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- (71) **Applicant:** KONINKLIJKE PHILIPS N.V. [NL/NL];
High Tech Campus 5, NL-5656 AE Eindhoven (NL).
- (72) **Inventors:** O'NEILL, Francis, Patrick; c/o High Tech
Campus, Building 5, NL-5656 AE Eindhoven (NL). REY,
Eduardo, Mario; c/o High Tech Campus, Building 5, NL-
5656 AE Eindhoven (NL). NELSON, Mark, Deems; c/o
High Tech Campus, Building 5, NL-5656 AE Eindhoven
(NL).
- (74) **Agents:** STEFFEN, Thomas et al.; High Tech Campus,
Building 5, NL-5656 AE Eindhoven (NL).

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[Continued on next page]

(54) **Title:** MAGNETIC RESONANCE SAFE ELECTRODE FOR BIOPOTENTIAL MEASUREMENTS

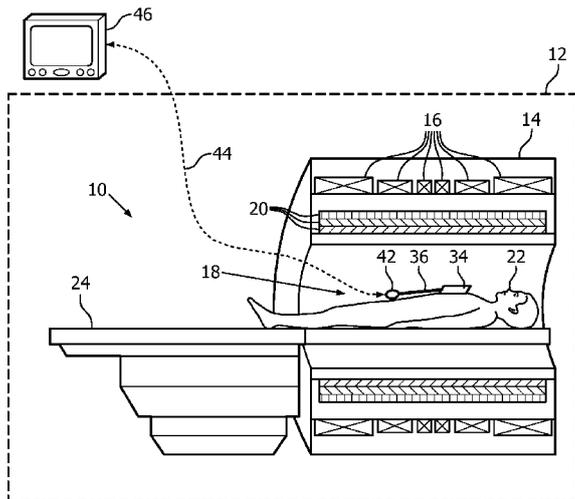


FIG. 1

(57) **Abstract:** An electrode patch (34) for use in biopotential measurements in a magnetic resonance (MR) environment includes: a plastic or polymer sheet (32); an electrically conductive trace (58) disposed on the plastic or polymer sheet, the electrically conductive trace having sheet resistance of one ohm/square or higher; and an electrode (30) disposed on the electrically conductive trace and configured for attachment to human skin. In some embodiments the electrically conductive trace is a carbon-based electrically conductive trace. The electrode may comprise a silver or other electrically conductive layer disposed on the electrically conductive trace and an electrolyte layer or other adhesive layer, such as a silver chloride-based electrolyte layer, disposed on the silver or other electrically conductive layer.



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MAGNETIC RESONANCE SAFE ELECTRODE FOR BIOPOTENTIAL MEASUREMENTS

DESCRIPTION

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The following relates to the sensor arts, measurement arts, magnetic resonance arts, safety arts, biopotential measurement arts including electrocardiography (ECG), electromyography (EMG), electroencephalography (EEG) electroretinography (ERG), and so forth, gated MR imaging arts employing cardiac gating or the like, and so forth.

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In conventional biopotential measurements such as electrocardiograph (ECG), electroencephalograph (EEG), and similar measurements, electrical potentials are measured by electrodes placed on the skin. Conventionally, cabling with high electrical conductivity, e.g. using copper wires, is employed to connect the electrodes with the monitoring electronics.

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When biopotential measurements are performed while the subject is disposed in a magnetic resonance (MR) scanner, the conventional high conductivity cabling is replaced by high resistance cabling. This is in deference to numerous problems that can arise in placing high conductivity cabling in the MR environment, including problems such as heating caused by RF pulses and/or magnetic field gradients, radio frequency interference issues, and so forth. Use of ECG or other biopotential measurement instruments in an MR setting has numerous applications. For example, ECG signals can be used to monitor the condition of the patient, and/or can be used to trigger or gate certain events such as imaging data acquisition. Cardiac gating performed in this way can reduce motion artifacts due to the beating heart.

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In the MR room due to the RF heating effects and burn hazards associated with the MRI environment, a distributed or discrete high-resistance cable is used to connect the electrode to the MRI patient monitor with ECG functionality. These high resistance cables are expensive and can still be susceptible to heating and consequent risk of burns to the patient. They are cumbersome to manufacture, can suffer from inductive pickup, are susceptible to triboelectric effects, can suffer from parasitic capacitance, and are sensitive

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to patient movement. Routing of discrete lead wires can lead to inconsistency and inaccuracies in ECG performance.

Radio frequency (RF) fields produced by the MR scanner can generate currents in the cable, or “hot-spots” that may increase surface temperatures enough to exceed those allowed by regulatory standards and pose discomfort or a burn hazard to the patient. MR magnetic field gradients can cause interference and can also induce currents on the ECG cables and connections points, producing an additive interference waveform components that potentially give false heart rate readings, obscure ECG R-wave detection schemes, or otherwise degrade the ECG analysis. Cables employing a plated snap connector at each electrode location also introduce a time-consuming manual task of connecting each disposable electrode to a re-usable cable consisting of discrete wires and connectors.

Tuccillo et al., U.S. Pub. No. 2006/0247509 A1 discloses an a cable for use in an MRI, which is adapted to resist motion in response to magnetic fields generated by the MR scanner. The cable of Tuccillo et al. is constructed of a flexible Kapton substrate on which a plurality of conductive traces are drawn using a conductive carbon ink. In the disclosed embodiment, the carbon ink has a resistance of 10 ohm/sq while the cable is six feet in length and has a distributed impedance of about 330 ohms/cm. The ends of the cable include expanded regions with copper pads for connection to an ECG electrode at one end and an ECG monitor at the opposite end.

Electrodes for biopotential measurements also pose difficulties in an MR environment. A known electrode is a silver-silver chloride (Ag-AgCl) electrode. This type of electrode is also used in the construction of MR-compatible ECG electrodes in efforts to reduce DC offset voltage created by the half-cell potential of the electrode and to minimize contact impedance. Either a paste or gel is used as the electrolyte interface to the patient. Van Genderingen et al., “Carbon-Fiber Electrodes and Leads for Electrocardiography during MR Imaging”, Radiology vol. 171 no. 3 page 872 (1989) discloses replacing conventional Ag-AgCl ECG electrodes with braided metal leads with ECG electrodes made of carbon fiber with plastic reinforced carbon fiber leads (Carbo Cone RE-I, Sundstroem, Sweden). They report that the carbon fiber electrodes did not degrade the images as compared with the conventional Ag-AgCl electrode/braided metal leads, and the

plastic reinforcement made the carbon fiber leads less susceptible to bending as compared with similar leads made of graphite.

