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[73]		Kop	py Tool Corporation	
	•		ndale, Mich.	
			tinuation-in-part of applic	
		627	,718, Apr. 3, 1967, now a	bandoned.
[54]	STRETCH	- I ME	THOD FOR MAKING A	TUBULAR
[54]	PRODUC	Г	Prawing Figs.	
[52]	U.S. Cl			29/155,
[22]			29/454, 64/11, 72/341, 72	
		,		113/116
[51]	Int. Cl			B23p 17/00
[50]	Field of Se	arch.		29/421,
	45	4, 16	3.5, 155 (C); 113/116 (B)	
			138/173; 74/492; 61/1	1;29/155 (C)
[56]			References Cited	
	J	JNIT:	ED STATES PATENTS	
1,05	7,098 3/1	913	Smith	(29/454UX)
1,10	5,539 7/1	914	Smith	(29/454UX)

1,602,449

1,617,857

10/1926

2/1927

Poe ..... (29/163.5UX)

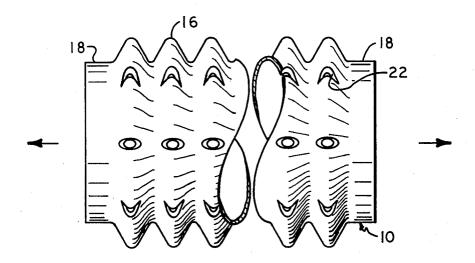
Mallory ...... (29/454UX)

2,032,555 2,083,943 2,371,991 2,800,321 3,326,091	6/1937 3/1945 7/1957	Ward Clifford Harding Jarret et al Allen	113/116(B) (29/454UX) 29/454X
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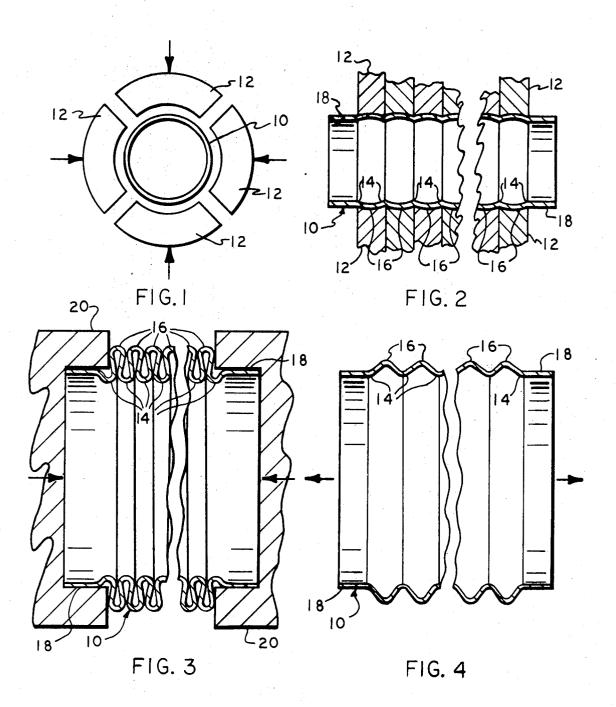
Primary Examiner—Charlie T. Moon Attorney—Hauke, Gifford & Patalidis

ABSTRACT: A tubular metal blank to be formed into a vehicle steering column or other corrugated tubular product is first deformed by radially inwardly moving dies to produce a plurality of substantially equally spaced shallow annular depressions separated by slightly raised crowns. The blank is then axially compressed to form and close a plurality of convolutions under a selected load within predetermined limits and to a selected closed length within predetermined limits, the variations being dependent on the strength of the material. Finally, the blank is stretched, expanding the convolutions to a plurality of generally similar spaced corrugations, with a selected stretch pressure within predetermined limits and to a selected expanded length within predetermined limits. If the end product is used as an energy-absorbing tube, the above method minimizes the variations in a selected compressive axial load required to collapse the finished column.

In another embodiment, a series of annularly spaced notches are cut in the convolutions after they have been compressed to abutting configuration to determine the hoop strains developed in the walls of the finished product corrugations when subjected to the axial collapse loading.



