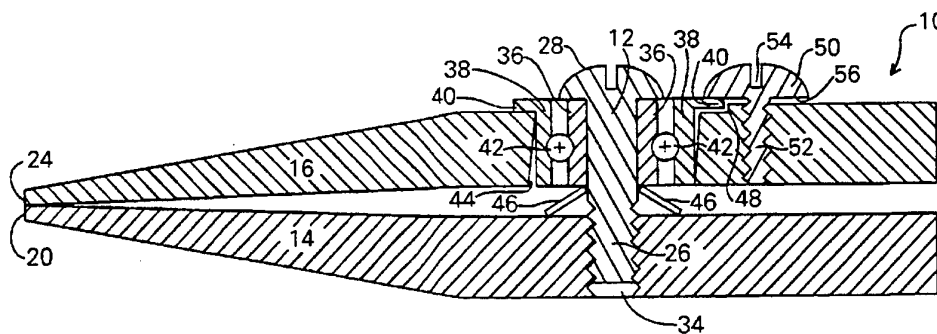




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(54) Title: RIDELESS SCISSORS WITH AN ADJUSTABLE TRANSVERSE PIVOT AXIAL LOAD ON A PIVOT JOINT



(57) Abstract

A scissors (10) includes a first blade member (14) and a second blade member (16) which is pivotally coupled to the first blade member about a pivot joint (12, 32, 46, 50), wherein the blade members include first (18) and second (22) cutting edges, respectively, that are in contact with one another. The pivot joint is coupled to the second blade member to incline the second blade member relative to the first blade member so that the inclination of the second blade member produces a transverse pivot axial load at the pivot joint to produce tension and friction along the cutting edges. Further, the first and second blade members include first and second ride areas, respectively, which are spaced from and free of contact with one another due to the pivot joint so that the scissors are substantially free of any friction or drag at the ride area.

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TITLE

RIDELESS SCISSORS WITH AN ADJUSTABLE TRANSVERSE PIVOT
AXIAL LOAD ON A PIVOT JOINT

FIELD OF THE INVENTION

5 This invention relates to scissors and, in
particular embodiments, rideless scissors with an
adjustable transverse pivot axial load on a pivot
joint.

BACKGROUND OF THE INVENTION

10 Scissors are commonly used to cut materials, such
as paper, fabric, hair and the like. Scissors also
come in a wide variety of sizes, from small scissors
for cutting nails to a metal cutting scissors (e.g.,
shears).

15 Typically, scissors are constructed with two
separate, slightly bowed blade members being pivotally
coupled together by a pivot joint. The blade members
are held at three main points: along the opposing
cutting edge of each blade member, at the pivot joint,
20 and by the contact between the blade members in back of
the pivot joint and before the handle of the scissors.
The pivot joint is placed under an axial load directed
along the pivot axis of the pivot joint to keep the
members together, while the contact in back of the
25 pivot joint acts as a lever with the pivot joint as the
fulcrum to produce tension and friction between the
cutting edges of the blade members which ensures proper
cutting action. There is also a corresponding friction
or drag in typical prior art scissors between the blade
30 members where they slide against each other at the
point of contact in back of the pivot joint which is
known in manufacturing as the "ride" or "half-moon."
It is the combination of the pivot joint axial load
with the lever contact in the "ride" area which
35 determines the tension and friction along the cutting
edges of typical prior art scissors.

Originally, the tension and friction in the

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scissors was non-adjustable. Typically, a threaded connecting pin with a pivot axis was passed through an oversized non-threaded hole in a movable blade member (with respect to the pin) and screwed into a threaded hole in the stationary blade member (with respect to the pin). The non-threaded pin end was enlarged to form a head or a bearing surface to press the opposing blade members against each other. The enlarged pin head served as the bearing surface for the pivotal movement of the moving member. The connecting pin could be adjusted slightly during manufacture to give slight variations in tension and friction. However, once manufactured, friction and tension in the scissors could not normally be adjusted by the user. Thus, the user was limited to the cutting tension and friction set by the manufacturer.

In non-adjustable scissors, the friction and tension changes over time from wear and loosening of the parts and by the accumulation of dirt and debris. As the parts wear and loosen, desirable tension and friction is reduced, thereby altering the alignment of the scissors. Misalignment causes poor cutting performance and efficiency, shortened tool life, as well as premature loss of edge sharpness. At the same time, undesirable friction or drag between moving parts greatly increases from a build up of dirt and debris between the pin head and the moving blade member, and between the opposing blade members where they make contact at the "ride" area. The result is impaired scissor movement or action due to excessive drag between moving parts.

In attempts to overcome these drawbacks, manufacturers have made the friction and tension in the scissors less sensitive to the effects of wear and the accumulation of dirt and debris. For example, either an anti-friction washer, bushing (usually nonmetallic), ball bearings, or sealed ball bearings have been

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interposed between the pin head and the moving blade member to reduce wear from friction. Threaded plastic bushings have been pressed into the threaded hole in the stationary blade member to accept the threaded pin and non-rotatively hold it, or the threaded pin is held in place by chemical thread-locking means (such as "Loctite thread locker") or by mechanical thread-locking means (such as deformable plastic strips, patch screws or lock nuts) to prevent wear on the threaded portion of the connecting pin and blade member. While these alternative designs may reduce wear in some parts, they do not eliminate wear along the cutting blades and wear at the "ride". Also, the alternative designs do not prevent or reduce the undesirable effects from the accumulation of dirt and debris between the moving parts and at the "ride" area.

In another alternative, thrust bearings have been interposed between the opposing blade members to reduce friction between the blade members. However, typical thrust bearings are relatively large and, thus, are limited to use on large scissors such as "pinking shears". Moreover, the large bearings cause the members to be widely separated, and thus the blades must exert a lever force on the rear most part of the thrust bearing, which extends into the "ride" area, to create the tension and friction in the cutting blades. This lever force produces wear with undesirable effects similar to that found in other typical prior art scissors. Also, the thrust bearings are especially prone to develop excessive drag through contamination by dirt and debris, because the thrust bearings are unsealed.