The following contemplates improved apparatuses and methods that overcome the aforementioned limitations and others.

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According to one aspect, an electrode patch is disclosed for use in biopotential measurements in a magnetic resonance (MR) environment. The electrode patch comprises: a plastic or polymer sheet; an electrically conductive trace disposed on the plastic or polymer sheet, the electrically conductive trace having sheet resistance of one ohm/square
10 or higher; and an electrode disposed on the electrically conductive trace and configured for attachment to human skin.

According to another aspect, an electrode patch is disclosed for use in biopotential measurements in a magnetic resonance (MR) environment. The electrode patch comprises: a plastic or polymer sheet; a carbon-based electrically conductive trace disposed on the
15 plastic or polymer sheet; and an electrode disposed on the electrically conductive trace and configured for attachment to human skin.

According to another aspect, a biopotential measurement apparatus is disclosed, comprising: an electrode patch as set forth in any one of the two immediately preceding paragraphs; a monitor or receiver unit configured to receive biopotential measurements;
20 and a cable electrically connecting the electrode of the electrode patch with the monitor or receiver unit.

According to another aspect, a system is disclosed, comprising a magnetic resonance scanner and a biopotential measurement apparatus as set forth in the immediately preceding paragraph wherein the electrode patch is disposed in an
25 examination region of the magnetic resonance scanner.

One advantage resides in providing a magnetic resonance-compatible electrode patch for ECG or other biopotential measurements with reduced susceptibility to eddy currents.

Another advantage resides in providing a magnetic resonance-compatible electrode
30 patch for ECG or other biopotential measurements that is robust against interference.

Another advantage resides in providing a magnetic resonance-compatible electrode patch for ECG or other biopotential measurements that provides one or more of the foregoing advantages in combination with effective electrode attachment to human skin.

Numerous additional advantages and benefits will become apparent to those of ordinary skill in the art upon reading the following detailed description.

The invention may take form in various components and arrangements of components, and in various process operations and arrangements of process operations. The drawings are only for the purpose of illustrating preferred embodiments and are not to be construed as limiting the invention.

FIGURE 1 diagrammatically shows a magnetic resonance (MR) system with an electrocardiograph (ECG) operating inside the MR scanner.

FIGURE 2 diagrammatically shows the ECG acquisition system.

FIGURE 3 diagrammatically shows an electrode and proximate portion of cable as disclosed herein.

FIGURE 4 diagrammatically shows an electrode patch with uniformly distributed high resistance printed circuitry.

FIGURE 5 diagrammatically shows an electrode patch with non-uniformly distributed high resistance printed circuitry.

FIGURES 6-8 show ECG results acquired using conventional electrode patches with ECG results acquired using electrode patches as disclosed herein.

With reference to FIGURE 1, a magnetic resonance environment includes a magnetic resonance (MR) scanner **10** disposed in a radio frequency isolation room **12** (diagrammatically indicated by a dashed box surrounding the MR scanner **10**), for example, comprising a wire mesh or other radio frequency screening structures embedded in or disposed on the walls, ceiling, and floor of the MR room containing the MR scanner **10**. The MR scanner **10** is shown in diagrammatic side-sectional view in FIGURE 1, and includes a housing **14** containing a main magnet windings **16** (typically superconducting and contained in suitable cryogenic containment, not shown, although a resistive magnet windings are also contemplated) that generate a static (B_0) magnetic field in a bore **18** or

other examination region. The housing **14** also contains magnetic field gradient coils **20** for superimposing magnetic field gradients on the static (B_0) magnetic field. Such gradients have numerous applications as is known in the art, such as spatially encoding magnetic resonance, spoiling magnetic resonance, and so forth. An imaging subject, such as an illustrative patient **22**, or an animal (for veterinary imaging applications), or so forth is loaded into the examination region (inside the bore **18** in the illustrative case) via a suitable couch **24** or other patient support/transport apparatus. The MR scanner may include numerous additional components known in the art which are not shown for simplicity, such as optional steel shims, optional whole body radio frequency (RF) coil disposed in the housing **14**, and so forth. The MR scanner also typically includes numerous auxiliary or ancillary components again not shown for simplicity, such as power supplies for the main magnet **16** and the magnetic field gradient coils **20**, optional local RF coils (e.g. surface coils, a head coil or limb coil, or so forth), RF transmitter and RF reception hardware, and various control and image reconstruction systems, by way of some examples. Moreover, it is to be understood that the illustrative MR scanner **10**, which is a horizontal-bore type scanner, is merely an illustrative example and that more generally the disclosed MR safe cables and electrodes are suitably employed in conjunction with any type of MR scanner (e.g., a vertical bore scanner, open-bore scanner, or so forth).

In operation, the main magnet **16** operates to generate a static B_0 magnetic field in the examination region **18**. RF pulses are generated by the RF system (including for example a transmitter and one or more RF coils disposed in the bore or a whole-body RF coil in the housing **14**) at the Larmor frequency (i.e., magnetic resonance frequency) for the species to be excited (usually protons, although other species may be excited, e.g. in MR spectroscopy or multinuclear MR imaging applications). These pulses excite nuclear magnetic resonance (NMR) in the target species (e.g., protons) in the subject **22** which are detected by a suitable RF detection system (e.g., a magnetic resonance coil or coils and suitable receiver electronics). Magnetic field gradients are optionally applied by the gradient coils **20** before or during excitation, during a delay period (e.g., time to echo or TE) period prior to readout, and/or during readout in order to spatially encode the NMR signals. An image reconstruction processor applies a suitable reconstruction algorithm comporting with the chosen spatial encoding in order to generate a magnetic resonance

image which may then be displayed, rendered, fused or contrasted with other MR images and/or images from other modalities, or otherwise utilized.

With continuing reference to FIGURE 1 and with further reference to FIGURE 2, as part of the MR procedure, biopotential measurements are acquired using electrodes **30** disposed on an appropriate portion of the patient (e.g., on chest skin and optionally also on limb skin in the case of ECG, or on the scalp in the case of EEG, or so forth). In illustrative FIGURE 1 four electrodes are disposed on a common substrate **32** to form an electrodes patch **34**. The common substrate **32** provides defined spacing and a supporting substrate for the (illustrative four) electrodes. The number, arrangement, and location of electrodes are chosen for the particular application. In the case of ECG some common electrode configurations include EASI configurations and variants thereof, which typically include about five electrodes, and so-called 12-lead ECG which employs ten electrodes disposed on the chest and limbs in a standard 12-lead ECG configuration. In some embodiments the electrodes may be discrete, rather than being disposed on a common patch as in the illustrative example.

