



(86) Date de dépôt PCT/PCT Filing Date: 2012/09/21
(87) Date publication PCT/PCT Publication Date: 2013/03/28
(45) Date de délivrance/Issue Date: 2020/02/18
(85) Entrée phase nationale/National Entry: 2014/03/21
(86) N° demande PCT/PCT Application No.: IB 2012/055030
(87) N° publication PCT/PCT Publication No.: 2013/042080
(30) Priorité/Priority: 2011/09/23 (EP11182585.7)

(51) Cl.Int./Int.Cl. *B01J 23/44* (2006.01),
B01J 23/42 (2006.01), *B01J 37/025* (2006.01)
(72) Inventeurs/Inventors:
GRUBERT, GERD, DE;
NEUBAUER, TORSTEN, DE;
PUNKE, ALFRED, DE;
HILGENDORFF, MARCUS, DE;
MULLER-STACH, TORSTEN, DE;
...
(73) Propriétaires/Owners:
BASF SE, DE;
BASF CORPORATION, US
(74) Agent: BORDEN LADNER GERVAIS LLP

(54) Titre : CATALYSEUR D'OXYDATION DIESEL A STRUCTURE EN COUCHES, CONTENANT UNE COMPOSITION D'OXYDE DE CERIUM COMME MATERIAU DE SUPPORT DE PALLADIUM POUR CONVERSION DE GAZ HC ET CO AMELIOREE

(54) Title: DIESEL OXIDATION CATALYST WITH LAYERED STRUCTURE CONTAINING CERIA COMPOSITION AS PALLADIUM SUPPORT MATERIAL FOR ENHANCED HC AND CO GAS CONVERSION

(57) **Abrégé/Abstract:**

A layered diesel oxidation catalyst (DOC) comprises: a) a carrier substrate; b) a diesel oxidation catalytic material comprising b1) a first layer located on the carrier substrate, the first layer comprising palladium impregnated on a support material comprising ceria in an amount of at least 45 weight% based on the total weight of the support material, and optionally comprising platinum; b2) a second layer located on the first layer, the second layer comprising palladium and platinum each impregnated on a support material comprising a metal oxide; wherein the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer.

(72) **Inventeurs(suite)/Inventors(continued)**: GERLACH, OLGA, DE; WEI, XINYI, US; HOKE, JEFFREY, US;
SUNG, SHIANG, US; ROTH, STANLEY, US

(12) INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(19) World Intellectual Property
Organization
International Bureau(10) International Publication Number
WO 2013/042080 A1(43) International Publication Date
28 March 2013 (28.03.2013)

(51) International Patent Classification:

B01J 23/44 (2006.01) **B01J 37/025** (2006.01)
B01J 23/42 (2006.01)

(21) International Application Number:

PCT/IB2012/055030

(22) International Filing Date:

21 September 2012 (21.09.2012)

(25) Filing Language:

English

(26) Publication Language:

English

(30) Priority Data:

11182585.7 23 September 2011 (23.09.2011) EP

(71) Applicants (for all designated States except US): **BASF SE** [DE/DE]; 67056 Ludwigshafen (DE). **BASF CORPORATION** [US/US]; 100 Park Avenue, Florham Park, New Jersey 07932 (US).(71) Applicant (for MN only): **BASF (CHINA) COMPANY LIMITED** [CN/CN]; 300, Jiang Xin Sha Road, Pudong, Shanghai 200137 (CN).

(72) Inventors; and

(71) Applicants (for US only): **GRUBERT, Gerd** [DE/DE]; Auf dem Lärchenberge 14 b, 30161 Hannover (DE). **NEUBAUER, Torsten** [DE/DE]; Robert-Koch-Str. 22 A, 30853 Langenhagen (DE). **PUNKE, Alfred** [DE/DE]; Im Dorfe 36C, 38179 Walle (DE). **HILGENDORFF, Marcus** [DE/DE]; Anecampstr. 49 F, 30539 Hannover (DE). **MÜLLER-STACH, Torsten** [DE/DE]; Jakobistr. 24, 30163 Hannover (DE). **GERLACH, Olga** [RU/DE]; Karl-Dillinger-Strasse 18, 67071 Ludwigshafen (DE). **WEI, Xinyi** [US/US]; 58 Sayre Drive, Princeton, New Jersey 08540 (US). **HOKE, Jeffrey** [US/US]; 1374 Luke Street, North Brunswick, New Jersey 08902 (US). **SUNG, Shiang**[US/US]; 300 E 90th Street, Apt 5D, New York, New York 10128 (US). **ROTH, Stanley** [US/US]; 167 Crestview Way, Yardley, Pennsylvania 19067 (US).(74) Agent: **ALTMANN, Andreas**; Herzog Fiesser & Partner, Patent Attorneys, Isartorplatz 1, 80331 Munich (DE).

(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BN, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PA, PE, PG, PH, PL, PT, QA, RO, RS, RU, RW, SC, SD, SE, SG, SK, SL, SM, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LR, LS, MW, MZ, NA, RW, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, RU, TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK, SM, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

Published:

- with international search report (Art. 21(3))
- before the expiration of the time limit for amending the claims and to be republished in the event of receipt of amendments (Rule 48.2(h))

(54) Title: DIESEL OXIDATION CATALYST WITH LAYERED STRUCTURE CONTAINING CERIA COMPOSITION AS PALLADIUM SUPPORT MATERIAL FOR ENHANCED HC AND CO GAS CONVERSION

(57) Abstract: A layered diesel oxidation catalyst (DOC) comprises: a) a carrier substrate; b) a diesel oxidation catalytic material comprising b1) a first layer located on the carrier substrate, the first layer comprising palladium impregnated on a support material comprising ceria in an amount of at least 45 weight% based on the total weight of the support material, and optionally comprising platinum; b2) a second layer located on the first layer, the second layer comprising palladium and platinum each impregnated on a support material comprising a metal oxide; wherein the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer.



WO 2013/042080 A1

Diesel Oxidation Catalyst with layered structure containing Ceria Composition as Palladium Support Material for Enhanced HC and CO Gas Conversion

Technical Field

5

The present invention relates to a layered oxidation catalyst, in particular for the treatment of diesel engine exhaust, containing ceria as palladium support material.

Background

10

Operation of lean burn engines, e.g. diesel engines and lean burn gasoline engines, provide the user with excellent fuel economy, and have very low emissions of gas phase hydrocarbons and carbon monoxide due to their operation at high air/fuel ratios under fuel lean conditions. Diesel engines, in particular, also offer significant advantages over gasoline engines in terms of their fuel economy, durability, and their ability to generate high torque at low speed. From the standpoint of emissions, however, diesel engines present problems more severe than their spark-ignition counterparts. Emission problems relate to particulate matter (PM), nitrogen oxides (NO_x), unburned hydrocarbons (HC) and carbon monoxide (CO). NO_x is a term used to describe various chemical species of nitrogen oxides, including nitrogen monoxide (NO) and nitrogen dioxide (NO₂), among others.

20

Oxidation catalysts comprising precious metals such as platinum group metals (PGM) dispersed on a refractory metal oxide support are known for use in treating the exhaust of diesel engines in order to convert both hydrocarbon and carbon monoxide gaseous pollutants by catalyzing the oxidation of these pollutants to carbon dioxide and water. Such catalysts have been generally contained in units called diesel oxidation catalysts (DOC), or more simply catalytic converters, which are placed in the exhaust flow path from a diesel powered engine to treat the exhaust before it vents to the atmosphere. Typically, the diesel oxidation catalysts are formed on ceramic or metallic substrate carriers upon which one or more catalyst coating compositions are deposited. In addition to the conversions of gaseous HC, CO and the soluble organic fraction (SOF) of particulate matter, oxidation catalysts containing platinum group metals dispersed on a refractory oxide support promote the oxidation of nitric oxide (NO) to nitric dioxide (NO₂).

