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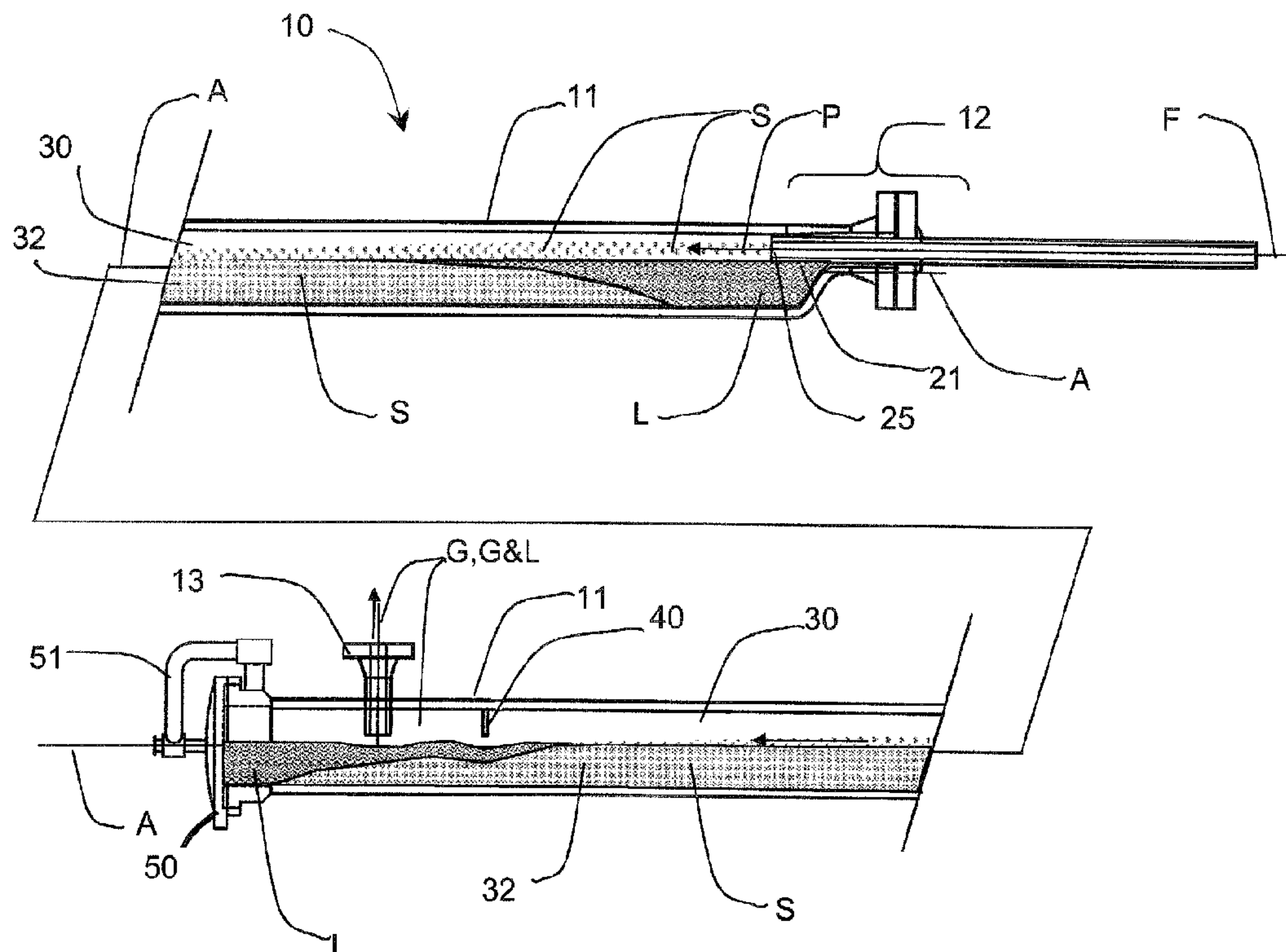
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(54) Titre : DISPOSITIF ET SYSTEME DE DESSABLAGE

(54) Title: DESANDING APPARATUS AND SYSTEM



(57) Abrégé/Abstract:

A desanding vessel is inserted in a high velocity fluid stream containing entrained particulates. The vessel comprises an upper freeboard portion having a large cross-sectional wherein the fluid stream velocity drops and particulates fall from suspension. Preferably the fluid stream is introduced offset upwardly from an axis of a horizontally oriented cylindrical vessel, released particulates falling to accumulate in a lower belly portion. The freeboard portion is maintained using a depending flow barrier adjacent the vessel's outlet which sets the depth of accumulation in the belly portion. A cleanout enables periodic removal of accumulations.



ABSTRACT OF THE INVENTION

1
2 A desanding vessel is inserted in a high velocity fluid stream
3 containing entrained particulates. The vessel comprises an upper freeboard
4 portion having a large cross-sectional wherein the fluid stream velocity drops and
5 particulates fall from suspension. Preferably the fluid stream is introduced offset
6 upwardly from an axis of a horizontally oriented cylindrical vessel, released
7 particulates falling to accumulate in a lower belly portion. The freeboard portion
8 is maintained using a depending flow barrier adjacent the vessel's outlet which
9 sets the depth of accumulation in the belly portion. A cleanout enables periodic
10 removal of accumulations.

1 **"DESANDING APPARATUS AND SYSTEM"**
2

3 FIELD OF THE INVENTION

4 The present invention relates to a system and apparatus for the
5 removal of particulates such as sand from fluid streams produced from a well
6 while minimizing abrasion of the involved equipment.

7
8 BACKGROUND OF THE INVENTION

9 Production from wells in the oil and gas industry often contain
10 particulates such as sand. These particulates could be part of the formation from
11 which the hydrocarbon is being produced, introduced particulates from hydraulic
12 fracturing or fluid loss material from drilling mud or fracturing fluids or from a
13 phase change of produced hydrocarbons caused by changing conditions at the
14 wellbore (Asphalt or wax formation). As the particulates are produced, problems
15 occur due to abrasion, and plugging of production equipment. In a typical startup
16 after stimulating a well by fracturing, the stimulated well may produce sand until
17 the well has stabilized, often up to a month after production commences. Other
18 wells may require extended use of the desander 10.

19 In the case of gas wells, fluid velocities can be high enough that the
20 erosion of the production equipment is severe enough to cause catastrophic
21 failure. High fluid stream velocities are typical and are even purposefully
22 designed for elutriating particles up the well and to the surface. An erosive failure
23 of this nature can become a serious safety and environmental issue for the well
24 operator. A failure such as a breach of high pressure piping or equipment
25 releases uncontrolled high velocity flow of fluid which is hazardous to service

1 personnel. Release to the environment is damaging to the environment resulting
2 in expensive cleanup and loss of production. Repair costs are also high.

3 In all cases, retention of particulates contaminates both surface
4 equipment and the produced fluids and impairs the normal operation of the oil
5 and gas gathering systems and process facilities.

6 In one prior art system, a pressurized tank ("P-Tank") is placed on
7 the wellsite and the well is allowed to produce fluid and particulates. The fluid
8 stream is produced from a wellhead and into a P-Tank until sand production
9 ceases. The large size of the P-Tank usually restricts the maximum operating
10 pressure of the vessel to something in the order of 1,000 – 2,100 kPa. In the
11 case of a gas well, this requires some pressure control to be placed on the well to
12 protect the P-Tank. Further, for a gas well, a pressure reduction usually is
13 associated with an increase in gas velocity which in turn makes sand-laden
14 wellhead effluent much more abrasive. Another problem associated with this
15 type of desanding technique is that it is only a temporary solution. If the well
16 continues to make sand, the solution becomes prohibitively expensive. In most
17 situations with this kind of temporary solution, the gas vapors are not conserved
18 and sold as a commercial product.

