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(54) HIGH-PRESSURE DISCHARGE LAMP OPERATING DEVICE

EINRICHTUNG ZUM BETRIEB EINER HOCHDRUCK-ENTLADUNGSLAMPE

DISPOSITIF DE FONCTIONNEMENT DE LAMPE À DÉCHARGE À HAUTE PRESSION

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Description

Disclosure of the Invention

Technical Field

Problem to be solved by the Invention

[0001] The present invention relates to a high-voltage discharge lamp lighting system and, more particularly, to a high-voltage discharge lamp lighting system provided with a starting-pulse generation circuit.

Background Technique

[0002] Fig. 7 is a block diagram showing a conventional high-voltage discharge lamp lighting system. The high-voltage discharge lamp lighting system is constituted in such a manner that, when a commercial power source 1 is turned on, a control power supply circuit 10 produces a control power supply to operate a control circuit 9, which thus transmits a control signal to a boosting inverter 3, a voltage-dropping inverter 4, a rectangular wave circuit 6 and a starting pulse generation circuit 7; and thus, these elements start to operate, respectively. The boosting inverter 3 boosts the output, which has been rectified by a rectifier circuit 2, up to a normal voltage, and the voltage-dropping inverter 4 adjusts its output so that the current flowing to a high-voltage discharge lamp 8 can become a normal current. A rectangular wave circuit 6 outputs an AC rectangular voltage of a normal frequency to a high-voltage discharge lamp 8. The rectangular wave circuit 6 outputs an AC rectangular voltage of a normal frequency. The starting pulse generation circuit 7 generates a high-voltage pulse to start the high-voltage discharge lamp 8.

[0003] Fig. 8 is a block diagram showing in detail the start pulse generation circuit 7. The start pulse generation circuit 7 operates to produce a high-voltage pulse only when the high-voltage discharge lamp 8 is to be started. The start pulse generation circuit 7 comprises a transformer T1, a FET (field-effect transistor) being a switching element which can be turned on or off by an external control signal, a capacitor C1 which is charged with a DC voltage Vcc which has been raised by a boosting inverter 3, an inductance L1 which performs the over-current protection of the FET, and a capacitor C2 which serves to block the high-voltage pulses, which are produced across the transformer T1, from running around into the rectangular wave circuit 6.

Patent Literature 1: JP Patent Application Disclosure No. (Hei) 11-307285.

Patent Literature 2: JP Patent Application Disclosure No. 2000-306688.

Patent Literature 3: JP Patent Application Disclosure No. 2002-75673.

[0004] In case of a high-voltage discharge lamp such as a high-luminance, high-voltage discharge lamp or the like, the start pulse voltage is prescribed to be 3 to 5 kVp, for example. In case of the high-voltage discharge lamp lighting system, if the length of the output wiring is increased, then the start pulse voltage is attenuated by the resulting increase of the output capacity and thus becomes lower than the normal voltage value of the starting pulse voltage of the lamp, so that, in case the output wiring length is 10 m for example, there occurs the problem that the lamp cannot start. Therefore, there is the rule according to which the output wiring length of a high-voltage discharge lamp lighting system must be 2 meters or less; and this serves as a restriction on the make-up of said system (See Fig. 9). If a high-voltage discharge lamp lighting system is constructed in such a manner that a starting pulse voltage of 4 kVp is outputted at a point of the output wiring length which point lies 10 meters ahead, then it is accepted, but, if this high-voltage discharge lamp lighting system is operated within a distance of 2 meters, then the starting pulse voltage becomes higher than 5.6 kVp, so that there is caused the danger that a leak may be caused in the wiring, the socket, the high-voltage discharge lamp or the like.

[0005] The present invention has been made in order to give a solution to the above-mentioned problem, and it is the object of the present invention to provide a high-voltage discharge lamp lighting system constructed in such a manner that, by the feedback of a starting pulse voltage, said starting pulse voltage is stabilized, whereby the starting pulse voltage can be maintained within a normal value range even if the output wiring length is increased to enhance the output capacity.

[0006] The high-voltage discharge lamp lighting system according to the present invention which comprises a high-voltage discharge lamp, a starting pulse generation circuit which feeds a high starting voltage to said high-voltage discharge lamp, and a control circuit for controlling said starting pulse generation circuit, characterized in that

said starting pulse generation circuit comprises a boosting transformer for raising the pulse voltage generated by the ON/OFF operation of a switching element, a feedback voltage detection winding provided to said transformer, a voltage division circuit for dividing the voltage produced across said feedback voltage detection winding, and a pulse detection circuit for detecting the starting pulse voltage component from the output delivered from said voltage division circuit and feeding back the thus detected pulse voltage component to said control circuit.

