



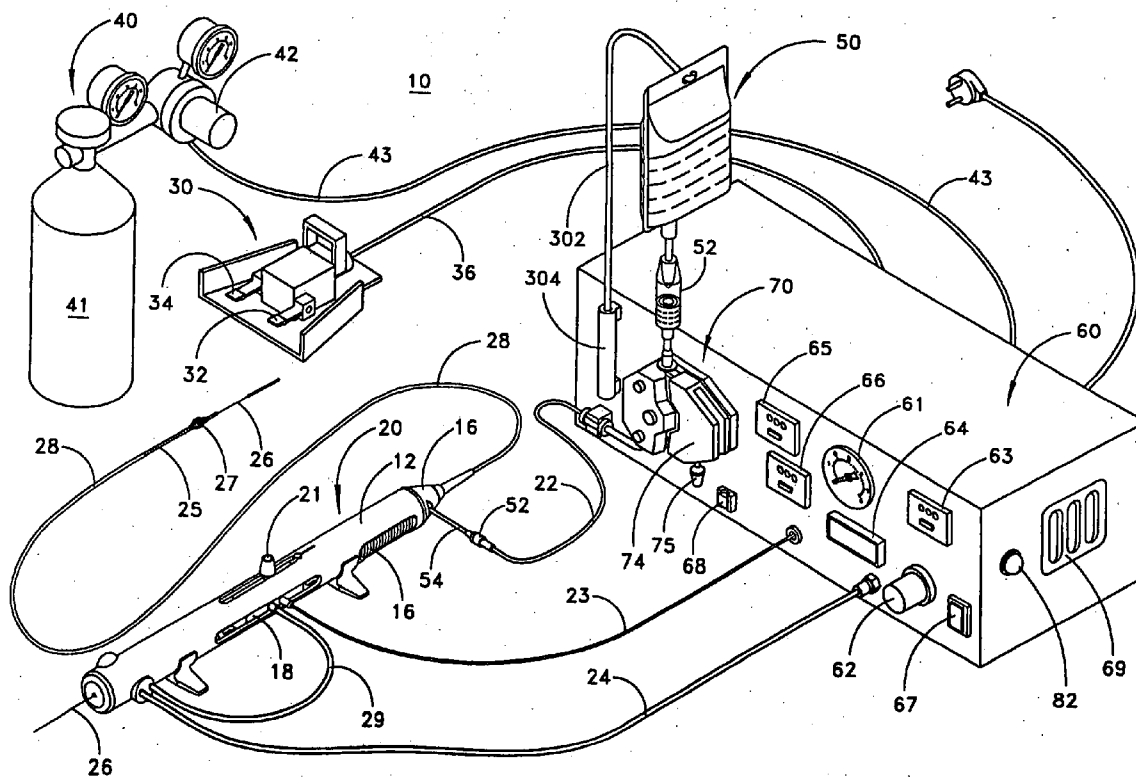
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(19) **United States**(12) **Patent Application Publication**
Shturman et al.(10) **Pub. No.: US 2006/0271242 A1**(43) **Pub. Date: Nov. 30, 2006**(54) **SYSTEM FOR CONTROLLING A FLOW OF
FLUID THROUGH A ROTATIONAL
ATHERECTOMY DEVICE****Related U.S. Application Data**(62) Division of application No. 10/272,126, filed on Oct.
16, 2002.(60) Provisional application No. 60/348,188, filed on Oct.
19, 2001.(75) Inventors: **Leonid Shturman**, Greenwich, CT
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Malgichev, Moscow (RU)**Publication Classification**(51) **Int. Cl.**
G05D 7/00 (2006.01)(52) **U.S. Cl.** **700/282**

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Minneapolis, MN 55344-7704 (US)(73) Assignee: **Shturman Cardiology Systems**(21) Appl. No.: **11/432,162**(22) Filed: **May 11, 2006****ABSTRACT**

A method system and controller for controlling fluid flow in a rotational atherectomy device. A source of fluid is provided through a pump to the rotational atherectomy device, wherein the pump maintains the fluid flow at a minimal rate during a time period when a drive shaft of the device is not rotating. A first control is activated to increase a rate of the fluid flow and second control is activate to initiate a rotation of the drive shaft during another time period when the fluid flow is at the increased rate.



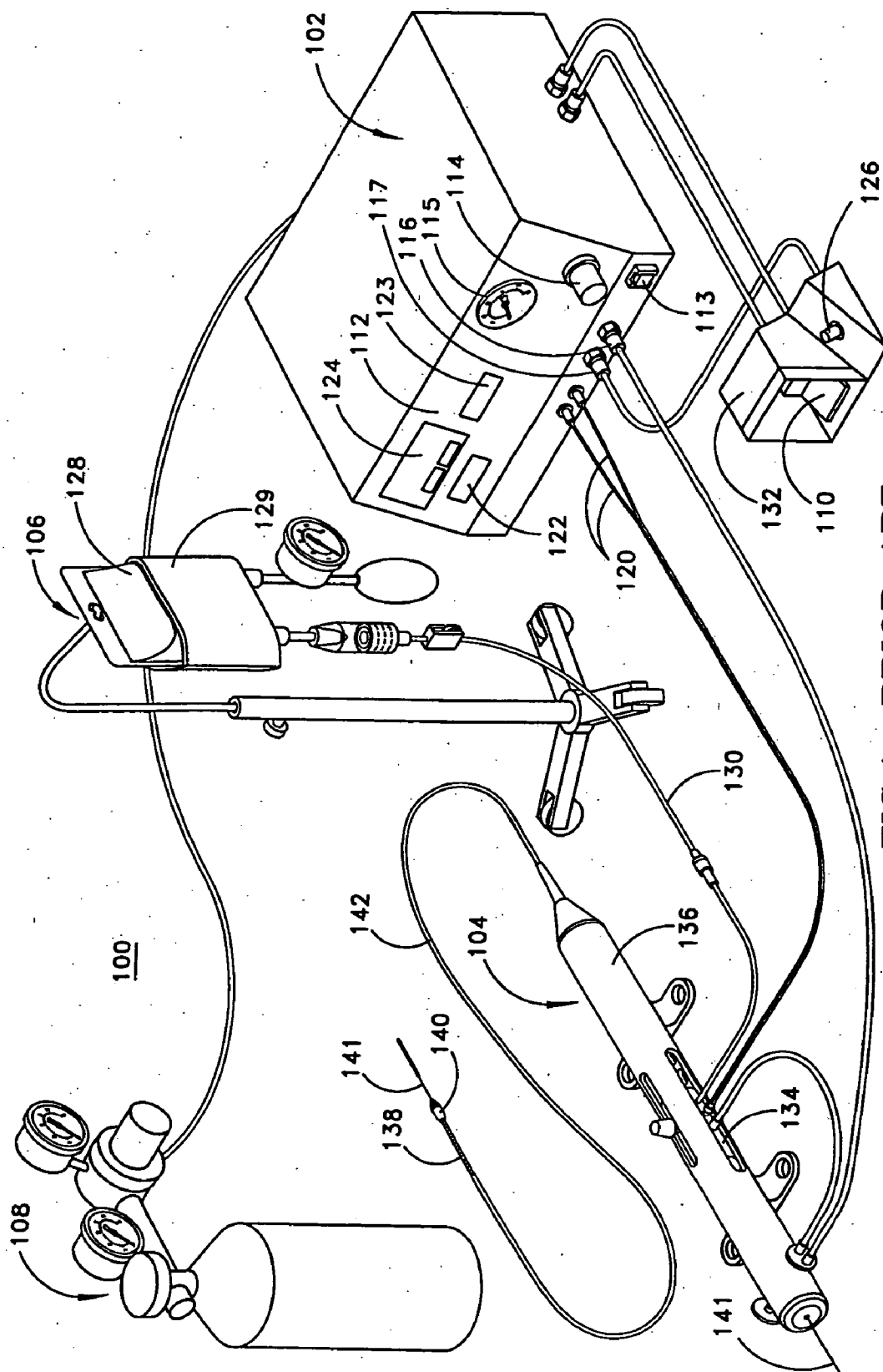
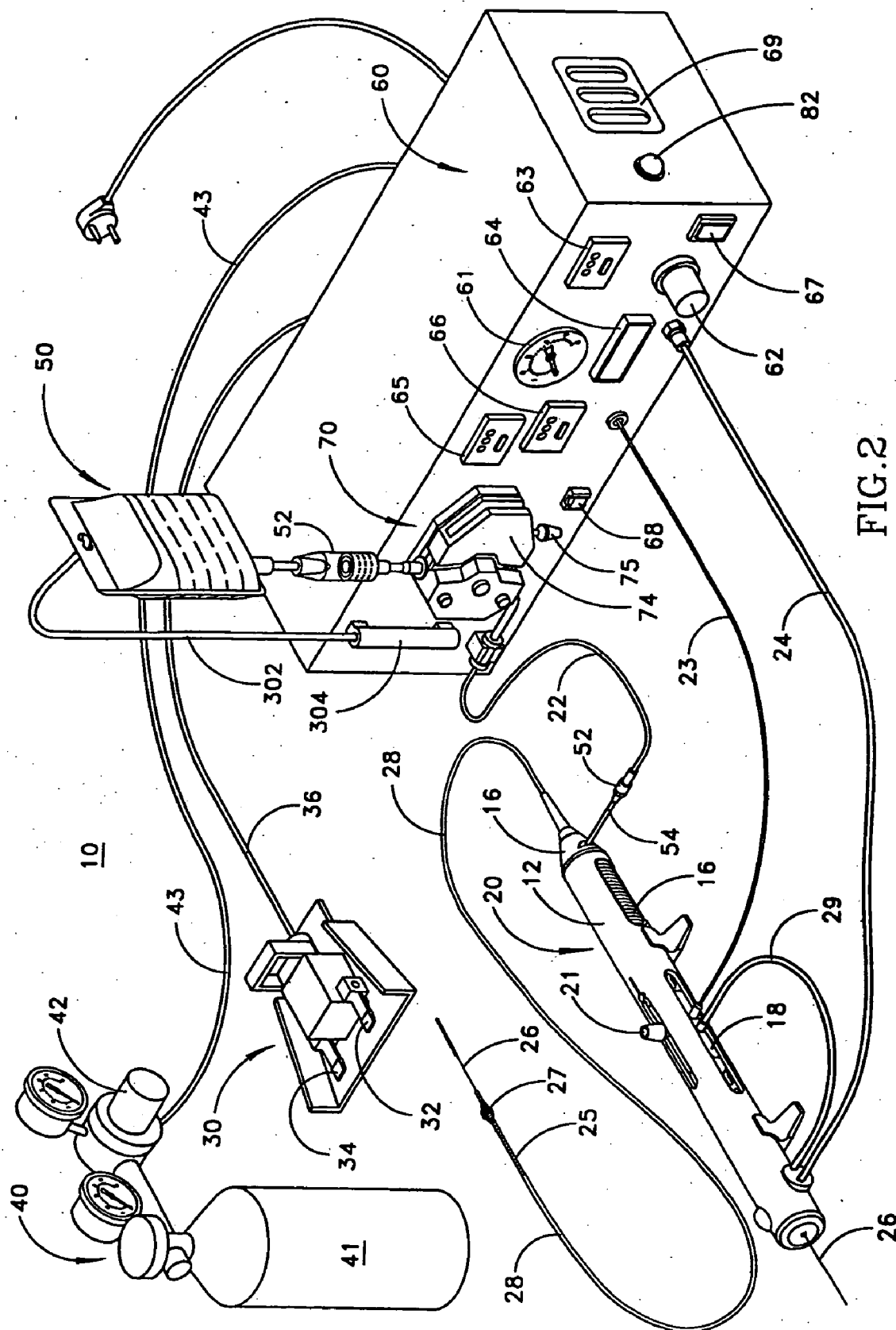