19 An alternate known prior art system includes employing filters to
20 remove particulates. A common design is to have a number of fiber-mesh filter
21 bags placed inside a pressure vessel. The density of the filter bag fiber-mesh is
22 matched to the anticipated size of the particulates. Filter bags are generally not
23 effective in the removal of particulates in a multiphase conditions. Usually
24 multiphase flow in the oil and gas operations is unstable. Large slugs of fluid
25 followed by a gas mist is common. In these cases, the fiber bags become a

1 cause a pressure drop and often fail due to the liquid flow therethrough. Due to
2 the high chance of failure, filter bags may not be trusted to remove particulates in
3 critical applications or where the flow parameters of a well are unknown. An
4 additional problem with filter bags in most jurisdictions is the cost associated with
5 disposal. The fiber-mesh filter bags are considered to be contaminated with
6 hydrocarbons and must be disposed of in accordance to local environmental
7 regulation.

8 Clearly there is a need for more versatile and cost effective system
9 of particulate handling.

10

11

SUMMARY OF THE INVENTION

12

Desanding apparatus is provided which is placed adjacent to a
13 well's wellhead for intercepting a fluid stream flow before prior to entry to
14 equipment including piping, separators, valves, chokes and downstream
15 equipment. The fluid stream can contain a variety of phases including liquid, gas
16 and solids.

17

In one embodiment, a pressure vessel is inserted in the flowstream
18 by insertion into high velocity field piping extending from the wellhead. The
19 vessel contains an upper freeboard portion having a cross-sectional area which is
20 greater than that of the field piping from whence the fluid stream emanates. As a
21 result, fluid stream velocity drops and particulates cannot be maintained in
22 suspension. A cross-sectional area of the freeboard portion is maintained
23 through a downcomer flow barrier adjacent the vessel's exit.

24

In a broad aspect, desanding apparatus vessel for removal of
25 particulates from a fluid stream containing particulates comprises: a fluid inlet

1 adjacent a first end of the vessel and adapted for receiving the fluid stream, the
2 fluid inlet discharging the fluid stream at an inlet velocity into a freeboard portion
3 at a top of the vessel, the fluid stream in the freeboard portion having an
4 elutriation velocity less than the inlet velocity and such that contained particulates
5 have a fall trajectory; a fluid outlet from the vessel, the outlet being spaced
6 horizontally from the inlet; and a flow barrier depending from the top of the vessel
7 and having a lower edge so as to direct the fluid stream below the barrier before
8 discharge from the outlet port for maintaining the freeboard portion above the
9 lower edge and forming a belly storage portion below the lower edge, the flow
10 barrier being positioned between the fluid inlet and fluid outlet and the flow barrier
11 being spaced from the fluid inlet so as to enable the fall trajectory of a substantial
12 amount of the particulates to intersect the belly portion so as accumulate
13 particulates in the belly portion prior to the flow barrier wherein the fluid stream at
14 the fluid outlet is substantially free of particulates.

15 Preferably, the flow barrier is a depending weir independent of the
16 outlet, or could be formed by the outlet itself. A cleanout port is preferably
17 included for periodic removal of accumulations of particulates.

18 More preferably, a vessel of an embodiment of the present
19 invention is incorporated in a desanding system to replace existing prior
20 connective piping, the vessel being supported using structure to align the vessel
21 with the wellhead piping and downstream equipment.

1 BRIEF DESCRIPTION OF THE DRAWINGS

2 Figure 1a is a schematic arrangement of connective wellsite piping
3 of the prior art;

4 Figure 1b is a schematic arrangement of one embodiment of the
5 invention having been installed in place of the prior connective wellsite piping of
6 Fig. 1a;

7 Figure 2a is an exploded view of the inlet to one embodiment of the
8 vessel of the invention which illustrates a nozzle arrangement in an eccentric
9 vessel inlet;

10 Figure 2b is an exploded view of the inlet to one embodiment of the
11 vessel of the invention which illustrates a nozzle arrangement adapted to a blind
12 flange;

13 Figure 3 is a cross-sectional side view of one embodiment of the
14 invention illustrating fluid streams, falling trajectory of particulates, and
15 accumulations of separated liquid, particulates and particulate-free fluid
16 discharge;

17 Figures 4a through 4c illustrate a variety of optional flow barriers
18 applied at the fluid outlet; and

19 Figure 5 is a performance graph of the achievable gas throughout
20 rates at various pressures while still achieving particulate removal for a
21 pessimistic case of a fluid stream containing fine 100 mesh sand.

22

23

1 DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

2 As shown in Figs. 1b and 3, a desander 10 comprises a
3 substantially horizontal, cylindrical pressure vessel 11 having a first fluid inlet end
4 12 adapted for connection to a fluid stream F such as from wellhead piping 9 and
5 a fluid outlet 13 connected to downstream equipment 14 such as multiphase
6 separators. The fluid stream F typically comprises a variety of phases including
7 gas G, some liquid L and entrained particulates such as sand S. The fluid stream
8 emanating from the fluid outlet 13 is typically liquid L and gas G, with a
9 substantial portion of the particulates S being captured by the desander 10. As a
10 system, the desander 10 is typically inserted as a replacement for existing piping
11 15 (shown in Fig. 1a). The desander 10 is preferably supported with structure 16
12 such as elevation adjustable jacks to align the desander 10 relative to the existing
13 wellhead piping 9 and downstream equipment 14.

14 With reference to Figs. 2a and 2b, the inlet 12 is fitted with a first
15 connector or inlet flange 20 so as to better facilitate installation, to allow easy
16 inspection for wear, to minimize equipment erosion and to simplify replacement
17 when erosion has reduced material thicknesses to acceptable minimums. A
18 nozzle 21 and a second connector or a nozzle flange 22 are adapted for
19 complementary and sealed connection to the inlet flange 20. Typically, the
20 nozzle 21 has a threaded inlet 23 which is adapted for threaded connection to an
21 existing coupling 24 from the wellhead piping 9. The nozzle inlet 23 is threaded
22 onto the coupling 24 and the vessel and inlet 12 is positioned over the nozzle 21
23 and the flanges 20,22 are connected.

24 In greater detail as shown in Figs. 2a,2b and 3, the nozzle 21 has a
25 protruding discharge portion 25 which extends adjacent the top of the vessel 11.

1 The inlet 12 is offset upwardly from an axis A of the vessel 11 and extends into
2 an upper freeboard portion 30. Preferably, as shown in Fig. 2a, an eccentric
3 fitting 31 is applied to the inlet 12. When coupled with the inlet flange 20 on the
4 eccentric fitting 31, the nozzle 21 is shifted upwardly from an axis A of the vessel
5 11. Similarly, as shown in Fig. 2b, the nozzle 21 can extend through a large
6 blind inlet flange 20 fit directly to the vessel 11 positioned so as to be shifted
7 upwardly from an axis A of the vessel 11. The nozzle 21 discharges the fluid
8 stream F along the nozzle's axis, a path P, substantially parallel to the vessel's
9 axis A. The nozzle inlet 23 is typically formed of heavy-wall piping to extend its
10 operational life in the abrasive environment of the particulate laden fluid stream F.
11 Further, the nozzle's discharge 25 protrudes into the vessel 11 sufficiently to
12 extend beyond the inlet 12 and into the freeboard portion 30, thereby aiding in
13 minimizing localized wear on the less easily replaced inlet 12, or eccentric fitting
14 31, of the vessel 11

15 In Fig. 3, the desander 10 further comprises belly portion 32,
16 formed below the freeboard portion 30, for receiving and temporarily storing
17 liquids L and sand S which separate from the fluid stream F. The fluid stream F
18 containing sand S enters through the inlet 12 and is received by a larger cross-
19 sectional area and substantially gas-phase volume of the freeboard portion 30.
20 Accordingly, the velocity of the fluid stream F slows to a point below the
21 entrainment or elutriation velocity of at least a portion of the particulates S in the
22 fluid stream. Those of skill in the art are able to determine and apply the
23 parameters of the fluid stream F, fluid stream velocity and those of the
24 particulates S so as to determine the elutriation characteristics. As the area of
25 the freeboard portion 30 increases, the velocity of the fluid stream F slows and a

1 lesser fraction of the particulates remain entrained; a greater fraction of
2 particulates S falling out of suspension from the fluid stream F. The particulates
3 S are discharged horizontally from the nozzle 21 along path P, and as they fall
4 from suspension, they adopt a downwardly curved trajectory under the influence
5 of gravity. Preferably, to avoid impingement-type erosion, the length of the
6 vessel is sufficient to permit the particulates to fall out of suspension before
7 impinging internals of the vessel 11. Given sufficient horizontal distance without
8 interference, the particulates S eventually fall from the freeboard portion 30 and
9 the trajectory intersects with the belly portion 32. The particulates S deposit and
10 accumulate over time in the belly portion 32. Typically, liquids L from the fluid
11 stream also collect in the vessel's belly portion 32.

