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(74) Common Representative: SIEMENS AKTIENGESELLSCHAFT; Postfach 22 16 34, 80506 München (DE).

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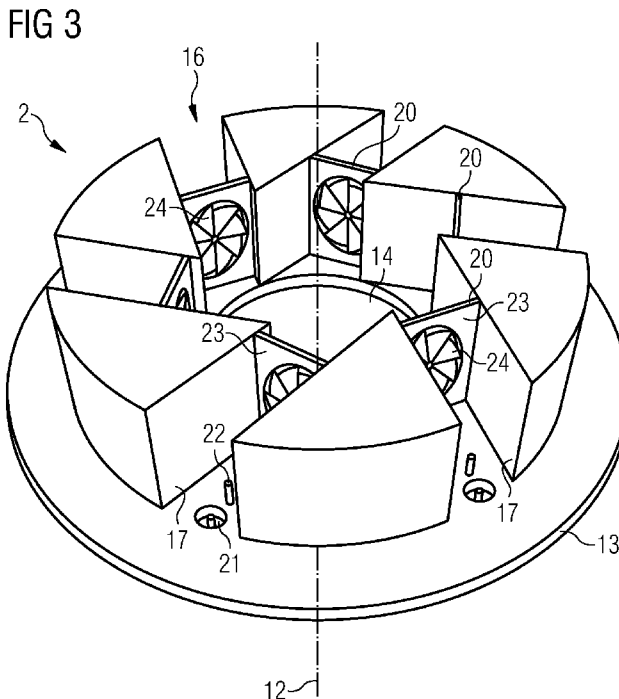
(71) Applicant (for all designated States except US): SIEMENS AKTIENGESELLSCHAFT [DE/DE]; Wiltelsbacherplatz 2, 80333 München (DE).

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(72) Inventor; and
(75) Inventor/Applicant (for US only): LIU, Kexin [GB/GB]; 116 Grantham Road Bracebridge Heath, Lincoln LN4 2QF (GB).

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(54) Title: SWIRLER, COMBUSTION CHAMBER, AND GAS TURBINE WITH IMPROVED SWIRL



(57) Abstract: The invention is directed to a swirler (2) for mixing fuel (25, 26) and air (6), a combustion chamber, and a gas turbine, the swirler (2) comprising a plurality of vanes (15) positioned radially around a central axis (12) of the swirler (2) and comprising a plurality of mixing channels for mixing fuel (25, 26) and air (6). At least one mixing channel (16) of the plurality of mixing channels is defined by opposite walls (17) of two adjacent vanes of the plurality of vanes (15) and is comprising at least one fuel injection opening (21, 22) arranged at an upstream sections of the at least one mixing channel (16). Furthermore the at least one mixing channel (16) is also comprising an axial swirler (20) arranged at a downstream section of the at least one mixing channel (16).

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Description

Swirler, Combustion Chamber, and Gas Turbine with improved
swirl

5

FIELD OF THE INVENTION

The invention relates to a swirler, particularly of a gas
turbine, and improvements for the further diminishment of air
10 pollutants such as nitrogen oxides (NO_x).

BACKGROUND OF THE INVENTION

In a gas turbine burner a fuel is burned to produce hot
15 pressurised exhaust gases which are then fed to a turbine
stage where they, while expanding and cooling, transfer
momentum to turbine blades thereby imposing a rotational
movement on a turbine rotor. Mechanical power of the turbine
rotor can then be used to drive a generator for producing
20 electrical power or to drive a machine. However, burning the
fuel leads to a number of undesired pollutants in the exhaust
gas which can cause damage to the environment. Therefore, it
takes considerable effort to keep the pollutants as low as
possible. One kind of pollutant is nitrogen oxide (NO_x). The
25 rate of formation of nitrogen oxide depends exponentially on
the temperature of the combustion flame. It is therefore
attempted to reduce the temperature over the combustion flame
in order to keep the formation of nitrogen oxide as low as
possible.

30

There are two main measures by which reduction of the
temperature of the combustion flame is achievable. The first
is to use a lean stoichiometry with a fine distribution of

fuel in the air, generating a fuel/air mixture with a low fuel fraction. The relatively small fraction of fuel leads to a combustion flame with a low temperature. The second measure is to provide a thorough mixing of fuel and air before the combustion takes place. The better the mixing, the more uniformly distributed the fuel is in the combustion zone and the fewer regions exist where the fuel concentration is significantly higher than average. This helps to prevent hotspots in the combustion zone which would arise from local maxima in the fuel/air mixing ratio. With a high local fuel/air concentration the temperature will rise in that local area and so does as a result also the NO_x in the exhaust.

Modern gas turbine engines therefore use the concept of premixing air and fuel in lean stoichiometry before the combustion of the fuel/air mixture. Usually the pre-mixing takes place by injecting fuel into an air stream in a swirling zone of a combustor which is located upstream from the combustion zone. The swirling leads to a mixing of fuel and air before the mixture enters the combustion zone.

GB 2334087 A is addressing the specific problem to improve the fuel to air ratio during start-up of a "lean burn" combustor. A combustor comprises a swirler with at least one restrictor to restrict the flow of fluid through the combustor. Preferably the restrictor may be biased or switched between restricting and non-restricting positions depending on the pressure of the airflow. This may optimise the fuel/air mixture. On the other hand the restrictors may cause dead zones in which the airflow is unstable and stagnant with a possibility that flashbacks may occur.

From US patent US 6,192,669 B1 it is known to arrange a plurality of burners, operatively connected to each other, in such a way, so that a swirl flow is initiated in a common combustion chamber which ensures the stability of the flame front. This is advantageous because this may to low pollutant emissions, e.g. NO_x, at part load.

US patent application US 2006/0257807 A1 discloses a combustor with a swirler. Circular mixing ducts may be applied to a radial type swirler. This is advantageous due to the absence of corners where excessive fuel could get trapped.

With respect to the mentioned state of the art it is an object of the invention to provide a swirler, in particular a swirler in a gas turbine combustion chamber, a combustion chamber equipped with such a swirler, and a gas turbine having a plurality of such combustion chambers, so that mixing fuel and air in a swirling area is improved by providing a homogenous fuel/air mixture, especially at all possible loads of the gas turbine.

SUMMARY OF THE INVENTION

This objective is achieved by the independent claims. The dependent claims describe advantageous developments and modifications of the invention.

In accordance with the invention there is provided a swirler for mixing fuel and air comprising a plurality of vanes positioned radially around a central axis of the swirler and comprising a plurality of mixing channels for mixing fuel and air. At least one mixing channel of the plurality of mixing

channels is defined by opposite walls of two adjacent vanes of the plurality of vanes. The at least one of the plurality of mixing channels is comprising at least one fuel injection opening arranged at an upstream sections of the at least one
5 mixing channel and is comprising an axial swirler arranged at a downstream section of the at least one mixing channel.