A cable **36** includes conductors in the form of electrically conductive traces **38** disposed on a substrate **40**. Although electrically conductive, the traces **38** are highly resistive compared with conventional printed circuitry such as copper traces. For example, in some embodiments the traces **38** have sheet resistance R_S of one ohm/sq or higher. (By comparison, a copper trace in typical printed circuitry has sheet resistance of about 0.05 ohm/sq or lower). More generally, the material resistivity ρ together with the thickness t and width W of the trace are chosen to provide the desired conductor resistance. As is known in the art, sheet resistance R_S is given by the bulk resistivity ρ of the material forming the layer divided by the layer thickness t , i.e. $R_S = \rho/t$. Then the resistance R of a trace (i.e., conductor) of thickness t having length L and width W is given as $R = R_S \times (L/W)$.

In some embodiments the conductive traces **38** are formed from a mixture of conductive particles disposed in a solvent matrix, which is applied to the substrate **40**. Upon curing the solvent dissipates leaving the conductive particles bonded to the substrate **40** by residue of the curing. In some embodiments the conductive traces **38** are formed of graphite, nanotubes, buckyballs, or other carbon-based particles disposed on the substrate **40** by screen printing or another deposition process to form the conductive traces **38**.

Instead of carbon-based particles, particles of other materials of suitable (bulk) resistivity and mechanical and thermal properties can be chosen, such as a doped semiconductor material, silicone particles, metal oxide materials, or so forth. Instead of screen printing, other processes can be used to form the traces **38** on the substrate **40**, such as depositing a
5 bulk layer and etching away to define the traces, depositing the traces by a vacuum evaporation process, or so forth. The material forming the traces **38** should also be non-ferromagnetic to avoid interference with the MR scanner.

The substrate **40** can be any substrate capable of supporting the conductors **38** in suitable electrical isolation. Some suitable substrates include a plastic or polymer substrate
10 such as a Melinex[®] sheet or film (available from DuPont Teijin Films, Chester, VA), a polyimide sheet or film, or so forth. The substrate should be electrically insulating as compared with the conductivity of the material of the traces **38**; alternatively the substrate can be electrically conductive but including an electrically insulating layer on which the traces are disposed, where the electrically insulating layer is insulating as compared with
15 the conductivity of the material of the traces **38**. In some embodiments, the substrate **40** advantageously has some flexibility (as is the case for a Melinex[®] sheet or film) to enable the cable **36** to be somewhat flexible.

The cable **36** runs from the electrodes **30** to a receiver unit **42**. In the illustrative example the receiver unit **42** is a wireless ECG module that receives the measured potential
20 signals and transmits them via a wireless channel **44** (diagrammatically indicated in FIGURE 1 by a dashed double-headed curved line) to an ECG monitor **46** located outside (or optionally inside) the MR room **12**. The wireless ECG module **42** can be located inside the bore **18** (as illustrated) or outside (for example, by running the cable through a passageway through the MR housing **14** or out the open end of the bore **18**). Moreover, it is
25 contemplated to omit the wireless ECG module and instead run the cable directly to the ECG monitor (in which case the ECG monitor is the receiver unit), although this will generally require a substantially longer cable. The ECG monitor **46** is configured to process and display the acquired biopotential measurements. For example, in the illustrative case of the ECG monitor **46**, the ECG data may be displayed as ECG traces,
30 and may optionally be processed to detect R-wave occurrences or other ECG events for use in gating of the MR imaging or so forth. In some embodiments the acquired ECG (or other

biopotential) data are stored on a non-transitory storage medium such as a hard disk drive, flash drive, or so forth, and/or are printed on paper (e.g., as ECG traces).

With reference to FIGURE 3, a suitable configuration for the cable **34** and electrodes **30** is shown in side sectional view so as to show the conductor or trace **38** disposed on the substrate **40**. Optionally, a protective layer **50** covers the traces **38** to provide electrical insulation and protection against damage by abrasion or the like. The protective layer **50** should be electrically insulating as compared with the material of the traces **38**, and should be non-ferromagnetic and MR compatible. Some suitable embodiments of the protective layer **50** include a polymer or polyimide sheet applied on top of the substrate **40** after depositing or otherwise forming the traces **38**, or depositing an insulating plastic, polymer, or other material on top of the substrate **40** and traces **38** to form the protective layer **50**. The protective layer **50** may also be a foam thermal insulating layer to provide patient comfort.

With continuing reference to FIGURE 3, the electrode patch **34** can be formed similarly, with the common substrate **32** being a Melinex[®] sheet or film or other suitable substrate with appropriate electrically insulating and MR compatible properties, and with flexibility as desired. The common substrate **32** of the electrodes can be the same material as the substrate **40** of the cable **36** (as in illustrative FIGURE 3), or can be different materials. The electrode **30** is disposed on a trace **58** formed on the substrate **32**. The trace **58** can be of the same material and deposition technique as the traces **38** of the cable **36**, e.g. a carbon-based printed trace. The traces **38** of the cable **36** and the traces **58** connecting and supporting the electrodes **30** can be of the same material (as illustrated), or can be different materials. The electrode **30** is formed on the trace **58** using a suitable layer or layer stack to facilitate electrical contact with skin **60** of the patient or other subject **22**. In one suitable embodiment, the electrodes **30** include a silver layer **62** disposed on the carbon-based trace **58**, and a silver chloride-based electrolyte layer **64** disposed on the silver layer **62**. The electrolyte layer **64** can serve as an adhesive, or an additional adhesive layer can be provided (not shown). The electrode patch **34** preferably includes a protective layer **70** which may be the same material as the protective layer **50** of the cable **36**. However, the protective layer **70** should include openings for the electrodes **30** to enable the electrodes **30** to contact the skin **60**. It is contemplated to include a pull-off tab or other

covering (not shown) disposed over the electrode **30** which is pulled off or otherwise removed just before the electrode is applied to the skin **60**.