Effect of the Invention

[0007] The high-voltage discharge lamp lighting system can maintain the starting pulse voltage within the normal range of values.

Brief Description of the Drawings

[0008]

[Fig. 1] shows Embodiment 1 of the present invention, wherein there is shown, particularly, the output voltage of the starting pulse generation circuit which (output voltage) is measured when the output wiring length is altered.

[Fig. 2] shows Embodiment 1 of the present invention, wherein there is shown, particularly, the result of the measurement of the starting pulse voltage when the wiring length is altered.

[Fig. 3] shows Embodiment 1 of the present invention, wherein there is shown, particularly, the result of the measurement of the starting pulse voltage when the wiring length is altered.

[Fig. 4] shows Embodiment 1, wherein there are shown, particularly, the results of measuring the FET voltage V (C) and the starting pulse voltage V (B) when the wiring length is altered.

[Fig. 5] shows Embodiment 1 of the present invention, wherein there are shown, particularly, the result of measuring the FET voltage V(C) and the starting pulse voltage VB when the wiring length is altered.

[Fig. 6] shows Embodiment 1 of the present invention, wherein, particularly, the starting pulse generation circuit is shown in detail.

[Fig. 7] is a block diagram showing the conventional high-voltage discharge lamp igniting system.

[Fig. 8] shows the conventional starting pulse generation circuit 7 in detail.

[Fig. 9] shows the relationship between the conventional high-voltage discharge lamp lighting system and the starting pulse voltage thereof.

Explanation of Reference Numerals

[0009] 1: Commercial power supply, 2: Rectifier circuit, 3: Boosting inverter, 4: Voltage-lowering inverter, 5: Current-detecting resistor, 6: Rectangular wave circuit, 7: Starting pulse generation circuit, 8: High-voltage discharge lamp, 9: Control circuit, 10: Control power source circuit, 11: Voltage division circuit, 12: Pulse detection circuit.

Most desirable Embodiment for Execution of the Invention

Embodiment 1

[0010] Figs. 1 to 6 show Embodiment 1 of the present

invention, of which Fig. 1 shows the output voltage measurement of the starting pulse generation circuit 7 when the output wiring length is altered, Figs. 2 and 3 show the measurement results of the starting pulse voltage when the wiring length is altered, Fig. 4 and 5 show the voltage V(C) of the FET (Field-effect transistor) and the measurement result of the starting pulse voltage V(B) when the wiring length is altered, and Fig. 6 shows in detail the starting pulse generation circuit 7.

[0011] Additionally, the overall arrangement of the high-voltage discharge lamp igniting system is the same as that of the conventional high-voltage discharge lamp lighting system; however, the feature of this embodiment of the present invention lies in the starting pulse generation circuit 7.

[0012] As stated in the foregoing part, entitled "Background Technique", of this specification, if the output wiring length is increased, then the starting pulse voltage value falls; and thus, if the starting pulse voltage value comes to fall below the starting voltage of the high-voltage discharge lamp, then there is caused, in some cases, even the inconvenience that the high-voltage discharge lamp does not start. Generally, in the case of a high-voltage discharge lamp lighting system, the output wiring length is stipulated to be two meters or shorter. The starting of the high-voltage discharge lamp becomes irregular in case the starting pulse voltage value is 3.5 kVp, and, in case the starting pulse voltage value is 3.0 kVp, the high voltage discharge lighting system does not start.

[0013] According to the present patent application, there is proposed a starting system constructed in such a manner that, by feeding back the starting pulse voltage, a reliable starting voltage value is secured, so that no failure is caused in the starting of the lamp.

[0014] For the realization of the above-mentioned starting system, it is indispensable to assure that the below-stated two conditional points be satisfied:

(1) The first point is that the values, at a point A and a point B, of the output voltage from a starting-pulse generation circuit 7 are approximately equal to each other. For example, in case the voltage at the point B is 3 kVp even if the voltage at the point A is 5 kVp, the lamp is not started even if the output voltage (which has a value approximately the same value as the voltage value at the point A) of the starting pulse generation circuit is fed back.