25

30

As is well-known in the art, catalysts used to treat the exhaust of internal combustion engines are less effective during periods of relatively low temperature operation, such as the initial cold-start period of engine operation, because the engine exhaust is not at a temperature sufficiently high for efficient catalytic conversion of noxious components in the exhaust. To this end, it is known in the art to include an adsorbent material, which may be a zeolite, as part of a catalytic treatment system in order to adsorb gaseous pollutants, usually hydrocarbons, and retain them during the initial cold-start period. As the exhaust gas temperature increases, the adsorbed hydrocarbons are driven from the adsorbent and subjected to catalytic treatment at the higher temperature. In this regard, US 5,125,231

40

discloses the use of platinum group metal-doped zeolites as low temperature hydrocarbon adsorbents as well as oxidation catalysts.

As discussed hereinabove, oxidation catalysts comprising a platinum group metal (PGM) dispersed on a refractory metal oxide support are known for use in treating exhaust gas emissions from diesel engines. Platinum (Pt) remains the most effective platinum group metal for oxidizing CO and HC in a DOC, after high temperature aging under lean conditions and in the presence of fuel sulfur. Nevertheless, one of the major advantages of using palladium (Pd) based catalysts is the lower cost of Pd compared to Pt. However, Pd based DOCs typically show higher light-off temperatures for oxidation of CO and HC, especially when used with HC storage materials, potentially causing a delay in HC and or CO light-off. Pd containing DOCs may poison the activity of Pt to convert paraffins and/or oxidize NO and may also make the catalyst more susceptible to sulfur poisoning. These characteristics have typically prevented the use of Pd as an oxidation catalyst in lean burn operations especially for light duty diesel applications where engine temperatures remain below 250 °C for most driving conditions. As emissions regulations become more stringent, there is a continuing goal to develop diesel oxidation catalyst (DOC) systems that provide improved performance, for example, light-off performance.

WO2010/133309 discloses Pd enriched diesel oxidation catalysts and their application as catalysts for the oxidation of CO and HC emissions from a compression ignition/diesel engine.

WO2010/083313 discloses a diesel oxidation catalyst comprising at least two, specifically three distinct layers, at least one of which contains an oxygen storage compound (OSC) that is present in a layer separate from the majority of the platinum group metal (PGM) components, such as palladium and platinum.

US 2008/045405 discloses a diesel oxidation catalyst for the treatment of exhaust gas emissions, such as the oxidation of unburned hydrocarbons and carbon monoxide, and the reduction of nitrogen oxides. More particularly, US 2008/045405 is directed to a washcoat composition comprising two distinct washcoat layers containing two distinctly different weight ratios of Pt:Pd.

However, these prior art DOCs still show unsatisfactory breakthrough of HC and CO. Further, hydrocarbon storage capacity of these prior art DOCs is enhanced at the expense of the catalytic activity of the catalyst.

Consequently, the present invention is directed to a diesel oxidation catalyst with a layered structure in order to maximize the hydrocarbon storage capacity without sacrificing the catalytic activity of the catalyst. Additionally, it was an object of the present invention to provide a DOC which continually supports the oxidation and abatement of CO and unburned HC and thus allows for a minimum breakthrough of HC and CO. Finally, it was an object of

the present invention to provide a DOC which, due to the rarity and consequently costs of precious metal components usually used for the preparation of DOCs, contains a reduced amount of platinum in the catalyst composition allowing for reduced costs for the DOC without reducing the catalytic efficiency. There is also a goal to utilize other components of DOCs, for example the zeolites, ceria, and palladium, as efficiently as possible.

Summary

Provided is a layered diesel oxidation catalyst (DOC) comprising:

- 10 a) a carrier substrate;
- b) a diesel oxidation catalytic material comprising
 - b1) a first layer located on the carrier substrate, the first layer comprising palladium impregnated on a support material comprising ceria in an amount of at least 45 weight-% based on the total weight of the support material, and optionally comprising platinum;
 - 15 b2) a second layer located on the first layer, the second layer comprising palladium and platinum each impregnated on a support material comprising a metal oxide;wherein the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer.

20 Further provided is a process for the preparation of such layered diesel oxidation catalyst comprising the steps of

- (i) providing a carrier substrate;
 - (ii) optionally applying an undercoat layer on the carrier substrate;
 - (iii) applying a first layer on the carrier substrate or the undercoat layer, the first layer 25 comprising palladium impregnated on a support material comprising ceria in an amount of at least 45 weight-% based on the total weight of the support material, and optionally comprising platinum;
 - (iv) applying a second layer on the first layer, the second layer comprising palladium and platinum each impregnated on a support material comprising a metal oxide,
 - 30 wherein the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer;
 - (v) optionally applying a third layer on the second layer, the third layer comprising palladium impregnated on a support material comprising ceria in an amount of at least 45 weight-% based on the total weight of the support material, and optionally comprising 35 platinum;
- wherein the platinum to palladium weight ratio of the third layer is lower than the platinum to palladium weight ratio of the second layer.

40 Yet further provided is a system for treating a gaseous exhaust stream of a diesel engine, the system comprising:

an exhaust conduit in fluid communication with the diesel engine via an exhaust manifold, the layered diesel oxidation catalyst as defined above, wherein the carrier substrate is a wall-flow substrate or a flow through substrate, and

one or more of the following in fluid communication with the layered diesel oxidation catalyst composite: a catalyzed soot filter (CSF), a selective catalytic reduction (SCR) article, a NO_x storage and reduction (NSR) catalytic article.

- 5 Still further provided is a method of treating a diesel exhaust stream, the method comprising contacting the exhaust stream with the layered diesel oxidation catalyst as defined above.

Brief Description of the Drawings

10 Figure 1 shows CO light-off curves obtained from the treatment of diesel exhaust using the DOCs according to Samples A), B), C), D) and E). The x-axis of the diagram denoted "Catalyst Inlet T / °C" shows the respective catalyst inlet temperature in °C and ranges from 120 °C to 280 °C, whereas the y-axis denoted "CO-Eff / %" shows the corresponding efficacy of CO oxidation to CO₂ in % and ranges from 0 % to 100 %. The values for Sample A) according to the invention are displayed in a solid line with bullets, the values for Sample B) according to the invention are displayed in a dotted line, the values for Sample C) according to the invention are displayed in a dashed line, the values for Sample D) not according to the invention are displayed in a solid line, and the values for Sample E) not according to the invention are displayed in a solid line with crosses.

20 Figure 2 shows HC light-off curves obtained from the treatment of diesel exhaust using the DOCs according to Samples A), B), C), D) and E). The x-axis of the diagram denoted "Catalyst Inlet T / °C" shows the respective catalyst inlet temperature in °C and ranges from 120 °C to 280 °C, whereas the y-axis denoted "HC-Eff / %" shows the corresponding efficacy of HC oxidation to CO₂ in % and ranges from 0 % to 100 %. The values for Sample A) according to the invention are displayed in a solid line with bullets, the values for Sample B) according to the invention are displayed in a dotted line, the values for Sample C) according to the invention are displayed in a dashed line, the values for Sample D) not according to the invention are displayed in a solid line, and the values for Sample E) not according to the invention are displayed in a solid line with crosses.

35 Figure 3 shows HC and CO light-off temperatures at 50 % conversion (CO) and 70 % conversion (HC) obtained from the treatment of diesel exhaust using the DOCs according to Samples A), B), C), D) and E). The x-axis of the diagram shows the respective Samples A) to E), whereas the y-axis denoted "CO Light-off @ 50 % Conversion / °C" and " HC Light-off @ 70 % Conversion / °C" shows the corresponding temperatures at which 50 % of CO are oxidized to CO₂ and at which 70 % of HC are oxidized to CO₂, respectively, and ranges from 100 °C to 260 °C. The values for CO conversion are displayed as checkered bars, and the values for HC conversion are displayed as dashed bars.

