading of the tubular
8 connection. This type of damage is known in the art as "galling" and, without being limited to
9 this or any other theory, is understood to be the result of high static or dynamic contact
10 stresses between predominantly tensile stress state materials. A common example would be
11 two newly manufactured box and pin connectors being threadably made up and torqued
12 together. The freshly machined surface of the thread form load flanks may be in a
13 predominantly tensile stress state due to the shearing nature of the cutting tools used in
14 manufacturing the connector thread, and thus the high stress state of the contacting load
15 flanks of the connection may induce galling between these surfaces, resulting in damage
16 requiring repair or replacement.

17 **[0013]** In efforts to prevent this damage, several technologies and methods have been
18 developed and employed. The most common technology is the surface coating of pin and
19 box connector threads which can take many forms including phosphate, copper, or spray
20 coatings among others and are moderately effective at providing an additional resistance to
21 galling and are generally highly desirable. However, coatings do not offer any strain
22 hardening thus do not alter the stress state of thread flanks. Instead, most coatings serve
23 only to reduce friction within the threads for a time as they are known to wear off through
24 multiple makeup and break out cycles of the tubular connection. Thus, it will be appreciated
25 that it would be desirable to impart strain hardening to thread flanks as this would be a
26 permanent preventative measure against damage.

27 **[0014]** Therefore, in efforts to strain harden thread flanks, one technique is the practice of
28 "Make and Break" where newly manufactured or repaired tubular connectors are subjected
29 to multiple makeup torque cycles prior to being put into operation. As a single makeup cycle
30 is known in the art to induce little if any cold work on the load flanks of a connector, it is
31 typical that 3 to 5 cycles are performed with the goal of creating a desirable stress state

1 within the thread load flanks where thread flank damage may be mitigated or eliminated
2 entirely.

3 **[0015]** Make and Break is convenient for threaded connectors on newly manufactured drill
4 pipe as typically the tool joints are not yet welded to the tube body and are thus easily
5 handled and threadably connected. However, in the case of repaired or remanufactured
6 tubular members it is often not feasible to perform Make and Break operations in a controlled
7 environment as most manufacturing facilities do not have the required equipment nor the
8 handling capability to threadably connect and torque full length tubular members. This
9 necessitates engaging costly third-party services to have Make and Break performed, for
10 example Make and Break service can often increase the price of manufacturing or repairing
11 a single rotary shouldered connector by as much as 100% or more. Alternatively, Make and
12 Break may be performed on a drilling rig during drilling operations while assembling the drill
13 string. This is highly undesirable as it consumes drilling rig time which can be orders of
14 magnitude more expensive than shop time, and further delays drilling operations as each
15 new connector is made up and broken apart multiple times.

16 **[0016]** Due to the time and costs associated with the practice, Make and Break is therefore
17 often not performed at all for newly manufactured connectors, even in cases where high
18 quantities of tubular members have been machined, for example a drill string tubular
19 connection conversion. In this way, each new connector in the drill string is highly
20 susceptible to damage when put into operation.

21 **[0017]** Additionally, the makeup torque of a tubular connection is known in the art to be
22 calculated predominately utilizing cross sectional area properties of the connection. These
23 cross sectional properties, and thus the calculated makeup torque, are greatly influenced by
24 the outside and inside diameters of the tubular connectors comprising the tubular connection
25 and can vary greatly even for a fixed thread geometry. For example, a DS40 connection
26 having an outside diameter of 5.250 inches and an inside diameter of 2.688 inches would
27 have a lower makeup torque than a DS40 connection having an outside diameter of 5.250
28 inches and an inside diameter of 2.437 inches due to the difference in cross sectional
29 strength, however the radial bearing strength of the tubular connection calculated based on
30 thread flank properties would remain identical. In this way the amount of force, and by
31 extension strain hardening, imparted on the thread load flanks during Make and Break may

1 not be consistent for a given tubular connection where cross sectional properties are utilized
2 to compute the makeup torque.

3 **[0018]** Further, for the majority of tubular connections the ratio of radial bearing strength to
4 cross sectional strength is disproportionately high, even climbing higher than 2.0 in some
5 cases, indicating that even for a fixed outside diameter and inside diameter the forces
6 applied to the thread load flanks during Make and Break are governed by the cross sectional
7 properties of the connection. In this way, the forces on the thread load flanks during tubular
8 connection makeup may be too low to induce any appreciable cold work thus strain
9 hardening of thread load flanks may not occur at all.

10 **[0019]** Historically the goals in developing a new tubular connection design was to maximize
11 the calculated torque carrying capability of a given connection outside diameter and inside
12 diameter. For example, US5908212, US7210710, and US9816646 disclose various tubular
13 connection designs which aim to increase the torsional capability and handling
14 characteristics of tubular connections, however these inventions do not reveal any methods
15 for inducing desirable compressive stress in the thread load flanks.

16 **[0020]** As disclosed in US5492375 it is preferred to have the pin nose or box counterbore of
17 the tubular connector yield prior to the thread shearing and teaches a method by which the
18 length of a connection thread zone may be established. However, patent '375 does not
19 make any assertion of the behavior of thread load flank bearing stresses and correlates the
20 length of the tubular connection thread with the various cross sectional areas with the goal of
21 achieving an optimal configuration where the threads are close to, but do not exceed their
22 shear strength under high torque loads. In this way, any alteration to the outside diameter
23 and inside diameter of a tubular connection design necessitates a thread length revision
24 which produces the undesirable side effect that the revised connection may no longer
25 remain compatible with all prior variants. Additionally, should the case of increased thread
26 length be required under patent '375's teachings to ensure thread shear is of little concern,
27 the tubular connection's radial bearing strength may increase due to increased load flank
28 area. This action would result in proportionally reducing force, and by extension strain
29 hardening, imparted on the thread load flanks during Make and Break or usage of the
30 connection.

1 **[0021]** A balanced thread form is disclosed in US10041307 which reveals thread forms that
2 aim to optimize the radial load flank bearing strength with the thread form shear strength,
3 however downhole failure of modern tubular connections due to thread shear is uncommon
4 particularly with double shouldered connections. High load cases downhole are typically
5 caused by high torsional loads which result in cross sectional yield failures such as swelling
6 of the primary and/or secondary shoulders, or the stretching of pin and/or box connectors.
7 Further in the case of purely tensile drill string loads, much like a simple threaded fastener,
8 the makeup torque of a rotary shouldered connection preloads the primary shoulder with
9 compressive force which must be overcome to apply direct shear loads on the thread form.
10 In many cases the drill string itself, in particular drill pipe tube bodies, possess less tensile
11 force capacity than could be applied to the tubular connection to separate the primary
12 shoulder let alone cause catastrophic shearing of the entire plurality of threads. Further, the
13 radial load flank bearing strength loads and stresses are not correlated to the cross sectional
14 area stresses nor by extension the makeup or drilling torque in the design of the thread form.
15 In this way, the present invention could be effectively applied to the style of connection
16 disclosed in '307 to further enhance its performance while maintaining compatibility.

17 **BRIEF SUMMARY**

18 **[0022]** There is provided a tubular member having a first end having a first threaded
19 connector and a second end having a second threaded connector, the first and second
20 connectors being configured to form a tubular connection with adjacent tubular members. In
21 the preferred embodiment the tubular connection is formed from the first connector being a
22 box connector and the second connector being a pin connection, though it will be
23 understood that other configurations of threaded connectors are possible without deviating
24 from the scope of the invention described herein. Further, the tubular connection between
25 tubular members includes an outer diameter, an inner throughbore diameter, a nominal pitch
26 diameter, and a longitudinal axis. In an embodiment, the tapered pin connector includes a
27 primary shoulder and a secondary shoulder configured to engage the tapered box connector
28 primary shoulder and secondary shoulder. In addition, between the primary and secondary
29 shoulders, the pin and box connectors include a zone of external and internal threads
30 respectively. The threaded zones comprise a plurality of threads which taper relative to the
31 longitudinal axis. Further, the plurality of threads includes a thread crest, a thread root, at
32 least one load flank extending along a line from the thread root to the crest, a stabbing flank

1 extending along a line from the thread root to the crest, and at least one load flank reduction
2 zone. The load flank of the pin connector is more proximate the primary shoulder, whereas
3 the box load flank is more proximate the secondary shoulder. The stabbing flank of the pin
4 connector is more proximate the secondary shoulder, whereas the box stabbing flank is
5 more proximate the primary shoulder. When the pin connector is threadably engaged with
6 the box connector each of the at least one load flanks on the pin connector contacts the at
7 least one load flanks of the corresponding thread on the box connector along a projected
8 radial direction such that at least one projected load flank radial contact face H_r measured in
9 inches is formed by the mating load flanks. Along the length of the zone of threads, this load
10 flank radial contact face corresponds to a radial bearing strength S_{rb} for the plurality of
11 threads representing the amount of force required to induce plastic deformation into the load
12 flanks, this deformation resulting in a layer of permanent compressive stress material within
13 the thread on load flanks. The connection has a cross sectional connection strength S_{cs}
14 based on the geometry of the primary shoulders, secondary shoulders, nominal pitch
15 diameter, and plurality of threads representing the amount of force required to induce plastic
16 deformation (or "yielding") in the weakest cross sectional areas of the connection, resulting
17 in permanent stretching, necking, belling, swelling, or compression of the connection cross
18 sectional geometry. More specifically in one embodiment, the at least one load flank
19 reduction zone is preferably configured such that the radial bearing strength is between
20 100% to 110% of the cross sectional connection strength. In this way, when the tubular
21 connection is threadably made up and torqued to the desired magnitude, the load flank of
22 the plurality of threads will experience approximately the same levels of stress as the tubular
23 connection cross section, enhancing the load flanks with increased cold work and residual
24 compressive stress thus greatly improving galling resistance, while also ensuring that the
25 bearing strength is always equal to or stronger than the cross sectional connection strength
26 thus preventing excessive plastic deformation to the threadform.

27 **[0023]** As known in the art, the torsional strength and makeup torque of the tubular
28 connection are determined by the connection cross sectional strength, thus by ensuring the
29 radial bearing strength is equal to, or marginally greater than the connection cross sectional
30 connection strength, the plurality of threads are protected from failure due to be being
31 overstressed. Further, should the at least one load flank reduction zone be configured
32 appropriately as in the preferred embodiments discussed herein the shear strength of the

1 tubular connection remains maximized thus eliminating concerns of catastrophic failure due
2 to thread shear failure.

3 **[0024]** In a preferred embodiment the load flank reduction zone includes a limiting flank
4 inset parallel from the load flank, a first radius extending between the thread crest and the
5 limiting flank having a first radius of curvature, a second radius extending from the limiting
6 flank to the load flank having a second radius of curvature. Further, the first radius has a first
7 convex radius of curvature, and the second radius has a second concave radius of
8 curvature. In this way, when the pin connector is threadably engaged with the box connector
9 each of load flanks on the pin connector contacts the load flanks of the corresponding thread
10 on the box connector along a projected radial direction such that at least one projected load
11 flank radial contact face H_r is formed by the mating load flanks and is equal to approximately
12 0.070 inches.

13 **[0025]** In an alternative embodiment the load flank reduction zone includes a limiting flank
14 inset parallel from the load flank, a first radius extending between the thread root and the
15 limiting flank having a first radius of curvature, a second radius extending from the limiting
16 flank to the load flank having a second radius of curvature. Further, the first radius has a first
17 convex radius of curvature, and the second radius has a second concave radius of
18 curvature. In this way, when the pin connector is threadably engaged with the box connector
19 each of load flanks on the pin connector contacts the load flanks of the corresponding thread
20 on the box connector along a projected radial direction such that at least one projected load
21 flank radial contact face H_r is formed by the mating load flanks and is equal to approximately
22 0.070 inches.

23 **[0026]** There is also provided a method for forming a tubular connector on a tubular member
24 for threadably connecting a tapered pin connector with a tapered box connector, the tubular
25 connection having an outer diameter, an inner throughbore diameter, a nominal pitch
26 diameter, and a longitudinal axis. In an embodiment, the method includes (a) forming a box
27 connector on the end of a first tubular member, the box connector comprising an outside
28 diameter, an inner throughbore diameter, a box primary shoulder, a box secondary shoulder,
29 and a zone of internal threads having a nominal pitch diameter wherein when the box
30 connector is threadably engaged with a pin connector the primary shoulders, secondary
31 shoulders, nominal pitch diameters, and plurality of threads form a cross sectional

1 connection strength S_{cs} . In addition, the method includes (b) forming a plurality of threads in
2 the region between the box primary shoulder and the box secondary shoulder, the plurality
3 of threads comprising a thread crest, thread root, a load flank, and a stabbing flank, wherein
4 when the box connector is threadably engaged with a pin connector each of the plurality of
5 threads on the box connector contacts a corresponding thread on the pin connector along a
6 projected radial direction such that a projected load flank radial contact face H_r' measured in
7 inches is formed by the mating load flanks. Further, the method includes (c) forming at least
8 one load flank reduction zone on the load flanks of the plurality of box connector threads
9 wherein when the box connector is threadably engaged with a pin connector, the at least
10 one load flank reduction zone reduces the projected load flank radial contact face H_r' and
11 forms at least one reduced projected load flank radial contact face H_r . More specifically in
12 one embodiment, the at least one load flank reduction zone is preferably configured such
13 that the radial bearing strength is between 100% to 110% of the cross sectional connection
14 strength when the box connector is threadably engaged with a pin connector.