Furthermore the invention is also directed at components comprising such a swirler, particularly a combustion chamber
10 of a gas turbine. Furthermore the invention is also directed to a gas turbine comprising at last one of such a combustion chamber.

The inventive swirler is advantageous because the axial
15 swirler provides an extra swirl, so that the fuel to air mixture is more homogenous.

Advantageously, the plurality of swirler airfoils may be arranged to provide a mixing channel individual rotating
20 airflow for the at least one of the plurality of mixing channels.

Specifically the plurality of vanes may be configured that way that the mixed fuel and air mixture generates a swirl
25 around the central axis of the swirler. The axial swirler preferably provides a rotational movement around the lateral axis of the mixing channel, to which the axial swirler is applied. As a result, from each mixing channel such rotating fuel/air mixture is entering a radially inner part of the
30 swirler, in which the rotation around the swirler axis is initiated. Thus, several fuel/air streams with rotational movement - generated by the axial swirlers - along the lateral movement in direction of the mixing channels, get

further mixed by the swirler resulting in an overall rotational movement along the central axis of the swirler. This results in an improved fuel to air mixture.

5 The mixing channel is a passage for fuel and air. The direction of this passage is defined by the orientation of the walls of the two adjacent opposite walls. Preferably the orientation of the walls is that way that - also ignoring the effect of the axial swirlers that are located in the mixing
10 channels - the fuel and air will progress towards a central area of a swirler or burner and enter that central area slightly off the exact centre, so that the overall movement of the fuel and air will result in a corkscrew like movement around the central axis of the swirler or burner. Preferably
15 the central axis of the swirler may be the same as the central axis of a burner, to which the swirler is applied.

Still ignoring the effect of the axial swirlers that are located in the mixing channels, the rotation of this
20 corkscrew like movement may however be slower than the mean velocity by which the flow is traveling. This phenomenon is caused by the fact that the flow is turning, given a more tangential path around the central axis of the burner, which gives rise to a pressure difference between the neighbouring
25 two swirler vanes in the flow passage.

In a preferred embodiment the axial swirler may extend between the walls of the two adjacent vanes. Preferably the axial swirler stretches over the complete cross section of
30 the mixing channel through which is fuel and air mixture flows, so that advantageously all of the fuel and air mixture will pass the axial swirler. In an alternative embodiment a fraction of the fuel and air mixture may bypass the axial

swirlers. This may occur, if the axial swirler does not extend over the complete cross section of the mixing channel.

5 In a further preferred embodiment the axial swirler may be arranged substantially perpendicular to the walls of the two adjacent vanes. This may result in a more symmetric swirl without any non-uniform turbulence. In an alternative construction the axial swirler may be in an angle different from 90 degrees in relation to the walls of the two adjacent
10 vanes. If the walls of the two adjacent vanes are not in parallel, the axial swirler may be arranged so that it is substantially perpendicular in relation to the main flow direction within the mixing channel. Again, in an alternative solution, the angle may also be different from 90 degrees in
15 relation to the main flow direction within the mixing channel.

In another preferred embodiment the axial swirler may have a plurality of swirler airfoils. The airfoils may be baffles to
20 redirect the fuel/air stream and provide an additional rotational movement to the fuel/air stream passing the mixing channel. This may result in a corkscrew like movement at the end of the mixing channel.

25 In a further embodiment the axial swirler may have a rectangular solid frame surrounding the plurality of swirler airfoils. Advantageously the shape of the frame matches the cross section of the mixing channel.

30 In yet another embodiment, the plurality of swirler airfoils may have an elliptic, particularly circular, outer perimeter connected to the solid frame via this outer perimeter. Alternatively the plurality of swirler airfoils may have a

rectangular, particularly square, outer perimeter connected to the solid frame via this outer perimeter.

5 The form of the swirler airfoils may be optimised to provide the best mixing in regards to a given arrangement of the walls and in regards to the position of the fuel injection openings. In one embodiment the plurality of swirler airfoils each may have a straight leading edge. Alternatively the plurality of swirler airfoils each may have a curved leading
10 edge. Furthermore the plurality of swirler air foils each may have flat or a curved surface.

The swirler may be applied to a combustion chamber operating with liquid and/or gaseous fuel. In one preferred embodiment,
15 the at least one fuel injection opening may be arranged to inject liquid fuel into an air flow flowing through the at least one of the plurality of mixing channels. In an alternative embodiment the at least one fuel injection opening may be arranged to inject gaseous fuel into an air
20 flow flowing through the at least one of the plurality of mixing channels.

As a further option, the fuel injection openings are provided for both liquid and gaseous fuels. The fuel injection
25 openings may be arranged in the same of at least one of the plurality of mixing channels for both types of fuels. Alternatively, the plurality of mixing channels may be equipped with fuel injection openings for liquid and gaseous fuels in an alternating or any other advantageous order.

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The fuel injection openings may be arranged in various ways. Preferably they are located in a base plate of the swirler, each positioned substantially in the centre of the respective

mixing channel. Alternatively the fuel injection openings may be positioned in the walls of the vanes. The fuel injection openings for gaseous fuel may be separate from the fuel injection openings for liquid fuel. Alternatively they may be arranged coaxially. The fuel injection openings for gaseous fuel may be positioned upstream of the fuel injection openings for liquid fuel.

Regarding their forms, orientations, and positions, the swirler itself, the vanes, the mixing channels, the fuel injection openings, and the axial swirlers may preferably be arranged in a homogeneous and substantially symmetric way, so that also a symmetric and uniform stream of mixed air and fuel is created.

In a further embodiment, the swirler or a burner-head may comprise at least one further fuel injection opening for providing pilot fuel - liquid or gas - arranged at a downstream section of the at least one mixing channel, further downstream of the axial swirler. Advantageously the pilot fuel may be controllable separately from the at least one fuel injection opening, which can be seen as "main fuel".

BRIEF DESCRIPTION OF THE DRAWINGS

Embodiments of the invention will now be described, by way of example only, with reference to the accompanying drawings, of which:

- FIG. 1 shows schematically a longitudinal section through a combustor,
FIG. 2 shows schematically a perspective view of a prior art swirler,

- FIG. 3 illustrates schematically a perspective view of a swirler according to the invention,
- FIG. 4 illustrates distribution of fuel and air in a passage of a swirler,
- 5 FIG. 5 shows a fraction of a swirler in a perspective view with an axial swirler in a swirler passage,
- FIG. 6 shows schematically a top view from the downstream side of a combustion chamber, as indicated in figure 1 by arrows A-A.
- 10 FIG. 7 shows schematically a first form of an axial swirler applicable to the swirler of FIG. 3,
- FIG. 8 shows schematically a second form of an axial swirler applicable to the swirler of FIG. 3.
- 15 The illustration in the drawing is schematically. It is noted that for similar or identical elements in different figures, the same reference signs will be used.

