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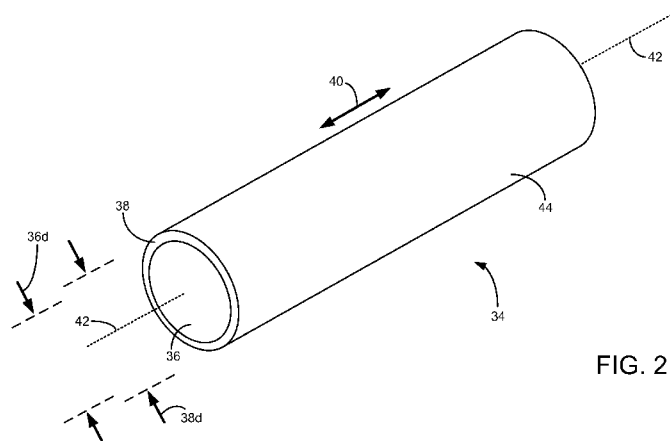


FIG. 2

(57) Abstract: A consumable filament (34, 134, 234) for use in an extrusion-based additive manufacturing system (10), where the consumable filament (34, 134, 234) comprises a first portion (36, 136, 236) of a first semi-crystalline polymeric material, and a second portion (38, 138, 238) of a second semi-crystalline polymeric material, and where the second semi-crystalline polymeric material has a crystallization temperature that is greater than a crystallization temperature of the first semi-crystalline polymeric material.



## **SEMI-CRYSTALLINE CONSUMABLE MATERIALS FOR USE IN EXTRUSION-BASED ADDITIVE MANUFACTURING SYSTEMS**

### **BACKGROUND**

The present disclosure is directed to additive manufacturing systems for building three-dimensional (3D) models. In particular, the present disclosure relates to consumable materials for use in extrusion-based additive manufacturing systems.

An extrusion-based additive manufacturing system is used to build a 3D model from a digital representation of the 3D model in a layer-by-layer manner by extruding a flowable modeling material. The modeling material is extruded through an extrusion tip carried by an extrusion head, and is deposited as a sequence of roads on a substrate in an x-y plane. The extruded modeling material fuses to previously deposited modeling material, and solidifies upon a drop in temperature. The position of the extrusion head relative to the substrate is then incremented along a z-axis (perpendicular to the x-y plane), and the process is then repeated to form a 3D model resembling the digital representation.

Movement of the extrusion head with respect to the substrate is performed under computer control, in accordance with build data that represents the 3D model. The build data is obtained by initially slicing the digital representation of the 3D model into multiple horizontally sliced layers. Then, for each sliced layer, the host computer generates a build path for depositing roads of modeling material to form the 3D model.

In fabricating 3D models by depositing layers of a modeling material, supporting layers or structures are typically built underneath overhanging portions or in cavities of objects under construction, which are not supported by the modeling material itself. A support structure may be built utilizing the same deposition techniques by which the modeling material is deposited. The host computer generates additional geometry acting as a support structure for the overhanging or free-space segments of the 3D model being formed. Support material is then deposited from a second nozzle pursuant to the generated geometry during the build process. The support material adheres to the modeling material during fabrication, and is removable from the completed 3D model when the build process is complete.

## SUMMARY

A first aspect of the present disclosure is directed to a consumable filament for use in an extrusion-based additive manufacturing system. The consumable filament includes a first portion that compositionally includes a first semi-crystalline polymeric material. The semi-crystalline filament also includes a second portion and at least partially encasing the first portion and that compositionally includes a second semi-crystalline polymeric material having a crystallization temperature that is greater than a crystallization temperature of the first semi-crystalline polymeric material. The consumable filament has an average cross-sectional area suitable for use in the extrusion-based additive manufacturing system. The second portion has an average volume ranging from about 5% to about 50% of an average volume of the consumable filament.

Another aspect of the present disclosure is directed to a three-dimensional object built with an extrusion-based additive manufacturing system. The three-dimensional object includes a plurality of solidified layers each comprising roads extruded with the extrusion-based additive manufacturing system from a consumable filament having a core portion and a shell portion. The core portion compositionally comprises a first semi-crystalline polymeric material having a first peak crystallization temperature, and the shell portion comprising a second semi-crystalline polymeric material having a second peak crystallization temperature that is greater than the first peak crystallization temperature. At least a portion of the roads of the plurality of solidified layers at least partially retain cross-sectional profiles corresponding to the core portion and the shell portion of the consumable filament.

Another aspect of the present disclosure is directed to a method for building a three-dimensional object with an additive manufacturing system having a heated build chamber and an extrusion head. The method includes feeding a consumable filament to the extrusion head, where the consumable filament includes a first portion and a second portion at least partially encasing the first portion. The first portion compositionally includes a first semi-crystalline polymeric material, and the second portion compositionally includes a second semi-crystalline polymeric material having a peak crystallization temperature that is greater than a peak crystallization temperature of the first semi-crystalline polymeric material. The method also includes melting the fed consumable filament in the extrusion head to form a molten material, and depositing the molten material in the heated build chamber as an extruded road that defines at least a portion of a layer of the three-

dimensional object, where the extruded road compositionally includes the first semi-crystalline polymeric material and the second semi-crystalline polymeric material. The method further includes crystallizing at least a portion of the second semi-crystalline polymeric material of the extruded road, and crystallizing at least a portion of the first semi-crystalline polymeric material of the extruded road after crystallizing the portion of the second semi-crystalline polymeric material.

## DEFINITIONS

Unless otherwise specified, the following terms used in this specification have the meanings provided below.

The term “semi-crystalline polymeric material” refers to a material comprising a polymer, where the polymer is capable of exhibiting an average percent crystallinity in a solid state of at least about 10% by weight. The term “semi-crystalline polymeric material” includes polymeric materials having crystallinities up to 100% (i.e., fully-crystalline polymeric materials). For ease of discussion, the term “semi-crystalline polymeric material” is used herein since most polymeric materials have at least a small number of amorphous regions.

The terms “percent crystallinity”, “peak crystallization temperature”, “slope-intercept crystallization temperature”, “peak melting temperature”, and “slope-intercept melting temperature” are defined below in the specification with reference to differential scanning calorimetry (DSC) plots and ASTM D3418-08.

The terms “core portion” and “shell portion” of a filament refer to relative locations of the portions along a cross-section of the filament that is orthogonal to a longitudinal length of the filament, where the core portion is an inner portion relative to the shell portion. Unless otherwise stated, these terms are not intended to imply any further limitations on the cross-sectional characteristics of the portions.

The term “three-dimensional object” refers to any object built using a layer-based additive manufacturing technique, and includes 3D models and support structures built using layer-based additive manufacturing techniques.

The terms “about” and “substantially” are used herein with respect to measurable values and ranges due to expected variations known to those skilled in the art (e.g., limitations and variabilities in measurements).

## BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is a front view of an extrusion-based additive manufacturing system for building 3D models with the use of consumable materials of the present disclosure.

FIG. 2 is a perspective view of a segment of a consumable, semi-crystalline filament of the present disclosure, where the semi-crystalline filament includes a core portion and a shell portion.

FIG. 3 is an illustrative differential scanning calorimetry plot of heat flow versus temperature during a cooling phase for a shell material of the shell portion.

FIG. 4 is an illustrative differential scanning calorimetry plot of heat flow versus temperature during a cooling phase for a core material of the core portion.

FIG. 5 is a side illustration of layers of a 3D model during a build operation, where the dimensions of the layers and the relative distance of an extrusion tip from the layers are exaggerated for ease of discussion.

FIG. 6A is a perspective view of a segment of an alternative consumable, semi-crystalline filament of the present disclosure, where the alternative semi-crystalline filament includes a core portion and a shell portion, where the shell portion is defined by an inner shell and outer shell.

FIG. 6B is a perspective view of a segment of a second alternative consumable, semi-crystalline filament of the present disclosure, where the second alternative semi-crystalline filament includes a rectangular cross-sectional geometry.

FIGS. 7 and 8 are photographs of cross-sectional segments of example semi-crystalline filaments of the present disclosure.

FIG. 9 is a differential scanning calorimetry plot of heat flow versus temperature for a shell material of the example semi-crystalline filaments.

FIG. 10 is a differential scanning calorimetry plot of heat flow versus temperature for a core material of the example semi-crystalline filaments.

FIGS. 11 and 12 are photographs of 3D models built with a first example semi-crystalline filament of the present disclosure.

FIGS. 13-16 are photographs of 3D models built with a second example semi-crystalline filament of the present disclosure.

## DETAILED DESCRIPTION

The present disclosure is directed to consumables material for use in extrusion-based additive manufacturing systems. The consumable materials compositionally include multiple semi-crystalline polymeric materials having different crystallization temperatures. As discussed below, this difference in crystallization temperatures desirably reduces distortions, internal stresses, and sagging of the semi-crystalline polymeric materials when deposited as extruded roads to form layers of 3D models. The resulting 3D models may accordingly be built with reduced levels of curling and distortion, with good dimensional accuracies, and with good interlayer z-bond strengths.

Extrusion-based additive manufacturing systems currently build 3D models with the use of amorphous polymeric materials, such as acrylonitrile-butadiene-styrene (ABS) resins and polycarbonate resins. Amorphous polymeric materials have little or no ordered arrangements of their polymer chains in their solid states. As such, these materials exhibit glass transition effects that render them suitable for building 3D models and support structures in extrusion-based additive manufacturing systems. For example, as disclosed in Batchelder, U.S. Patent No. 5,866,058, an amorphous polymeric material may be deposited into a build region maintained at a temperature that is between a solidification temperature and a glass transition temperature of the material. This reduces the effects of curling and plastic deformation in the resulting 3D model or support structure.

Semi-crystalline polymeric materials, however, have different mechanical and thermal characteristics from amorphous polymeric materials. For example, due to their crystallinity, 3D models built with semi-crystalline polymeric materials may exhibit superior mechanical properties compared to 3D models built with amorphous polymeric materials. However, due to their higher levels of crystallinity, semi-crystalline polymeric materials exhibit discontinuous changes in volume upon solidification. Therefore, when supplied as a monofilament, a semi-crystalline polymeric material may contract and shrink when deposited to form a 3D model in an extrusion-based additive manufacturing system. This is particularly true for materials that are highly crystalline in their solid states.

This shrinkage initially occurs when an extruded road is deposited to form a portion of a layer of a 3D model. Additional shrinkage also occurs upon further cooling of the 3D model. These shrinkages can cause cumulative distortions, internal stresses, and curling of the 3D model being fabricated. For amorphous polymeric materials, curling and

distortion can be reduced by elevating the temperature in the build region. However, for semi-crystalline polymeric materials, which exhibit discontinuous changes in volume upon solidification, the elevated temperature required to reduce distortions results in sagging of the extruded roads, which may also result in distortions of the 3D model being built.

Accordingly, in one embodiment, the consumable materials of the present disclosure include a consumable, semi-crystalline filament having a first or core portion and a second or shell portion, where the first and second portions are derived from semi-crystalline polymeric materials having different crystallization temperatures. As discussed below, this difference in crystallization temperatures allows the material of the second portion to crystallize upon deposition, while the material of the first portion crystallizes upon further cooling. This desirably reduces distortions, internal stresses, and sagging of the semi-crystalline polymeric materials when deposited as extruded roads to form layers of 3D models.

As shown in FIG. 1, system 10 is an extrusion-based additive manufacturing system for building 3D models with a semi-crystalline filament. As such, the resulting 3D models may be built with semi-crystalline polymeric materials, while exhibiting reduced distortions. Examples of suitable systems for system 10 include extrusion-based additive manufacturing systems, such as those commercially available from Stratasys, Inc., Eden Prairie, MN under the trade designations "FUSED DEPOSITION MODELING" and "FDM".

System 10 includes build chamber 12, platen 14, gantry 16, extrusion head 18, and supply sources 20 and 22. Build chamber 12 is an enclosed, heatable environment that contains platen 14, gantry 16, and extrusion head 18 for building a 3D model (referred to as 3D model 24) and a corresponding support structure (referred to as support structure 26). Platen 14 is a platform on which 3D model 24 and support structure 26 are built, and desirably moves along a vertical z-axis based on signals provided from computer-operated controller 28. Platen 14 may also include a polymeric film (not shown) to further facilitate the removal of 3D model 24 and support structure 26.

Gantry 16 is a guide rail system that is desirably configured to move extrusion head 18 in a horizontal x-y plane within build chamber 12 based on signals provided from controller 28. The horizontal x-y plane is a plane defined by an x-axis and a y-axis (not shown), where the x-axis, the y-axis, and the z-axis are orthogonal to each other. In an alternative embodiment, platen 14 may be configured to move in the horizontal x-y

plane within build chamber 12, and extrusion head 18 may be configured to move along the z-axis. Other similar arrangements may also be used such that one or both of platen 14 and extrusion head 18 are moveable relative to each other.