# SHEET 1 OF 3



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# SHEET 2 OF 3

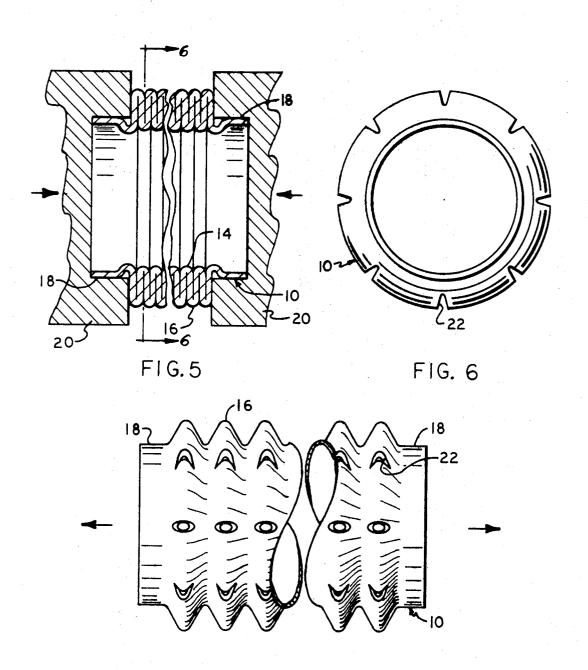


FIG. 7

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# SHEET 3 OF 3

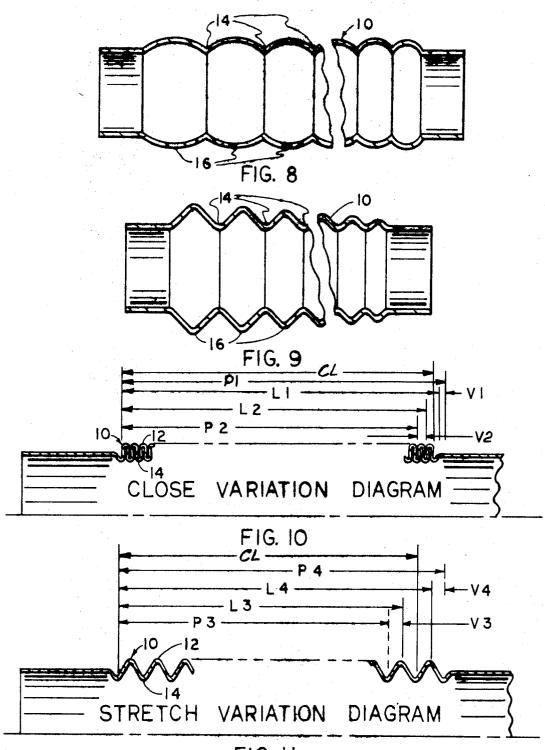


FIG. II

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# STRETCH METHOD FOR MAKING A TUBULAR PRODUCT

# CROSS REFERENCE TO RELATED APPLICATIONS

The present invention is a continuation-in-part of U.S. application Ser. No. 627,718, filed Apr. 3, 1967, now abandoned.

#### **BACKGROUND OF THE INVENTION**

# 1. Field Of The Invention

This invention relates to methods for making a tubular annularly corrugated member, and to a method of manufacturing an energy-absorbing tubular member having predictable collapsing characteristics when subjected to an axial compressive load.

2. Description of the Prior Art

Tubular members having axial collapsing characteristics are increasingly being employed as energy absorbing structural members in modern automotive vehicles to transmit torsional 20 or axial force between components attached to opposite end sections; for example, in the steering column of an automotive

When the impact of a collision or the like tends to throw the driver against the steering wheel or produce rearward dis- 25 placement of vehicle structure against the other end of the steering column, resultant forces will tend to collapse of the column. The driver of the vehicle when thrown against the steering wheel will experience a cushioned deceleration as the energy of his momentum is absorbed in the work required to 30 collapse the steering column. If forces against the lower end of the column cause it to collapse, this will prevent the steering wheel from being driven back against the driver.

There have been relatively few economical manufacturing techniques developed heretofor for producing a tubular 35 member having sidewalls which will collapse into a predictable pattern in reaction to a predetermined axial compressive force moving the ends of the tube walls toward one another. It is the broad purpose of the present invention to provide an improved method for producing a corrugated collapsible tube of 40 this character which is readily suitable in high-production manufacturing processes while at the same time producing a product having predictable energy-absorbing characteristics.

Further, in the manufacture of corrugated tubing generally, there have been no methods heretofor developed for economically and easily controlling the length and strength characteristics of the finished product.

# SUMMARY OF THE INVENTION

In the preferred embodiment of the present invention, a selected section of a tubular blank for use as a vehicle steering column or other corrugated tubular product is first deformed by the use of radially inwardly moving dies or the like to provide a plurality of substantially equally spaced shallow annular 55 depressions separated by slightly raised annular crowns, this deformation being a factor which will determine both the number and the volumes of convolutions to be formed in the second step.