15 BRIEF DESCRIPTION OF THE DRAWINGS

16 **[0027]** These and other features will become more apparent from the following description in
17 which references are made to the following drawings, in which numerical references denote
18 like parts. The drawings are for the purpose of illustration only, are not necessarily to scale,
19 and are not intended to in any way limit the scope of the invention to the particular
20 embodiments shown. In the interest of clarity and brevity, certain aspects discussed herein
21 may be illustrated in an exaggerated scale or in a simplified schematic form having some
22 details of conventional elements omitted.

23 **[0028]** FIG. 1 is an example of an engineering stress-strain curve.

24 **[0029]** FIG. 2 is an example of an engineering stress-strain curve showing a loading and
25 unloading curve.

26 **[0030]** FIG. 3 is a perspective view of an embodiment of a tubular member having tubular
27 connectors.

28 **[0031]** FIG. 4 is a perspective view in partial section of a tubular member having tubular
29 connectors.

- 1 **[0032]** FIG. 5 is a side view in quarter section of a threaded pin connector.
- 2 **[0033]** FIG. 6 is a side view in section of a threaded box connector.
- 3 **[0034]** FIG. 7 is a perspective view in partial section of a tubular connection without being
4 threadably engaged.
- 5 **[0035]** FIG. 8 is a side view section of a tubular connection having been threadably
6 engaged.
- 7 **[0036]** FIG. 9 is an enlarged cross section view of a portion of a prior art pin connector.
- 8 **[0037]** FIG. 10 is an enlarged cross section view of a portion of a prior art connector having
9 been threadably engaged.
- 10 **[0038]** FIG. 11 is an enlarged cross section view of a portion of a pin connector having a
11 preferred embodiment of a load flank reduction zone.
- 12 **[0039]** FIG. 12 is an enlarged cross section view of a portion of a tubular connection formed
13 by pin connectors and box connectors both having a preferred embodiment of a load flank
14 reduction zone.
- 15 **[0040]** FIG. 13 is a sequence of images depicting an enlarged cross section view of a
16 portion of a pin connector having a preferred embodiment of a load flank reduction zone
17 before during and after an external load is applied, with exaggerated imagery of atomic
18 interactions.
- 19 **[0041]** FIG. 14 is an enlarged cross section view of a portion of a pin connector having an
20 alternative embodiment of a load flank reduction zone formed near the thread root.
- 21 **[0042]** FIG. 15 is an enlarged cross section view of a portion of a pin connector having an
22 alternative embodiment of a load flank reduction zone groove.
- 23 **[0043]** FIG. 16 is an enlarged cross section view of a portion of a tubular connection formed
24 by pin and box connectors both having an alternative embodiment of a load flank reduction
25 zone.

1 [0044] FIG. 17 is an enlarged cross section view of a portion of a pin connector having an
2 alternative embodiment of two load flank reduction zone grooves.

3 [0045] FIG. 18 is an enlarged cross section view of a portion of a pin connector having an
4 alternative embodiment of a plurality of load flank reduction zone grooves.

5 [0046] FIG. 19 is a block diagram for a method for manufacturing a tubular connector in
6 accordance with the principles and embodiments discussed herein.

7 DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

8 [0047] The units of measurement and methods of describing thread load flank interactions
9 as used herein are not meant to limit the scope of the invention and should be interpreted in
10 the broadest sense possible. The terms “pin connector” and “box connector” should be
11 interpreted equivalent to “male connector” and “female connector”, respectively, as these
12 terms are known in the art. Thus, a pin or male connector comprises a zone at one end of a
13 tubular member having a threaded external surface. Similarly, a box or female connection
14 end comprises a zone at one end of a tubular member having a threaded internal surface.

15 [0048] Referring to FIG. 3 and FIG. 4 a tubular member **10** is shown having a top end **12**
16 and a bottom end **14** and a longitudinal axis **16**. Threaded connectors are disposed at each
17 end to permit the connection of the tubular member **10** to an additional axially adjacent
18 tubular member. For example, as illustrated the tubular member **10** has a box connector **152**
19 disposed at the top end **12** and a pin connector **102** disposed at the bottom end **14** such that
20 further tubular members **10** may be threadably connected, forming the tubular connection
21 **100** shown later in FIG. 8. This may be performed in succession to assemble a drill string;
22 however, it should be appreciated that tubular member **10** may have any combination of box
23 connector **152** or pin connector **102** at either or both of the top end **12** or bottom end **14**
24 without deviating from the scope of the invention described herein. Further details of the
25 tubular connection **100** and the pin connector **102** and the box connector **152** are presented
26 below.

27 [0049] Referring now to FIG. 5, a side view of pin connector **102** is shown in quarter section.
28 The pin connector **102** has an outside diameter **120** and a throughbore inside diameter **122**
29 and consists of a primary shoulder **104** and a secondary shoulder **106** with a zone of
30 external threads **108** between the two shoulders wherein the zone of external threads

consists of a plurality of fully formed threads **110**. Further details of the fully formed threads **110** are presented below. The pin connector **102** has a cross sectional area **130** substantially determined by the pin connector thread **110** and nominal pitch diameter **54** and the inside diameter **122**. Additionally, the pin connector **102** has a nose cross sectional area **132** formed by the pin nose outer diameter **124** and inside diameter **122**.

[0050] Referring now to FIG. 6, a side view of box connector **152** is shown in full cross section. The box connector **152** has an outside diameter **170** and a throughbore inside diameter **172** and consists of a primary shoulder **154** and a secondary shoulder **156** with a zone of internal threads **158** between the two shoulders wherein the zone of internal threads consists of a plurality of fully formed threads **160**. Further details of the fully formed threads **160** are presented below. The box connector **152** has a cross sectional counterbore area **180** formed by the outside diameter **170** and counterbore inner diameter **174**. Additionally, the box connector **152** has a cross sectional area **182** formed by the outer diameter **170** and inside diameter **172**.

[0051] FIG. 7 shows the pin connector **102** and the box connector **152** in an isometric view aligned with each other on the longitudinal axis **16** prior to the connectors being threadably engaged to form a tubular connection **100**. In the embodiment shown in FIG. 7 and FIG. 8 the pin connector outer and inner diameters **120** and **122** respectively, are substantially the same as the box connector outer and inner diameters **170** and **172** respectively; however, it will be appreciated by those skilled in the art that the connector outer diameters **120** and **170** may differ from one another without deviating from the principles disclosed herein. Likewise, the connection inside diameters **122** and **172** may differ from one another without deviating from the principles disclosed herein. Critically then, it is the fully formed pin threads **110** and fully formed box threads **160** which must remain compatible with one another to ensure the tubular connection **100** remains threadable.

[0052] Further referring then to FIG. 8, an embodiment of the tubular connection **100** is shown, the pin connector **102** shown in FIG. 5 and the box connector **152** shown in FIG. 6 having been threadably engaged. Without being limited to this theory or any other, it will be appreciated by those skilled in the art the cross sectional strength S_{CS} of tubular connection **100** may be calculated by:

$$S_{CS} = Y_S \times (A_N + \text{lesser of } A_{PIN} \text{ or } A_{CB})$$

1 where:

2 **[0053]** Y_s is the yield strength of the material, in pounds per square inch (psi) making up the
3 tubular connection **100**,

4 **[0054]** A_N is the pin nose cross sectional area **132** in square inches,

5 **[0055]** A_{PIN} is the pin cross sectional area **130** at the last engaged thread in square inches,

6 **[0056]** A_{CB} is the box counterbore cross sectional area **180** in square inches.

7 **[0057]** Referring to FIG. 9, FIG. 11, FIG. 13 to 15, and FIG. 17 to 18, enlarged views of
8 various embodiments of fully formed pin threads **110** are shown. It should be appreciated
9 that fully formed threads **160** on box connector **152** may be formed substantially the same as
10 the pin connector threads **110** except that the box connector threads **160** would be formed in
11 such a way that they would be flipped horizontally and vertically relative to the pin threads
12 shown. As such the description of fully formed pin connector threads **110** fully describes
13 equivalent fully formed box connector threads **160**, thus a separate detailed description of
14 fully formed box connector threads **160** is omitted herein for brevity.

15 **[0058]** Referring now to FIG. 9 and FIG. 10 enlarged views of fully formed pin threads **110'**
16 and fully formed box threads **160'** are shown in a configuration that may be common to
17 embodiments of prior art threads. Those skilled in the art will appreciate that each pin thread
18 **110'** features a crest **200**, a root **202**, a load flank **204**, and a stabbing flank **206**. When a
19 connection **100'** is threadably engaged, as shown in FIG. 10 each of the pin thread **110'** load
20 flanks **204** contacts the load flank of a corresponding box thread **160'** along a projected
21 radial direction such that a radial contact face H_r' is formed by the mating load flanks, for
22 example in this prior art H_r' is equal to .082 inches.

23 **[0059]** Without being limited to this theory or any other, it will be appreciated by those skilled
24 in the art the radial bearing strength of the S_{rb} of a tubular connection **100** may be calculated
25 by:

26
$$S_{rb} = \pi \cdot Y_s \cdot D \cdot L \cdot TPI \cdot H_r$$

27 **[0060]** where:

1 [0061] Y_s is the yield strength of the material, in pounds per square inch (psi) making up the
2 tubular connection **100**,

3 [0062] D is the average diameter of the tubular connection **100** pin threads **110** and box
4 threads **160** in inches,

5 [0063] L is the length of the zone of threads engaged between the pin connector **102** and
6 box connector **152** in inches,

7 [0064] TPI is the thread density of the tubular connection **100** in Threads Per Inch,

8 [0065] H_r is the total radial contact face in inches, where it will be appreciated by those
9 skilled in the art that H_r may be a single measured value of a single radial contact face or
10 may be a summation of multiple radial contact faces without deviating from the concepts
11 disclosed herein.

12 [0066] Referring now to FIG. 11, an enlarged view of fully formed pin threads **110** of tubular
13 connection **100** is shown on a preferred embodiment of tubular member **10**. Each thread **110**
14 features a crest **200**, a root **202**, a load flank **204**, and a stabbing flank **206**. Further, each
15 thread includes a load flank reduction zone **220** which acts to reduce the load flank contact
16 area between the pin connector threads **110** and box connector threads **160** when the pin
17 connector **102** is threadably engaged with a box connector **152**. Similarly, while not
18 specifically shown, as one skilled in the art would appreciate the load flank reduction zone
19 **220** may instead be included on the box connector threads **160** as an alternative to the pin
20 connector threads **110**. In the preferred embodiment the load flank reduction zone **220** is
21 included on the box connector threads **160** and on the pin connector threads **110**. It will be
22 understood that it is not a requirement of the present invention that the pin connector threads
23 **110** are a perfect mirror of the box connector threads **160**, only that at least one of the pin
24 connector threads **110** or the box connector threads **160** feature a load reduction zone **220**.
25 In a more specific embodiment, the at least one load flank reduction zone **220** is configured
26 such that the radial bearing strength S_{rb} of the tubular connection **100** is between 100% to
27 110% of the cross sectional connection strength S_{cs} .

28 [0067] Referring still to the embodiment shown in FIG. 11 the load reduction zone **220**
29 consists of a limiting flank **222** inset from the load flank **204** by an inset distance **224**, a
30 concave radius $R_{204-222}$ extending from the load flank **204** to the limiting flank **222**, and a

1 convex radius $R_{222-200}$ extending from the limiting flank **222** to the thread crest **200**.
2 Particularly, in the preferred embodiment the radii $R_{204-222}$ and $R_{222-200}$ are equal and the inset
3 distance **224** of the limiting flank **222** is between approximately .002 and .010 inches. More
4 particularly, the inset distance **224** is equal to .005 inches and the radii $R_{204-222}$ and $R_{222-200}$
5 are equal to .015 inches; however, it should be appreciated that values of the inset distance
6 **224**, and radii $R_{204-222}$ and $R_{222-200}$ may range greatly in other embodiments without deviating
7 from the principles disclosed herein. Further details of the load reduction zone **220** and the
8 resulting interaction of pin connector threads **110** with box connector threads **160** are
9 presented below.

10 **[0068]** Referring to FIG. 12 of the preferred embodiment, when a tubular connection **100** is
11 threadably engaged as shown, each of the pin connector thread **110** load flanks **204**
12 contacts the load flank of a corresponding box connector thread **160** along a projected radial
13 direction such that a radial contact face H_r is formed by the mating load flanks. More
14 specifically in this preferred embodiment H_r is equal to .070 inches.