With continuing reference to FIGURE 3, electrical connection between the electrode patch **34** and the cable **36** (or, between individual electrodes and the cable **36** in
5 embodiments employing individual electrodes rather than a patch), and electrical connection between the cable **36** and the receiver unit **42** can take various forms. In the illustrative example of FIGURE 3, at the end of the cable **36** distal from the electrodes patch **34** each conductor or trace **38** is coated with a layer or layer stack **72** of a suitably electrically conductive material (that is, more electrically conductive than the conductors or
10 traces **38**). In the illustrative example, layer **72** is a silver layer comparable to the silver layer **62** of the electrodes **30**, but omitting the silver chloride coating **64**. In other embodiments, the layer **72** may be silver, copper, or another material having higher conductivity than the material forming the trace **38**. In some embodiments the layer **72** is an added piece of metal foil. The protective layer **50** does not cover these layers **72**. The effect is to form an edge connector **74** that can plug into a mating socket of the receiver
15 unit **42**. Unless the distal end of the cable extends outside of the MR scanner, the layer or layers **72** should be made of an MR compatible material, e.g. a non-ferromagnetic material. Although not shown in FIGURE 3, the connection between the electrodes patch **34** and the cable **36** can employ a similar arrangement except with a mating connector attached to one
20 of the components **34**, **36**.

By manufacturing the cable **36** and the electrodes patch **34** as separate elements, the cable can be reused while the patch would typically be a disposable consumable item that is used once for a patient and then discarded. Alternatively, in some embodiments the electrodes patch **34** and the cable **36** are formed as a single unitary structure on a single-
25 piece substrate that embodies both substrates **32**, **40**, and with the traces **38**, **58** forming single continuous traces. This approach simplifies patient workflow as the single-piece ECG patch/cable is utilized by plugging the edge connector **74** into the mating socket of the receiver unit **42** (or alternatively into the mating socket of the ECG monitor), applying the electrodes **30** to the patient, and running the ECG. The step of connecting the cable
30 with the ECG electrodes is eliminated. Because the cable and patch are fabricated as a single unitary structure, the additional cost of discarding the cable is reduced.

In various embodiments, the traces **38**, **58** are suitably formed of carbon-based ink with specific electrical resistance applied to the planar flexible substrate **32**, **40**, such as polymer resin-based film, by any reproductive method, such as by screen printing. The printed trace **38**, **58** may be solid or may contain features such as hatching to reduce eddy current generation in the trace or to vary resistance with identical geometry. The cable may have any number of conductors from 1 to 12 (or more, if appropriate for the application). For example, in a 12-lead ECG setup the cable may include 12 conductors **38**, while in an EASI ECG setup only 5 conductors may be included. All conductors may be on a single substrate or may be on different substrates to accommodate various patient body shapes and/or to simplify cable routing.

In other contemplated aspects, the resistance of the conductors **38**, **58** may be evenly or unevenly distributed along the trace **38**, **58**. Uneven distribution can be achieved, for example, by varying the trace width and/or thickness, or by using a “checkerboard” pattern or other nonuniform printing pattern for the trace. It is also contemplated to add electrical components to the cable **36** and/or to the electrode patch **34**. For example, a discrete resistance component may be added, or a small region of higher-resistance material may be interposed along the trace to form a localized resistance. The cable **36** and/or electrode patch **34** is optionally surrounded by a protective shield (e.g., Faraday cage) to minimize electrical interference. Notch filters or low pass filters, integrated circuit components, antenna circuits, power supplies, sensors (e.g., piezo sensors or MEMS accelerometers), or optical elements are optionally be incorporated into the cable **36** and/or electrode patch **34** by adhering or otherwise attaching such components to the substrate **32**, **40** and connecting to various traces **38**, **58** as appropriate.

With reference to FIGURES 4 and 5, some illustrative configurations for the electrodes patch **34** are shown. In these embodiments, the patch **34** includes a connector **80** that may, for example, accept an edge connector (not shown) of the cable **36** that is similar to the edge connector **74** shown in FIGURE 3, except located at the end of the cable **36** proximate to the electrodes patch **34**. In the patch embodiment of FIGURE 4, the traces **58** are continuous traces. In the patch embodiment of FIGURE 5, traces **58C** have the same layout as the traces **58**, but are deposited in a “checkerboard” pattern with only 50% coverage (see inset of FIGURE 5). By reducing the area coverage of the traces the sheet

resistance R_S is effectively increased (e.g., typically by a factor of about two for 50% area coverage).

By printing the electrode and lead connections, repeatability and reproducibility of the lead-wire routing is assured between cases and for the same patient. Patient movement is less likely to induce voltages or introduce noise to the biopotential measurement, because such motion does not change the relative spacing of the electrodes or the leads (i.e., conductors **38**, **58**). If the substrates **32**, **40** have some flexibility then some motion related voltage induction and noise may result, but the amount of motion (and hence the introduced noise) is substantially reduced versus the case for individual wires. Moreover, a tradeoff between patient comfort and preparation convenience (facilitated by making the substrates flexible) and noise (suppressed by making the substrates rigid) can be achieved by appropriate design of the substrate flexibility (controlled, for example, by the thickness of the substrate, as a thicker substrate is generally less flexible).

The materials for the electrodes and the cable are selected so that proton emissions do not obscure the MR image, and to minimize contact impedance, and to minimize offset voltages. The disclosed cables and electrodes are readily constructed to be “MR Safe” rather than merely “MR Conditional”. (The distinction is that for “MR safe” there should be no condition under which the component poses a risk to the patient or introduces functional limitations in the MRI).

Although in the disclosed embodiments the electrodes **30** are attached by adhesive, alternatively a mechanical mechanism can be used to attach the patch rather than adhesive. Moreover, materials other than silver-silver chloride may be used to create the electrode tissue interface circuit. For example, gel soaked sponge or paste may be used to create the electrode tissue interface circuit. As with protective layer **50**, the protective layer **70** of the electrode patch **34** may advantageously be a foam thermal insulating layer.

With reference to FIGURES 6-8, test ECG results are shown for a prototype of the electrodes patch **34**. The tests were performed in a Philips 3.0T Achieva™ MRI Scanner. Several high dB/dT scan sequences were evaluated using an existing commercial electrode patch (i.e. “current electrode”) versus the electrodes patch **34** (i.e., “Disclosed electrode”). Criteria used to evaluate performance include the R-wave to T-wave amplitude ratio (where the bigger the ratio, the better because it prevents the T-wave from being detected

as an R-wave creating false triggering/synchronization to the MRI) and the variation (or RMS noise) in the baseline (where lower is the better because it prevents the R-wave from being obscured during R-wave detection). FIGURE 6 shows results for a diffusion-weighted imaging (DWI) scan. FIGURE 7 shows results for a field-echo, echo planar imaging (FE-EPI) scan. FIGURE 8 shows results for a survey scan.

The invention has been described with reference to the preferred embodiments. Obviously, modifications and alterations will occur to others upon reading and understanding the preceding detailed description. It is intended that the invention be construed as including all such modifications and alterations insofar as they come within the scope of the appended claims or the equivalents thereof.