The ends of the blank are retained in press mandrels and the 60 deformed section is axially compressed so that the deformations fold in accordion fashion to form a plurality of annular and adjacent closed convolutions. The pressure necessary to close these convolutions, and the length of the section after closing, will be dependent on the material strength of the wall 65 of the blank, so that the selected load and length will vary within predetermined limits.

Next, the convoluted section is stretched to partially unfold the convolutions, forming an annularly corrugated section, under a stretch pressure which will vary between minimum 70 and maximum limits and to a length which will also vary between minimum and maximum limits, the actual stretch pressure and the actual finished length again being determined by the strength of the material. However, proper balancing of the stretch pressure and length variations will produce a 75 the finished corrugated length;

finished product having a proper length within allowable tolerances and will be such that a predictable axial compressive force encountered in the event of a collision or the like will cause controlled collapse of the corrugated section, so that it can act predictably as an energy-absorbing device for use as a vehicle steering column or the like. For any axial forces below that predicted, the column will be substantially rigid and capable of performing in its intended fashion as, for 10 example, in steering the vehicle.

In a collision or the like, if the vehicle driver is thrown against the steering wheel with sufficient force, or if vehicle structure buckles to exert such forces against the lower end of the steering column, it will then collapse, the kinetic energy producing the collapse being absorbed in the work of deforming the corrugations as the tube ends approach one another. The rate at which the opposite tube ends move toward one another is related to the circumferential or hoop strains developed in the annular ridges of the corrugations.

In an optional method of forming, the blank is compressed further in the second step to flatten the annular walls of the adjacent convolutions against each other. Then, before stretching, a series of annularly spaced notches are cut across the outer periphery of the collapsed convolutions. The final tubular section after stretching then has a pattern of apertures in the partially unfolded corrugations which reduce the magnitude of the hoop stresses, depending on the depth and number of notches, thereby reducing the magnitude of the axial force required to initiate the collapsing movement This step provides a means for additionally closely controlling the axial strength of the tube. The walls of the corrugations in this type of tube will take a more angular configuration than in the previously described embodiment.

The preformed tubular blank may be deformed into a series of annular corrugations successively having gradually reduced major diameters. This can be done by spacing the preliminary depressions, formed in the first die operation, successively closer from one end to the other. Thus, the corrugations of the finished tubular member will tend to collapse in a progressive pattern as distinguished from a random or uncontrolled pattern which would be the case with equally spaced corrugations.

It is therefore a general object of the present invention to provide a method for making a tubular product having a predictable collapsing characteristic by applying a compressive axial force to a tubular blank sufficient to move the opposite ends of the blank toward one another so that the tube wall collapses into a predetermined convoluted pattern and then applying a selected tensile axial force within limits to the collapsed blank so that the convoluted section is partially unfolded to a selected axial length within limits.

Further objects and advantages of the present invention will be apparent to one skilled in the art to which the invention pertains upon reference to the following detailed description.

### DESCRIPTION OF THE DRAWINGS

A more complete understanding of the invention may be had by reference to the accompanying drawings illustrating preferred embodiments of the invention in which like reference characters refer to like parts throughout the several views and in which:

FIG. 1 is a diagrammatic cross-sectional view illustrating a preferred method of preforming a tubular blank;

FIG. 2 is a longitudinal cross-sectional view illustrating the preforming operation;

FIG. 3 is a longitudinal cross-sectional view illustrating the step of applying an axial compressive force to collapse the wall of the preformed tubular blank into a convoluted configura-

FIG. 4 is a longitudinal cross-sectional view illustrating the step of stretching and partially unfolding the convolutions to

FIG. 5 is a longitudinal cross-sectional view illustrating an alternative step of fully collapsing the convolutions formed in the tubular blank;

FIG. 6 is a cross-sectional view taken substantially on the line 6-6 of FIG. 5 and illustrating the collapsed tubular blank provided with a series of annularly spaced notches;

FIG. 7 is a longitudinal elevational view illustrating the tubular section of FIG. 5 after stretching;

FIG. 8 is a longitudinal cross-sectional view showing a tubular blank initially deformed to provide progressively closer spaced depressions;

FIG. 9 is a longitudinal cross-sectional view showing the blank of Flg. 8 after compression and expansion to its final form:

FIG. 10 is a close variation diagram for the collapsed tubular section; and

FIG. 11 is a stretch variation diagram for the expanded tubular section.

#### DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring first to FIGS. 1 and 2, the preferred method of practicing the first step of invention comprises providing a tubular metal blank 10 having sidewalls deformed so that the application of an axial compressive force on the opposite ends 25 causes the blank 10 to collapse in a predetermined pattern. For purposes of illustration, the preformed blank 10 is made by radially converging a set of dies 12 thereon to simultaneously engage the outer wall surface and deform it into a continuous series of shallow annular depressions 14 substantially equally spaced by slightly raised annular crowns 16. Preferably the dies 12 deform the sidewalls of the blank 10 in a single stroke. The compressive force applied by the dies 12 is sufficient to deform the walls of the tube 10 as shown, but insufficient to produce a thinning or uneven metal forging of the

The blank 10 is preferably formed with undeformed end sections 18. The next step comprises applying by means of press mandrels 20 an axial compression to the end sections 18 40 sc that they are forced toward one another as indicated by the directional arrows of FIG. 3, causing the crowns 16 to radially enlarge as they fold about their major diameter and move axially toward one another until they abut to form the plurality of convolutions as shown, having substantially equal volumes, 45 the depressions 14 forming similar inner diameter convolutions as shown.

Next, as shown in FIG. 4, a stretch pressure is applied to the opposite end sections 18 of the blank 10 so that they are pulled away from one another, partially unfolding the con- 50 lapse load, volutions until they assume the predetermined corrugated configuration indicated.

The stretch pressure used to expand the blank to its finished form will be the determining factor in predetermining that force which will produce a controlled collapse if the column is later subjected to impacts from a collision or the like, and the way in which stretch pressure and length variations are balanced to minimize collapse load variations will be explained in relation to FIGS. 10 and 11.

FIGS. 5, 6 and 7 illustrate an alternative method of practicing the invention to additionally control the magnitude of the hoop strains developed in each of the corrugations when the tubular member 10 is subjected to an axial collapsing force. As shown in FIG. 5, the convolutions formed from the crowns 65 16 are completely collapsed by compressing of the press mandrels 20 until the adjacent convolute surfaces are in full faceto-face abutment and disposed substantially in a plane normal to the axis of the blank 10.

While the blank 10 is so compressed, a series of preferably 70 equally annularly spaced notches 22 are cut across the outer peripheries of each convolution by any suitable cutting tool to a predetermined radial depth as shown in FIG. 6. The notches 22 provide a series of discontinuities in the convolutions which radially enlarge when the expanding stretch pressure is 75 of close and stretch pressures, within tolerable limits.

applied to the tube 10 in the final forming step. Thus, by carefully selecting the number of notches 22 and the depth to which they are cut, a further control over the predetermined force necessary to initiate collapse of the finished column is available.

The blank 10 is finally axially stretched and takes the configuration shown in FIG. 7 after the notching step to produce a finished column similar to that illustrated in FIG. 4, but with a carefully selected pattern of apertures provided in the corrugations, which in the present case are of a more angular na-

FIG. 8 illustrates in exaggerated form another preferred method of forming a blank 10 in which the shallow annular depressions 14 are spaced successively closer from left to right by forming progressively axially shorter raised crowns 16. After the compression and the expansion steps, the successive corrugations from left to right will consequently have progressively smaller volumes as seen in FIG. 9 and will vary in their resistance to collapse if later subjected to the axial forces resulting from impacts of collision or the like. In such event the corrugations will collapse progressively from the relatively weaker corrugations on the left to the relatively stronger corrugations on the right. In actual practice, the difference in spacing of successive depressions will be very slight but for clarity the drawing illustrates rather radical successively diminishing spacings, and the depressions and intermediate crowns are of exaggerated radial dimensions.

FIG. 10 is a close variation diagram showing the compressed blank 10 of FIG. 3 in which:

C<sub>L</sub> is the center length relative to the left end of the compressed blank section to which a mean material would compress at a selected close pressure,

P<sub>i</sub> is the length to which the strongest material could be compressed at such selected close pressure,

P<sub>2</sub> is the length to which the weakest material could be compressed at such selected close pressure,

L<sub>1</sub> is the maximum length to which the strongest material will actually be compressed,

L<sub>2</sub> is the minimum length to which the weakest material will actually be compressed.

V<sub>1</sub> is the differential between the P<sub>1</sub> and L<sub>1</sub> lengths, and  $V_2$  is the differential between the  $P_{2 \text{ and } L2}$  lengths.