(2) In the case of controlling the starting-pulse voltage, the starting pulse voltage is a high voltage of 3 to 5 kVp, and thus, it is necessary to use a large number of high voltage-withstanding parts, so that the structure is large-sized. Further, even if such high voltage-withstanding parts are mounted, they will prove to be useless at the ordinary lighting time. The voltage to be fed back is suitably 10 Vp or so. In the starting-pulse generator circuit 7 shown in Fig. 8, a transformer T1 is used, but, if there is a correlation between the FET voltage V(C) before the voltage is

boosted and the starting pulse voltage V (B) being the voltage at a point B positioned ahead of the output wiring length, then the voltage at the point B located ahead of the output wiring length becomes controllable by controlling the FET voltage V (C) which is the lower voltage.

[0015] Thus, the starting pulse voltage V (A) and the starting pulse voltage V(B) at the point A and the point B in Fig. 1 referred to in the above Item (1) were measured by varying the output wiring length. The wiring used in this experiment is a VVF cable. The result of this measurement is shown in Figs. 2 and 3. Concerning the output wiring lengths, 0, 0.5, 1, 2, 4, 6, 8 and 10 meters, the starting pulse voltage V(A) and the starting pulse voltage V (B) at point A and point B were measured. As a result, it was confirmed that, as shown in Figs. 2 and 3, the starting pulse voltage V(A) and the starting pulse voltage V(B) at the point A and at the point B are approximately equal to each other irrelevantly to the output wiring length. Accordingly, if, for example, the starting pulse voltage V(A) is controlled to 4 kVp, then the starting pulse voltage V(B) can also be controlled to approximately 4 kVp.

[0016] Next, in order to confirm what is stated in above Item (2), the FET voltage V (C) and the starting voltage V(A) before the boosting by the transformer T1 were measured; and the result thus obtained is shown in Figs. 4 and 5.

[0017] It has been found that, as shown in Figs. 4 and 5, the FET voltage V(C) and the starting pulse voltage V(A) are correlated to each other; that is, by controlling the FET voltage V(C) which is low in voltage value, the starting pulse voltage V (A) can be controlled. The FET voltage V(C) is less than 1/10 of the starting pulse voltage V(A). It is sufficient to feed back a voltage which is lower than 1/10 of the starting pulse voltage V (A); and thus, the system can be made of a small-sized circuit. The FET voltage V (C) is higher than the desirable voltage, 10 VP which is desirable for the feedback, but, if said FET voltage V(C) is sufficient to be about 300 Vp though it is greater than 10 Vp desirable for the feedback, then the feedback circuit can be composed by the use of a plurality, yet small in number, of circuit parts.

[0018] By reference to Fig. 6, explanation will now be made concerning the starting pulse generation circuit 7 according to this embodiment of the present invention. To a transformer T1, a feedback voltage detection winding N3 is added. More concretely, if, for example, a primary winding N1 is made of 6 turns of a wire, a secondary winding N2 is made of 88 turns of a wire, and a feedback voltage detection winding N3 is made of 1 turn of a wire, then it results that the FET voltage V(C) = 300 Vp, the starting pulse voltage (A) = 4.4 kVp, and the feedback voltage V(F) = 50 Vp.

[0019] To the feedback voltage detection winding N3, a voltage division circuit 11 is connected. The voltage division circuit 11 is made of, e.g. a resistor, whereby the given voltage is divided to arbitrary voltages. As the feed-

back voltage, it is also possible to lower the given voltage to the order of 10 Vp.

[0020] Moreover, to the voltage division circuit 11, a pulse detection circuit 12 is connected. In the output of the voltage division circuit 11, various voltage components are contained in addition to the necessary starting pulse voltage component. The pulse detection circuit 12 detects the starting pulse voltage component from among these voltage components.

[0021] Then the output from the pulse detection circuit 12 is fed back to a control circuit 9. This control circuit 9 controls the FET voltage V(C) so that the starting pulse voltage V (A) may become a fixed voltage of, for example, 4 kVp.

[0022] As mentioned above, according to this embodiment of the present invention, a low voltage (for example, 50 Vp) across the feedback voltage winding N3 provided in the transformer T1 is further divided, by the voltage division circuit 11, to a still lower voltage, whereby a necessary starting pulse voltage component is detected by the pulse detection circuit 12 and fed back to the control circuit 9; and therefore, the starting pulse voltage V (A) can be maintained at, e.g. 4 kVp. It has been confirmed that, up to about 10 meters in length of the output wiring, the starting pulse voltage remains approximately the same without regard to the output wiring length, so that, if the starting pulse voltage V(A) is maintained at the above-mentioned 4 kVp, then the starting pulse voltage at a point 10 meters ahead can also be held at approximately the same voltage value.