12 The freeboard portion 30 is maintained using means such as a
13 depending flow barrier 40 to ensure that the collected liquids L and particulates S
14 only reach a maximum depth in the belly portion 32 of the vessel 11. A minimum
15 cross-section area of the freeboard portion and preferred length of the freeboard
16 portion 30 are determinable based on the elutriation characteristics and are
17 established so as to maximize release of the particulates S before they reach the
18 outlet 13. The greater the length or spacing between the inlet 12 and the flow
19 barrier 40, the greater is the opportunity to drop and release entrained
20 particulates S.

21 Typically, liquid L out of the fluid stream F accumulates in the belly
22 portion 32 to a steady state level and then is re-entrained for discharge with fluids
23 exiting the outlet 13 without affecting the capability of the vessel 11 and belly
24 portion 32 to continue to accumulate particulates S. Regardless of dropout of
25 liquids L from gas G and collection of liquid L in the vessel 11, this upper

1 freeboard portion 30 remains substantially gas-filled. However, should a
2 maximum depth of particulates S be reached during operation and encroach on
3 the freeboard portion 30, operations may yet continue as if the vessel 11 were
4 not even installed; both incoming liquid L and particulates S being temporarily re-
5 entrained with the fluid stream flowing from the vessel outlet 13 until the earliest
6 opportunity to perform maintenance. Typically the belly portion 32 vessel 11 is
7 periodically cleaned out or emptied of accumulated particulates and liquid at
8 sufficient intervals to ensure that the maximum accumulated depth does not
9 encroach on the freeboard portion 30. Maintenance and operations personnel
10 are further able to physically view sand production volumes during the cleanout
11 and inspection.

12 The flow barrier 40 depends downwardly from the top of the vessel
13 11. The flow barrier 40 has a lower edge 41 which sets the maximum depth of
14 the belly portion 32. As discussed above, the flow barrier 40 is preferably spaced
15 sufficiently from the inlet 11 to enable the fall trajectory of the particles to intersect
16 the belly portion 32 before impinging on the flow barrier 40 itself.

17 As shown in Figs. 4a-4c, the flow barrier 40 can comprise a discrete
18 or separate plate 40a,40b as shown in Figs. 4a and 4b, spaced from the outlet
19 13, or as shown in Fig. 4c, a flow barrier 40c can be formed by the outlet 13 itself.
20 All of the various flow barriers 40,40a,40b,40c have a lower edge 41 which forces
21 the fluid stream S thereunder before discharging from the vessel 11 at outlet 13.
22 Accumulated levels L,S encroaching above the lower edge 41 will result in high
23 velocities and re-entrainment of liquids L and particulates S from the area about
24 the flow barrier 40, inherently resulting in a steady state maximum level of
25 accumulation of the belly portion 32.

1 In the embodiment shown in some detail in Fig. 4c, the outlet 13 itself acts as the
2 flow barrier 40, which incorporates a tubular portion 43 protruding downwardly
3 and depending through the freeboard portion 30. The tubular portion 43 also has
4 a lower edge 41 spaced from the top of the vessel 11 which forces the fluid
5 stream F to exit from a point nearer the vessel axis A. Particulate-free fluid,
6 typically being gas G and some liquid L, is collected about the axis A for
7 discharge through the discharge tubing 40 and outlet 13. An advantage of
8 providing a separate flow barrier 40,40a,40b is that any abrasion and erosion is
9 borne by the barrier 40 and not by the outlet's 13 tubular portion 43.

10 As shown in Figs 4a,4c, the outlet 13 for the vessel 10 is preferably
11 arranged perpendicular to the axis A of the vessel 10 for further inertial rejection
12 of re-entrained particulates S.

13 Referring once again to Fig. 3, a quick release pressure-vessel
14 compatible cleanout 50 is provided for access to the vessel 11 for cleanout of the
15 accumulated particulates. The vessel must be depressurized before opening and
16 cleaning out particulates. Typically, mechanically-interlocked safety means 51
17 are provided so that the vessel must be de-pressurized before the cleanout can
18 be opened. For de-pressurization, the vessel is isolated from the fluid stream F
19 and pressure is bled off from the freeboard portion 30 until the cleanout 50 be
20 removed. As shown in Fig. 1b, a catch basin 52 or other suitable collection
21 means is provided for accepting the collected liquid L and particulates S. Manual
22 cleanout is performed although automated cleanout could be incorporated
23 without diverging from the intent of the invention.

1 EXAMPLES

2 A typical vessel according to the present invention, and for
3 reference are roughly approximated by the proportions of Fig. 3, can be a 6" or
4 an 8" diameter. Using an 8" diameter, schedule 160 shell for the vessel 11 can
5 result in a fluid stream capacity of about 8 million cubic feet of gas per day. A 2"
6 schedule 160 inlet nozzle extends about 1" beyond an eccentric inlet 12 and into
7 the vessel 11. With a flow barrier 40 placed about 8 feet from the nozzle
8 discharge 25, the desander 10 achieved a corresponding and typical collection
9 rate of 1.5 gallons of sand particulates per day, determined in a worst case
10 scenario of particles of about 100 mesh. Applied to problem wells in several
11 exceptional cases, using no vessel at all, one prior art wellhead, piping and
12 equipment experienced four breaches and in another case, seven breaches.
13 After installation of a preferred vessel of the present invention, no further
14 breaches were experienced. In one case, the resulting collection of particulates,
15 as sand, was about 5 liters per day.

16 Further, as shown in Fig. 5, the throughput capability of 8 inch and
17 10 inch diameter desanding vessels are illustrated for a variety of fluid pressures.

18 A system incorporating a desanding apparatus according to one of
19 the embodiments disclosed herein will benefit from advantages including: As a
20 desander 10 is more cost effective than a "P Tank", the desander can be
21 economically placed on a wellsite for long term sand protection (substantially
22 permanent as required); with a pressure rating that allows the vessel to operate
23 at the wellhead conditions, minimal pressure drop is experienced across the
24 vessel; the desander is designed to exceed ASME code for pressure vessels;
25 sand is removed from the fluid stream without erosive effects on the operator's

1 downstream equipment and; as the vessel is passive, having no moving parts,
2 plugging from particulates is not an issue; sand can be removed simply and
3 mechanically from the vessel at regular intervals; by removing the sand prior to it
4 entering the producing system, contamination of equipment and produced fluids
5 is avoided; and the desander is capable of handling multiphase production and
6 has demonstrated an ability to remove sand from both gas and oil streams. This
7 results in a wider application than prior art filter methods.