40

Detailed Description

The present invention relates to a layered diesel oxidation catalyst (DOC) comprising:

- a) a carrier substrate;
- b) a diesel oxidation catalytic material comprising
- b1) a first layer located on the carrier substrate, the first layer comprising palladium impregnated on a support material comprising ceria in an amount of at least 45 weight-% based on the total weight of the support material, and optionally comprising platinum;
- 5 b2) a second layer located on the first layer, the second layer comprising palladium and platinum each impregnated on a support material comprising a metal oxide;
- wherein the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer.

10

Generally, there are no specific restrictions as far as the platinum to palladium weight ratio of the first layer is concerned provided that the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer. Preferably, the platinum to palladium weight ratio of the first layer is in the range of from 0:1 to 1.1:1.

15

Therefore, the present invention also relates to the diesel oxidation catalyst as defined above, wherein the platinum to palladium weight ratio of the first layer is in the range of from 0:1 to 1.1:1.

20

Likewise, there are no specific restrictions as far as the platinum to palladium weight ratio of the second layer is concerned provided that the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer. Preferably, the platinum to palladium weight ratio of the second layer is in the range of from 1:0 to 1.1:1, more preferably in the range of from 10:1 to 1.5:1, even more preferably in the range of from

25 5:1 to 2:1, most preferably in a ratio of 2:1, provided that the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer.

30

Therefore, the present invention also relates to the diesel oxidation catalyst as defined above, wherein the platinum to palladium weight ratio of the second layer is in the range of from 1:0 to 1.1:1, preferably in the range of from 10:1 to 1.5:1, more preferably in the range of from 5:1 to 2:1, most preferably in a ratio of 2:1.

35

According to the present invention, the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer. Preferably, the ratio of the platinum to palladium weight ratio of the first layer to the platinum to palladium weight ratio of the second layer is lower than or equal to 0.9.

40

Therefore, the present invention also relates to the diesel oxidation catalyst as defined above, wherein the ratio of the platinum to palladium weight ratio of the first layer to the platinum to palladium weight ratio of the second layer is lower than or equal to 0.9.

According to the present invention, the first layer comprises palladium impregnated on a support material comprising ceria in an amount of at least 45 weight-% based on the total

weight of the support material. Preferably, the support material of the first layer comprises ceria in an amount of at least 65 weight-%, more preferably at least 85 weight-%, even more preferably at least 95 weight-%, most preferably 100 weight-% based on the total weight of the support material.

5

Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the support material of the first layer comprises ceria in an amount of at least 65 weight-%, preferably at least 85 weight-%, more preferably at least 95 weight-%, most preferably 100 weight-% based on the total weight of the support material.

10

Preferably, the support material of the first layer further comprises zirconia and/or alumina.

Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the support material of the first layer further comprises zirconia and/or alumina.

15

Preferably, the support material of the first layer further comprises a modifier selected from the group consisting of La_2O_3 , Pr_6O_{11} , HfO_2 , Y_2O_3 , Yb_2O_3 , YbO , Nd_2O_3 , NdO , WO_3 , SiO_2 , TiO_2 and combinations of two or more thereof.

20

Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the support material of the first layer further comprises a modifier selected from the group consisting of La_2O_3 , Pr_6O_{11} , HfO_2 , Y_2O_3 , Yb_2O_3 , YbO , Nd_2O_3 , NdO , WO_3 , SiO_2 , TiO_2 and combinations of two or more thereof.

25

Most preferably, the support material of the first layer comprises a ceria-zirconia material consisting of CeO_2 : 45 wt%, ZrO_2 : 43.5 wt%, La_2O_3 : 8 wt%, Pr_6O_{11} : 2 wt%, and HfO_2 : 1.5 wt%.

According to the present invention, the support material of the second layer may comprise a metal oxide. Preferably, the support material of the second layer comprises a metal oxide selected from the group consisting of alumina, zirconia, silica, titania, silica-alumina, alumina-zirconia, titania-silica, titania-zirconia, titania-alumina, and combinations of two or more thereof.

35

Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the support material of the second layer comprises a metal oxide selected from the group consisting of alumina, zirconia, silica, titania, silica-alumina, alumina-zirconia, titania-silica, titania-zirconia, titania-alumina, and combinations of two or more thereof.

40

According to the present invention, it is further preferred that the metal oxide of the second layer comprises alumina, more preferably gamma alumina or activated alumina, such as gamma or eta alumina. Preferably, the activated alumina has a specific surface area,

determined according to BET surface area measurements, of from 60 to 300 m²/g, preferably from 90 to 200 m²/g, mostly preferred from 100 to 180 m²/g.

5 It is further preferred that the second layer has a ceria content of not more than 5 weight-%, preferably not more than 1 weight-%, more preferably not more than 0.1 weight-%.

10 Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the second layer has a ceria content of not more than 5 weight-%, preferably not more than 1 weight-%, more preferably not more than 0.1 weight-%.

15 Generally, there are no specific restrictions as far as the palladium content of the first layer is concerned provided that the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer. Preferably, the first layer comprises palladium in an amount of from 6 to 60 g/ft³.

20 Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the first layer comprises palladium in an amount of from 6 to 60 g/ft³.

25 Generally, there are no specific restrictions as far as the platinum content of the first layer is concerned provided that the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer. Preferably, the first layer comprises platinum in an amount of from 15 to 40 g/ft³.

30 Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the first layer comprises platinum in an amount of from 15 to 40 g/ft³.

35 Generally, there are no specific restrictions as far as the total content of platinum and palladium of the second layer is concerned provided that the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer. Preferably, the second layer comprises platinum and palladium in a total amount of from 30 to 180 g/ft³.

40 Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the second layer comprises platinum and palladium in a total amount of from 30 to 180 g/ft³.

45 While there are no specific restrictions as far as the total amount of platinum and palladium of the diesel oxidation catalytic material is concerned provided that the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer, it is preferred that the diesel oxidation catalytic material comprises platinum and palladium in a total amount of from 30 to 240 g/ft³.

Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the diesel oxidation catalytic material comprises platinum and palladium in a total amount of from 30 to 240 g/ft³.

- 5 Preferably, the second layer further comprises a hydrocarbon storage compound, preferably a zeolite. If present, the second layer comprises the hydrocarbon storage compound in a total amount of from 0.1 to 1 g/ft³, preferably of from 0.3 to 0.8 g/ft³, more preferably in an amount of 0.5 g/ft³.
- 10 Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the second layer further comprises a hydrocarbon storage compound, preferably a zeolite.

Typically, any structure types of zeolites/aluminosilicates can be used, such as structure
15 types of ABW, ACO, AEI, AEL, AEN, AET, AFG, AFI, AFN, AFO, AFR, AFS, AFT, AFX, AFY, AHT, ANA, APC, APD, AST, ASV, ATN, ATO, ATS, ATT, ATV, AWO, AWW, BCT, BEA, BEC, BIK, BOG, BPH, BRE, CAN, CAS, SCO, CFI, SGF, CGS, CHA, CHI, CLO, CON, CZP, DAC, DDR, DFO, DFT, DOH, DON, EAB, EDI, EMT, EON, EPI, ERI, ESV, ETR, EUO, FAU, FER, FRA, GIS, GIU, GME, GON, GOO, HEU, IFR, IHW, ISV, ITE, ITH, ITW, IWR, IWW,
20 JBW, KFI, LAU, LEV, LIO, LIT, LOS, LOV, LTA, LTL, LTN, MAR, MAZ, MEI, MEL, MEP, MER, MFI, MFS, MON, MOR, MOZ, MSO, MTF, MTN, MTT, MTW, MWW, NAB, NAT, NES, NON, NPO, NSI, OBW, OFF, OSI, OSO, OWE, PAR, PAU, PHI, PON, RHO, RON, RRO, RSN, RTE, RTH, RUT, RWR, RWY, SAO, SAS, SAT, SAV, SBE, SBS, SBT, SFE, SFF, SFG, SFH, SFN, SFO, SGT, SOD, SOS, SSY, STF, STI, STT, TER, THO, TON, TSC, UEI,
25 UFI, UOZ, USI, UTL, VET, VFI, VNI, VSV, WIE, WEN, YUG, ZON or a mixture of one or more thereof.