FIG.1 PRIOR ART



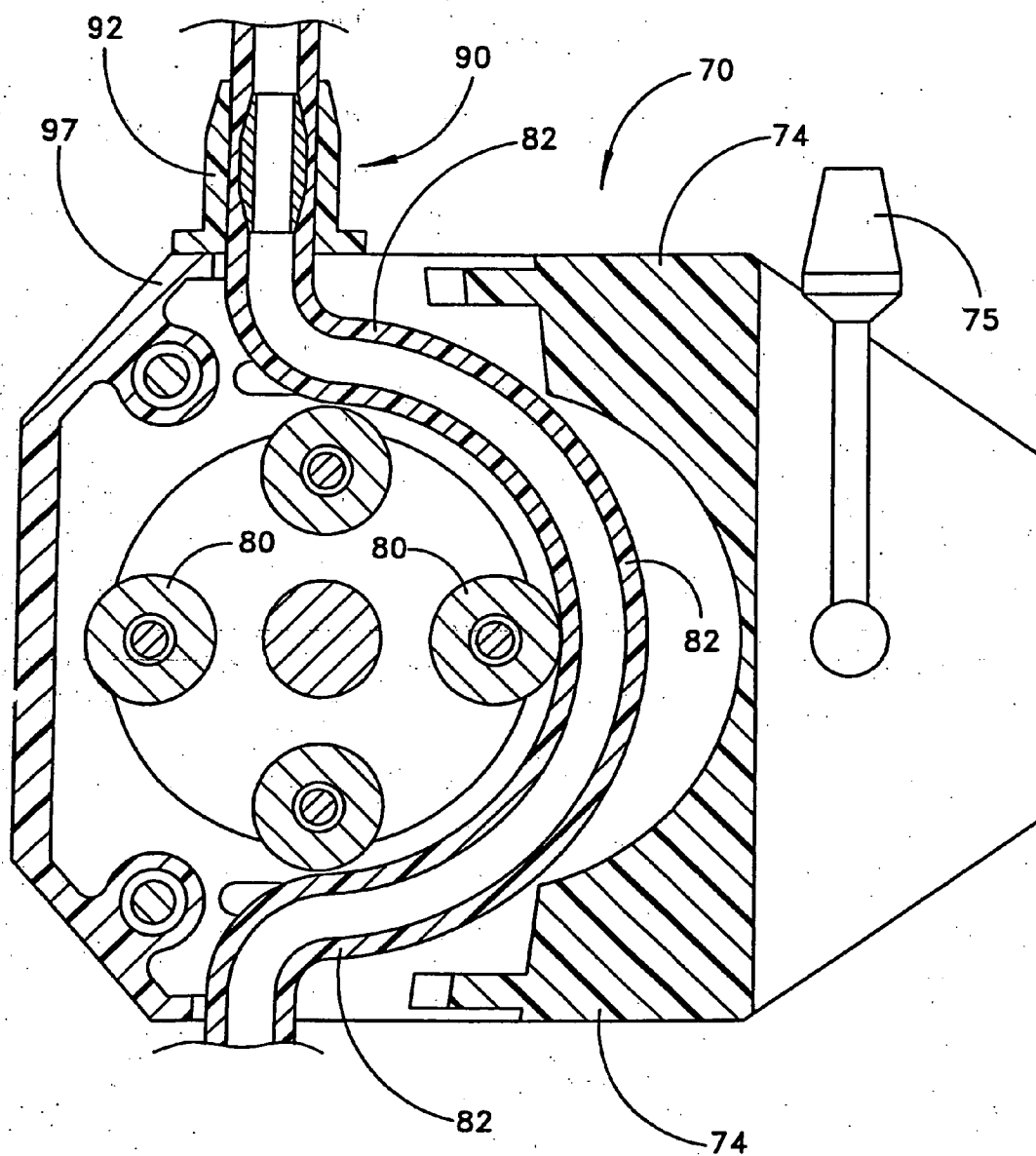


FIG. 3

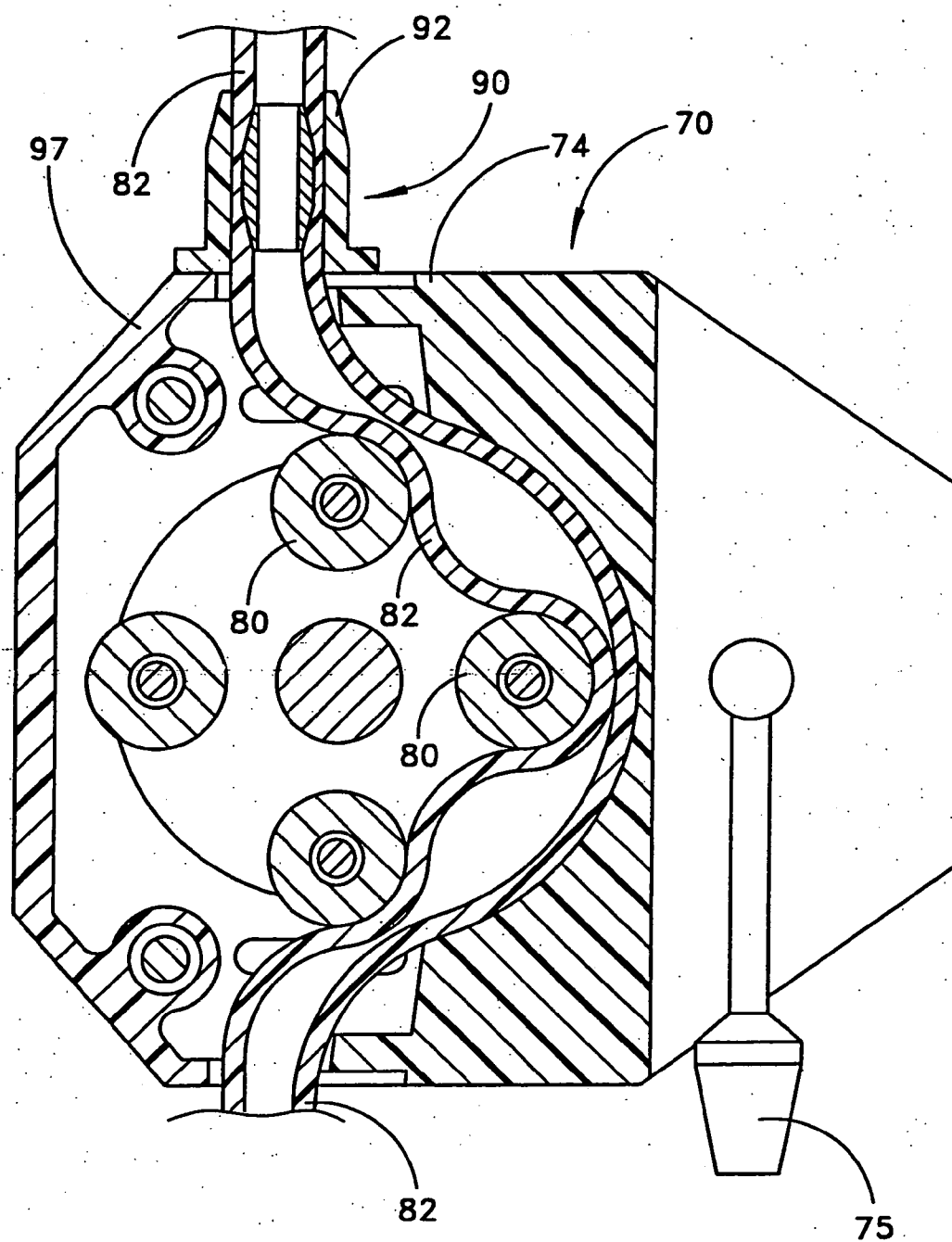


FIG. 4

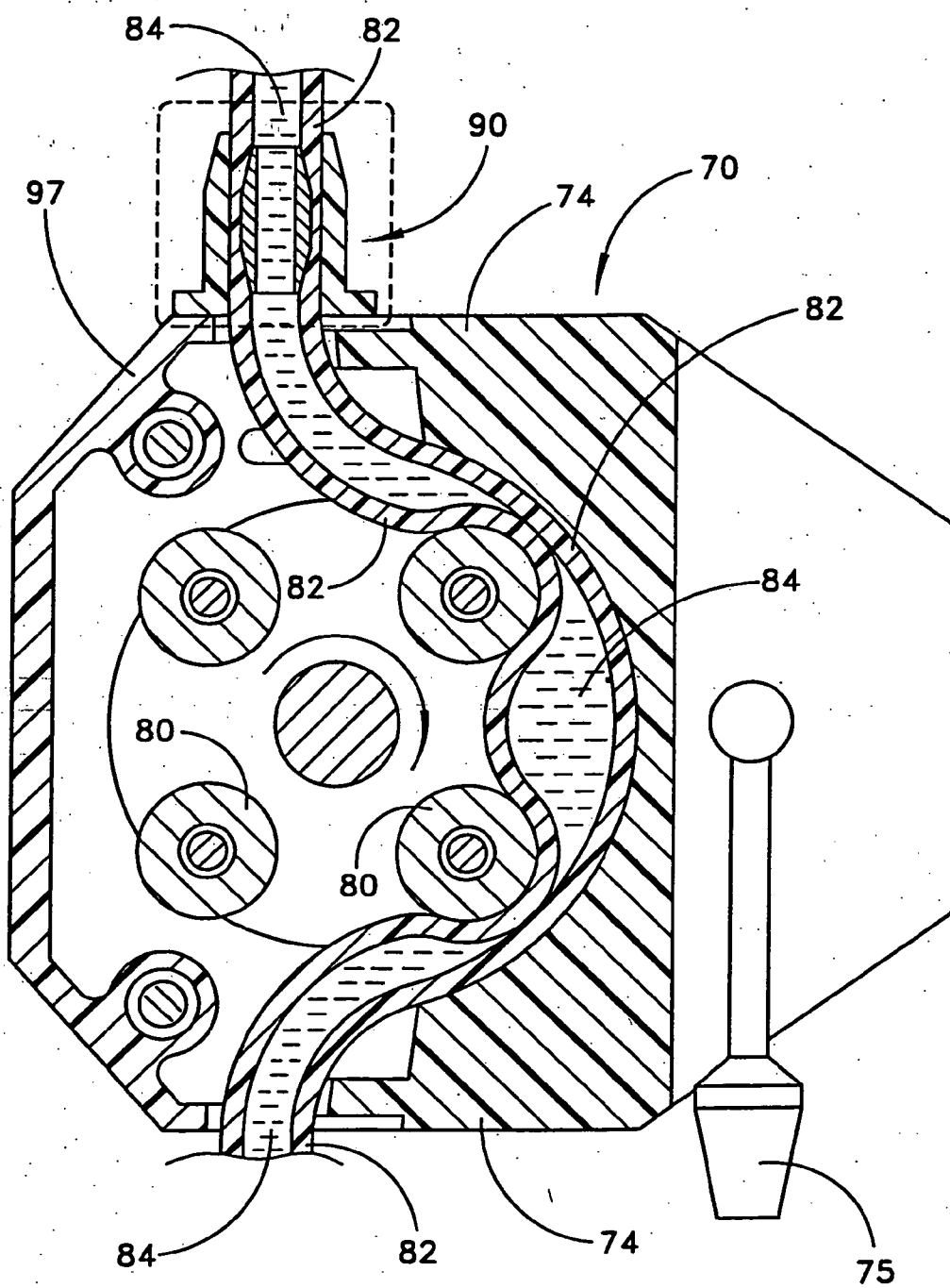


FIG. 5

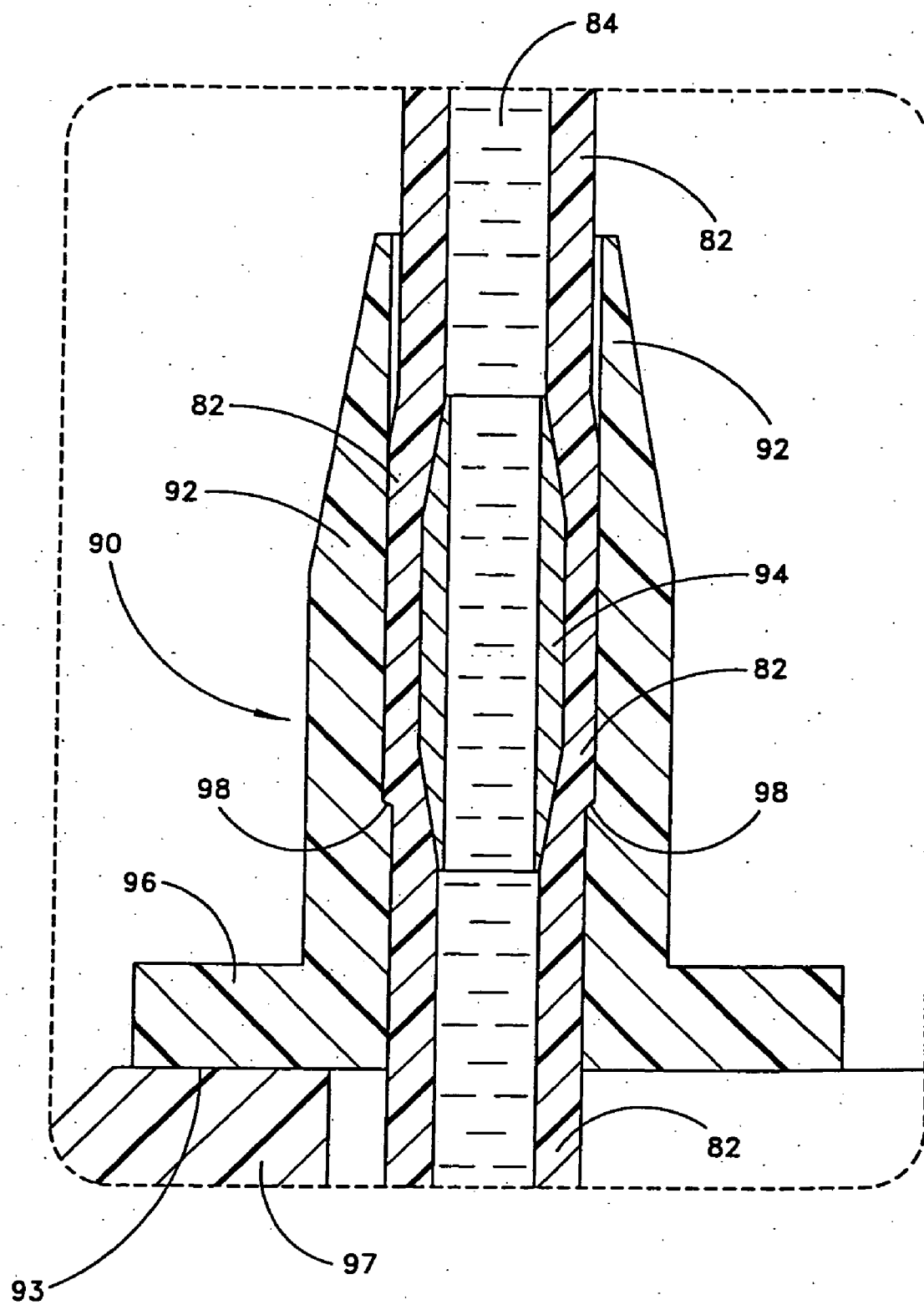


FIG. 6

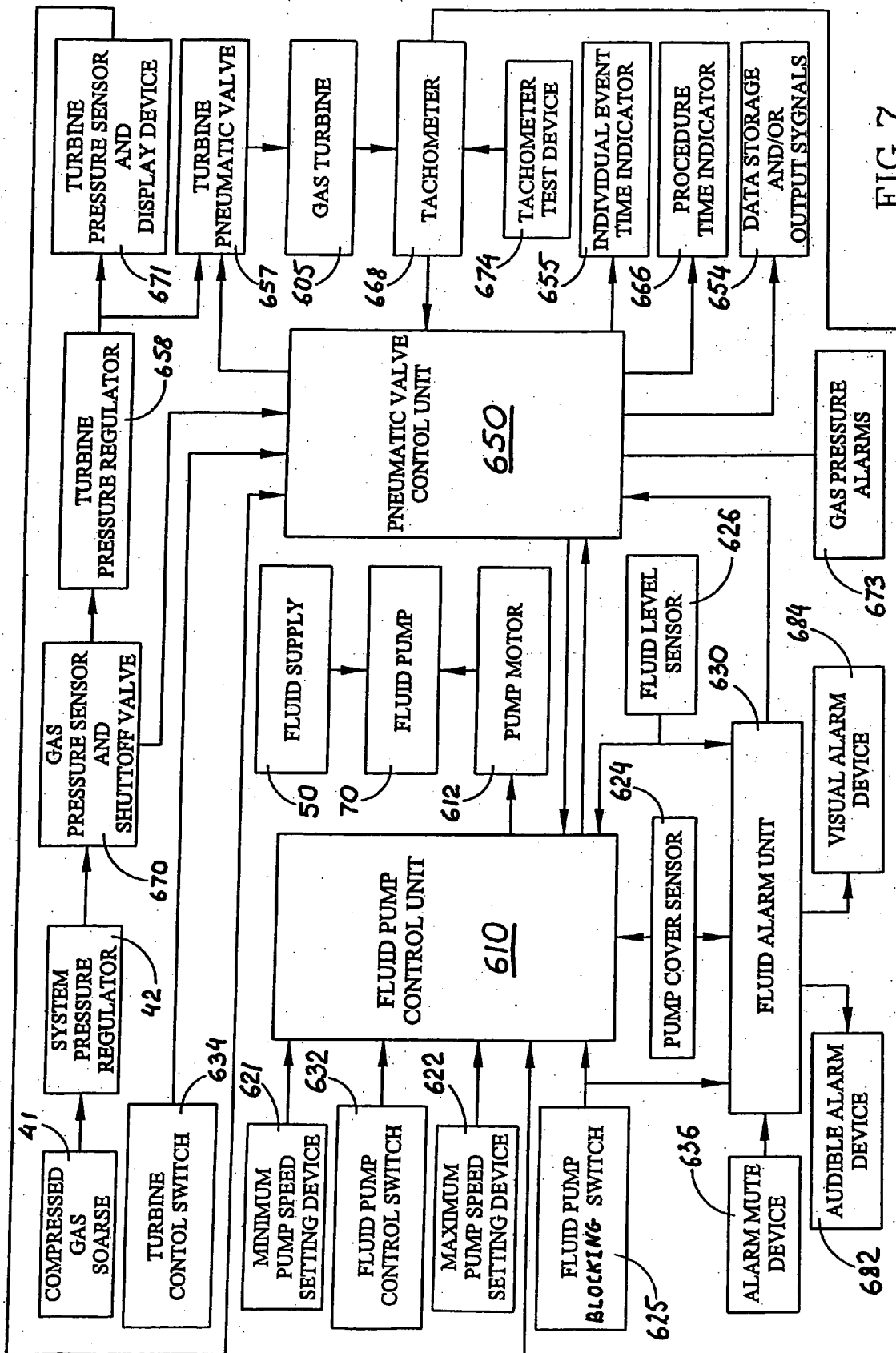