Extrusion head 18 is supported by gantry 16 for building 3D model 24 and support structure 26 on platen 14 in a layer-by-layer manner, based on signals provided from controller 28. In the embodiment shown in FIG. 1, extrusion head 18 is a dual-tip extrusion head configured to deposit materials from supply source 20 and supply source 22, respectively. Examples of suitable extrusion heads for extrusion head 18 include those disclosed in Crump et al., U.S. Patent No. 5,503,785; Swanson et al., U.S. Patent No. 6,004,124; LaBossiere, et al., U.S. Patent No. 7,604,470; and Leavitt, U.S. Patent No. 7,625,200. Furthermore, system 10 may include a plurality of extrusion heads 18 for depositing modeling and/or support materials.

The semi-crystalline filament may be used as the modeling material for building 3D model 24. As such, the semi-crystalline filament may be supplied to extrusion head 18 from supply source 20 via feed line 30, thereby allowing extrusion head 18 to melt and deposit the semi-crystalline polymeric materials as a series of extruded roads to build 3D model 24 in a layer-by-layer manner. Correspondingly, the support material may be supplied to extrusion head 18 from supply source 22 via feed line 32, thereby allowing extrusion head 18 to melt and deposit the support material as a series of extruded roads to build support structure 26 in a layer-by-layer manner. Suitable devices for supply sources 20 and 22 include those disclosed in Swanson et al., U.S. Patent No. 6,923,634; Comb et al., U.S. Patent No. 7,122,246; and Taatjes et al, U.S. Patent Application Publication Nos. 2010/0096485 and 2010/0096489.

In one embodiment, the support material used to build support structure 26 may be an amorphous polymeric material, such as the water-soluble and break-away support materials commercially available from Stratasys, Inc., Eden Prairie, MN. In an alternative embodiment, a semi-crystalline filament of the present disclosure may also be used as the support material for building support structure 26. As such, in this alternative embodiment, support structure 26 may also be built using semi-crystalline polymeric materials.

During a build operation, gantry 16 moves extrusion head 18 around in the horizontal x-y plane within build chamber 12, and one or more drive mechanisms are directed to intermittently feed the modeling and support materials through extrusion head 18



from supply sources 20 and 22. Examples of suitable drive mechanisms for use in extrusion head 18 include those disclosed in Crump et al., U.S. Patent No. 5,503,785; Swanson et al., U.S. Patent No. 6,004,124; LaBossiere, et al., U.S. Patent Nos. 7,384,255 and 7,604,470; Leavitt, U.S. Patent No. 7,625,200; and Batchelder et al., U.S. Patent Application Publication No. 2009/0274540.

The received modeling and support materials are then deposited onto platen 14 to build 3D model 24 and support structure 26 as extruded roads using a layer-based additive manufacturing technique. Build chamber 12 is desirably heated to one or more suitable temperatures to allow the extruded roads of 3D model 24 to crystallize in two stages. In particular, the temperature(s) of build chamber 12 desirably allow the semi-crystalline polymeric material of the second or shell portion to crystallize upon deposition, while the semi-crystalline polymeric material of the first or core portion desirably crystallizes upon further cooling. This allows the extruded roads to resist gravity and the pressures of subsequent layers, while also reducing distortions of 3D model 24.

Support structure 26 is desirably deposited to provide vertical support along the z-axis for overhanging regions of the layers of 3D model 24. This allows 3D object 24 to be built with a variety of geometries. After the build operation is complete, the resulting 3D model 24/support structure 26 may be removed from build chamber 12. Support structure 26 may then be removed from 3D model 24. For example, in embodiments in which the support material is water soluble, the resulting 3D model 24/support structure 26 may be placed in a bath containing an aqueous liquid and/or solution (e.g., an aqueous alkaline solution) to remove support structure 26 from 3D model 24.

FIG. 2 illustrates a segment of filament 34, which is an example of a suitable consumable, semi-crystalline filament of the present disclosure. As shown, filament 34 includes core portion 36 and shell portion 38, which extend along longitudinal length 40. Core portion 36 is the inner portion of filament 34, located around central axis 42, and shell portion 38 is the outer portion of filament 34, located adjacent to outer surface 44. Core portion 36 compositionally includes a first semi-crystalline polymeric material, referred to as a core material. Shell portion 38 compositionally includes a second semi-crystalline polymeric material, referred to as a shell material, where the shell material has a higher crystallization temperature than the core material.

The core and shell materials each include one or more base polymers and, optionally, one or more additives to modify the crystallization temperatures of the base

polymers. Examples of suitable base polymers for use in each of the core and shell materials include polyamides, polyethylenes, polypropylenes, copolymers thereof, and combinations thereof. Suitable polyamides include aliphatic nylon polyamides, such as nylon 6, nylon 6-6, nylon 6-10, nylon 6-12, nylon 10, nylon 10-10, nylon 11, nylon 12, and combinations thereof. Suitable polyethylenes include low-density polyethylene, medium-density polyethylene, high-density polyethylene, and combinations thereof. Suitable polypropylenes include isotactic polypropylenes, syndiotactic polypropylenes, branched and linear variations thereof, and combinations thereof. Unless indicated otherwise, the base polymers for the core and shell materials are not intended to be limited to these listed polymers.

As defined above, the base polymers for the core and shell materials are each capable of achieving an average percent crystallinity in a solid state of at least about 10% by weight. In one embodiment, the base polymer(s) for the core material and/or the shell material is capable of achieving an average percent crystallinity in a solid state of at least about 25% by weight. In another embodiment, the base polymer(s) for the core material and/or the shell material is capable of achieving an average percent crystallinity in a solid state of at least about 50% by weight. The term “percent crystallinity” is defined below with reference to a differential scanning calorimetry (DSC) plot and ASTM D3418-08.

The difference in crystallization temperatures between the core and shell materials may be attained with a variety of different material combinations. In one embodiment, the core and shell materials include different base polymers to attain different crystallization temperatures. For example, core portion 36 may be derived from polyethylene, and shell portion 38 may be derived from an isotactic polypropylene having a crystallization temperature greater than that of the polyethylene of core portion 36.

In another embodiment, the core and shell materials may include base polymers derived from the same or similar monomer units, but have different molecular properties to produce different crystallization temperatures, such as different relative molar masses, different molecular weights, different terminal group chemistries, different stereochemistries, and combinations thereof. For example, core portion 36 may be derived from a highly-branched isotactic polypropylene, and shell portion 38 may be derived from a linear isotactic polypropylene.

In yet another embodiment, the core and shell materials may include the same or similar base polymers, where the core material also includes one or more additives

to decrease its crystallization temperature. For example, the shell material may include a base polymer (e.g., nylon-12 polyamide), and the core material may include the same or similar base polymer (e.g., nylon-12 polyamide) and one or more crystallization inhibitors to decrease the crystallization temperature of the core material relative to the shell material.

Crystallization inhibitors may slow down the crystal growth of the base polymer in the core material by blocking growth sites on the crystal surfaces. Examples of suitable crystallization inhibitors for use in the core material include polyether block amide (PEBA) copolymers, and the like. The crystallization inhibitors may be blended with the base polymer and/or incorporated in the backbone of the base polymer.

Examples of suitable concentrations of crystallization inhibitors in the core material range from about 0.1% by weight to about 20% by weight. In one embodiment, suitable concentrations of crystallization inhibitors in the core material range from about 0.5% by weight to about 15% by weight. In yet another embodiment, suitable concentrations of crystallization inhibitors in the core material range from about 1% by weight to about 10% by weight.

In an additional embodiment, the core and shell materials may include the same or similar base polymers, where the shell material also includes one or more additives to increase its crystallization temperature. For example, the core material may include a base polymer (e.g., nylon-12 polyamide), and the shell material may include the same or similar base polymer (e.g., nylon-12 polyamide) and one or more nucleating agents to increase the crystallization temperature of the shell material relative to the core material.

The nucleating agents may increase the nucleation rate of the base polymer in the shell material, thereby providing higher crystallinity and smaller crystals. This may also render the shell material more transparent to visible light. As such, in some embodiments, the nucleating agents may also function as clarifying agents. Examples of suitable nucleating agents for use in the shell material include silica (e.g., fumed silica), alumina (e.g., fumed alumina), molybdenum disulfide, sodium benzoate, talk, graphite, calcium fluoride, clay, sodium phenylphosphinate, zinc phenylphosphinate, sorbitol-based agents, and combinations thereof.

Example of suitable sorbitol-based agents include those commercially available under the trade designation "MILLARD" from Milliken & Company, Spartanburg, SC, such as "MILLARD 3988" nucleating agent. Additional examples of suitable sorbitol-based agents include those commercially available under the trade

designation "IRGACLEAR" from Ciba Specialty Chemicals, Basel, Switzerland (subsidiary of BASF SE, Ludwigshafen, Germany), such as "IRGACLEAR XT 386" nucleating agent.

Examples of suitable concentrations of the nucleating agents in the shell material of shell portion 38 range from about 0.01% by weight to about 20% by weight. In one embodiment, suitable concentrations of the nucleating agents in the shell material range from about 1% by weight to about 10% by weight. In yet another embodiment, suitable concentrations of the nucleating agents in the shell material range from about 1% by weight to about 5% by weight.

In some embodiments, the base polymer of the core material may be polymerized in a manner such that the core material is free or substantially free of impurities that promote crystallization. For example, the core material is desirably free or substantially free of polymerization catalysts or particulate additives that may promote crystallization, such as providing a polyamide that has been polymerized as an uncatalyzed hydrolytically-polymerized material.

The above-discussed material combinations for the core and shell materials may also be further combined together. For example, the core and shell materials may include the same or similar base polymers, where the core material includes one or more additives to decrease its crystallization temperature, and where the shell material includes one or more additives to increase its crystallization temperature. Accordingly, the core and shell materials may include a variety of compositional combinations to attain a desired difference in crystallization temperatures.

In the shown embodiment, filament 34 has a cylindrical geometry. Core portion 36 has an outer diameter referred to as core diameter 36d, and shell portion 38 has an outer diameter referred to as shell diameter 38d, where shell diameter 38d also corresponds to the outer diameter of filament 34. The relative dimensions for shell diameter 38d to core diameter 36d are desirably selected such that the amount of the shell material that is extruded falls within a balanced range for use in system 10 (shown in FIG. 1).

The amount of the shell material in filament 34 is desirably high enough such that the extruded roads used to build each layer of 3D model 24 (shown in FIG. 1) have sufficient quantities of the shell material (which crystallizes upon deposition in build chamber 12) to resist gravity and the pressures exerted on the extruded roads during the formation of subsequent layers of 3D model 24. On the other end, the amount of the shell material is desirably low enough to prevent substantial distortions of 3D model 24 upon

deposition. The amount of the shell material in filament 34 may be determined by dividing the average volume of shell portion 38 from the overall average volume of filament 34 (i.e., the sum of the average volumes of core portion 36 and shell portion 38). The average diameters, cross-sectional areas, and volumes referred to herein are based on average measurements taken for a suitable segment of filament 34 along longitudinal length 40, such as a distance of 6.1 meters (20 feet).

In embodiments in which core diameter 36d and shell diameter 38d are each substantially uniform along longitudinal length 40, measurements of the volumes of shell portion 38 and filament 34 may be simplified to functions of the respective cross-sectional areas. For cylindrical filament 34, the cross-sectional areas for core portion 36, shell portion 38, and filament 34 may be determined based on core diameter 36d and shell diameter 38d.

Examples of suitable average diameters for core diameter 36d range from about 0.76 millimeters (about 0.03 inches) to about 2.5 millimeters (about 0.10 inches). In one embodiment, suitable average diameters for core diameter 36d range from about 1.0 millimeter (about 0.04 inches) to about 1.5 millimeters (about 0.06 inches). Examples of suitable average diameters for shell diameter 38d range from about 1.0 millimeter (about 0.04 inches) to about 3.0 millimeters (about 0.12 inches). In one embodiment, suitable average diameters for shell diameter 38d range from about 1.0 millimeter (about 0.04 inches) to about 1.5 millimeters (about 0.06 inches). In another embodiment, suitable average diameters for shell diameter 38d range from about 1.5 millimeters (about 0.06 inches) to about 2.0 millimeters (about 0.08 inches).

Correspondingly, examples of suitable average cross-sectional areas for core portion 36 range from about 0.5 square millimeters to about 5 square millimeters. In one embodiment, suitable average cross-sectional areas for core portion 36 range from about 0.75 square millimeters to about 2 square millimeters. Examples of suitable average cross-sectional areas for filament 34 range from about 0.5 square millimeters to about 8 square millimeters. In one embodiment, suitable average cross-sectional areas for filament 34 range from about 1 square millimeter to about 3 square millimeters. In another embodiment, suitable average cross-sectional areas for filament 34 range from about 1 square millimeter to about 2 square millimeters. In yet another embodiment, suitable average cross-sectional areas for filament 34 range from about 2 square millimeters to about 3 square millimeters.

The use of cross-sectional areas is also suitable for determining the cross-sectional dimensions of semi-crystalline filaments of the preset disclosure that have non-cylindrical geometries (e.g., oval, rectangular, triangular, star-shaped, and the like), as discussed below. For example, suitable average cross-sectional areas for the core portion of a non-cylindrical consumable filament of the present disclosure range from about 0.25 square millimeters to about 0.75 square millimeters. Correspondingly, examples of suitable average cross-sectional areas for the non-cylindrical consumable filament range from about 0.5 square millimeters to about 1.5 square millimeters.