The zeolite can be a natural or synthetic zeolite such as faujasite, chabazite, clinoptilolite, mordenite, silicalite, zeolite X, zeolite Y, ultrastable zeolite Y, ZSM-5 zeolite, ZSM-12 zeolite,
30 SSZ-3 zeolite, SAPO 5 zeolite, offretite, or a beta zeolite. Preferred zeolite materials have a high silica to alumina ratio. The zeolites may have a silica:alumina molar ratio of from at least 25:1, preferably at least 50:1, with useful ranges of from 25:1 to 1000:1, 50:1 to 500:1 as well as 25:1 to 300:1, from 100:1 to 250:1, or alternatively from 35:1 to 180:1 is also exemplified. Preferred zeolites include ZSM, Y and beta zeolites. A particularly preferred beta zeolite is of
35 the type disclosed in US 6,171,556. The zeolite can be present in its H-Form and/or its Na-Form. Further, the zeolite can be metal-doped.

It is further preferred that the diesel oxidation catalyst further comprises an undercoat layer located between the carrier substrate and the first layer, the undercoat layer preferably
40 comprising alumina, more preferably gamma-alumina.

Therefore, the present invention relates to the diesel oxidation catalyst as defined above further comprising an undercoat layer located between the carrier substrate and the first layer, the undercoat layer preferably comprising alumina, more preferably gamma-alumina.

- 5 According to the present invention, the carrier substrate may be a flow-through substrate or a wall flow substrate.

Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the carrier substrate is a flow-through substrate or a wall flow substrate.

10

Wall flow substrates useful for the diesel oxidation catalysts of the present invention have a plurality of fine, substantially parallel flow passages extending along the longitudinal axis of the substrate. Each passage is blocked at one end of the substrate body, with alternate passages blocked at opposite end-faces. Such monolithic carriers may contain up to about
15 400 flow passages (or "cells") per square inch ((2.54 cm)²) of cross section, although far fewer may be used. For example, the carrier may have from 7 to 400, preferably from 100 to 400, cells per square inch ("cps"). The cells can have cross sections that are rectangular, square, circular, oval, triangular, hexagonal, or are of other polygonal shapes.

- 20 Preferred wall flow substrates are composed of ceramic-like materials such as cordierite, alpha-alumina, silicon carbide, silicon nitride, zirconia, mullite, spodumene, alumina-silica-magnesia or zirconium silicate, or of refractory metals such as stainless steel. Preferred wall flow substrates are formed from cordierite and silicon carbide. Such materials are able to withstand the environment, particularly high temperatures, encountered in treating the
25 exhaust streams. Ceramic wall flow substrates are typically formed of a material having a porosity of about 40 to 70. The term "porosity" as used in this context is understood as being determined according to mercury porosity measurement according to DIN 66133. According to the present invention, wall flow substrates are preferred having a porosity in the range from 38 to 75.

30

It is further preferred that the carrier substrate comprises a material selected from the group consisting of cordierite, cordierite-alumina, silicon nitride, silicon carbide, zircon mullite, spodumene, alumina-silica magnesia, zircon silicate, sillimanite, magnesium silicate, zircon, petalite, alumina, aluminosilicate and combinations of two or more thereof.

35

Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the carrier substrate comprises a material selected from the group consisting of cordierite, cordierite-alumina, silicon nitride, silicon carbide, zircon mullite, spodumene, alumina-silica magnesia, zircon silicate, sillimanite, magnesium silicate, zircon, petalite,
40 alumina, aluminosilicate and combinations of two or more thereof.

Generally, there are no specific restrictions as far as the number of layers of the layered diesel oxidation catalyst is concerned. With the proviso that the diesel oxidation catalytic material comprises at least

- 5 b1) a first layer located on the carrier substrate, the first layer comprising palladium impregnated on a support material comprising ceria in an amount of at least 45 weight-% based on the total weight of the support material, and optionally comprising platinum; and
- b2) a second layer located on the first layer, the second layer comprising palladium and platinum each impregnated on a support material comprising a metal oxide;
- 10 wherein the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer, the number of layers of the layered diesel oxidation catalyst can be varied. Preferably, the layered diesel oxidation catalyst further comprises
- b3) a third layer located on the second layer, the third layer comprising palladium impregnated on a support material comprising ceria in an amount of at least 45 weight-%
- 15 based on the total weight of the support material, and optionally comprising platinum, wherein the platinum to palladium weight ratio of the third layer is lower than the platinum to palladium weight ratio of the second layer.

Therefore, the present invention relates to the diesel oxidation catalyst as defined above, further comprising

20

- b3) a third layer located on the second layer, the third layer comprising palladium impregnated on a support material comprising ceria in an amount of at least 45 weight-% based on the total weight of the support material, and optionally comprising platinum, wherein the platinum to palladium weight ratio of the third layer is lower than the platinum to
- 25 palladium weight ratio of the second layer.

According to the present invention, if a third layer is present, the platinum to palladium weight ratio of the third layer is lower than the platinum to palladium weight ratio of the second layer. Preferably, the ratio of the platinum to palladium weight ratio of the third layer to the platinum to

30 palladium weight ratio of the second layer is lower than or equal to 0.9.

Therefore, the present invention also relates to the diesel oxidation catalyst as defined above, wherein the ratio of the platinum to palladium weight ratio of the third layer to the platinum to palladium weight ratio of the second layer is lower than or equal to 0.9.

35

According to the present invention, if a third layer is present, the third layer comprises palladium impregnated on a support material comprising ceria in an amount of at least 45 weight-% based on the total weight of the support material. Preferably, the support material of the third layer comprises ceria in an amount of at least 65 weight-%, more preferably at

40 least 85 weight-%, most preferably at least 95 weight-% based on the total weight of the support material.

Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the support material of the third layer comprises ceria in an amount of at least 65 weight-%, preferably at least 85 weight-%, more preferably at least 95 weight-% based on the total weight of the support material.

5

Preferably, the support material of the third layer further comprises zirconia and/or alumina.

Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the support material of the third layer further comprises zirconia and/or alumina.

10

Preferably, the support material of the third layer further comprises a modifier selected from the group consisting of La_2O_3 , Pr_6O_{11} , HfO_2 , Y_2O_3 , Yb_2O_3 , YbO , Nd_2O_3 , NdO , WO_3 , SiO_2 , TiO_2 and combinations of two or more thereof.

15

Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the support material of the third layer further comprises a modifier selected from the group consisting of La_2O_3 , Pr_6O_{11} , HfO_2 , Y_2O_3 , Yb_2O_3 , YbO , Nd_2O_3 , NdO , WO_3 , SiO_2 , TiO_2 and combinations of two or more thereof.

20

Most preferably, the support material of the third layer comprises a ceria-zirconia material consisting of CeO_2 : 45 wt%, ZrO_2 : 43.5 wt%, La_2O_3 : 8 wt%, Pr_6O_{11} : 2 wt%, and HfO_2 : 1.5 wt%.

25

Generally, there are no specific restrictions as far as the palladium content of the third layer is concerned provided that the platinum to palladium weight ratio of the third layer is lower than the platinum to palladium weight ratio of the second layer. Preferably, the third layer comprises palladium in an amount of from 2 to 30 g/ft³.