1 **THE EMBODIMENTS OF THE INVENTION FOR WHICH AN**
2 **EXCLUSIVE PROPERTY OR PRIVILEGE IS CLAIMED ARE DEFINED AS**
3 **FOLLOWS:**
4

5 1. A desanding vessel for removal of particulates from a fluid
6 stream containing particulates, comprising:

7 a fluid inlet adjacent a first end of the vessel and adapted for
8 receiving the fluid stream, the fluid inlet discharging the fluid stream at an inlet
9 velocity into a freeboard portion at a top of the vessel, the fluid stream in the
10 freeboard portion having an elutriation velocity less than the inlet velocity and
11 such that contained particulates have a fall trajectory;

12 a fluid outlet from the vessel, the outlet being spaced horizontally
13 from the inlet; and

14 a flow barrier depending from the top of the vessel and having a
15 lower edge so as to direct the fluid stream below the barrier before discharge
16 from the outlet port for maintaining the freeboard portion above the lower edge
17 and forming a belly storage portion below the lower edge, the flow barrier being
18 positioned between the fluid inlet and fluid outlet and the flow barrier being
19 spaced from the fluid inlet so as to enable the fall trajectory of a substantial
20 amount of the particulates to intersect the belly portion so as to accumulate
21 particulates in the belly portion prior to the flow barrier wherein the fluid stream at
22 the fluid outlet is substantially free of particulates.

23

24 2. The desanding vessel of claim 1 further comprising a cleanout
25 port for periodically accessing and removing particles accumulated in the belly
26 portion.

1 **3.** The desanding vessel of claim 1 or 2 wherein the flow barrier is
2 spaced from the fluid outlet.

3

4 **4.** The desanding vessel in any one of claims 1 to 3 wherein the
5 flow barrier further comprises a plate having a substantially horizontal lower edge
6 and the fluid outlet is located in the freeboard volume adjacent to the flow barrier
7 opposite the fluid inlet.

8

9 **5.** The desanding vessel in any one of claims 1 to 4 wherein the
10 flow barrier is formed by the fluid outlet, the fluid outlet further comprising a
11 tubular portion extending downwardly through the freeboard portion for forming
12 the flow barrier and terminating at the lower edge.

13

14 **6.** The desanding vessel in any one of claims 1 to 5 wherein the
15 vessel is cylindrical having a substantially horizontal axis, a top wall and a bottom
16 wall.

17

18 **7.** The desanding vessel of claim 6 wherein the cylindrical vessel
19 has a first end and a second end, and wherein the inlet port is located at the first
20 end and discharges the fluid stream into the freeboard portion along a fluid path
21 which is substantially parallel to the vessel's axis.

22

23 **8.** The desanding vessel of claim 7 wherein the inlet port is offset
24 above the vessel's axis.

1 **9.** The desanding vessel of claim 7 wherein the inlet port further
2 comprises:

3 an inlet flange;

4 a nozzle forming the fluid inlet; and

5 a nozzle flange for releasably connecting to the inlet flange.

6

7 **10.** The desanding vessel of claim 7 wherein the inlet port further
8 comprises an eccentric fitting positioned between the vessel and the inlet flange
9 for aligning the nozzle offset above the vessel's axis.

10

11 **11.** The desanding vessel in any one of claims 7 to 10 wherein
12 lower edge of the flow barrier depends below the inlet port.

13

14 **12.** The desanding vessel of claim 7 wherein the inlet port further
15 comprises:

16 a first connection at the first end of the vessel,

17 a second connection adapted for releasably and sealingly
18 connecting to the first connection, the second connection further comprising a
19 nozzle extending through the second connection, the nozzle having

20 a first end adapted for connection to the source of the fluid stream,

21 and

22 a second end protruding into the vessel for discharging the fluid
23 stream and particulates into the freeboard portion spaced inwardly from the first
24 end.

25

1 **13.**The desanding vessel of claim 12 wherein lower edge of the
2 flow barrier depends below the inlet port.

3

4 **14.**The desanding vessel in any one of claims 7 to 13 further
5 comprising a cleanout port for periodically accessing and removing particles
6 accumulated in the belly portion further comprising:

7 a cleanout connection at the second end of the vessel and aligned
8 with the belly portion; and

9 a cleanout cover for coupling with the cleanout connection and
10 operable between a sealed position and an open position for permitting removal
11 of particulates from the belly portion.

12

13 **15.**The desanding vessel of claim 2 or 14 further comprising
14 means for isolating the vessel from the fluid stream and de-
15 pressurizing the vessel before opening the cleanout port.

16

17 **16.**The desanding vessel in any one of claims 2, 14 or 15 further
18 comprising:

19 means for de-pressurizing the vessel before opening the cleanout
20 port.

21

1 **17.A** desanding system for adaptation to an existing wellhead
2 having a fluid stream flowing to downstream equipment and for the removal of
3 particulates from the fluid stream, comprising:
4 a vessel positioned between the wellhead and the downstream
5 equipment for intercepting the fluid stream;
6 a structure for supporting the vessel relative to the wellhead and
7 downstream equipment, wherein
8 the vessel comprises a fluid inlet adjacent a first end of the vessel
9 and adapted for receiving the fluid stream, the fluid inlet discharging the fluid
10 stream at an inlet velocity into a freeboard portion at a top of the vessel, the fluid
11 stream in the freeboard portion having an elutriation velocity less than the inlet
12 velocity and such that contained particulates have a fall trajectory, a fluid outlet
13 from the vessel, the outlet being spaced horizontally from the inlet; and a flow
14 barrier depending from the top of the vessel and having a lower edge so as to
15 direct the fluid stream below the barrier before discharge from the outlet port for
16 maintaining the freeboard portion above the lower edge and forming a belly
17 storage portion below the lower edge, the flow barrier being positioned between
18 the fluid inlet and fluid outlet and the flow barrier being spaced from the fluid inlet
19 so as to enable the fall trajectory of a substantial amount of the particulates to
20 intersect the belly portion so as to accumulate particulates in the belly portion
21 prior to the flow barrier wherein the fluid stream at the fluid outlet is substantially
22 free of particulates.
23

1 **18.**The desanding system of claim 17 wherein the vessel is
2 cylindrical and further comprises
3 a substantially horizontal axis, a top wall and a bottom wall;
4 a first end and a second end, and wherein the inlet port is located at
5 the first end and discharges the fluid stream into the freeboard portion along a
6 fluid path which is substantially parallel to the vessel's axis and offset above the
7 vessel's axis.

8
9 **19.**The desanding system of claim 17 or 18 wherein the inlet port
10 further comprises an eccentric fitting positioned between the vessel and the inlet
11 flange for aligning the nozzle offset above the vessel's axis.

12
13 **20.**The desanding system in any one of claims 17 to 19 further
14 comprising a cleanout port for periodically accessing and removing particles
15 accumulated in the belly portion further comprising:

16 a cleanout connection at the second end of the vessel and aligned
17 with the belly portion; and

18 a cleanout cover for coupling with the cleanout connection and
19 operable between a sealed position and an open position for permitting removal
20 of particulates from the belly portion.