Claims

1. A high-voltage discharge lamp lighting system which has a high-voltage discharge lamp (8), a starting pulse generation circuit (7) for feeding a starting high-voltage to said high-voltage discharge lamp (8), and a control circuit (9) for controlling said starting pulse generation circuit (7),
characterized in that
said starting pulse generation circuit (7) comprises a transformer (T1) for boosting a pulse voltage produced by an ON/OFF operation of a switching element (FET),
a feedback voltage detection winding (N3) provided to said transformer (T1),
a voltage division circuit (11) for dividing the voltage produced across said feedback voltage detection winding (N3), and
a pulse detection circuit (12) which detects a starting pulse voltage component from the output of said voltage division circuit (11) and feeds it back to said control circuit,
wherein said control circuit (9) maintains, at a predetermined value, the voltage after it is boosted by said transformer (T1).

Patentansprüche

1. Hochspannungsentladungslampen-Beleuchtungssystem, das eine Hochspannungsentladungslampe (8), eine Startimpuls-generierungsschaltung (7) zum Liefern einer Starthochspannung an die Hochspannungsentladungslampe (8) und eine Steuerschaltung (9) zum Steuern der Startimpuls-generierungsschaltung (7) aufweist, 5
dadurch gekennzeichnet, dass 10
 die Startimpuls-generierungsschaltung (7) Folgendes umfasst:

 einen Transformator (T1) zum Verstärken einer durch einen Ein/Aus-Betrieb eines Schaltelements (FET) erzeugten Impulsspannung, 15
 eine Rückkopplungsspannungsdetektionswicklung (N3), die am Transformator (T1) vorgesehen ist,
 eine Spannungsteilungsschaltung (11) zum Teilen der an der Rückkopplungsspannungsdetektionswicklung (N3) erzeugten Spannung und 20
 eine Impulsdetektionsschaltung (12), die eine Startimpulsspannungskomponente vom Ausgang der Spannungsteilungsschaltung (11) detektiert und sie an die Steuerschaltung zurückkoppelt, 25
 wobei die Steuerschaltung (9) die Spannung, nachdem sie durch den Transformator (T1) verstärkt ist, auf einem vorbestimmten Wert hält. 30

Revendications

1. Système d'éclairage à lampe à décharge à haute tension possédant une lampe à décharge à haute tension (8), un circuit d'amorçage générateur d'impulsions (7) afin de fournir une haute tension d'amorçage à ladite lampe à décharge à haute tension (8) et un circuit de commande (9) pour commander ledit circuit d'amorçage générateur d'impulsions (7), **caractérisé en ce que** ledit circuit d'amorçage générateur d'impulsions (7) comprend un transformateur (T1) pour amplifier une tension d'impulsion produite par une opération ON/OFF d'un élément de commutation (FET), un bobinage de détection de tension de rétroaction (N3) fournie audit transformateur (T1), un circuit de division de tension (11) pour diviser la tension produite à travers ledit bobinage de détection de tension de rétroaction (N3) et un circuit de détection d'impulsion (12) qui détecte un composant de tension d'impulsion d'amorçage au départ de la sortie dudit circuit de division de tension (11) et le renvoie audit circuit de commande, dans lequel ledit circuit de commande (9) maintient la tension à une valeur prédéterminée après qu'elle a été amplifiée par ledit transformateur (T1). 35
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50
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Fig. 1

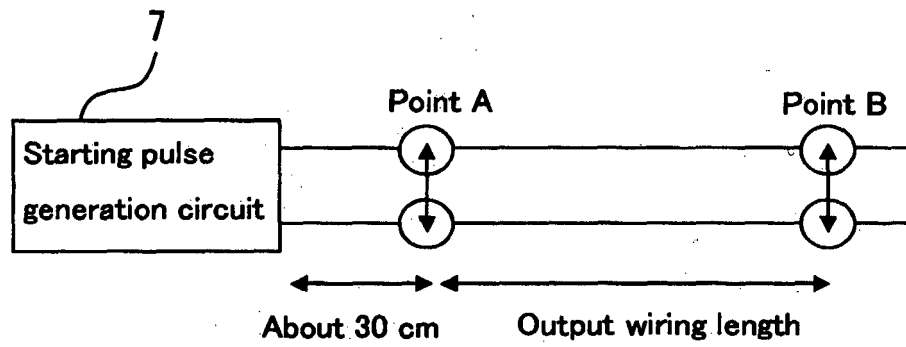


Fig. 2

Starting pulse voltage (Unit: kVp)