30

Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the third layer comprises palladium in an amount of from 2 to 30 g/ft³.

35

Generally, there are no specific restrictions as far as the platinum content of the third layer is concerned provided that the platinum to palladium weight ratio of the third layer is lower than the platinum to palladium weight ratio of the second layer. Preferably, the third layer comprises platinum in an amount of from 4 to 16 g/ft³.

40

Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the third layer comprises platinum in an amount of from 4 to 16 g/ft³.

40

Preferably, the third layer further comprises a hydrocarbon storage compound, preferably a zeolite. If present, the third layer comprises the hydrocarbon storage compound in a total amount of from 0.1 to 1 g/ft³, preferably of from 0.3 to 0.8 g/ft³, more preferably in an amount of 0.5 g/ft³.

Therefore, the present invention relates to the diesel oxidation catalyst as defined above, wherein the third layer further comprises a hydrocarbon storage compound, preferably a zeolite.

5

Typically, any structure types of zeolites/aluminosilicates can be used. In this respect, reference is made to the structure types mentioned for the second layer.

10

The layered diesel oxidation catalyst of the present invention can be used in an integrated system for treating a gaseous exhaust stream of a diesel engine.

Therefore, the present invention also relates to the layered diesel oxidation catalyst as defined above comprised in a system for treating of a gaseous exhaust stream of a diesel engine, the system further comprising:

15

an exhaust conduit in fluid communication with the diesel engine via an exhaust manifold, and

one or more of the following in fluid communication with the layered diesel oxidation catalyst composite: a catalyzed soot filter (CSF), a selective catalytic reduction (SCR) article, a NOx storage and reduction (NSR) catalytic article.

20

Each of the layers of the diesel catalytic material according to the present invention is formed from a washcoat composition that contains the respective support material as described above. Other additives such as binders and stabilizers can also be included in the washcoat composition. As disclosed in United States Patent No. 4,727,052, porous support materials, such as activated alumina, can be thermally stabilized to retard undesirable alumina phase transformations from gamma to alpha at elevated temperatures. Stabilizers can be selected from at alkaline earth metal components selected from the group consisting of magnesium, barium, calcium and strontium, preferably strontium and barium. When present, stabilizer materials are added at from about 0.01 g/in³ (g/(2.54 cm)³) to 0.15 g/in³ (g/(2.54 cm)³) in the coating.

30

The first layer is disposed on the surface of the carrier substrate or the undercoat layer. The second layer is disposed on the first layer which had been applied onto the surface of carrier substrate or the undercoat layer. Further, it is conceivable that a third layer is disposed on the second layer. It is to be understood that a given layer may partially permeate the substrate or the layer onto which it is applied.

35

For the preparation of the washcoat compositions mentioned above, it is preferred to disperse a suitable Pt and/or Pd component precursor on a suitable support material as described hereinabove. More preferably, a water-soluble or water-dispersible Pt and/or Pd component precursor is/are impregnated on a suitable support material, followed by drying and fixing steps. Suitable Pt and/or Pd component precursors include, for example, potassium platinum chloride, ammonium platinum thiocyanate, amine-solubilized platinum

40

hydroxide, chloroplatinic acid, palladium nitrate, and the like. Other suitable precursors will be apparent to those of skill in the art. The impregnated support material is preferably dried with the Pt and/or Pd component fixed thereon. Generally, drying temperatures are in the range from 60 to 250 °C, preferably from 90 to 210 °C, more preferably from 100 to 150°C.

5 Drying can be carried out in any suitable atmosphere, with N₂ or air being preferred. After drying, it is preferred to finally fix the Pt and/or Pd component on the support material by suitable calcination and/or other suitable methods such as treatment with acetic acid. In general, any method resulting in the Pt and/or Pd component being in water-insoluble form is suitable. Generally, calcination temperatures are in the range from 250 to 800 °C, preferably

10 from 350 to 700 °C, more preferably from 400 to 600 °C. Calcination can be carried out in any suitable atmosphere, with N₂ or air being preferred. By, for example, calcination, the catalytically active elemental Pt and/or Pd or the respective oxide is obtained. It is to be understood that the term "platinum" or "palladium" present in the finally obtained layered diesel oxidation catalyst as used in the context of the present invention relates to the Pt

15 and/or Pd component in the form of the catalytically active elemental Pt and/or Pd, or the oxide thereof, or the mixture of elemental Pt and/or Pd and the oxide thereof.

Therefore, the present invention also relates to a process for the preparation of the layered diesel oxidation catalyst as defined above, comprising the steps of

20 (i) providing a carrier substrate;

(ii) optionally applying an undercoat layer on the carrier substrate;

(iii) applying a first layer on the carrier substrate or the undercoat layer, the first layer comprising palladium impregnated on a support material comprising ceria in an amount of at least 45 weight-% based on the total weight of the support material, and optionally

25 comprising platinum;

(iv) applying a second layer on the first layer, the second layer comprising palladium and platinum each impregnated on a support material comprising a metal oxide, wherein the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer;

30 (v) optionally applying a third layer on the second layer, the third layer comprising palladium impregnated on a support material comprising ceria in an amount of at least 45 weight-% based on the total weight of the support material, and optionally comprising platinum,

wherein the platinum to palladium weight ratio of the third layer is lower than the platinum to

35 palladium weight ratio of the second layer.

Further, the present invention relates to a system for treating of a gaseous exhaust stream of a diesel engine, the system comprising:

an exhaust conduit in fluid communication with the diesel engine via an exhaust manifold,

40 the layered diesel oxidation catalyst as described above, wherein the carrier substrate is a wall-flow substrate or a flow through substrate, and

one or more of the following in fluid communication with the layered diesel oxidation catalyst composite: a catalyzed soot filter (CSF), a selective catalytic reduction (SCR) article, a NOx storage and reduction (NSR) catalytic article.

- 5 Preferably, in this system, if present, the layered diesel oxidation catalyst is located upstream of the catalyzed soot filter.

Therefore, the present invention relates to a system for treating a gaseous exhaust stream of a diesel engine as defined above comprising a catalyzed soot filter, wherein the layered
10 diesel oxidation catalyst is located upstream of the catalyzed soot filter.

A suitable SCR article for use in the exhaust conduit is typically able to catalyze the reaction of O₂ with any excess NH₃ to N₂ and H₂O, so that NH₃ is not emitted to the atmosphere. Suitable SCR articles are described, for instance, in US 4,961,917 and US 5,516,497.
15 Suitable SCR articles include one or both of an iron and a copper promoter typically present in a zeolite in an amount of from about 0.1 to 30 percent by weight, preferably from about 1 to 5 percent by weight, of the total weight of promoter plus zeolite. Typical zeolites may exhibit a CHA framework structure.

20 Finally, the present invention relates to a method of treating a gaseous exhaust stream of a diesel engine, said method comprising contacting the exhaust stream with the layered diesel oxidation catalyst as defined above.

In the following, the present invention is further illustrated by the following examples.
25

Examples

1. Catalyst preparation

30 Sample A) according to the invention

For the 1st (bottom) layer a Palladium nitrate solution was added to 0.75 g/in³ high porous gamma-alumina resulting in 22 g/ft³ Pd. The resulting frit was dispersed in water and acetic acid and milled to a particle size d₉₀ of 25 micrometer. Into this slurry 0.75 g/in³ of a material
35 consisting of ZrO₂: 43.5 wt%, CeO₂: 45 wt%, La₂O₃: 8 wt%, Pr₆O₁₁: 2 wt%, and HfO₂: 1.5% was dispersed and milled to a particle size d₉₀ of 7 micrometer. The final slurry was coated onto a monolith, dried at 110°C in air and calcined at 450°C in air.