21

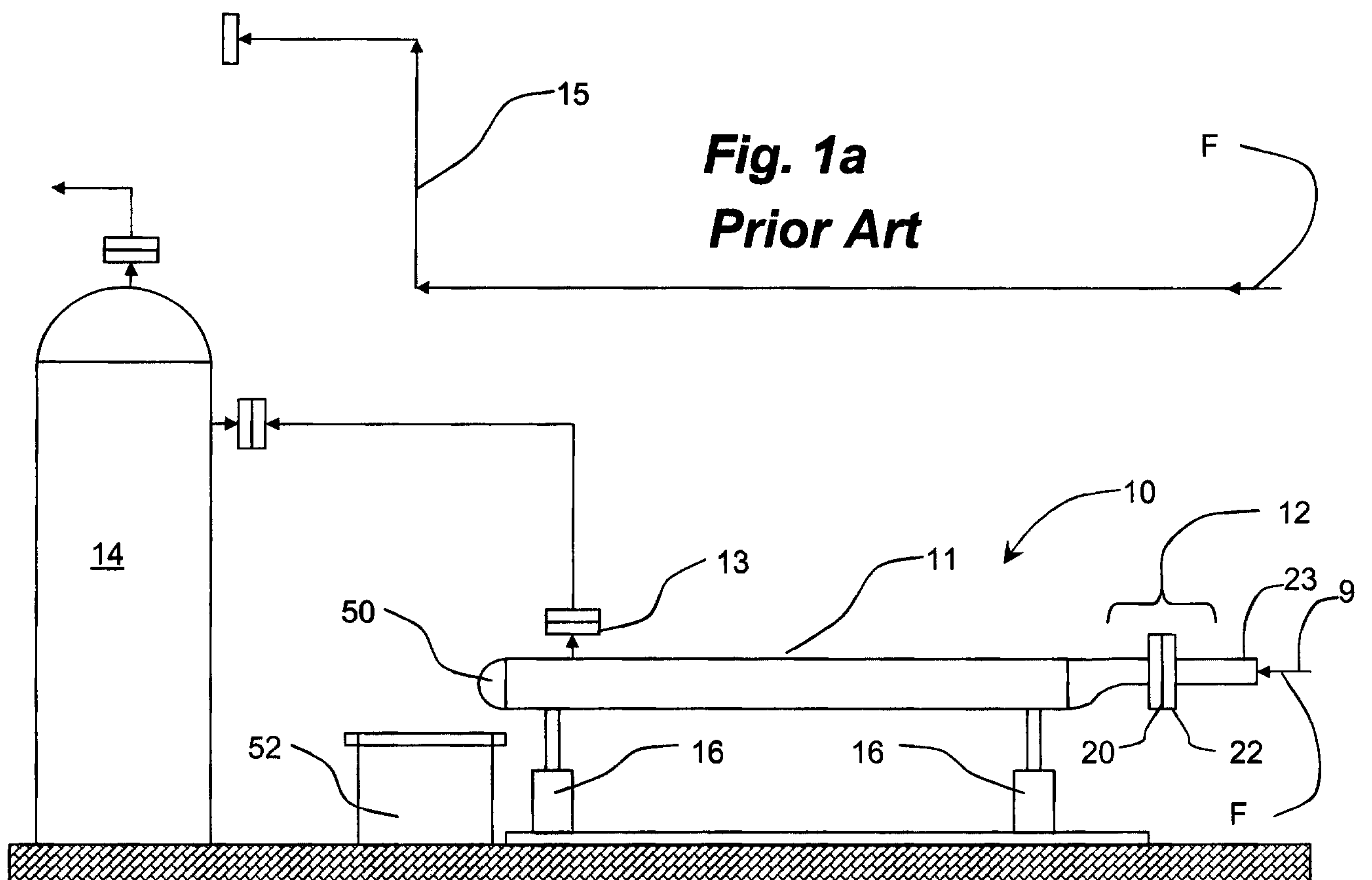
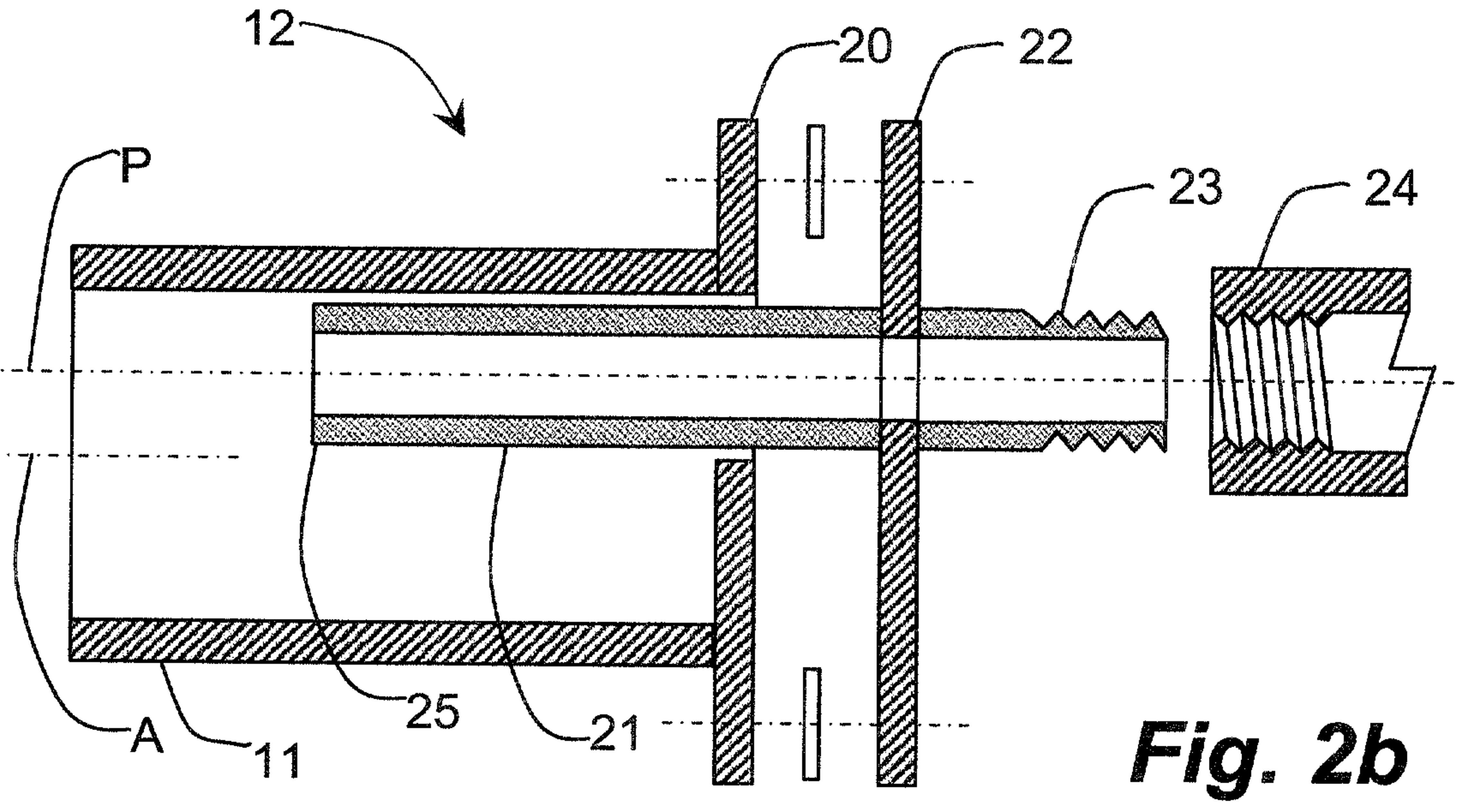
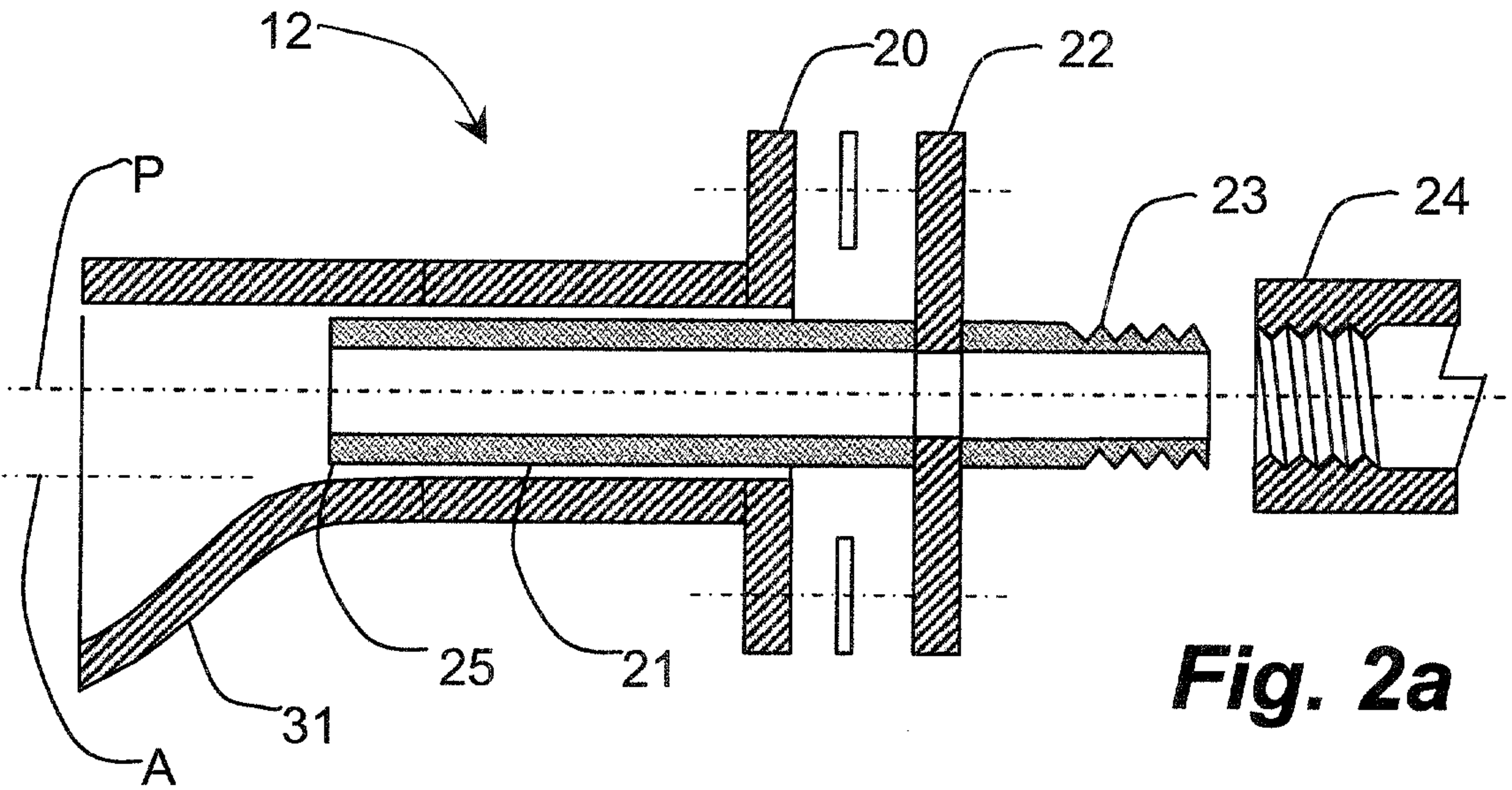