Output wiring length (m)	V (A)	V (B)
0	4.23	4.24
0.5	4.11	4.13
1	4.04	4.06
2	3.71	3.75
4	3.40	3.41
6	3.09	3.09
8	2.76	2.76
10	2.51	2.48

Fig. 3

Output wiring length – Starting pulse voltage

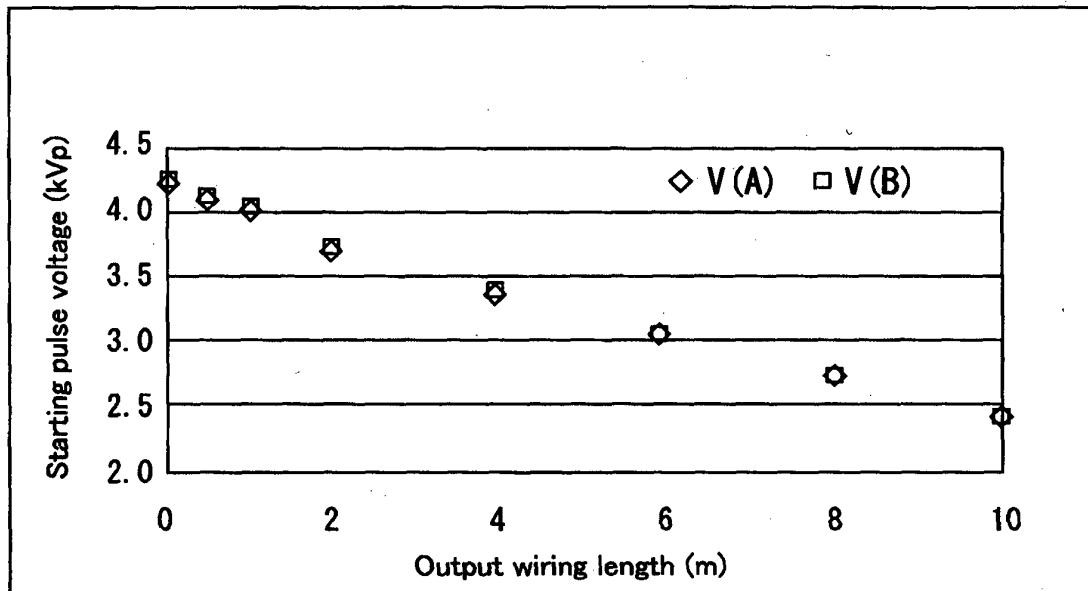


Fig. 4

Output wiring length (m)	FET voltage V(C) (Vp)	Starting pulse voltage V(A) (kVp)
0	302	4.404
0.5	304.8	4.384
1	294	4.208
2	286	4.028
3	262.8	3.688
6	226	3.184
9	189.6	2.72