DETAILED DESCRIPTION OF THE INVENTION

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Not shown, a gas turbine engine comprises a compressor section, a combustor section and a turbine section which are arranged adjacent to each other. In operation of the gas turbine engine air is compressed by the compressor section and output to the burner section with one or more combustors.

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Figure 1 shows a longitudinal section through a combustor, specifically a combustor within a gas turbine engine (not shown). The combustor comprises relative to a flow direction: a burner comprising a burner-head 1 and a swirler 2 attached to the burner-head 1, a transition piece referred to as combustion pre-chamber 3 and a main combustion chamber 4. The main combustion chamber 4 has a diameter being larger than

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the diameter of the pre-chamber 3. The main combustion chamber 4 is connected to the pre-chamber 3 via a dome portion 10 comprising a dome plate 11. In general, the transition piece 3 may be implemented as a one part continuation of the burner towards the combustion chamber 4, as a one part continuation of the combustion chamber 4 towards the burner, or as a separate part between the burner and the combustion chamber 4. The burner and the combustion chamber assembly show substantially rotational symmetry about a longitudinally symmetry axis 12.

A fuel supply 5 is provided for leading gaseous and/or liquid fuel to the burner which is to be mixed with inflowing air 6 - particularly compressed air from a compressor (not shown) - in the swirler 2. By the swirler 2, the fuel and the air is mixed as will be explained later. The resulting fuel/air mixture 7 is then guided towards the primary combustion zone 9 where it is burnt to form hot, pressurised exhaust gases 8 flowing in a direction indicated by arrows to a turbine (not shown) of the gas turbine engine (not shown).

A perspective view of a prior art swirler 2 is shown in Figure 2. The swirler 2, which is a radial swirler, comprises a ring-shaped swirler vane support 13 or base plate with a central opening 14, which leaves a space for the burner face of the burner-head 1 once assembled as the overall burner (burner-head 1 is not shown in Figure 2). As an example, six swirler vanes 15 each with asymmetric pie slice shape or in shape of an asymmetric cheese piece are disposed about the central axis 12 and arranged on the swirler vane support 13. The swirler vanes 15 can be fixed to the burner-head 1 (see Figure 1) with their sides showing away from the swirler vane support 13. Swirler passages 16 as mixing channels are

defined and delimited by opposing side faces 17 as walls of swirler vanes 15, by the surface of the swirler vane support 13 which shows to the burner-head 1 and by a surface (not shown) of the burner to which the swirler vanes 15 are fixed.

5 Compressor air 6 flows from radially outside into these swirler passages 16 directed inwards and is mixed with fuel which is added through fuel injection openings (not shown).

The swirler passages 16 are arranged like that, that the fluid passing the passages 16 are directed to a radial outer section of the central opening 14. Furthermore the swirler passages 16 are substantially directed tangential to the radial outer section of the central opening 14. In this embodiment of the invention the opposing side faces 17 of a specific one of the swirler passages 16 are substantially planar and parallel to each other.

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Referring now to FIG. 3, based on the swirler shown in Figure 2, the inventive swirler is described. The explanation of the form and the components of the swirler 2 given in respect to Figure 2 still applies also for Figure 3.

20

For each of the swirler passages 16, in Figure 3 an axial swirler 20, a liquid fuel injector 22 and a gas fuel injector 21 is shown. Several fuel injectors, main and supplementary ones, may be provided. In this case, the shown fuel injectors 22, 21 should represent the main injectors. The gas fuel injector 21 is located at the radially outward end of the swirler passages 16, i.e. at the upstream end of the flowing air 6. The gas orifice may be plain to a surface of the swirler vane support 13. Next to the gas fuel injector 21, further downstream, the liquid fuel injector 22 may be

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located with an orifice that protrudes the surface of the swirler vane support 13.

Further downstream, in figure 3 close to the end of one of the side faces 17, the axial swirler 20 is located in each swirler passage 16. The axial swirler 20 is a device that provides a rotational movement to the fluid flowing through the swirler passage 16. Hence, fuel and air mixing is improved, which also may lead to a reduced emission.

10

In figure 3, the axial swirler 20 extends perpendicular to the side faces 17 over the complete width of the swirler passage 16. The axial swirler 20 also has the same height as the swirler vanes 15. The axial swirler 20 is arranged with an axial swirl generating arrangement, secured via a frame 23, the axial swirl generating arrangement comprising a plurality airfoils 24 each designed to redirect the fuel enriched air flow and apply a rotational or curling movement to this originally lateral flow along the direction of the swirler passage 16.

20

Referring now to figure 4, the distribution of fuel and air in the swirler passage 16 is shown, when no axial swirler is provided for additional mixing. The swirler passage 16 is defined by the walls 17 (one of them is only indicated by a single line). One of the swirler vanes 15 is shown, together with the liquid fuel injector 22 and the gas fuel injector 21 in the adjacent swirler passage 16. The direction of the main air 6 is indicated by a broad arrow, leading straight into the swirler passage 16 from the upstream end of the swirler passage 16. The directions of the liquid fuel 26 and gas fuel 25 are bent arrows to indicate, that liquid fuel 26 and gas fuel 25 get entrained by the air 6 to the downstream side.

25

30

The fuel 25, 26 get mixed with the air 6, resulting in an exemplary distribution indicated by arrows 40, 41, and 42, which is a shear flow in the swirler passage 16. Stream 41 may be the wanted fuel to air ratio, which is an optimum
5 regarding flame stabilisation and emissions. Stream 40 may be an air enriched fuel/air mixture, whereas stream 42 may be a fuel enriched fuel/air mixture, which both may lead to decreased flame stabilisation in case of a lean fuel/air mixture or may lead to higher emissions of NO_x in non-lean
10 operation.

This is overcome by applying the axial swirler 20 in the swirler passage 16, as it can be seen in figure 3 and figure 5. With that the air 6, the liquid fuel 26, and gas fuel 25
15 all pass the axial swirler 20 and get redirected and mixed.