40 For the 2nd (middle) layer 1.5 g/in³ of high porous gamma-alumina was impregnated with an aqueous solution of Palladium nitrate giving a final dry Pd content of 30 g/ft³. The resulting powder was dispersed in water. Platinum solution with Platinum as an ammine stabilized hydroxo Pt IV complex was added to give a dry Pt content of 60 g/ft³. After adjusting the pH

of the slurry to 4.5 the slurry was milled to a particle size d_{90} of 16 μ m. The slurry was subsequently coated onto the 1st layer, dried at 110°C in air and calcined at 450°C in air.

5 For the 3rd (top) layer 0.25g/in³ of high porous gamma-alumina and 0.5 g/in³ of a material consisting of ZrO₂: 43.5 wt%, CeO₂: 45 wt%, La₂O₃: 8 wt%, Pr₆O₁₁: 2 wt%, and HfO₂: 1.5% were mixed and impregnated with an aqueous solution of Palladium nitrate giving a final dry Pd content of 8 g/ft³. Subsequently the impregnated material was dispersed in water and acetic acid and milled to a particle size d_{90} of 20 micrometer. 0.5g/in³ H-beta zeolite was immersed in water to a solid content of 45%. The precious metal containing slurry was mixed
10 with the H-beta zeolite containing slurry, milled to a particle size d_{90} of 15 μ m and subsequently coated onto the 2nd layer, dried at 110°C in air and calcined at 450°C in air.

Sample B) according to the invention

15 For the 1st (bottom) layer a Palladium nitrate solution was added to a mixture of high porous gamma-alumina (0.75 g/in³) and 100% Ceria material (0.75 g/in³) resulting in 36 g/ft³ Pd. The resulting frit was dispersed in water and acetic acid and milled to a particle size d_{90} of 7 micrometer. The final slurry was coated onto a monolith, dried at 110°C in air and calcined at 450°C in air.

20 For the 2nd (middle) layer 1.5 g/in³ of high porous gamma-alumina was impregnated with an aqueous solution of Palladium nitrate giving a final dry Pd content of 26 g/ft³. The resulting powder was dispersed in water. Platinum solution with Platinum as an ammine stabilized hydroxo Pt IV complex was added to give a dry Pt content of 52 g/ft³. After adjusting the pH
25 of the slurry to 4.5 the slurry was milled to a particle size d_{90} of 16 μ m. The slurry was subsequently coated onto the 1st layer, dried at 110°C in air and calcined at 450°C in air.

30 For the 3rd (top) layer high porous gamma-alumina (0.25g/in³) and 100% Ceria material (0.5 g/in³) were mixed and impregnated with an aqueous solution of Palladium nitrate giving a final dry Pd content of 8 g/ft³. Subsequently the impregnated material was dispersed in water and acetic acid and milled to a particle size d_{90} of 20 micrometer. 0.5g/in³ H-beta zeolite was immersed in water to a solid content of 45%. The precious metal containing slurry was mixed with the H-beta zeolite containing slurry, milled to a particle size d_{90} of 15 μ m and subsequently coated onto the 2nd layer, dried at 110°C in air and calcined at 450°C in air.

35

Sample C) according to the invention

40 For the 1st (bottom) layer a Palladium nitrate solution was added to a mixture of high porous gamma-alumina (0.75 g/in³) and 100% Ceria material (0.75 g/in³) resulting in 30 g/ft³ Pd. The resulting frit was dispersed in water and acetic acid and milled to a particle size d_{90} of 7 micrometer. The final slurry was coated onto a monolith, dried at 110°C in air and calcined at 450°C in air.

For the 2nd (top) layer 1 g/in³ of high porous gamma-alumina was impregnated with an aqueous solution of Palladium nitrate giving a final dry Pd content of 30 g/ft³. The resulting powder was dispersed in water. Platinum solution with Platinum as an ammine stabilized hydroxo Pt IV complex was added to give a dry Pt content of 60 g/ft³. After adjusting the pH of the slurry to 4.5 the slurry was milled to a particle size d₉₀ of 16µm. H-beta zeolite was immersed in water to a solid content of 45%. The precious metal containing slurry was then mixed with the H-beta zeolite containing slurry, milled to a particle size d₉₀ of 15µm and subsequently coated onto the 1st layer, dried at 110°C in air and calcined at 450°C in air.

10 **Sample D) not according to the invention**

For the 1st (bottom) layer a Palladium nitrate solution was added to 0.75 g/in³ high porous gamma-alumina resulting in 22 g/ft³ Pd. The resulting frit was dispersed in water and acetic acid and milled to a particle size d₉₀ of 25 micrometer. Into this slurry 0.75 g/in³ high porous gamma-alumina was dispersed and milled to a particle size d₉₀ of 7 micrometer. The final slurry was coated onto a monolith, dried at 110°C in air and calcined at 450°C in air.

For the 2nd (middle) layer 1.5 g/in³ of high porous gamma-alumina was impregnated with an aqueous solution of Palladium nitrate giving a final dry Pd content of 30 g/ft³. The resulting powder was dispersed in water. Platinum solution with Platinum as an ammine stabilized hydroxo Pt IV complex was added to give a dry Pt content of 60 g/ft³. After adjusting the pH of the slurry to 4.5 the slurry was milled to a particle size d₉₀ of 16µm. The slurry was subsequently coated onto the 1st layer, dried at 110°C in air and calcined at 450°C in air.

For the 3rd (top) layer 0.75 g/in³ high porous gamma-alumina was impregnated with an aqueous solution of Palladium nitrate giving a final dry Pd content of 8 g/ft³. Subsequently the impregnated material was dispersed in water and acetic acid and milled to a particle size d₉₀ of 20 micrometer. 0.5g/in³ H-beta zeolite was immersed in water to a solid content of 45%. The precious metal containing slurry was mixed with the H-beta zeolite containing slurry, milled to a particle size d₉₀ of 15µm and subsequently coated onto the 2nd layer, dried at 110°C in air and calcined at 450°C in air.

Sample E) not according to the invention

For the 1st (bottom) layer 1g/in³ high porous gamma-alumina was dispersed in water and acetic acid and milled to a particle size d₉₀ of 15 micrometer. The final slurry was coated onto a monolith, dried at 110°C in air and calcined at 450°C in air.

For the 2nd (middle) layer 1.5 g/in³ high porous gamma-alumina was impregnated with an aqueous solution of Palladium nitrate giving a final dry Pd content of 28g/ft³. The resulting powder was dispersed in water. Platinum solution with Platinum as an ammine stabilized hydroxo Pt IV complex was added to give a dry Pt content of 52 g/ft³. After adjusting the pH

of the slurry to 4.5 the slurry was milled to a particle size d_{90} of 16 μ m. The slurry was subsequently coated onto the 1st layer, dried at 110°C in air and calcined at 450°C in air.

5 For the 3rd (top) layer 0.25g/in³ high porous gamma-alumina was dispersed in water and acetic acid and milled to a particle size d_{90} of 20 micrometer. 0.5g/in³ H-beta zeolite was immersed in water to a solid content of 45%. To this slurry a platinum precursor solution with platinum as an ammine stabilized hydroxo Pt IV complex was added to give a Pt content of 8g/ft³. The precious metal containing slurry was mixed with the alumina containing slurry, milled to a particle size d_{90} of 15 μ m and subsequently coated onto the 2nd layer, dried at
10 110°C in air and calcined at 450°C in air.