Fig. 5

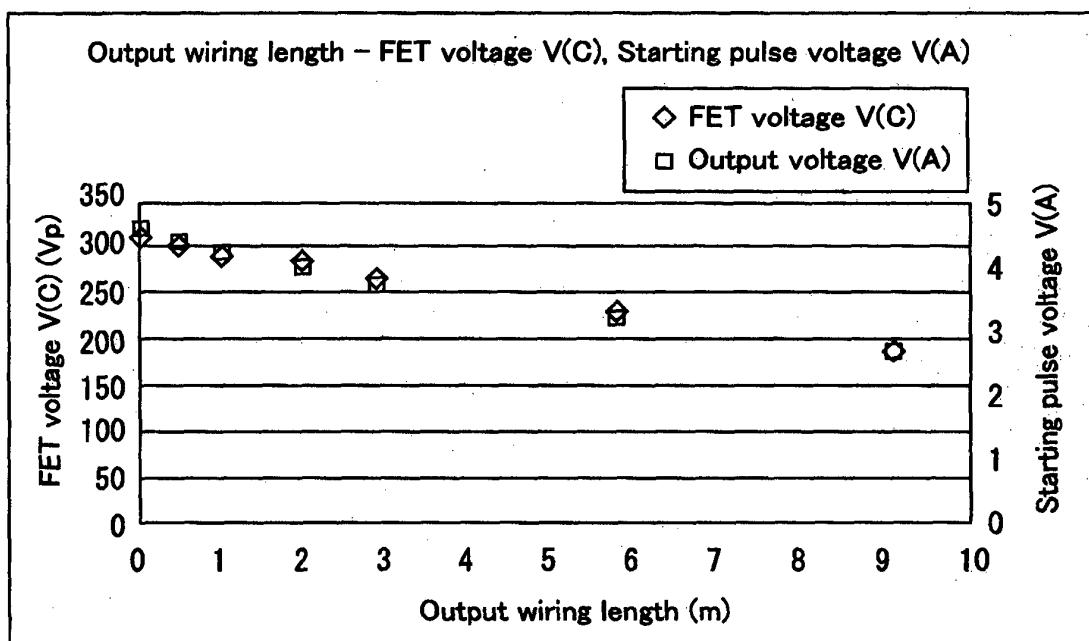
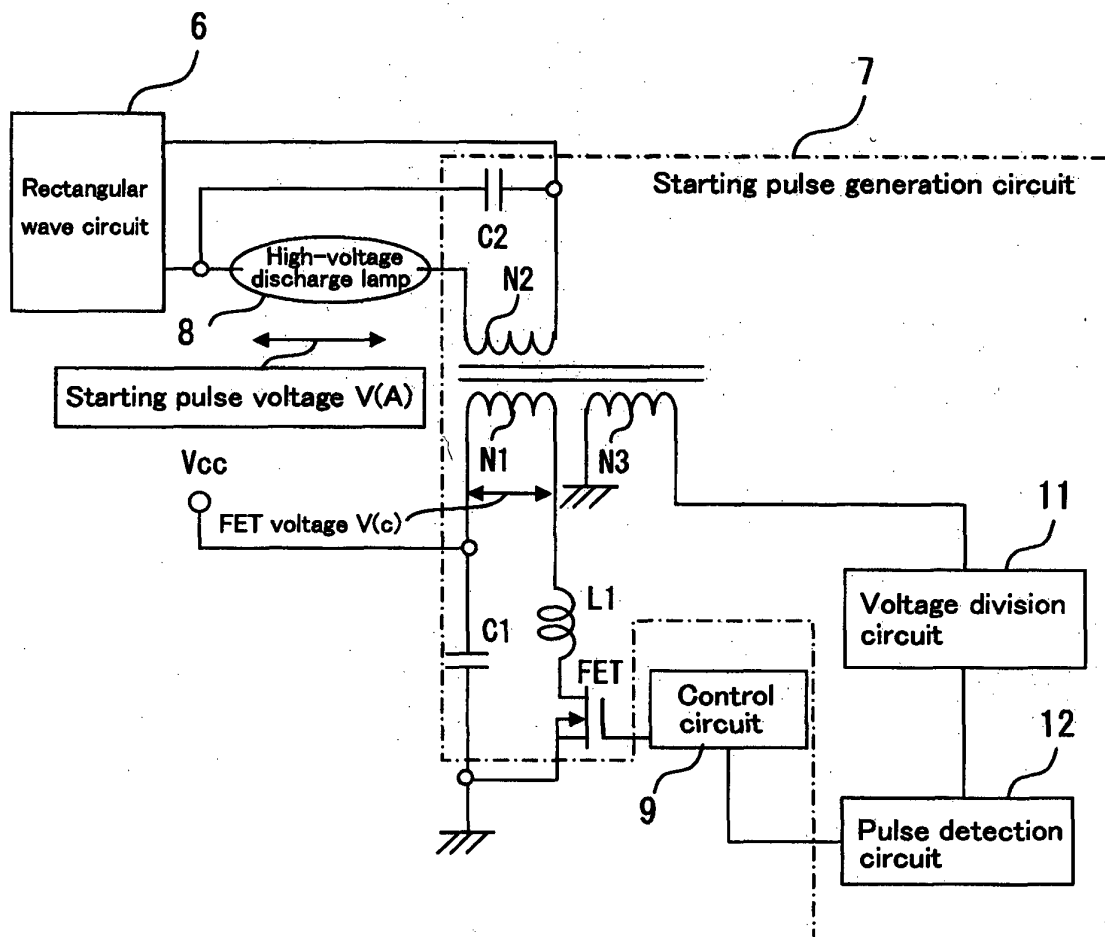


Fig. 6



C1, C2: Capacitors

FET: Field-effect transistor (an example of the switching element)