15 **[0069]** Referring now to FIG. 13, a sequence of enlarged and exaggerated views of fully
16 formed pin connector threads **110** of tubular connection **100** is shown having exaggerated
17 illustrations of atomic spacing within. Without being limited to this theory or any other, when
18 the tubular connection **100** is threadably engaged, the pin connector threads **110** experience
19 load on the load flanks **204** as shown in FIG. 13b. Due to the presence of a preferred
20 embodiment of the load reduction zone **220** the load flank **204** may experience strain
21 hardening, illustrated here by the deformation and dislocation of atoms, whereby new
22 interatomic bonds are formed. Upon removal of the load, it will be understood that a small
23 amount of plastic deformation will have occurred to the load flank **204** due to the presence of
24 the load flank reduction zone **220** and the increased interatomic bonding, however it will be
25 appreciated that the macroscopic geometry and properties of the pin connector threads **110**
26 (for example the shear strength) has not been appreciably altered and that the pin connector
27 threads **110** remain compatible with mating box connector thread **160**.

28 **[0070]** Referring now to FIG. 14 an enlarged view of fully formed pin connector threads **110**
29 of tubular connection **100** is shown having an alternative embodiment of the load reduction
30 zone **220**. The load flank reduction zone **220** consists of a limiting flank **222** inset from the
31 load flank **204** by an inset distance **224**, a concave radius $R_{202-220}$ extending from the thread

1 root **202** to the limiting flank **222**, and a convex radius $R_{220-204}$ extending from the limiting
2 flank **222** to the load flank **204**. Particularly, in the preferred embodiment the radii $R_{202-220}$
3 and $R_{220-204}$ are equal to .030 and .015 inches respectively, and the inset distance **224** of the
4 limiting flank **222** is between approximately .002 and .010 inches. More particularly, the inset
5 distance **224** is equal to .005 inches; however, it should be appreciated that values of the
6 inset distance **224**, and radii $R_{204-222}$ and $R_{222-200}$ may range greatly in other embodiments
7 without deviating from the principles disclosed herein.

8 **[0071]** Referring now to FIG. 15 an enlarged view of fully formed pin connector threads **110**
9 of tubular connection **100** is shown having an alternative embodiment of the load reduction
10 zone **220**. The load flank reduction zone **220** consists of a limiting flank **222** inset from the
11 load flank **204** by an inset distance **224** such that the load flank **204** is bifurcated into a first
12 load flank **204a** more proximate the thread crest **200**, and a second load crest **204b** more
13 proximate the thread root **202**. In this way, FIG. 16 demonstrates when a tubular connection
14 **100** is threadably engaged, each of the pin connector thread **110** load flanks **204a** and **204b**
15 contacts the at least one load flank of a corresponding box connector thread **160** along a
16 projected radial direction such that at least two radial contact faces H_{r1} and H_{r2} are formed by
17 the mating load flanks. It will be appreciated by those skilled in the art that the summation of
18 H_{r1} and H_{r2} form a comparable total radial contact face H_r to that disclosed in a preferred
19 embodiment above. The load reduction zone **220** further consists of a convex radius R_{220}
20 extending from the second load flank **204b** to the limiting flank **222** and connecting to the
21 first load flank **204a**. Particularly, in this embodiment the inset distance **224** of the limiting
22 flank **220** is between approximately .002 and .010 inches. More particularly, the inset
23 distance **224** is equal to .005 inches and the radius R_{220} is equal to .010 inches; however, it
24 should be appreciated that values of the inset distance **224**, and radius R_{220} may range
25 greatly in other embodiments without deviating from the principles disclosed herein. It will be
26 appreciated by those skilled in the art that it is undesirable to position the load reduction
27 zone **220** in a location that would compromise the shear strength of the pin connector
28 threads **110** or box connector threads **160**.

29 **[0072]** Referring now to FIG. 19 a method **300** for manufacturing a tubular connector is
30 presented. Initially, the method **300** includes forming a pin connector (e.g., pin connector
31 **102**) or box connector (e.g., box connector **152**) on one end of a first tubular member (e.g., a
32 tubular member **10**) in block **305**. A plurality of threads (e.g. pin connector threads **110'** or

box connector threads **160'**) are formed on the threaded connector in block **310** such that when the tubular connection (e.g. tubular connection **100**) is threadably engaged, each of the threads (e.g. pin connector threads **110'** or box connector threads **160'**) of the tubular connector contacts the load flanks of the mating connector, and form a projected load flank radial contact face H_r' , and the tubular connection having a corresponding cross sectional connection strength S_{cs} and a radial bearing strength S_{rb}' . Finally in block **315**, at least one load flank reduction zone (e.g. load flank reduction zone **220**) is formed on the threads (e.g. pin connector threads **110'** or box connector threads **160'**) in such a way that the projected load flank radial contact face H_r' is reduced to H_r and the threads are formed into fully formed threads (e.g. fully formed pin connector threads **110** or fully formed box connector threads **160**) having a reduced radial bearing strength S_{rb} along the length of the zone of threads. In a more specific embodiment, the at least one load flank reduction zone **220** is configured such that the radial bearing strength S_{rb} of the tubular connection **100** is between 100% to 110% of the cross sectional connection strength S_{cs} .

[0073] It will be understood by persons skilled in the art that while some figures specifically illustrate at least one load reduction zone formed on pin connector threads **110** or box connector threads **160**, this is for illustrative consistency and brevity, and that such load reduction zones **220** may be formed on the pin connector threads **110**, box connector threads **160**, or both the mating pin connector threads **110** and box connector threads **160** without deviating from the scope of the principles disclosed herein. It will be further understood by persons skilled in the art that any combination of load flank reduction zones **220** may occur (for example the further embodiments presented in FIG. 16 and FIG. 17, or combinations of the load flank reduction zones discussed herein) provided that when the tubular connection **100** is threadably made up the at least one load flank reduction zones **220** is configured such that the radial bearing strength S_{rb} of the tubular connection **100** is reduced, and in a preferred embodiment is between 100% to 110% of the cross sectional connection strength S_{cs} .

[0074] Any use herein of terms describing an interaction between elements is not meant to limit the interaction to direct interaction between the subject elements and may also include indirect interaction between the elements such as through secondary or intermediary structure unless specifically stated otherwise. Further, unless expressly stated otherwise the steps in a method or method claim may be performed in any order. The use of identifiers a) ,

1 b) , c) and so forth before steps in describing a method should not be interpreted to specify a
2 particular order to the steps, but instead are used for clarity and brevity in subsequent
3 reference to such steps.

4 **[0075]** It will be apparent that changes may be made to the illustrative embodiments, while
5 falling within the scope of the invention. As such, the scope of the following claims should
6 not be limited by the preferred embodiments set forth in the examples and drawings
7 described above but should be given the broadest interpretation consistent with the
8 description as a whole.

9

10

WHAT IS CLAIMED IS:

1. A tubular member having a box connector provided on a first end thereof, the box connector being adapted to receive a corresponding pin connector provided on another tubular member, the box connector comprising:

- a nominal pitch diameter, a longitudinal axis, a primary shoulder, a secondary shoulder, and a zone of internal threads;
- the zone of internal threads comprising a plurality of threads which taper relative to the longitudinal axis, the plurality of threads comprising: a thread crest, a thread root, at least one load flank, a stabbing flank, and at least one load flank reduction zone;
- the box connector being adapted to be threadably engaged with a corresponding pin connector provided on another tubular member, whereby a tubular connection is formed wherein each of the at least one load flanks on the box connector contacts the at least one load flanks of a corresponding thread on the corresponding pin connector along a projected radial direction such that at least one projected load flank radial contact face H_r is formed by the mating load flanks;
- wherein the at least one load flank reduction zone reduces the radial bearing strength of the tubular connection.

2. A tubular member having a pin connector provided on a first end thereof, the pin connector being adapted to be received in a corresponding box connector provided on another tubular member, the pin connector comprising:

- a nominal pitch diameter, a longitudinal axis, a primary shoulder, a secondary shoulder, and a zone of external threads;
- the zone of external threads comprising a plurality of threads which taper relative to the longitudinal axis, the plurality of threads comprising: a thread crest, a thread root, at least one load flank, a stabbing flank, and at least one load flank reduction zone;
- the pin connector being adapted to be threadably engaged with a corresponding box connector provided on another tubular member, whereby a tubular connection is formed wherein each of the at least one load flanks on the pin connector contacts the at least one load flanks of a corresponding thread on the corresponding box connector along a projected radial direction such that at least one projected load flank radial contact face H_r is formed by the mating load flanks;

- wherein the at least one load flank reduction zone reduces the radial bearing strength of the tubular connection.
3. The tubular member of claim 1 or 2 wherein the load flank reduction zone includes:
- a limiting flank inset parallel to the load flank;
 - a first radius extending between the thread crest and the limiting flank having a first radius of curvature;
 - a second radius extending from the limiting flank to the load flank having a second radius of curvature;
 - wherein the first radius has a convex radius of curvature and the second radius has a concave radius of curvature.
4. The tubular member of claim 3 wherein the limiting flank is inset from the load flank between .002 and .010 inches.
5. The tubular member of claim 4 wherein the first convex radius of curvature is .015 inches and wherein the second concave radius of curvature is .015 inches.
6. The tubular member of claim 1 or 2 wherein the load flank reduction zone includes:
- a limiting flank inset parallel to the load flank;
 - a first radius extending between the thread root and the limiting flank having a first radius of curvature;
 - a second radius extending from the limiting flank to the load flank having a second radius of curvature;
 - wherein the first radius has a concave radius of curvature and wherein the second radius has a concave radius of curvature.
7. The tubular member of claim 6 wherein the limiting flank is inset from the load flank between .002 and .010 inches.
8. The tubular member of claim 7 wherein the first concave radius of curvature is .030 inches and wherein the second concave radius of curvature is .015 inches.

9. The tubular member of claim 1 or 2 wherein the load flank reduction zone includes:
 - at least one limiting flank inset parallel to the load flank;
 - a radius extending between the load flank and the limiting flank having a concave radius of curvature.
10. The tubular member of claim 9 wherein the limiting flank is inset from the load flank between .002 and .010 inches.
11. The tubular member of claim 10 wherein the concave radius of curvature is .010 inches.
12. The tubular member of any one of claims 1 to 11 wherein when a connection between tubular members is made the tubular connection projected load flank radial contact face H_r is equal to approximately 0.070 inches.
13. The tubular member of any one of claims 1 to 12 wherein when a connection between tubular members is made the tubular connection primary shoulders, secondary shoulders, average diameter, and plurality of threads correspond to a cross sectional connection strength S_{cs} ;
 - and wherein the at least one projected load flank radial contact face H_r corresponds to a radial bearing strength S_{rb} along the entire length of the zone of threads;
 - and wherein the at least one load flank reduction zone alters the projected load flank radial contact face such that the relationship $1.00 \leq \frac{S_{rb}}{S_{cs}} \leq 1.10$ is satisfied.
14. The tubular member of any one of claims 1 to 13 wherein upon being threadably engaged and torqued, the material directly adjacent the thread load flanks has a strain hardened metallurgical grain structure oriented parallel to the load flanks.
15. A tubular connection between a pin connector and a box connector, wherein the pin connector is adapted to be threadably engaged with the box connector, each of said connectors having an outer diameter, an inner throughbore diameter, a nominal pitch diameter, and a longitudinal axis, the connection comprising:

- a tapered pin connector comprising a pin primary shoulder, a pin secondary shoulder, and a zone of external threads, and a tapered box connector comprising a box primary shoulder, a box secondary shoulder, and a zone of internal threads;
- the threaded zones comprising a plurality of threads which taper relative to the longitudinal axis, the plurality of threads comprising: a thread crest, a thread root, at least one load flank, a stabbing flank, and at least one load flank reduction zone;
- wherein each of the at least one load flanks on the pin connector contacts the at least one load flanks of the corresponding thread on the box connector along a projected radial direction such that at least one projected load flank radial contact face is formed by the mating load flanks;
- wherein the at least one load flank reduction zone reduces the radial bearing strength of the tubular connection.

16. The tubular connection of claim 15 wherein the primary shoulders, secondary shoulders, average diameter, and plurality of threads correspond to a cross sectional connection strength S_{cs} ;

- wherein the at least one projected load flank radial contact face corresponds to a radial bearing strength S_{rb} along the entire length of the zone of threads;
- wherein the at least one load flank reduction zone alters the projected load flank radial contact face such that the relationship $1.00 \leq \frac{S_{rb}}{S_{cs}} \leq 1.10$ is satisfied.