Suitable volumes and cross-sectional areas for shell portion 38 may be determined based on these above-discussed suitable cross-sectional areas. Examples of suitable average volumes for shell portion 38 range from about 5% to about 75% of the average volume of filament 34. In one embodiment, suitable average volumes for shell portion 38 range from about 15% to about 65% of the average volume of filament 34. In another embodiment, suitable average volumes for shell portion 38 range from about 25% to about 55% of the average volume of filament 34.

Correspondingly, in embodiments in which core portion 36 and shell portion 38 are each substantially uniform along longitudinal length 40, examples of suitable average cross-sectional areas for shell portion 38 range from about 5% to about 75% of the average cross-sectional area of filament 34. In one embodiment, suitable average cross-sectional areas for shell portion 38 range from about 15% to about 65% of the average cross-sectional area of filament 34. In another embodiment, suitable average cross-sectional areas for shell portion 38 range from about 25% to about 55% of the average cross-sectional area of filament 34.

As further shown in FIG. 2, shell portion 38 extends entirely around core portion 36 along longitudinal length 40. In alternative embodiments, shell portion 38 may extend only partially around core portion 36, such as with a “C” shaped arrangement. In additional alternative embodiments, shell portion 38 may extend partially or fully around core portion 36 in non-contiguous segments along longitudinal length 40. These alternative embodiments are suitable for modifying the feed mechanics of filament 34 through system 10, and for attaining desired volume fractions of the shell material.

Filament 34 may be manufactured with a co-extrusion process, where the core and shell materials may be separately compounded and co-extruded to form filament 34. While core portion 36 and shell portion 38 are illustrated in FIG. 2 as having a defined

interface, it is understood that the core and shell materials may at least partially interdiffuse at this interface due to the co-extrusion process. After formation, filament 34 may be wound onto a spool or be otherwise packaged for use with system 10 (e.g., within supply source 20).

While the consumable, semi-crystalline filaments of the present disclosure are discussed herein as having a core portion and one or more shell portions, the semi-crystalline filaments of the present disclosure may alternatively include different arrangements of the multiple semi-crystalline polymeric materials, such that each semi-crystalline filament includes a first portion that compositionally includes a first semi-crystalline polymeric material, and a second portion that compositionally includes a second semi-crystalline polymeric material having a higher crystallization temperature than the first semi-crystalline polymeric material.

For example, in one embodiment, the semi-crystalline filament may be manufactured to provide a gradual or step-wise gradient of the semi-crystalline filament materials between a central axis and an outer surface. In this embodiment, the semi-crystalline filament materials may be highly interdiffused to provide a gradual interface between a first portion (e.g., a core portion) and second portion (e.g., a shell portion). At the central axis, the composition of the semi-crystalline filament desirably includes a first semi-crystalline polymeric material (e.g., a core material), and at the outer surface, the composition of the semi-crystalline filament desirably includes only a second semi-crystalline polymeric material (e.g., a shell material). Inbetween the central axis and the outer surface, the concentration of the second semi-crystalline polymeric material may gradually increase in an outward direction from the central axis to the outer surface.

FIGS. 3 and 4 respectively illustrate DSC plots of heat flow versus temperature during cooling stages for the shell and core materials of filament 34. As discussed above, the shell material of shell portion 38 has a higher crystallization temperature than the core material of core portion 36. DSC provides a suitable technique for measuring the percent crystallinities, the crystallization temperatures, and the melting temperatures for the core and shell materials, where the DSC plots referred to herein are measured pursuant to ASTM D3418-08.

As shown in FIG. 3, after being heated beyond its melting temperature and allowed to cool, the shell material of shell portion 38 generates DSC plot 46. In particular, as the measured temperature drops, as indicated by arrow 48, the heat flow remains

substantially constant until the crystallization onset temperature of the shell material is reached. At this point, the shell material crystallizes and releases heat, as indicated by exothermic crystallization peak 50. After crystallizing, the shell material then cools down further, as indicated by arrow 52.

Peak 50 may be used to determine the crystallization temperature of the shell material, where the crystallization temperature of the shell material may be identified by a peak crystallization temperature or a slope-intercept crystallization temperature. As used herein, the term “peak crystallization temperature” refers to a temperature corresponding to a peak point of an exothermic crystallization peak on a DSC plot, and corresponds to the maximum rate of crystallization for the shell material. For example, as shown in FIG. 3, peak 50 has a peak point 54 at temperature T1. Thus, temperature T1 is the peak crystallization temperature for the shell material of shell portion 38.

As used herein, the term “slope-intercept crystallization temperature” refers to a temperature corresponding to a point at which the slope of the rising curve of an exothermic crystallization peak on a DSC plot intersects with a baseline of the exothermic crystallization peak. The rising curve of an exothermic crystallization peak is based on the measured heat flow as the material begins to crystallize from the molten state. For example, as shown in FIG. 3, peak 50 for the shell material includes rising curve 56 and baseline 58, where rising curve 56 has a slope defined by line 60. Line 60 intersects baseline 58 at intersection point 62, which is located at temperature T2. Thus, temperature T2 is the slope-intercept crystallization temperature for the shell material of shell portion 38.

Correspondingly, as shown in FIG. 4, after being heated beyond its melting temperature and allowed to cool, the core material of core portion 36 generates DSC plot 64. In particular, as the measured temperature drops, as indicated by arrow 66, the heat flow remains substantially constant until the crystallization onset temperature of the core material is reached. At this point, the core material crystallizes and releases heat, as indicated by exothermic crystallization peak 68. After crystallizing, the core material then cools down further, as indicated by arrow 70.

Peak 68 may be used to determine the crystallization temperature of the core material in the same manner as peak 50 for the shell material, where the crystallization temperature of the core material may also be identified by a peak crystallization temperature or a slope-intercept crystallization temperature. For example, as shown in FIG. 4, peak 68 has a peak point 72 at a temperature T3. Thus, temperature T3 is the peak crystallization



temperature for the core material of core portion 36. Furthermore, peak 68 for the core material includes rising curve 74 and baseline 76, where rising curve 74 has a slope defined by line 78. Line 78 intersects baseline 76 at intersection point 80, which is located at temperature T4. Thus, temperature T4 is the slope-intercept crystallization temperature for the core material of core portion 36.

A comparison of FIGS. 3 and 4 show that as the temperatures cool down from the molten states of the materials, the shell material begins to crystallize prior to the crystallization of the core material. As such, at the crystallization temperature of the shell material (e.g., temperatures T1 and T2), the core material remains in a non-crystallized or substantially non-crystallized state until the temperature cools down to the crystallization temperature of the core material (e.g., temperatures T3 and T4). When the crystallization temperature of the core material is reached, the core material then crystallizes. This difference in crystallization temperatures desirably reduces distortions, internal stresses, and sagging of the core and shell materials when deposited as extruded roads to form layers of 3D model 24 (shown in FIG. 1).

Measurements based on peak crystallization temperatures typically provide greater differences between the crystallization temperatures of the shell and core materials compared to measurements based on slope-intercept crystallization temperatures. Examples of suitable differences in peak crystallization temperatures between the shell and core materials (e.g., between temperatures T1 and T3) include temperatures of at least about 2°C. In one embodiment, suitable differences in peak crystallization temperatures between the shell and core materials include temperatures of at least about 5°C. In another embodiment, suitable differences in peak crystallization temperatures between the shell and core materials include temperatures of at least about 10°C. In yet another embodiment, suitable differences in peak crystallization temperatures between the shell and core materials include temperatures of at least about 15°C.

Examples of suitable differences in slope-intercept crystallization temperatures between the shell and core materials (e.g., between temperatures T2 and T4) include temperatures of at least about 3°C. In one embodiment, suitable differences in slope-intercept crystallization temperatures between the shell and core materials include temperatures of at least about 5°C. In another embodiment, suitable differences in slope-intercept crystallization temperatures between the shell and core materials include temperatures of at least about 8°C.

In some embodiments, it is desirable to maintain the difference in the crystallization temperatures at an even greater difference to provide less stringent operating parameters in system 10. For example, suitable differences in peak crystallization temperatures between the shell and core materials include temperatures of at least about 20°C. In one embodiment, suitable differences in peak crystallization temperatures between the shell and core materials include temperatures of at least about 30°C. In another embodiment, suitable differences in peak crystallization temperatures between the shell and core materials include temperatures of at least about 40°C.

In other embodiments, it is desirable to maintain the difference in the crystallization temperatures below an upper threshold. Accordingly, examples of suitable differences in peak crystallization temperatures between the shell and core materials also include temperatures less than about 25°C. In one embodiment, suitable differences in peak crystallization temperatures between the shell and core materials include temperatures less than about 20°C. Correspondingly, examples of suitable differences in slope-intercept crystallization temperatures between the shell and core materials also include temperatures less than about 20°C. In one embodiment, suitable differences in slope-intercept crystallization temperatures between the shell and core materials include temperatures less than about 15°C.

The DSC plots may also be used to determine the percent crystallinity of the shell and core materials, which is known to those skilled in the art. For example, peak 50 (shown in FIG. 3) maybe used to determine the enthalpy of fusion for base polymer of the shell material. The enthalpy of fusion for the base polymer of the shell material may then be normalized to the enthalpy of fusion of a 100% crystalline polymer corresponding to the base polymer of the shell material, to determine the percent crystallinity of the base polymer in shell portion 38. Similarly, peak 68 (shown in FIG. 4) maybe used to determine the enthalpy of fusion for the base polymer of the core material. The enthalpy of fusion for the base polymer of the core material may then be normalized to the enthalpy of fusion of a 100% crystalline polymer corresponding to the base polymer of the core material, to determine the percent crystallinity of the base polymer in core portion 36.

Furthermore, the melting temperatures of the core and shell materials are desirably the same or similar to allow filament 34 to be readily melted in a liquefier of extrusion head 18. As such, the core material and the shell material may be selected to minimize the differences in melting temperatures. DSC also provides a suitable technique

for measuring the melting temperatures for the core and shell materials, where the melting temperatures may also be identified by peak melting temperatures or slope-intercept melting temperatures.

As used herein, the “peak melting temperature” refers to a temperature corresponding to a peak point of an endothermic melting peak on a DSC plot (not shown in FIGS. 3 or 4). Correspondingly, the “slope-intercept melting temperature” refers to a temperature corresponding to a point at which the slope of the rising curve of an endothermic melting peak on a DSC plot intersects with a baseline of the endothermic melting peak. The rising curve of an endothermic melting peak is based on the measured heat flow as the material begins to melt from the solid state.

Examples of suitable differences in peak melting temperatures include temperatures of about 8°C or less. In one embodiment, suitable differences in peak melting temperatures include temperatures of about 3°C or less. Examples of suitable differences in slope-intercept melting temperatures include temperatures of about 10°C or less. In one embodiment, suitable differences in slope-intercept melting temperatures include temperatures of about 5°C or less.

FIG. 5 illustrates a build operation to build 3D model 24 (shown in FIG. 1) from the semi-crystalline polymeric materials of filament 34 (shown in FIG. 2). As discussed above, during a build operation with system 10 (shown in FIG. 1), filament 34 is fed to extrusion head 18 in a solid state from supply source 20. While passing through extrusion head 18, filament 34 is heated in a liquefier to a temperature that is greater than the melting temperatures of the shell and core materials. The molten materials are then deposited onto platen 14 from extrusion tip 82 of extrusion head 18 in a series of extruded roads to form layers 84 of 3D model 24. One or more layers of a support material (not shown) may also be deposited below layers 84 to facilitate the removal of 3D model 24 from platen 14.

In the shown example, the extruded roads of the core and shell materials may at least partially retain their core/shell cross-sectional profile from filament 34. For example, top extruded road 86 includes core region 88 of the core material and shell region 90 of the shell material, where shell region 90 may extend around and encase core region 88. In one embodiment, at least a portion of the extruded roads at least partially retain their core/shell cross-sectional profile from filament 34. In a further embodiment, substantially

all of the extruded roads at least partially retain their core/shell cross-sectional profile from filament 34.

While not wishing to be bound by theory, it is believed that a substantially laminar flow of the molten core and shell materials through a liquefier of extrusion head 18 may allow the extruded roads (e.g., road 86) to at least partially retain their core/shell profile. It is understood that interdiffusion of the molten core and shell materials may occur at the interface between core region 88 and shell region 90. As such, the resulting extruded roads (e.g., road 86) may exhibit a cross-sectional profile that is the same or substantially similar to that of filament 34 (as shown in FIG. 2), may exhibit a blend of the core and shell materials, or may exhibit a cross-sectional profile that is a variation between these two profiles (e.g., a profile in which the core and shell materials are partially interdiffused).

As discussed above, build chamber 12 is desirably heated to one or more suitable temperatures to allow the extruded roads to crystallize in two stages. In one embodiment, the envelope of build chamber 12 may be heated and maintained at one or more temperatures that are about equal to, or within a small range above or below, the crystallization temperature of the shell material. For example, the envelope of build chamber 12 may be heated and maintained at one or more temperatures that are about equal to, or are within about 20°C above or below, the peak crystallization temperature of the shell material, since the shell material may begin crystallizing over a temperature range around its peak crystallization temperature. In this embodiment, the temperature(s) of build chamber 12 are also desirably greater than the crystallization temperature of the core material, at least at the upper region of build chamber 12, adjacent to extrusion head 18.