Figure 6 shows schematically a top view from the downstream side of a combustion chamber, as indicated in figure 1 by arrows A-A. The swirler 2 is shown and a burner face 53 of
20 the burner-head 1. It is shown for one specific swirler passage 16, that air 6 entering the swirler passage 16 will flow through the swirler passage 16 - indicated by two smaller arrows with the reference sign 6 - and the liquid fuel 26 and gas fuel 25 will be injected into the swirler
25 passage 16. All of these streams, partly mixed, then flow downstream and get additionally mixed by the axial swirler 20, which is present in the swirler passage 16. A more homogenous air/fuel mixture 43 leaves the individual swirler passages 16 and will enter the centre zone of the swirler 2.
30 Finally, all of these passage individual air/fuel mixtures 43 will experience a swirl as indicated by arrow 44 around the central axis of the swirler 2.

Further components that can be seen in figure 6 are an igniter 50 in the area of the burner face 53, a first pilot fuel injection 51 for liquid fuel and a second pilot fuel injection 52 for gaseous fuel. Both fuel injections 51 and 52 will be considered the "further fuel injection opening" or the "additional fuel injection opening" according to the claims.

The pilot fuel injections may optionally be present in all of the embodiments of the invention. The first pilot fuel injection 51 for liquid fuel is in the form of a valve. Only a single first pilot fuel injection 51 is shown in the figure but several can be present, preferably near the centre of the burner. The second pilot fuel injection 52 is shown in form of a ring so that pilot gas can be injected circumferentially at the ends of the swirler passages 16. It has to be noted that also other forms and locations of fuel injections may be possible. And as in all embodiments of the invention, a burner may be limited to only liquid fuel or only to gaseous fuel.

Advantageously the first pilot fuel injection 51 for liquid fuel and the second pilot fuel injection 52 for gaseous fuel are located downstream of the axial swirler 20. During operation of the gas turbine, the fuel - either gas or liquid - is introduced in two stages: with a main injection via the liquid fuel injector 22 and/or the gas fuel injector 21, which results in a high degree of premixedness and hence low NO_x emissions, and a pilot injection via the first pilot fuel injection 51 for liquid fuel and/or the second pilot fuel injection 52 for gaseous fuel. The pilot injection may steadily be increased as the load demand decreases in order to ensure flame stability, which may not be guaranteed with

lower loads. The first pilot fuel injection 51 for liquid fuel and/or the second pilot fuel injection 52 for gaseous fuel are arranged, such that as the pilot fuel split increases, the fuel is biased towards the axis - axis 12 as indicated in figure 1 - of the combustor. This avoids problems with combustion instability at lower loads.

In operation mode with lean premix combustion, which may be selected to reduce NO_x , pilot fuel injection may even be advantageous to stabilize the flame even at full load, however, the percentage of fuel injected via the pilot fuel injection 51 and 52 compared to the overall fuel injection may be small for full load, for example 5%.

With the pilot fuel injection severe combustion dynamics may be avoided, which otherwise could take place due to combustion at near limit of flammability.

In figures 7 and 8, exemplary forms of the axial swirler 20 is schematically shown, seen from a direction as indicated by the arrow 6 in figure 5.

In figure 7 the axial swirler 20 has a rectangular frame 23, and a central structure with a tube like round perimeter 30, the central structure comprising a plurality of airfoils 24 from which only the leading edges 33 and a part of the leading surfaces can be seen. The airfoils 24 are tilted and are overlapping each other so that passages are created to pass the pre-mixed stream of air and fuel (indicated in figure 6 by reference signs 6, 25, and 26) giving it a rotational movement.

In the example the airfoils 24 are fixed at a specific position between perimeter 30 and an inner ring 32. The sizes of the perimeter 30 and the inner ring 32 in the figure may only be seen as examples.

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Figure 8 shows an alternative to the embodiment of figure 7, in which an outer perimeter 31 is a rectangular, if seen from the upstream side. It can also be seen as a cuboid with missing side faces at the upstream and downstream sides. The airfoils 24 will extend up the perimeter 31. Besides that they may not differ substantially to the airfoils 24 of figure 7.

The axial swirler 20 may be constructed in several ways. Besides the two examples of figures 7 and 8, also several modifications are possible. For example the leading edges 33 may not be straight but curved. The leading edges 33 may be rounded or sharp. The surfaces of the airfoils 24 may be flat or bent. The inner ring 32 and the outer frame 23 may be of different sizes and forms in different embodiments. All of these possibilities should be optimised so that the shear flow in the swirler passage 16 is overcome and the mixing is more perfectly. This then leads to a more stabilised flame, also in a lean operation, and consequently also to less NO_x emissions.

25

Patent claims

1. Swirler (2) for mixing fuel (25, 26) and air (6) comprising:
5 - a plurality of vanes (15) positioned radially around a central axis (12) of the swirler (2);
 - a plurality of mixing channels for mixing fuel (25, 26) and air (6),
 at least one mixing channel (16) of the plurality of
10 mixing channels defined by opposite walls (17) of two adjacent vanes of the plurality of vanes (15) and comprising at least one fuel injection opening (21, 22) arranged at an upstream section of the at least one mixing channel (16) and comprising an axial swirler (20), particularly
15 extending between the walls (17) of the two adjacent vanes, arranged at a downstream section of the at least one mixing channel (16).

2. Swirler (2) according to one of the preceding claims,
20 characterised in that
 the axial swirler (20) being arranged substantially perpendicular to the walls (17) of the two adjacent vanes.

3. Swirler (2) according to one of the preceding claims,
25 characterised in that
 the axial swirler (20) having a plurality of swirler airfoils (24).

4. Swirler (2) according to claim 3,
30 characterised in that
 the axial swirler (20) having a rectangular solid frame (23) surrounding the plurality of swirler airfoils (24).

5. Swirler (2) according to claim 4,
characterised in that
the plurality of swirler airfoils (24) having an elliptic,
particularly circular, outer perimeter (30) connected to
5 the solid frame (23) via this outer perimeter (30).
6. Swirler (2) according to claim 4,
characterised in that
the plurality of swirler airfoils (24) having a rectangu-
10 lar, particularly square, outer perimeter (31) connected
to the solid frame (23) via this outer perimeter (31).
7. Swirler (2) according to claim 3 to 6,
characterised in that
15 the plurality of swirler airfoils (24) being arranged to
provide a mixing channel individual rotating airflow (43)
for the at least one mixing channel (16).
8. Swirler (2) according to claim 3 to 7,
20 characterised in that
the plurality of swirler airfoils (24) each having a
straight leading edge (33).
9. Swirler (2) according to claim 3 to 7,
25 characterised in that
the plurality of swirler airfoils (24) each having a
curved leading edge.
10. Swirler (2) according to claims 1 to 9,
30 characterised in that
- a first one of the at least one fuel injection opening
(21, 22) being arranged to inject liquid fuel (26) into an
air (6) flow flowing through the at least one mixing

channel (16) or through any one of the plurality of mixing channels, and/or

- a second one of the at least one fuel injection opening (21, 22) being arranged to inject gaseous fuel (25) into the air (6) flow flowing through the same one of at least one mixing channel (16) or through any one of the plurality of mixing channels.

