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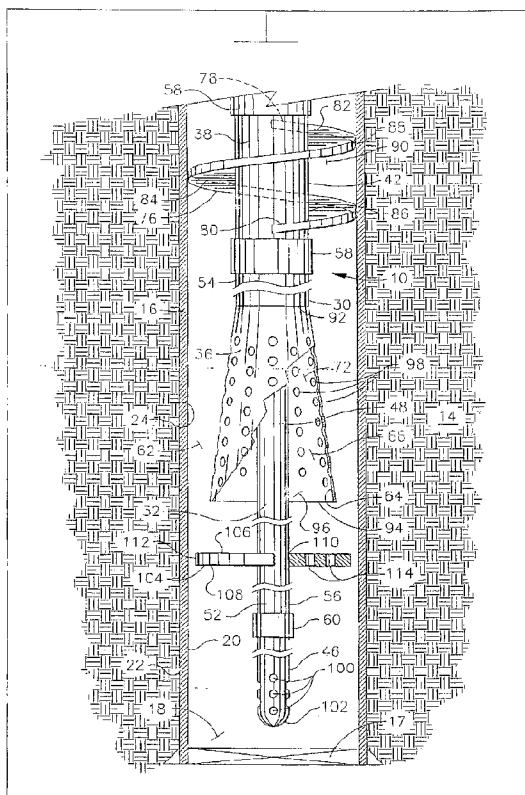
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(54) Title: A GAS-LIQUID SEPARATOR POSITIONABLE DOWN HOLE IN A WELL BORE



(57) Abstract: A gas-liquid separator positionable down hole in a well bore includes an external tube having an external tube interior and an internal tube having an internal tube interior. The internal tube is positioned in the external tube interior to form an internal annulus defining a gas flowpath and the internal tube interior defines a reduced-gas fluid flowpath. A plate at least partially encircles the external tube to form a curved flow channel, which defines a produced fluid mixture flowpath. A first internal annulus opening is provided in the external tube, which defines a gas inlet port. An internal tube interior opening is provided in the internal tube, which defines a reduced-gas fluid inlet port. A produced fluid mixture is conveyed through the flow channel, which spins the produced fluid mixture about the external tube. At least a portion of a gas in the produced fluid mixture is separated from the liquid in response to spinning, thereby producing a separated free gas which enters the gas flowpath via the gas inlet port and a reduced-gas fluid which enters the reduced-gas fluid flowpath via the reduced gas-fluid inlet port.

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- 1 -

GAS-LIQUID SEPARATOR POSTIONABLE DOWN HOLE IN A WELL BORE

The present invention relates generally to oil recovery, and more particularly to
5 down hole separation of produced fluid in a well bore into gases and liquids.

BACKGROUND OF THE INVENTION

Many oil production wells require artificial lift equipment to raise the produced
oil to the surface well head after the oil enters the well bore from an adjacent fluid
10 production zone penetrated by the well bore. However, the oil entering the well bore
from the fluid production zone is typically contained within a produced fluid mixture
having two phases, a gas phase and a liquid phase. The liquid phase includes the oil
as well as water, while the gas phase includes dissolved or otherwise entrained gases
and/or free gases. The artificial lift equipment is generally effective for raising the
15 liquids to the surface, but conversely is relatively ineffective when produced fluid
mixtures having a high gas content are encountered. Therefore, it is desirable to
separate the produced fluid mixture into the gases and liquids before employing the
artificial lift equipment to raise the liquids to the surface.

20 The present invention recognizes the need for a gas-liquid separator
positionable down hole in a well bore which effectively separates a produced fluid
mixture into gases and liquids before utilizing artificial lift equipment to raise the liquids
to the surface. Accordingly, it is an object of the present invention to provide such a
gas-liquid separator and a method of operating the same. More particularly, it is an
25 object of the present invention to provide an essentially static gas-liquid separator for
centrifugally separating a produced fluid mixture into gases and liquids, including
hydrocarbon liquids, down hole in a well bore before raising the liquids to the surface
by means of an artificial lift assembly associated with the gas-liquid separator. These
objects and others are accomplished in accordance with the invention described
30 hereafter.

2003268103 05 May 2008

- 2 -

SUMMARY OF THE INVENTION

According to the present invention, there is provided a gas-liquid separator positionable down hole in a well bore comprising:

- 5 an external tube having an external tube interior;
- an internal tube having an internal tube interior defining a reduced-gas fluid flowpath, wherein said internal tube is positioned in said external tube interior to form an internal annulus between said external tube and said internal tube, said internal annulus defining a free gas flowpath;
- 10 a plate having a start point and at least partially encircling said external tube to form a curved flow channel defining a produced fluid mixture flowpath;
- an internal annulus opening beyond said start point defining a free gas inlet port for said free gas flowpath, wherein said external tube has a flared portion positioned at or proximal to said internal annulus opening and flaring outwardly as
- 15 said flared portion extends away from said start point of said plate; and
- an internal tube interior opening beyond said start point defining a reduced-gas fluid inlet port for said reduced-gas fluid flowpath.

20 The invention also provides a gas-liquid separator positionable down hole in a well bore comprising:

- an external tube having an external tube interior;
- an internal tube having an internal tube interior defining a reduced-gas fluid flowpath, wherein said internal tube is positioned in said external tube interior to form an internal annulus between said external tube and said internal tube defining a free
- 25 gas flowpath;
- means for spinning a produced fluid mixture about said external tube;
- an internal annulus opening through said external tube defining a free gas inlet port for said free gas flowpath, wherein said external tube has a flared portion positioned at or proximal to said internal annulus opening and flaring outwardly as
- 30 said flared portion extends away from said spinning means; and
- an internal tube interior opening through said internal tube defining a reduced-gas fluid inlet port for said reduced-gas fluid flowpath.

The present invention is further described by way of example only with reference to the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

Figures 1A and 1B are an elevational view of a gas-liquid separator of the present invention positioned in a cased well bore.

Figure 2A and 2B are a conceptualized operational view of the gas-liquid separator of Figures 1A and 1B.

Figures 3A and 3B are an elevational view of an alternate embodiment of a gas-liquid separator of the present invention positioned in a cased well bore.

Figure 4 is an elevational view of the fixed auger of the gas-liquid separator of Figure 3A.

Figure 5 is an elevational view of the fixed auger of the gas-liquid separator of Figure 4, but rotated 90° from the view of Figure 4.

Figure 6 is a cross-sectional view of the gas-liquid separator of Figure 3A taken along cross section line 6-6.

Figure 7A and 7B are a conceptualized operational view of the gas-liquid separator of Figures 3A and 3B.

DESCRIPTION OF PREFERRED EMBODIMENTS

Referring to Figures 1A and 1B, a gas-liquid separator of the present invention is shown and generally designated 10. The gas-liquid separator 10 is positioned down hole within a well bore 12, which extends from an earthen surface (not shown) through an earthen formation 14. A "well bore", as defined herein, is the actual bore hole of a well. The well bore 12 is bounded by the walls of the earthen formation 14, through which the well bore 12 extends. The walls of the earthen formation 14 bounding the well bore 12 are termed the "well bore face".

The gas-liquid separator 10 and the well bore 12 are parallelly, and preferably concentrically, aligned with reference to their respective longitudinal axes. The longitudinal axes of the gas-liquid separator 10 and the well bore 12 are likewise preferably vertically aligned relative to the earthen surface overlying the earthen formation 14. As such, earth's gravitational force is downwardly directed in the well bore 12, thereby exerting a downward force against any fluids residing in the well bore 12. The terms "down" and "up" are used herein with reference to the earthen surface and the earth center, wherein "down" is away from the earthen surface

2003268103 26 May 2008

toward the earth center and "up" is toward the earthen surface away from the earth center.

Although the well bore 12 is shown and described herein as preferably being a vertical well bore, it is understood that it is within the scope of the present invention to position the gas-liquid separator 10 in a directional well bore as long as the longitudinal axis of the well bore is not perpendicular to the direction of the gravitational forces in the well bore as in the case of a horizontal well bore. Nevertheless, for the gas-liquid separator 10 to operate most effectively, the longitudinal axis of the well bore preferably does not deviate more than about 45° from vertical.