Fig. 1b



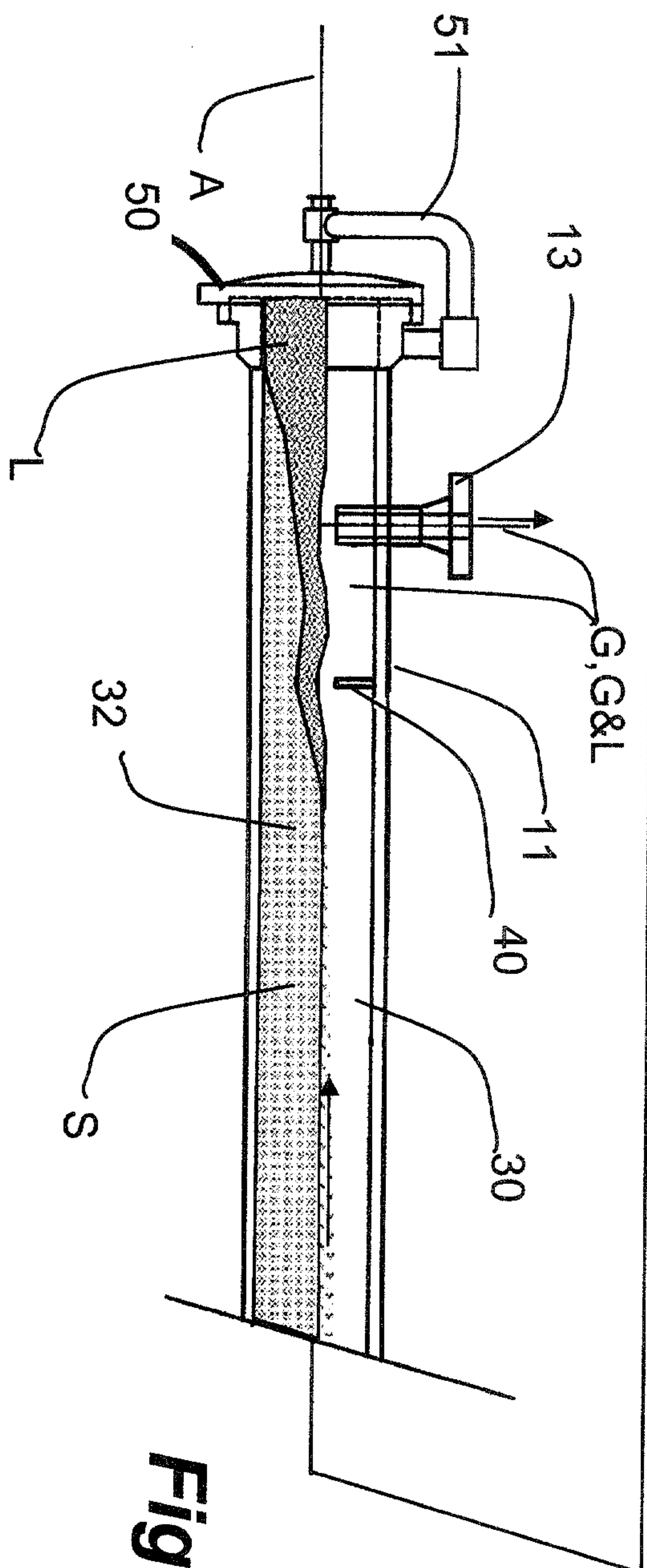
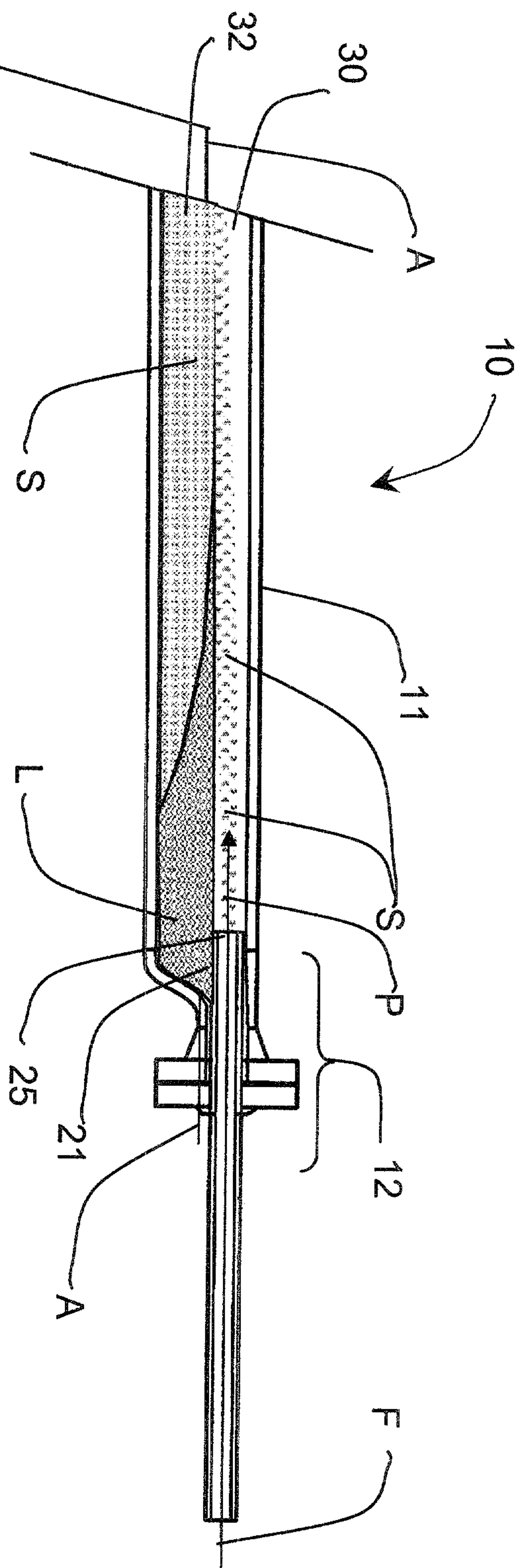