FIG. 7

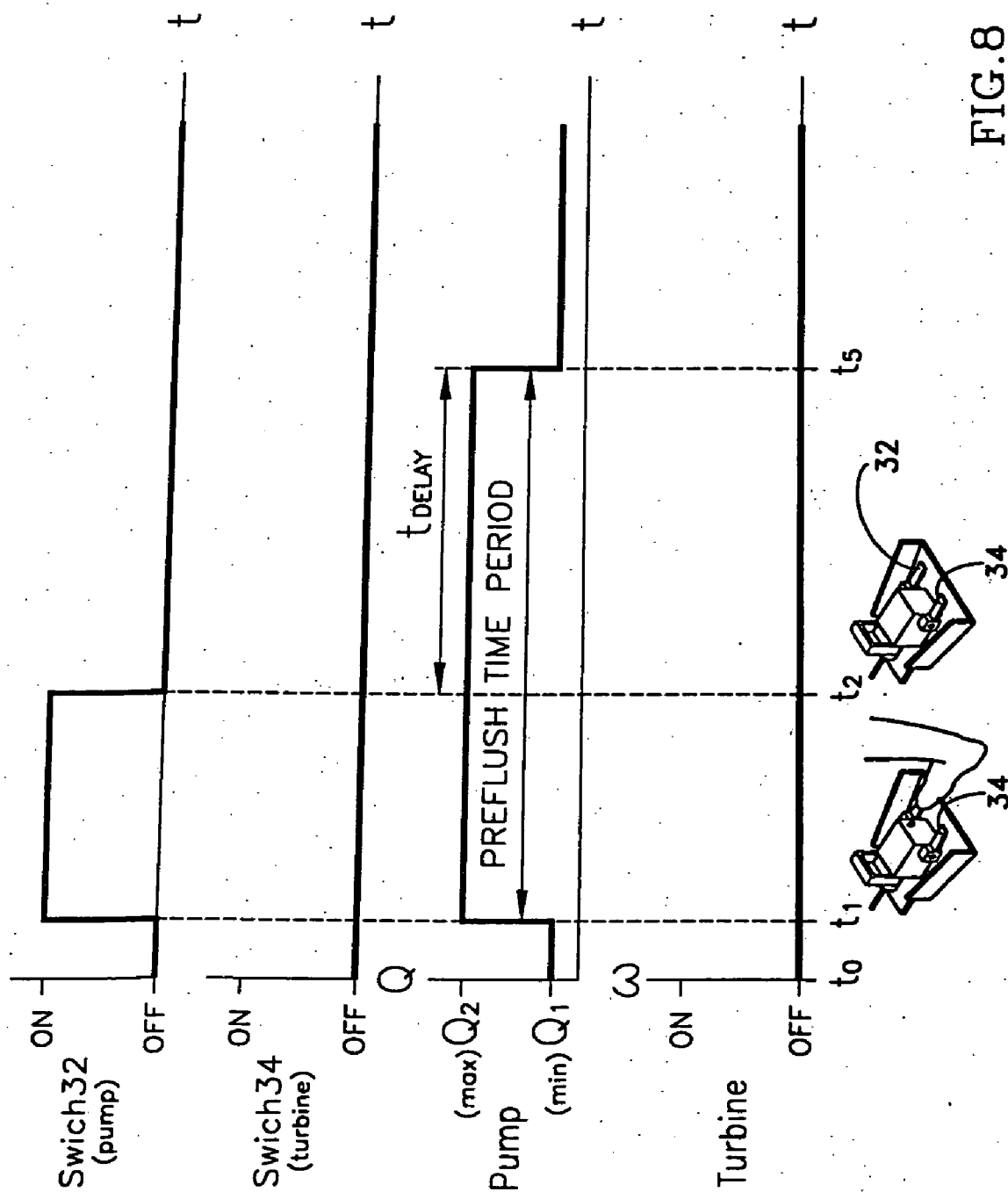


FIG. 8

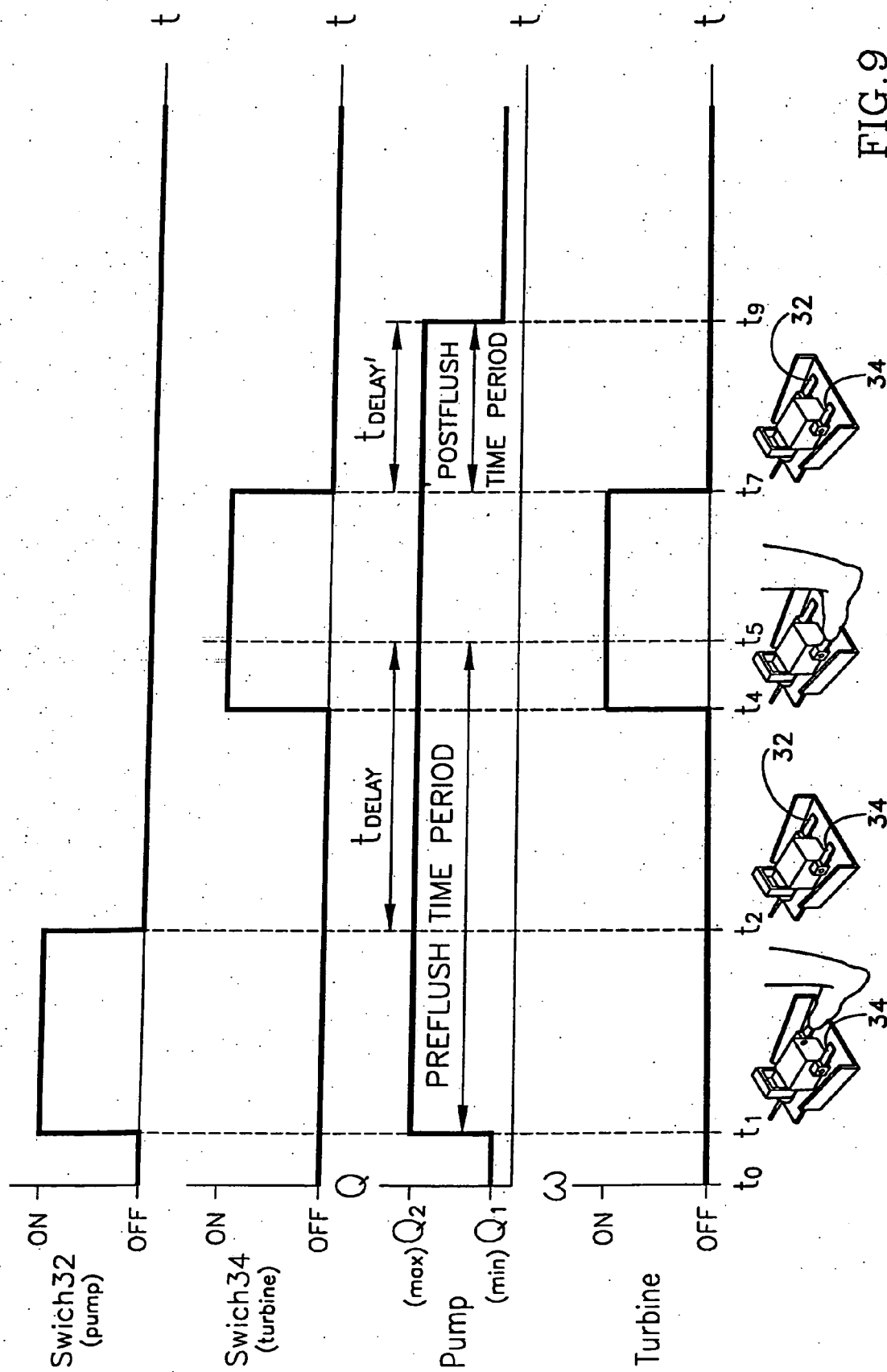


FIG. 9

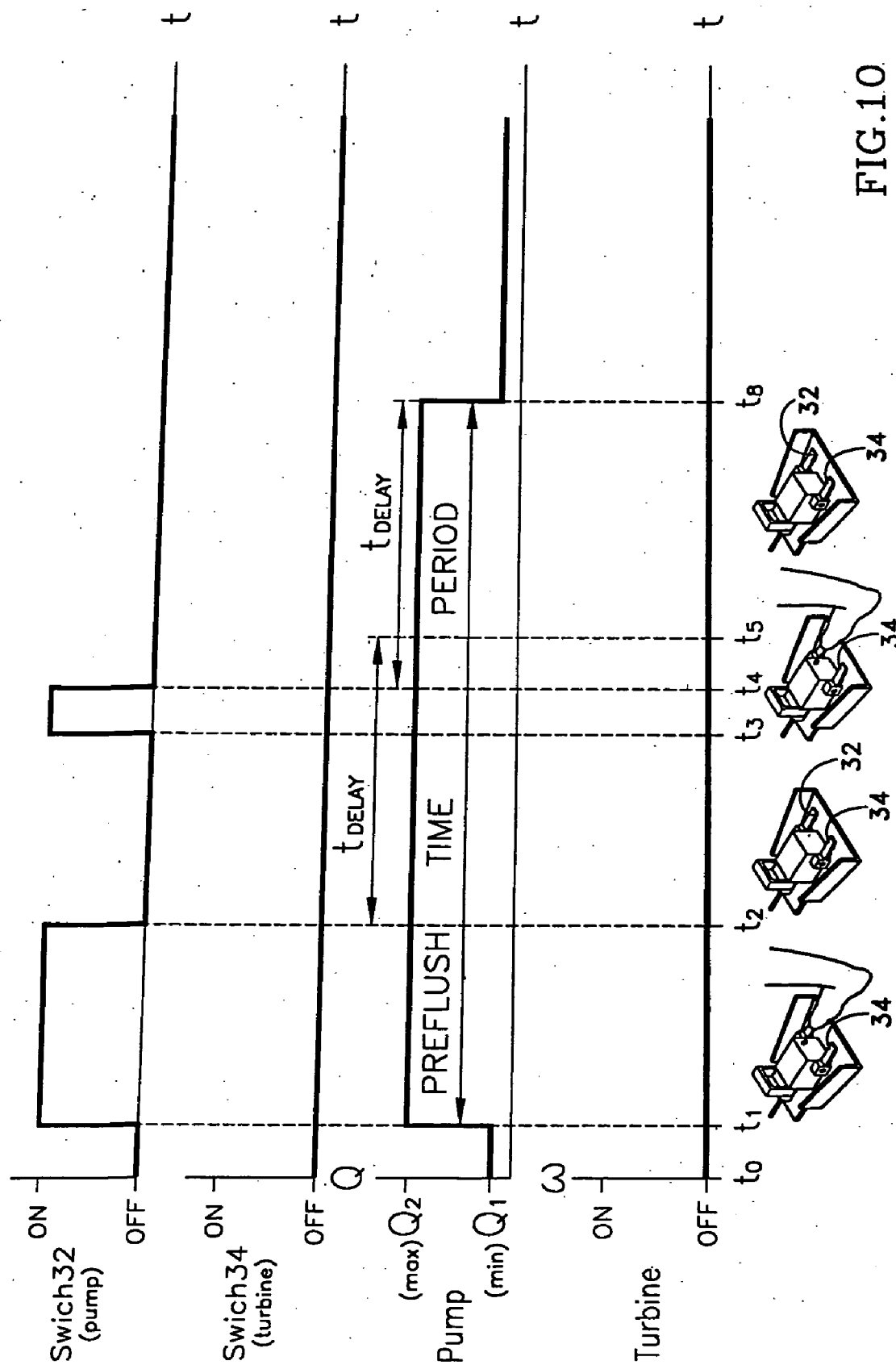


FIG.10

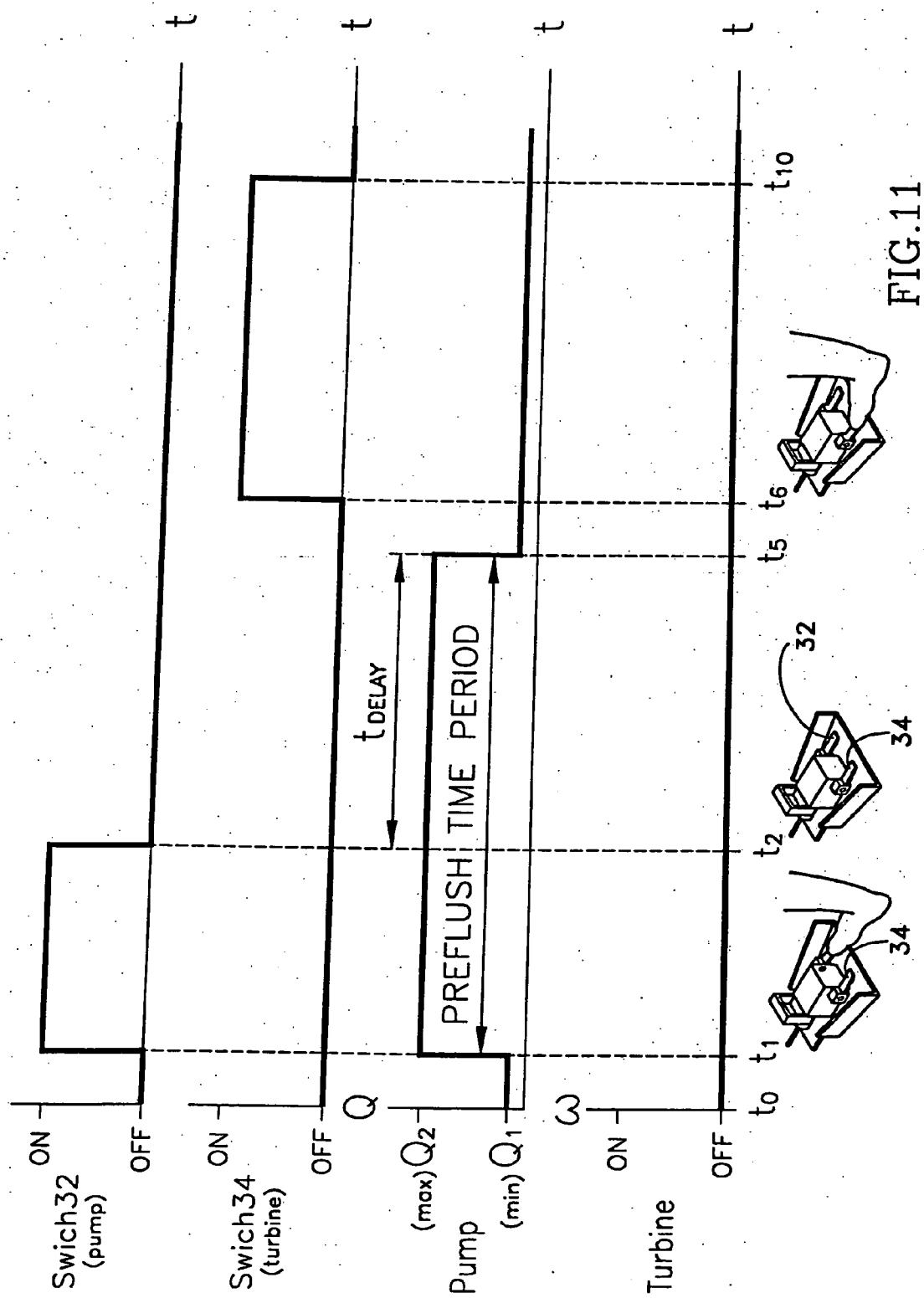


FIG.11

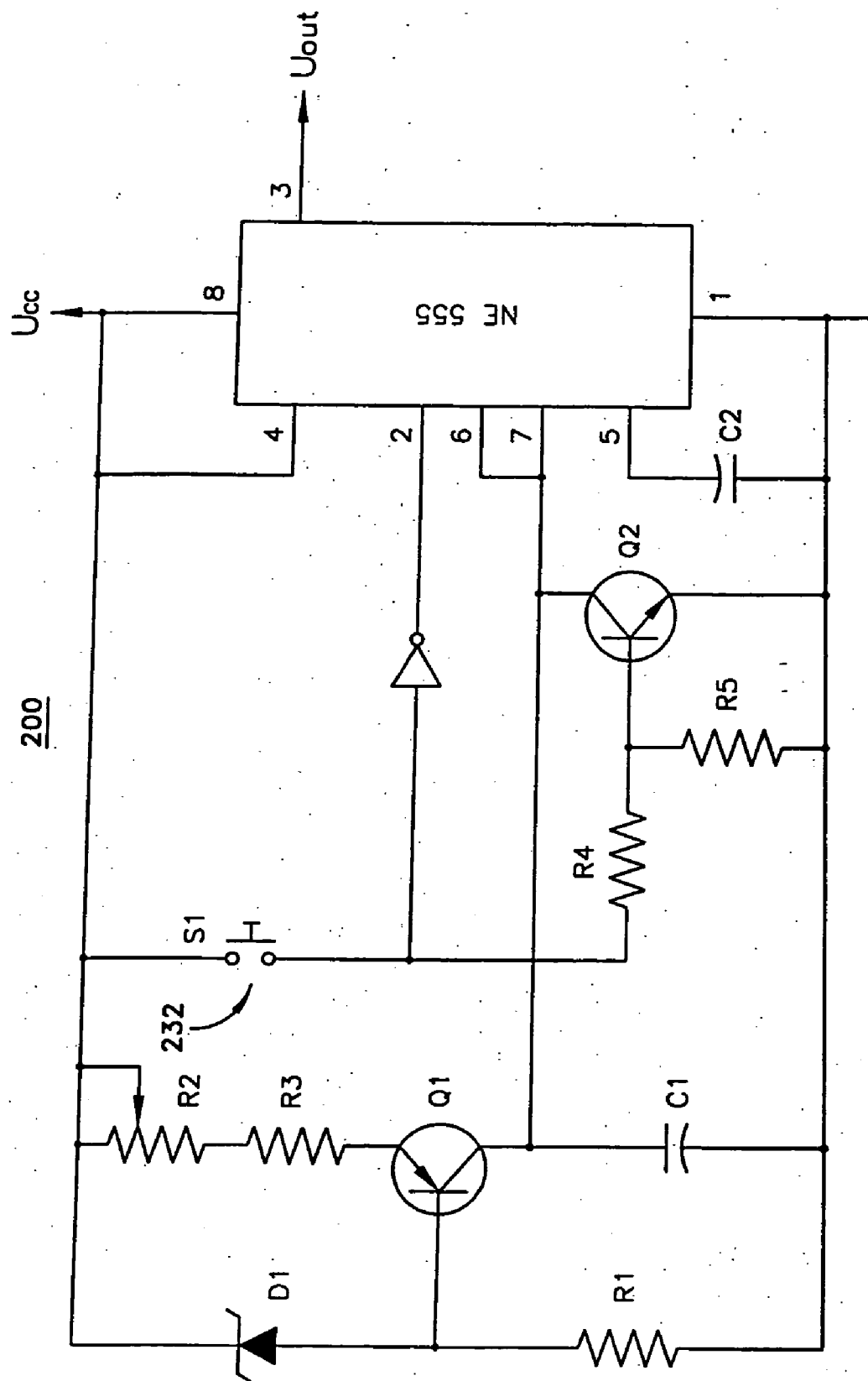