17. A method for manufacturing a box connector on a tubular member, the box connector being adapted to receive a corresponding pin connector provided on another tubular member having an outer diameter, an inner throughbore diameter, and longitudinal axis, the method comprising:

- a) forming a box connector on the end of the first tubular member, the box connector comprising an outside diameter, an inner throughbore diameter, a box primary shoulder, a box secondary shoulder, and a zone of internal threads having a nominal pitch diameter;

wherein, when the box connector is threadably engaged with a corresponding pin connector, the primary shoulder, secondary shoulder, nominal pitch diameter, and plurality of threads form a cross sectional connection strength S_{cs} ;

- b) forming a plurality of threads in the region between the box primary shoulder and the box secondary shoulder, the plurality of threads comprising a thread crest, thread root, a load flank, and a stabbing flank;

wherein, when the box connector is threadably engaged with a corresponding pin connector, each of the plurality of threads on the box connector contacts a corresponding thread on the corresponding pin connector along a projected radial direction such that a projected load flank radial contact face H_r' is formed by the mating load flanks, corresponding to a radial bearing strength S_{rb}' of the tubular connection;

- c) forming at least one load flank reduction zone on the load flanks of the plurality of box connector threads wherein when the box connector is threadably engaged with a corresponding pin connector, the at least one load flank reduction zone reduces the projected load flank radial contact face H_r' to H_r such that the radial bearing strength of the tubular connection S_{rb}' is reduced to S_{rb} .

18. A method for manufacturing a pin connector on a tubular member, the pin connector being adapted to be received in a corresponding box connector provided on another tubular member having an outer diameter, an inner throughbore diameter, and longitudinal axis, the method comprising:

- a) forming a pin connector on the end of the first tubular member, the pin connector comprising an outside diameter, an inner throughbore diameter, a pin primary shoulder, a pin secondary shoulder, and a zone of external threads having a nominal pitch diameter;

wherein, when the pin connector is threadably engaged with a corresponding box connector, the primary shoulder, secondary shoulder, nominal pitch diameter, and plurality of threads form a cross sectional connection strength S_{cs} ;

- b) forming a plurality of threads in the region between the pin primary shoulder and the pin secondary shoulder, the plurality of threads comprising a thread crest, thread root, a load flank, and a stabbing flank;

wherein, when the pin connector is threadably engaged with a corresponding box connector, each of the plurality of threads on the pin connector contacts a corresponding thread on the corresponding box connector along a projected

radial direction such that a projected load flank radial contact face H_r' is formed by the mating load flanks, corresponding to a radial bearing strength S_{rb}' of the tubular connection;

- c) forming at least one load flank reduction zone on the load flanks of the plurality of pin connector threads wherein when the pin connector is threadably engaged with a corresponding box connector, the at least one load flank reduction zone reduces the projected load flank radial contact face H_r' to H_r such that the radial bearing strength of the tubular connection S_{rb}' is reduced to S_{rb} .

19. The method of claim 17 or 18 wherein the load flank reduction zone of (c) further comprises:

- forming a limiting flank inset parallel to the load flank, a first radius extending between the thread crest and the limiting flank having a first radius of curvature, a second radius extending from the limiting flank to the load flank having a second radius of curvature;
- wherein the first radius has a first convex radius of curvature and the second radius has a second concave radius of curvature.

20. The method of claim 19 wherein the limiting flank is inset from the load flank between .002 and .010 inches.

21. The method of claim 20 wherein the first convex radius of curvature is .015 inches and wherein the second concave radius of curvature is .015 inches.

22. The method of claim 17 or 18 wherein the load flank reduction zone of (c) further comprises:

- forming a limiting flank inset parallel to the load flank, a first radius extending between the thread root and the limiting flank having a first radius of curvature, a second radius extending from the limiting flank to the load flank having a second radius of curvature
- wherein the first radius has a first concave radius of curvature and wherein the second radius has a concave radius of curvature.

23. The method of claim 22 wherein the limiting flank is inset from the load flank between .002 and .010 inches.
24. The method of claim 23 wherein the first concave radius of curvature is .030 inches and wherein the second concave radius of curvature is .015 inches.
25. The method of claim 17 or 18 wherein the load flank reduction zone of (c) further comprises:
- forming a limiting flank inset parallel to the load flank, and a radius extending between the load flank and the limiting flank having a concave radius of curvature.
26. The method of claim 25 wherein the limiting flank is inset from the load flank between .002 and .010 inches.
27. The method of claim 26 wherein the concave radius of curvature is .010 inches.
28. The method of any one of claims 17 to 27 wherein (c) further comprises:
- forming the load reduction zone wherein the projected load flank radial contact face H_r is equal to approximately 0.070 inches.
29. The method of any one of claims 17 to 28 wherein when the connector is threadably engaged with a corresponding connector, a tubular connection is formed whereby the at least one load flank reduction zone alters the tubular connection such that the relationship $1.00 \leq \frac{S_{rb}}{S_{cs}} \leq 1.10$ is satisfied.

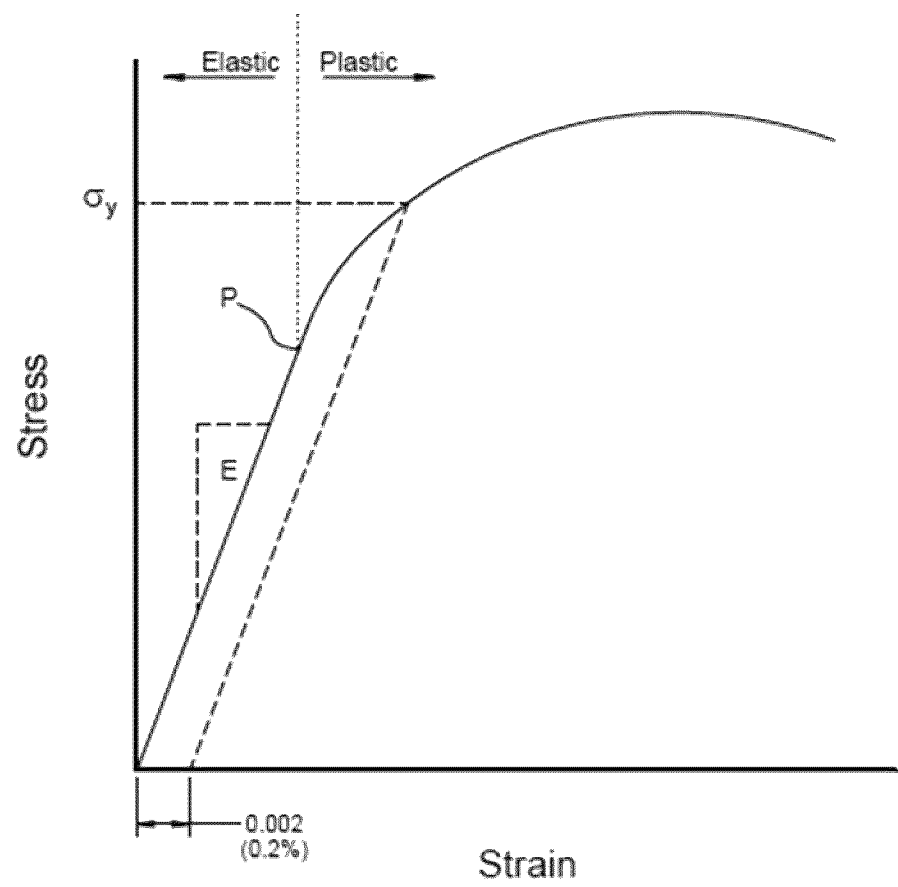


FIG. 1

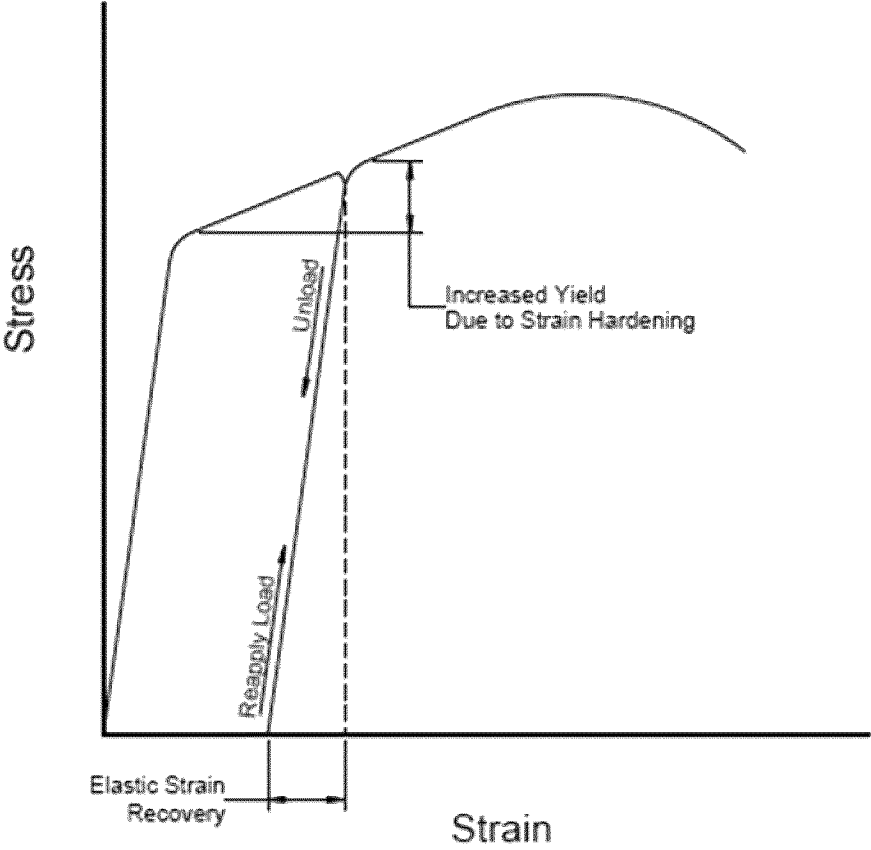
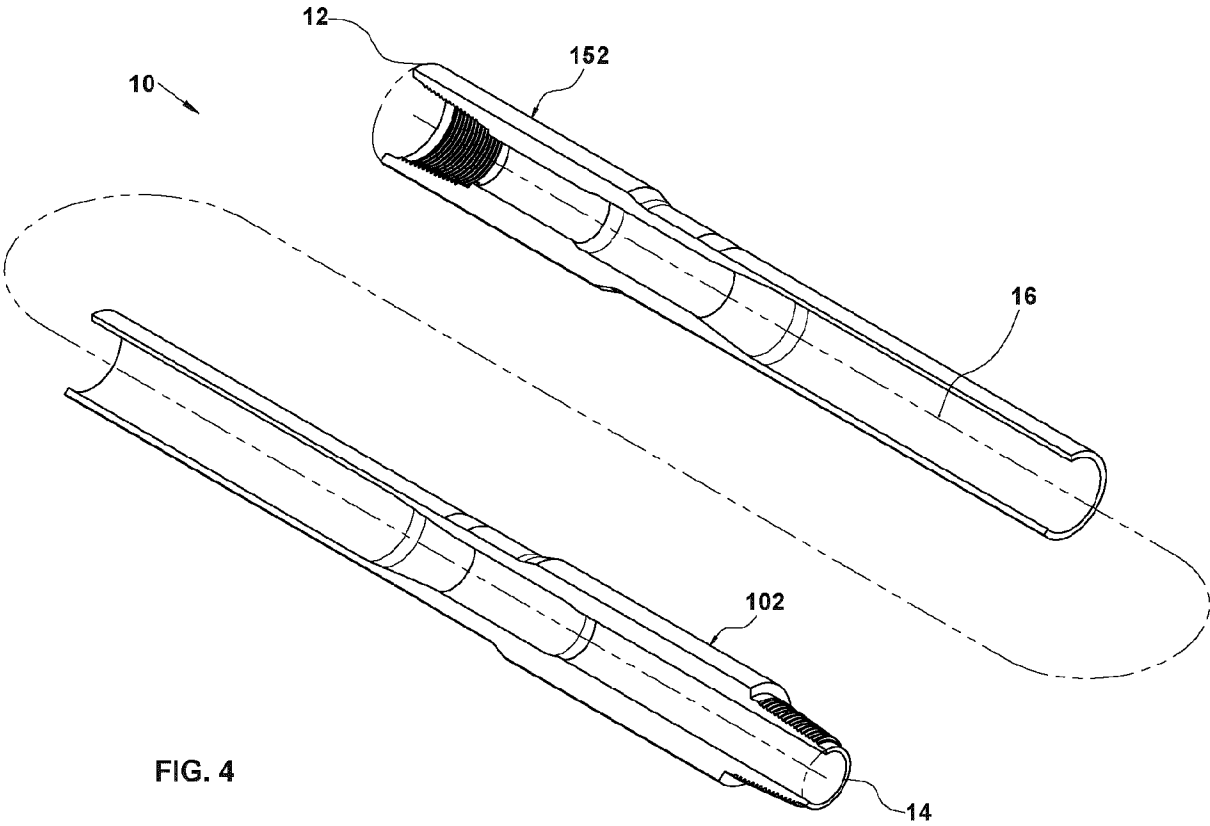
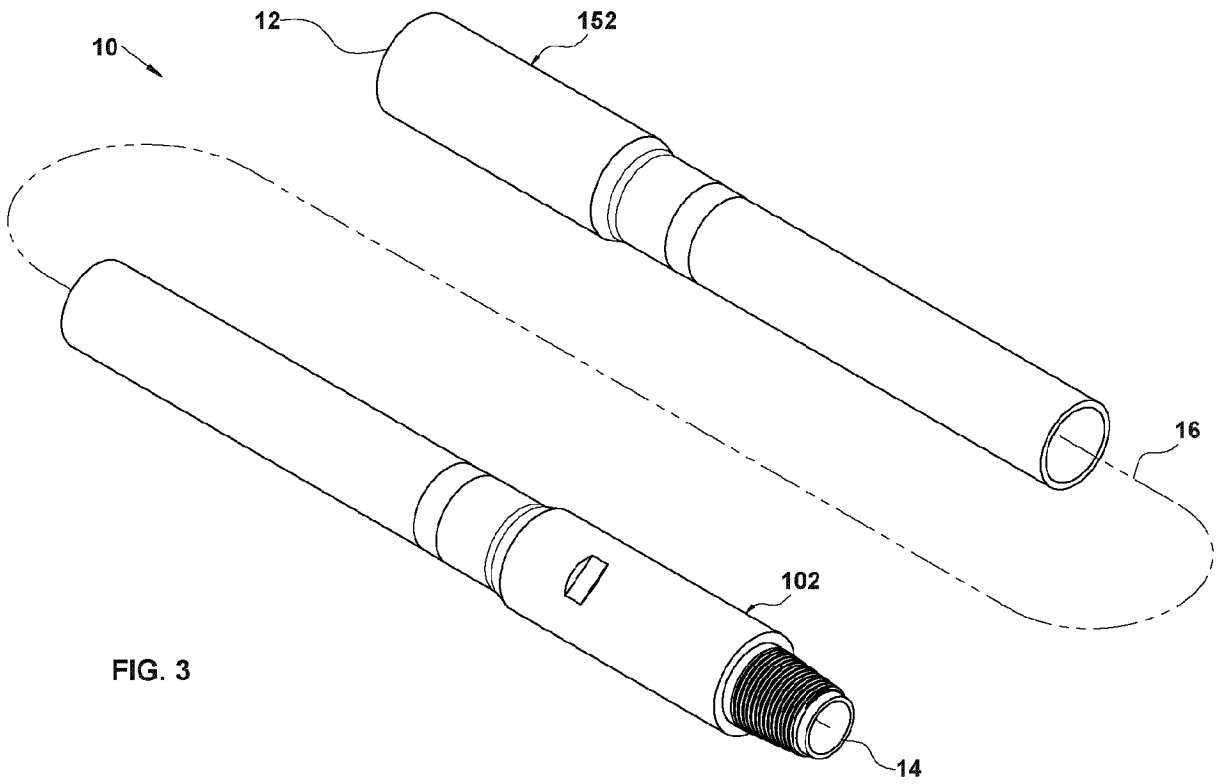