CLAIMS

Having described the preferred embodiments, the invention is now claimed to be:

1. An electrode patch (34) for use in biopotential measurements in a magnetic resonance (MR) environment, the electrode patch comprising:
 - a plastic or polymer sheet (32);
 - an electrically conductive trace (58) disposed on the plastic or polymer sheet, the electrically conductive trace having sheet resistance of one ohm/square or higher; and
 - an electrode (30) disposed on the electrically conductive trace and configured for attachment to human skin.

2. An electrode patch (34) for use in biopotential measurements in a magnetic resonance (MR) environment, the cable comprising:
 - a plastic or polymer sheet (32); and
 - a carbon-based electrically conductive trace (58) disposed on the plastic or polymer sheet; and
 - an electrode (30) disposed on the carbon-based electrically conductive trace and configured for attachment to human skin.

3. The electrode patch (34) of claim 2, wherein the carbon-based electrically conductive trace (58) has sheet resistance of one ohm/square or higher.

4. The electrode patch (34) of any one of claims 1-3, wherein the electrically conductive trace (58) comprises a graphite-based trace.

5. The electrode patch (34) of any one of claims 1-4, wherein the electrically conductive trace (58) comprises a carbon-based ink deposited on the plastic or polymer sheet by screen printing.

6. The electrode patch (34) of any one of claims 1-5, wherein the electrode (30) includes an attachment layer (64) disposed on the electrically conductive trace (58) and configured for attachment to human or animal skin includes a silver layer.

7. The electrode patch (34) of claim 6, wherein the attachment layer (64) includes silver chloride.

8. The electrode patch (34) of claim 6, wherein the attachment layer (64) is a silver chloride-based electrolyte layer.

9. The electrode patch (34) of claim 8, wherein the electrode (30) further includes a silver layer interposed between the electrically conductive trace (58) and the silver chloride-based electrolyte layer (64).

10. The electrode patch (34) of any one of claims 1-9, wherein the electrode (30) includes a layer (62) of electrically conductive material disposed on the electrically conductive trace (58) that is more electrically conductive than the material comprising the electrically conductive trace.

11. The electrode patch (34) of claim 10, wherein the layer (62) of electrically conductive material comprises silver.

12. The electrode patch (34) of any one of claims 1-11, further comprising:
an electrically insulating protective layer (70) disposed over the electrically conductive trace (58) and the plastic or polymer sheet (32), the electrically insulating protective layer not covering the electrode (30).

13. The electrode patch (34) of claim 12, wherein the electrically insulating protective layer (70) comprises a foam thermally insulating layer.

14. The electrode patch (34) of any one of claims **1-13**, including a cable (36) defined by a protrusion of the plastic or polymer sheet (32) along which the electrically conductive trace runs.

15. The electrode patch (34) of any one of claims **1-13**, further comprising:
a connector (80) configured to connect with a cable (36).

16. A biopotential measurement apparatus comprising:
an electrode patch (34) as set forth in any one of claims **1-15**;
a monitor or receiver unit (42) configured to receive biopotential measurements;
and
a cable (36) electrically connecting the electrode (30) of the electrode patch with the monitor or receiver unit.

17. The biopotential measurement apparatus of claim **16**, wherein the biopotential measurements are electrocardiography (ECG) measurements.

18. The biopotential measurement apparatus of claim **16**, wherein the biopotential measurements are one of electrocardiography (ECG) measurements, electromyography (EMG) measurements, electroencephalography (EEG) measurements, and electroretinography (ERG) measurements.

19. A system comprising:
a magnetic resonance scanner (10); and
a biopotential measurement apparatus as set forth in any one of claims **16-18** wherein the electrode patch (34) is disposed in an examination region of the magnetic resonance scanner.

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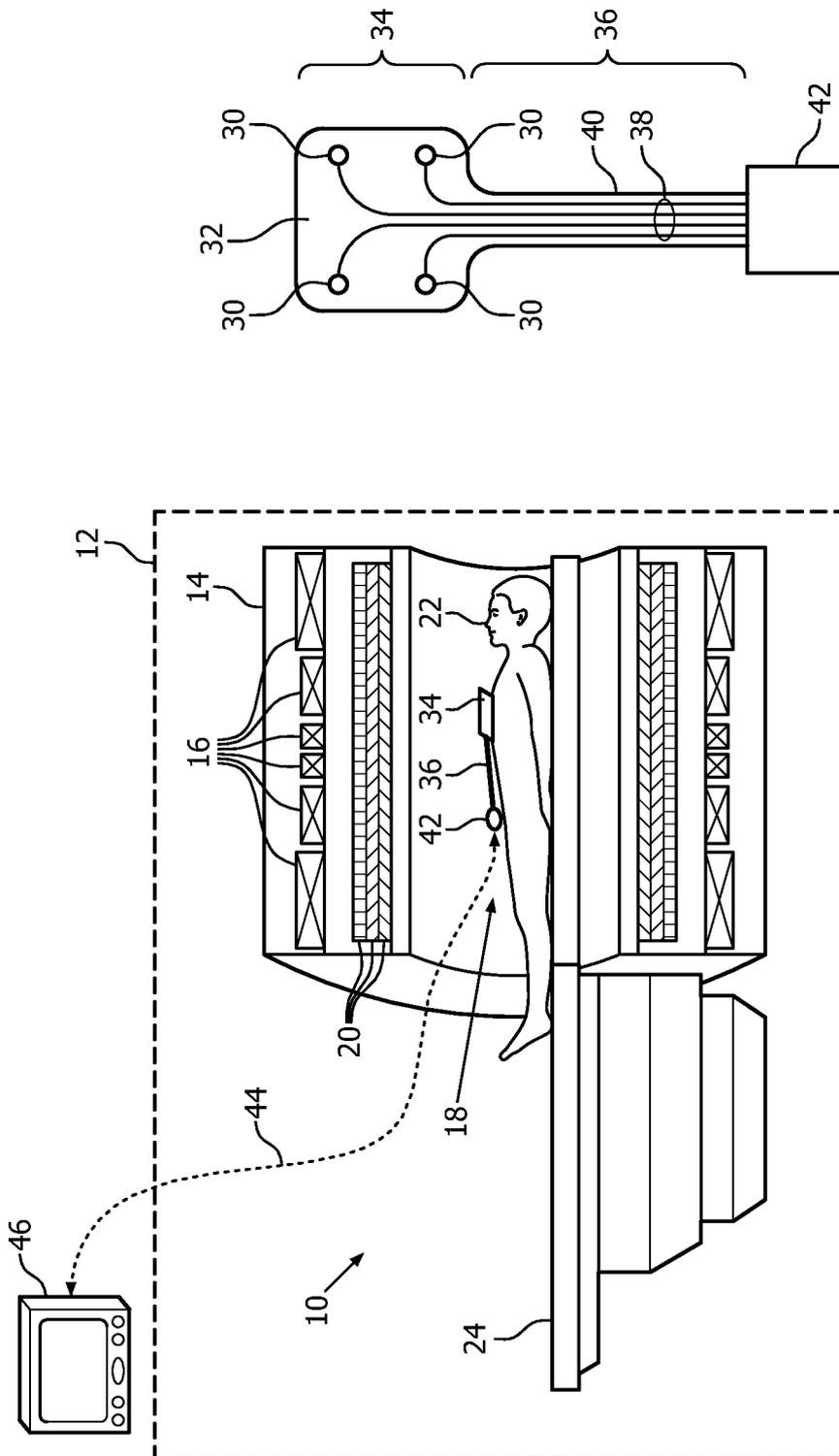