FIG.12A

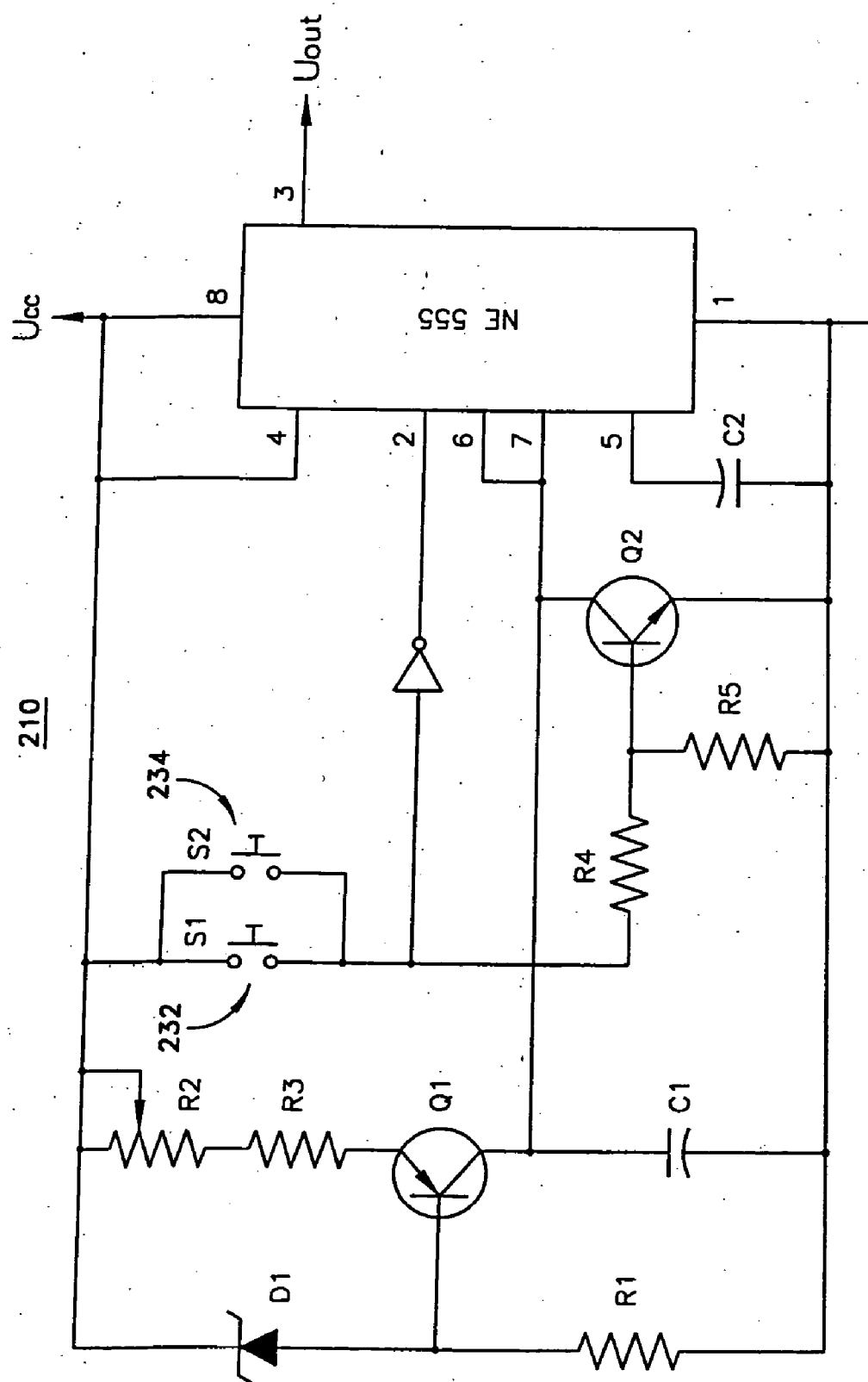


FIG. 12B

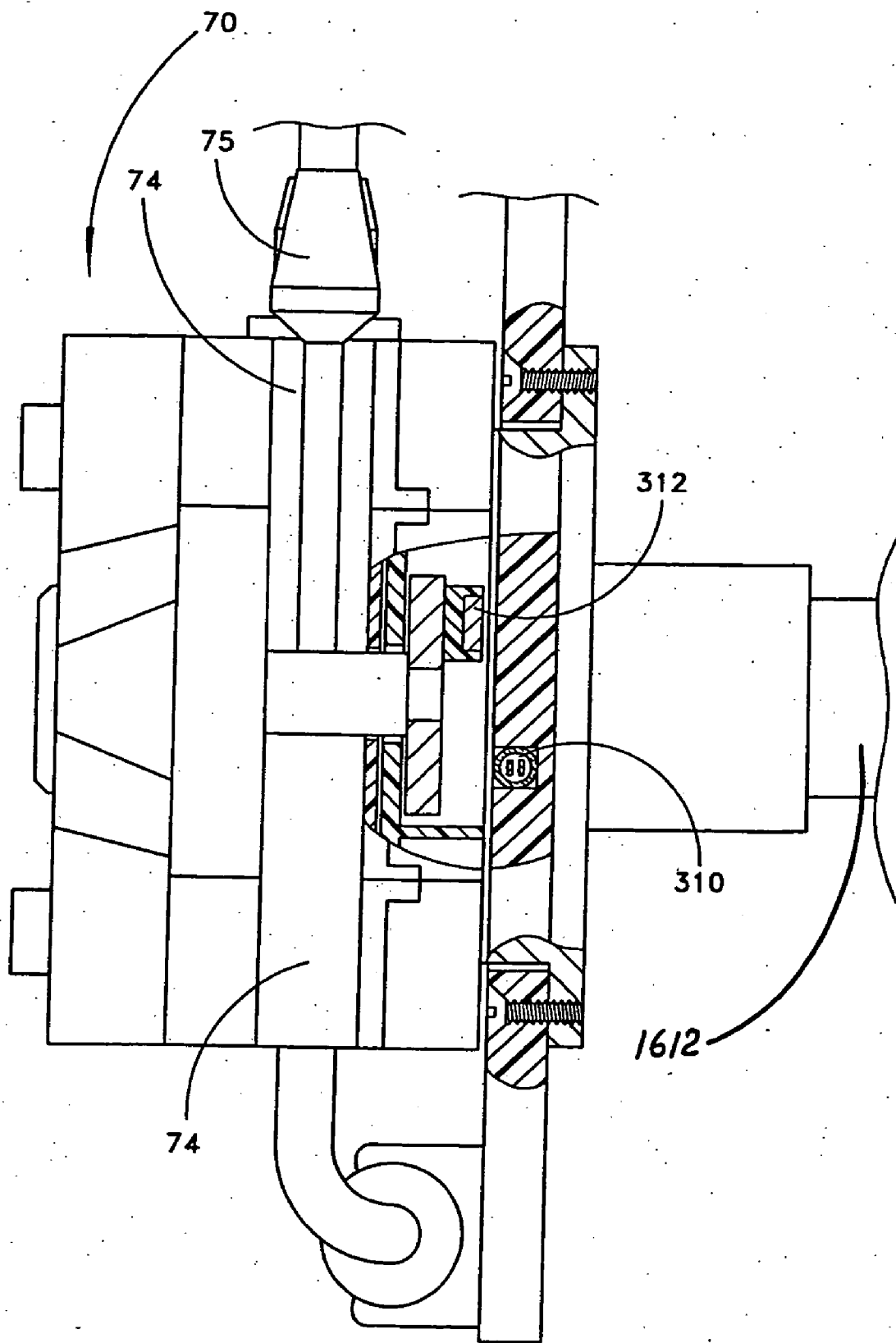


FIG.13

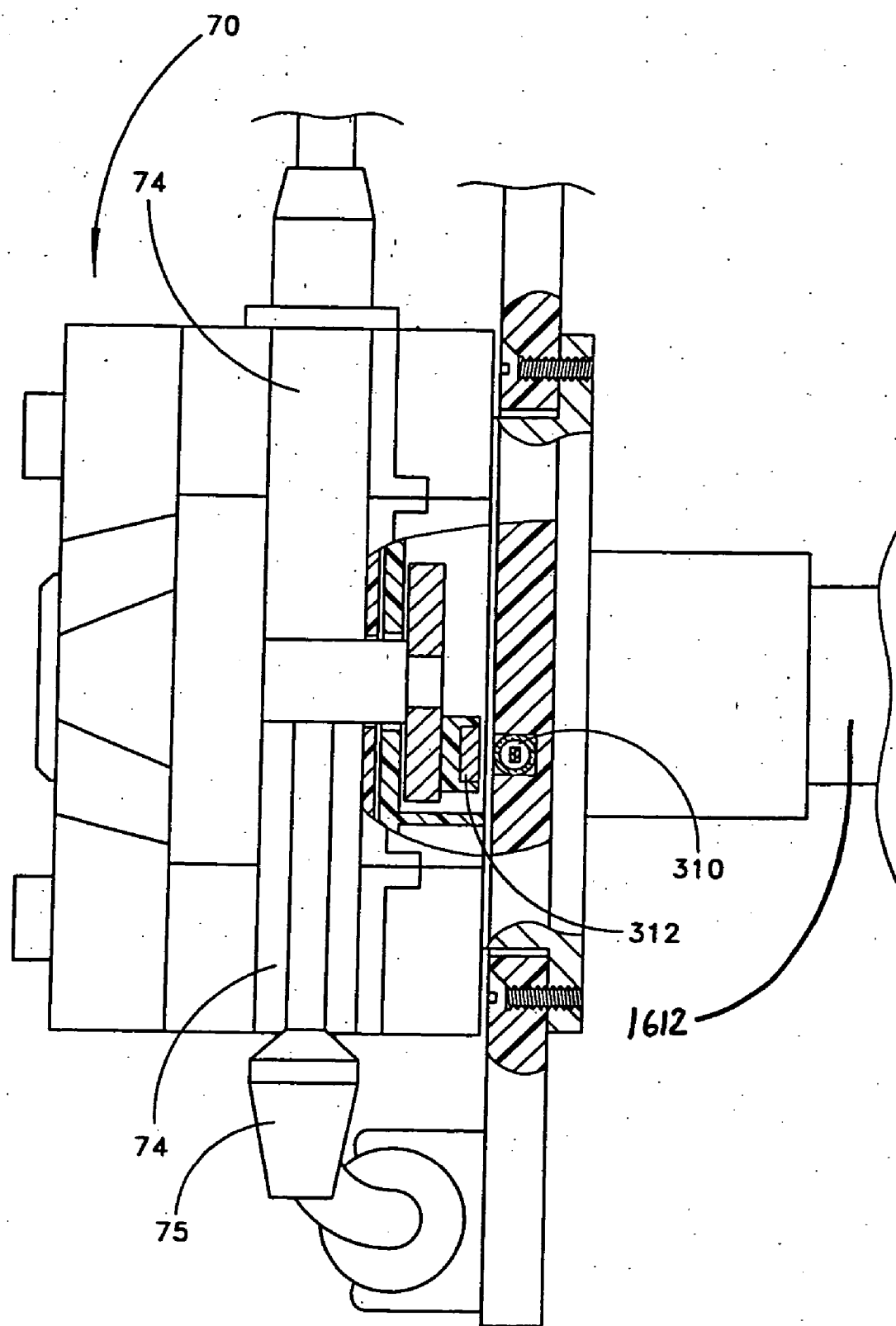


FIG.14

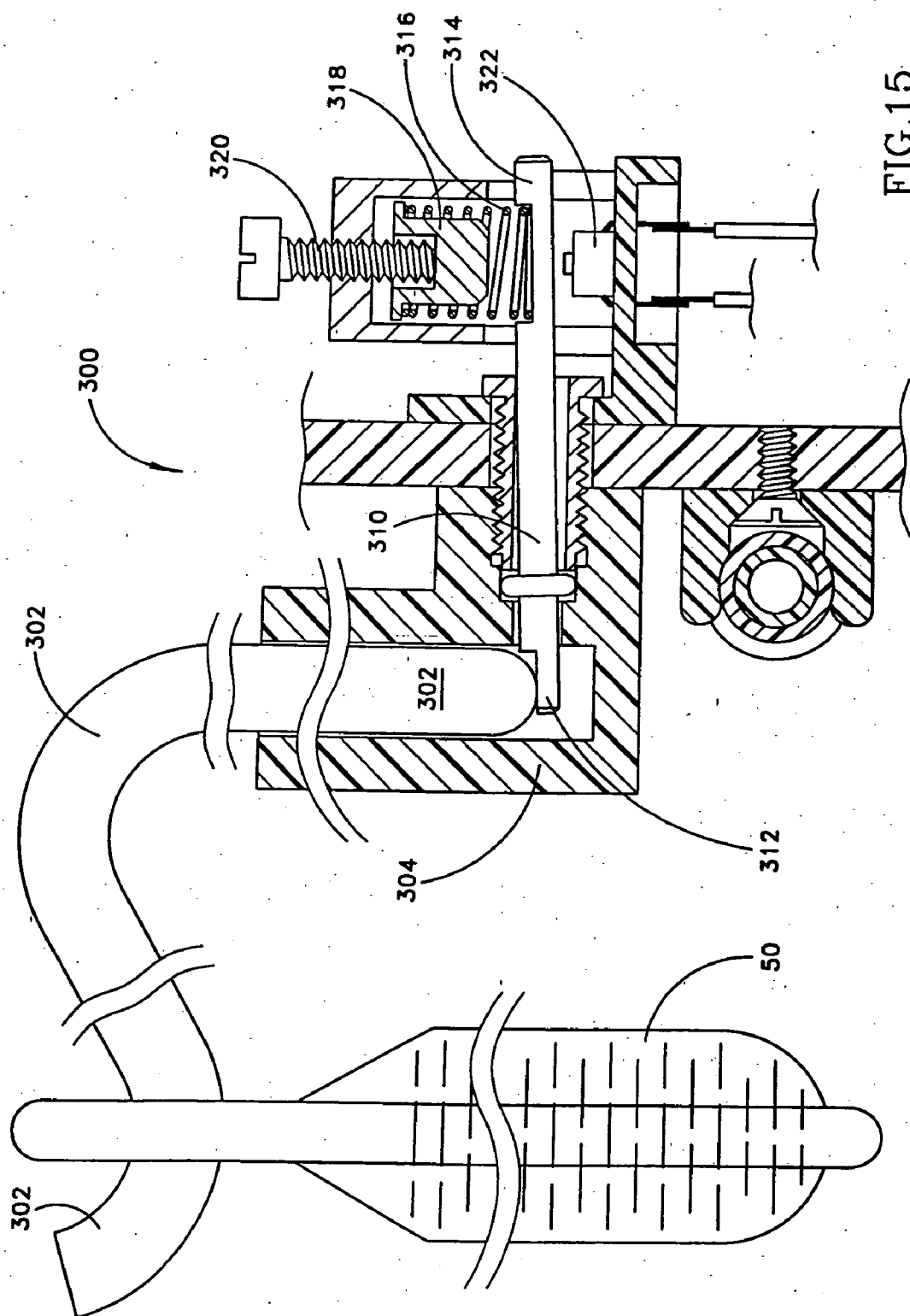
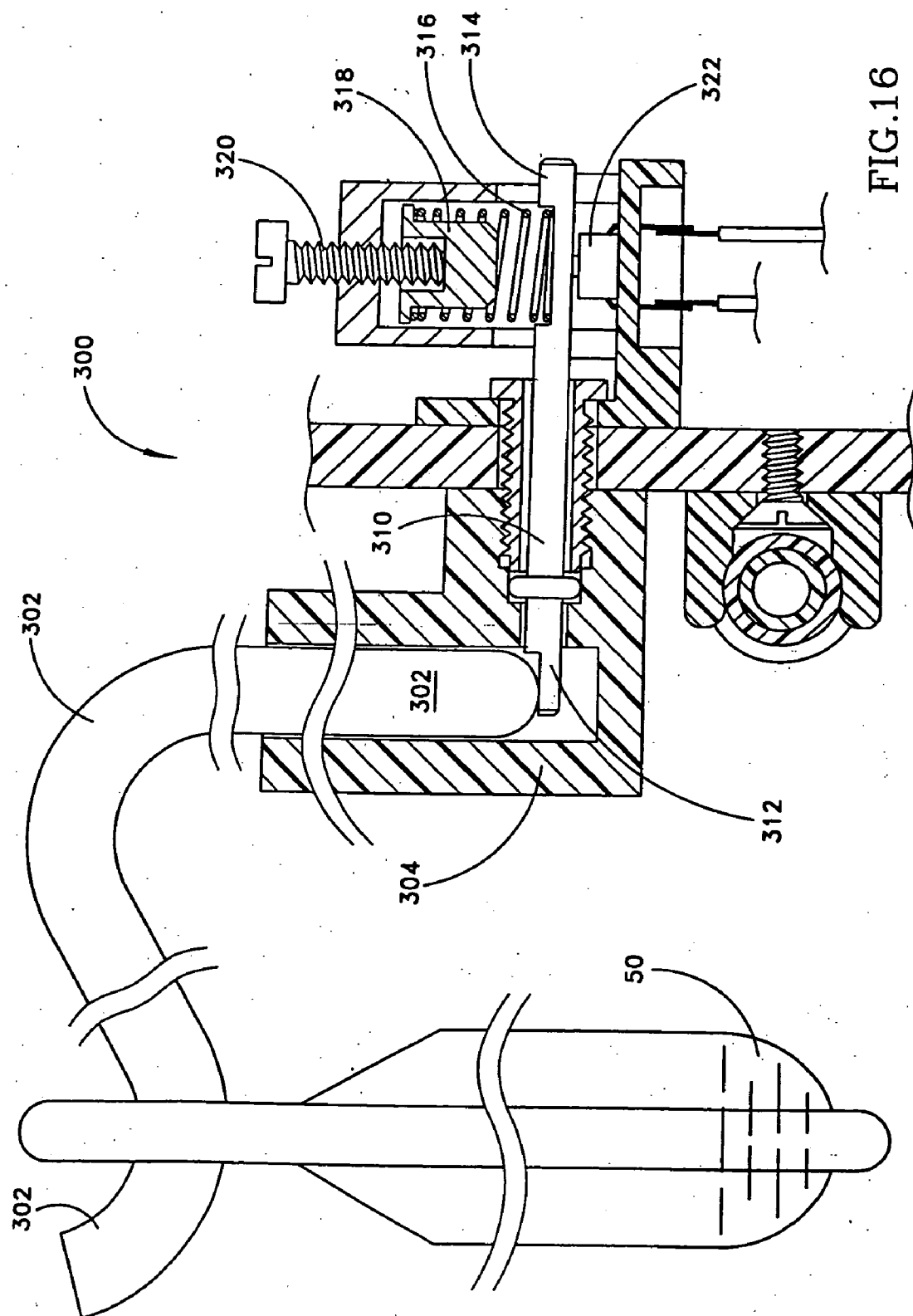