Upon being deposited into build chamber 12, the molten core and shell materials of road 86 cool from the elevated liquefier temperature within extrusion head 18 to the temperature(s) of build chamber 12. This desirably cools road 86 to or below the crystallization temperature of the shell material, but above the crystallization temperature of the core material, thereby allowing the shell material to at least partially crystallize, while preventing the core material from substantially crystallizing. While not wishing to be bound by theory, it is believed that when the shell material solidifies to form shell region 90 of extruded road 86, the latent heat of transformation emitted from the shell material is at least partly absorbed by the core material, thereby reducing the rate at which core region 88 crystallizes relative to shell region 90. It is further believed that this provides good

interlayer fusing, which results in good interlayer z-bond strengths (i.e., good interlayer bonds along the vertical z-axis).

The shell material of core region 90 desirably crystallizes in less time than is required to build a single layer of 3D model 24, such that the shell material exhibits at least about 30% crystallinity prior to the deposition of a subsequent layer, and more desirably at least about 50% crystallinity. In comparison, the core material of core region 88 desirably crystallizes more slowly such that shrinkage may occur after the formation of one or more subsequent layers. For example, the core material may exhibit less than about 10% crystallinity prior to the deposition of a subsequent layer, more desirably less than about 5% crystallinity.

This difference in crystallization rates within build chamber 12, due to the difference in crystallization temperatures of the core and shell materials, allows the shell material to crystallize upon deposition. This allows road 86 to resist gravity and the pressures of subsequently deposited layers. While the crystallized portions of shell region 90 contract, the non-crystallized core material of core region 88 prevents road 86 from fully contracting and distorting, which would otherwise occur with an extruded road derived from a single semi-crystalline material.

In an alternative embodiment, the envelope of build chamber 12 may be maintained at one or more temperatures that define a temperature gradient that decreases in a downward direction along the vertical z-axis. For example, the upper region of build chamber 12 may be heated and maintained at one or more temperatures that are about equal to, or within a small range above or below, the crystallization temperature of the shell material. The lower region of build chamber 12, however, may be maintained at one or more lower temperatures. For example, the lower region of build chamber 12 may be heated and maintained at one or more temperatures that are about equal to, or within a small range above or below, the crystallization temperature of the core material. As platen 14 lowers downward in an incremental manner along the vertical z-axis, the gradual or stepwise cooling may allow the core material to slowly crystallize over time as subsequent layers are built.

Instead, the above-discussed suitable volume fractions of the shell material provide a balance that allows crystallized shell region 90 to support subsequently deposited layers, while also reducing or minimizing the shrinkage of road 86. As road 86 subsequently cools down below the crystallization temperature of the core material, the core

material may then gradually crystallize to fully solidify road 86. As such, this two-stage crystallization desirably reduces distortions, internal stresses, and sagging of the semi-crystalline polymeric materials when deposited as extruded roads to form the layers of 3D model 24.

In an alternative embodiment, to the core and shell materials of filament 34 may be switched such that the core material has a crystallization temperature that is greater than a crystallization temperature of the shell material. In this embodiment, upon deposition in build chamber 12, the core portion may crystallize prior to the shell portion, such as with an “islands in the sea” geometry with the islands nucleating and crystallizing prior to the crystallization of the shell material.

FIG. 6A illustrates filament 134, which is another example of a suitable consumable, semi-crystalline filament of the present disclosure. Filament 134 is similar to filament 34 (shown in FIG. 2), where the respective reference labels are increased by “100”. As shown in FIG. 6A, shell portion 138 of filament 134 is a multi-shell portion that includes inner shell 192 and outer shell 194. In this embodiment, inner shell 192 and outer shell 194 each desirably includes a semi-crystalline polymeric material, which provides further individual tailoring of the desired crystallization characteristics.

Suitable materials for each of inner shell 192 and outer shell 194 include those discussed above for shell portion 38 (shown in FIG. 2). For example, the semi-crystalline polymeric material of inner shell 192 may have a crystallization temperature that is between the crystallization temperatures of core portion 136 and outer shell 194. This may allow a stair-step crystallization gradient to be achieved in build chamber 12 (shown in FIG. 1). Alternatively, inner shell 192 may include a material that restricts or prevents interdiffusion and/or crystal growth between the materials of core portion 136 and outer shell 194. In this alternative embodiment, suitable materials for inner shell 192 may include one or more amorphous polymers.

Suitable dimensions for inner shell 192 and outer shell 194 may vary depending on the particular materials used. In some embodiments, the combined dimensions of inner shell 192 and outer shell 194 may include the suitable dimensions discussed above for shell portion 38. Accordingly, the consumable materials of the present disclosure may include two or more layers to attain desired crystallization growth characteristics for use in building 3D models with layer-based additive manufacturing techniques.

Additionally, the core portions of the semi-crystalline filaments may vary from the embodiments discussed above for filaments 34 and 134. For example, in some embodiments, the core portions (e.g., core portions 36 and 136) may be located off-axis from the central axis of the semi-crystalline filament. In additional alternative embodiments, the geometries of the core portions may be non-cylindrical (e.g., oval, rectangular, triangular, and the like) and/or hollow to modify the crystallization characteristics of the resulting extruded roads.

For example, as shown in FIG. 6B, filament 234 is similar to filament 34 (shown in FIG. 2), where the respective reference labels are increased by “200”. As shown in FIG. 6B, filament 234 includes a non-cylindrical cross-sectional geometry with core portion 236 and shell portion 238 each having a rectangular cross-sectional geometry. Examples of suitable materials for core portion 236 and shell portion 238 include those discussed above for core portion 36 and shell portion 38 (shown in FIG. 2).

Suitable cross-sectional areas include those discussed above. For example, suitable average cross-sectional areas for core portion 236 range from about 0.25 square millimeters to about 0.75 square millimeters. Correspondingly, examples of suitable average cross-sectional areas for filament 234 range from about 0.5 square millimeters to about 1.5 square millimeters. In addition, the multiple-layered shell embodiment of filament 134 (shown in FIG. 6A) may also be applied to filament 234 to provide a non-cylindrical, semi-crystalline filament having multiple shell layers.

## EXAMPLES

The present disclosure is more particularly described in the following examples that are intended as illustrations only, since numerous modifications and variations within the scope of the present disclosure will be apparent to those skilled in the art. Unless otherwise noted, all parts, percentages, and ratios reported in the following examples are on a weight basis, and all reagents used in the examples were obtained, or are available, from the chemical suppliers described below, or may be synthesized by conventional techniques.

### I. Examples 1 and 2

Consumable, semi-crystalline filaments of Examples 1 and 2 were coextruded in a core and shell arrangement corresponding to filament 34 (shown in FIG. 2).

The core material of the core portion included nylon-12 polyamide commercially available under the trade designation “GRILAMID L16” from EMS-Grivory, a unit of EMS-CHEMIE North America, Inc., Sumter, SC. The shell material of the shell portion included a blend of the nylon-12 polyamide and a nucleating agent, which was commercially available under the trade designation “GRILAMID L16-LM” from EMS-Grivory, a unit of EMS-CHEMIE North America, Inc., Sumter, SC. The nucleating agent also functioned as a clarifying agent. The shell material was also dyed with a black colorant to visibility distinguish the core portion from the shell portion.

FIGS. 7 and 8 are photographs of cross-sectional segments of the semi-crystalline filaments of Examples 1 and 2, respectively. The shell portions of the semi-crystalline filaments are shown with darker shade due to the colorant dyes. The core portions of the semi-crystalline filaments are shown with lighter shades.

The semi-crystalline filaments of Examples 1 and 2 were coextruded with varying feed rates to vary the volume fractions for the shell portions. The filament of Example 1 (shown in FIG. 7) had an average shell portion volume fraction of about 29%, and the filament of Example 2 (shown in FIG. 8) had an average shell portion volume fraction of about 43%.

FIGS. 9 and 10 are respective DSC plots of the shell and core materials used to form the filaments of Examples 1 and 2. The DSC plots were measured using a differential scanning calorimeter commercially available under the trade designation “DSC Q2000” from TA Instruments, New Castle, DE, with a nitrogen atmosphere introduced at 50 cubic-centimeters/minute, and a heat increase rate of 10°C/minute. The sample size of the shell material was 5.1 milligrams, and the sample size of the core material was 5.9 milligrams.

As shown in the bottom plot of FIG. 9, during a heating phase, the shell material generated an endothermic melting peak, from which the peak melting temperature (about 179°C) and the slope-intercept melting temperature (about 172°C) were calculated. After melting, the shell material was allowed to cool down, as illustrated in the top plot of FIG. 9. While cooling down, the shell material generated an exothermic crystallization peak, from which the peak crystallization temperature (about 162°C) and the slope-intercept crystallization temperature (about 163°C) were calculated.

As shown in the bottom plot of FIG. 10, during a heating phase, the core material generated an endothermic melting peak, from which the peak melting temperature



(about 180°C) and the slope-intercept melting temperature (about 174°C) were calculated. After melting, the core material was allowed to cool down, as illustrated in the top plot of FIG. 10. While cooling down, the core material generated an exothermic crystallization peak, from which the peak crystallization temperature (about 144°C) and the slope-intercept crystallization temperature (about 153°C) were calculated.

The calculated results from the DSC plots in FIGS. 9 and 10 provided a difference in the peak melting temperatures of about 1°C, a difference in the slope-intercept melting temperatures of about 2°C, a difference in the peak crystallization temperatures of about 18°C, and a difference in the slope-intercept crystallization temperatures of about 10°C. Accordingly, the inclusion of the nucleating agent in the shell material raised the crystallization temperature of the base polymer of the shell material (i.e., nylon-12 polyamide) relative to the same base polymer of the core material. As such, the shell and core materials of the semi-crystalline filaments of Examples 1 and 2 were suitable for crystallization in two stages.

Furthermore, the shell and core materials exhibited similar melting temperatures, thereby allowing both the shell and core materials to be readily melted within a liquefier of an extrusion head. This combination of a two-stage crystallization with similar melting temperatures renders the semi-crystalline filaments of Examples 1 and 2 suitable for extrusion from an extrusion-based layered deposition system to build 3D models that desirably have reduced levels of curling and distortion. As such, the 3D models may be built with semi-crystalline polymeric materials while maintaining dimensional accuracies.

The semi-crystalline filaments of Examples 1 and 2 were then used to build 3D models. FIGS. 11 and 12 are photographs of 3D models built with the exemplary semi-crystalline filaments. The 3D model shown in FIG. 11 was a cylinder having a diameter of 6 inches and a height of 8 inches. The 3D model shown in FIG. 12 had a star-shaped geometry. Each 3D model was built in an extrusion-based additive manufacturing system commercially available from Stratasys, Inc., Eden Prairie, MN under the trade designation "FDM TITAN". The filaments were melted in an extrusion head liquefier of the system at a set temperature range of 240°C to 255°C, which was greater than the melting temperatures of the core and shell materials.

The molten materials were then extruded and deposited into a build chamber envelope maintained at a temperature range of about 160°C to 180°C. This envelope

temperature was close to the peak crystallization temperatures of the shell materials of the filaments, and greater than the peak crystallization temperatures of the core materials of the filaments. This allowed the deposited materials to crystallize in two stages, as discussed above, where the shell materials began crystallizing upon deposition and the core materials crystallized at later points in time, such as when the 3D models were removed from the build chamber.

As shown in FIGS. 11 and 12, the 3D models were built with reduced levels of curling and distortion, and maintained dimensional accuracies. Furthermore, the 3D models were black in color from the black colorant of the shell material. This shows that the extruded roads of the molten materials retained their core/shell cross-sectional profile, as discussed above for core region 88 and shell region 90 of extruded road 86 (shown in FIG. 5). The 3D models also exhibited good interlayer z-bond strengths, which is believed to be due to the reduced rate at which the core material crystallized relative to the shell material.

## II. Example 3

Consumable, semi-crystalline filaments of Example 3 were also coextruded in a core and shell arrangement corresponding to filament 34 (shown in FIG. 2). The core material of the core portion included nylon-12 polyamide commercially available under the trade designation "GRILAMID L20" from EMS-Grivory, a unit of EMS-CHEMIE North America, Inc., Sumter, SC. The shell material of the shell portion included a blend of the nylon-12 polyamide and a nucleating agent, where the nucleating agent also functioned as a clarifying agent. In this example, the shell material was dyed with an orange colorant. The shell material had a peak-crystallization temperature of about 170°C, and the core material had a peak-crystallization temperature of about 142°C.

The semi-crystalline filament of Example 3 was then used to build 3D models. FIGS. 13-16 are photographs of 3D models built with the exemplary semi-crystalline filaments. Each 3D model was built in an extrusion-based additive manufacturing system commercially available from Stratasys, Inc., Eden Prairie, MN under the trade designation "FDM TITAN". The filaments were melted in an extrusion head liquefier of the system at a set temperature range of 240°C to 255°C, which was greater than the melting temperatures of the core and shell materials.