Fig. 3

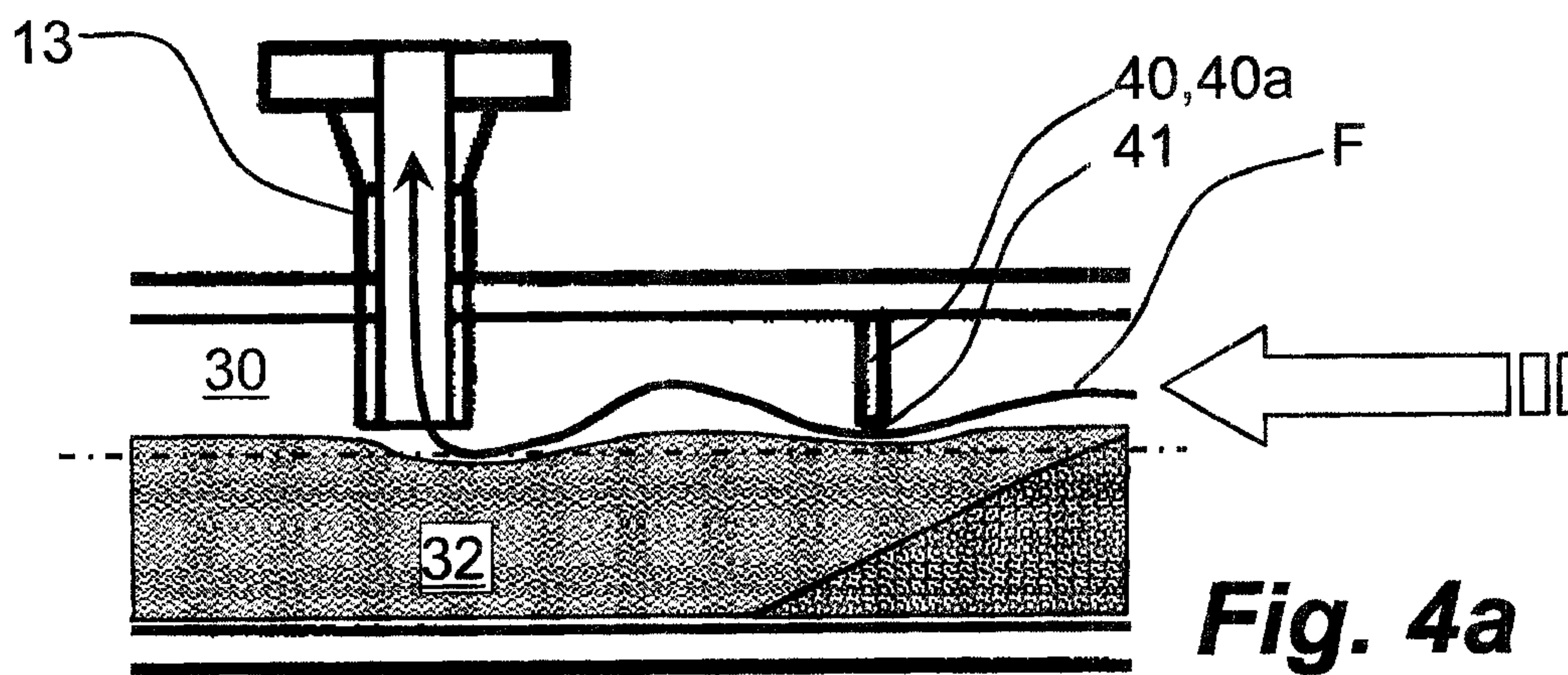


Fig. 4a

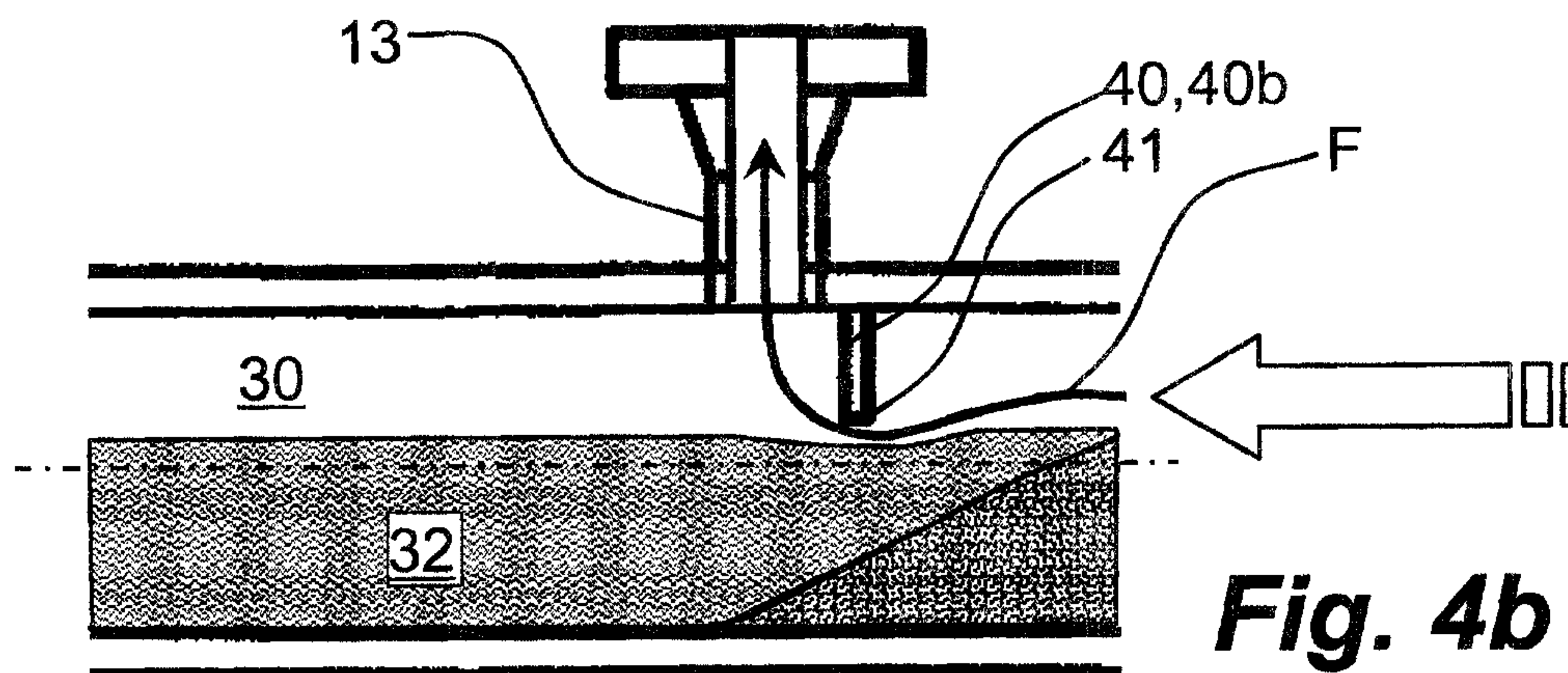