FIG. 15



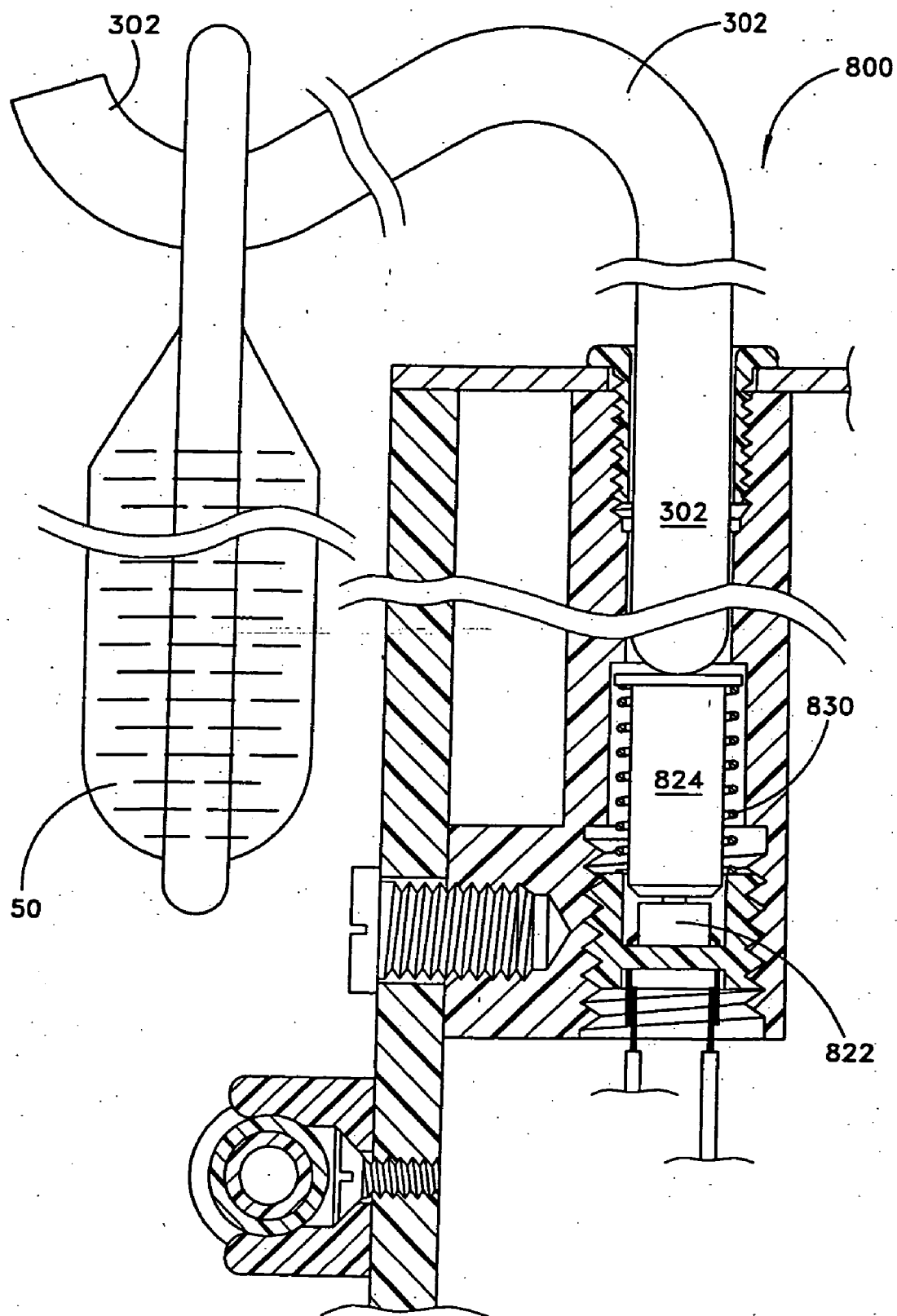


FIG.17

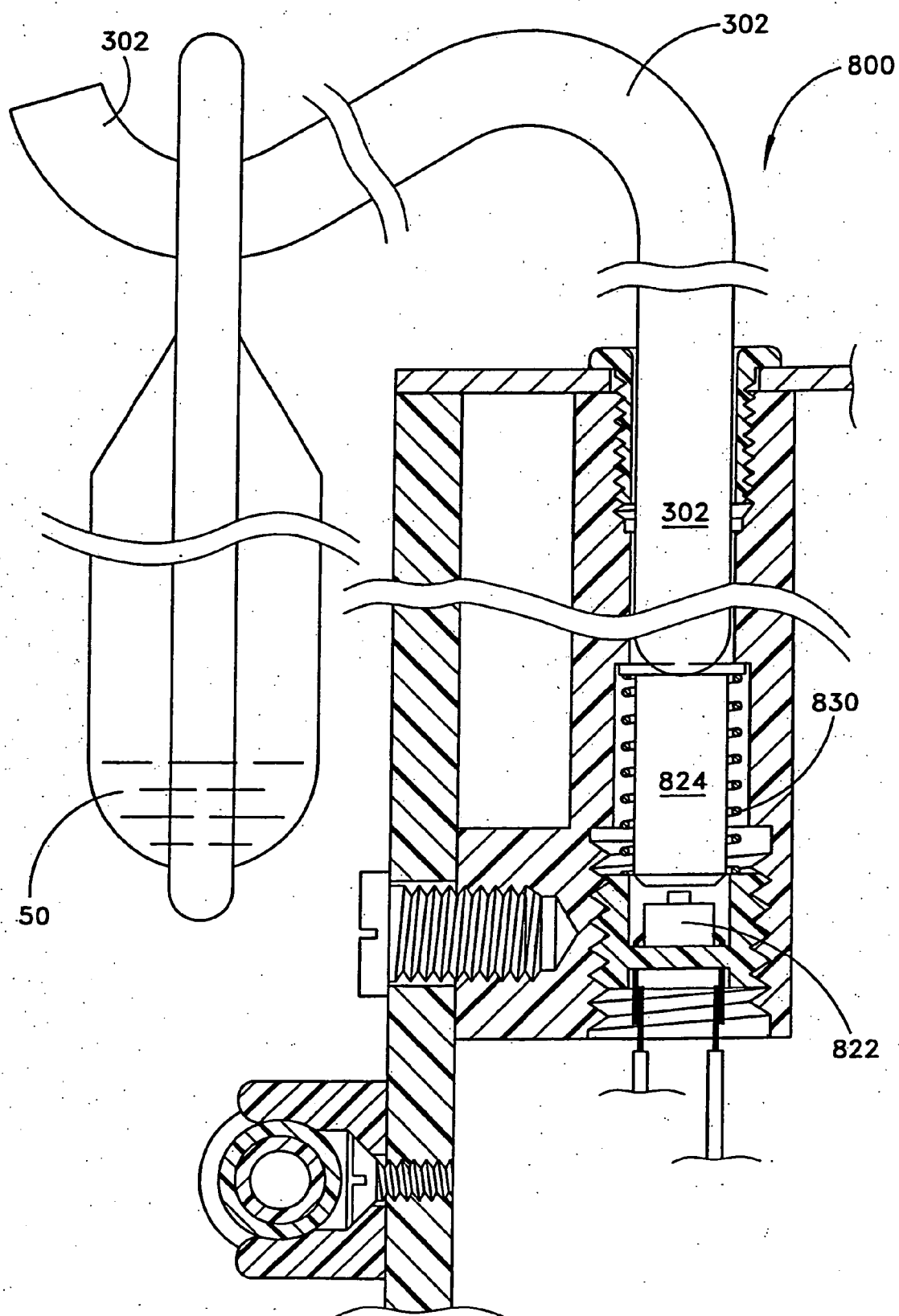


FIG.18

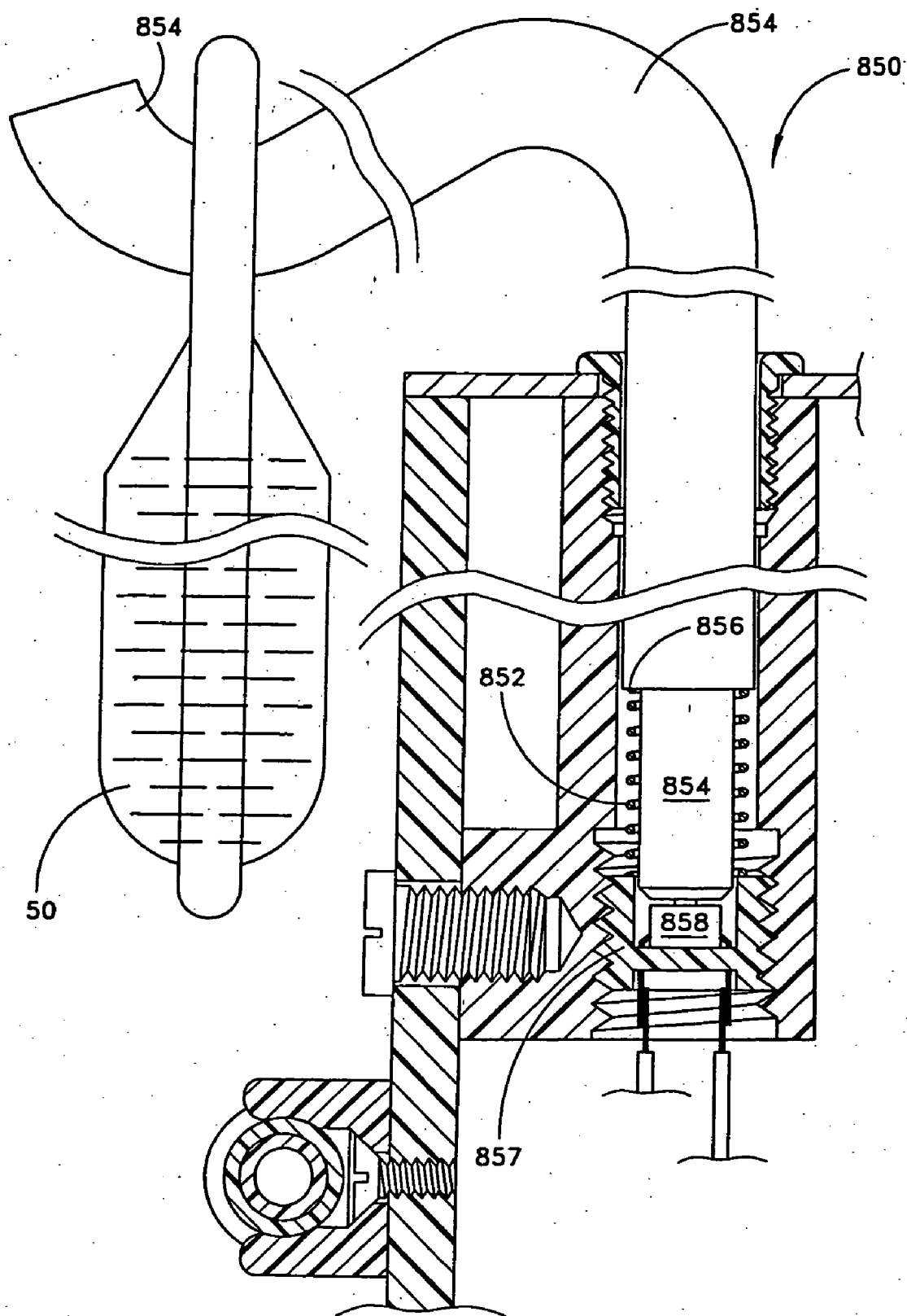


FIG.19

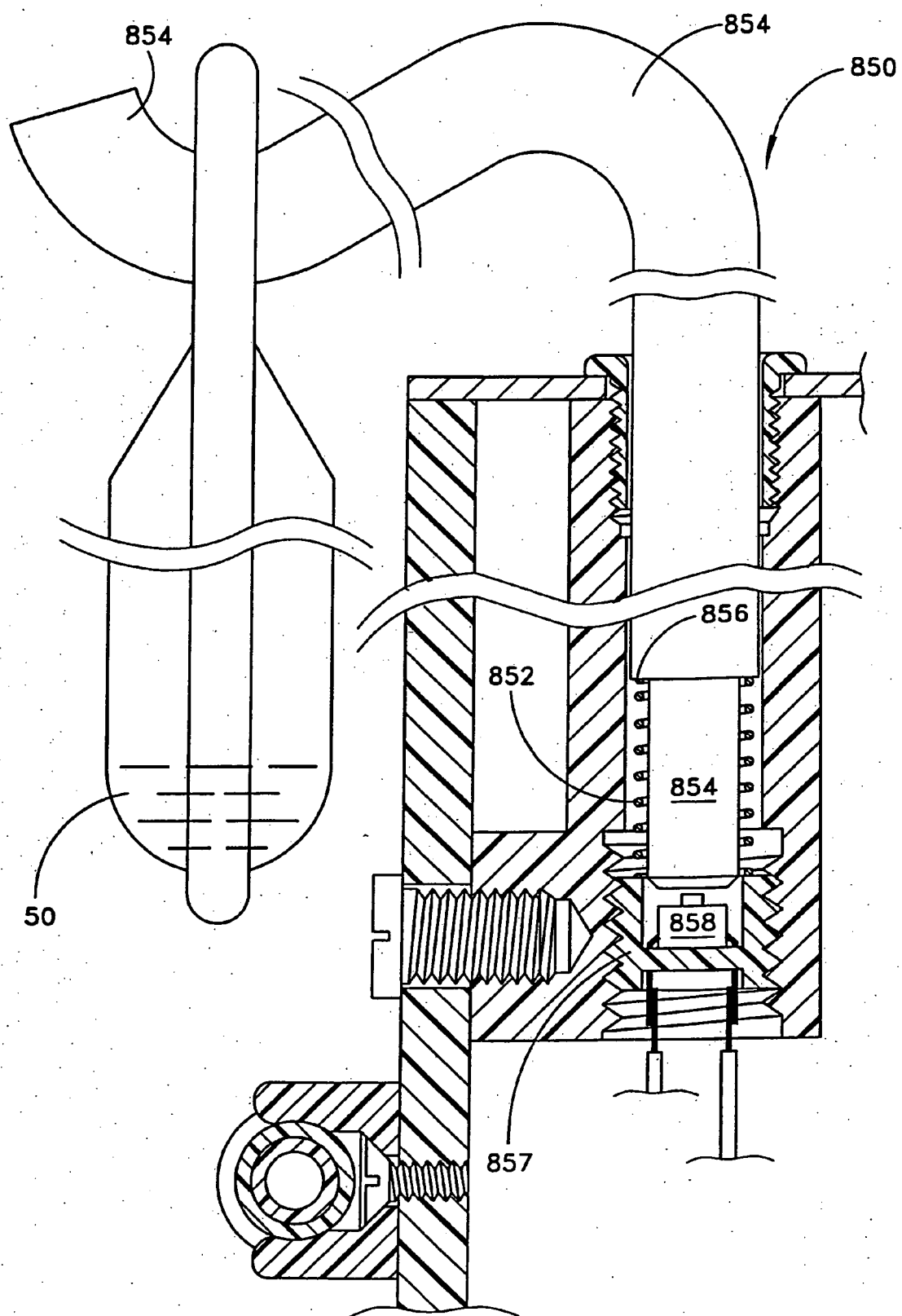


FIG. 20

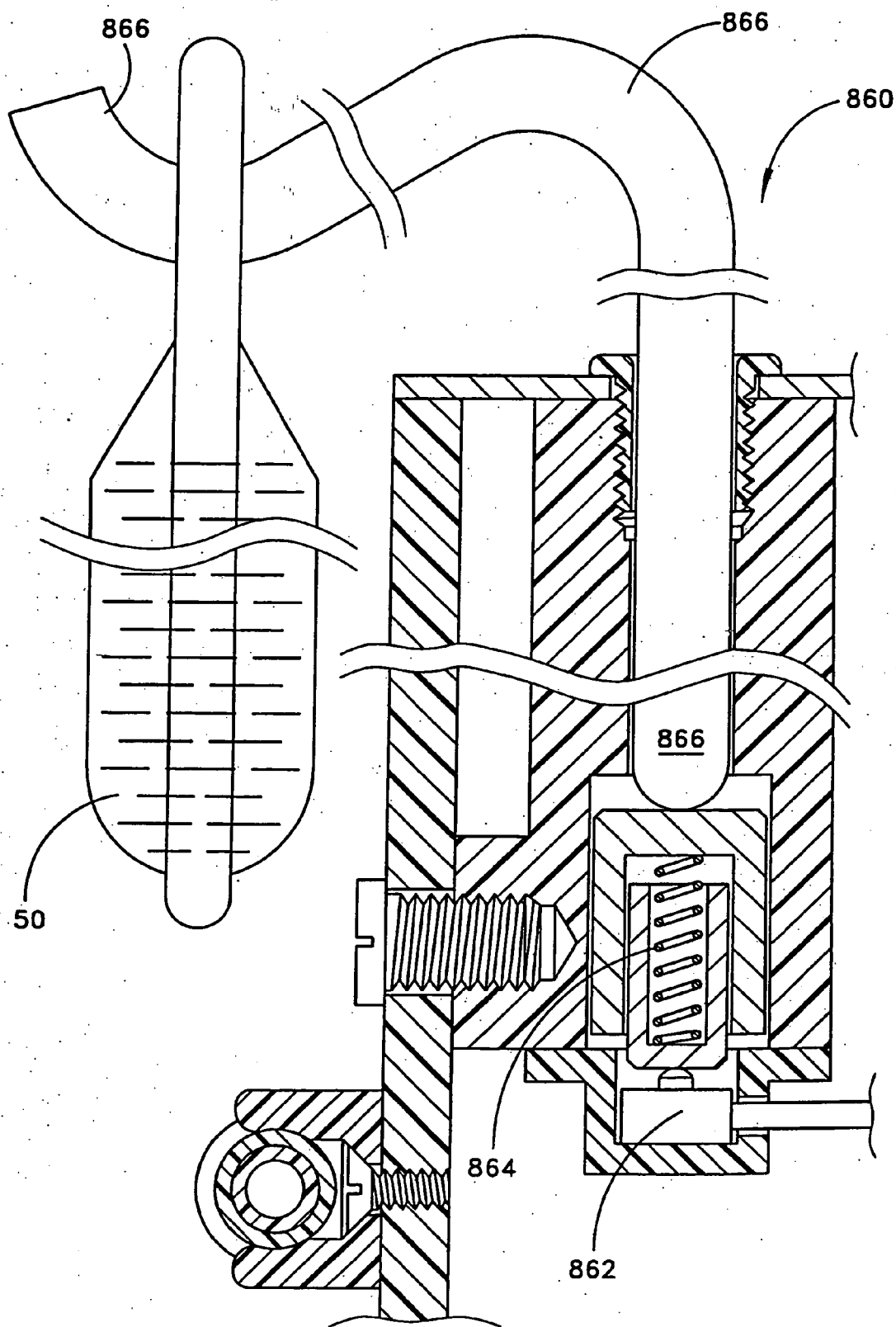


FIG. 21

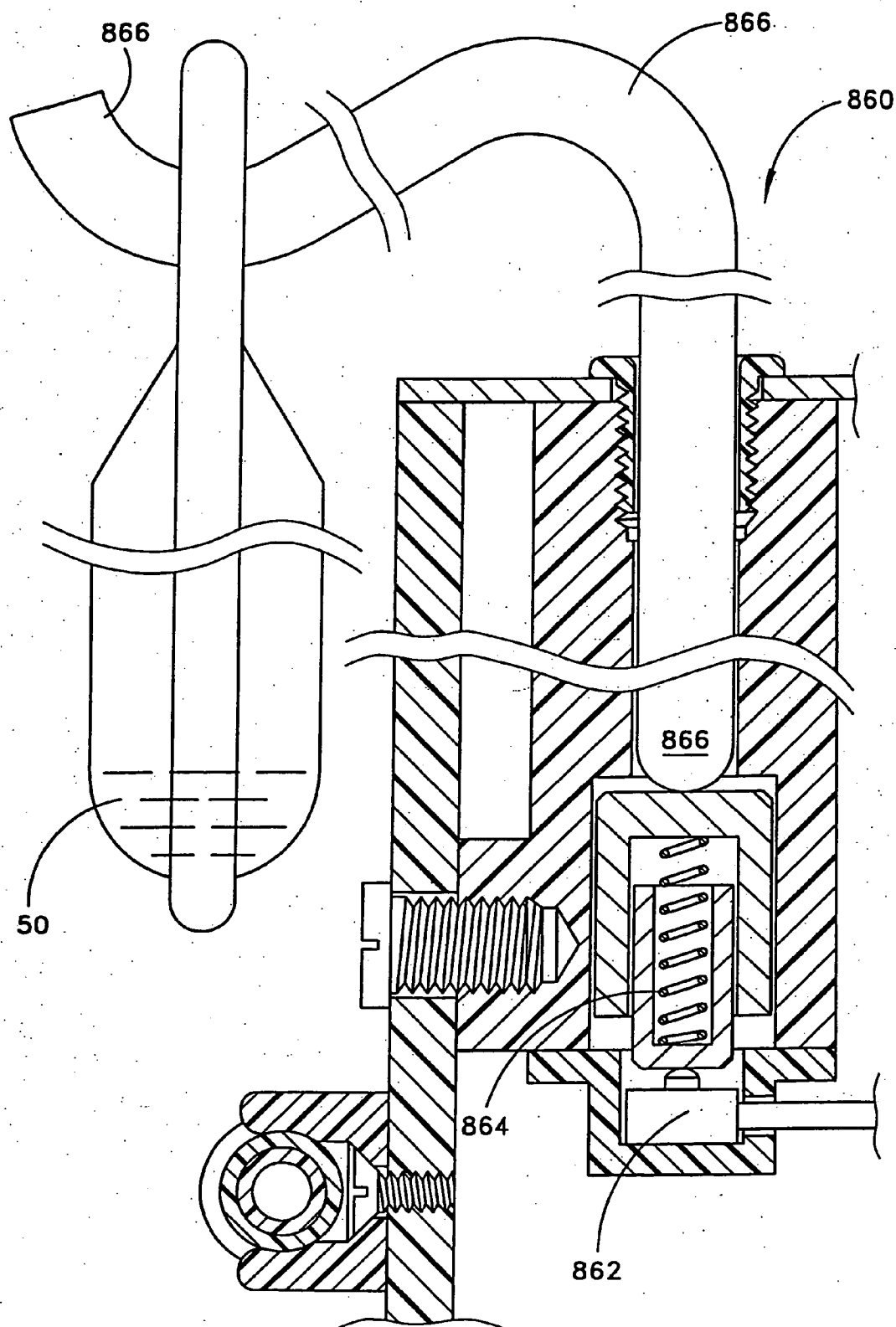


FIG. 22

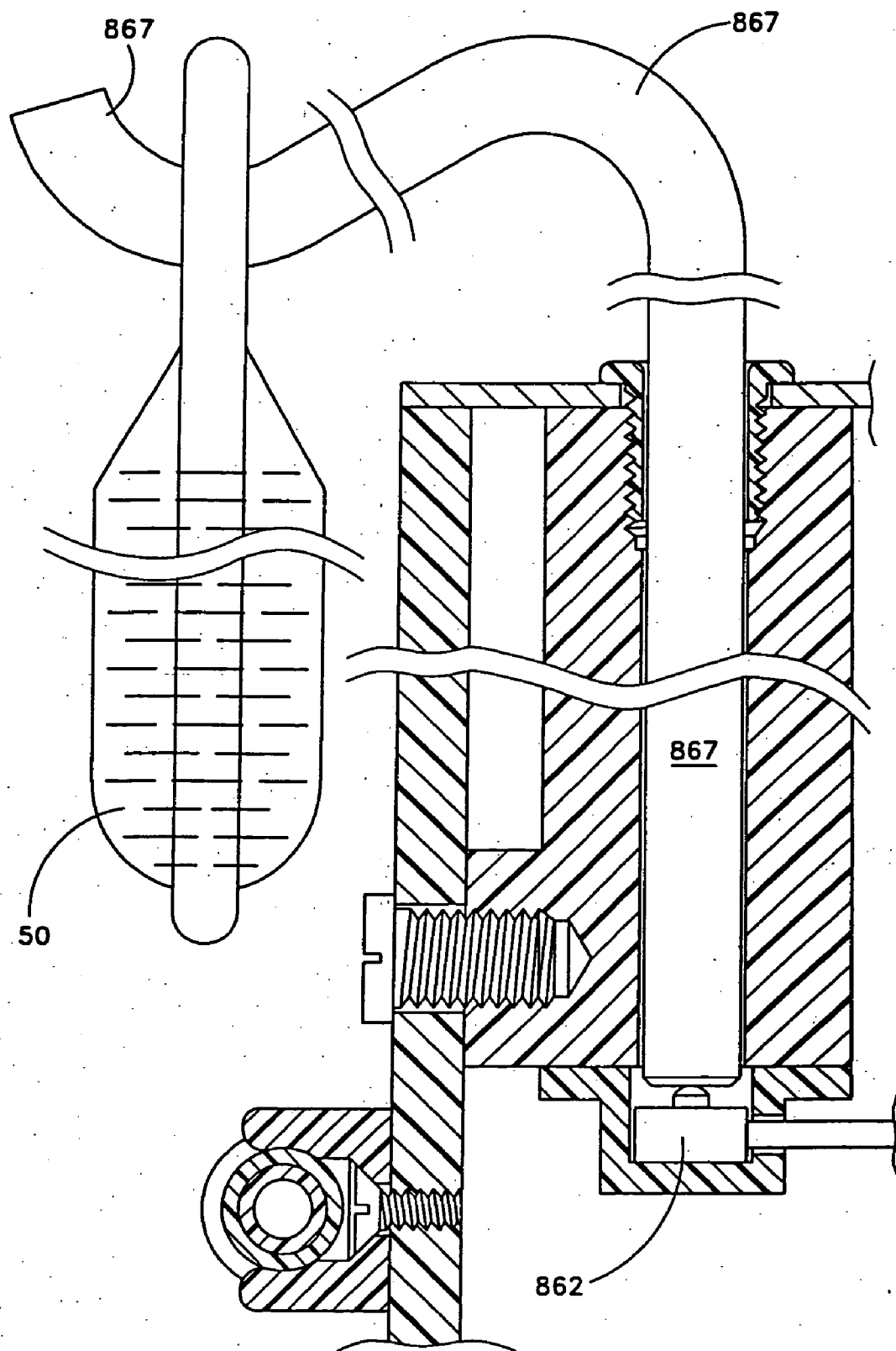


FIG. 23

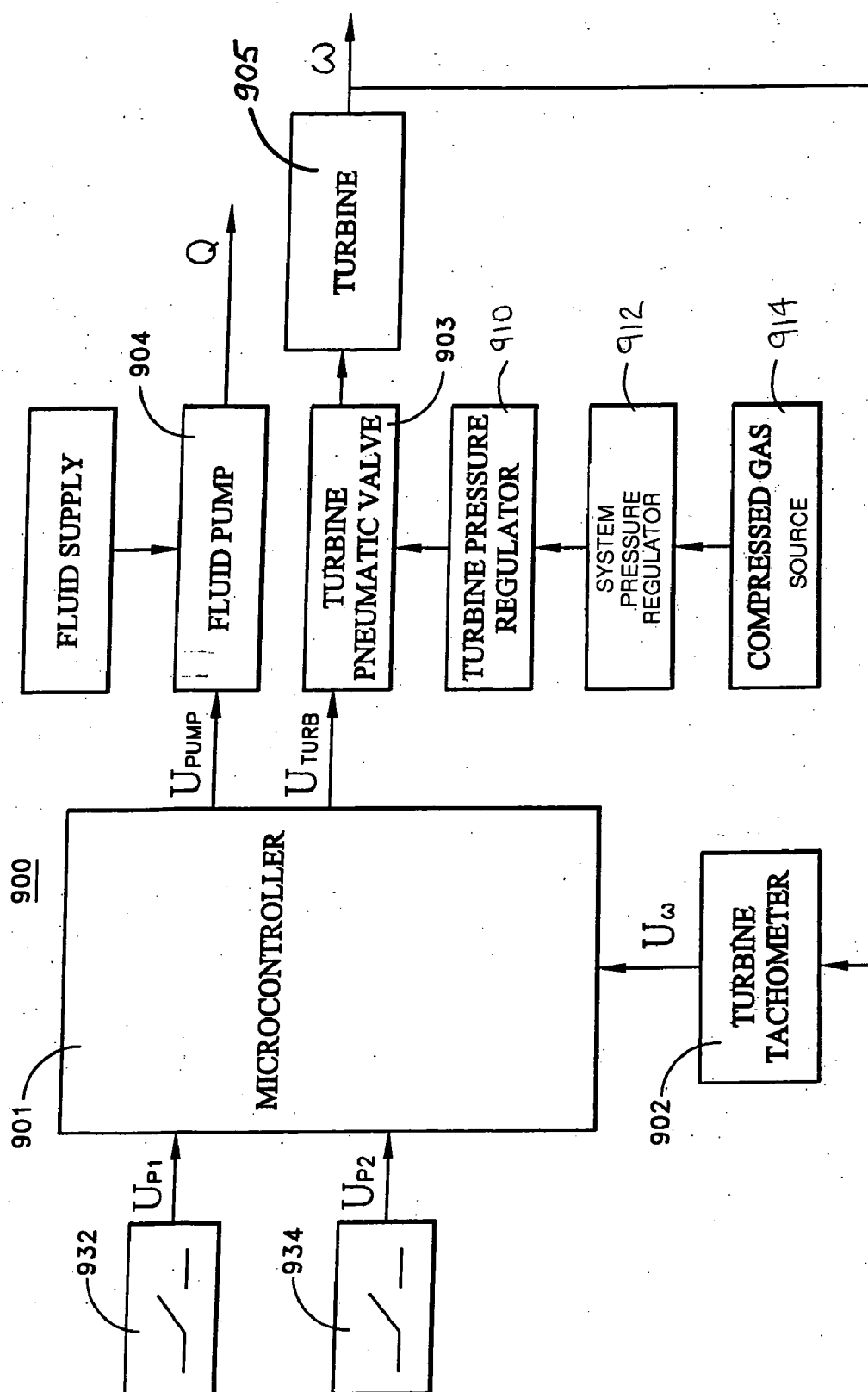


FIG. 24

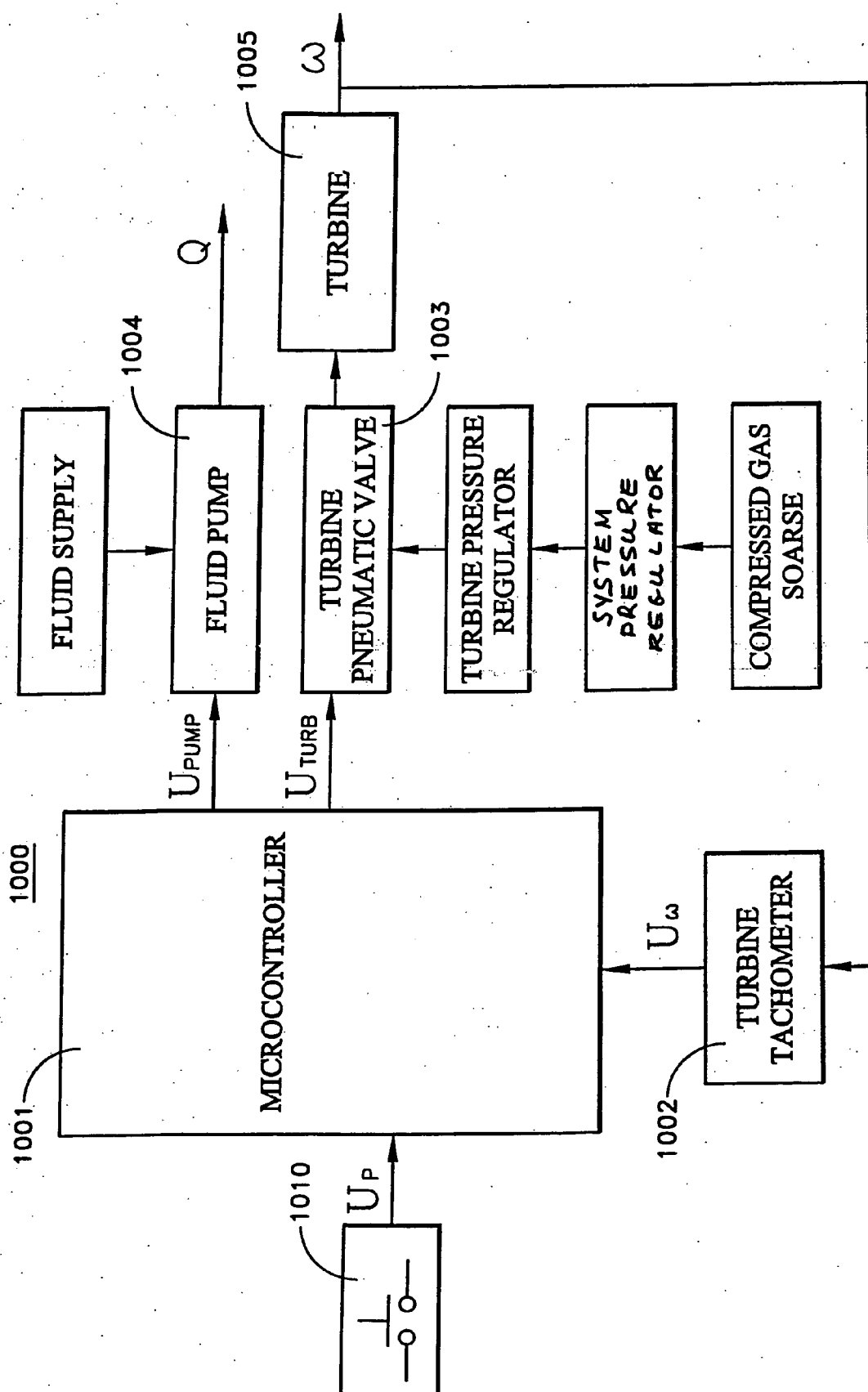


FIG. 25

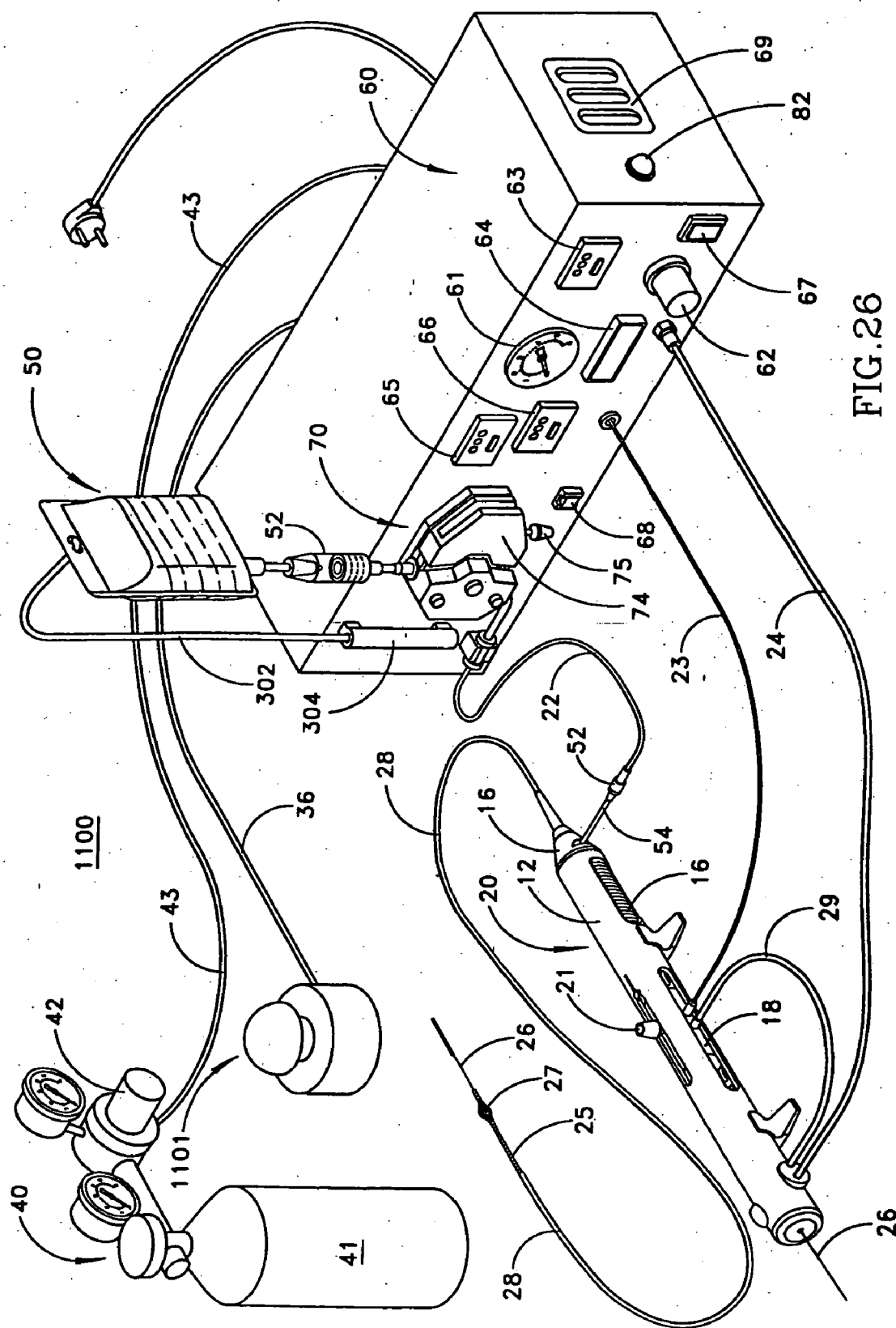


FIG. 26

SYSTEM FOR CONTROLLING A FLOW OF FLUID THROUGH A ROTATIONAL ATHERECTOMY DEVICE

BACKGROUND OF THE INVENTION

[0001] 1. Field of the Invention

[0002] The present invention generally relates to devices and methods for removing tissue from body passageways and, more particularly, to a control system for a rotational and/or orbital angioplasty device.

[0003] 2. Brief Description of Related Developments

[0004] There are a number of different techniques and devices which have been developed for use in removal and/or repair of arteries and other similar body passages. One objective of some of the aforementioned devices and techniques is removal of atherosclerotic plaques from patient's arteries. Atherosclerosis is characterized by buildup of fatty deposits (atheromas) in the intimal layer (under the endothelium) of a patient's blood vessels. Very often over time, what initially is deposited as relatively soft, cholesterol-rich atheromatous material hardens into a calcified atherosclerotic plaque. Such atheromas restrict the flow of blood, and therefore often are referred to as stenotic lesions or stenoses. If left untreated, such stenoses can cause angina, hypertension, myocardial infarction, strokes and the like.

[0005] Rotational angioplasty procedures are a common technique for removing such stenotic material. Such procedures are used most frequently to commence the opening of calcified lesions in coronary arteries. Often the rotational angioplasty procedure is not used alone, but is followed by a balloon angioplasty procedure. This, in turn, may frequently be followed by placement of a stent to assist in keeping the artery open. For noncalcified lesions, balloon angioplasty most often is used alone to open the artery, with stents often placed to maintain the opened artery. Studies have shown, however, that a significant percentage of patients who have undergone balloon angioplasty and had a stent placed in an artery experience in-stent restenosis (i.e., blockage of the stent) which most frequently develops over a period of time as a result of excessive growth of scar tissue within the stent. Rotational angioplasty devices were utilized in removing the excessive scar tissue from the stents and, thereby were useful in providing assistance in restoring the patency of the arteries.

[0006] It should be understood that rotational angioplasty devices and rotational angioplasty procedures are often referred to as rotational atherectomy devices and rotational atherectomy procedures. These terms may be used interchangeably herein.

[0007] One example of a rotational angioplasty device is shown in U.S. Pat. No. 4,990,134 (issued to Auth), wherein a front or distal portion of a burr is covered with an abrasive cutting material such as diamond particles. The diamond coated burr is mounted at the distal end of a flexible drive shaft. The burr is rotated at high speeds (typically, e.g., in the range of about 140,000-180,000 rpm) while it is advanced across the stenosis. The burr has a solid cross-section and thus, as the burr is removing stenotic tissue, it blocks blood flow through the artery. Once the burr has been advanced across the stenosis, the artery will have been opened to a

diameter equal to or only slightly larger than the maximum outer diameter of the burr. A series of different size burrs may be utilized to open the artery to a desired diameter. U.S. Pat. No. 5,897,566 (issued to Shturman) shows another rotational angioplasty device having a drive shaft made from helically wound wires. A section of the drive shaft has an enlarged diameter. In one embodiment at least a front or distal segment of this enlarged diameter section is covered with an abrasive material to define an abrasive segment of the drive shaft. The enlarged diameter section is hollow. This Shturman Device of the '566 patent is capable of opening an artery only to a diameter about equal to the maximum diameter of the enlarged diameter section of the drive shaft, thereby providing results similar to the Auth Device of the '134 patent. The Shturman Device of the '566 patent possesses certain advantages over the Auth Device of the '134 patent because it is more flexible. Another example of a rotational angioplasty device is provided in U.S. Pat. No. 6,132,444 (issued to Shturman et al.) describes a rotational atherectomy device having a flexible, elongated, rotatable drive shaft with an eccentric enlarged diameter section. At least part of the eccentric enlarged diameter section has a tissue removing surface with an abrasive surface to define a tissue removing segment of the drive shaft. When placed within an artery against stenotic tissue and rotated at sufficiently high speeds (e.g. in the range of about 40,000 rpm to about 200,000 rpm) the eccentric nature of the enlarged diameter section of the drive shaft causes such section to rotate in such a fashion as to open the stenotic lesion to a diameter substantially larger than the maximum diameter of the enlarged diameter section. Preferably the eccentric enlarged diameter section of the drive shaft has a center of mass spaced radially from the rotational axis of the drive shaft, facilitating the ability of the device to open the stenotic lesion to a diameter substantially larger than the maximum diameter of the enlarged diameter section. A drive shaft having an eccentric enlarged diameter tissue removal section with a diameter of not more than 2 mm is capable of opening stenotic lesions to a diameter equal to the original diameter of the coronary arteries (i.e., to a diameter of more than 3 mm) so that in a significant percentage of cases balloon angioplasty may not be needed to complete the procedure. The device is particularly useful for cleaning out partially blocked stents.

[0008] U.S. Pat. No. 5,314,407 to Auth, which is incorporated herein by reference in its entirety, shows the details of a type of an advancer (handle) that may be used in conjunction with rotational atherectomy devices of the type described in Auth '134 patent and Shturman '566 and '444 patents. A handle of the type shown in Auth '407 patent has been commercialized by Heart Technology, Inc. (Redmond, Wash.), now owned by Boston Scientific Corporation (Natick, Mass.), in the rotational atherectomy (angioplasty) device sold under the trademark Rotablator®.

[0009] FIG. 1 is an illustration of a rotational angioplasty system 100 of the prior art. As shown in FIG. 1, the prior art system comprises a rotational angioplasty device 104, a fluid supply 106, a gas supply 108, a controller 102 and a foot pedal device 110.

[0010] The rotational angioplasty device 104 comprises an advancer assembly 134 that is located within a body or handle 136. A gas driven turbine (not shown) is located within the advancer assembly 134 and rotates a flexible,

hollow drive shaft **138**. An ablative, diamond coated burr **140** is attached at the distal end of the flexible drive shaft **138**. The flexible drive shaft **138** together with the burr **140** may be rotated over a guide wire **141**.

[0011] As shown in **FIG. 1**, a flexible sheath **142** extends distally from the handle **136** and surrounds the flexible drive shaft **138** substantially along its entire length.

[0012] The advancer assembly **134** also carries a water (saline) pump (not shown). This water pump is located distally to the gas turbine and has a shaft that is connected to the turbine shaft. The output of the fluid pump is in fluid connection with the lumen formed between the flexible drive shaft **138** and the flexible sheath **142**.

[0013] The rotational angioplasty system **100** shown in **FIG. 1** includes an infusion bag **128** to administer a saline solution. The saline bag **128** is pressurized with a pressure cuff **129** to ensure a steady supply of saline to the water pump within the advancer assembly **134** and around the drive shaft **138**. The rotation of the gas turbine rotates the fluid pump and increases the fluid flow rate in a lumen between the flexible drive shaft **138** and the sheath **142**. The fluid flow rate in this system depends on the rotational speed of the gas turbine. Thus, the fluid acceleration in the lumen between the drive shaft **138** and the sheath **142** can only take place simultaneously with the increase in rotational speed of the gas turbine, and the system can not increase the fluid flow rate in the lumen between the drive shaft **138** and the sheath **142** without increasing the rotational speed of the gas turbine.

[0014] A certain amount of static pressure must be applied and maintained against the saline bag **128** in order to provide an adequate fluid flow rate in the lumen between the drive shaft **138** and the sheath **142**. This requires repeated repressurization of the pressure cuff **129** disposed around the saline bag **128**.

[0015] The controller **102** has a front panel **112** that includes a power switch **113**, a turbine control knob **114** (adjusts turbine pressure and RPMs), a turbine pressure gauge **115**, a turbine (pneumatic) connector **116**, a DynaGlide™ (pneumatic) connector **117**, and a pair of fiber optic connectors **120**. The front panel **112** also includes an event timer **122**, a procedure timer **123**, and an optical tachometer display **124**. The optical tachometer provides or registers information about the rotational speed of the gas turbine of the rotational angioplasty device **104**.