The gas-liquid separator of the present invention has general utility in either a cased or an uncased (i.e., open) well bore. Nevertheless, the gas-liquid separator 10 of the present embodiment is preferably utilized in a cased well bore. Accordingly, a tubular well bore casing 16, more specifically termed a production casing, shown cross-sectionally is fixed within the well bore 12 by cementing or other conventional means. A casing shoe 17 is positioned across the bottom opening 18 of the casing 16 to effectively prevent fluid migration from the earthen formation 14 into the casing interior through the bottom opening 18. The casing 16 has a casing inner face 20 and a casing outer face 22. The terms "inner" and "outer" are used herein to designate the relative positions of the recited elements along the radial axis of the well bore 12, wherein "inner" is radially nearer the longitudinal axis of the well bore 12 than "outer". The casing inner face 20 is directed toward the well bore 12 and the casing outer face 22 is directed toward the well bore face 24 of the earthen formation 14. One or more perforations 26, more specifically termed production perforations, are formed in the casing 16 and extend through the casing 16 from the casing outer face 22 to the casing inner face 20.

The production perforations 26 are positioned at a depth point which corresponds to a depth point of a fluid production zone 28 in the earthen formation 14. Accordingly, the production perforations 26 provide fluid communication between the fluid production zone 28 and the well bore 12 (i.e., the casing interior) and enable produced fluids to flow from the fluid production zone 28 through the casing 16 into the well bore 12 as described hereafter. The production perforations 26 are shown

as being formed in only one side of the casing 16 for purposes of clarity. However, it is understood that a plurality production perforations are typically distributed around the entire circumference of the casing because the fluid production zone typically surrounds the entire circumference of the casing.

5 The gas-liquid separator 10 comprises an external tube 30 and an internal tube 32. The terms "external" and "internal" are used herein to designate the relative positions of the recited elements, wherein the "internal" element is surrounded at least in part by the "external" element. The external tube 30 is more specifically termed a gas conduit and the internal tube 32 is more specifically termed a pump
10 intake extension or a stinger in the present embodiment. The external tube 30 has a top end portion 34 and a bottom end portion 36. The terms "top" and "bottom" are used herein to designate the relative positions of the recited elements along the longitudinal axis of the well bore 12 with reference to the earthen surface and the earth center, wherein "top" is closer to the earthen surface than "bottom". The
15 external tube 30 also has an intermediate portion 38 extending between the top and bottom end portions 34, 36 and has an essentially continuous outer face 42.

 The internal tube 32 similarly has a top end portion 44 and a bottom end portion 46. The internal tube 32 also has an intermediate portion 48 extending between the top and bottom end portions 44, 46 and has an essentially continuous
20 outer face 52. The internal tube 32 is concentrically positioned within the external tube 30 with the top and bottom end portions 44, 46 of the internal tube 32 extending from the top and bottom end portions 34, 36, respectively, of the external tube 30. By way of example, the height of the external tube 30 is on the order of about 100 to 250 feet and the internal tube 32 extends on the order of about 300 to 500 feet from
25 the bottom end portion 36 of the external tube 30. The height of the internal tube 32 in combination with the production tubing string described hereafter is typically on the order of about 8,000 to 10,000 feet. Due to the relatively long lengths of the external and internal tubes 30, 32, respectively, the external and internal tubes 30, 32 are
30 each typically (although not necessarily) formed by serially joining a plurality of external and internal tube segments 54, 56, respectively, in sealed fixed engagement by means of external and internal tube couplings 58, 60, respectively.

 The external tube 30 and internal tube 32 each has an outside diameter,

which is substantially less than the inside diameter of the casing 16 (or diameter of the well bore face in the situation of an open well bore) to define an external annulus 62. The external annulus 62 is bounded by the casing inner face 20 (or the well bore face in the situation of an open well bore) and the outer face 42 of the external tube 30. The external annulus 62 is bounded by the casing inner face 20 (or the well bore face in the situation of an open well bore) and the outer face 52 of the internal tube 32 where the internal tube 32 extends beyond the top or bottom end portions 34, 36 of the external tube 30. The external tube 30 is shown in partial cut-away to expose an inner face 64 of the external tube 30, an external tube interior 66, and the internal tube 32 therein. The internal tube 32 is also shown in partial cut-away to expose an inner face 68 of the internal tube 32 and an internal tube interior 70. The internal tube interior 70 is essentially open along its length to define a reduced-gas fluid flowpath.

The internal tube 32 has an outside diameter which is substantially less than the inside diameter of the external tube 30. For example, the outside diameter of the internal tube 32 is on the order of about 2 7/8 inches and the inside diameter of the external tube 30 is on the order of about 4 inches. Accordingly, the external and internal tubes 30, 32 define an internal annulus 72 which is bounded on its sides by the inner face 64 of the external tube 30 and the outer face 52 of the internal tube 32. The internal annulus 72 is essentially open along its length to define an internal separated free gas flowpath. The top of the internal annulus 72 is closed off by an external tube hanger 74, which is a conventional tubing hanger connecting the top end portion 34 of the external tube 30 to the internal tube 32. The external tube hanger 74 extends around and fixably engages the outer face 52 of the internal tube 32 proximal to the top end portion 44 of the internal tube 32. The top end portion 34 of the external tube 30 is hung from the external tube hanger 74, which bears the entire weight of the external tube 30 and fixably maintains the concentric position of the internal tube 32 relative to the external tube 30.

The gas-liquid separator 10 further comprises a fixed auger, which has a single fin configuration comprising a spiral plate 76. The spiral plate 76 is arcuately shaped with 1.5 turns about the external tube 38 to encircle the external tube 30 1.5 times. The present invention is not limited by the number of turns of the spiral plate

76 about the external tube 30, but the spiral plate 76 preferably has at least approximately a one-half turn to partially encircle the external tube 30, more preferably at least about 1 turn to fully encircle the external tube 30, and most preferably at least about 1.5 or more turns to multiply encircle the external tube 30.

5 The spiral plate 76 has a start point 78 (shown in phantom), an end point 80, an upper face 82, a lower face 84, an inner edge 86, and an outer edge 88. The spiral plate 76 is positioned in the external annulus 62 and is preferably fixed to the intermediate portion 38 of the external tube 30. The linear height of the spiral plate 76 from the start point 78 to the end point 80 is, for example, on the order of about 1
10 to 2 feet. The width of the upper face 82 and the lower face 84 are identical, being about equal to the width of the external annulus 62. The inner edge 86 of the spiral plate 76 is helically configured to spirally track the outer face 42 of the external tube 30. The inner edge 86 conformingly and fixably engages the outer face 42 of the external tube 30 along the intermediate portion 38 of the external tube 30. The
15 junction of the inner edge 86 and the outer face 42 preferably essentially forms a seal to prevent the substantial flow of fluids between the inner edge 86 and the outer face 42.

 The spiral plate 76 has a diameter approximately equal to the inside diameter of the casing 16 (or the well bore face in the situation of an open well bore). As such,
20 the outer edge 88 of the spiral plate 76 is helically configured to spirally track the casing inner face 20 of the casing 16 (or the well bore face in the situation of an open well bore). The outer edge 88 conformingly engages the casing inner face 20 (or the well bore face in the situation of an open well bore). The outer edge 88 and the casing inner face 20 (or the well bore face in the situation of an open well bore) are
25 preferably in tight fitting engagement with one another at their interface to essentially form a seal which prevents the substantial flow of fluids between the outer edge 88 and the casing inner face 20 (or the well bore face in the situation of an open well bore). The start and end points 78, 80 and upper and lower faces 82, 84 of the spiral plate 76, the outer face 42 of the external tube 30, and the casing inner face 20 (or
30 the well bore face in the situation of an open well bore) bound a restrictive curved flow channel 90 through the external annulus 62, which is more specifically termed a spiral channel. The spiral channel 90 corresponds to the spiral plate 76 insofar as

the spiral channel 90 preferably spirally descends at least approximately a one-half complete turn, more preferably at least approximately 1 turn, and most preferably at least approximately 1.5 or more turns about the outer face 42 of the external tube 30, as shown in the present embodiment.

5 The gas-liquid separator 10 further comprises a lower first internal annulus opening, which provides fluid communication between the internal annulus 72 and the external annulus 62. The lower first internal annulus opening is positioned in the external tube 30 at a point or points beyond the start point 78 of the spiral plate 76 and preferably at a point or points beyond the end point 80 of the spiral plate 76
10 proximal to the bottom end portion 36 of the external tube 30. The lower first internal annulus opening defines a separated free gas inlet port which opens into the internal separated free gas flowpath (i.e., the internal annulus 72) from the exterior thereof.