L1: Inductance

N1: Primary winding

N2: Secondary winding

N3: Feed-back voltage detection winding

T1: Transformer

Fig. 7

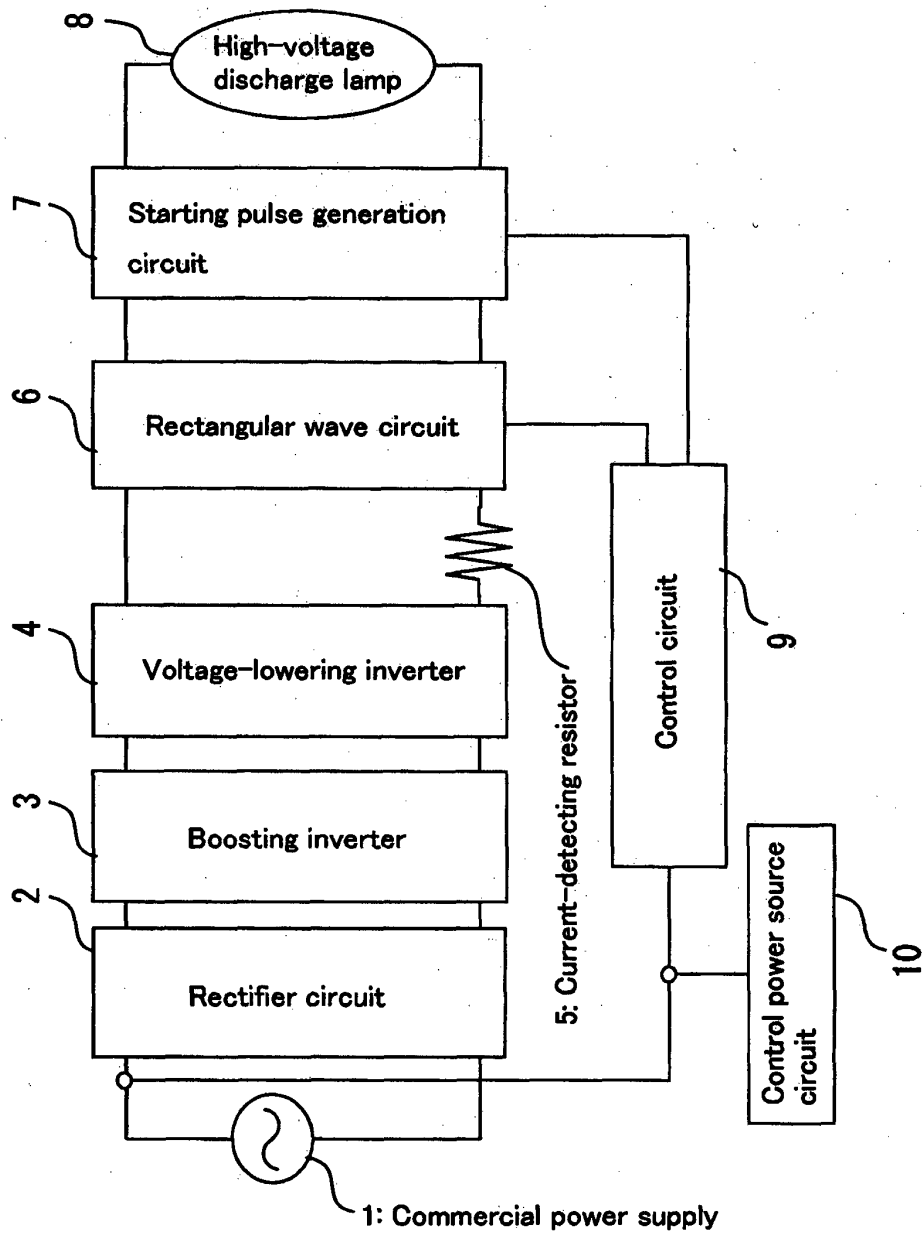


Fig. 8