[0016] The foot pedal **110** is used as an on/off control for the gas turbine of the rotational angioplasty device **104**. A DynaGlide™ button **126** is located on the right side of the foot pedal housing **132** and is used as an on/off control for the DynaGlide™ mode of operation.

SUMMARY OF THE INVENTION

[0017] A method system and controller for controlling fluid flow in a rotational atherectomy device. A source of fluid is provided through a pump to the rotational atherectomy device, wherein the pump maintains the fluid flow at a minimal rate during a time period when a drive shaft of the device is not rotating. A first control is activated to increase a rate of the fluid flow and second control is activate to initiate a rotation of the drive shaft during another time period when the fluid flow is at the increased rate.

BRIEF DESCRIPTION OF THE DRAWINGS

[0018] The foregoing aspects and other features of the present invention are explained in the following description, taken in connection with the accompanying drawings, wherein:

[0019] **FIG. 1** is a block diagram of a prior art rotational angioplasty device;

[0020] **FIG. 2** is a perspective view of one embodiment of a rotational angioplasty system incorporating features of the present invention;

[0021] **FIG. 3** is a cross-sectional view of one embodiment of a roller pump;

[0022] **FIG. 4** is a cross-sectional view of a roller pump in a closed position;

[0023] **FIG. 5** is a cross-sectional view of one embodiment of a roller pump in a closed position with fluid in the fluid line in a system incorporating features of the present invention;

[0024] **FIG. 6** is a cross-sectional view of one embodiment of a fluid supply line securing device incorporating features of the present invention;

[0025] **FIG. 7** is a block diagram illustrating one embodiment of the functional aspects of a controller for a system incorporating features of the present invention;

[0026] **FIG. 8** is a timing diagram for pump and turbine activation periods in one embodiment of a system incorporating features of the present invention;

[0027] **FIG. 9** is a timing diagram illustrating pump and turbine activation periods in one embodiment of a system incorporating features of the present invention;

[0028] **FIG. 10** is a timing diagram of pump and turbine activation periods in one embodiment of a system incorporating features of the present invention;

[0029] **FIG. 11** is a timing diagram of pump and turbine activation periods in one embodiment of a system incorporating features of the present invention;

[0030] **FIG. 12A** is a schematic diagram of one embodiment of a timing circuit to produce a delayed time period feature of a system incorporating features of the present invention;

[0031] **FIG. 12B** is a schematic diagram of one embodiment of a timing circuit to produce a delayed time period in a system incorporating feature of the present invention;

[0032] **FIGS. 13 and 14** are partial cross-sectional views of a pump cover sensor in embodiments of systems incorporating features of the present invention;

[0033] **FIGS. 15 and 16** are partial cross-sectional views of embodiments of fluid level detection systems for a system incorporating features of the present invention;

[0034] **FIGS. 17 and 18** are embodiments of fluid level detection systems for a system incorporating features of the present invention;

[0035] **FIGS. 19 and 20** are embodiments of fluid level detection systems for a system incorporating features of the present invention;

[0036] **FIGS. 21 and 22** are embodiments of fluid level detection systems for a system incorporating features of the present invention;

[0037] **FIG. 23** is one embodiment of a fluid level detection system for a system incorporating features of a present invention;

[0038] **FIG. 24** is a block diagram of one embodiment of a control system for a system incorporating features of the present invention;

[0039] **FIG. 25** is a block diagram of one embodiment of a control system for a system incorporating features of the present invention; and

[0040] **FIG. 26** is a perspective view of one embodiment of a system incorporating features of the present invention.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENT

[0041] Referring to **FIG. 2**, there is shown a perspective view of a rotational angioplasty system **10** incorporating features of the present invention. Although the present invention will be described with reference to the embodiment(s) shown in the drawings, it should be understood that the present invention can be embodied in many alternate forms of embodiments. In addition, any suitable size, shape or type of elements or materials could be used.

[0042] As shown in **FIG. 2**, the system **10** generally comprises a rotational angioplasty device ("RAD") **20**. The rotational angioplasty device **20** can also comprise, or may be referred to as a rotational atherectomy device. As shown in **FIG. 2**, the RAD is generally coupled to a controller **60** and a fluid supply **50**. The system **10** can also include an activation device **30** and a gas supply system **40**. Both the activation device **30** and gas supply system **40** can be coupled or connected to the controller **60**. In an alternate embodiment, the system **10** can include such other components suitable for use in a system for removing tissue from a passageway in the body.

[0043] Descriptions of some examples of such RAD devices can be found in U.S. Pat. Nos. 5,897,566; 6,024,749; 6,077,282; 6,129,734; and 6,132,444 issued to Shturman, each of which is incorporated herein by reference in its entirety; and in U.S. Pat. Nos. 4,990,134 and 5,314,407 issued to Auth.

[0044] As shown in **FIG. 2**, the RAD **20** can include a prime mover carriage **18** and a drive shaft cartridge **16**. A fluid supply line **22**, a prime mover speed monitoring line **23**, and a gas supply line **24** are adapted to be connected or coupled to the RAD **20**. In one embodiment, the lines **22**, **23** and **24** can be a physical part of and extend from the RAD **20**. In an alternate embodiment, the RAD **20** could include one or more couplings or connection ports to allow one or more of the lines **22**, **23** or **24** to be connected to the RAD. Any one of the lines **22**, **23** or **24** could be separate from the RAD **20**.

[0045] Extending from one end of the RAD **20** is an elongated tube **28**. The elongated tube **28** can include a rotatable flexible drive shaft **25** that has a tissue removal implement **27** located near the distal end of the flexible drive shaft **25**. The elongated tube **28** can also include an inner lumen (not shown) between an interior surface of the

elongated tube and the drive shaft **25** along or around which fluid can flow at any suitable or desired rate of flow.

[0046] A control knob **21** operatively secured to the prime mover carriage **18** is adapted to facilitate advancing and retracting the prime mover carriage **18** with respect to the housing **12** of the RAD **20**.

[0047] The prime mover carriage **18** generally carries a prime mover (not shown). Preferably, the prime mover is a compressed gas driven turbine, and for purposes of this description, will be referred to herein as a gas turbine. It should be understood however, that any suitable device can be used to rotate the drive shaft **25** at a desired rotational speed. For example, an electrically powered motor could be used. The gas turbine may be powered, for example, by compressed nitrogen or compressed air supplied from system **40**. The system **40** usually includes a tank **41** with compressed gas and a pressure regulator **42**.

[0048] As shown in **FIG. 2**, the RAD **20** includes a drive shaft cartridge **16** that includes the elongated tube **28** extending distally from the drive shaft cartridge **16**. The rotatable flexible drive shaft **25** is generally disposed within the elongated tube **28**. The flexible drive shaft **25** may be rotated over a guide wire **26**. A distal portion of the drive shaft **25** may extend distally from the elongated tube **28** and may include the tissue removal implement **27**.

[0049] Referring to **FIG. 2**, the RAD **20** can be coupled to the controller **60** through one or more connections, including for example a fluid supply connection, a gas supply connection and a turbine speed monitoring line connection. Fluid is supplied to the drive shaft cartridge **16** from the fluid supply **50** through a fluid supply line **22**. As shown in **FIG. 2**, the fluid supply line **22** is comprised of more than one sequentially connected fluid lines. In alternate embodiments a single line, or any suitable combination of fluid lines may be used. For example, referring to **FIG. 2**, a short fluid supply line **54** extends from the drive shaft cartridge **16** and is coupled to a longer fluid supply line **22** with a luer lock device **52**. The fluid line **54** is connected or coupled to the inner lumen of the elongated tube **28**. In an alternate embodiment, the drive shaft cartridge **16** could include a fitting or coupling to which the fluid supply line **22** can be directly connected. In this manner a fluid, such as for example saline, is supplied to the inner lumen of the elongated tube **28** from the fluid supply **50**. The fluid supply line **22** could also comprise one or more parallel fluid lines to couple the fluid supply(s) to the inner lumen(s) of the elongated tube **28**.