11. Swirler (2) according to one of the preceding claims,

characterised in that

comprising at least one further fuel injection opening (51, 52) arranged at a downstream section of the at least one mixing channel (16), further downstream of the axial swirler (20).

12. Swirler (2) according to claim 11,

characterised in that

the further fuel injection opening (51, 52) being configured such that the fuel injection is controllable separately from the at least one fuel injection opening (21, 22).

13. Combustion chamber comprising a swirler (2) according to one of the claims 1 to 12.

14. Combustion chamber according to claim 13,

further comprising a burner-head (1), the burner-head (1) comprising at least one additional fuel injection opening (51, 52) arranged downstream of the plurality of mixing channels for mixing fuel (25, 26) and air (6).

15. Gas turbine comprising at least one combustion chamber,
the at least one combustion chamber comprising a swirler
(2) according to one of the claims 1 to 12.

FIG 1

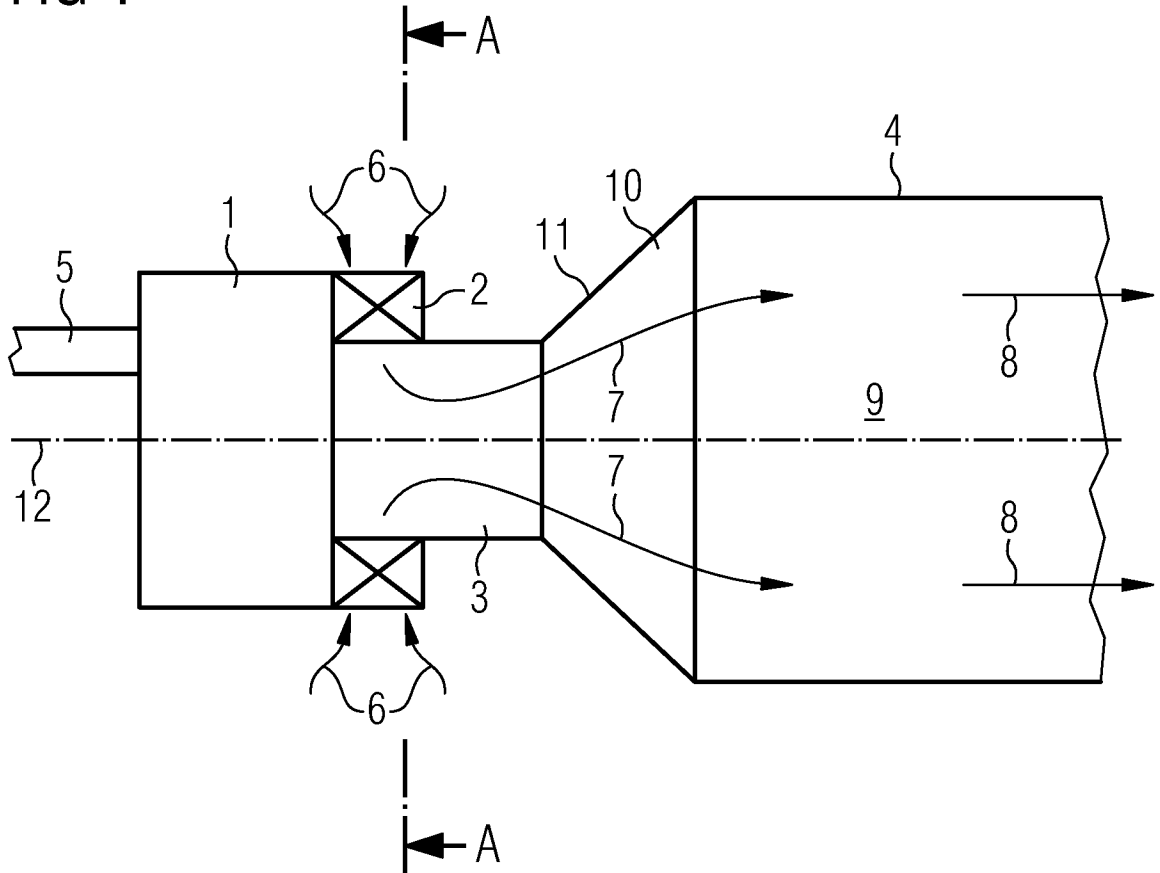


FIG 2 PRIOR ART

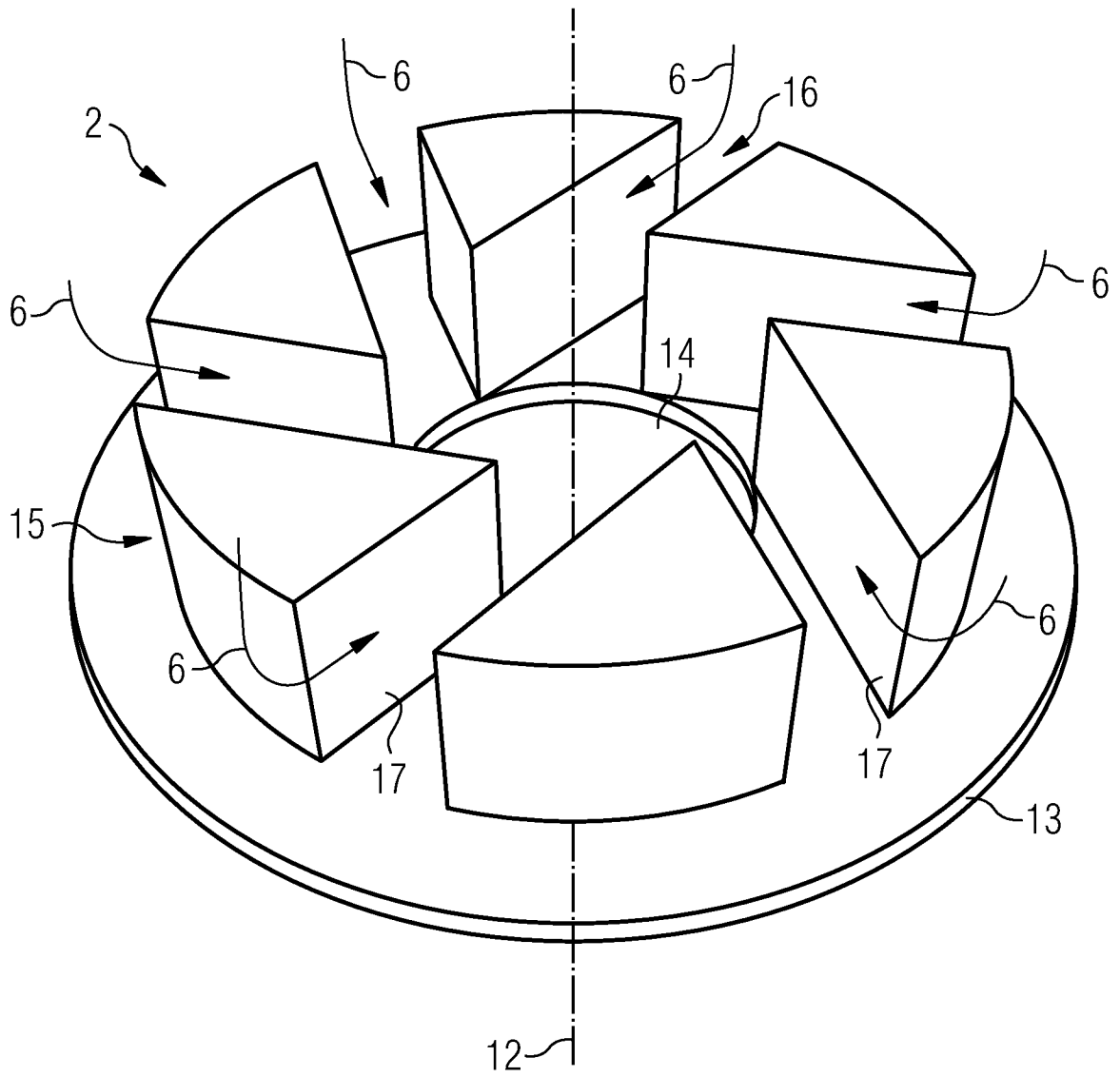


FIG 3

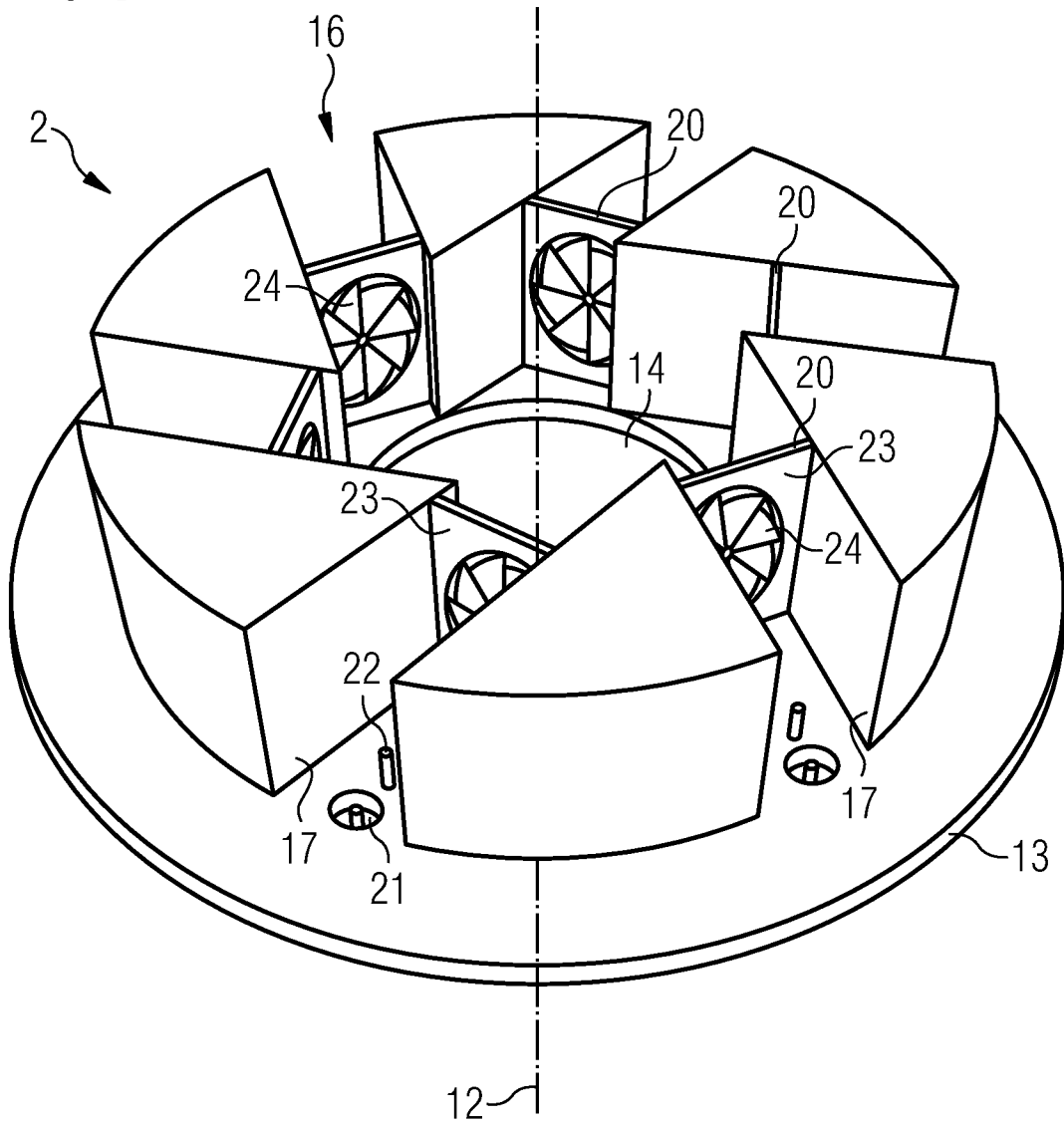


FIG 4

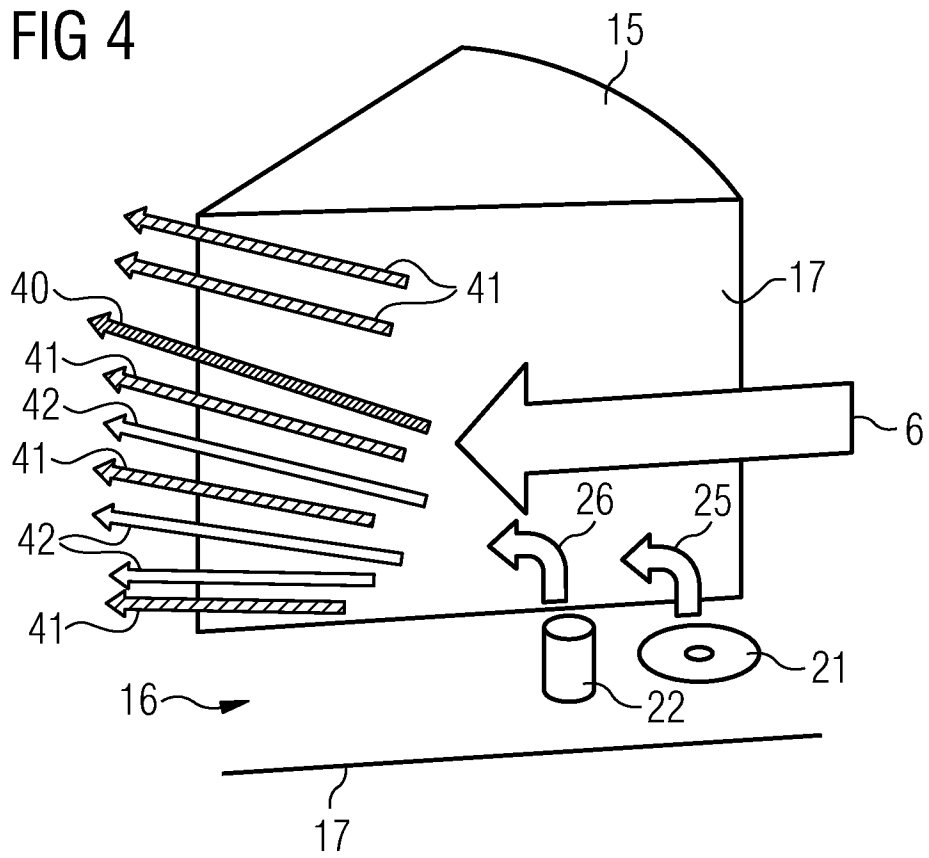


FIG 5

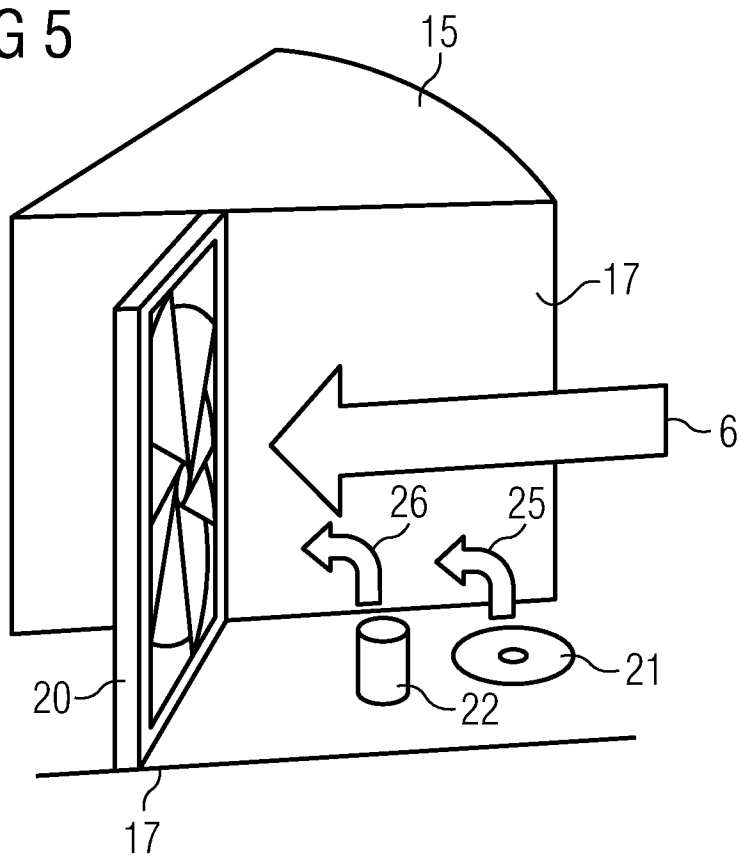


FIG 6

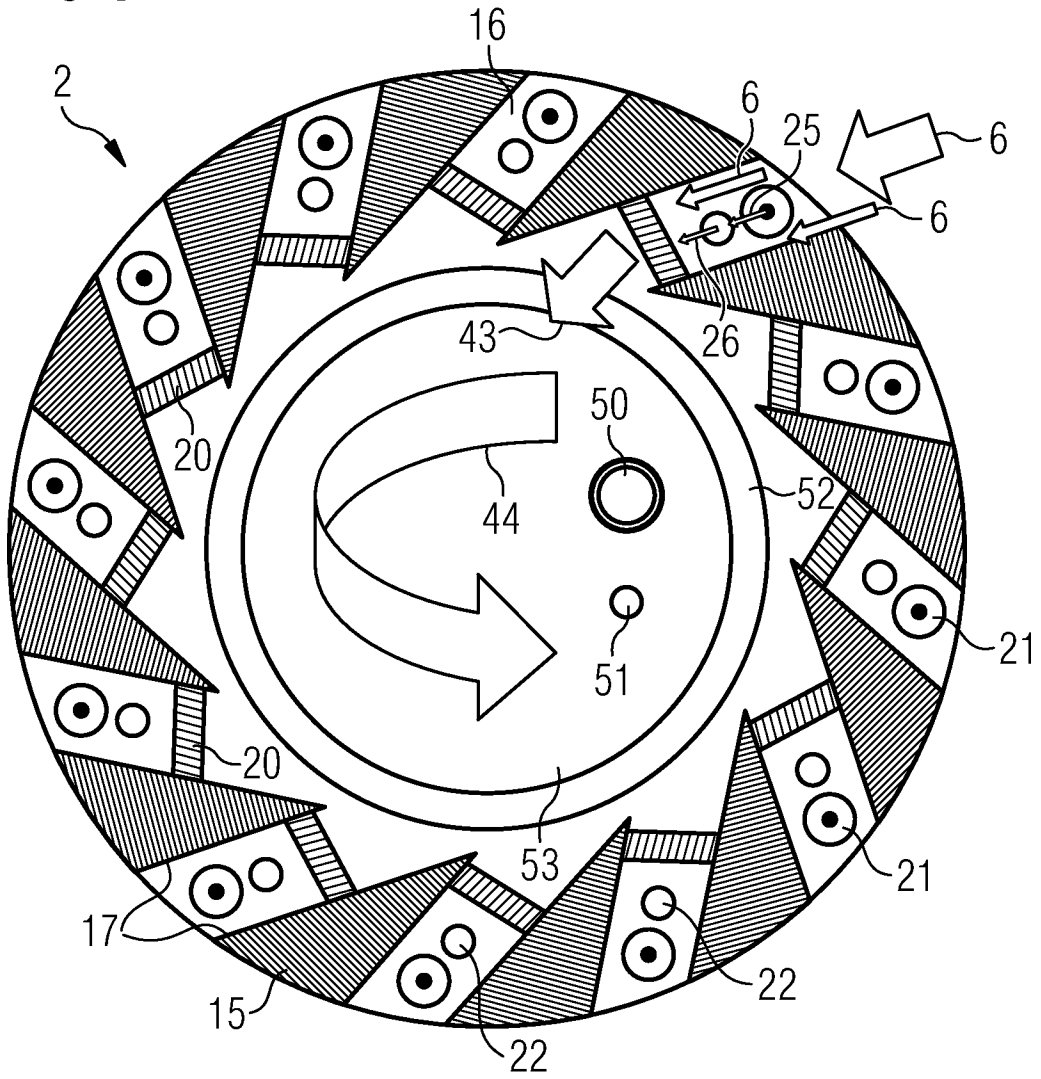


FIG 7

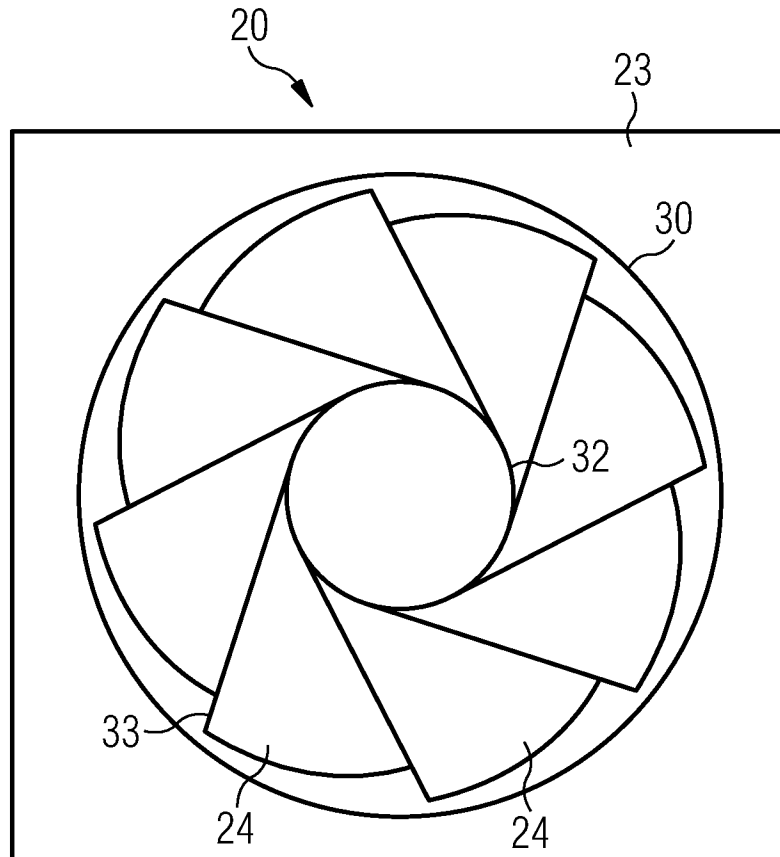