 In accordance with the present embodiment, the bottom end portion 36 of the external tube 30, more specifically termed a gas cone and shown in partial cut-away,
15 has a flared or conical configuration, which increases in diameter with distance away from the spiral plate 76. In contrast, the top end portion 34 and the intermediate portion 38 of the external tube 30 each has a substantially constant outside diameter along its length approximately equal to the diameter of the other, for example, on the order of about 4 1/2 inches. The bottom end portion 36 has opposite ends, in
20 particular a narrow end 92 and a flared end 94. The narrow end 92 is more proximal to the spiral plate 76 than the flared end 94 and is coupled with the intermediate portion 38 of the external tube 30. The narrow end 92 has a diameter which is approximately equal to that of the intermediate portion 38. The flared end 94 is a free end opposite the narrow end 92 and has a diameter which is substantially
25 greater than that of the narrow end 92 and the intermediate portion 38, for example, on the order of about 6 1/2 inches. The flared end 94 is open to the external annulus 62 to define a flared orifice 96. Because the flared orifice 96 dimensionally corresponds to the open flared end 94, the flared orifice 96 has a diameter approximately equal to the diameter of the flared end 94.

30 A plurality of flared perforations 98 are also distributed along the bottom end portion 36 of the external tube 30 above the flared orifice 96 more proximal to the spiral plate 76. The flared perforations 98 are formed in the wall of the external tube

30 and extend from the outer face 42 to the inner face 64. Like the flared orifice 96, the flared perforations 98 provide fluid communication between the internal annulus 72 and the external annulus 62, albeit through the wall of the external tube 30 rather than through the open flared end 94. The diameter of each of the flared perforations 98 is approximately equal to the others (for example, on the order of about 5/8 to 3/4 inches) and is substantially less than the diameter of the flared orifice 96. In the present embodiment, the lower first internal annulus opening comprises in combination the flared orifice 96 and the plurality of flared perforations 98 which functionally complement one another as described hereafter. However, in accordance with alternate embodiments not shown, the lower first internal annulus can consist essentially of the flared orifice 96 alone, the plurality of flared perforations 98 alone, or other configurations of single or multiple orifices readily apparent to the skilled artisan.

The gas-liquid separator 10 further comprises an internal tube interior opening, which provides fluid communication between the internal tube interior 70 and the external annulus 62. The internal tube interior opening is positioned in the internal tube 32 at a point or points beyond the start point 78 of the spiral plate 76 and preferably at a point or points beyond the end point 80 of the spiral plate 76. The internal tube opening is more preferably positioned at a point or points above the casing shoe 17 and below the lower first internal annulus opening 96, 98 proximal to the bottom end portion 46 of the internal tube 32, which extends from the bottom end portion 36 of the external tube 30. The internal tube interior opening defines a reduced-gas fluid inlet port which opens into the reduced-gas fluid flowpath (i.e., the internal tube interior 70) from the exterior thereof.

In accordance with the present embodiment, the top end portion 44, intermediate portion 48, and bottom end portion 46 of the internal tube 32 each has a substantially constant diameter along its length approximately equal to the diameter of the other, for example, on the order of about 2 3/8 inches. The bottom end portion 46, more specifically termed a perforated tubing sub or an artificial lift intake point in the present embodiment, has a plurality of internal tube interior perforations 100 distributed along a free end 102 of the bottom end portion 46 of the internal tube 32. The internal tube interior perforations 100 are positioned below the flared orifice 96

and flared perforations 98 more distal from the spiral plate 76. The internal tube interior perforations 100 are formed in the wall of the internal tube 32 and extend through the internal tube 32 from the outer face 52 to the inner face 68. The diameter of each of the internal tube interior perforations 100 is approximately equal to the others, for example, on the order of about 1/2 to 5/8 inches. In the present embodiment, the internal tube interior opening comprises the plurality of internal tube interior perforations 100. However, in accordance with alternate embodiments not shown, the internal tube interior opening can consist essentially of a single enlarged orifice rather than a plurality of perforations.

A perforated disk 104, more specifically termed a vortex spoiler, shown in partial cut-away is positioned in the external annulus 62, preferably below the bottom end portion 36 of the external tube 30 and above the bottom end portion 46 of the internal tube 32. The perforated disk 104 is more preferably positioned between the lower first internal annulus opening 96, 98 and the internal tube interior opening 100. The perforated disk 104 has a circular planar configuration with a diameter approximately equal to or less than the inside diameter of the casing 16 (or diameter of the well bore face in the situation of an open well bore) to fit within the external annulus 62. The plane of the perforated disk 104 is aligned in the external annulus 62 substantially perpendicular to the longitudinal axis of internal tube 32 and the well bore 12.

The perforated disk 104 has an upper face 106, a lower face 108, a central opening 110, an outer edge 112, and a plurality of disk perforations 114 distributed across the upper and lower faces 106, 108. The central opening 110 has a diameter greater than the outside diameter of the internal tube 32 which enables the internal tube 32 to readily pass through the central opening 110. Each of the plurality of disk perforations 114 has a diameter approximately equal to the others, for example, on the order of about 5/8 to 3/4 inches, and each extends through the perforated disk 104 from the upper face 106 to the lower face 108, thereby enabling fluid communication between the external annulus 62 on opposite sides of the disk 104.

The gas-liquid separator 10 further comprises an upper second internal annulus opening, which, like the lower first internal annulus opening, provides fluid communication between the internal annulus 72 and the external annulus 62.

However, the upper second internal annulus opening is positioned in the external tube 30 at a point or points above the start point 78 of the spiral plate 76 and preferably at a point or points proximal to the top end portion 34 of the external tube 30. The upper second internal annulus opening defines an internal separated free gas outlet port which opens from the internal annulus 72 into the exterior thereof.

In the present embodiment, a plurality of external tube perforations 118 are distributed around the top end portion 34 of the external tube 32 below the external tube hanger 74, which define the upper second internal annulus opening. Each external tube perforation 118 has a diameter approximately equal to the diameter of each flared perforation 98, i.e., for example, on the order of about 5/8 to 3/4 inches. The external tube perforations 118 are formed in the wall of the external tube 30 and extend from the outer face 42 to the inner face 64 to provide fluid communication between the internal annulus 72 and the external annulus 62, through the wall of the external tube 30. A sufficient number of external tube perforations 118 are provided so that the total surface area of all the external tube perforations 118 is about equal to or greater than the cross sectional area of the internal annulus 72 to minimize back pressure in the internal annulus 72. In the present embodiment, the upper second internal annulus opening comprises the plurality of external tube perforations 118. However, in accordance with alternate embodiments not shown, the upper second internal annulus opening can consist essentially of a single enlarged orifice rather than a plurality of perforations.

The gas-liquid separator 10 terminates at the top end portion 44 of the internal tube 32. The top end portion 44 has a proximal end 120 and a distal end 122, wherein the terms "proximal" and "distal" are relative to the spiral plate 76. The proximal end 120 is coupled with the intermediate portion 48 of the internal tube 32 and the distal end 122 is coupled with a down hole artificial lift assembly, which is structurally and functionally cooperative with the gas-liquid separator 10. The artificial lift assembly of the present embodiment is generally designated 124. The artificial lift assembly 124 is an in-line assembly comprising in series a conventional submersible pump 126 and a shroud 128 which houses a conventional electric pump motor (not shown). It is understood that the present invention is not limited to the specific artificial lift assembly 124 described herein by way of example. It is within

the scope of the present invention to employ alternate conventional artificial lift assemblies in cooperation with the gas-liquid separator 10, which are within the purview of the skilled artisan.

5 In any case, the artificial lift assembly 124 further comprises a swage 130 positioned at the junction of the shroud 128 and the distal end 122, which transitions the distal end 122 into the shroud 128. A shroud hanger 132 is positioned at the junction of the shroud 128 and the submersible pump 126 to couple them together. A production tubing string 134 extends upwardly from the submersible pump 126 through the well bore 12 to the earthen surface (not shown). The production tubing
10 string 134 has a diameter approximately equal to the diameter of the internal tube 32. The production tubing string 134 and artificial lift assembly 124 in series extend the reduced-gas fluid flowpath from the internal tube interior 70 to the earthen surface by providing fluid communication therebetween. An auxiliary line 136, such as an electric cable or one or more capillary strings, is optionally run from the earthen
15 surface to the artificial lift assembly 124 through the well bore 12 alongside the production tubing string 134 to serve the artificial lift assembly 124.

The artificial lift assembly 124 and production tubing string 134 each has an outside diameter, which is substantially less than the inside diameter of the casing 16 (or diameter of the well bore face in the situation of an open well bore), thereby
20 extending the external annulus 62 through the well bore 12 from the top end portion 44 of the internal tube 32 to the earthen surface. The artificial lift assembly 124 and production tubing string 134 are appropriately configured such that they do not substantially impede the flow of fluids through the external annulus 62.