FIG. 2



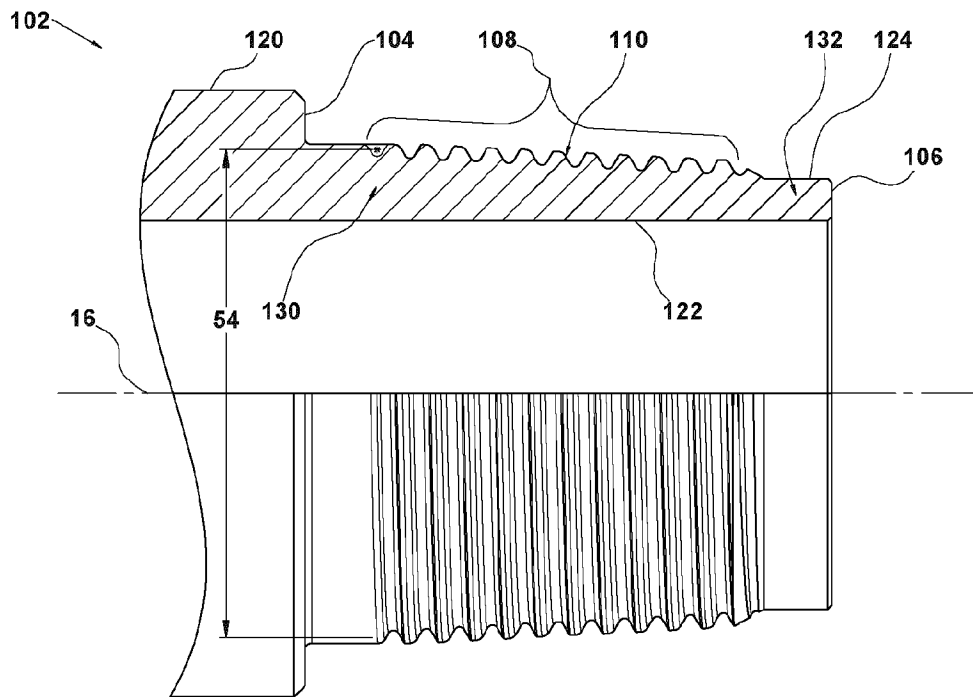


FIG. 5

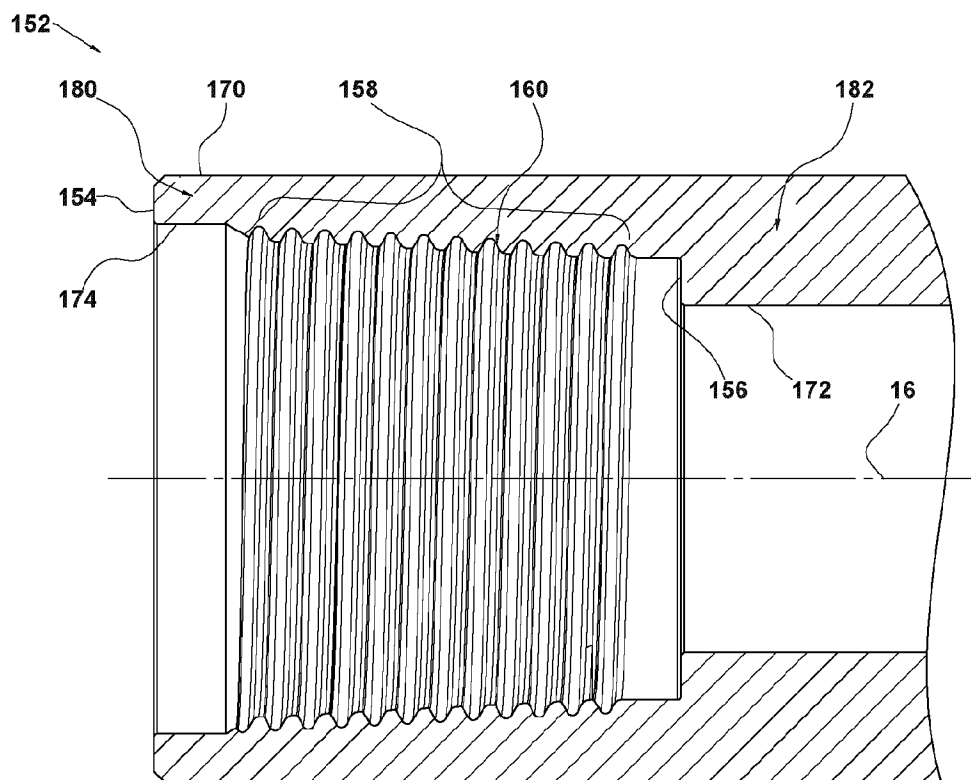


FIG. 6

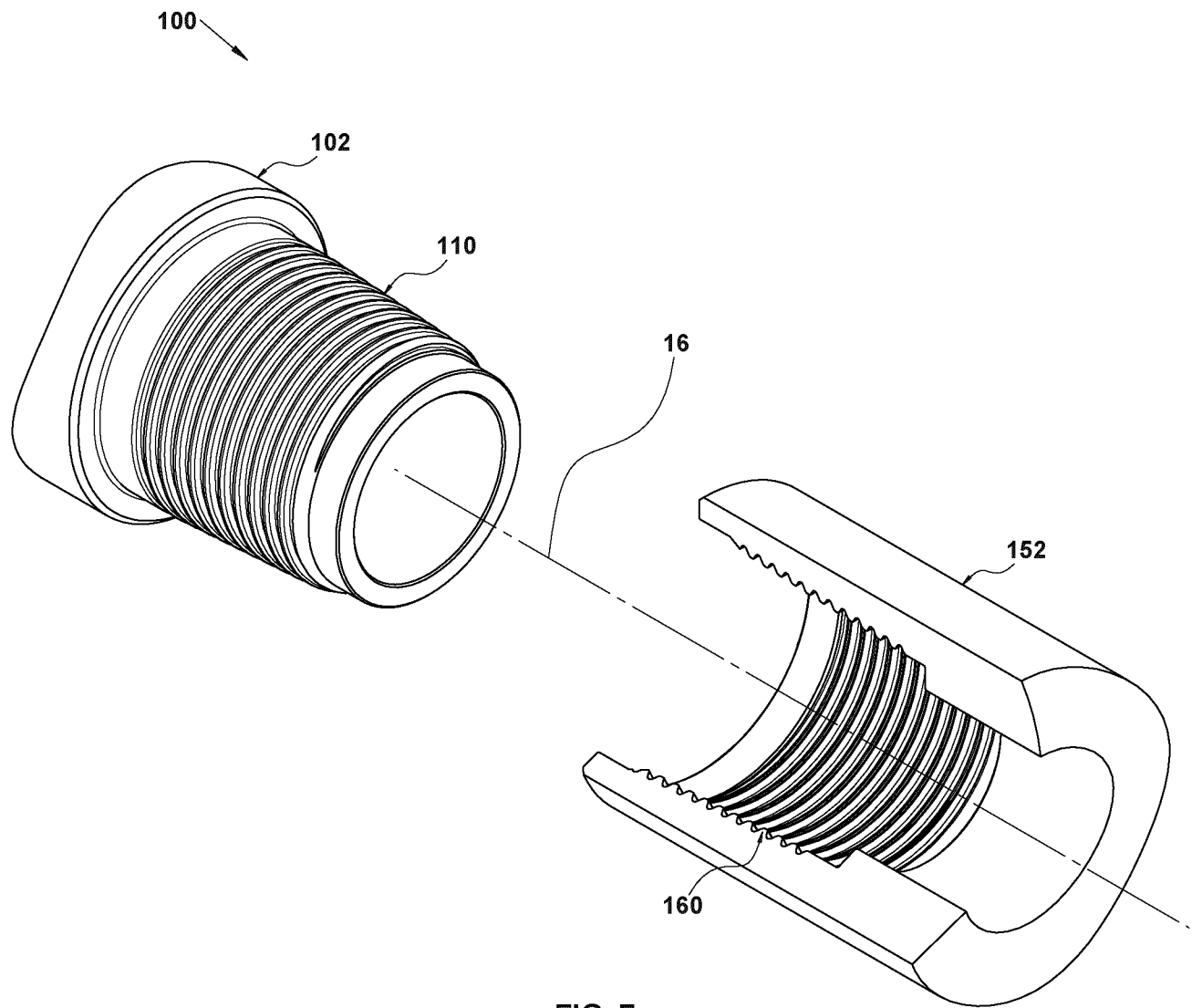
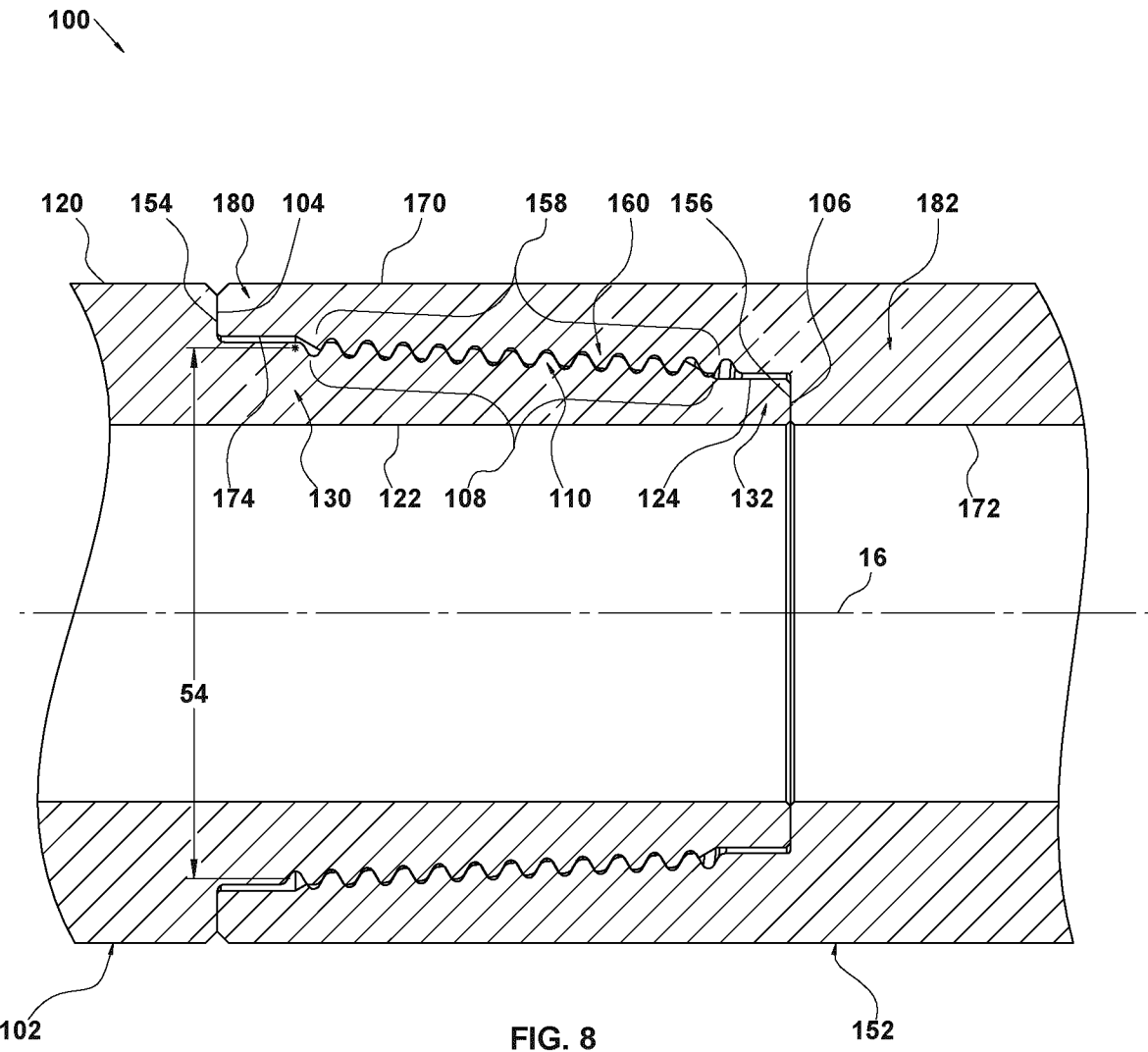