Typically, the above-described alternative designs do not provide for alteration of the tension and friction by the user. To allow adjustment of the tension and friction, as well as to address some of the above-described drawbacks, an adjustable tension

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positive-locking type pivot joint has been used. Typical scissors of this type are constructed like the non-adjustable scissors, except that the connecting pin is provided with either internal or external threads, to which a locking screw or nut is affixed for engaging the opposing blade members together with varying pivot axial loads to adjust the tension and friction. In some scissors, the locking screw or nut is user adjustable, thereby allowing for tailoring of the friction and tension to fit the needs of the individual user.

However, while this type of scissors has adjustable tension and friction, it still suffers from several drawbacks. The operator-adjustable pivot joint may be large and bulky so that it interferes when the scissors are used with another device, such as a guide, a comb or the like. Moreover, frequent adjustment of the adjustable pivot joint may be required to compensate for the locking screw or nut loosening rotationally due to an inadequate locking force (i.e., caused by wear or by poor design) or unintentional contact with the operators hand, or other object, while in use. Also, like in the previously described scissors, continual adjustment of the adjustable pivot joint is required to compensate for loosening blade member tension from wear of sliding parts. Moreover, adjustments of the adjustable pivot joint may be required to compensate for the increased friction or drag between other moving parts from the collection of dirt, debris and corrosion. Typically this accumulation occurs between the pin head and the moving blade member, and between the opposing blade members where they make contact at the "ride".

Thus, even with tension adjustable scissors, the operator is distracted from efficient cutting by the intrusive protrusion of the tension adjusting pivot joint, and the necessity of adjusting the blade member

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tension to compensate for wear or the loosening of the adjustable pivot joint itself. Tension adjustable scissors give the user greater control over tension and friction, but they do not reduce effects of wear and accumulation of dirt and debris. Therefore, the wear in tension adjustable scissors still results in poor cutting performance and efficiency, shortened tool life, and loss of cutting edge sharpness.

SUMMARY OF THE DISCLOSURE

10 It is an object of an embodiment of the present invention to provide an improved scissors, which obviates for practical purposes the above-mentioned limitations.

15 An improved scissors, according to one embodiment of the present invention, includes a pivot joint having a pivot axis, a first blade member having a first cutting edge and a longitudinal axis, and a second blade member having a second cutting edge. The second blade member is pivotally coupled by the pivot joint to the first blade member with the first cutting edge adjacent and in contact with the second cutting edge. Moreover, the pivot joint is coupled to the first blade member to incline the first blade member relative to the second blade member and the pivot joint, so that the inclination of the first blade member produces a transverse pivot axial load on the pivot axis of the pivot joint, which corresponds to the direction along the longitudinal axis of the first blade member to produce and determine the tension and friction along the cutting edges. In preferred embodiments, the transverse pivot axial load is oblique to the pivot axis of the pivot joint and may also be inclined between 0.1 to 10.0 degrees from an axis perpendicular to the pivot axis and along the longitudinal axis of the first blade member. Further, the first blade member may also include a first ride area, and the second blade member may also include a second ride

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area, so that the first ride area is spaced from and free of contact with the second ride area. Therefore, the scissors may be substantially free of any friction or drag at the "ride" area.

5 In further embodiments of the present invention, the pivot joint in the scissors may be adjustable to increase or decrease the tension and friction between the blade members at the points of contact. A separate adjustment screw or the like is coupled to the first
10 blade member and may be used to increase or decrease the transverse pivot axial load and the tension and friction between the blade members by adjusting the tilt or incline of the first blade member with respect to the pivot joint and the second blade member. In
15 other embodiments of the present invention, the pivot joint passes through a pivot bore in each blade member, and the various inclination and tilts provided by the adjustment screw place the pivot joint under various transverse pivot axial loads to increase or decrease
20 the tension and friction along the cutting edges.

 In preferred embodiments of the present invention, the pivot joint includes a substantially frictionless, sealed bearing assembly, a washer, and a pivot pin having a flanged head and a threaded end. The pivot
25 pin passes through the bearing assembly and the washer and has the threaded end of the pin secured in a threaded pivot bore of the second blade member. The bearing assembly is coupled to the pivot bore of the first blade member, which is sized to allow inclination
30 of the first blade member in the direction along the longitudinal axis of the first blade member. The bearing assembly is held in place between the washer and the flanged head of the pivot pin. Preferably, the bearing assembly has an outer flange. The adjustment
35 screw is positioned to engage the outer flange and tilt or incline the first blade member with respect to the pivot joint and the second blade member.

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In a still further embodiment of the present invention, the scissors includes a tension lever with two threaded bores, and the pivot joint includes a substantially frictionless sealed bearing assembly, a washer and a pivot pin having a flanged head and a threaded end. The pivot pin passes through the bearing assembly, the washer, the sized pivot joint hole in the first blade member and the threaded end of the pivot pin is secured in one of the threaded bores in the tension lever. The bearing assembly is held in the pivot joint hole of the second blade member between the head of the pivot pin and the washer. The adjustment member is threaded into the other threaded bore of the tension lever to incline the first blade member with respect to the pivot joint and the second blade member, rather than engaging the outer flange of the bearing assembly.

Other features and advantages of the invention will become apparent from the following detailed description, taken in conjunction with the accompanying drawings which illustrate, by way of example, various features of embodiments of the invention.

BRIEF DESCRIPTION OF THE DRAWINGS

A detailed description of embodiments of the invention will be made with reference to the accompanying drawings, wherein like numerals designate corresponding parts in the several figures.

Fig. 1 is a partial perspective view of a scissors in accordance with a first embodiment of the present invention.

Fig. 2 is a partial cross-sectional view of the scissors shown of Fig. 1 as viewed along the line 2-2.

Fig. 3 is an exploded view of the scissors shown in Fig. 1.

Fig. 4 is a partial top perspective view of a scissors in accordance with a second embodiment of the present invention.

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Fig. 5 is a partial bottom perspective view of the scissors shown in Fig. 4.

Fig. 6 is a partial cross-sectional view of the scissors shown of Fig. 4 as viewed along the line 6-6.