The molten materials were then extruded and deposited into a build chamber envelope maintained at a temperature range of about 170°C. This envelope temperature

was about equal to the peak crystallization temperature of the shell material of the filament, and greater than the peak crystallization temperature of the core materials of the filament. This allowed the deposited materials to crystallize in two stages, as discussed above, where the shell materials began crystallizing upon deposition and the core materials crystallized at later points in time, such as when the 3D models were removed from the build chamber.

As shown in FIGS. 13-16, these 3D models were also built with reduced levels of curling and distortion, and maintained dimensional accuracies. Furthermore, the 3D models were orange in color from the orange colorant of the shell material. This shows that the extruded roads of the molten materials retained their core/shell cross-sectional profile, as discussed above for core region 88 and shell region 90 of extruded road 86 (shown in FIG. 5). The 3D models also exhibited good interlayer z-bond strengths, which, as discussed above, is believed to be due to the reduced rate at which the core material crystallized relative to the shell material.

Although the present disclosure has been described with reference to several embodiments, workers skilled in the art will recognize that changes may be made in form and detail without departing from the spirit and scope of the disclosure.

## CLAIMS:

1. A consumable filament for use in an extrusion-based additive manufacturing system, the consumable filament comprising:
  - a first portion extending along a longitudinal length of the consumable filament, the first portion compositionally comprising a first semi-crystalline polymeric material having a first peak crystallization temperature; and
  - a second portion extending along the longitudinal length of the consumable filament and at least partially encasing the first portion, the second portion compositionally comprising a second semi-crystalline polymeric material having a second peak crystallization temperature that is greater than the first peak crystallization temperature, wherein the consumable filament has an average cross-sectional area ranging from about 0.5 square millimeters to about 8 square millimeters, and wherein the second portion has an average volume ranging from about 5% to about 50% of an average volume of the consumable filament.
2. The consumable filament of claim 1, wherein the second peak crystallization temperature is greater than the first peak crystallization temperature by at least about 5°C.
3. The consumable filament of claim 2, wherein the first portion and the second portion are coextruded portions.
4. The consumable filament of claim 1, wherein the average volume of the second portion ranges from about 5% to about 75% of the average volume of the consumable filament.
5. The consumable filament of claim 1, wherein the average cross-sectional area of the consumable filament ranges from about 1 square millimeter to about 3 square millimeters.
6. The consumable filament of claim 1, wherein the first semi-crystalline polymeric material and the second semi-crystalline polymeric material have substantially the same peak melting temperatures.
7. The consumable filament of claim 1, wherein the first semi-crystalline polymeric material and the second semi-crystalline polymeric material each comprise a

polymer selected from the group consisting of polyamides, polyethylenes, polypropylenes, copolymers thereof, and combinations thereof.

8. The consumable filament of claim 7, wherein the second portion comprises an inner shell and an outer shell, the inner shell being disposed between the first portion and the outer shell.

9. The consumable filament of claim 7, wherein the first semi-crystalline polymeric material comprises a first base polymer, and the second semi-crystalline polymeric material comprises a second base polymer that is substantially the same as the first base polymer, and wherein at least one of the first semi-crystalline polymeric material and the second semi-crystalline polymeric material further comprises one or more additives to promote a difference in the first peak crystallization temperature and the second peak crystallization temperature.

10. A three-dimensional object built with an extrusion-based additive manufacturing system, the three-dimensional object comprising:

a plurality of solidified layers each comprising roads extruded with the extrusion-based additive manufacturing system from a consumable filament having a core portion and a shell portion, wherein the core portion compositionally comprises a first semi-crystalline polymeric material having a first peak crystallization temperature, and the shell portion comprising a second semi-crystalline polymeric material having a second peak crystallization temperature that is greater than the first peak crystallization temperature;

wherein at least a portion of the roads of the plurality of solidified layers at least partially retain cross-sectional profiles corresponding to the core portion and the shell portion of the consumable filament.

11. The three-dimensional object of claim 10, wherein the first semi-crystalline polymeric material and the second semi-crystalline polymeric material each comprise nylon-12 polyamide.

12. The three-dimensional object of claim 11, wherein the second semi-crystalline polymeric material further comprises a nucleating agent.

13. The three-dimensional object of claim 10, wherein the second peak crystallization temperature is greater than the first peak crystallization temperature by at

least about 10°C, and wherein the shell portion and the core portion have substantially the same peak melting temperatures.

14. The three-dimensional object of claim 10, wherein substantially all of the roads of the plurality of solidified layers at least partially retain cross-sectional profiles corresponding to the core portion and the shell portion of the consumable filament.

15. A method for building a three-dimensional object with an additive manufacturing system having a heated build chamber and an extrusion head, the method comprising:

feeding a consumable filament to the extrusion head, the consumable filament comprising a first portion and a second portion at least partially encasing the first portion, wherein the first portion compositionally comprises a first semi-crystalline polymeric material, and wherein the second portion compositionally comprises a second semi-crystalline polymeric material having a peak crystallization temperature that is greater than a peak crystallization temperature of the first semi-crystalline polymeric material;

melting the fed consumable filament in the extrusion head to form a molten material;

depositing the molten material in the heated build chamber as an extruded road that defines at least a portion of a layer of the three-dimensional object, wherein the extruded road compositionally comprises the first semi-crystalline polymeric material and the second semi-crystalline polymeric material;

crystallizing at least a portion of the second semi-crystalline polymeric material of the extruded road prior to formation of a subsequent layer of the three-dimensional object; and

crystallizing at least a portion of the first semi-crystalline polymeric material of the extruded road after crystallizing the portion of the second semi-crystalline polymeric material.

16. The method of claim 15, wherein the peak crystallization temperature of the second semi-crystalline polymeric material is greater than the peak crystallization temperature of the first semi-crystalline polymeric material by at least about 5°C.

17. The method of claim 15, wherein the semi-crystalline filament has an average cross-sectional area ranging from about 0.5 square millimeters to about 8 square millimeters.
18. The method of claim 17, wherein the second portion has an average volume ranging from about 5% to about 75% of an average volume of the consumable filament.
19. The method of claim 15, wherein the second semi-crystalline polymeric material exhibits at least about 30% crystallinity prior to the formation of the subsequent layer of the three-dimensional object, and wherein the first semi-crystalline polymeric material exhibits less than about 10% crystallinity prior to the formation of the subsequent layer of the three-dimensional object.
20. The method of claim 15, and further comprising maintaining an environment within the heated build chamber at one or more temperatures that are about equal to, or are within a range of about 10°C above or below, the peak crystallization temperature of the second semi-crystalline polymeric material.

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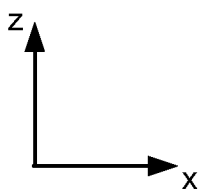
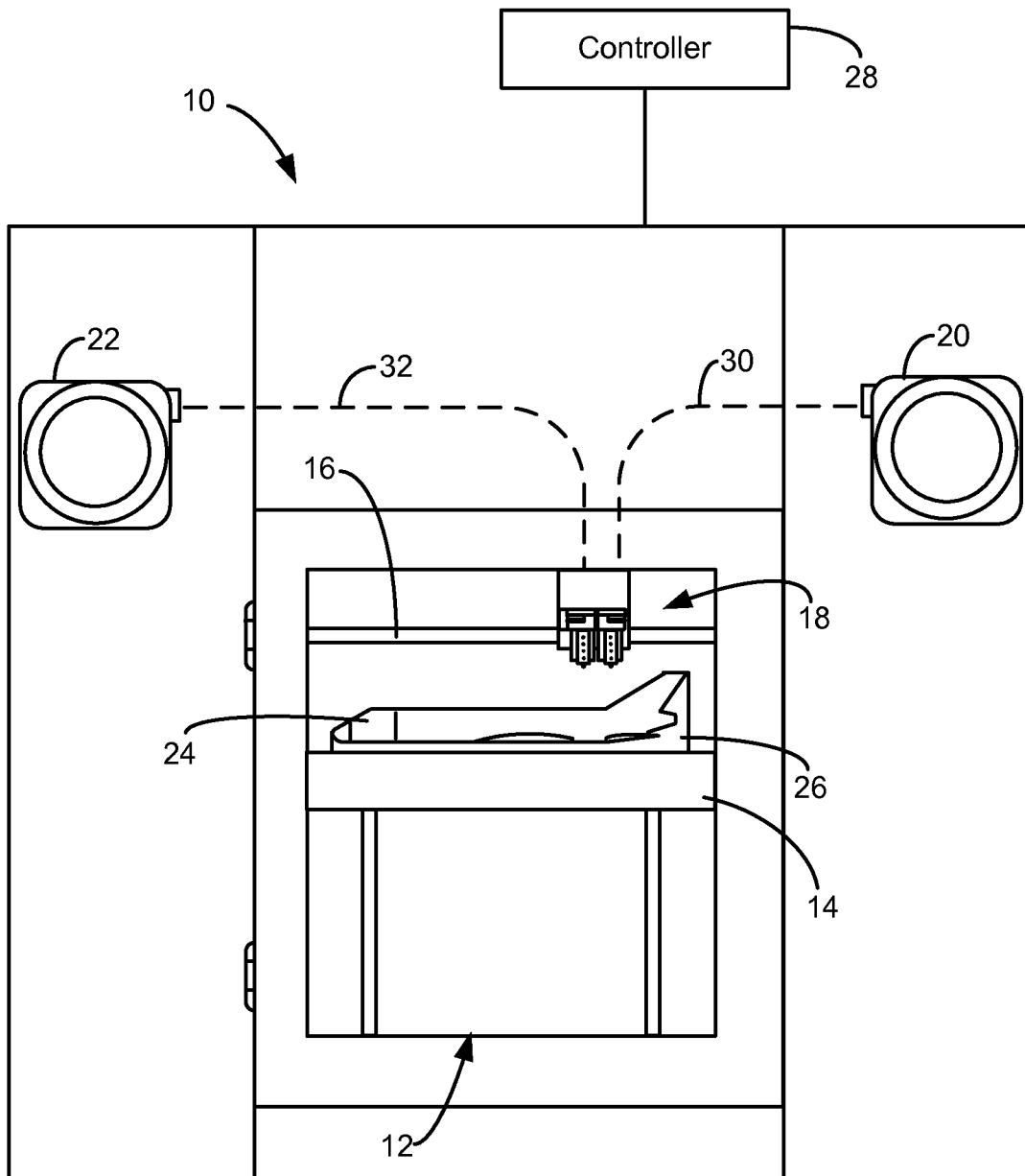