FIG. 7



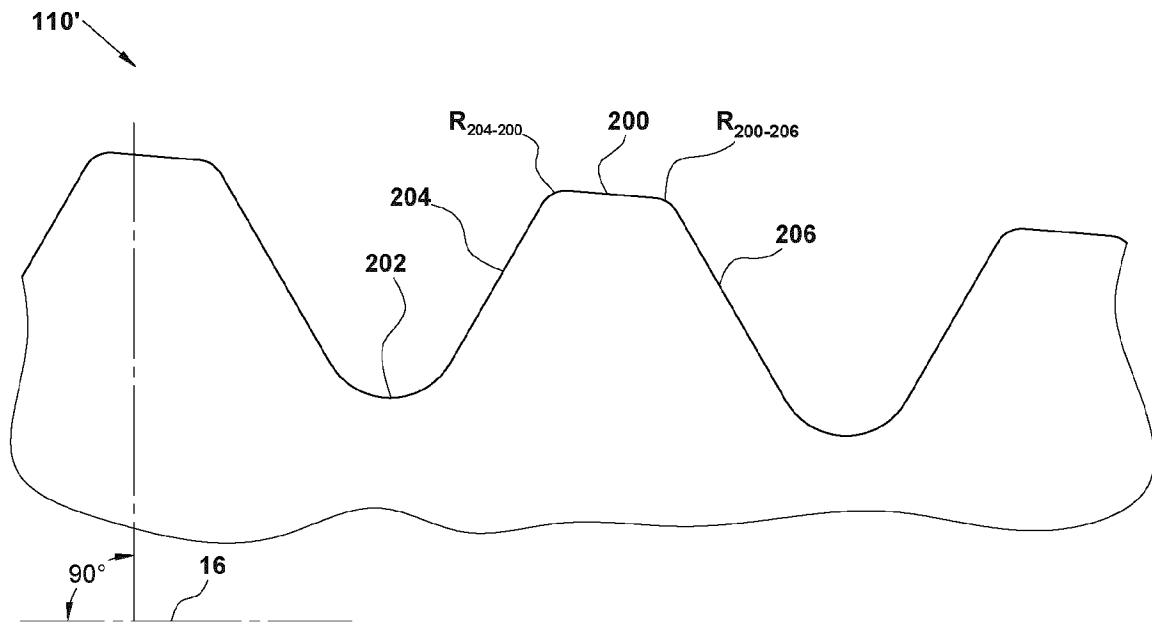


FIG. 9 - (PRIOR ART)

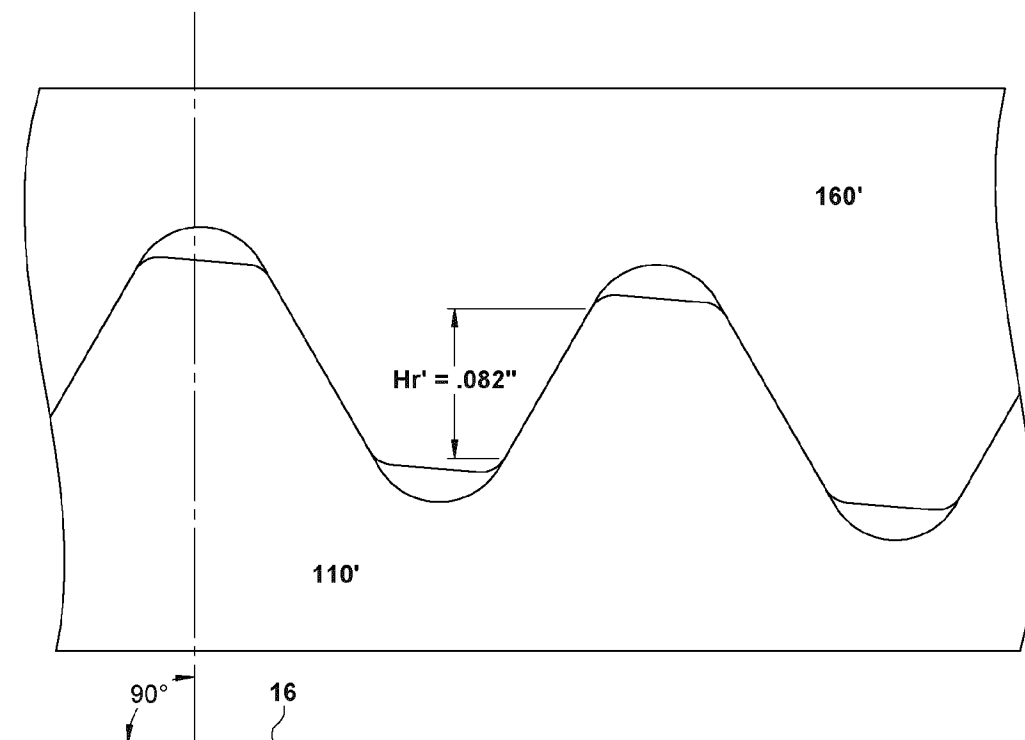


FIG. 10 - (PRIOR ART)

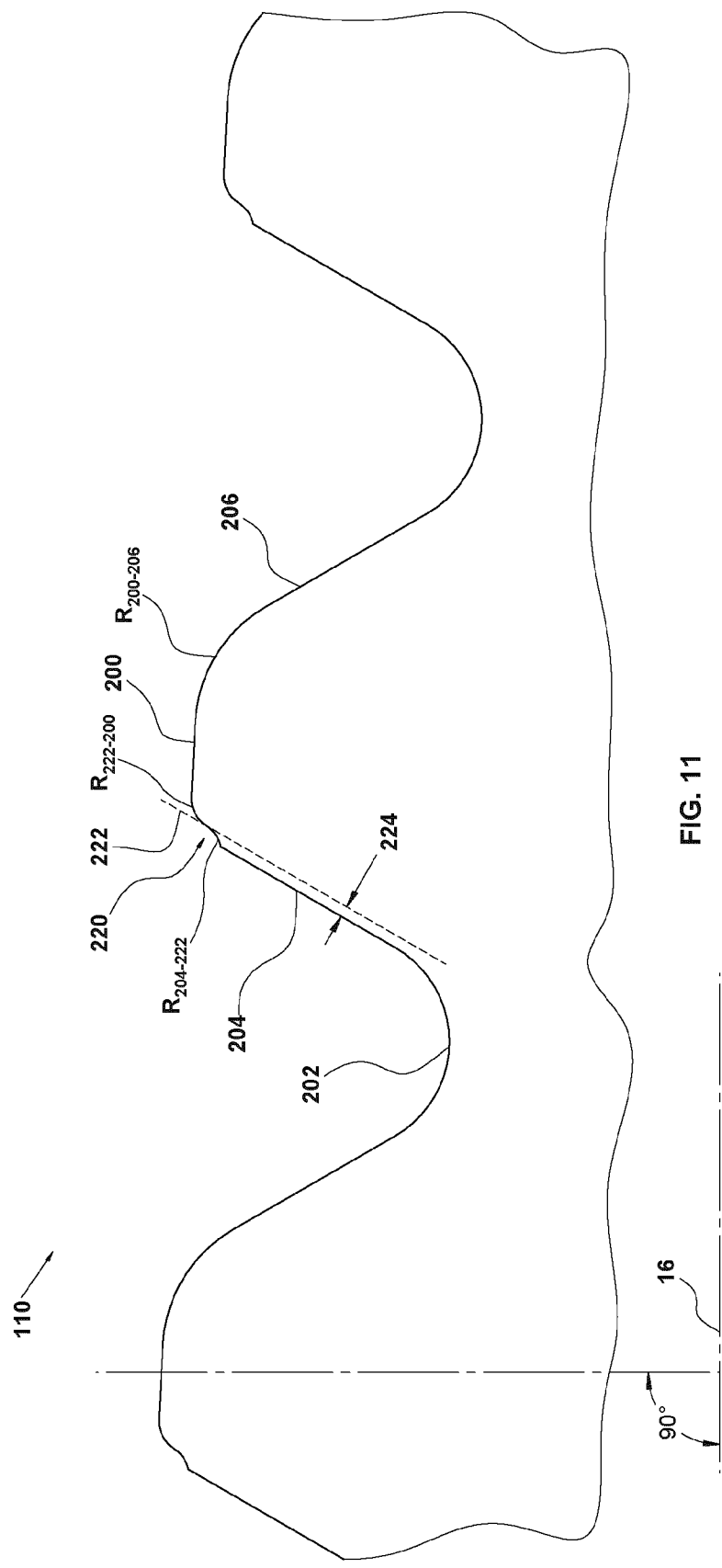
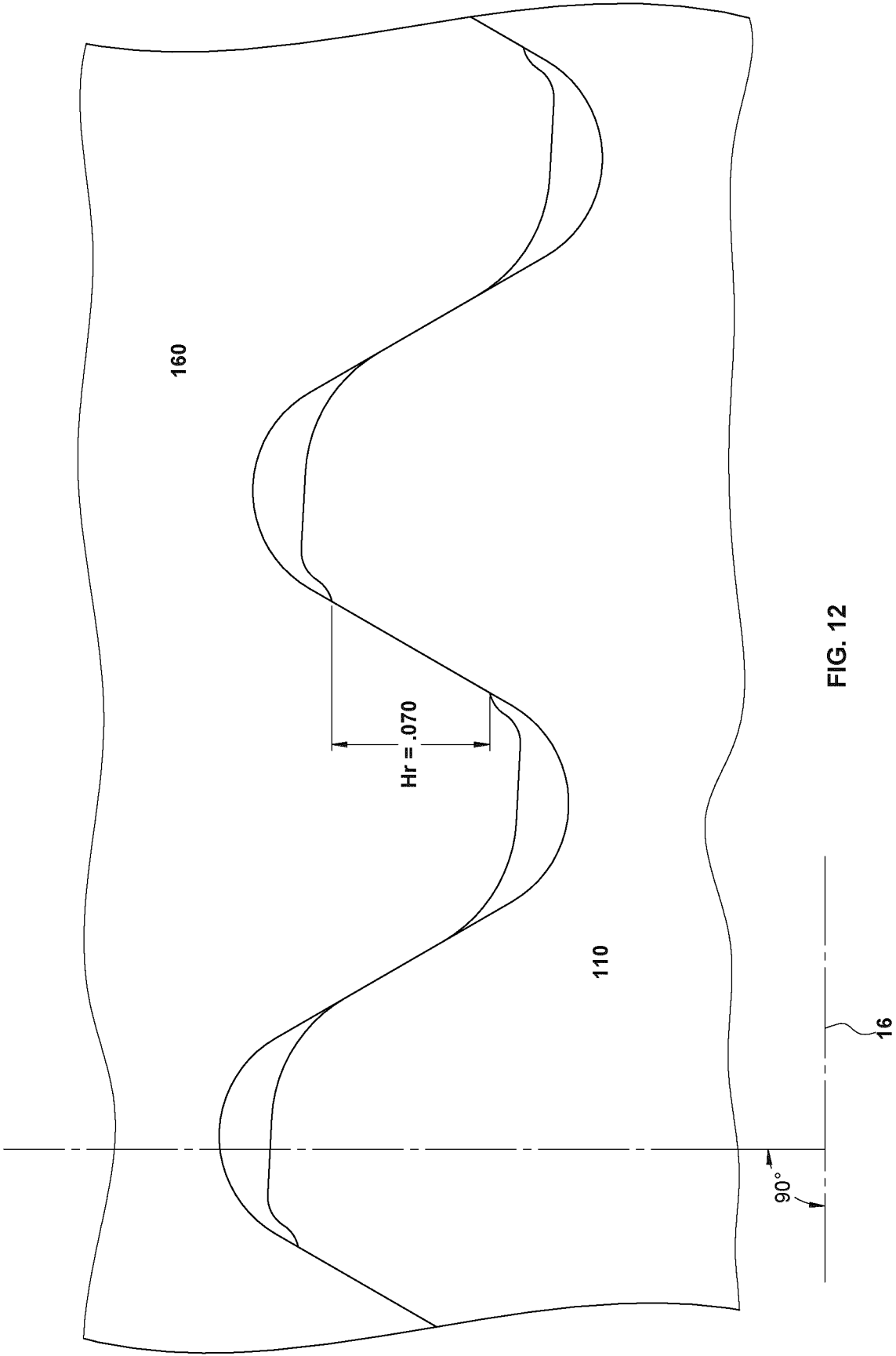
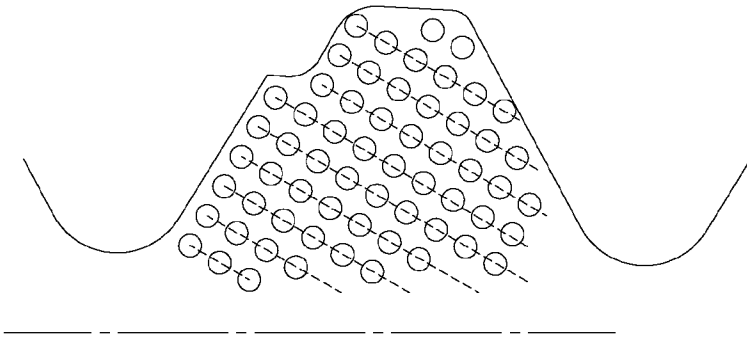
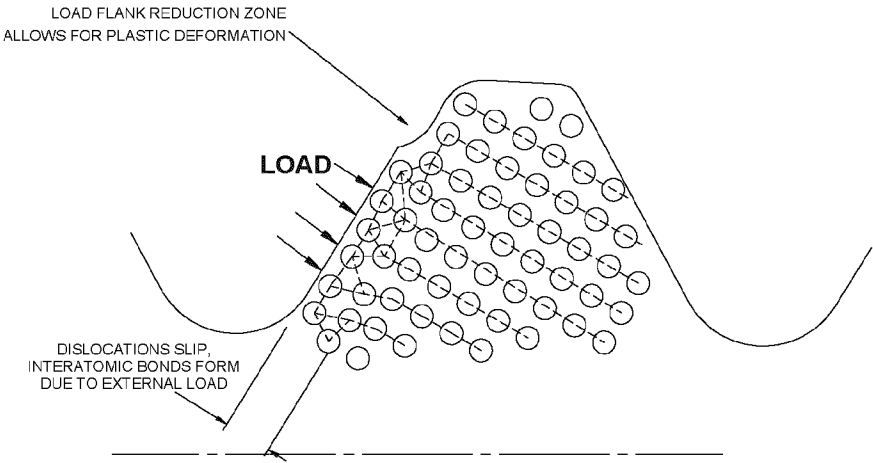