[0050] One or more prime mover speed monitoring lines **23** may be used to monitor the rotational speed of the gas turbine. For example, in one embodiment the line **23** could comprise a fiber optic line that is adapted to couple pulses of light from an element of an optical tachometer (not shown) of the RAD **20** to the controller **60**. The number of such pulses per unit of time can be used to determine a rotational speed of the gas turbine. In an alternate embodiment any suitable device can be used to communicate the rotational speed of the gas turbine of the RAD **20** to the controller **60**.

[0051] The gas supply line **24** is used to provide a compressed gas to the guide wire brake (not shown) and further via gas supply line **29** to the prime mover carriage **18** to power the prime mover or gas turbine. As shown in **FIG. 2**,

the gas supply system 40 is a compressed gas system that can provide a steady flow of gas to the controller 60. Generally, any conventional or suitable system 40 can be used to supply the flow of compressed gas via a gas line 43 to the controller 60. As shown in FIG. 2, the compressed gas system 40 comprises one or more tanks or bottles 41 coupled to a regulator device 42. In an alternate embodiment, the gas system could comprise a hospital gas system where the supply of compressed gas is generally delivered via a compressed gas line 43 to the controller unit 60.

[0052] As shown in FIG. 2, the system 10 can also include a fluid pump 70. The fluid pump 70 is generally adapted to pump the fluid from the fluid supply 50 through the fluid supply line 22 to an inner lumen(s) of the elongated tube 28 and to some other moving parts of the RAD. Although the elongated tube 28 is referred to herein as generally having a lumen, in alternate embodiments, the elongated tube 28 could also include a plurality of lumens.

[0053] The speed at which the pump 70 pumps the fluid is generally variable and controlled through the controller 60. In the preferred embodiment, the pump 70 comprises a peristaltic (roller) pump. An example of one embodiment of a peristaltic pump is shown in FIGS. 3-5. As shown in FIG. 3, a portion 82 of the fluid supply line 22 is passed through the pump 70 and around an outer edge of rollers 80. The tubing portion 82, also referred to herein as the tube or tubing 82, of the fluid supply line 22 is generally different from the remainder of the fluid supply line 22 and comprises a tube that has special mechanical properties that allow the tubing to be used within the roller portion of the fluid pump 70. In one embodiment, the tubing 82 can be made from Tygon®. LFL tubing or a tubing with similar mechanical properties. One type of tubing suitable for use with peristaltic (roller) pump(s) is commercially available from the Plastron, a Tekni-Plex Co., City of Industry, Calif. In one embodiment, the length of the tubing 82 can be approximately 300 millimeters, although any suitable length can be used.

[0054] In FIG. 3, the pump handle 75 is in an upward position and the pump cover 74 is open. In the open position, the rollers 80 do not apply pressure to the tube 82. When the handle 75 is moved downward, or into a closed position as shown in FIGS. 4 and 5, the pump rollers 80 apply pressure, or squeeze the tube 82. As the pump motor rotates as shown in FIG. 5, the rollers 80 rotate and force fluid 84 in the tube 82 to be pumped through the fluid line 22. Although the fluid pump 70 shown in FIGS. 3-5 has four rollers, any suitable number of rollers 80 can be used to provide a desired, relatively steady fluid flow. In the preferred embodiment, the pump 70 has 6 rollers in order to reduce the amplitude of fluid pulsations in the fluid line 22. One example of a roller pump that can be used in one embodiment of the present invention is roller pump model number 900-1021 manufactured by the Barnant Company, Barrington, Ill. In the preferred embodiment of the invention, the roller pump can be powered by an electric motor model number 118752 and planetary gearhead model number 110396, commercially available from Maxon Precision Motors, Burlingame, Calif.

[0055] Referring to FIGS. 2-6, in one embodiment, a fluid supply line securing device 90 can be used to keep the tubing portion 82 of the fluid supply line from being pulled through the roller pump when the pump 70 is operating.

[0056] As shown in FIG. 6, the fluid supply line securing device 90 generally comprises a receiving member 92 that at least partially surrounds tube 82 and prevents tube 82 from being pulled through the roller pump. The outer surface of the tube 82 can be bonded in any suitable manner, such as for example gluing, to an inner surface of a generally tubular channel of the receiving member 92.

[0057] Referring to FIG. 6, in one embodiment, a generally hollow sleeve 94 can be adapted to be inserted into a proximal portion of the tube 82. An outer diameter of the sleeve 94 is generally larger than an inner diameter of the tube 82 so that a portion of the tube 82 around the sleeve 94 is distended when the sleeve 94 is inserted into the tube 82. The portion of the tube 82 around the sleeve 94 becomes wedged against the shoulder 98 formed in the tubular channel of the receiving member 92 and prevents the proximal portion of the tube 82 from being pulled through the receiving member 92.

[0058] As shown in FIG. 6, appropriate placement of the tube 82 within the fluid pump 70 requires that a distal end section 96 of the receiving member 92 becomes abutted against a corresponding surface 93 of a fluid pump housing 97. This prevents the receiving member 92 and the tube 82 from being pulled through the fluid pump when the rollers 80 are rotating.

[0059] Although as shown in FIG. 2, the pump 70 is shown as integrated into the controller 60, it should be understood that the pump 70 could also be located externally to the controller 60, and comprise for example, a stand alone fluid pumping system. In an alternate embodiment, any suitable device for pumping fluid can be used, such as for example, a centrifugal pump or syringe type device. It is a feature of the present invention to be able to provide a variable and/or regulated flow of fluid through the inner lumen of elongated tube 28 during the operation of the system 10.

[0060] As shown in FIG. 2, in one embodiment, the fluid supply system 50 can comprise a fluid bag connected to a drip chamber 52 that is connected to the fluid line 22. The fluid supply line 22 can generally comprise one or more sections of fluid supply tubing that can be coupled together in any suitable manner. As discussed above, in the preferred embodiment, the fluid supply line 22 includes a tubing portion 82 that has special mechanical properties suitable for use with a peristaltic (roller) pump. Preferably, the tubing portion 82 is not only made from a material that has special mechanical properties different from the rest of the fluid supply line 22, but also has inner and/or outer diameters that are different from the inner and/or outer diameters of the rest of the fluid supply line 22.

[0061] The system 10 also includes the activation device 30 that is coupled to the controller 60 via control line or lines 36. Although as shown in FIG. 2, line 36 is a single line, it should be understood that in the preferred embodiment, the line 36 comprises a cable that includes one or more electrical or fiberoptic lines 36. In an alternate embodiment, the line 36 could include pneumatic or other suitable types of communication lines. The activation device 30 is generally adapted to control or activate an increased flow rate of fluid from or through the pump 70. The activation device 30 can also be used to control the activation of the gas turbine of the RAD. Generally, the activation device 30 is a switching device

having “ON” and “OFF” positions. In one embodiment as shown in **FIG. 2**, the activation device **30** comprises a pair of pedal switches, a pump pedal **32** and a turbine pedal **34**. In a preferred embodiment, pedal switches **32** and **34** are electrical switches and control line **36** comprises an electrical cable with more than one wire therein, each wire adapted to carry electrical or communication signals. It is a feature of the present invention to allow an operator of the RAD **20** to increase the speed of the pump **70** or activate the gas turbine using the foot pedals **32** and **34** shown in **FIG. 2**, or a single foot switch **1101** as shown in **FIG. 26**.

[0062] In an alternate embodiment any suitable switching or control device can be used other than a pedal activated switch to provide an “ON” or “OFF” activation signal. For example, as shown in **FIGS. 25 and 26**, a single pedal switch **1010** or **1101** and control systems **1000** or **1100**, may be utilized in such a fashion so that a first activation of the switch (the first pulse or the first control signal) causes the fluid pump **70** to increase its speed of rotation, then the second activation of the switch (the second pulse or the second control signal) causes the fluid pump **70** to continue to rotate at the increased speed and activates the gas turbine, and finally, the third activation of the switch (the third pulse or the third control signal) turns off both the gas turbine and (after a delay if needed) the fluid pump **70**, bringing the entire system to its “steady-state” or “static” mode. For example, in such static mode the fluid pump **70** returns to its minimum or “min” fluid flow rate and the gas turbine is turned “OFF.”

[0063] The controller **60** shown in **FIG. 2** is generally adapted to control and monitor the operations of the system **10**, including the fluid flow rate and gas turbine function and speed. The controller **60** can include displays **61**, **63**, **64**, **65** and **66** to monitor compressed gas pressure applied to the gas turbine of the RAD, turbine rotational speed, various procedure time intervals, and other functions of the system **10**, controls and switches **62**, **67** and **68** to operate the various functions of the system **10** as well as connections to each of the components of the system **10**. The controller **60** will also include the electronics and circuitry needed to operate the system **10**.

[0064] For example, as shown in **FIG. 2**, display **65** can comprise an “individual” event timer adapted to display and/or record the length of time during which the turbine was rotating after each individual activation (“individual event time”). Display **66** can comprise a “procedure timer” that displays the sum of the individual event times, i.e. the total time during which the gas turbine was operational throughout the angioplasty procedure. Each of the displays can include a reset button to reset the time. For example, the “procedure timer” may be used to record a total time used to completely open the stenotic lesion and then reset back to “zero.” Display **63** can be used to display a rotational speed of the turbine **19**. In an alternate embodiment, any suitable number or types of displays can be used for indicating the functions and events of the system **10**.

[0065] Referring to **FIG. 7**, a block diagram illustrating the functional aspects of one embodiment of the controller **60** is shown. With reference to **FIGS. 2 and 7**, the controller **60** can be used to control the activation and speed of the pump **70**, the activation and speed of the gas turbine of the RAD and, for these purposes, can include a fluid pump control unit **610** and a pneumatic valve control unit **650**.

[0066] The pump control unit **610** is generally adapted to control the speed of a fluid pump motor **612** in order to regulate the flow rate of fluid through the inner lumen of the catheter **28**. The fluid pump motor **612** is also shown in **FIGS. 13 and 14** as a fluid pump motor **1612**. The controller **60** can include a minimum pump speed setting control or device **621**, which can be adjusted to set the minimum fluid flow rate or speed of the pump motor **612** when the gas turbine and the drive shaft **25** of the RAD are not rotating, for example. The maximum pump speed setting control or device **622** can be adjusted to set a maximum fluid flow rate, or the maximum speed of the pump motor **612**.

[0067] When electric power is applied to the controller **60**, the pump control unit **610** can set the pump motor **612** to operate in a “steady-state” or “static” mode. In this static mode the gas turbine and the drive shaft **25** are generally not rotating and minimal flow rate of fluid is maintained. When, for example, the fluid pump control switch **632** (which is similar to pedal switch **32** in **FIG. 2**) is activated, the pump control unit **610** can send a signal to the pump motor **612** to increase its speed. The increase of the speed of the pump motor **612** will increase the fluid flow rate.

[0068] The pneumatic valve control unit **650** generally controls the operation of the gas turbine **605** of the RAD. When the turbine control switch **634** (similar to pedal switch **34** in **FIG. 2**) is activated the pneumatic valve control unit **650** sends a signal to activate the turbine pneumatic valve **657**, which allows compressed gas from the turbine pressure regulator **658** to be applied to the gas turbine **605** of the RAD. The fluid pump control unit **610** also communicates with the pneumatic valve control unit **650** to coordinate operation of the fluid pump **70** with the gas turbine of the RAD. It is a feature of the present invention that the turbine control switch **634** needs to be activated within a predetermined time period after the fluid pump control switch **632** is deactivated in order to activate the gas turbine of the RAD. If the turbine control switch **634** is not activated within the predetermined time period after deactivation of the fluid control switch **632**, operation of the gas turbine of the RAD can be either prevented or delayed. In one embodiment, when the turbine control switch **634** is activated before activation of the pump control switch **632**, or after the expiration of the predetermined time period, operation of the gas turbine of the RAD will be delayed for another predetermined time period after activation of turbine control switch **634** during which time the fluid pump **70** is pumping fluid at an increased or maximum speed.

[0069] The turbine pressure regulator **658** could comprise a Precision Low Pressure Regulator, Type LPR-1/4-4, commercially available from FESTO Corporation, Hauppauge, N.Y. The turbine pneumatic valve **657** could comprise a single solenoid valve type MFM-5-1/8-S-B, also available from the FESTO Corporation.

[0070] Compressed gas pressure at the output of the turbine pressure regulator **658** is measured and displayed by the turbine pressure sensor and display device **671**, (which is similar to the turbine pressure display device **61** in **FIG. 2**). Both turbine pressure sensor **671** and turbine tachometer **668** may be in communication with the pneumatic valve control unit **650**, which may be programmed to turn off or deactivate the turbine pneumatic valve **657** if a discrepancy

of predetermined magnitude develops between pressure applied to the gas turbine 605 and the rotational speed of the turbine.

[0071] When the gas turbine of the RAD is activated, the controller 60 can include an “individual” event time indicator 655 (display 65 in FIG. 2) that indicates the length of time during which the turbine was rotating after each individual activation. A “procedure” time indicator 666 (display 66 in FIG. 2) can be used to display a total time during which the gas turbine was operational throughout the angioplasty procedure or part thereof.

[0072] The pneumatic valve control unit 650 could also provide data storage and/or output signal(s) 654 that could be used to plot the operation of the gas turbine and other components of the system 10. For example, the data storage and/or output signal(s) 654 could be fed to a logger or chart recorder in order to plot the time and functions of the gas turbine 605, fluid pump 70 and other elements of the controller 60, such as for example, gas pressure applied to the gas turbine and its rotational speed, under such pressure, may be logged.

[0073] During a rotational angioplasty procedure a fluid such as saline is pumped from the fluid supply 50 through the elongated tube 28. When the gas turbine of the RAD is activated the drive shaft 25 is rotated at a high speed. The turbine block 18 can be moved forward and/or backward with respect to the housing 12 of the RAD 20 thereby allowing the operator to move the drive shaft 25 and its abrasive element 27 forward and/or backward across the stenotic lesion. Generally, in the present invention, when the drive shaft 25 is rotating, saline is being pumped from or through the pump 70 at a higher rate of flow than when the drive shaft 25 is not rotating. The increased flow of saline can provide, among other things, enhanced cooling of the treated area and substantially uninterrupted flushing away of the small particles generated as the stenotic material is removed by the abrasive element 27. Saline is pumped through the elongated tube 28 at a minimal flow rate when the system 10 is in a static state and the drive shaft 25 is not rotating.

[0074] In the present invention, the controller 60 and the activation device 30 are adapted to “delay” activation of the gas turbine of the RAD to provide a “preflush” of saline prior to initiating “active” rotation of the gas turbine. The term “preflush” as used herein describes pumping of saline through the elongated tube 28 at an increased flow rate. For example, referring to FIG. 8, at time $t_{sub.0}$, the gas turbine, represented by its rotational speed ω , is off, and the saline flow rate Q is at flow rate $Q_{sub.1}$. In one embodiment flow rate $Q_{sub.1}$ could be at a minimum or “min” level when the system 10 is in a static mode. Upon activation of switch 32, the saline flow rate Q increases from flow rate $Q_{sub.1}$ to $Q_{sub.2}$. Saline flow rate $Q_{sub.2}$ is a higher flow rate than $Q_{sub.1}$, being for example, a maximum or “max” flow rate. The gas turbine remains off. It should be understood that although the saline flow rate $Q_{sub.2}$ is shown as increasing to the “max” upon activation of pedal switch 32, any suitable flow rate $Q_{sub.2}$ can be used. At time $t_{sub.2}$, the pedal switch 32 is deactivated, or is “OFF.” The saline flow rate remains at increased flow rate $Q_{sub.2}$ for a period of time shown as $t_{sub.delay}$. In FIG. 8 this $t_{sub.delay}$ time period corresponds to the time period between $t_{sub.2}$ and

$t_{sub.5}$. A period of time between $t_{sub.1}$ and $t_{sub.2}$, together with that period of time within $t_{sub.delay}$ during which saline flow is maintained at an increased flow rate prior to activation of the gas turbine, is referred to herein as the “preflush time period.” The drive shaft 25 and its abrasive element 27 are not rotating during the preflush time period.

[0075] The preflush time period prior to activation of the drive shaft 25 provides several advantages. Some of these advantages can include for example, flushing both the abrasive element 27 and the stenotic area to be treated with saline that can include a suitable concentration of heparin and other pharmaceuticals that can prevent platelet aggregation and thrombus formation. The dilution of the blood that flows through the area of treatment and around the abrasive element may be sufficient to significantly reduce the potential for platelet activation, platelet aggregation and thrombus formation. Dilution or even hydrolic occlusion of blood flow through the area of treatment may also reduce the number of red blood cells in the treatment area and or around the abrasive element 27 of the drive shaft 25, and, therefore, prevent hemolysis of the red blood cells at the time when the drive shaft 25 and its abrasive element 27 begin and continue to rotate. In general, the “preflush” flow of fluid to the site of the tissue removal prior to the turbine activation provides a more favorable environment for the rotational angioplasty procedure.

[0076] It is a feature of the present invention to provide a preflush time period so that activation of the gas turbine of the RAD is prevented or precluded without a continuous preflush time period. In the present invention, the acceleration of the saline flow rate is substantially independent from rotation of the gas turbine and drive shaft 25 of the RAD 20. For example, referring to FIG. 9, at time $t_{sub.4}$, the turbine pedal switch 34 is activated or is “ON.” This activation of switch 34 instructs the controller 60 to activate the gas turbine of the RAD 20 and initiate rotation of the gas turbine and drive shaft 25. Since the activation of switch 34 occurs at time $t_{sub.4}$ and within the time period $t_{sub.delay}$, the gas turbine of the RAD is activated. As shown in FIG. 9, the saline flow rate Q remains at increased flow rate $Q_{sub.2}$ during at least the time period $t_{sub.4}$ to $t_{sub.7}$ when the gas turbine is “ON” or rotating.

[0077] Referring to FIG. 10, the $t_{sub.delay}$ time period can be extended or repeated by reactivating the fluid pump pedal switch 32. For example, at time $t_{sub.0}$, the gas turbine is “OFF” and the fluid flow rate is at $Q_{sub.1}$. At time $t_{sub.1}$, fluid pump pedal switch 32 is activated, which, as shown in FIG. 10, is represented as a depression of pump pedal switch 32.

[0078] Activation of the fluid pump switch 32 causes the saline flow rate Q to increase from $Q_{sub.1}$ to $Q_{sub.2}$. At time $t_{sub.2}$, pump pedal switch 32 is released or deactivated and the fluid flow remains at increased flow rate $Q_{sub.2}$. The saline flow rate shall remain at increased saline flow rate $Q_{sub.2}$ for the $t_{sub.delay}$ period, shown as from time $t_{sub.2}$ to time $t_{sub.5}$. As shown in FIG. 10, at the time $t_{sub.3}$ (before the end of the time period $t_{sub.delay}$) fluid pump pedal switch 32 has been activated for a time period $t_{sub.3}$ to $t_{sub.4}$. At the time $t_{sub.4}$, when the fluid pump pedal switch 32 is deactivated, the time period $t_{sub.delay}$ starts again, running from time $t_{sub.4}$ to $t_{sub.8}$. It is a

feature of the present invention that this “preflush” or preflush time period can be executed or extended as many times as desired by the operator of the system 10.