FIG. 1



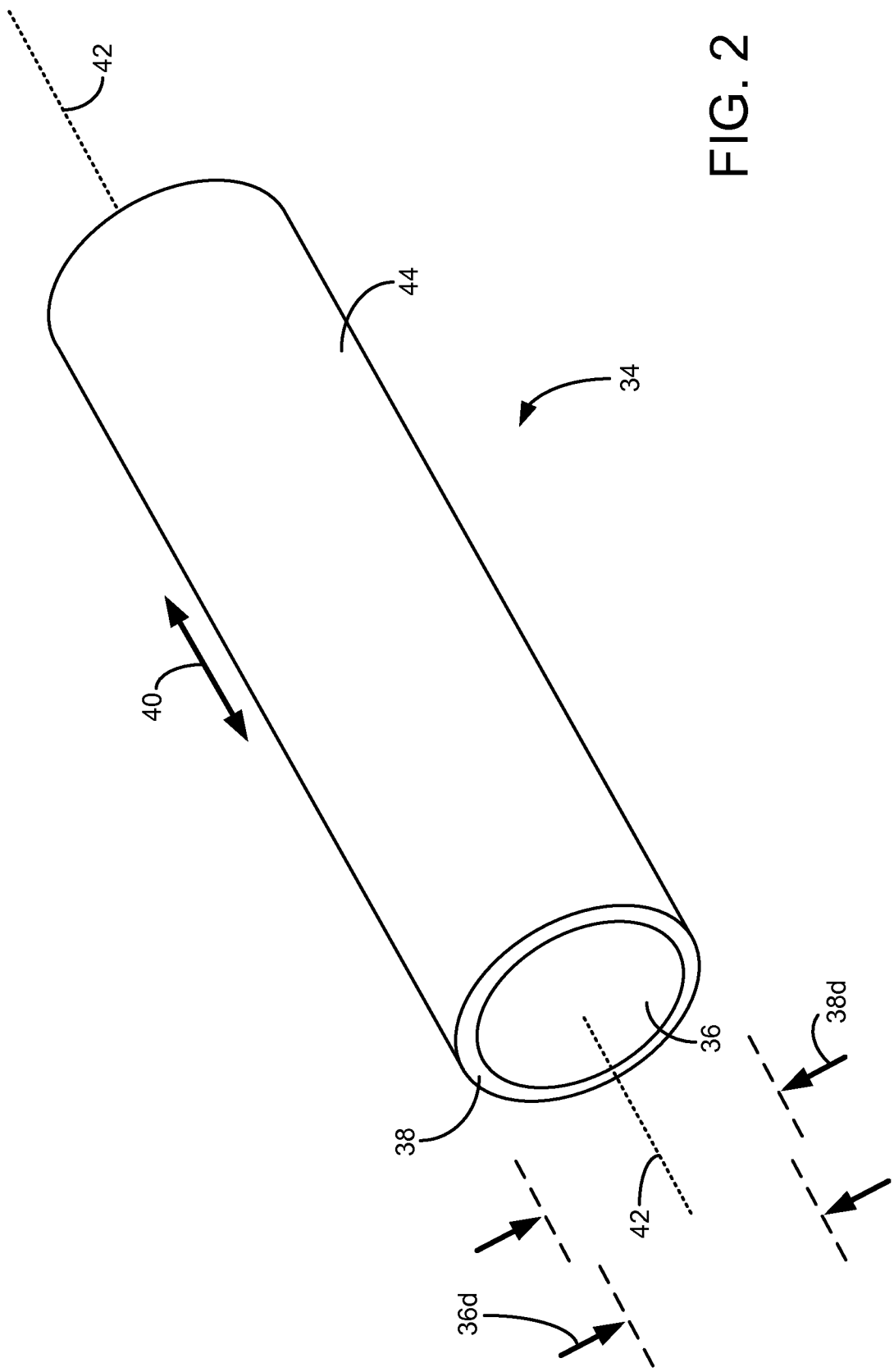
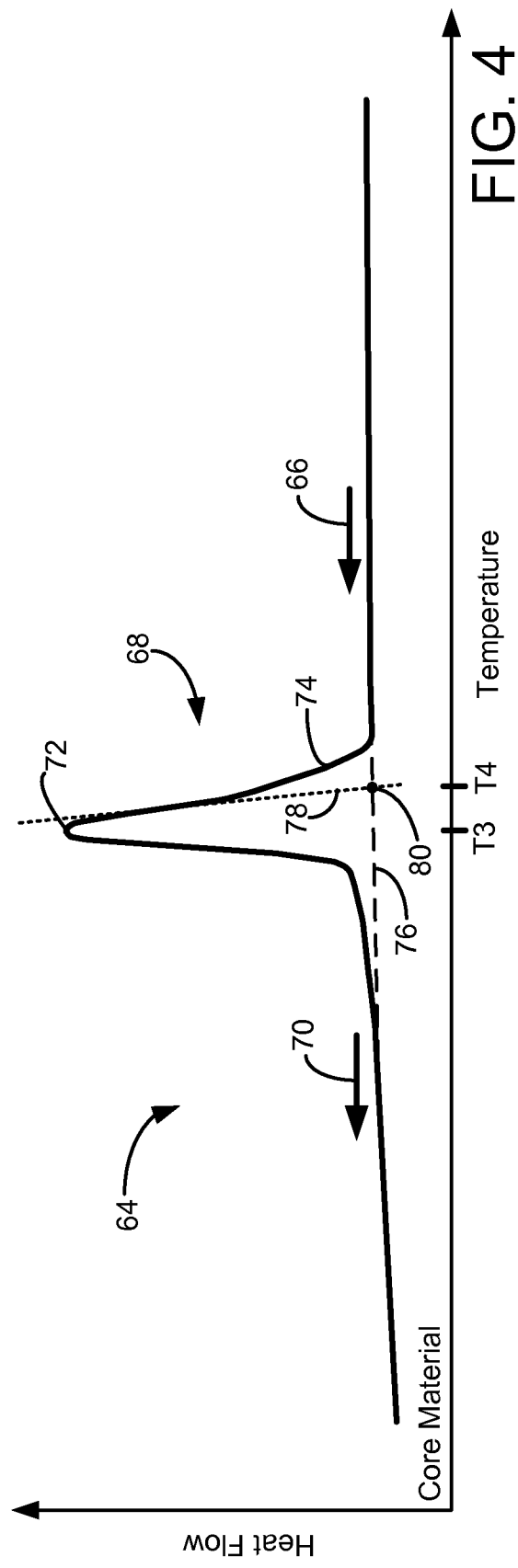
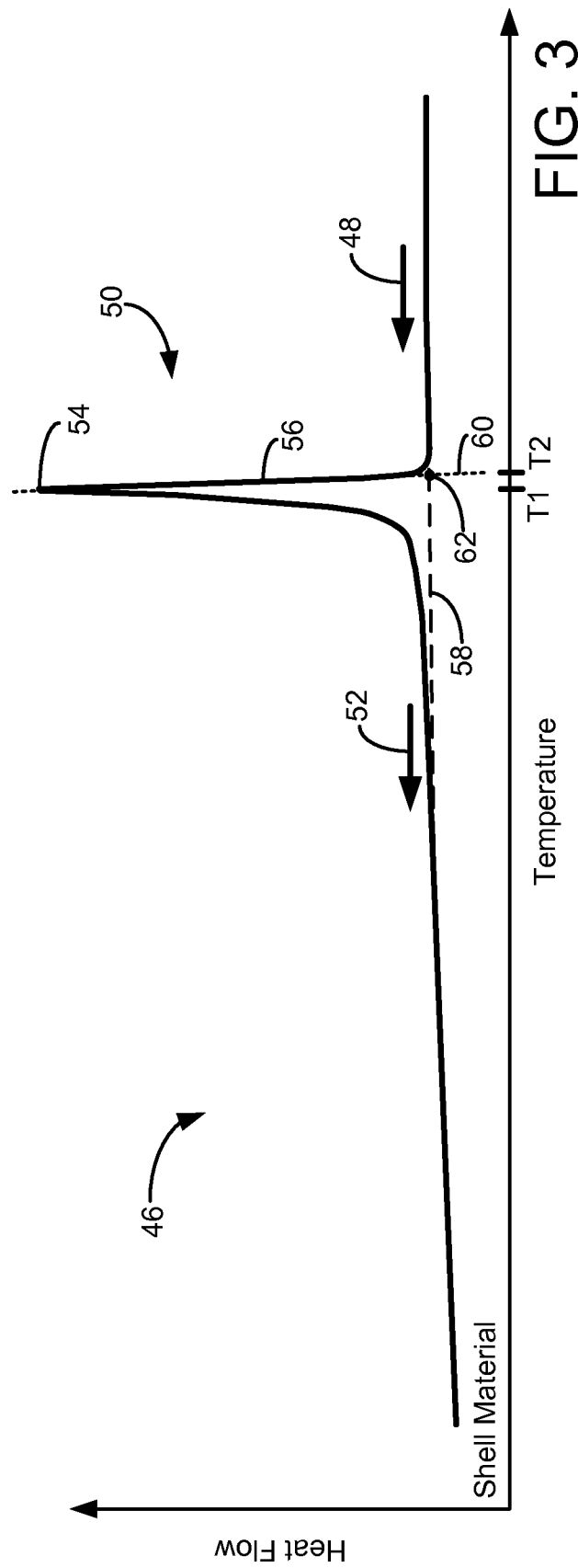
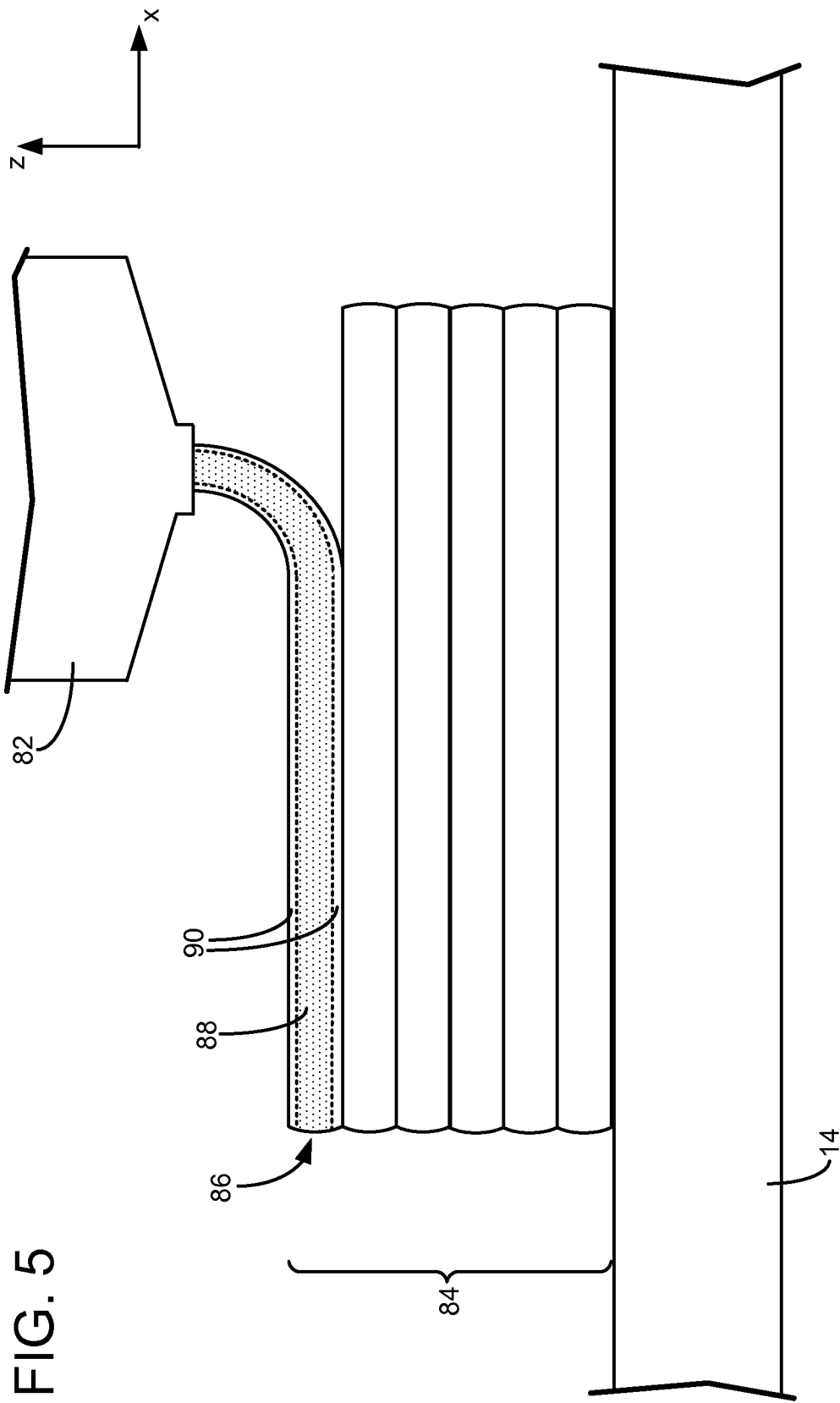
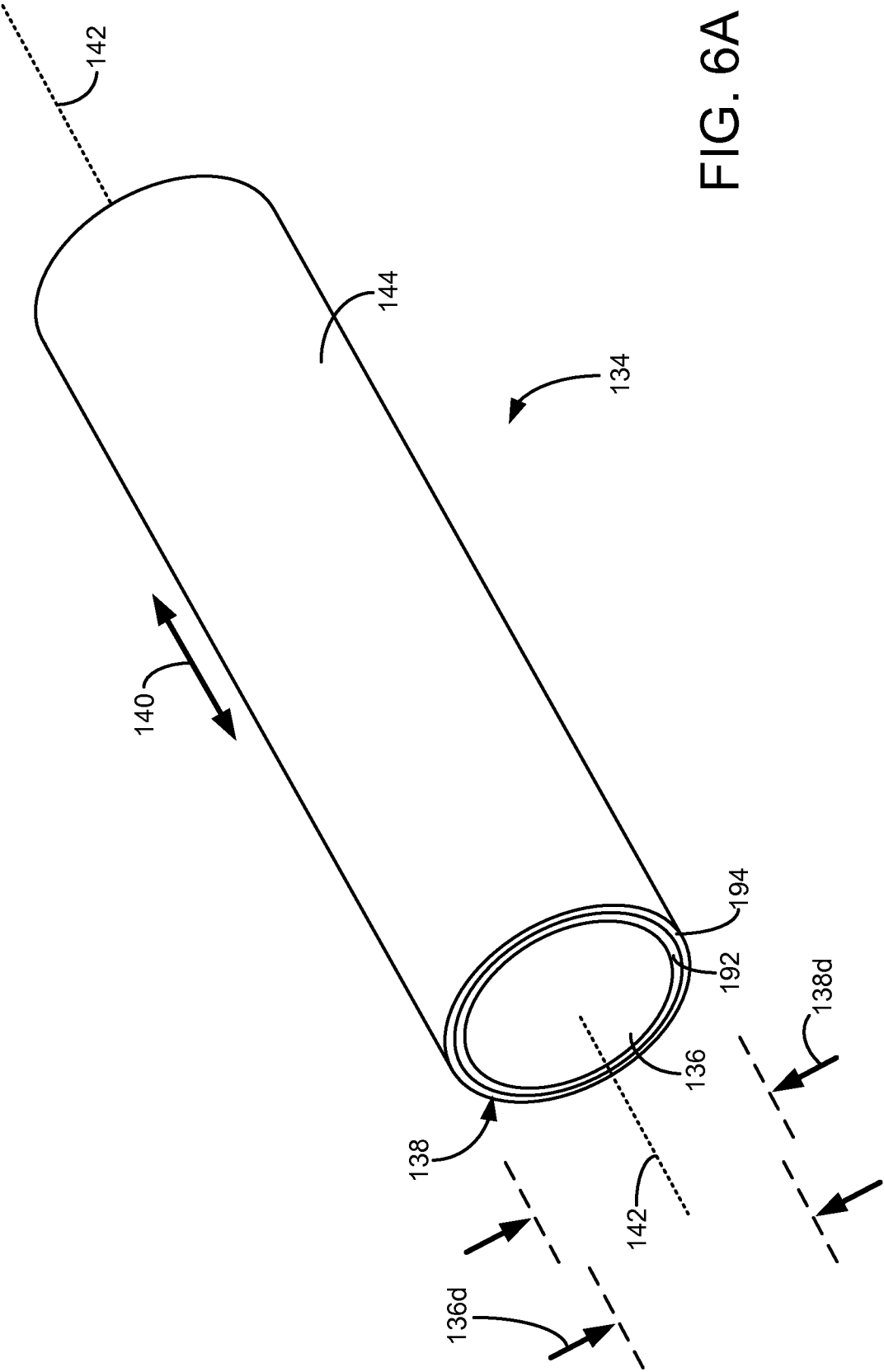