FIG. 11

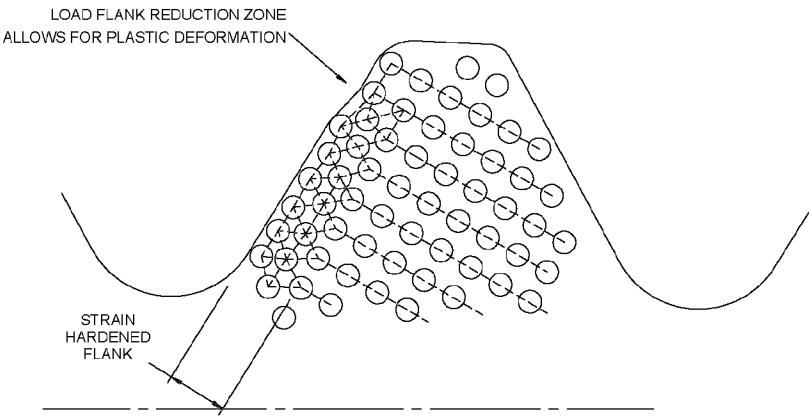




13a

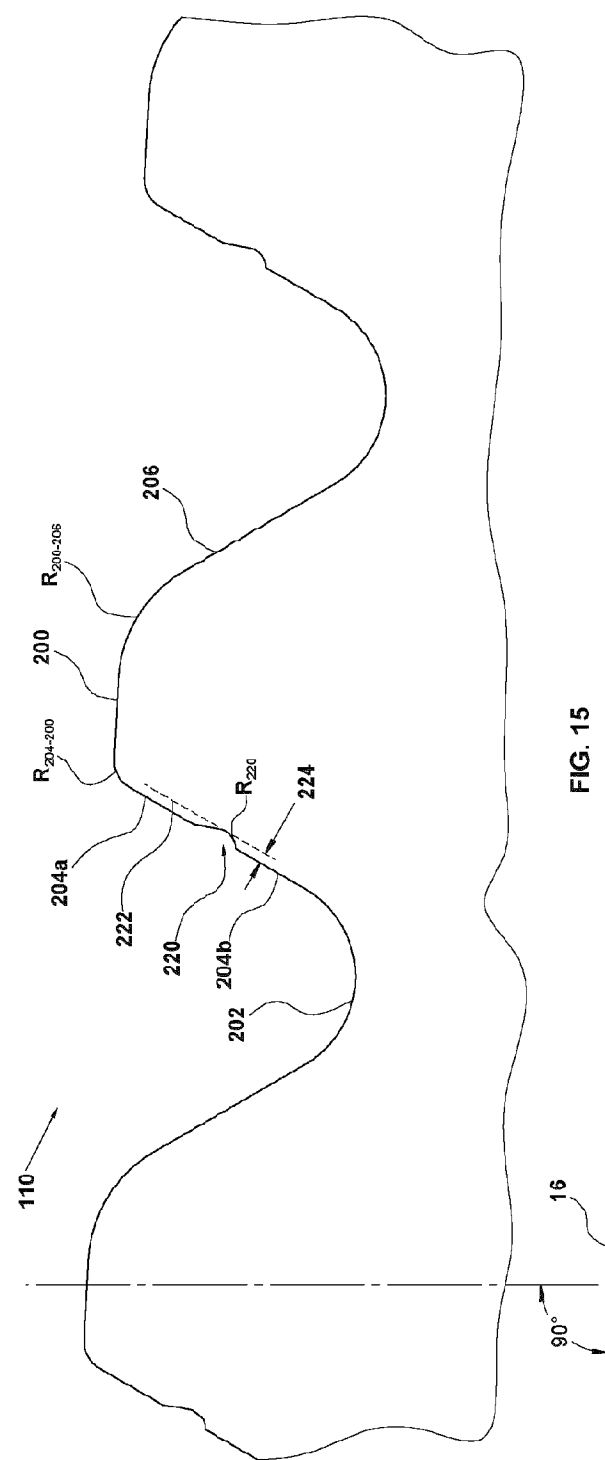
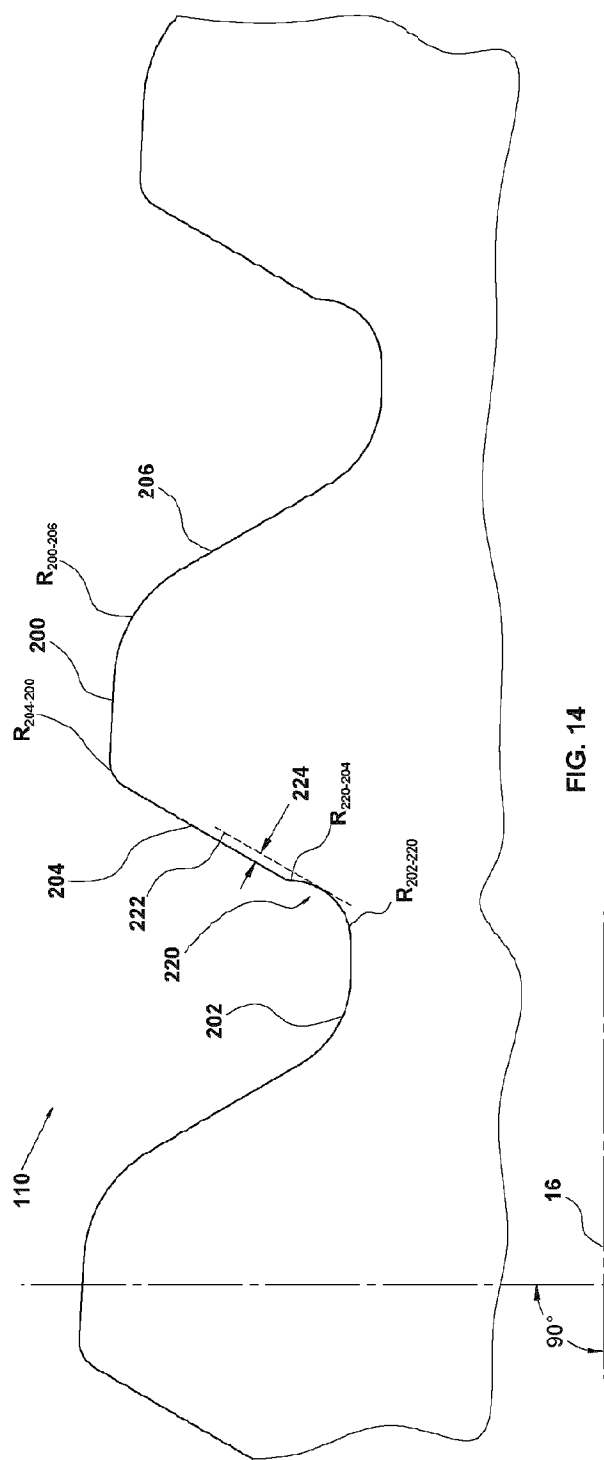