Substantially all of the above-described components of the gas-liquid
25 separator 10 are fabricated from high-strength, durable, relatively rigid materials, such as steel or the like, which do not readily physically deform or chemically degrade under normal down hole operating conditions. The gas-liquid separator 10 is a static apparatus, which has essentially no moving parts exclusive of the artificial lift assembly 124. Thus, the gas-liquid separator 10 remains static relative to the well
30 bore 12 during operation once it is placed down hole in a manner described hereafter. The gas-liquid separator 10 has been described above as being assembled from a number of discrete individual components, but it is understood that

the present invention is not so limited. Combinations of one or more above-described components of the gas-liquid separator 10 can alternatively be integrally fabricated as single components. Finally, it is noted that a number of dimensional values are recited above. These values are recited merely by way of example and are not to be construed in any way as limiting the scope of the present invention.

Operation of the gas-liquid separator 10 is described hereafter with continuing reference to Figures 1A and 1B and further reference to Figures 2A and 2B. The gas-liquid separator 10 and associated artificial lift assembly 124 and production tubing string 134 are mounted in series within the well bore 12. In accordance with the present embodiment, the entire gas-liquid separator 10, including the spiral plate 76 and external tube perforations 118, is positioned below the production perforations 26. Produced fluids designated by the arrow 138 are displaced from a depth point in the fluid production zone 28 through the production perforations 26 into the external annulus 62. The produced fluids 138 comprise in combination oil, water and gas. The produced fluids 138 diverge at the production perforations 126 into two streams, a produced free gas designated by arrows 140 and a produced fluid mixture designated by arrows 142. The produced free gas 140 is a hydrocarbon gas, such as natural gas, which is conveyed by its own buoyancy up the segment of the external annulus 62 above the gas-liquid separator 10 and artificial lift assembly 124, specifically termed the casing/tubing annulus, to the well head (not shown) at the earthen surface. The produced fluid mixture 142 includes primarily oil and water in a liquid state and a hydrocarbon gas in a gaseous state. The liquids are typically combined in a suspension or emulsion and the gas is dissolved or otherwise entrained in the liquids. The produced fluid mixture 142 descends through the production perforations 26 down the external annulus 62 past the artificial lift assembly 124 under the force of gravity to the gas-liquid separator 10.

The components of the gas-liquid separator 10 functionally partition the external annulus 62 adjacent thereto into a plurality of functional chambers which extend continuously in series the length of the gas-liquid separator 10. In particular, the segment of the external annulus 62 between the external tube perforations 118 and the start point 78 of the spiral plate 76 is characterized as a produced fluid mixture conveyance chamber, which directs the produced fluid mixture 142

downward to the spiral plate 76. The segment of the external annulus 62 between the start point 78 and end point 80 of the spiral plate 76 (i.e., the spiral channel 90) is characterized as a gas-liquid separation chamber. As the produced fluid mixture 142 descends through the spiral channel 90, the produced fluid mixture 142 spins about the external tube 30, which in turn causes centrifugal separation of the oil, water and gas in the produced fluid mixture 142 due to density differences between them. In particular, separated free gas is concentrated more proximal to the outer face 42 of the external tube 30 than the liquids (i.e., toward the inner portion of the spiral channel 90).

The segment of the external annulus 62 below the spiral plate 76 and above the perforated disk 104 (i.e., adjacent to the bottom end portion 36 of the external tube 30) is characterized as a separated free gas recovery chamber. When the fluids descend out of the spiral channel 90 into the separated free gas recovery chamber, they continue to spin about the external tube 30, thereby forming a vortex 144. Separated free gas 146 is forced to the center of the vortex 144. The remainder of the vortex 144 is a reduced-gas fluid 148 (primarily oil and water in a liquid state), which moves toward the outside of the vortex 144. The separated free gas 146 at the center of the vortex 144 is compressed by the outward flaring bottom end portion 36 of the external tube 30, which forces the separated free gas 146 through the flared perforations 98 into the internal annulus 72.

The vortex 144 is essentially stopped at the point where the vortex 144 contacts the upper face 106 of the perforated disk 104. When the vortex 144 is stopped or is "spoiled" at the upper face 106, the remaining separated free gas 146 from the vortex 144 is discharged upward through the flared orifice 96 into the internal annulus 72 and combines with the separated free gas 146 which has entered the internal annulus 72 through the flared perforations 98. The separated free gas 146 is conveyed by its own buoyancy up through the internal annulus 72 until it reaches the external tube perforations 118. The separated free gas 146 is discharged upward from the internal annulus 72, out the external tube perforations 118, and into the external annulus 62 below the production perforations 26. The separated free gas 146 continues traveling upward through the external annulus 62 past the artificial lift assembly 124 counter-current to the produced fluid mixture 142.

The separated free gas 146 mixes with the produced free gas 140 at the production perforations 26 and continues upward as a free gas or coalesced in large gas bubbles through the casing/tubing annulus to the well head at the earthen surface. The separated free gas 146 and produced free gas 140 are captured at the well head for further treatment and/or downstream applications.

The segment of the external annulus 62 between the perforated disk 104 and the internal tube interior perforations 100 (i.e., adjacent to the bottom end portion 46 of the internal tube 32 extending from the external tube 30) is characterized as a reduced-gas fluid recovery chamber. As described above, when the perforated disk 104 stops the vortex 144, the separated free gas 146 rises into the internal annulus 72. However, the reduced-gas fluid 148 does not rise because it is heavier, containing mostly liquids. Accordingly, the reduced-gas fluid 148 passes downward through the disk perforations 114 of the perforated disk 104 into the reduced-gas fluid recovery chamber, where the reduced-gas fluid 148 is drawn through the internal tube interior perforations 100 into the internal tube interior 70. The artificial lift system 124 pumps the reduced-gas fluid 148 upward through the internal tube interior 70, past the artificial lift system 124, and through the production tubing string 134. The reduced-gas fluid 148 is captured at the well head for further treatment and/or downstream applications.

By way of example, the produced fluids entering the well bore typically contain within a range of about 95 to 97% gases by volume, the remainder being liquids. Before being processed by the gas-liquid separator of the present invention, the produced fluid mixture typically contains within a range of about 10 to 15% gases by volume, the remainder being liquids. After being processed by the gas-liquid separator of the present invention, the final gas-reduced fluid typically contains within a range of about 3 to 4% gases by volume, the remainder being liquids. Thus, the present gas-liquid separator effectively reduces the gas volume of the produced fluid mixture by about 60 to 80%.

Referring to Figures 3A and 3B, an alternate embodiment of a gas-liquid separator of the present invention is shown and generally designated 150. The gas-liquid separator 150 of Figures 3A and 3B is essentially identical to the gas-liquid separator 10 of Figures 1A and 1B except for the configuration of the fixed auger, the

position of the artificial lift assembly relative to the fixed auger, and the position of the second internal annulus opening relative to the production perforations. Accordingly, elements of the gas-liquid separator 150 in Figures 3A and 3B which correspond to elements of the gas-liquid separator 10 in Figures 1A and 1B are identified by the same reference characters.

Referring additionally to Figures 4 and 5, the fixed auger of the gas-liquid separator 150 has a dual fin configuration comprising a first pitched plate 152 and a second pitched plate 154. The first and second pitched plates 152, 154 are configured substantially identical to each other. Each pitched plate 152, 154 is arcuately shaped and forms a half circle. As such, each pitched plate 152, 154 has a one-half turn to partially encircle the external tube 30. The present invention is not limited by the number of turns of each pitched plate 152, 154 about the external tube 30, but each pitched plate 152, 154 has at least a partial turn, preferably at least a one-quarter turn, and most preferably at least a one-half turn about the external tube 30.

Each pitched plate 152, 154 has a start point 156, an end point 158, an upper face 160, a lower face 162, an inner edge 164, and an outer edge 166. Each pitched plate 152, 154 is preferably fixed to the intermediate portion 38 of the external tube 30 and is positioned in the external annulus 62 at a pitch angle of about 45° with reference to the longitudinal axes of the well bore 12 and the external and internal tubes 30, 32. The pitched plates 152, 154 are positioned in parallel to one another. The term "parallel" refers to a position, whereby the first pitched plate 152 is substantially fixed to the opposite side of the external tube 30 from the second pitched plate 154, but at substantially the same vertical level on the external tube 30. The linear height of each pitched plate 152, 154 from the start point 156 to the end point 158, for example, is on the order of about 1 to 2 feet. The width of the upper face 160 and the lower face 162 are identical, being about equal to the width of the external annulus 62. The inner edge 164 of each pitched plate 152, 154 conformingly and fixably engages the outer face 42 of the external tube 30 along the intermediate portion 38 of the external tube 30. The junction of the inner edge 164 and the outer face 42 preferably essentially forms a seal to prevent the substantial flow of fluids between the inner edge 164 and the outer face 42.