FIG. 2







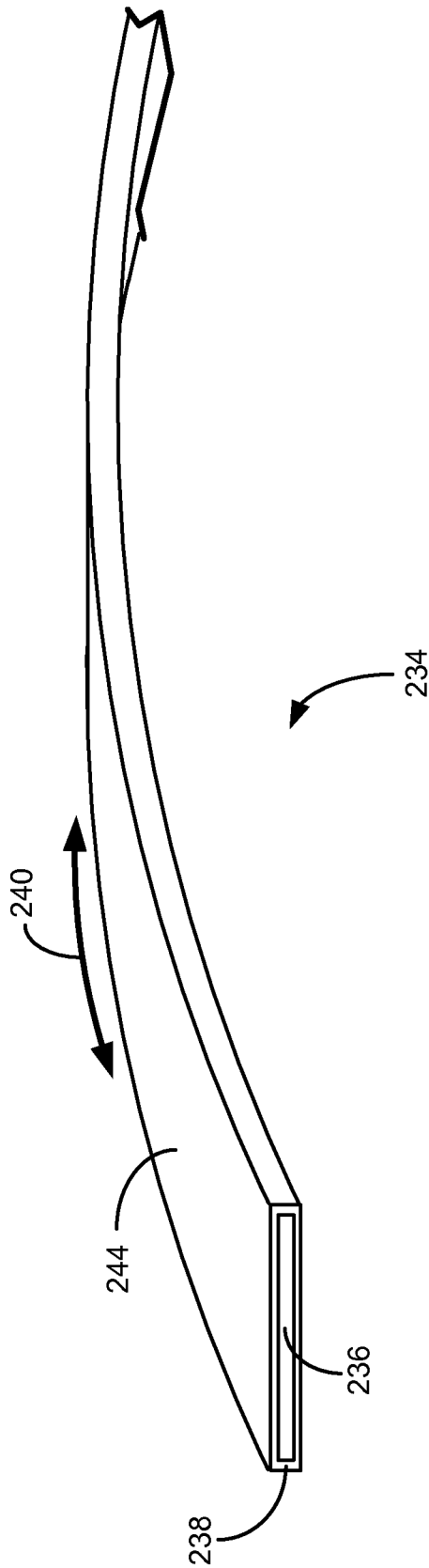


FIG. 6B

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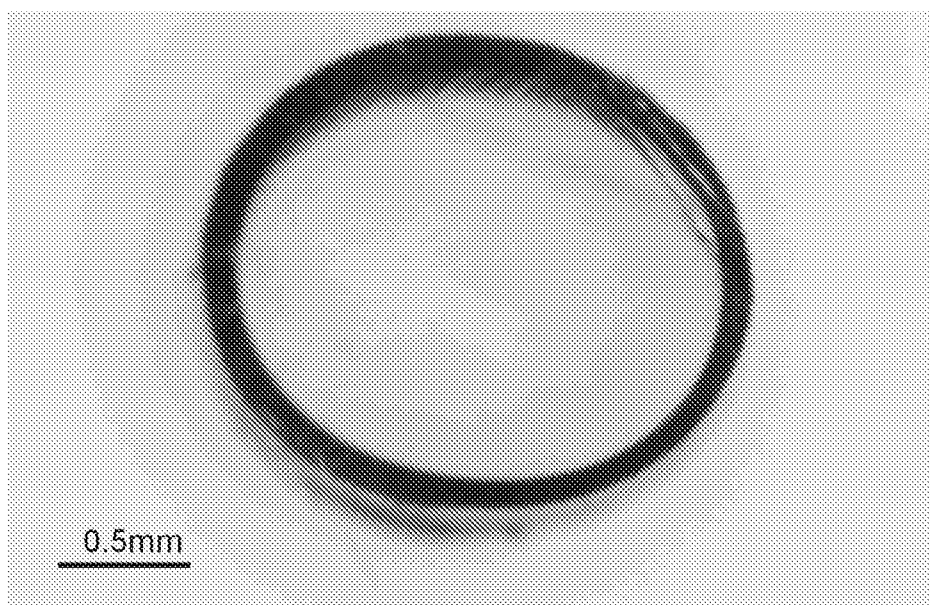