FIG. 2

FIG. 1

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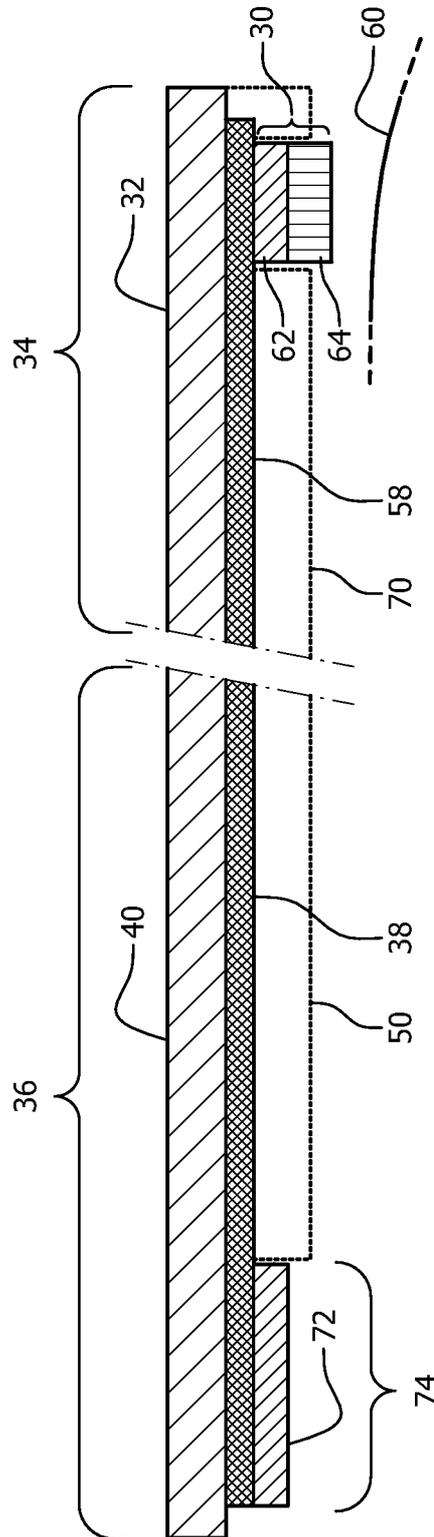
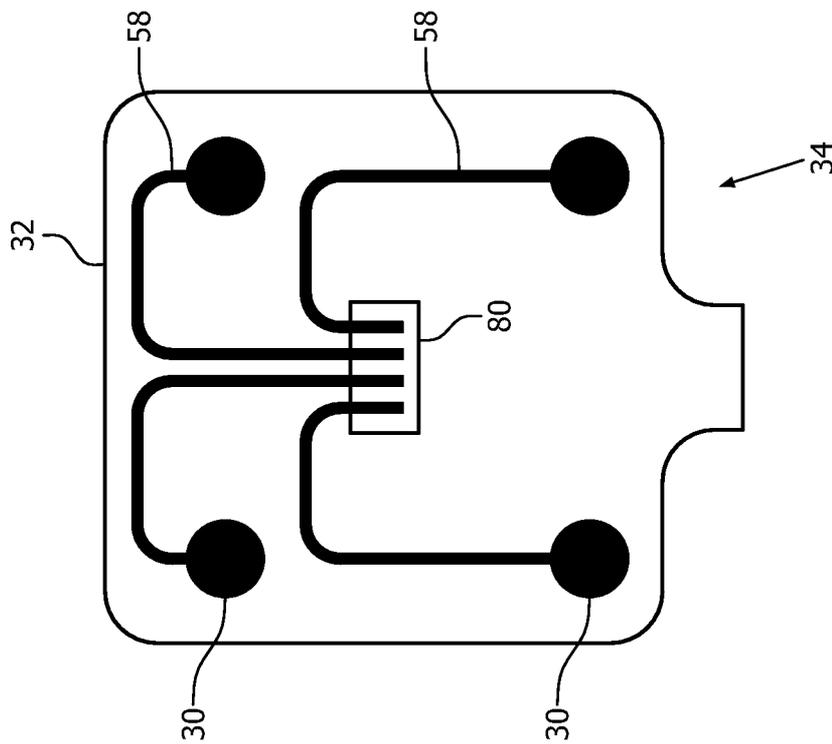
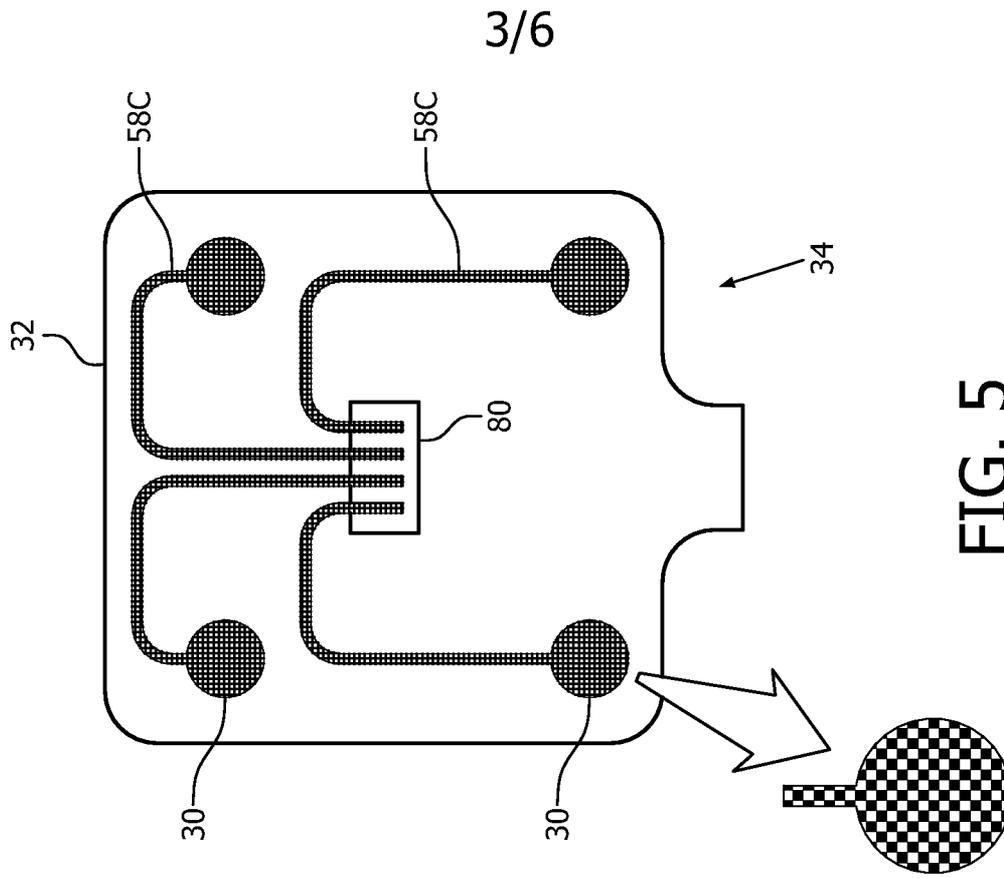