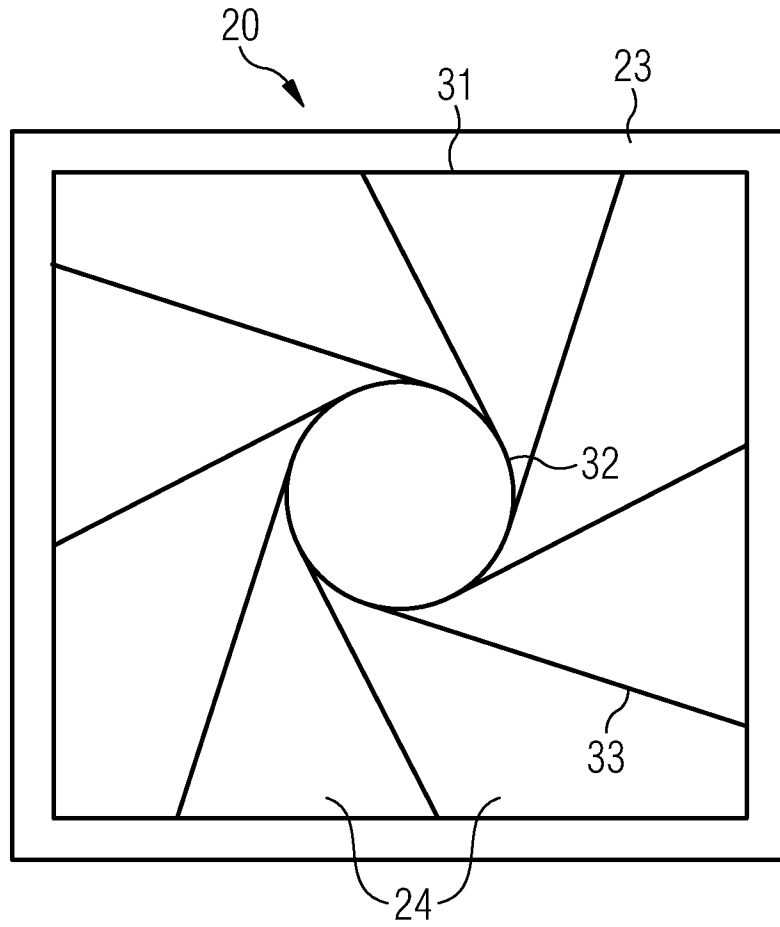


FIG 8



INTERNATIONAL SEARCH REPORT

International application No
PCT/EP2010/051667

A. CLASSIFICATION OF SUBJECT MATTER INV. F23D14/02 F23R3/14 F23R3/28 ADD.		
According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED Minimum documentation searched (classification system followed by classification symbols) F23D F23R		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practical, search terms used) EPO-Internal		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	GB 2 443 431 A (SIEMENS AG [DE]) 7 May 2008 (2008-05-07) figures 1,2 -----	1
A	GB 2 444 737 A (SIEMENS AG [DE]) 18 June 2008 (2008-06-18) abstract; figure 3 -----	1
A	GB 2 435 508 A (SIEMENS AG [DE]) 29 August 2007 (2007-08-29) abstract -----	1
A	EP 1 992 878 A (SIEMENS AG [DE]) 19 November 2008 (2008-11-19) figure 3 -----	1
<input type="checkbox"/> Further documents are listed in the continuation of Box C. <input checked="" type="checkbox"/> See patent family annex.		
* Special categories of cited documents :		
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4 June 2010	14/06/2010	
Name and mailing address of the ISA/ European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Fax: (+31-70) 340-3016	Authorized officer Munteh, Louis	

INTERNATIONAL SEARCH REPORT

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			WO 2008141955 A1	27-11-2008