5 Fig. 7 is an exploded view of the scissors shown in Fig. 4.

DETAILED DESCRIPTION OF PREFERRED EMBODIMENTS

As shown in the drawings for purposes of illustration, the invention is embodied in an improved
10 scissors. In preferred embodiments of the present invention, the scissors have a transverse pivot axial load and no drag or friction at the "ride" area. Also, the tension and friction may be easily adjusted by the user. However, it will be recognized that further
15 embodiments of the invention include shears, cutters or other instruments which use a scissoring action or a compound shear action with a pivot joint or the like. Moreover, further embodiments of the present invention may be used with scissors having straight blades,
20 curved blades, pinking blades, serrated blades, detachable blades, non-cutting blades, crimping blades or the like.

According to the preferred embodiments of the present invention, the scissors have two blade members
25 pivotally coupled together by a pivot joint. Each blade member contacts the pivot joint and the other blade member along a cutting edge. There may be substantially no contact in the "ride" area (e.g., the scissors are rideless), so that all friction and
30 tension, and therefore wear, in the "ride" area may be eliminated. It is important to note, that scissors made in accordance with the preferred embodiments of the invention, do not need tension and friction produced in the "ride" area to function, since one
35 member is inclined relative to the pivot joint and the other member to produce a transverse pivot axial load which force the cutting edges of the members together

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with the proper tension and friction. However, typical prior art scissors require tension and friction in the "ride" area to work properly. Also, typical prior art scissors only have a pivot axial load (directed along the pivot axis) at the pivot joint.

Moreover, the scissors, in accordance with the preferred embodiments, may use a sealed ball bearing assembly to further reduce friction between the moving parts in the pivot joint. Thus, friction and wear in the pivot joint is minimized (i.e., only minimal friction is generated between moving parts in the ball bearing assembly).

Minimizing friction in the moving parts and eliminating friction in the "ride" area allows the scissors to maintain a more constant state of adjustment with regard to cutting blade tension settings and blade member alignment. Therefore, wear and loosening will only occur along the cutting edges of each blade member, and only to a very minor degree within the sealed, lubricated environment of the sealed bearing assembly. Thus, the tension and friction set by the manufacturer or user is substantially unaffected by the wear and loosening of the parts, which is commonly encountered in typical prior art scissors.

Also, the presence of dirt and debris have less of an affect on the scissors in accordance with embodiments of the present invention. For instance, because there is substantially no contact between the blade members in the "ride" area, this area is easier to clean. Also, dirt and debris have minimal affect on the operation of the sealed ball bearing, since it is sealed and all moving parts are contained within the sealed environment.

In still further embodiments, the tension and friction of the scissors may be user adjustable. The operator can use an adjustment screw, detent, bolt, spring, shim, spacer, tab or the like (i.e., a

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relatively small and unobtrusive adjustment member), to increase or decrease the transverse pivot axial load which adjusts the tension and friction in the members and the cutting edge blades. In preferred embodiments, the adjustment member may be part of the pivot joint.

A first improved scissors 10 in accordance with a preferred embodiment of the present invention is shown in Figs. 1-3. The scissors 10 include a connecting pin 12 having a pivot axis, a stationary blade member 14 (i.e., with respect to pin 12) and a moving blade member 16 (i.e., with respect to the pin 12). The stationary blade member 14 has a cutting edge 18 and a tip 20, and the moving blade member 16 has a cutting edge 22 and a tip 24. The connecting pin 12 has a threaded end 26 at one end and a flanged head 28 at the other end.

As shown in Fig. 2, stationary blade member 14 and moving blade member 16 are pivotally coupled together by the connecting pin 12. The connecting pin 12 passes through the center opening 30 of a sealed ball bearing assembly 32 and is screwed into a threaded connecting pin hole 34 in the stationary member 14 by threaded end 26. The connecting pin 12 may be threaded directly into the stationary blade member 14, or the threaded connecting pin hole 34 may be provided with deformable plastic strips or patch inserts to produce a positive locking force to secure the connecting pin 12 non-rotatively to the stationary blade member 14. Other connecting pin arrangements may be used in alternative embodiments, including nut and bolt arrangements, attached stud, rivet arrangement, pin and cotter pin arrangements or the like.

In the illustrated embodiment, the ball bearing assembly 32 is of a prelubricated, sealed stainless steel arrangement. The ball bearing assembly 32 includes an inner race 36, an outer race 38, a flange 40, and ball bearings 42. The sealed ball bearing

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assembly 32 is seated within a ball bearing assembly hole 44 in the moving member 16. Certain dimensions of the ball bearing assembly hole 44 are oversized (as shown in Fig. 2) to allow clearance for outer race 38 of the ball bearing assembly 32 to tilt or incline with respect to the longitudinal axis (parallel to line 2-2 in Fig. 1) of the moving blade member 16.

A conical spring washer 46 is interposed between the stationary blade member 14 and the ball bearing assembly 32 to provide variable clearance between the moving blade member 16 and the stationary blade member 14. The inner race 36 of the ball bearing assembly 32 is the only part of ball bearing assembly 32 to contact the top of conical spring washer 46. In preferred embodiments, the conical spring washer 46 is made of spring steel and may be a Belleville washer which deflects under pressure. However, non-metallic washers, laminated washers, spacers, bushings, shim washers or the like may be used. Also, proper spacing may be made integral with the blade member or may be made integral with the bearing assembly without using a washer. Moreover, the washer may extend beyond the rear of the pivot joint into the "ride" area, this extension may increase friction. The ball bearing assembly 32 is held and secured in the ball bearing assembly hole 44 between the conical spring washer 46 and the flanged head 28 of the connecting pin 12.

As shown in Figs. 1-3, the moving blade member 16 has a semicircular recess 48 which defines a half-circle around the rear portion (i.e., the portion farthest from the tips 20 and 24) of the ball bearing assembly hole 44. The semicircular recess 48 is counterbored on an axis that is offset (i.e., approximately 5°, although other oblique angles may be used) to the rear of an axis which is perpendicular to the longitudinal axis of moving blade member 16.