13b



13c

FIG. 13



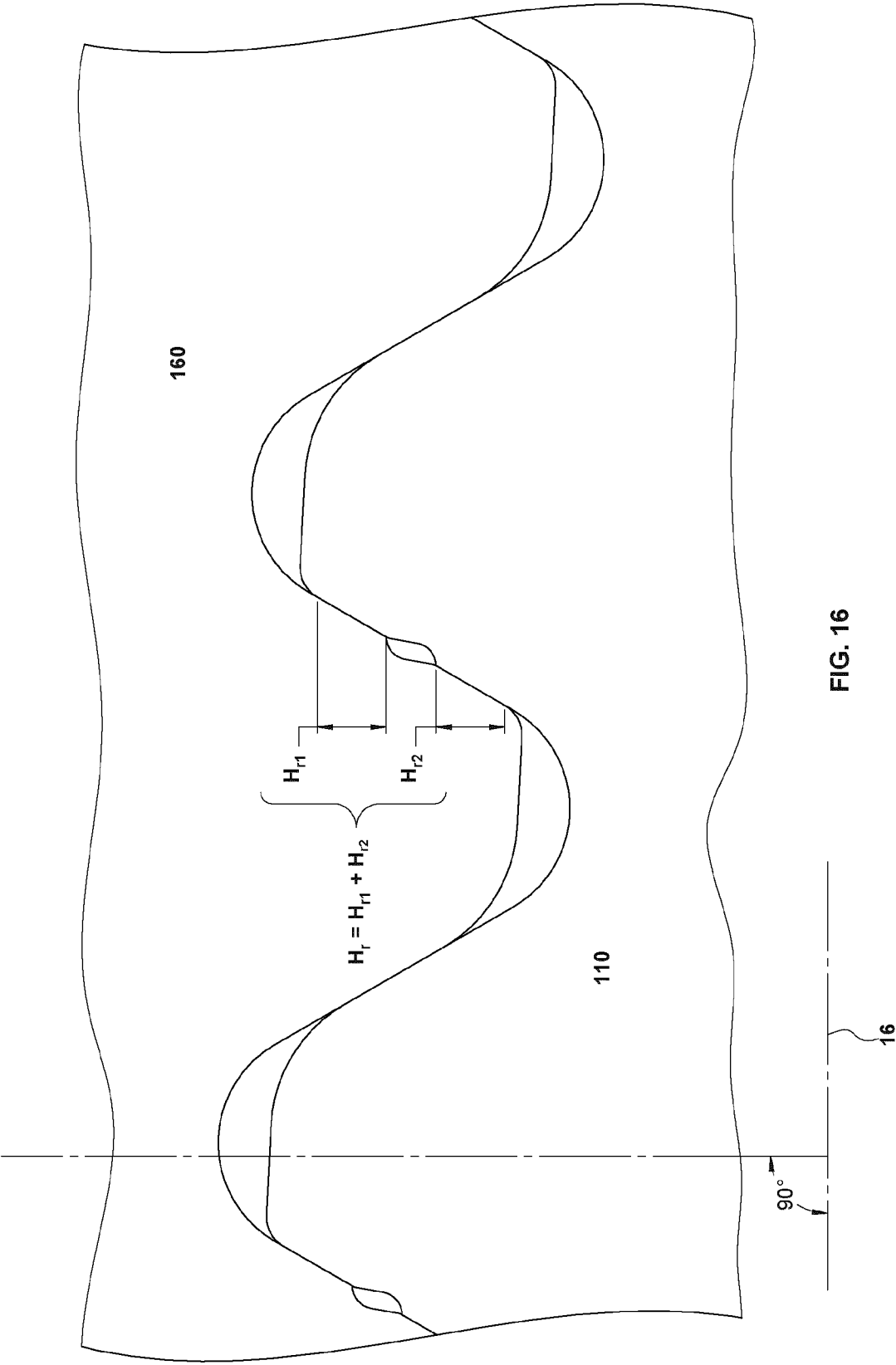


FIG. 16

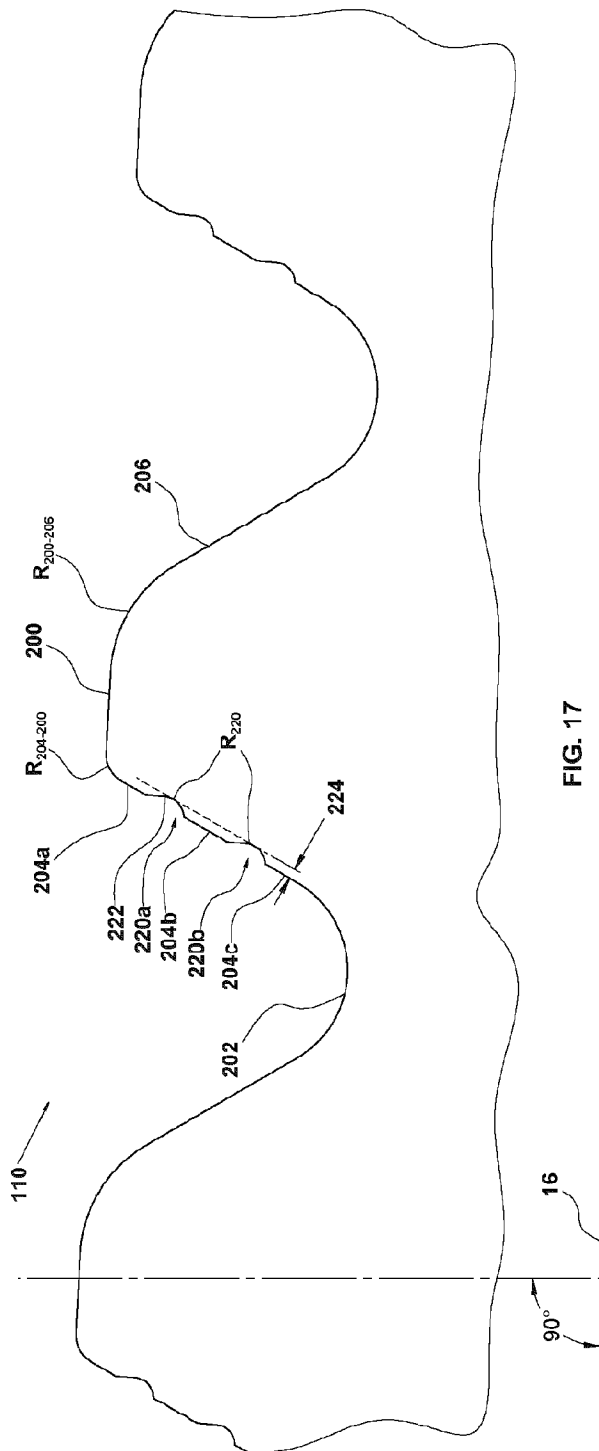


FIG. 17

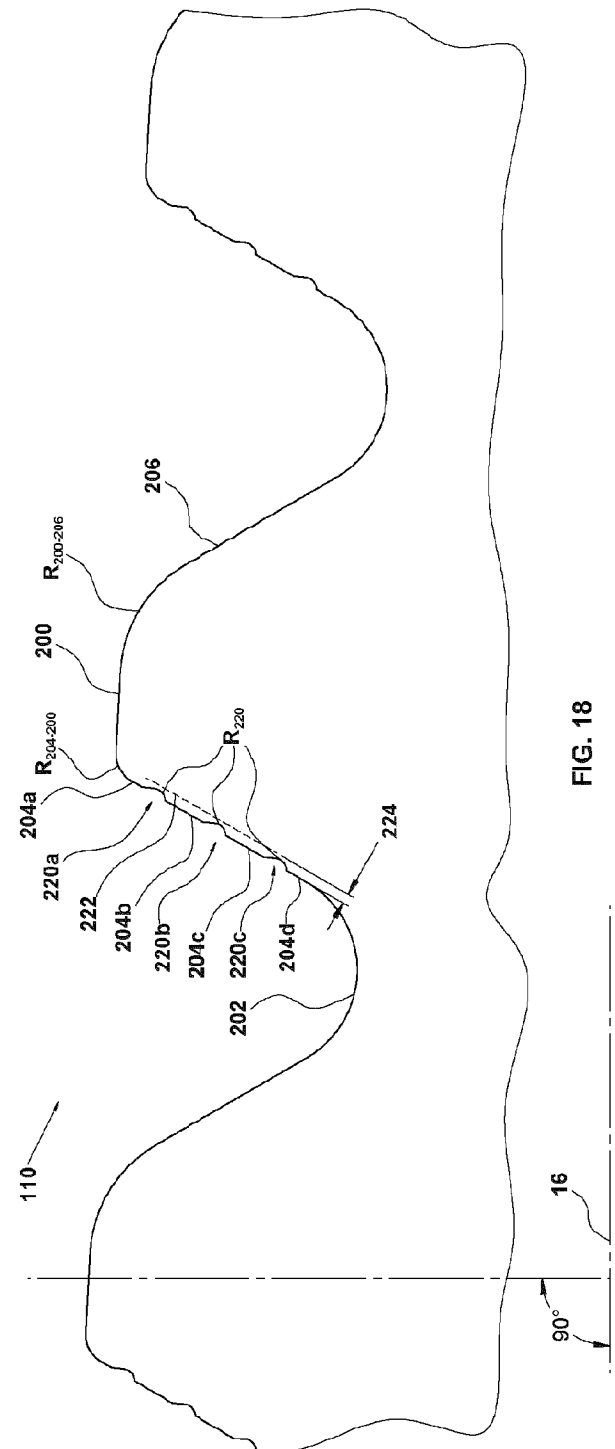


FIG. 18

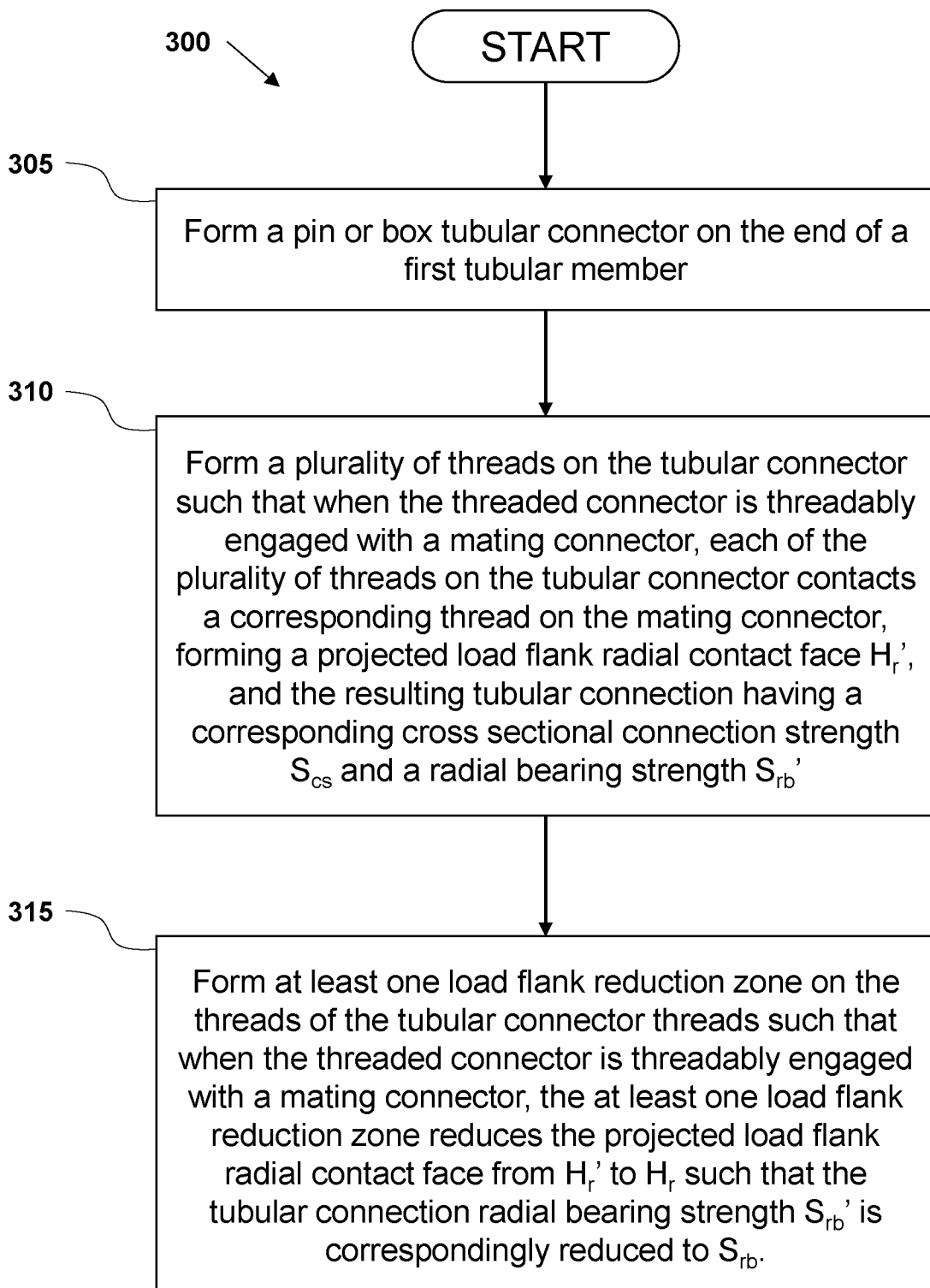


FIG. 19

INTERNATIONAL SEARCH REPORT

International application No.

PCT/CA2022/051667

A. CLASSIFICATION OF SUBJECT MATTER

IPC: **F16L 15/06** (2006.01), **E21B 17/042** (2006.01)

CPC: , E21B 17/042 (2020.05), F16L 15/001 (2020.01), F16L 15/06 (2020.01)

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC: F16L 15/06 (2006.01), E21B 17/042 (2006.01) CPC: E21B 17/042 (2020.05), F16L 15/001 (2020.01), F16L 15/06 (2020.01)

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic database(s) consulted during the international search (name of database(s) and, where practicable, search terms used)

Questel Orbit (fampat); Keywords (flank)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US2012286507A1, (MAILLON et al.) 15 November 2012 (15-11-2012) *whole document*	1, 2, 6-12, 14-15, 17-18, 22-28
A	US2013147191A1, (MAZZAFERRO et al.) 13 June 2013 (13-06-2013) *whole document*	1-29
A	US6412831B1, (NOEL et al.) 02 July 2002 (02-07-2002) *whole document*	1-29

☐ Further documents are listed in the continuation of Box C.☒ See patent family annex.

* “A” “D” “E” “L” “O” “P”	Special categories of cited documents: document defining the general state of the art which is not considered to be of particular relevance document cited by the applicant in the international application earlier application or patent but published on or after the international filing date document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) document referring to an oral disclosure, use, exhibition or other means document published prior to the international filing date but later than the priority date claimed	“T” “X” “Y” “&”	later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art document member of the same patent family
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Date of the actual completion of the international search
08 February 2023 (08-02-2023)Date of mailing of the international search report
08 February 2023 (08-02-2023)Name and mailing address of the ISA/CA
Canadian Intellectual Property Office
Place du Portage I, C114 - 1st Floor, Box PCT
50 Victoria Street
Gatineau, Quebec K1A 0C9
Facsimile No.: 819-953-2476

Authorized officer

Jarret Diggins (819) 639-7846

INTERNATIONAL SEARCH REPORT
Information on patent family members

International application No.

PCT/CA2022/051667

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International application No.

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