Fig. 4b

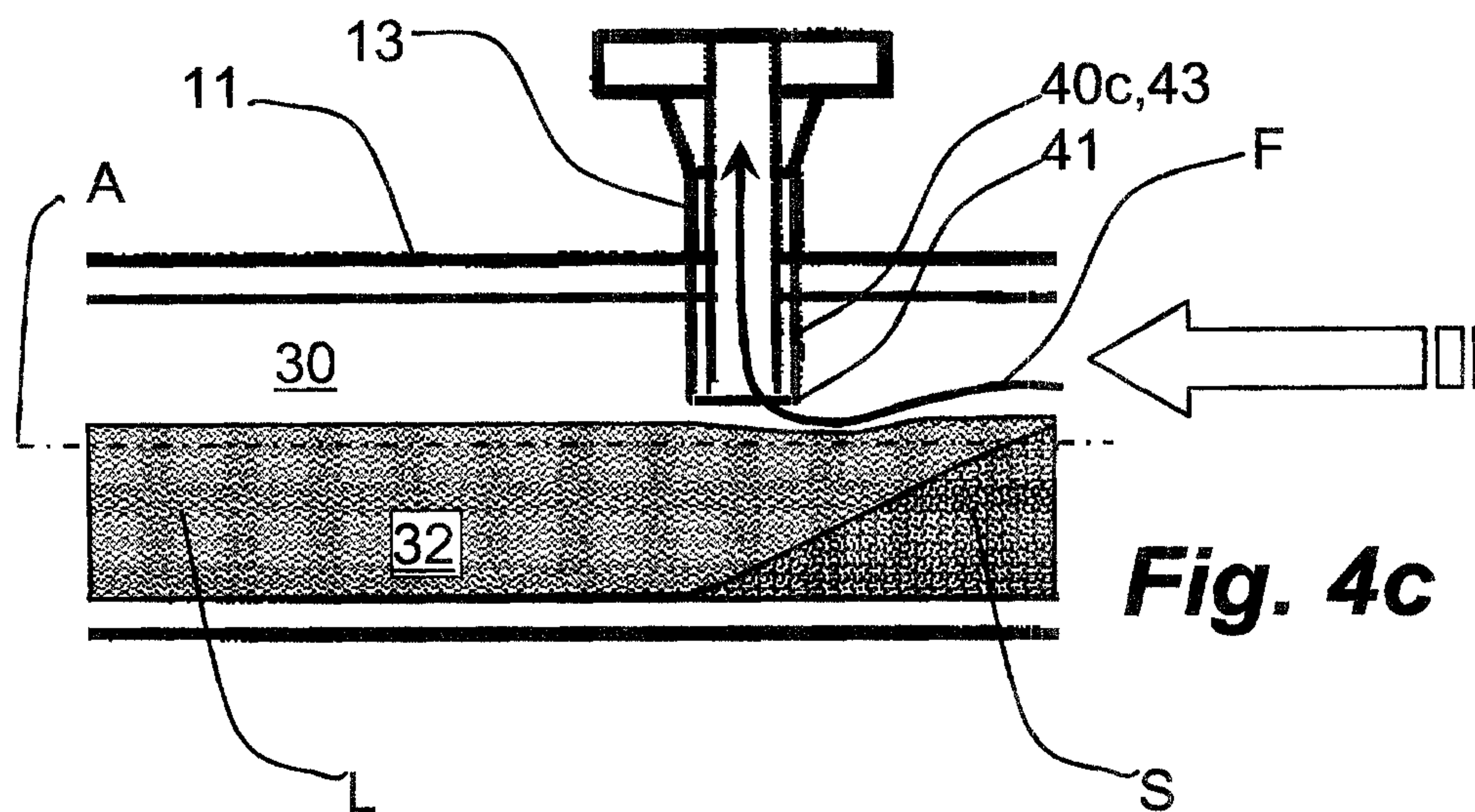


Fig. 4c

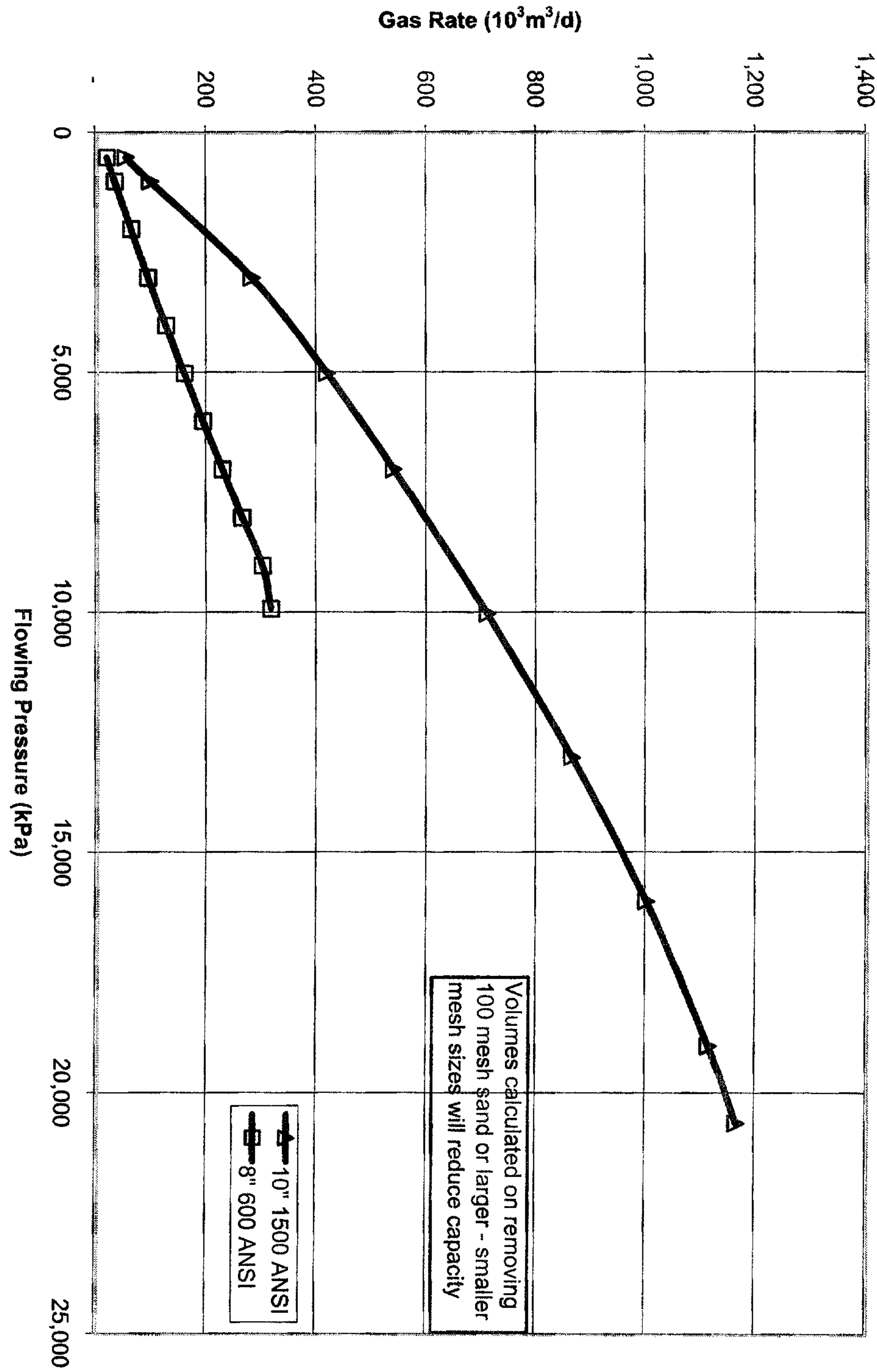


FIG. 5