Each pitched plate 152, 154 has a diameter approximately equal to the inside diameter of the casing 16 (or the well bore face in the situation of an open well bore). As such, the outer edge 166 of each pitched plate 152, 154 is configured to conformingly engage the casing inner face 20 (or the well bore face in the situation of an open well bore). The outer edge 166 and the casing inner face 20 (or the well bore face in the situation of an open well bore) are preferably in tight fitting engagement with one another to essentially form a seal which prevents the substantial flow of fluids between the outer edge 166 and the casing inner face 20 (or the well bore face in the situation of an open well bore). The start and end point 156, 158 and upper and lower faces 160, 162 of each pitched plate 152, 154, the outer face 42 of the external tube 30 and the casing inner face 20 (or the well bore face in the situation of an open well bore) bound restrictive first and second curved flow channels 168, 170, respectively, through the external annulus 62, which are more specifically termed first and second pitched channels. Each pitched channel 168, 170 corresponds to each pitched plate, respectively, insofar as each pitched channel 168, 170 preferably descends in at least a partial turn, more preferably at least a one-quarter turn, and most preferably a one-half turn about the outer face 42 of the external tube 30, as shown in the present embodiment.

The down hole artificial lift assembly 124 is integral with the gas-liquid separator 150 and is positioned in-line with the internal tube 32 between the perforated disk 104 and the internal tube interior perforations 100 beneath the first and second pitched plates 152, 154. The auxiliary line 136 extends from the earthen surface alongside the production tubing string 134, the top end portion 44 of the internal tube 32, the external tube 30 (down to the bottom end portion 36), and the bottom end portion 46 of the internal tube 32 until reaching the artificial lift assembly 124. An opening (not shown) is formed through the bottom end portion 36 which directs the auxiliary line 136 from the outer face 42 of the external tube 30 into the external tube interior 66 at the bottom end portion 36. A plurality of metal straps 172, such as stainless steel bands, are periodically provided along the length of the gas-liquid separator 150, which fixably secure the auxiliary line 136 to the top end portion 44 of the internal tube 32, the external tube 30 down to the bottom end portion 36, and the bottom end portion 46 of the internal tube 32 down to the artificial lift

assembly 124. The relative positions of the auxiliary line 136, external tube 30, internal tube 32, and casing 16 are shown with reference to Figure 6.

Operation of the gas-liquid separator 150 is substantially similar to operation of the gas-liquid separator 10 described above. Operation of the gas-liquid separator is summarized hereafter with continuing reference to Figures 3A and 3B and further reference to Figures 7A and 7B. The gas-liquid separator 150 (including the integral artificial lift assembly 124) and production tubing string 134 are mounted in series within the well bore 12. In accordance with the present embodiment, the first and second pitched plates 152, 154 are positioned in the well bore 12 below the production perforations 26 and the external tube perforations 118 are positioned in the well bore 12 above the production perforations 26. The produced fluids designated by the arrow 138 are displaced from a depth point in the fluid production zone 28 through the production perforations 26 into the external annulus 62 below the external tube perforations 118. The produced fluids 138 diverge at the production perforations 126 into the produced free gas designated by the arrows 140 and the produced fluid mixture designated by the arrows 142. The produced free gas 140 is conveyed up the casing/tubing annulus to the well head, while the produced fluid mixture 142 descends down the external annulus 62. The produced fluid mixture conveyance chamber, which is the segment of the external annulus 62 between the production perforations 26 and the start points 156 of the first and second pitched plates 152, 154, directs the produced fluid mixture 142 downward to the pitched plates 152, 154.

The gas-liquid separation chamber, which is defined by the first and second pitched channels 168, 170, centrifugally separates the oil, water and gas in the produced fluid mixture 142 in substantially the same manner as described above with respect to the gas-liquid separator 10. The circular fluid flow through the gas-liquid separation chamber causes vortex formation in the separated free gas recovery chamber, which is the segment of the external annulus 62 below the first and second pitched channels 168, 170 and above the perforated disk 104. The separated free gas 146 is forced into the internal annulus 72 via the lower first internal annulus opening 96, 98 and conveyed up through the internal annulus 72 to the external tube perforations 118 and out into the external annulus 62 above the production

perforations 26. The separated free gas 146 mixes with the produced free gas 140 from the production perforations 26 in the external annulus 62 and continues upward as a free gas or coalesced in large gas bubbles through the casing/tubing annulus to the well head.

5 The remaining reduced-gas fluid 148 continues downward into the reduced-gas fluid recovery chamber, which is the segment of the external annulus 62 from below the perforated disk 104 to the internal tube interior perforations 100, and is drawn through the internal tube interior perforations 100 into the internal tube interior 70. The artificial lift system 124 pumps the reduced-gas fluid 148 upward through the
10 internal tube interior 70 and production tubing string 134 to the well head.

 Although the gas-liquid separator 150 is described above as being positioned in the well bore 12 with the first and second pitched plates 152, 154 below the production perforations 26 and the external tube perforations 118 above the production perforations 26, it is within the scope of the present invention to position
15 the entire gas-liquid separator 150, including the first and second pitched plates 152, 154 and external tube perforations 118, below the production perforations 26, in the manner described above with respect to the gas-liquid separator 10. Conversely, it is within the scope of the present invention, and generally preferred, to position the spiral plate 76 of the gas-liquid separator 10 below the production perforations 26
20 and the external tube perforations 118 above the production perforations 26 in the manner described above with respect to the gas-liquid separator 150.

 Further alternate embodiments of a gas-liquid separator not shown are within the scope of the present invention, wherein the fixed auger is alternately configured, but functions in substantially the same manner as the fixed augers of the above-recited embodiments to spin the produced fluid mixture about the external tube and effect centrifugal separation of the oil, water and gas in the produced fluid mixture.
25 For example, the fixed auger of an alternate gas-liquid separator may include three or more pitched plates serially and/or parallelly positioned along the length of the external tube. The term "serial" refers to a position, whereby multiple pitched or
30 spiral plates are substantially fixed to the external tube at different vertical levels on the external tube. The fixed auger of another alternate gas-liquid separator may include multiple spiral plates serially and/or parallelly positioned along the length of

2003268103 05 May 2008

- 21 -

the external tube. The fixed auger of yet another alternate gas-liquid separator may include one or more pitched plates serially and/or parallelly positioned in combination with one or more spiral plates along the length of the external tube.

5 While the foregoing preferred embodiments of the invention have been described and shown, it is understood that alternatives and modifications, such as those suggested and others, may be made thereto and fall within the scope of the invention.

10 Throughout this specification and the claims which follow, unless the context requires otherwise, the word "comprise", and variations such as "comprises" and "comprising", will be understood to imply the inclusion of a stated integer or step or group of integers or steps but not the exclusion of any other integer or step or group of integers or steps.

15 The reference in this specification to any prior publication (or information derived from it), or to any matter which is known, is not, and should not be taken as an acknowledgment or admission or any form of suggestion that that prior publication (or information derived from it) or known matter forms part of the common general knowledge.

2003268103 05 May 2008

- 22 -

THE CLAIMS DEFINING THE INVENTION ARE AS FOLLOWS:

1. A gas-liquid separator positionable down hole in a well bore comprising:
an external tube having an external tube interior;
5 an internal tube having an internal tube interior defining a reduced-gas fluid flowpath, wherein said internal tube is positioned in said external tube interior to form an internal annulus between said external tube and said internal tube, said internal annulus defining a free gas flowpath;
a plate having a start point and at least partially encircling said external tube to
10 form a curved flow channel defining a produced fluid mixture flowpath;
an internal annulus opening beyond said start point defining a free gas inlet port for said free gas flowpath, wherein said external tube has a flared portion positioned at or proximal to said internal annulus opening and flaring outwardly as said flared portion extends away from said start point of said plate; and
15 an internal tube interior opening beyond said start point defining a reduced-gas fluid inlet port for said reduced-gas fluid flowpath.
2. The gas-liquid separator of claim 1, wherein said internal tube has a longitudinal axis and said external tube has a longitudinal axis, and further wherein
20 said longitudinal axis of said internal tube is substantially aligned with said longitudinal axis of said external tube.
3. The gas-liquid separator of claim 1 wherein said internal tube extends from said external tube interior beyond said internal annulus opening.
25
4. The gas-liquid separator of claim 1 wherein said internal annulus opening comprises a plurality of flared perforations extending through said flared portion of said external tube.
- 30 5. The gas-liquid separator of claim 1 further comprising a disk having a plurality of disk perforations extending through said disk, wherein said disk is positioned above said internal tube interior opening and below said internal annulus opening.