2. Testing of HC/CO Gas Activity Performance

Sample A) according to the invention

15 1st Layer: 22 g/ft³ Pd, 0.75 g/in³ (ZrO₂: 43.5 wt%, CeO₂: 45 wt%, La₂O₃: 8 wt%, Pr₆O₁₁: 2 wt%, and HfO₂: 1.5%), 0.75 g/in³ high porous gamma-alumina
2nd Layer: 60 g/ft³ Pt, 30 g/ft³ Pd, 1.5 g/in³ high porous gamma-alumina
3rd Layer: 8 g/ft³ Pd, 0.25 g/in³ high porous gamma-alumina, 0.5 g/in³ H-Beta zeolite, 0.5 g/in³ (ZrO₂: 43.5 wt%, CeO₂: 45 wt%, La₂O₃: 8 wt%, Pr₆O₁₁: 2 wt%, and HfO₂: 1.5%)
20

Sample B) according to the invention

1st Layer: 36 g/ft³ Pd, 0.75 g/in³ Ceria, 0.75 g/in³ high porous gamma-alumina
2nd Layer: 52 g/ft³ Pt, 26 g/ft³ Pd, 1.5 g/in³ high porous gamma-alumina
3rd Layer: 16/ft³ Pd, 0.25 g/in³ high porous gamma-alumina, 0.5 g/in³ H-Beta zeolite, 0.5 g/in³
25 100% Ceria

Sample C) according to the invention

1st Layer: 36 g/ft³ Pd, 0.75 g/in³ Ceria, 0.75 g/in³ high porous gamma-alumina
2nd Layer: 60 g/ft³ Pt, 30 g/ft³ Pd, 1 g/in³ high porous gamma-alumina 0.5 g/in³ H-Beta zeolite
30

Sample D) not according to the invention

1st Layer: 22 g/ft³ Pd, 1.5 g/in³ high porous gamma-alumina
2nd Layer: 60 g/ft³ Pt, 30 g/ft³ Pd, 1.5 g/in³ high porous gamma-alumina
3rd Layer: 8 g/ft³ Pd, 0.75 g/in³ high porous gamma-alumina, 0.5 g/in³ H-Beta zeolite
35

Sample E) not according to the invention

1st Layer: 1 g/in³ high porous gamma-alumina
2nd Layer: 72 g/ft³ Pt, 40 g/ft³ Pd, 1.5 g/in³ high porous gamma-alumina
3rd Layer: 8 g/ft³ Pt, 0.25 g/in³ high porous gamma-alumina, 0.5 g/in³ H-Beta zeolite
40

3. Light-Off Performance Testing

Samples A), B), C), D) and E) were tested for CO and HC light-off performance. Prior to testing the samples were aged in the exhaust stream of a 4 cylinder light duty diesel engine with 2.7L engine displacement for 25h. The temperature of the exhaust stream was raised by an upstream burner DOC to 750°C steady state.

5

For light-off testing each sample was placed downstream in the exhaust line of a 6 cylinder light duty diesel engine with a 3 L engine displacement. The CO and HC concentration in the exhaust stream was constant at 1500 ppm and 300 ppm (C₃ basis), respectively. The gas flow under standard conditions was around 60 m³/h. The temperature ramp was 40°C/min.

10

A lower light-off temperature characterizes a better gas activity.

As can be taken from Figure 1 showing the CO light-off curves for Samples A), B), C), D) and E), Samples A), B) and C) according to the invention show higher CO conversion at lower temperatures compared to Samples D) and E) not according to the invention.

15

As can be taken from Figure 2 showing the HC light-off curves for Samples A), B), C), D) and E), Samples A) and B) according to the invention show higher HC conversion at lower temperatures compared to Samples D) and E) not according to the invention. Sample C) according to the invention shows a lower light-off temperature at around 70% HC conversion compared to Samples D) and E) not according to the invention.

20

As can be taken from Figure 3 showing the HC and CO light-off temperatures for Samples A), B), C), D) and E), precious metal cost reduced Samples A), B), and C) according to the invention show lower light-off temperatures at 50 % CO conversion and 70% HC conversion compared to Samples D) and E) not according to the invention.

25

CLAIMS:

1. A layered diesel oxidation catalyst (DOC) comprising:
 - a) a carrier substrate;
 - b) a diesel oxidation catalytic material comprising
 - b1) a first layer located on the carrier substrate, the first layer comprising palladium impregnated on a support material comprising ceria in an amount of at least 65 weight-% based on the total weight of the support material, and optionally comprising platinum;
 - b2) a second layer located on the first layer, the second layer comprising palladium and platinum each impregnated on a support material comprising a metal oxide;wherein the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer.
2. The layered diesel oxidation catalyst according to claim 1, wherein the platinum to palladium weight ratio of the first layer is in the range of from 0:1 to 1.1:1.
3. The layered diesel oxidation catalyst according to claim 1 or 2, wherein the platinum to palladium weight ratio of the second layer is in the range of from 10:1 to 1.1:1.
4. The layered diesel oxidation catalyst according to any one of claims 1 to 3, wherein the ratio of the platinum to palladium weight ratio of the first layer to the platinum to palladium weight ratio of the second layer is lower than or equal to 0.9.
5. The layered diesel oxidation catalyst according to any one of claims 1 to 4, wherein the support material of the first layer comprises ceria in an amount of at least 85 weight-% based on the total weight of the support material.
6. The layered diesel oxidation catalyst according to any one of claims 1 to 5, wherein the support material of the first layer further comprises zirconia and/or alumina.

7. The layered diesel oxidation catalyst according to any one of claims 1 to 6, wherein the support material of the first layer further comprises a modifier selected from the group consisting of La_2O_3 , Pr_6O_{11} , HfO_2 , Y_2O_3 , Yb_2O_3 , YbO , Nd_2O_3 , NdO , WO_3 , SiO_2 , TiO_2 and combinations of two or more thereof.
8. The layered diesel oxidation catalyst according to any one of claims 1 to 7, wherein the support material of the second layer comprises a metal oxide selected from the group consisting of alumina, zirconia, silica, titania, silica-alumina, alumina-zirconia, titania-silica, titania-zirconia, titania-alumina, and combinations of two or more thereof.
9. The layered diesel oxidation catalyst according to any one of claims 1 to 8, wherein the second layer has a ceria content of not more than 5 weight-%.
10. The layered diesel oxidation catalyst according to any one of claims 1 to 9, wherein the first layer comprises palladium in an amount of from 6 to 60 g/ft³.
11. The layered diesel oxidation catalyst according to any one of claims 1 to 10, wherein the first layer comprises platinum in an amount of from 15 to 40 g/ft³.
12. The layered diesel oxidation catalyst according to any one of claims 1 to 11, wherein the second layer comprises platinum and palladium in a total amount of from 30 to 180 g/ft³.
13. The layered diesel oxidation catalyst according to any one of claims 1 to 12, wherein the diesel oxidation catalytic material comprises platinum and palladium in a total amount of from 30 to 240 g/ft³.
14. The layered diesel oxidation catalyst according to any one of claims 1 to 13, wherein the second layer further comprises a hydrocarbon storage compound.

15. The layered diesel oxidation catalyst according to any one of claims 1 to 14, further comprising an undercoat layer located between the carrier substrate and the first layer.
16. The layered diesel oxidation catalyst according to claim 15, wherein the undercoat layer comprises alumina.
17. The layered diesel oxidation catalyst according to any one of claims 1 to 16, wherein the carrier substrate is a flow-through substrate or a wall flow substrate.
18. The layered diesel oxidation catalyst according to any one of claims 1 to 17, wherein the carrier substrate comprises a material selected from the group consisting of cordierite, cordierite-alumina, silicon nitride, silicon carbide, zircon mullite, spodumene, alumina-silica magnesia, zircon silicate, sillimanite, magnesium silicate, zircon, petalite, alumina, aluminosilicate and combinations of two or more thereof.
19. The layered diesel oxidation catalyst according to any one of claims 1 to 18, further comprising
 - b3) a third layer located on the second layer, the third layer comprising palladium impregnated on a support material comprising ceria in an amount of at least 45 weight-% based on the total weight of the support material, and optionally comprising platinum,wherein the platinum to palladium weight ratio of the third layer is lower than the platinum to palladium weight ratio of the second layer.
20. The layered diesel oxidation catalyst according to claim 19, wherein the ratio of the platinum to palladium weight ratio of the third layer to the platinum to palladium weight ratio of the second layer is lower than or equal to 0.9.