[0079] Referring to FIG. 9, if the turbine pedal switch 34 is activated during the $t_{sub.delay}$ time period, the gas turbine switches “ON.” For example, as shown in FIG. 9, at time $t_{sub.2}$, the fluid pump pedal switch 32 is deactivated and the $t_{sub.delay}$ time period starts, with the fluid flow rate remaining at the increased flow rate $Q_{sub.2}$. At time $t_{sub.4}$, or before the time period $t_{sub.delay}$ has expired, the turbine pedal switch 34 is activated. The gas turbine goes from “OFF” to “ON” and the saline flow rate remains at the increased flow rate $Q_{sub.2}$. At time $t_{sub.7}$ the gas turbine is switched “OFF” by the release of turbine pedal switch 34. In one embodiment, as shown in FIG. 9, the saline flow rate Q can remain at the increased level $Q_{sub.2}$ for another delay time period from time $t_{sub.7}$ to time $t_{sub.9}$ as represented by $t_{sub.delay'}$. In an alternate embodiment, the fluid flow rate could go from $Q_{sub.2}$ to $Q_{sub.1}$ at time $t_{sub.7}$. It is a feature of the present invention to provide a “postflush” or “postflush time period” of accelerated or increased fluid flow rate after the gas turbine and drive shaft 25 stop rotating. The time period for $t_{sub.delay}$ or $t_{sub.delay'}$, can be any suitable or desired time period. The $t_{sub.delay}$ and $t_{sub.delay'}$ time periods may comprise time periods of different length.

[0080] Referring to FIG. 11, if the turbine pedal switch 34 is activated at any time $t_{sub.6}$ after the time period $t_{sub.delay}$ has expired at the time $t_{sub.5}$, then the controller 60 could prevent the turbine from activating. If the gas turbine of the RAD 20 has not been activated during an uninterrupted preflush time period as shown in FIG. 11, then the controller 60 may also be designed or programmed to switch the fluid pump 70 into the “preflush” mode upon activation of the turbine pedal switch 34 and activate the gas turbine of the RAD 20 only after a predetermined preflush time period has expired. It is a feature of the present invention to provide an increased level of fluid flow through an elongated tube 28, and around the drive shaft and through the stenotic treatment area prior to rotation of the drive shaft 25.

[0081] The fluid pump 70 is not powered by or brought into motion by the gas turbine or any other prime mover of the RAD and therefore an acceleration of the fluid flow around the driveshaft 25 is only modestly affected by the rapid rotation of the drive shaft, which when rapidly rotated can act as a screw pump. In the preferred embodiment the rapid rotation of the drive shaft 25 causes about a 30% decrease in accelerated fluid flow rate when compared to accelerated fluid flow rate around a non-rotating drive shaft.

[0082] Referring to FIG. 12A, a timing circuit 200 could be used to provide the $t_{sub.delay}$ time period after deactivation of the pump pedal switch 32 in the embodiment(s) of the invention shown in FIG. 2 and FIGS. 7-11.

[0083] Switch 232 of the timing circuit 200 remains “open” for as long as the pump pedal switch 32 is not activated. During that time period voltage across the capacitor $C_{sub.1}$ is equal to the voltage across capacitor $C_{sub.2}$ (voltages at inputs 5 and 7 of the Digital Circuit NE 555 are equal) and a control signal $U_{sub.out}$ is 0 (zero). Activation of pedal switch 32 at the time $t_{sub.1}$ in FIG. 8, for example, will “close” switch 232 thereby causing immediate discharge of the capacitor $C_{sub.1}$ through the transistor $Q_{sub.2}$. The control signal $U_{sub.out}$ of the Digital Circuit NE 555 will immediately change from 0 to 1.

[0084] At the time $t_{sub.2}$ in FIG. 8, for example, when the fluid pump pedal 32 is released and switch 232 opens, the capacitor $C_{sub.1}$ charges and the Digital Circuit NE 555 provides control signal $U_{sub.out}$ equal to 1 until the capacitor $C_{sub.1}$ is fully charged. Therefore the fluid pump 70 continues to pump fluid at an accelerated or increased fluid flow rate only for as long as the control signal $U_{sub.out}$ remains at 1.

[0085] At the time $t_{sub.5}$ in FIG. 8, when the capacitor $C_{sub.1}$ of the timing circuit 200 becomes fully charged (voltages at the inputs 7 and 5 become equal), the control signal $U_{sub.out}$ will change from 1 to 0, thereby causing the fluid pump 70 to return to pumping fluid at the minimum or “min” fluid flow rate.

[0086] The $t_{sub.delay}$ time period shown in FIGS. 8-11 is defined by a charge time of the capacitor $C_{sub.1}$, in the timing circuit 200. The charge time of the capacitor $C_{sub.1}$, and the $t_{sub.delay}$ time period shown in FIGS. 8-11 may be adjusted within certain limits by the potentiometer $R_{sub.2}$ in the timing circuit 200.

[0087] A separate timing circuit similar to the timing circuit 200 can be used with the turbine pedal switch 34 in order to provide the $t_{sub.delay'}$ time period and “postflush” of accelerated flow of fluid after the turbine pedal switch 34 is released.

[0088] As shown in FIG. 12B a single timing circuit 210 may provide equal $t_{sub.delay}$ and $t_{sub.delay'}$ time periods. This is accomplished by connecting in parallel switches 232 and 234, which correspond to pedal switches 32 and 34 in FIG. 2 and FIGS. 8-11.

[0089] The controller 60 could also include one or more safety devices to monitor proper operation of the system 10. For example, in one embodiment as shown in FIG. 7, the controller 60 could include a pump cover sensor 624. The pump cover sensor 624 could indicate whether the pump cover 74 shown in FIG. 2 is in an open or closed position. For example, as shown in FIG. 4, when the pump handle 75 is in a “DOWN” position, the pump cover sensor 624 can provide the pump control unit 610 with a suitable signal which allows the pump control unit 610 to activate the pump motor 612. If the pump cover 74 is “OPEN”, as indicated by the pump cover handle 75 being in an “UP” position as shown in FIG. 3, pump cover sensor 624 will either not provide the signal that is needed to activate the pump motor 612 or can generate a signal that prevents the pump motor from being activated. Therefore, when the pump cover 74 is “OPEN”, operation of the pump motor 612 can be prevented or interrupted.

[0090] In one embodiment as shown in FIGS. 13 and 14 the pump cover sensor 624 could comprise a switch device 310 adapted to detect a closed or open position of the pump cover 74. For example, as shown in FIG. 13 when the pump handle 75 is in an “UP” position, the pump cover 74 is in an “OPEN” position. In FIG. 14 when the pump handle 75 is “DOWN”, the pump cover 74 is “CLOSED.” In the preferred embodiment, the switch 310 could comprise a magnetically operated sealed switch that uses a magnet 312 to preferably determine a “CLOSED” position of the pump cover 74. Such a switch, also called a reed switch, is commercially available from Premier Farnell plc of Chicago, Ill. In an alternate embodiment, any suitable device or

switch can be used to determine an "OPEN" or "CLOSED" position of the pump cover 74, such as for example, a Hall effect switch, an optical switch, a mechanical switch or a limit switch.

[0091] As shown in FIG. 7, a fluid alarm unit 630 could be used to provide an audible and/or visual warning of the pump cover condition. For example, when the pump cover 74 is open, an audible alarm device 682 and/or a visual alarm device 684 can be activated to warn the user of the condition. An indicator 64 of the controller 60 shown in FIG. 2 could be used to display the visual warning. An audible alarm or verbal warning may be provided via siren or speaker 69 shown in FIG. 2.

[0092] As shown in FIG. 7 the controller 60 could also include a fluid level sensor 626. The fluid level sensor 626 could be used to detect a low level of fluid in the fluid supply system 50. The fluid level sensor 626 is in communication with both the fluid pump control unit 610 and the fluid alarm unit 630. If during an angioplasty procedure the fluid level in the saline bag 50 reaches a predetermined low level, then a fluid alarm unit 630 can activate visual and audible alarm devices 684 and 682 in order to warn or advise the operator of the system 10 of the condition. The controller 60 could also include an alarm mute device 636 that can allow the user to silence or mute the audible alarm device 682 for a predetermined period of time or a predetermined number of revolutions of the pump motor 612. Furthermore, in one embodiment of the invention, operation of the pump motor 612 and/or the gas turbine could be prevented or stopped if the fluid level sensor 626 detects a predetermined low level of fluid in the saline bag of the fluid supply 50. If the pump motor 612 is operating and the fluid sensor 626 detects a low fluid level, in one embodiment the fluid alarm unit 630 could activate the visual alarm device 684 and/or provide a verbal warning or activate audible alarm device 682 to indicate the situation to the user. The alarm mute device 636 can allow the user to silence the alarm 682 and continue the procedure. The visual alarm 684 could remain active. The controller 60 could also be adapted to reactivate the audible alarm 682 after it was silenced if a predetermined time period elapses or if the fluid pump 70 or pump motor makes a predetermined number of revolutions or if the fluid level reaches a next predetermined low level. This process could continue for as long as the operator desires or until a predetermined minimum level of fluid is reached. The controller 60 could also include a fluid pump blocking control switch 625, that when activated, could prevent operation of the fluid pump motor 612. Referring to FIG. 2, in one embodiment of the present invention, a push button 82 can be used to silence the audible alarm device 69 and push button 68 to operate the pump blocking control or device 625 shown in FIG. 7. In the preferred embodiment of the invention push button 68 comprises a pushbutton switch with a red screen. If an operator of the controller 60 activates push button 68 (prevents or stops operation of the fluid pump 70), then red screen of the pushbutton switch becomes illuminated by a filament or LED lamp.

[0093] The pushbutton switches of the type used in the preferred embodiment of this invention are commercially available from Apem Components, Inc. of Wakefield, Mass.

[0094] Referring to FIGS. 15 and 16, one embodiment of a fluid level detection system 300 is shown. In FIG. 2, the

fluid container 50 is suspended from a mounting pole or member 302. One end of the pole 302 is inserted into a receptacle 304. As shown in FIG. 15, the lower end of the pole member 302 comes to rest against a horizontal beam member 310. The beam member 310 is adapted to pivot around a point (not shown). In one embodiment, one end 312 of the beam member 310 is adapted to move in a downward direction as the combined weight of the fluid bag 50 and the pole member 302 bears down on the end 312 of the beam member 310. The combined weight or force exerted by the fluid bag 50 and the pole member 302 determines the movement or displacement of the end 312. The other end 314 of the beam member 310 is adapted to move in a direction opposite to the movement of the end 312. A bias element 316, such as for example a spring, can be used to apply to the end 314 a biasing force directed in the direction opposite to the direction of movement of the end 314 of the beam member 310. Compressing the bias element 316 using a bolt or screw type device 320 can increase the tension of the bias element 316 and the force that the bias element 316 exerts on the end 314. For example, as shown in FIG. 15, a bolt 320 is inserted into a block 318 and as the bolt 320 is turned, the block 318 moves in a downward direction compressing the spring 316 and increasing its tension. The increased tension of the spring 316 increases the biasing force applied to the end 314. In operation, when a full saline bag is placed on the pole 302, the end 312 is forced by the combined weight of the bag 50 and pole 302 to deflect downward a certain distance. As the fluid in the bag 50 is depleted, the weight of the fluid bag 50 decreases and the end 312 moves in an upward direction while the end 314 moves downward. As shown in FIG. 16, when the fluid level in the saline bag 50 reaches a predetermined level, the end 314 of beam member 310 comes in contact with a switch device 322. The contact of the member 314 with the switch device 322 can cause the fluid alarm unit 630, shown in FIG. 7, to activate visual and audible alarm devices 684 and 682. In an alternate embodiment, any suitable device or mechanism can be used to monitor the fluid level in the saline bag. It is a feature of the present invention to provide a warning to the operator of the system 10 that the fluid level in the fluid supply 50 has reached a predetermined low level.

[0095] FIGS. 17 and 18 show another embodiment of a fluid level detection system 800. In this embodiment, the pole member 302 rests on a rod 824 that activates switch device 822 when the fluid level in the fluid supply 50 is above a predetermined low level. As the fluid level decreases and reaches a predetermined level, a spring 830 or other biasing element starts to move rod 824 in an upward direction. As shown in FIG. 18, when the fluid level in the fluid bag 50 reaches a predetermined low level, rod 824 gets out of contact with and deactivates switch 822, thereby causing fluid alarm unit 630, shown in FIG. 7, to activate visual alarm device 634 and audible alarm 932.

[0096] In the preferred embodiment, audible alarm device 682 is activated with a certain predetermined delay with respect to the visual alarm device 684. Such a sequence of alarms is advantageous in order to limit any disturbance to the patient.

[0097] FIGS. 19 and 20 show yet another embodiment of a fluid level detection system 850. In this embodiment a biasing element or spring 852 is disposed around the lower portion of the pole 854. In operation, when a full saline bag

50 is placed on the pole **854**, the biasing element **852** becomes compressed between a shoulder **850** of the pole **854** and an adjustment element or screw **857**. The combined weight of the full bag **50** and the pole itself will force the lower end of the pole against a switch device **858**, thereby providing for direct activation of the switch device **858** by the lower end of the pole.

[0098] As shown in **FIG. 20**, when the fluid level in the bag **50** reaches a predetermined low level, the biasing spring **852** moves the pole **854** in an upward direction, thereby deactivating switch device **858** and causing fluid alarm unit to activate visual and audible alarms.

[0099] **FIGS. 21 and 22** show yet another embodiment of a fluid detection system **860** in which a tensiometer device **862** is utilized instead of a switch device. The tensiometer device measures the pressure applied to the device and generates a corresponding electrical signal. A spring type device incorporating e.g. spring **864** can be used to dampen the impact of the pole **866** against the tensiometer device **862** in order to prevent damage to the tensiometer device. However, as shown in **FIG. 23**, the pole **867** of a modified fluid level detection system **860'** can directly contact the tensiometer device **862**. In one embodiment, the tensiometer device **862** can include internal mechanisms to dampen the impact on of the pole on the tensiometer device, when, for example, a fluid bag **50** is placed on the pole **867**.

[0100] As shown in **FIG. 7**, the controller **60** could also include an input compressed gas pressure sensor(s) combined with a compressed gas shutoff valve(s) **670**. In the preferred embodiment, the shutoff valve **670** is generally adapted to shut off the compressed gas supply to the turbine pressure regulator or the controller **60** when the input compressed gas pressure from the system pressure regulator **42** of the compressed gas source **40** exceeds a predetermined level. An additional pressure sensor combined with its own low pressure shutoff valve may be adapted to shut off the compressed gas supply to the turbine pressure regulator **658** or the controller **60** when the input gas pressure is at or below a predetermined level. In addition, input pressure sensors may generate a signal to the pneumatic valve control unit **650** that preclude activation of the turbine pneumatic valve **657** and therefore, the gas turbine **605** of the RAD. The signal from the input pressure sensor(s) may also activate a visual and/or audible alarm device, either directly or indirectly via the pneumatic valve control unit **650**. The gas pressure alarm device or gas pressure alarm(s) **673** may be programmed to warn about the input gas pressure being or becoming either too high or too low. Input compressed gas pressure that does not exceed a predetermined upper level, or is within a predetermined range between upper and lower levels is supplied to the turbine pressure regulator **658**. A control knob **62** of the turbine pressure regulator **658** is shown in **FIG. 2** and can be used to adjust the gas pressure applied to the gas turbine of the RAD.

[0101] A turbine pressure sensor and turbine pressure display device **671** can be used to display the gas pressure applied to the gas turbine. The turbine pressure sensor and the turbine pressure display device **671** can be combined into one device, such as for example an analog pressure gauge **61** as shown in **FIG. 2**. Although the gauge **61** shown in **FIG. 2** is illustrated as an analog device, any suitable indicator can be used, such as for example a digital display.

In an alternate embodiment, the pressure could be displayed on a system other than the controller **60**, such as for example an external display or monitor.

[0102] The rotational speed of the gas turbine of the RAD shown in **FIG. 2** can be monitored by a turbine tachometer **668** shown in **FIG. 7**. In the preferred embodiment an improved optical tachometer for the RAD, such as that described in U.S. Pat. No. 6,039,747 to Shturman can be used. Referring to **FIG. 2**, in the preferred embodiment, the optical tachometer **63** utilizes only one optical fiber **23** to conduct both uninterrupted light from the controller **60** to the RAD **20** and pulsed light back to the controller **60**. In the rotational angioplasty system of the prior art, shown in **FIG. 1** and described in U.S. Pat. No. 5,314,407 to Auth the turbine optical tachometer utilizes two optical fibers. The controller **60** of the present invention can be adapted to interface with this turbine tachometer of the prior art. In an alternative embodiment, any suitable device can be used to monitor the rotational speed of the turbine, including for example optical, electro-optical, electromagnetic and acoustic tachometers can be used.

[0103] As shown in **FIG. 2**, the rotational speed of the turbine of the RAD can be displayed on a turbine tachometer display **63**. In the preferred embodiment of the invention, shown in **FIG. 2**, a digital tachometer display **63** is utilized. In an alternate embodiment, any suitable device, including for example an analog display device, can be used to display the rotational speed of the gas turbine of the RAD.

[0104] As shown in **FIG. 7**, in the preferred embodiment, the controller **60** may also include a tachometer test device **674** to test for adequate function of that portion of the turbine tachometer that is located in the controller **60**. A pushbutton switch could be included on the controller **60** for this purpose.

[0105] In one embodiment, as shown in **FIG. 7**, the turbine tachometer **668** can be coupled or connected to the pump control unit **610**. The turbine tachometer **668** could provide an input signal to the pump control unit **610**, thereby causing adjustment of the rotational speed of the fluid pump motor **612** depending on the rotational speed of the gas turbine.

[0106] It should be understood that although the switches **32** and **34** in **FIG. 2**, and similar switches in **FIGS. 7 and 24**, are shown as two separate pedal activated switches, any suitable switching device(s) can be used, including a switching device comprising a single switch.

[0107] Referring to **FIG. 24**, one embodiment of a control system **900** for controlling fluid pump **904** and gas turbine **305** of rotational angioplasty device is illustrated. As shown in **FIG. 24**, a microcontroller **901**, receives a combination of inputs comprising U.sub.P1 from pump pedal switch **932** (which is similar to the fluid pump pedal switch **32** in **FIG. 2**), U.sub.P2 from turbine pedal switch **934** (which is similar to the turbine pedal switch **34** in **FIG. 2**), and a turbine speed signal U.omega. from a turbine tachometer **902**. It should be understood that the microcontroller based control system shown in **FIG. 24** can be programmed to perform substantially all of the functions of the control system shown in **FIGS. 2 and 7**. In particular, in one embodiment, the microcontroller **901** can be programmed to activate a turbine pneumatic valve **903** only if the fluid pump **904** was acti-

vated to pump saline at an accelerated rate for at least a minimum predetermined period of time using the pump pedal switch **932** and if the turbine pedal switch **934** was activated within a predetermined time period $t_{sub.delay}$ after the pump pedal switch **932** has been deactivated.

[0108] As shown in **FIG. 25**, a single pedal activated switch **1010** could be used to control microcontroller **1001** where a first switch activation establishes a first mode of operation for the system **1000** (e.g. the fluid pump **1004** is “ON”). A second switch activation establishes a second mode of operation for the system **1000** (e.g. both the fluid pump **1004** and the gas turbine **1005** are “ON” or active). A third switch activation returns the system to its “static” state where the fluid pump is at minimum or “min” flow rate and the gas turbine is “OFF.”

[0109] An example of a single pedal switch **1101** is shown in **FIG. 26**. All other elements of the system **1100** shown in **FIG. 26** are similar and have the same numbers as the elements of the system **10** shown in **FIG. 2**.

[0110] It should be understood that the foregoing description is only illustrative of the invention. Various alternatives and modifications can be devised by those skilled in the art without departing from the invention. Accordingly, the present invention is intended to embrace all such alternatives, modifications and variances which fall within the scope of the appended claims.

1-87. (canceled)

88. A system for controlling a flow of fluid through a rotational atherectomy device comprising:

controller coupled to the atherectomy device, the controller comprising:

- a pump control device adapted to control the flow of fluid to the atherectomy device;
- a drive shaft control device adapted to control a rotation of a drive shaft in the atherectomy device;
- a fluid supply unit;
- a first control device coupled to the controller and adapted to increase a flow of fluid to the atherectomy device via the pump control device; and
- a second control device coupled to the controller and adapted to initiate a rotation of the drive shaft via the drive shaft control device after activation of the first control device.

89. The system of claim 88, wherein an increased flow of fluid to the atherectomy device is relatively independent of a rotation speed of the drive shaft.

90. The system of claim 88, wherein the controller further comprises a fluid flow delay device adapted to maintain the increased flow of fluid through the rotational atherectomy device for a predetermined time period after a deactivation of the first control device.

91. The system of claim 88, wherein the controller further comprises a drive shaft disable device adapted to prevent the rotation of the drive shaft if the second control device is activated after the end of a predetermined time period after a deactivation of the first control device.

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