2003268103 05 May 2008

- 23 -

6. The gas-liquid separator of claim 1 wherein said internal annulus opening is a first internal annulus opening, said gas-liquid separator further comprising a second internal annulus opening beyond said start point of said plate defining a free gas outlet port for said free gas flowpath.
- 5 7. The gas-liquid separator of claim 1 further comprising an artificial lift assembly positioned below said plate.
8. The gas-liquid separator of claim 1 wherein said internal tube interior opening
10 comprises a plurality of inlet perforations.
9. The gas-liquid separator of claim 1 wherein said plate is a spiral plate.
10. The gas-liquid separator of claim 1 wherein said plate is a pitched plate.
- 15 11. The gas-liquid separator of claim 10 wherein said pitched plate is a first pitched plate, said gas-liquid separator further comprising a second pitched plate aligned in parallel or in series with said first pitched plate.
- 20 12. A gas-liquid separator positionable down hole in a well bore comprising:
an external tube having an external tube interior;
an internal tube having an internal tube interior defining a reduced-gas fluid flowpath, wherein said internal tube is positioned in said external tube interior to form an internal annulus between said external tube and said internal tube defining a free
25 gas flowpath;
means for spinning a produced fluid mixture about said external tube;
an internal annulus opening through said external tube defining a free gas inlet port for said free gas flowpath, wherein said external tube has a flared portion positioned at or proximal to said internal annulus opening and flaring outwardly as
30 said flared portion extends away from said spinning means; and
an internal tube interior opening through said internal tube defining a reduced-gas fluid inlet port for said reduced-gas fluid flowpath.

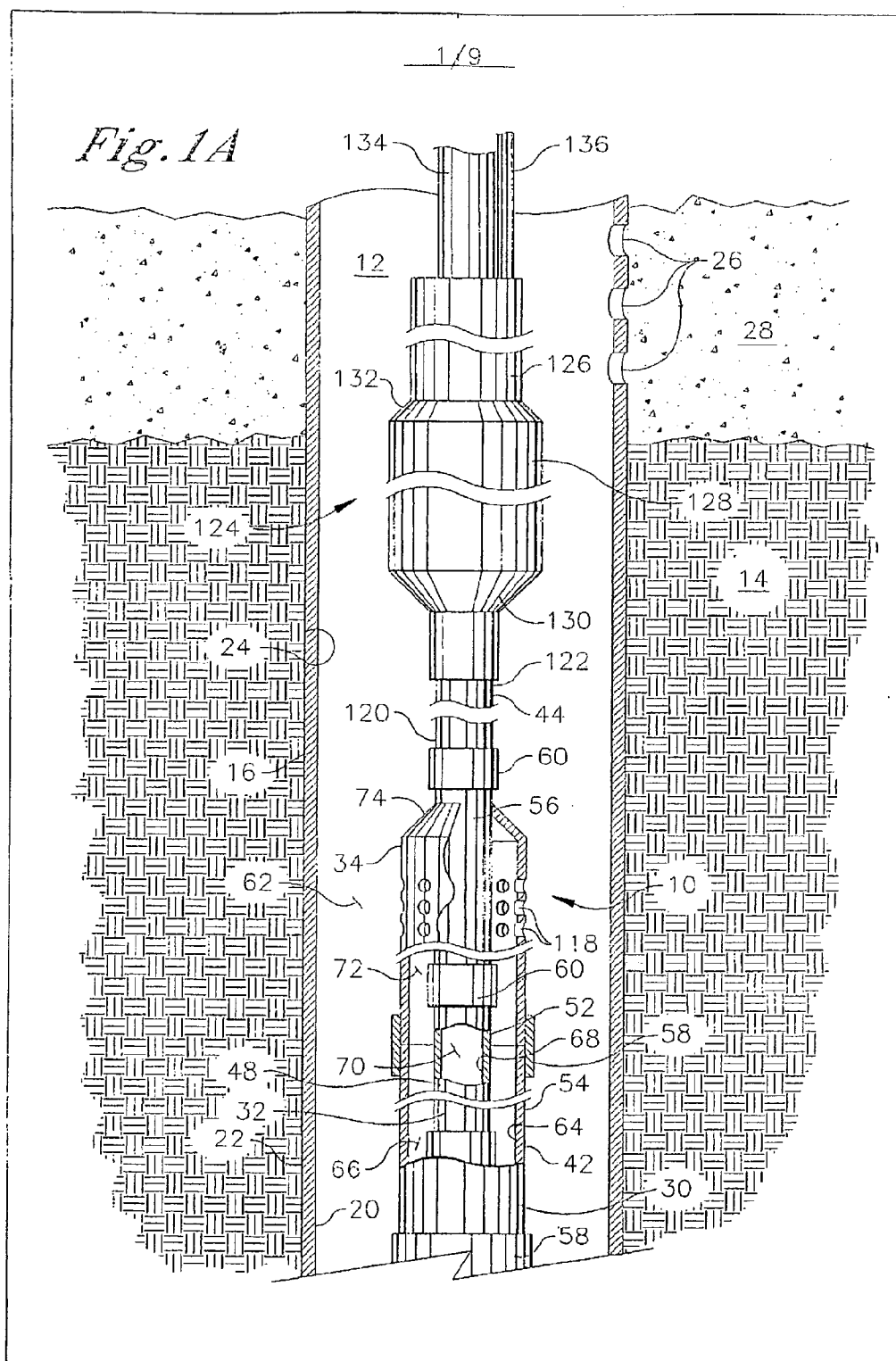
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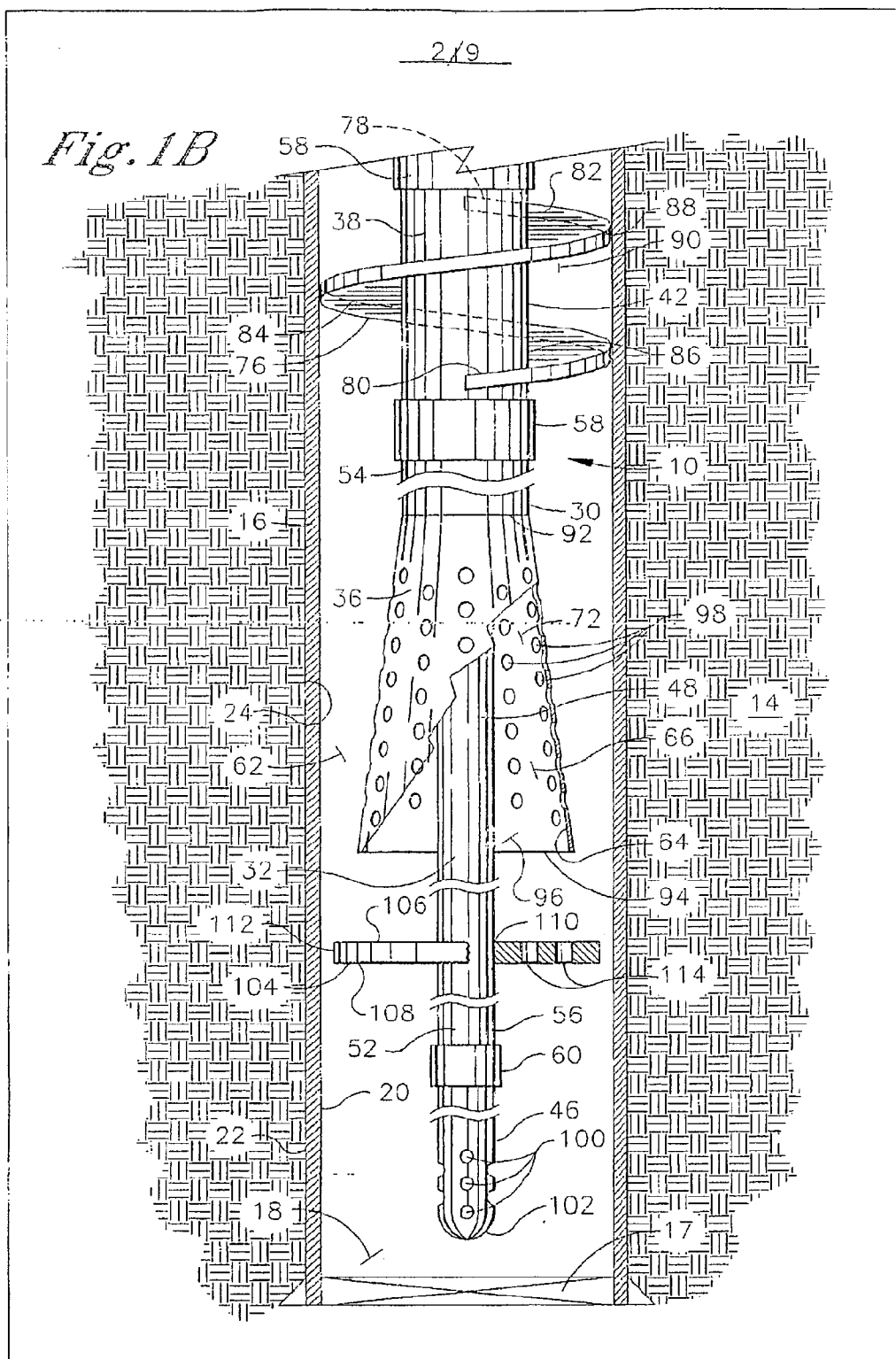
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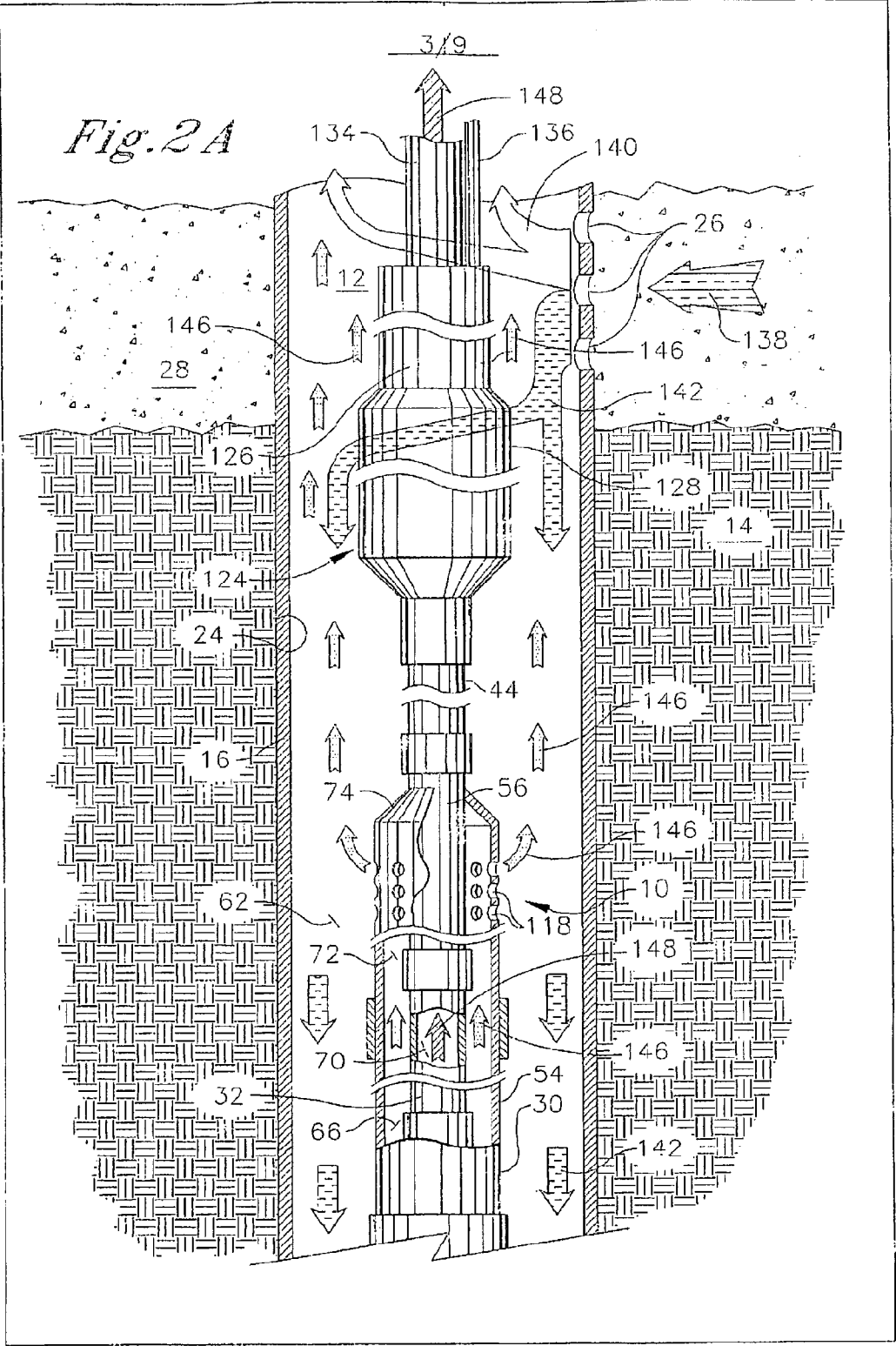
13. The gas-liquid separator of claim 12 wherein said internal annulus opening is a first internal annulus opening, said gas-liquid separator further comprising a second internal annulus opening through said external tube defining a free gas outlet port for said free gas flowpath, wherein said first and second internal annulus openings are
5 positioned on opposite sides of said spinning means.