FIG. 11 is a stretch variation diagram showing the finally expanded blank 10 of FIG. 4 in which:

C<sub>L</sub> is the length relative to the left end of the expanded blank section to which a means material would be expanded at a selected stretch pressure to predetermine the desired col-

P<sub>3</sub> is the length to which the strongest material could be expanded at such selected stretch pressure,

P4 is the length to which the weakest material could be expanded at such selected stretch pressure,

L<sub>a</sub> is the minimum length to which the strongest material will actually be expanded,

L4 is the maximum length to which the weakest material will actually be expanded,

V<sub>3</sub> is the differential between the P<sub>3</sub> and L<sub>3</sub> lengths, and V<sub>4</sub> is the differential between the P<sub>4</sub> and L<sub>4</sub> lengths.

Since L<sub>3</sub> and L<sub>4</sub> are balanced about C<sub>L</sub>, collapse load variations will thus be minimized.

It will be apparent that, to establish this desired collapse load as an inherent characteristic of the finished product, the close and stretch pressures will be determined on development over a full range of material variables, with the convoluted length variations chosen to compensate for the physical variations of different blank materials, thus minimizing collapse load variables.

Depending on the material uses, the finished length of the blank can be predetermined within allowable tolerances, and that force which will be required to produce a controlled collapse of the column can be predetermined by proper selection The above described system for determining pressures and lengths is an economical method for developing a tubular product to be used as a vehicle steering column with walls having a carefully controlled axial strength.

Although I have described only a few embodiments of my invention, it is to be understood that various changes and modifications can be made therein without departing from the spirit of the invention as expressed in the scope of the ap-

pended claims.

1. A method for making a tubular member, comprising the steps of:

 a. providing a tubular blank with an intermediate section deformable symmetrically about its axis into a predictable number of longitudinally adjacent corrugations,

b. applying a selected axial compression force within predetermined limits to said section deforming same into adjacent annular convolutions; and to move the adjacent convolutions into close face to face contact to form substantially flat abutting wall sections,

 c. cutting out annularly spaced notches across the adjacent annular convolutions at such time as the wall sections of the annular adjacent convolutions are in abutting contact;

d. subsequently applying a predetermined axial tension to said convoluted section to partially expand said convoluted section to an approximately selected finished corrugated length, whereby on applying said axial tension expansion said convolutions of said wall sections will take substantially equal angular positions relative to the tube axis and will meet to form angular edges having alternate 30 lesser and greater diameters.

2. The method as defined in claim 1 wherein the predetermined tension is selected within minimum and maximum limits to substantially predetermine the compressive axial load which would subsequently be required to collapse said section 35

when used as an energy absorbing column.

3. The method as defined in claim 1 wherein the step of providing said tubular blank with a deformable intermediate section comprises converging preformed dies radially inwardly on said section to impress on said blank a plurality of axially spaced shallow annular depressions separated by slightly raised annular crowns thereby defining the number and volumes of the later formed corrugations.

4. The method as defined in claim 1 wherein the step of applying axial compression comprises applying a selected compressive force within predetermined limits to move the adjacent convolutions into contact to form alternate radially in-

wardly and outwardly facing annular looped wall sections having respectively lesser and greater diameters.

5. The method as defined in claim 1 and in which the number and extent of said notches controls the circumferential hoop strains in said corrugations to predetermine that axial compressive force which would later be required to collapse said section when used as an energy-absorbing column.

6. A method for making a tubular member of selected

10 material comprising the steps of:

 a. preforming a tubular blank to predetermine the number and volumes of to be formed annular convolutions,

b. axially compressing said blank under a selected closing load within predetermined limits and to a selected closed length within predetermined limits, the variation depending on the strength of the material, to form a plurality of adjacent annular convolutions, the selected closing load being sufficient to flatten said convolutions such that when said convolutions are later expanded, corrugations formed by such expansion will meet at annular substantially sharp angles,

 c. cutting a selected number of annularly spaced notches to selected depths across the outer diameters of the flat-

tened convolutions,

d. subsequently axially stretching said blank with a selected stretch pressure within predetermined limits and to a selected expanded lengths within predetermined limits, the variations depending upon the strength of the material, to partially unfold the convolutions forming a plurality of adjacent annular corrugations, said expanded member having apertures formed by said last-mentioned cutting step in which said apertures reduce the hoop strains of said corrugations to predetermined values when subjected to a collapse load.

7. The method as defined in claim 6 wherein the preforming step comprises forming a plurality of shallow annular depressions in said blank spaced by slightly raised annular crowns.

8. The method as defined in claim 7 wherein said depressions are equally spaced whereby the later formed convolutions will be of substantially equal dimensions.

The method as defined in claim 7 wherein said depressions are unequally spaced whereby the later formed convolu-

tions will be of different diameters.

10. The method as defined in claim 9 wherein said depressions are successively lesser spaced from one end to the other of said blank.

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