FIG. 3



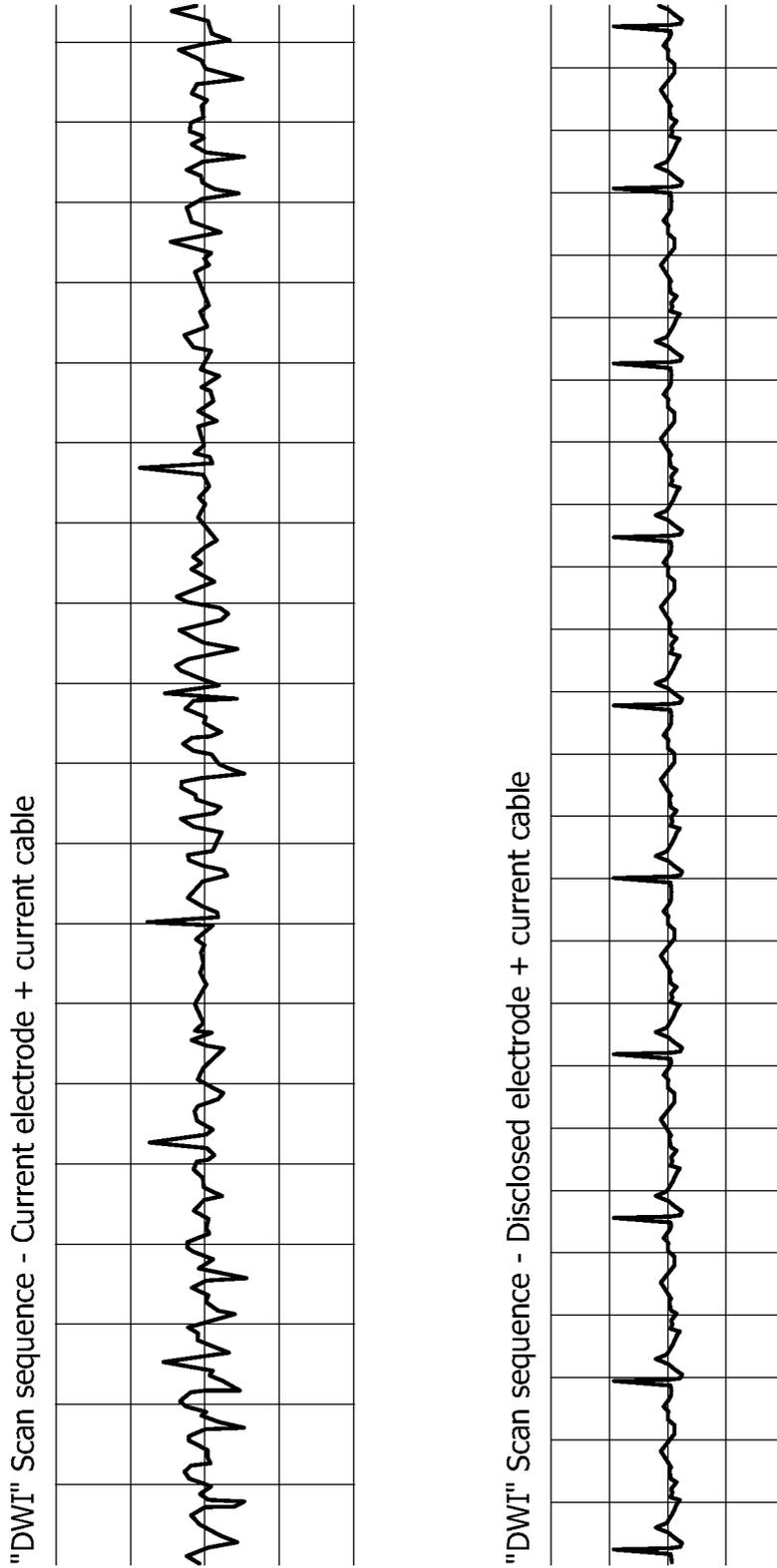


FIG. 6

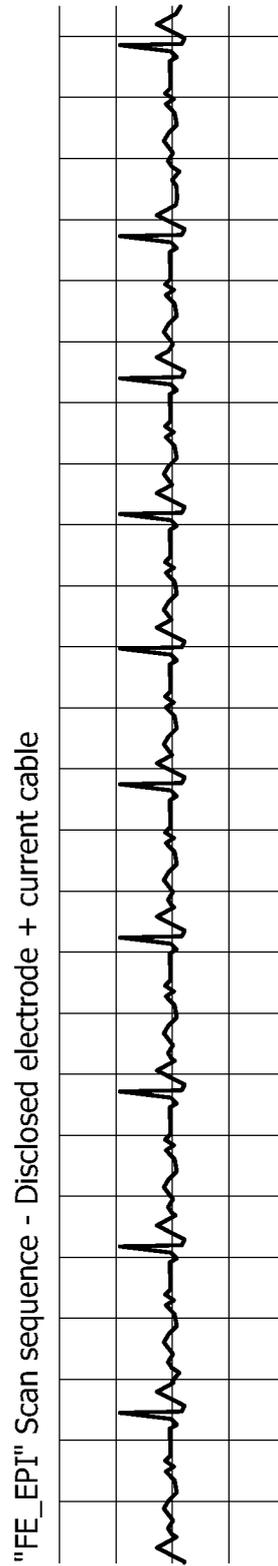
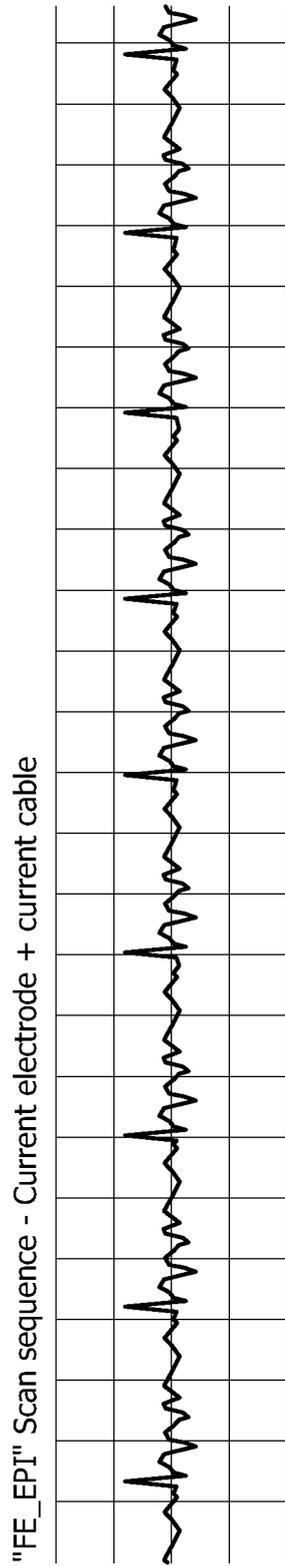


FIG. 7

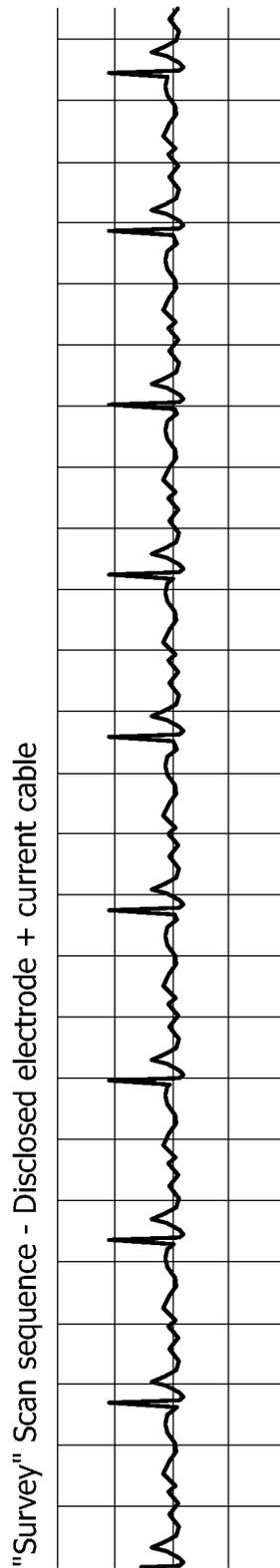
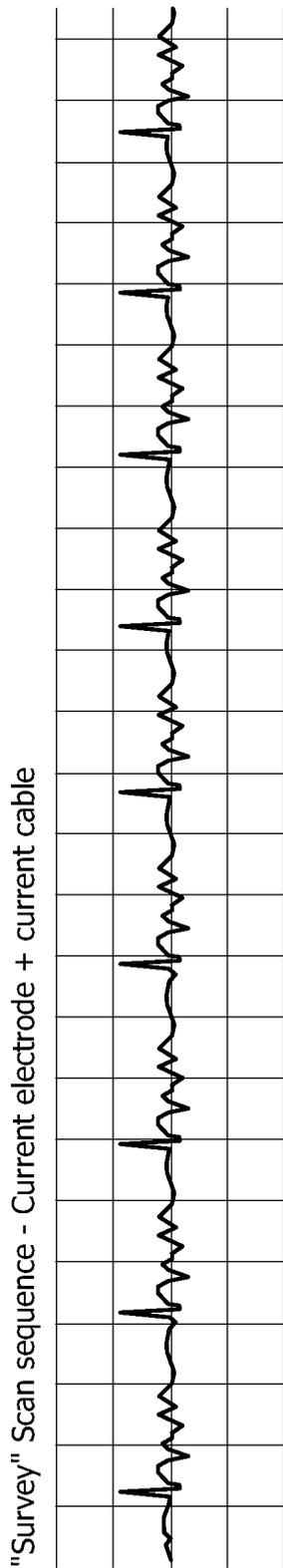


FIG. 8

INTERNATIONAL SEARCH REPORT

International application No
PCT/IB2013/053887

A. CLASSIFICATION OF SUBJECT MATTER
INV. A61B5/0408 A61B5/0478 A61B5/0492
ADD.
According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED
Minimum documentation searched (classification system followed by classification symbols)
A61N A61B G01R
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
EPO-Internal, WPI Data

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X A	WO 2009/055397 A2 (HMICRO INC [US]; BECK JAMES [US]) 30 April 2009 (2009-04-30) figures 1, 2, 5A, B paragraphs [0002], [0007], [0020], [0025], [0026], [0028], [0029], [0031], [0035]	1,4-19 2,3
X A	EP 2 388 913 A1 (IVY BIOMEDICAL SYSTEMS INC [US]) 23 November 2011 (2011-11-23) figure 9 paragraphs [0001], [0014], [0034], [0056], [0057]	1-15,19 16-18
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Further documents are listed in the continuation of Box C. See patent family annex.

* Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
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"O" document referring to an oral disclosure, use, exhibition or other means	"&" document member of the same patent family
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Date of the actual completion of the international search 27 August 2013	Date of mailing of the international search report 03/09/2013
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Name and mailing address of the ISA/ European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Fax: (+31-70) 340-3016	Authorized officer Almeida, Mariana
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INTERNATIONAL SEARCH REPORT

International application No
PCT/IB2013/053887

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