14. The gas-liquid separator of claim 12 wherein said spinning means is essentially static relative to said external tube.

10 15. A gas-liquid separator positionable down hole in a well bore, substantially as hereinbefore described, with reference to the accompanying drawings.







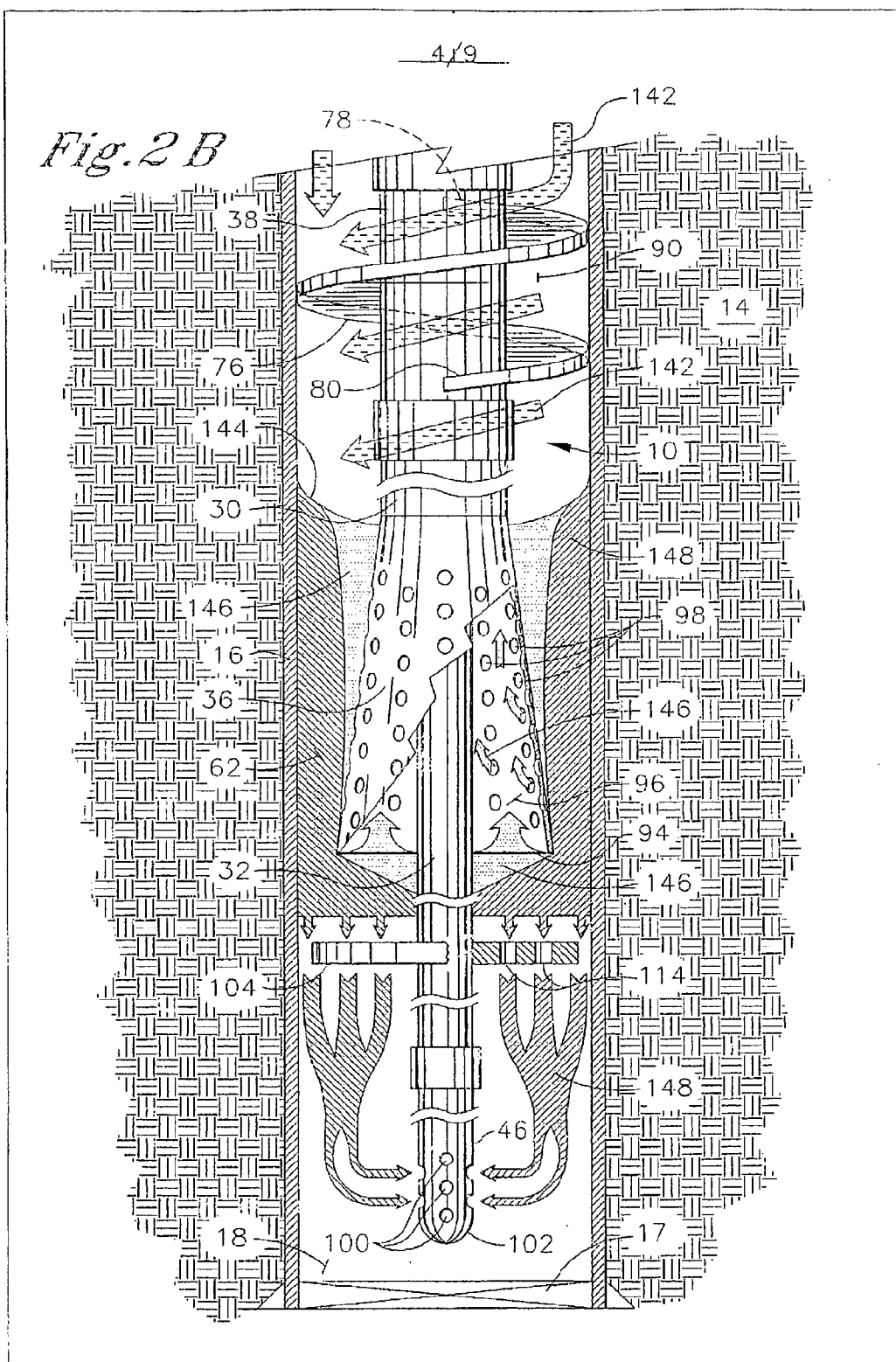
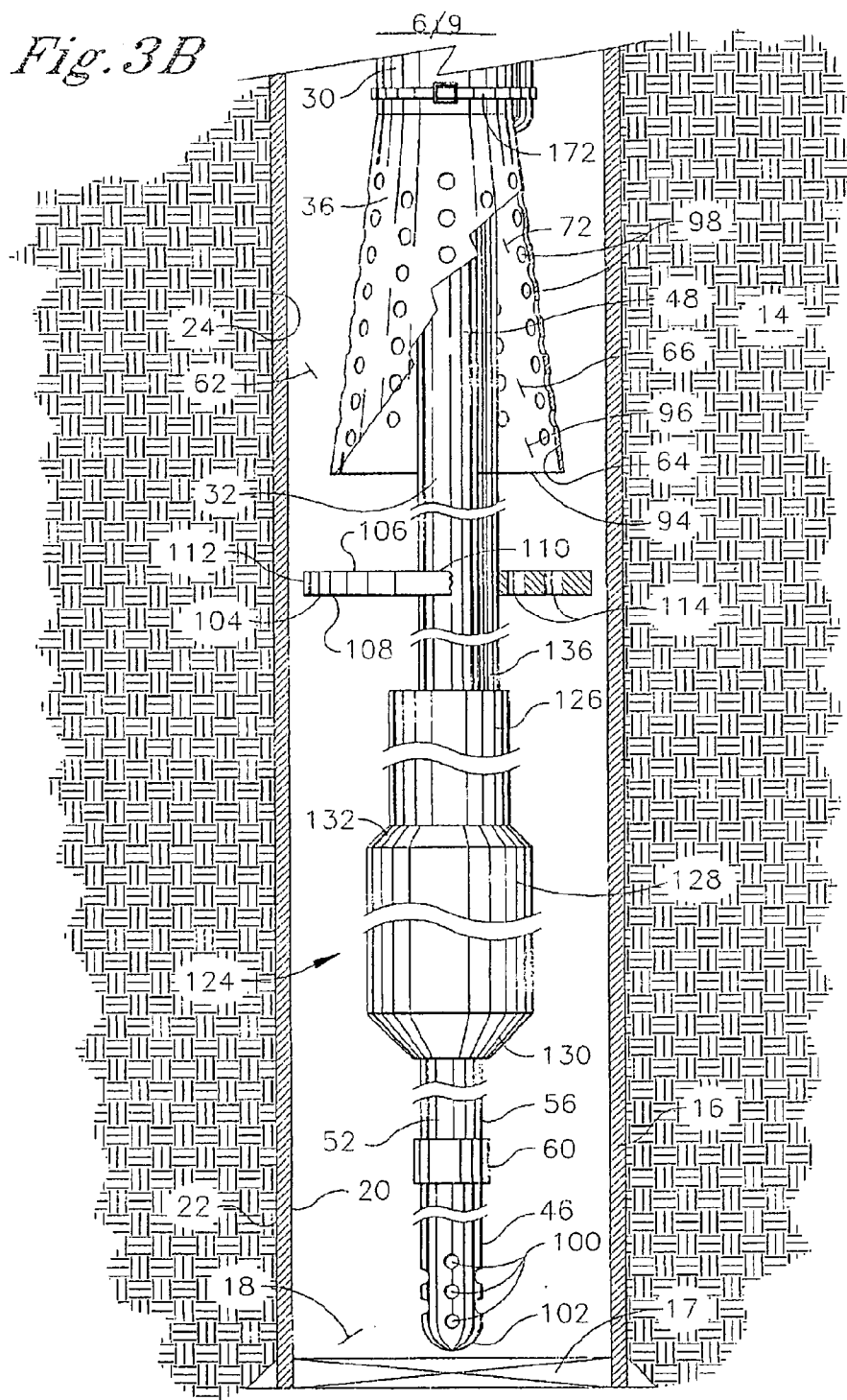


Fig. 3B



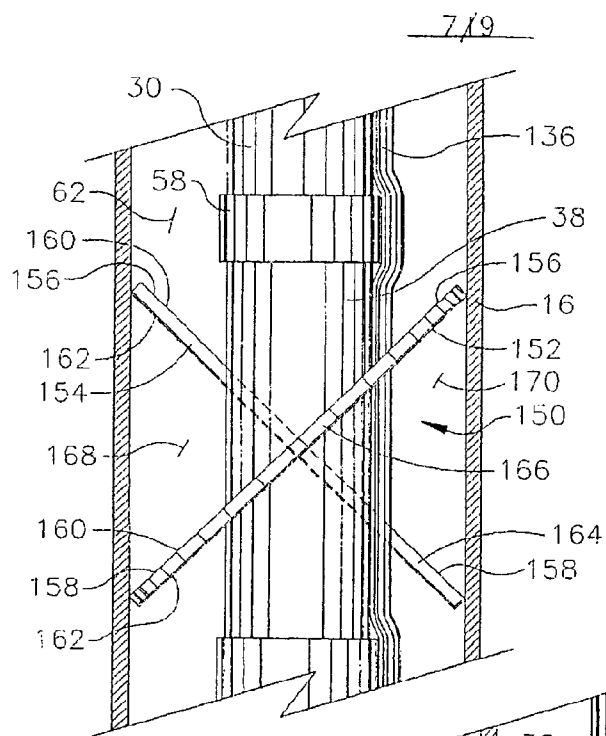


Fig. 4

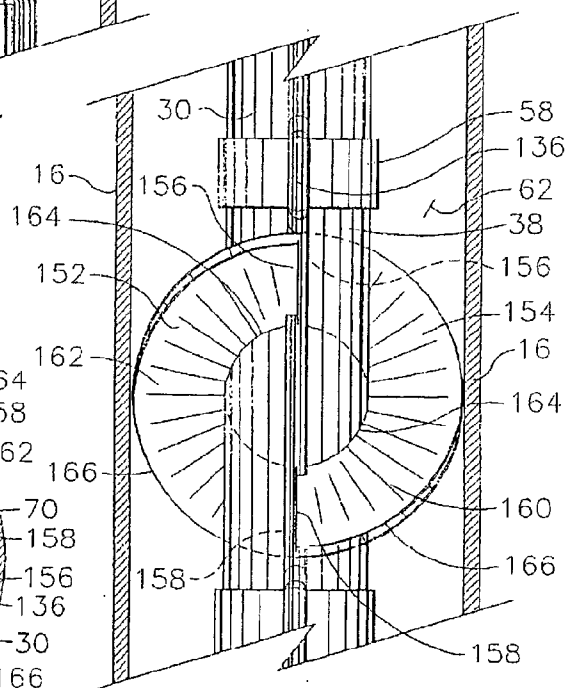


Fig. 5

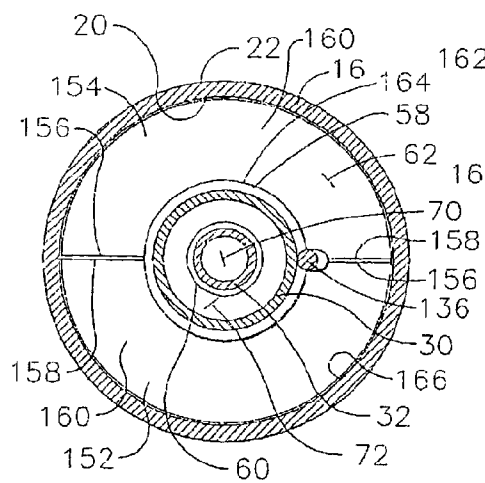


Fig. 6