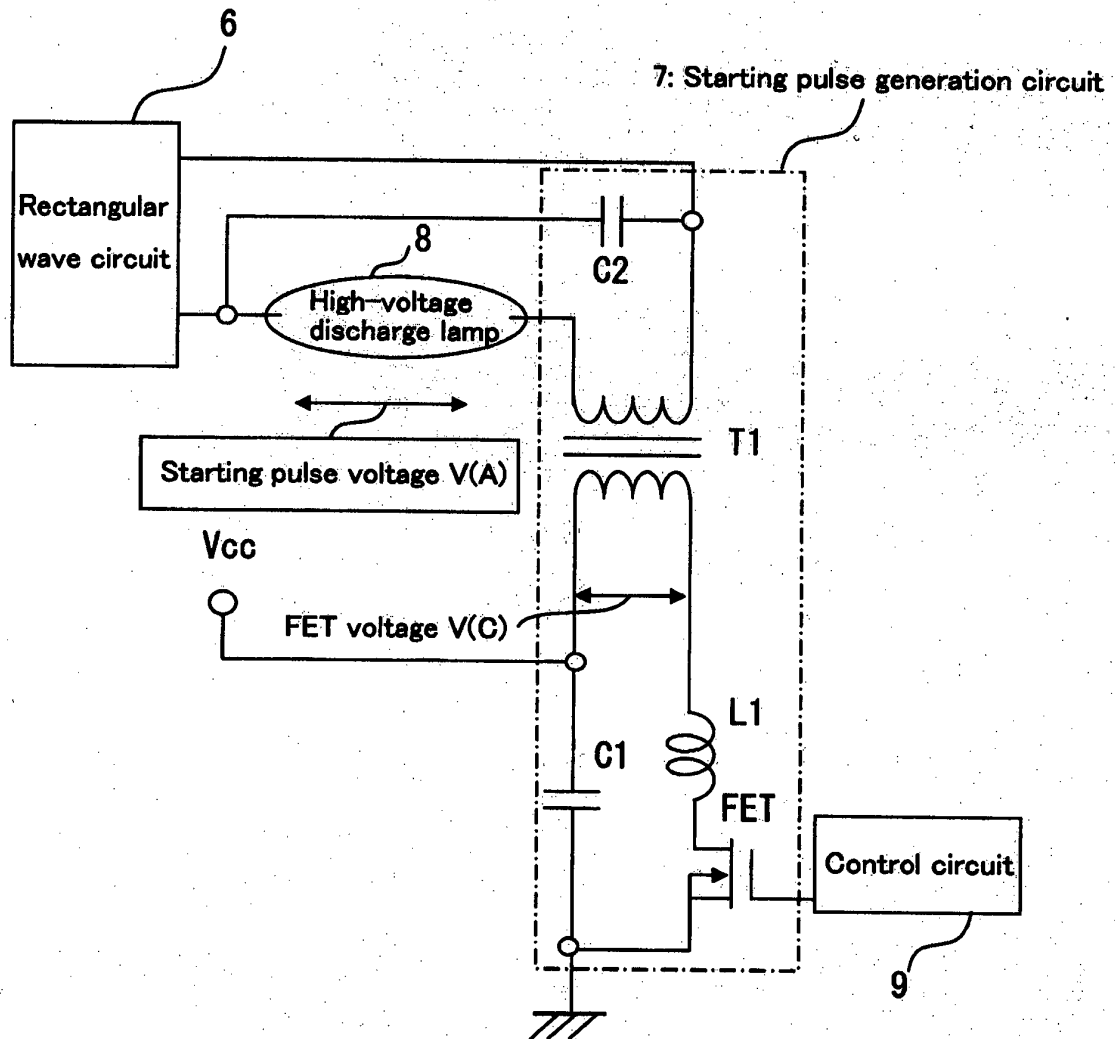
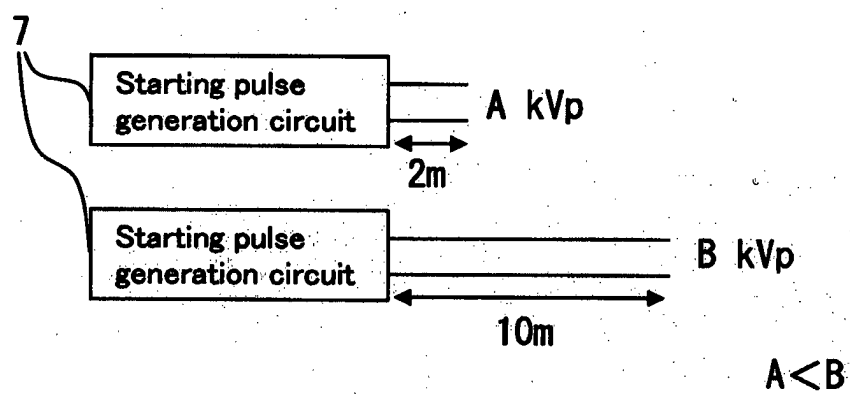


Fig. 9



REFERENCES CITED IN THE DESCRIPTION

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