Fig. 2 shows that the flange 40 on the outer race

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38 of the ball bearing assembly 32 is positioned within the semicircular recess 48. A tension screw 50 has threads 52, a slot 54, and an engagement surface 56. The engagement surface 56 contacts the flange 40 of the ball bearing assembly 32 to control the tilt or incline of one blade member relative to the other and the pivot joint. The tension screw 50 is screwed into a threaded tension screw hole 58 to increase or decrease the tension and friction, and thus produce a corresponding transverse pivot axial load in the connecting pin 12 and the ball bearing assembly 32 portions of the pivot joint. The tension screw 50 may be screwed directly into the tension screw hole 58 or it may be provided with a deformable plastic strip or patch insert on the threads 52 to produce a positive locking effect, which is still easily adjustable by the operator. To further facilitate tension and friction adjustment, the slot 54 in tension screw 50 is made wide enough to use a coin, screwdriver, or nail file to turn the tension screw 50.

In the preferred embodiments, corrosion resistance for the entire scissors is achieved by making all metallic components of stainless steel. However, other materials such as plastics, ferrous alloys, non-ferrous alloys ceramics or the like may be used, the choice being partially dependent on the material to be cut and the environment in which the scissors 10 will be used. The ball bearing assembly 32 is preferably selected from the group of ball bearings known as stainless steel, sealed ball bearings. For example, the sealed ball bearing part no. B2-14-S available from Winfred M. Berg, Inc., East Rockaway, New York may be used. These assemblies provide permanent lubrication of all actively moving parts in the pivot area of the scissors 10, and are thus an effective barrier to dirt, debris, and corrosion. However, other bearing assemblies may be used which provide smooth operation, resistance to dirt and debris, and resistance to wear and corrosion.

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The operation of the above-described preferred embodiment is best illustrated in Fig. 2. The engagement surface 56 of the tension screw 50 presses against the flange 40 of the ball bearing assembly 32 with increasing pressure as the tension screw 50 is screwed into the tension screw hole 58. As the pressure on the flange 40 increases, the moving blade member 16 is tilted or inclined (i.e., towards the tips 20 and 24 to increase tension and friction) in relation to the outer race 38 of the ball bearing assembly 32. The increased inclination of the moving blade 16 increases the transverse pivot axial load on the pivot joint parts, such as the connecting pin 12 and the ball bearing assembly 32. The transverse pivot axial load is oblique to the pivot axis, and in preferred embodiments ranges from 0.1° to 10.0° from an axis perpendicular to the pivot axis and along the longitudinal axis of the moving member 16. This transverse pivot axial load replaces the lever contact in the "ride" area which is required in typical prior art scissors. Therefore, preferred embodiments of the scissors 10 may be rideless.

This transverse pivot axial load causes the moving blade member 16 to be pressed against the stationary blade member 14 at their mutual point of contact along cutting edges 18 and 22. In Figs. 1 and 2, this point of contact is shown as being the tips 20 and 24, since the scissors 10 are shown in the closed position. Tightening or loosening of the tension screw 50 correspondingly places a greater or lesser tilt or incline and transverse pivot axial load on the ball bearing assembly 32 and connecting pin 12, which then correspondingly increases or decreases the tension and friction between the cutting edges 18 and 22.

Clearance between the moving blade member 16 and the stationary blade member 14 is decreased or increased by correspondingly tightening or loosening

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the connecting pin 12, causing the ball bearing assembly 32, through the inner race 36, to press on and deform the conical spring washer 46. This pressure through the inner race 36 may also aid in holding the connecting pin 12 in a non-rotational position with respect to stationary blade member 14.

As the blade members 14 and 16 of the scissors 10 pivot back and forth relative to each other, the lack of friction and drag in the "ride" area (i.e., the scissors are rideless) and the smooth, lubricated movement in the ball bearing assembly 32 in the pivot area provides ease of operation in the scissor action due to the exceptionally low friction between these moving parts. Also, the friction and tension tend to be less susceptible to change resulting from wear, dirt and debris. Thus, the scissors 10 substantially eliminate the wear between scissor parts commonly found in typical prior art scissors, which have drag and friction at the "ride" area and do not use an anti-friction bearing interposed between frictionally contacting parts. Therefore, the scissors 10 provide optimum edge sharpness and long-lasting edge durability, due to excellent blade member stability and constancy of adjustment and alignment.

Moreover, care and maintenance of the scissors 10 is easier than in typical prior art scissors, since the permanently lubricated sealed stainless steel ball bearing assembly, as used in the preferred embodiments, is resistant to wear, corrosion, and the affects of dirt. The lack of contact and friction at the "ride" area also makes this area easier to clean. The use of a tension screw 50 provides a low profile to the adjustment member and, thus, avoids the problem of having large and bulky parts to adjust the tension in the scissors 10.

A second improved scissors 100 in accordance with preferred embodiments of the present invention is shown

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in Figs. 4-7. Structural differences between the scissors 100 and the embodiment described above are shown in Figs. 5 and 6. The connecting pin 112 passes through the center of the ball bearing assembly 132 and the conical washer 146. However, the connecting pin 112 also passes through a non-threaded connecting pin hole 134 in the stationary blade member 114. The connecting pin 112 is screwed into a threaded tension lever connecting hole 162 in a tension lever 160. A tension lever screw 164 is screwed into a tension lever screw hole 166 in one end of tension lever 160. The tension lever screw 164 has a tip 168 which contacts and presses against the stationary blade member 114 at its point of contact in a tension bore 170.

Other differences are that the ball bearing assembly 132 need not tilt or incline and is seated with a press fit in a ball bearing assembly hole 144. Also, certain dimensions of the connecting pin hole 134 are oversized to allow clearance for the connecting pin 112 to tilt or incline with respect to the longitudinal axis of the moving blade member 116 and produce a transverse axial load on the connecting pin 112. Moreover, in this embodiment, the tension screw 50 with its related parts and the semicircular recess 48 are eliminated.

The operation of the above-described second embodiment is best illustrated in Fig. 6. The tip 168 presses against the stationary blade member 114 at the tension bore 170 with increasing pressure as the tension lever screw 164 is screwed into the tension lever screw hole 166. As the pressure on the stationary blade member 114 increases, the stationary blade member 114 is tilted or inclined in relation to the connecting pin 112, the ball bearing assembly 132, and the moving blade member 116. The inclination of the stationary blade member 114 produces a transverse pivot axial load to maintain the tension and friction

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along the cutting edges. The stationary blade member 114 is pressed against the moving blade member 116 at their mutual point of contact along cutting edges 120 and 124 as the scissors 100 open or close, or at the tips 118 and 122 when the scissors are in the closed position, as shown in Fig. 6.

In the illustrated embodiments, the scissors are shown with a tension adjustment screw or member. However, in further embodiments the adjustment screw is omitted and the connecting pin is used alone, without an adjustment screw or member, to adjust the tension and friction in the scissors. For instance, the ball bearing assembly hole 44 may not be oversized as described above. Rather, the ball bearing assembly hole 44 may precisely fit the ball bearing assembly 32. However, the ball bearing assembly hole 44 would be tilted or inclined with respect to the longitudinal axis of the moving member 16. This inclination would produce a transverse pivot axial load that determines the tension and friction along the cutting edges.

While the description above refers to particular embodiments of the present invention, it will be understood that many modifications may be made without departing from the spirit thereof. The accompanying claims are intended to cover such modifications as would fall within the true scope and spirit of the present invention.

The presently disclosed embodiments are therefore to be considered in all respects as illustrative and not restrictive, the scope of the invention being indicated by the appended claims, rather than the foregoing description, and all changes which come within the meaning and range of equivalency of the claims are therefore intended to be embraced therein.

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WHAT IS CLAIMED IS:

1. A scissors, comprising:
 - a pivot joint having a pivot axis;
 - a first blade member having a first cutting edge
 - 5 and a longitudinal axis; and
 - a second blade member having a second cutting edge,
 - the second blade member being pivotally coupled by the
 - pivot joint to the first blade member with the first
 - cutting edge adjacent and in contact with the second
 - 10 cutting edge, and the pivot joint being coupled to the
 - first blade member to incline the first blade member
 - relative to the second blade member and the pivot
 - joint, wherein the inclination of the first blade
 - member produces a transverse pivot axial load on the
 - 15 pivot axis of the pivot joint corresponding to the
 - direction along the longitudinal axis of the first
 - blade member to produce tension and friction along the
 - cutting edges.
2. A scissors according to claim 1, wherein the
- 20 transverse pivot axial load is oblique to the pivot
- axis of the pivot joint.
3. A scissors according to claim 1, wherein the
- transverse pivot axial load is inclined between 0.1 to
- 10.0 degrees from an axis perpendicular to the pivot
- 25 axis and along the longitudinal axis of the first blade
- member.
4. A scissors according to claim 1, wherein the first
- blade member further includes a first ride area, and
- wherein the second blade member further includes a
- 30 second ride area, and wherein the first ride area is
- spaced from and free of contact with the second ride
- area.
5. A scissors according to claim 4, wherein the pivot
- joint includes a substantially frictionless sealed
- 35 bearing assembly.

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6. A scissors according to claim 4, wherein the first blade member may be adjusted to different inclinations relative to the second blade member and the pivot joint to produce different transverse pivot axial loads and
5 increase or decrease the tension and friction along the cutting edges.

7. A scissors according to claim 4, further comprising a separate adjustment member coupled to the first blade member to engage a portion of the pivot joint to
10 increase or decrease transverse pivot axial load and the tension and friction along the cutting edges.

8. A scissors according to claim 7, wherein each blade member has a pivot joint hole, wherein the pivot joint hole in the first member is sized to allow the first
15 member to be inclined in the direction along the longitudinal axis of the first blade member relative to the second blade member and the pivot joint, wherein the pivot joint passes through the pivot joint hole in each blade member, and wherein the inclination from the
20 adjustment member places the pivot joint in the sized pivot joint hole under various transverse pivot axial loads to increase or decrease the tension and friction along the cutting edges.

9. A scissors according to claim 8, wherein the pivot
25 joint includes a substantially frictionless sealed bearing assembly, a washer and a pivot pin having a flanged head and a threaded end, wherein the pivot joint hole in the second blade member is threaded, wherein the pivot pin passes through the bearing
30 assembly and the washer, and has the threaded end of the pivot pin secured in the threaded pivot joint hole in the second blade member, and wherein the bearing assembly is held in the sized pivot joint hole of the first blade member between the head of the pivot pin
35 and the washer.

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10. A scissors according to claim 9, wherein the bearing assembly has an outer flange, and wherein the adjustment member engages the outer flange to incline the first blade member with respect to the pivot joint and the second blade member.

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11. A scissors according to claim 8, further comprising a tension lever with two threaded bores, and the pivot joint includes a substantially frictionless sealed bearing assembly, a washer and a pivot pin having a flanged head and a threaded end, wherein the pivot pin passes through the bearing assembly, the washer, the sized pivot joint hole in the first blade member and the threaded end of the pivot pin is secured in one of the threaded bores in the tension lever, wherein the bearing assembly is held in the pivot joint hole of the second blade member between the head of the pivot pin and the washer, and wherein the adjustment member is threaded into the other threaded bore of the tension lever to incline the first blade member with respect to the pivot joint and the second blade member.

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12. A method of manufacturing scissors, comprising the steps of:

forming a pivot joint with a pivot axis;

5 forming a first blade member having a first cutting edge and a longitudinal axis;

forming a second blade member having a second cutting edge;

10 pivotally coupling the second blade member by the pivot joint to the first blade member with the first cutting edge adjacent and in contact with the second cutting edge;

coupling the pivot joint to the first blade member to incline the first blade member relative to the second blade member and the pivot joint; and

15 producing a transverse pivot axial load on the pivot axis of the pivot joint from the inclination of the first blade member which corresponds to the direction along the longitudinal axis of the first blade member and which produces tension and friction
20 along the cutting edges.

13. A method according to claim 12, wherein the transverse pivot axial load is produced obliquely to the pivot axis of the pivot joint.

14. A method according to claim 12, wherein the
25 transverse pivot axial load is inclined between 0.1 to 10.0 degrees from an axis perpendicular to the pivot axis and along the longitudinal axis of the first blade member.

15. A method according to claim 12, further comprising
30 the steps of:

further forming the first blade member with a first ride area;

further forming the second blade member with a second ride area; and

35 spacing the first ride area from and free of contact with the second ride area.

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16. A method according to claim 15, further comprising the steps of:
- providing a separate adjustment member coupled to the first blade member; and
 - 5 engaging the pivot joint with the separate adjustment member to adjust the transverse pivot axial load and the inclination of the first blade member to adjust the tension and friction between the blade members.
- 10 17. A method according to claim 16, further comprising the steps of:
- providing each blade member with a pivot joint bore;
 - sizing the pivot joint bore in the first blade
 - 15 member to allow the first blade member to be inclined in the direction of the longitudinal axis of the first blade member relative to the second blade member and the pivot joint;
 - passing the pivot joint through the pivot joint
 - 20 bore in each blade member; and
 - adjusting the adjustment member to incline the first blade member and place the pivot joint in the sized pivot joint hole under various transverse pivot axial loads to increase or decrease the tension and
 - 25 friction.

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18. A method according to claim 17, further comprising the steps of:

threading the pivot joint bore in the second blade member;

5 forming the pivot joint with a substantially frictionless sealed bearing assembly, a washer and a pivot pin having a flanged head and a threaded end;

passing the pivot pin through the bearing assembly and the washer;

10 threading the pivot pin into the threaded pivot joint bore in the second blade member; and

securing the bearing assembly in the sized pivot joint bore of the first blade member by the washer and the flanged head of the pivot pin.

15 19. A method according to claim 18, further comprising the steps of:

forming an outer flange on the bearing assembly; engaging the outer flange with the adjustment member; and

20 inclining the first blade member with respect to the pivot joint and the second blade member to produce a transverse pivot axial load.

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20. A method according to claim 17, further comprising the steps of:

providing a tension lever with two threaded bores;

5 forming the pivot joint with a substantially frictionless sealed bearing assembly, a washer and a pivot pin having a flanged head and a threaded end;

passing the pivot pin through the bearing assembly, the washer and the sized pivot joint bore in the first blade member;

10 securing the threaded end of the pivot pin in one of the threaded bores in the tension lever;

securing the bearing assembly in the pivot joint bore of the second blade member by the washer and the flanged head of the pivot pin; and

15 threading the adjustment member into the other threaded bore of the tension lever to incline the first blade member with respect to the pivot joint and the second blade member to produce a transverse pivot axial load.

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21. A scissors, comprising:

a pivot joint having a pivot axis;

a first blade member having a first cutting edge, a first ride area and a longitudinal axis; and

5 a second blade member having a second cutting edge and a second ride area, the second blade member being pivotally coupled by the pivot joint to the first blade member with the first cutting edge adjacent and in contact with the second cutting edge, the first ride area being spaced from and free of contact with the
10 second ride area, and the pivot joint being coupled to the first blade member to incline the first blade member relative to the second blade member and the pivot joint, wherein the inclination of the first blade
15 member produces a transverse pivot axial load on the pivot axis of the pivot joint corresponding to the direction along the longitudinal axis of the first blade member to produce tension and friction along the cutting edges.

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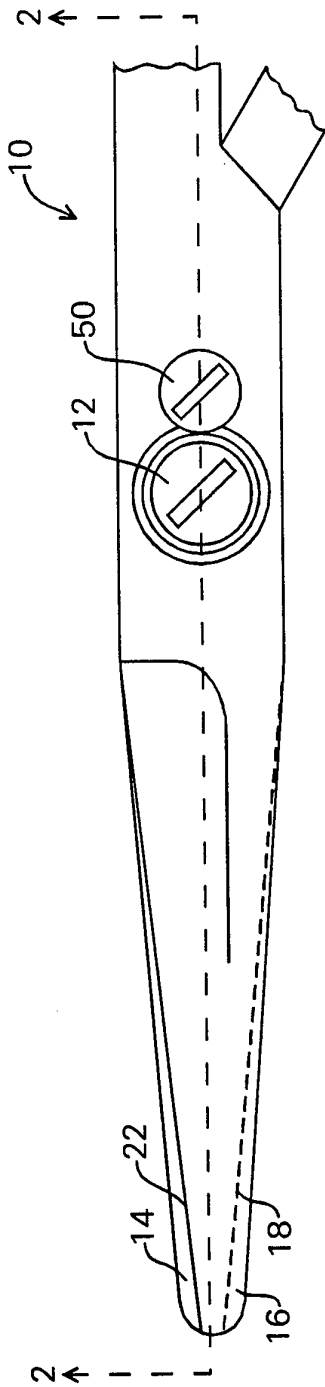


FIG. 1

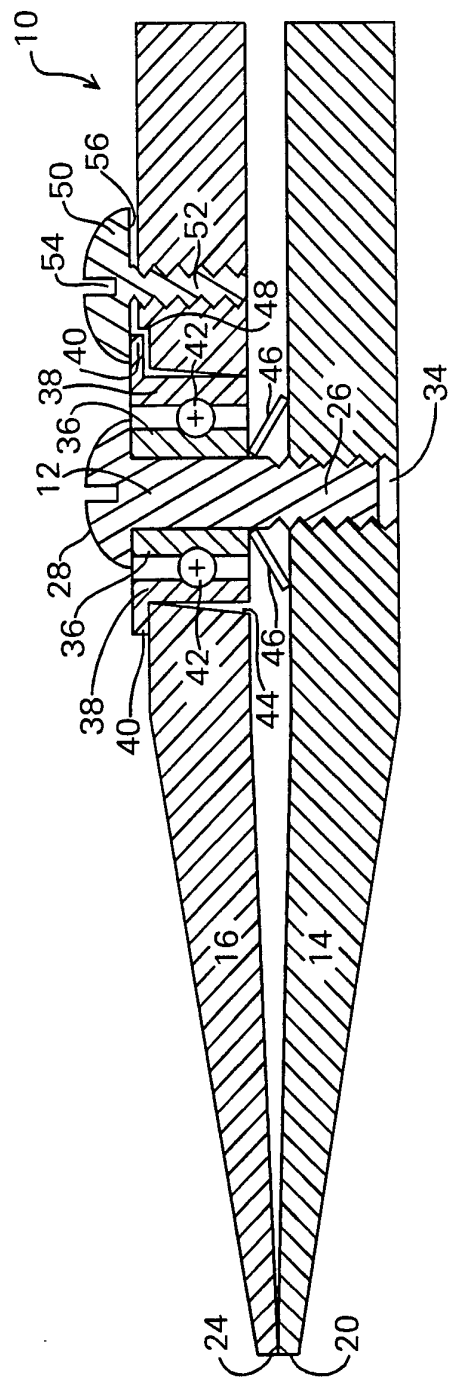


FIG. 2

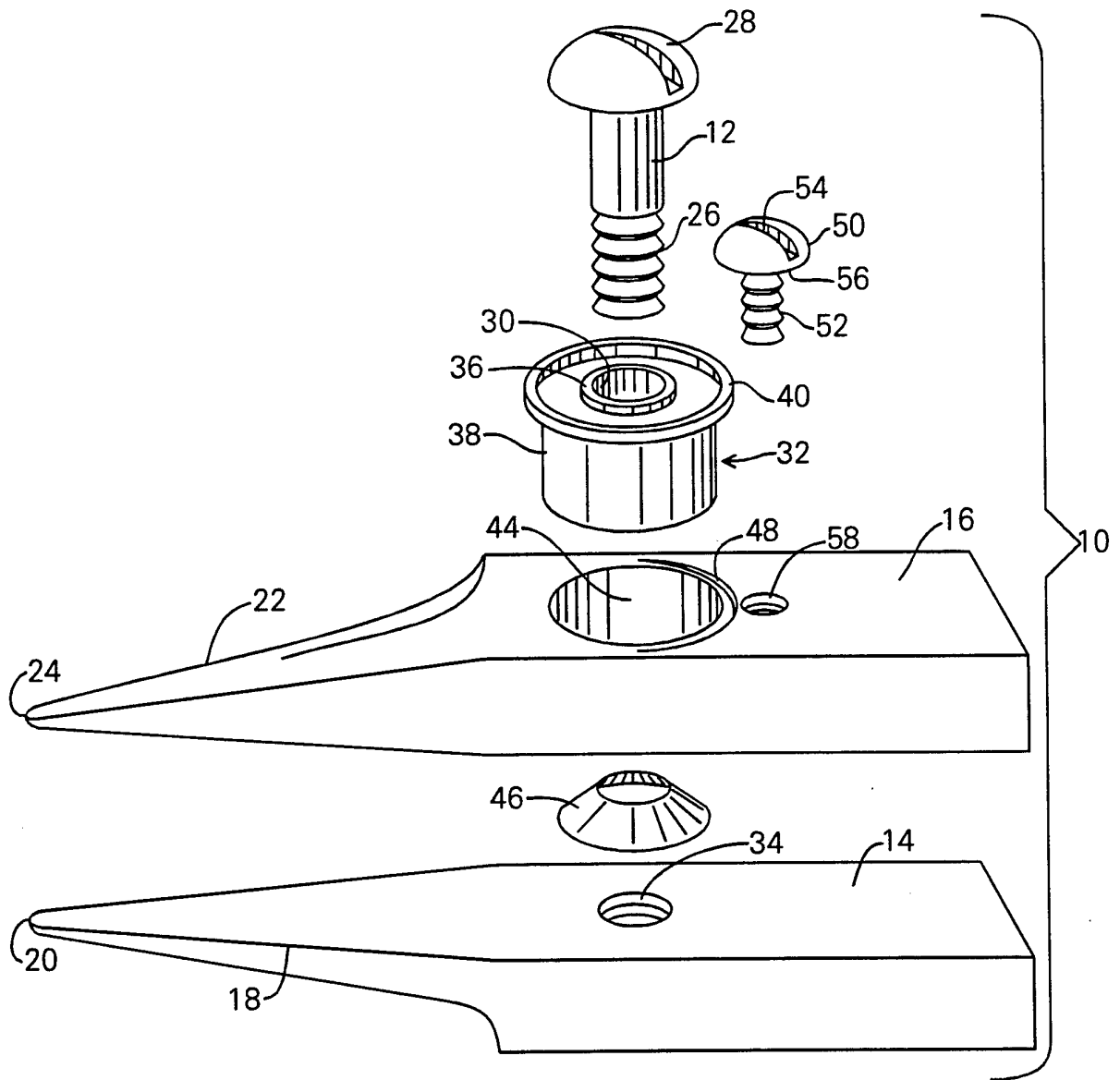


FIG. 3

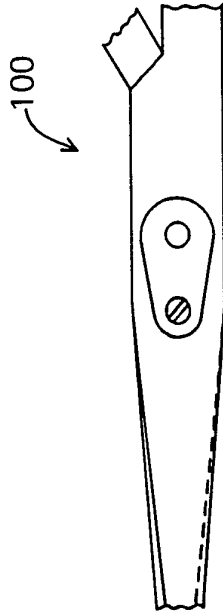


FIG. 5

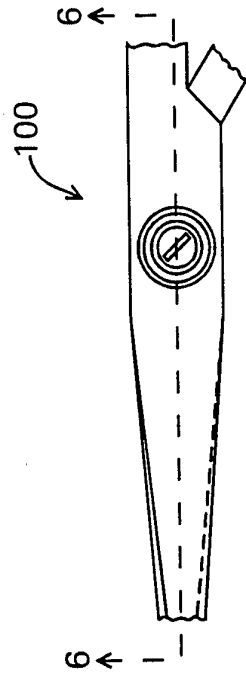


FIG. 4

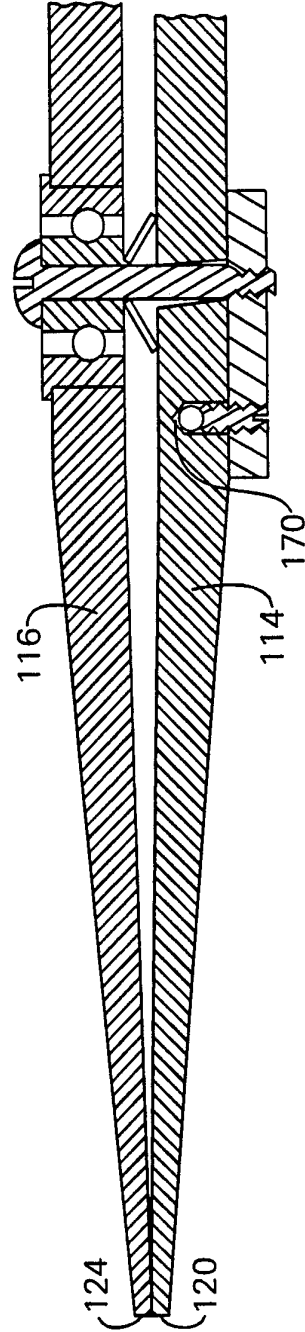


FIG. 6

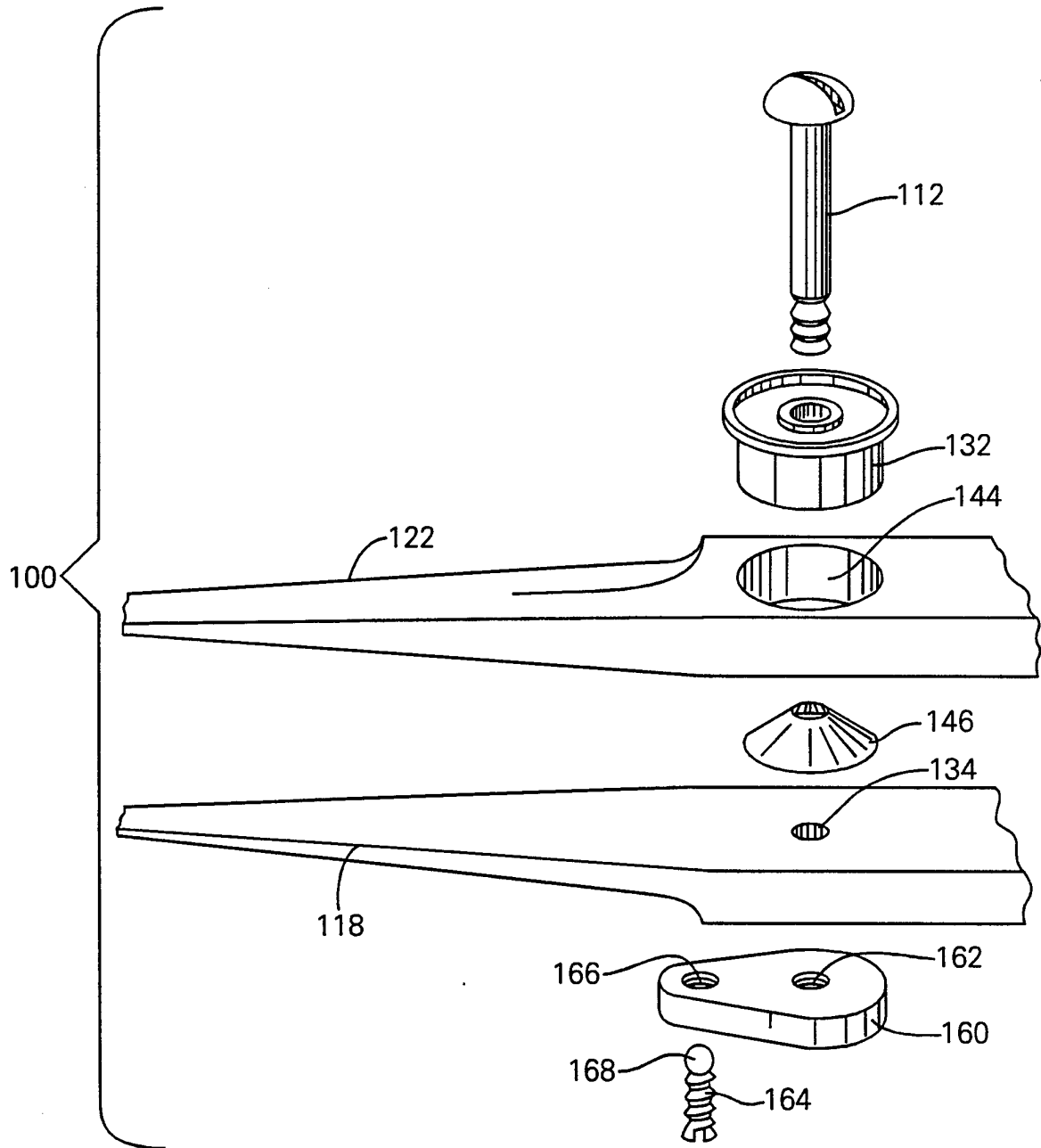


FIG. 7

INTERNATIONAL SEARCH REPORT

International application No.
PCT/US94/06222

A. CLASSIFICATION OF SUBJECT MATTER
 IPC(5) :B26B 13/28
 US CL :30/254, 266, 267; 29/434, 525.1; 76/106.5
 According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED
 Minimum documentation searched (classification system followed by classification symbols)
 U.S. : 30/254, 260, 266-271; 29/434, 525.1; 76/106.5; 16/273, 275; 81/416

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched
 NONE

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)
 NONE

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X -- Y	US, A, 3,170,237 (WEIDAUER) 23 February 1965, col. 2, lines 17-51.	1-6, 12-15, 21 ----- 7-9, 11, 16-18, 20
Y	US, A, 923,621 (BOWES) 01 June 1909, lines 9-19, 72-102.	7-9, 11, 16-18, 20
A	US, A, 672,050 (WILLIAMSON) 16 April 1901.	1-21
A	US, A, 951,236 (CRIDER) 08 March 1910.	1-21
A	US, A, 2,436,560 (FEATHER) 24 February 1948.	1-21
A	US, A, 2,469,373 (FEATHER) 10 May 1949.	1-21

Further documents are listed in the continuation of Box C. See patent family annex.

* Special categories of cited documents:	"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"A" document defining the general state of the art which is not considered to be part of particular relevance	"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"E" earlier document published on or after the international filing date	"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)	"&" document member of the same patent family
"O" document referring to an oral disclosure, use, exhibition or other means	
"P" document published prior to the international filing date but later than the priority date claimed	

Date of the actual completion of the international search 26 JULY 1994	Date of mailing of the international search report 10 AUG 1994
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Name and mailing address of the ISA/US Commissioner of Patents and Trademarks Box PCT Washington, D.C. 20231 Facsimile No. (703) 305-3230	Authorized officer Rinaldi I. Rada Joe Hill Telephone No. (703) 308-1148
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INTERNATIONAL SEARCH REPORT

International application No.
PCT/US94/06222

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	GB, A, 491,853 (BARTLETT) 09 September 1938.	1-21
A	DD, A, 807,771 (MUNCHEN ET AL.) 06 March 1952.	1-21