FIG. 7

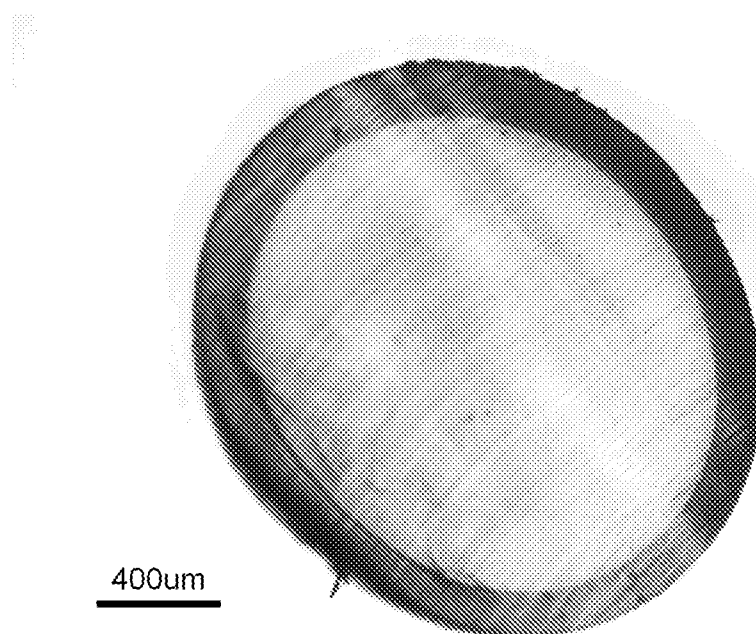


FIG. 8

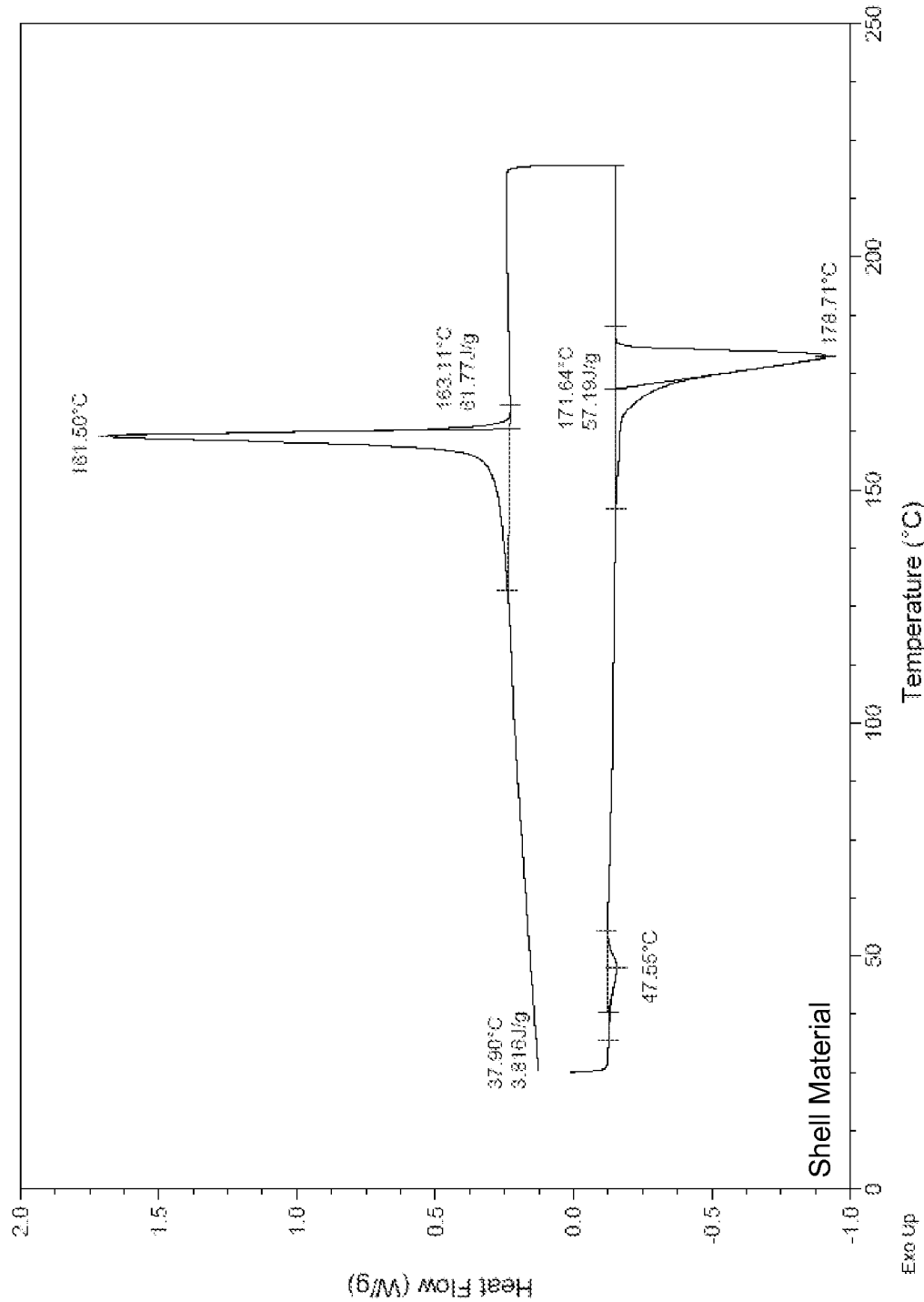


FIG. 9

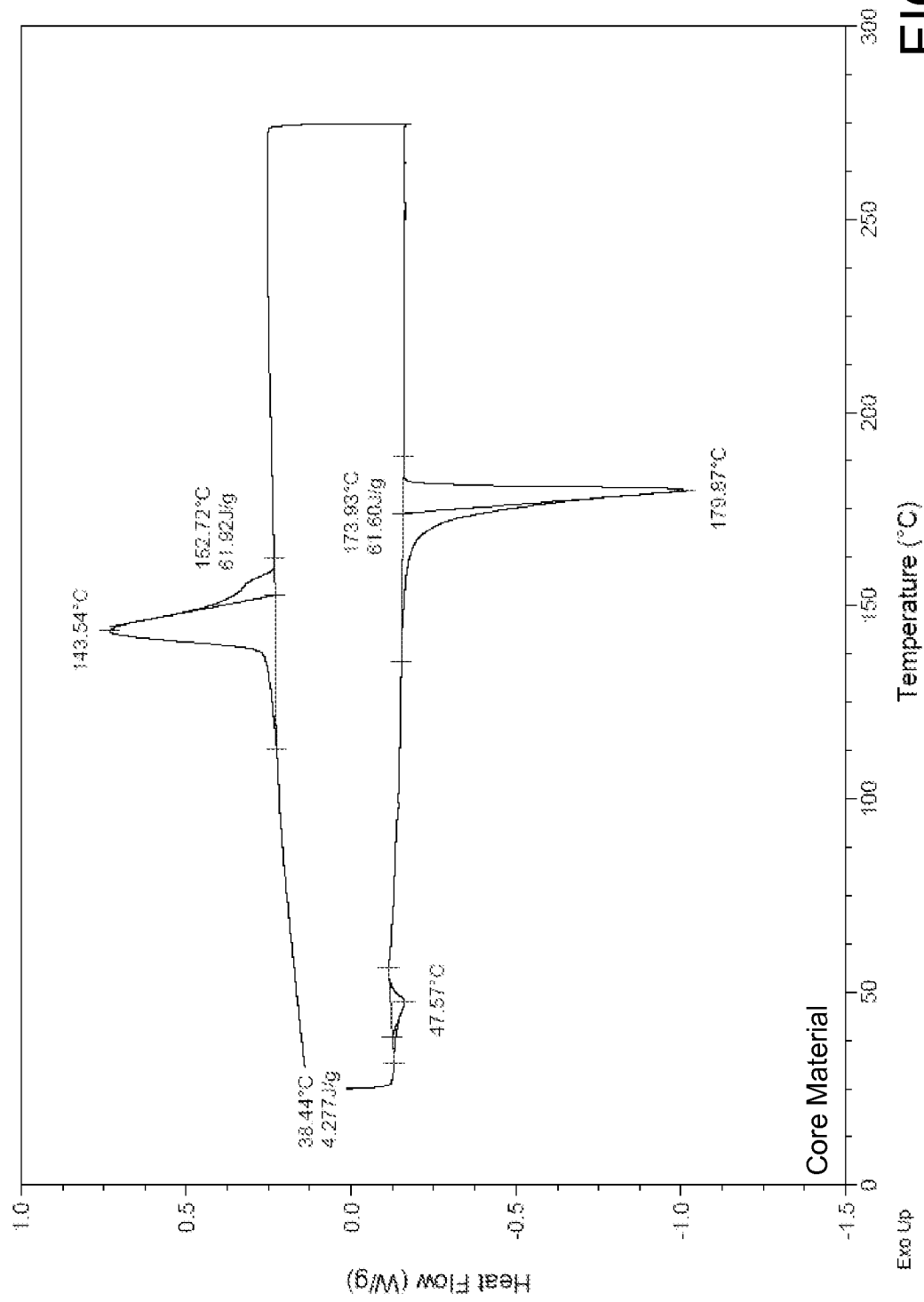


FIG. 10



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FIG. 11

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FIG. 12



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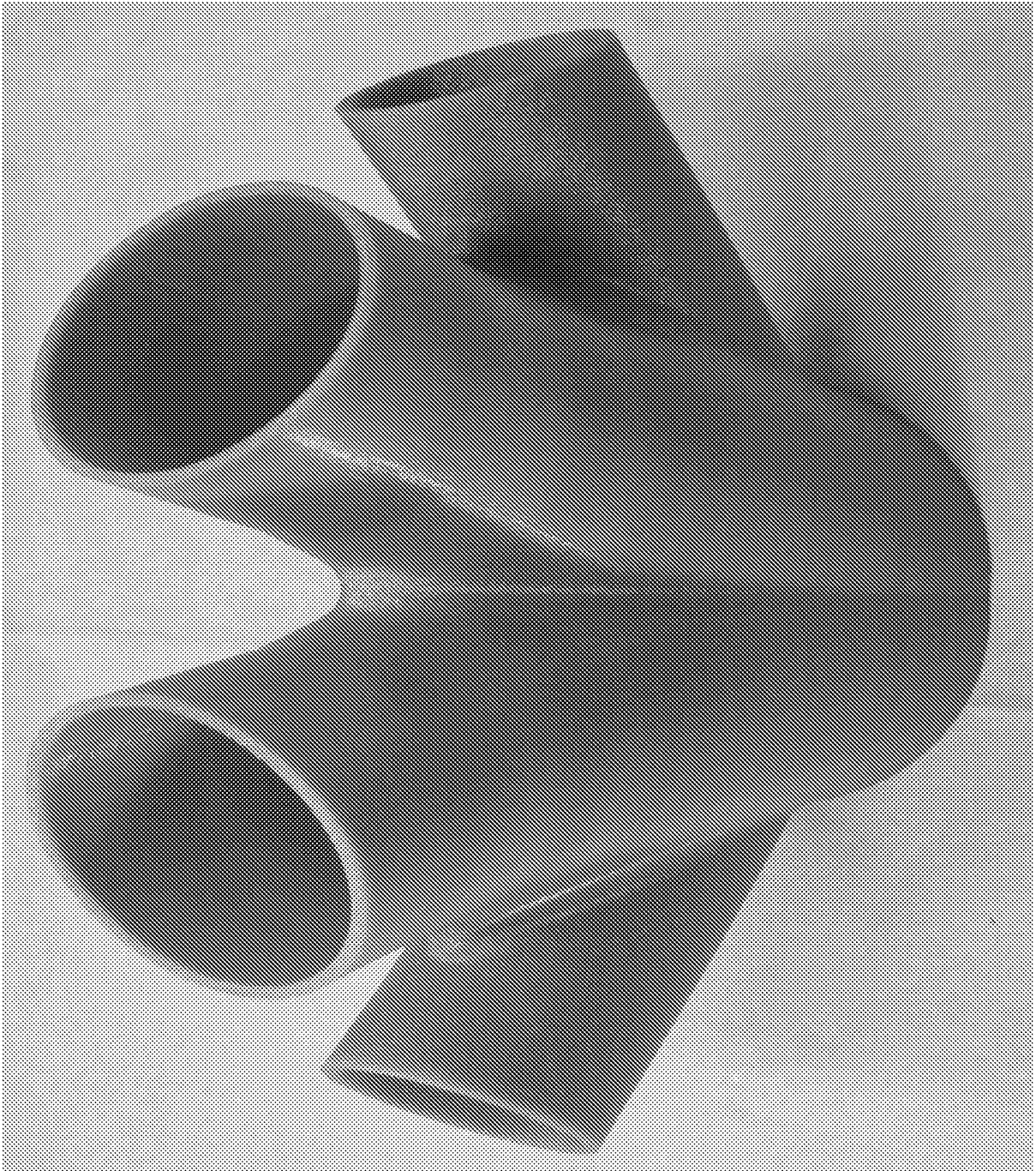


FIG. 13



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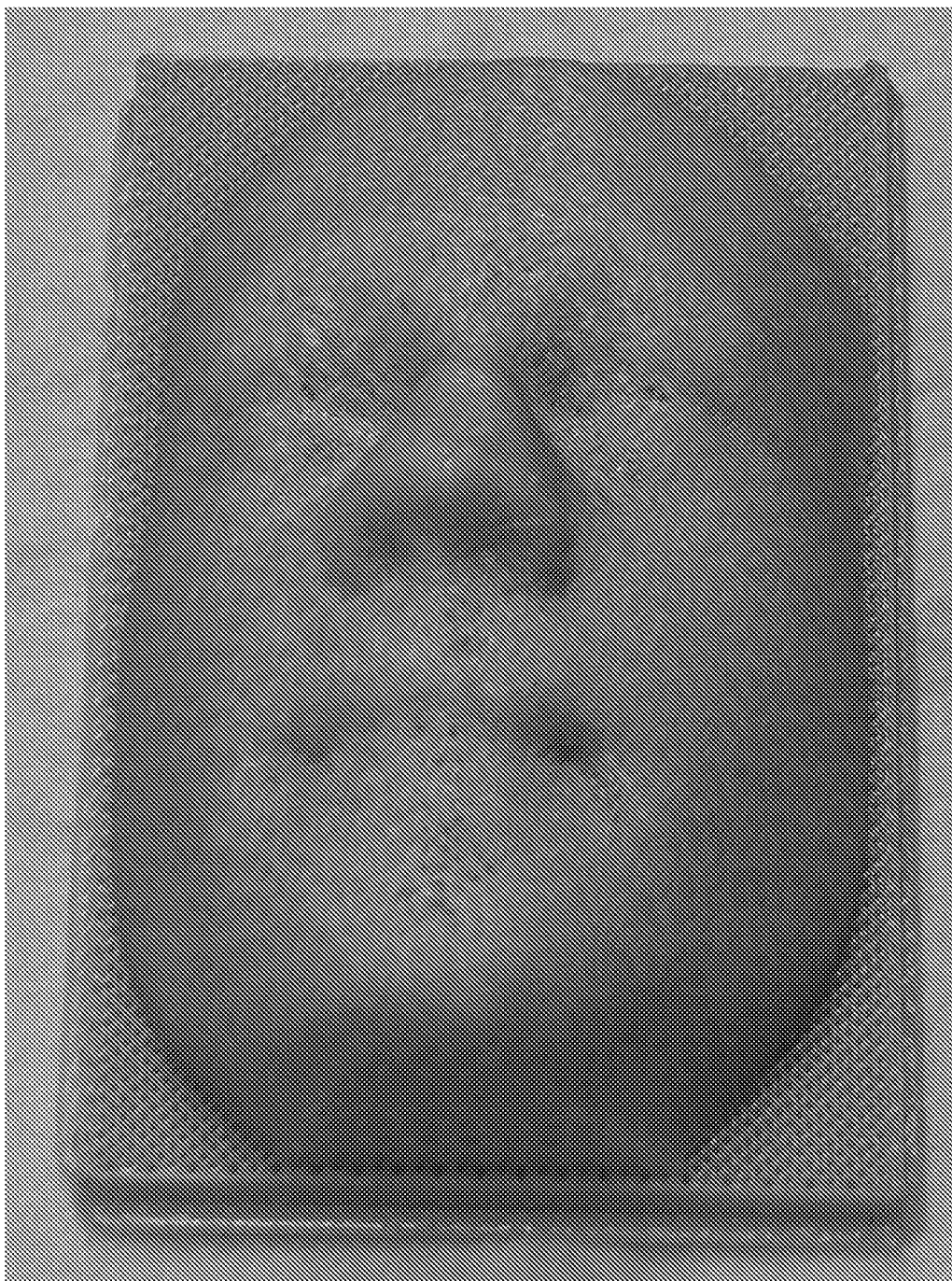


FIG. 14

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FIG. 15

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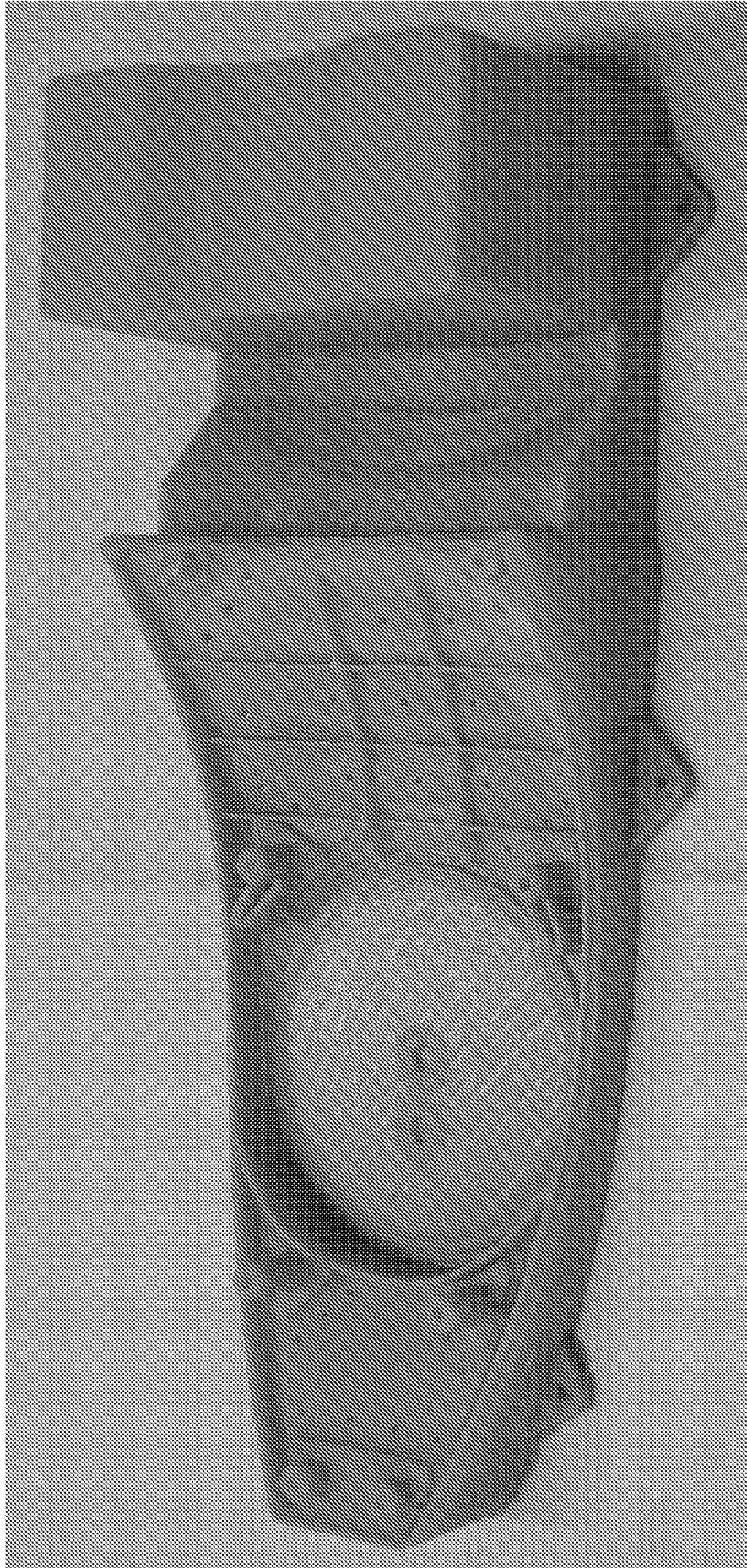


FIG. 16