21. The layered diesel oxidation catalyst according to claim 19 or 20, wherein the support material of the third layer comprises ceria in an amount of at least 65 weight-% based on the total weight of the support material.
22. The layered diesel oxidation catalyst according to any one of claims 19 to 21, wherein the support material of the third layer further comprises zirconia and/or alumina.
23. The layered diesel oxidation catalyst according to any one of claims 19 to 22, wherein the support material of the third layer further comprises a modifier selected from the group consisting of La_2O_3 , Pr_6O_{11} , HfO_2 , Y_2O_3 , Yb_2O_3 , YbO , Nd_2O_3 , NdO , WO_3 , SiO_2 , TiO_2 and combinations of two or more thereof.
24. The layered diesel oxidation catalyst according to any one of claims 19 to 23, wherein the third layer comprises palladium in an amount of from 2 to 30 g/ft³.
25. The layered diesel oxidation catalyst according to any one of claims 19 to 24, wherein the third layer comprises platinum in an amount of from 4 to 16 g/ft³.
26. The layered diesel oxidation catalyst according to any one of claims 19 to 25, wherein the third layer further comprises a hydrocarbon storage compound.
27. The layered diesel oxidation catalyst according to any one of claims 1 to 26 comprised in a system for treating of a gaseous exhaust stream of a diesel engine, the system further comprising:
 - an exhaust conduit in fluid communication with the diesel engine via an exhaust manifold, and
 - one or more of the following in fluid communication with the layered diesel oxidation catalyst composite: a catalyzed soot filter (CSF), a selective catalytic reduction (SCR) article, and a NO_x storage and reduction (NSR) catalytic article.
28. A process for the preparation of the layered diesel oxidation catalyst according to any one of claims 1 to 26, comprising the steps of

- (i) providing a carrier substrate;
 - (ii) optionally applying an undercoat layer on the carrier substrate;
 - (iii) applying a first layer on the carrier substrate or the undercoat layer, the first layer comprising palladium impregnated on a support material comprising ceria in an amount of at least 65 weight-% based on the total weight of the support material, and optionally comprising platinum;
 - (iv) applying a second layer on the first layer, the second layer comprising palladium and platinum each impregnated on a support material comprising a metal oxide, wherein the platinum to palladium weight ratio of the first layer is lower than the platinum to palladium weight ratio of the second layer;
 - (v) optionally applying a third layer on the second layer, the third layer comprising palladium impregnated on a support material comprising ceria in an amount of at least 45 weight-% based on the total weight of the support material, and optionally comprising platinum, wherein the platinum to palladium weight ratio of the third layer is lower than the platinum to palladium weight ratio of the second layer.
29. A system for treating a gaseous exhaust stream of a diesel engine, the system comprising:
an exhaust conduit in fluid communication with the diesel engine via an exhaust manifold,
the layered diesel oxidation catalyst according to any one of claims 1 to 26, wherein the carrier substrate is a wall-flow substrate or a flow through substrate, and one or more of the following in fluid communication with the layered diesel oxidation catalyst composite: a catalyzed soot filter (CSF), a selective catalytic reduction (SCR) article, and a NO_x storage and reduction (NSR) catalytic article.
30. The system according to claim 29, comprising a catalyzed soot filter, wherein the layered diesel oxidation catalyst is located upstream of the catalyzed soot filter.
31. Use of the layered diesel oxidation catalyst according to any one of claims 1 to 26, for treating a gaseous exhaust stream of a diesel engine.

Fig. 1:

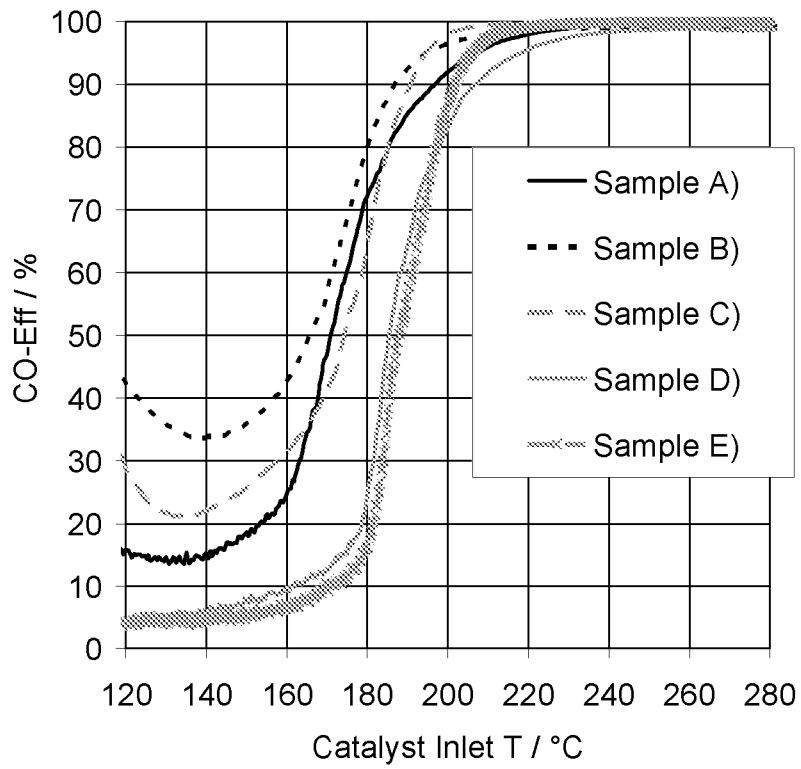


Fig. 2:

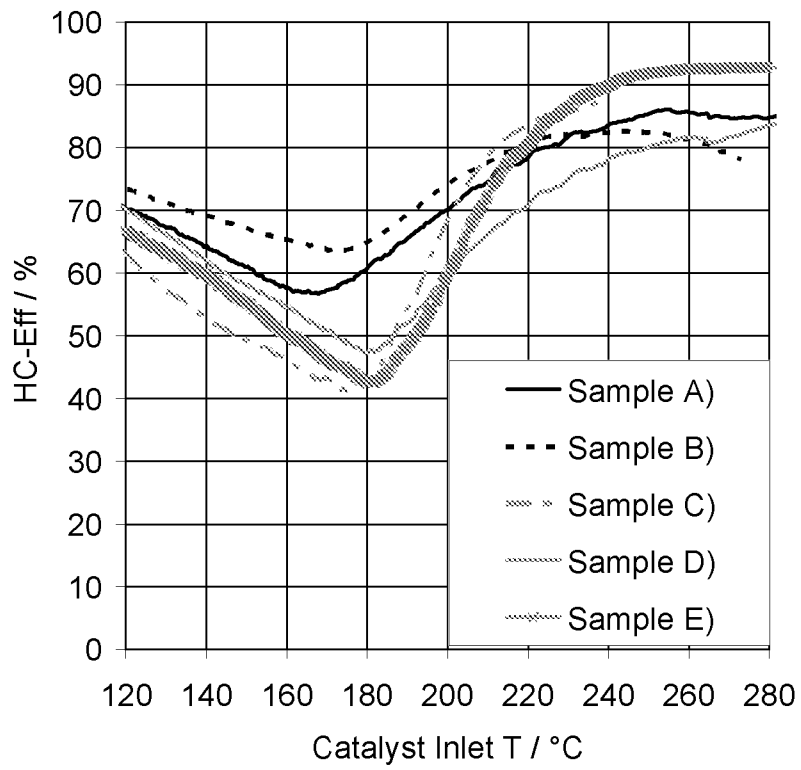


Fig. 3:

