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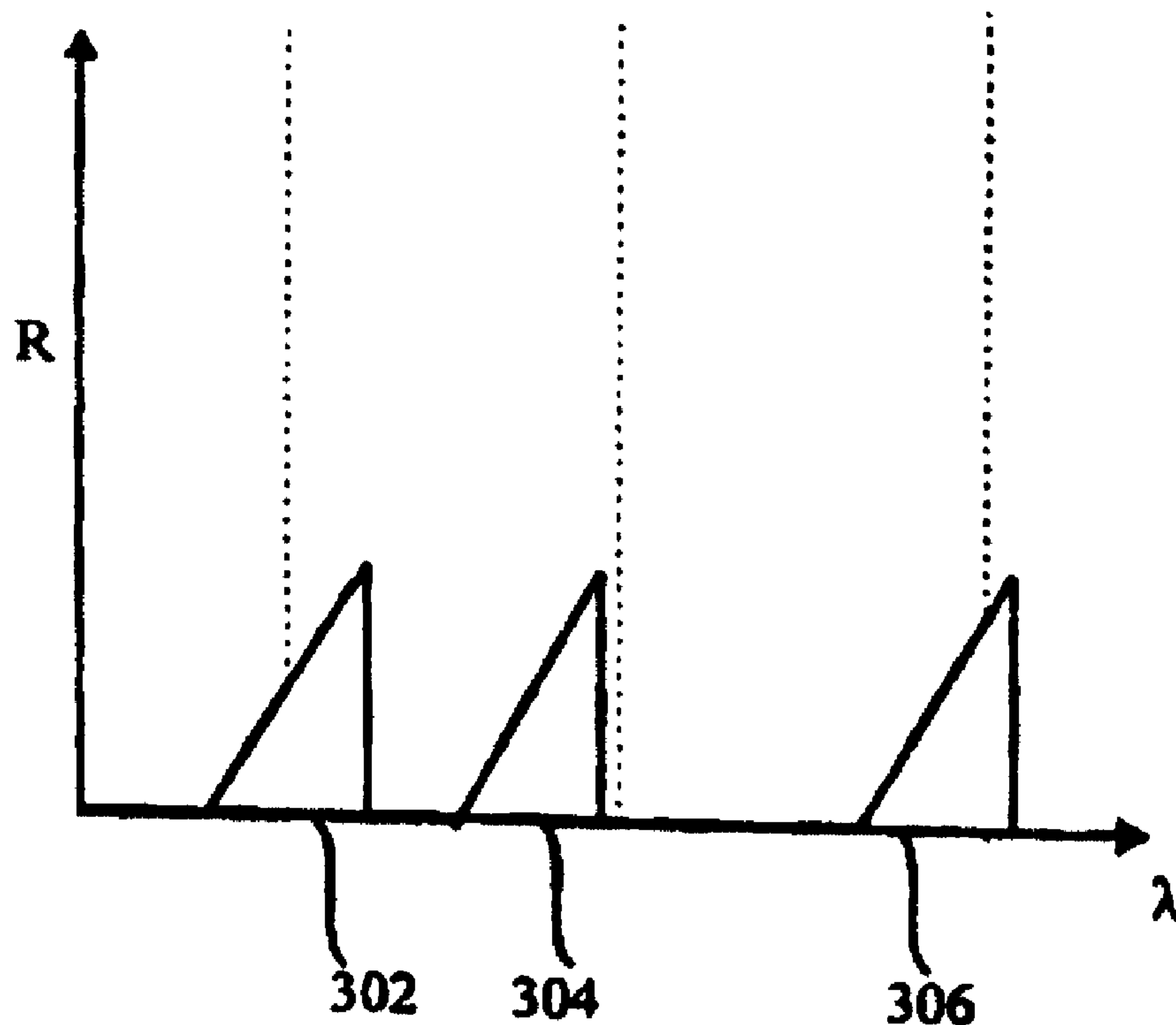
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(57) Abrégé/Abstract:

An attenuator capable of controllably attenuating at least two wavelengths of light is configured to have an optical waveguide section having at least two Bragg gratings disposed therein in series. The Bragg gratings have a sloped reflectivity response within a predetermined wavelength range. The sloped response is a function of refractive index variations within each of the grating elements. By compressing or expanding at least one of the gratings, the periodicity is modified so as to shift its central wavelength within a predetermined wavelength range.

Abstract of the Disclosure

An attenuator capable of controllably attenuating at least two wavelengths of light is configured to have an optical waveguide section having at least two Bragg gratings disposed
5 therein in series. The Bragg gratings have a sloped reflectivity response within a predetermined wavelength range. The sloped response is a function of refractive index variations within each of the grating elements. By compressing or expanding at least one of the gratings, the periodicity is modified so as to shift its central wavelength within a predetermined wavelength range.

Variable Attenuator

Field of the Invention

- 5 This invention relates generally to a Bragg grating disposed within a waveguide and more particularly, the principal focus of this invention relates to but is not limited to Bragg gratings embedded in the core of an optical fibre.

Background of the Invention

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Various constructions of optical filters are known however so-called Bragg filters are gaining popularity. One type of a Bragg filter, which has been developed for sensing stress and/or temperature changes in structures is incorporated or embedded in the core of an optical fiber by a method disclosed, for instance, in United States patent number 4,807,850. As is
15 discussed in this patent permanent periodic gratings of this kind can be provided or impressed in the core of an optical fibre by exposing the core through the cladding to the interference pattern of two coherent beams of ultraviolet light that are directed against the optical fibre symmetrically to a plane normal to the fiber axis. This results in a situation where the material of the fiber core has permanent periodic variations in its refractive index impressed
20 therein by the action of the interfering ultraviolet light beams thereon, with the individual grating elements (i.e. the periodically repetitive regions of the core exhibiting the same refractive index behavior) being oriented normal to the fiber axis so as to constitute the Bragg grating. The embedded Bragg grating of this kind reflects the light launched into the fiber core for guided propagation therein, in a propagation direction; only that light having a
25 wavelength within a very narrow range dependent on the grating element periodicity is reflected back along the fibre axis opposite to the original propagation direction, while being substantially transparent to light at wavelengths outside the aforementioned narrow band so that it does not adversely affect the further propagation of such other light. In effect, this type of grating creates a narrow notch in the transmission spectrum, and by the same token a

similarly narrow peak in the reflection spectrum. In the applications for which this kind of Bragg filter has been developed, any stresses or temperature changes encountered at the location of the structure in which the Bragg filter is embedded affect the grating and change its periodicity, or the index of the refraction of the material of the core, or both so that the position of the central wavelength in the spectrum is shifted, thus providing an indication of the stress or temperature changes existing or taking place in the structure being monitored at the location of the grating. Although the significance of these applications of Bragg gratings are formidable, further development in this area is disclosed in United States patent number 5,007,705 (hereafter referred to as the '705 patent) that relates to a different aspect or use of these earlier discovered principles. In the '705 patent various means are disclosed for intentionally shifting the reflection wavelength response of a Bragg grating. By deliberately varying the period of the grating or altering the index of refraction in a predetermined manner, by external forces or actions on the fibre section containing the grating in a controlled manner, a variable light filtering element is provided. Furthermore, tuning a grating by various means such as the application of heat, compression, or stretching are all known.

One useful application of the principals described heretofore, can be found in United States patent number 5,446,809 in the name of Fritz et al. who discloses an optical fiber wavelength selective optical switch, utilizing tunable Bragg fibre gratings. The fiber wavelength selective switch has one or more $1 \times N$ input optical couplers and utilizes a plurality of in-line Bragg fiber gratings in series along multiple parallel paths. For a given wavelength of light to pass through a particular grating, the grating must be detuned. By providing a plurality of Bragg gratings in series, each designed to reflect a different wavelength, and having means for controlling or shifting the response of each grating individually, signals can selectively be passed through a fibre or can be reflected backwards in a binary on-off fashion. Although the prior art describes a plurality of modes and means for varying the output response of a Bragg grating within an optical fibre, there remains a need for useful

application of this technology that provides a non-binary response. For example, there remains a need for a variable attenuator or equalizer that utilizes Bragg grating technology.

Therefore, it is an object of this invention to provide an optical equalizer that incorporates
5 Bragg gratings.

It is yet a further object of the invention to provide a multi-channel equalizer.

Summary of the Invention

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In accordance with the invention, there is provided, an attenuator capable of controllably variably attenuating at least two wavelengths of light independently, comprising: an optical waveguide section having a plurality of Bragg grating elements disposed therein in series, at least two Bragg grating elements having an inclined or sloped reflectivity response within a
15 predetermined wavelength range that is determined by the periodicity and refractive index variations of the grating elements; and, means for so applying at least to one grating element of the optical waveguide section an external influence to modify the periodicity of the at least one grating element to shift its central wavelength within a predetermined wavelength range.

20 In accordance with the invention, there is provided, an attenuator capable of controllably attenuating at least two wavelengths of light independently, comprising:
an optical waveguide section having a plurality of Bragg grating elements disposed therein in series, at least two Bragg grating elements having a sloped reflectivity response within a predetermined wavelength range that is determined at least in part by refractive index
25 variations of the grating elements;
and means for so applying at least to one grating element of the optical waveguide section an external influence to modify a periodicity of the at least one grating element to shift its central wavelength within a predetermined wavelength range.

In accordance with the invention, there is further provided, a wavelength selective optical attenuator for attenuating an input signal having a predetermined wavelength, comprising: an optical waveguide having an input port and an output port;

at least one optical reflective element located along said optical waveguide between the input
5 port and the output port, said reflecting element reflecting a predetermined wavelength band of light centred at a predetermined central wavelength, said central wavelength being at a base wavelength when said reflective element is not detuned, said base wavelength including a predetermined offset corresponding to the predetermined wavelength of said input signal, said optical reflective element having a reflectivity along its length that varies such that one
10 end of the grating is substantially more reflective than another end; and, tuning means, attached to said reflective element for detuning said central wavelength away from said base wavelength and towards the wavelength of the input signal so as to attenuate said corresponding wavelength of said input signal.

15 **Brief Description of the Drawings**

Exemplary embodiments of the invention will now be described, in conjunction with the drawings, in which:

20 Fig. 1 is a prior art schematic block diagram of an all fiber 2 x 2 wavelength selective optical switch utilizing tunable Bragg gratings as selective switching elements;

Fig. 2a is a schematic block diagram of multi-channel equalizer in accordance with an embodiment of the invention;

25 Fig. 2b is a schematic block diagram of multi-channel equalizer including feedback circuitry in accordance with an alternative embodiment of the invention;

Fig. 2c is a schematic block diagram of multi-channel equalizer similar to that shown in Fig. 2b however including 3 couplets of Bragg gratings;

Figs. 3a is a graph showing the amplitude wavelength response of three optical signals transmitted into the multi-channel equalizer in an unequalized form, prior to being attenuated;

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Fig. 3b is a graph showing the reflectivity wavelength response of three Bragg gratings corresponding to the circuit of Fig. 2b, including a first wavelength of which is shifted, the grating being stretched state, a second grating which is unstretched and not wavelength shifted, and a third grating which is stretched and wavelength shifted to achieve substantial
10 attenuation of a particular wavelength of light;

Fig. 3c is a graph showing the reflectivity wavelength response of three couplets of Bragg gratings, in accordance with the embodiment of the invention that corresponds to Fig. 2c;

15 Fig. 4 is a prior art pictorial view showing the bending and stretching of a Bragg grating non-uniformly over a bending form;

Detailed Description

20 As was described heretofore, United States patent number 5,446,809 discloses an optical switch shown in Fig. 1, wherein Bragg gratings are used as controllable, selective, transmissive / reflective binary elements that are capable of transmitting a predetermined wavelength of light or alternatively reflecting that wavelength in dependence upon the period of the grating. A piezo-electric transducer is coupled to each grating; and when a particular
25 transducer is energized it stretches the grating, changing its period, and thus changes its reflectivity response by shifting it in wavelength. In this patent the Bragg gratings operate in a binary "on-off" manner to either reflect a particular wavelength of light or transmit that wavelength of light.

As described in US 5,446,809 referring to FIG. 1, an all fiber, wavelength selective 2 x 2 optical switch has a first optical input signal 10 which travels along an input port optical fiber 12. The optical signal 10 comprises a plurality of wavelengths $\lambda_1, \lambda_2, \lambda_3$, each wavelength acting as an optical carrier for analog or digital information in a multi-wavelength communication system. Any number of wavelengths may be used if desired limited only by the overall optical bandwidth of the system and individual grating wavelength width. The optical fiber 12 is fed to an optical isolator 14 which prevents light from exiting the input line 12 and disrupting the optical components, e.g., lasers, up-stream from the input.

10 The optical signal 10 exits the isolator 14 as indicated by a line 16 to a 1 x 2 optical coupler 20 (e.g., a 2 x 2 coupler configured as a 1 x 2 coupler in a known way). The coupler 20 couples a predetermined amount, e.g., 50% or 3 dB, of the input signal 16 to an output port 22 as a signal 24 on a fiber 26. The remaining portion, e.g., 50%, of the optical signal 16 exits from a port 28 from the coupler 20 as a signal 30 on a fiber 32. Thus, both output
15 signals 24,30 comprise all the wavelengths of the input signal 10, both having reduced power, e.g., 50%.

The optical signal 24 is incident on a first Bragg grating 34 embedded in the fiber 26. A Bragg grating, as is known, reflects a narrow wavelength band of light centered at a reflection
20 wavelength and passes through all other wavelengths, as described in U.S. Pat. No. 4,725,110, "Method for Impressing Gratings within Fiber Optics," to Glenn et al.

The grating 34 reflects a narrow wavelength band of light 36 centered at a wavelength λ_1 and passes all remaining wavelengths as indicated by a line 38. The light 38 is incident on a
25 second grating 40 embedded in the fiber 26 which reflects a narrow wavelength band of light 42 centered at a reflection wavelength λ_2 and passes all remaining wavelengths as indicated by a line 44. Similarly, the light 44 travels along the fiber 24 and is incident on a third grating 46 which reflects a narrow wavelength band of light 48 centered at a reflection wavelength λ_3 and passes all other wavelengths as indicated by a line 50.

Each of the gratings 34,40,46 on the fiber 26 has a piezo-electric tuner (or PZT) or stretcher 52,54,56 attached to the gratings 34,40,46, respectively. A PZT, as is known, expands with applied voltage and is used herein to stretch Bragg grating, thereby tuning the Bragg grating to a different reflection wavelength or "detuning" the Bragg grating from its original reflection wavelength. The PZT's 52,54,56 are individually controlled by control lines 57 from a tuner control circuit 58. The control circuit 58 contains known electronic components necessary to drive the PZT's and to perform the functions described herein, and is not critical to the invention. Also, any other type of stretcher or tuning device, including a thermal heater, may be used if desired. Some alternative grating tuning devices are discussed in U.S. Pat. No. 5,007,705, entitled "Variable Optical Fiber Bragg Filter Arrangement," to Morey et al.

The light 36,42,48 reflected by the gratings 34,40,46, respectively, are collectively indicated by a line 59 which re-enters the coupler 20 at the port 22 and is coupled to the input fiber 18 as indicated by a line 60. The signal 60 enters the isolator 14 but does not exit the isolator 14 on the fiber 12 due to the properties of the isolator which are known. Similarly, the light 38,44,50 which is passed through the gratings 34,40,46, respectively, are collectively indicated by a line 62 which travels along the fiber 24 to an input port 64 of a 2 x 1 3 dB (or 50/50) optical coupler 66. The coupler 66 couples a predetermined amount (e.g., 50%) of the light 62 to an output port 68 and onto a fiber 70 as indicated by a line 72 which represents one of the output lines of the optical switch of the invention. Other percentages or power ratios may be used if desired.

When each of the gratings 34,40,46 are in their unstretched state, i.e., having their central reflection wavelength at their base wavelengths λ_1 , λ_2 , λ_3 , respectively, the reflected light 59 will comprise all three input wavelengths and the passed signal 62 will not contain these wavelengths. Thus, if the input signal 10 contains only the wavelengths λ_1 , λ_2 , λ_3 , the signal 62 would be 0 or dark. However, when the PZT 52 stretches the grating 34 such that the reflection wavelength shifts from λ_1 or is "detuned" to some other wavelength, e.g., λ_a , as

indicated by a line 206 in FIG. 2, the reflection signal 59 will now comprise only λ_2 and λ_3 , and the passed signal 62 will now comprise λ_1 .

A similar situation occurs if the grating 40 is also "detuned" by the PZT 54 so as to shift the reflection wavelength λ_2 to a different wavelength λ_6 , as indicated by a line 208 in FIG. 2. In that case, the reflection signal 59 would contain only the wavelength λ_3 and the passed signal 62 would comprise the wavelengths λ_1 and λ_2 . A similar situation occurs for wavelength λ_3 and the grating 46.

Thus, by "detuning" any one of the gratings 34,40,46 the passed signal 62 will comprise the wavelengths of the gratings which have been detuned. Consequently, the invention in its most fundamental sense can be viewed as a single input, single output multiple wavelength selective switch which allows any one of or any combination of input wavelengths on the input fiber 12 to be coupled to the output fiber 26 based on control lines 57 from the tuner control circuit 58 which individually control the tuners 52,54,56 attached to the gratings 34,40,46 along the fiber 26.

A similar arrangement exists for the fiber 32 where a plurality of gratings 80,82,84 are embedded along the fiber 32, each having a reflection wavelength λ_1 , λ_2 , λ_3 , respectively, and each having a PZT 86,88,90 attached thereto, respectively. Light collectively reflected from the gratings 80,82,84 is indicated by a line 92 and light passed by the gratings 80,82,84 are indicated collectively by a line 94 along the fiber 32. The fiber 32 is fed to a first port 96 of a 2 x 1, 3 dB (50/50) optical coupler 98, which couples a predetermined amount, e.g., 50%, of the light 94 to an output port 100 along the fiber 102 as indicated by a line 104.

In another fundamental configuration of the present invention, a single-input dual-output, wavelength selective optical switch is provided at the output signals 62,94 where the outputs would be the fiber 26 and the fiber 32. This would allow any one of or any combination of the input wavelengths λ_1 , λ_2 , λ_3 to be selectively switched to either the output line 26 or the

output line 32 or both.

Because many communication systems allow input signals from different laser optical sources, where each source provides common wavelength carriers, any communication switching network must provide for a plurality of inputs, one from each of such different optical source. Consequently, a second input optical fiber 110 carries a second optical input 112 comprising a plurality of wavelengths, e.g., λ_1' , λ_2' , λ_3' , these being the same wavelengths as those on the first input line 12, however, being from a different source and thus carrying different information on the carrier wavelengths. Line 110 is fed to an optical isolator 114 (similar to the isolator 14) which prevents light from exiting along the input line 110. The signal 112 exits the isolator as the optical signal 116 on a fiber 118. The optical fiber 118 is fed to an optical 1 x 2 3 dB (50/50) coupler. The coupler 120 couples a predetermined portion (e.g., 50%) of the light 116 to an output port 122 as indicated by a line 124 on a fiber 126.

The light 124 on the fiber 126 is incident on a series of three fiber gratings 128,130,132 impressed in series along the fiber 124. Similar to the gratings on the fibers 26 and 32, discussed hereinbefore, the gratings 128,130,132 have central reflection wavelengths of λ_1 , λ_2 , λ_3 , respectively. Similarly, the gratings 128,130,132 have PZT's 134,136,138 attached thereto respectively, similar to that discussed for the gratings on the fiber 26 and 32. The light reflected by the gratings 128,130,132 is collectively indicated by a line 140 and the light passed by the gratings 128,130,132 is collectively indicated by a line 142. Reflected light 140 re-enters the coupler 120 at the port 122 and a portion (e.g., 50%) exits the coupler onto the fiber 118 as indicated by a line 144. The light 144 is incident on the isolator 114 which prevents the light from exiting the input fiber 112 and disrupting any up-stream optical sources.

The fiber 126, along which the passed optical signal 142 travels, is connected to a second input port 150 of the coupler 66. The coupler 66 couples a predetermined amount, e.g., 50%, of the light 142 to the output port 68 onto the output fiber 70, as indicated by a line 72.

Symmetrically, the coupler 120 couples a predetermined amount, e.g. 50%, of the light 116 to an output port 154 as indicated by a line 156 along a fiber 158. The light 156 is incident on a plurality of gratings 160,162,164 impressed in the fiber 158 in series in a similar fashion to the gratings of the fibers 26,32,126, as discussed hereinbefore. Similarly, each of the gratings 160,162,164 has a central reflection wavelength λ_1 , λ_2 , λ_3 , respectively, and has a PZT 166,168,170 attached thereto, respectively. The light reflected by the gratings 160,162,164 is collectively indicated by a line 172, and the light passed by the gratings 160,162,164 is indicated collectively by a line 174. The reflected light 172 re-enters the coupler 120 at the port 154 and the coupler 120 couples a predetermined amount (e.g., 50%) of the light 172 onto the fiber 118 as also indicated by the line 144. The light 144 enters the isolator 114 which prevents such reflected light from exiting along the input line 110 and disrupting upstream sources, as discussed hereinbefore.

The passed light 174 travels along the fiber 158 which is fed to an input port 176 of the coupler 98. The coupler 98 couples a predetermined amount (i.e., 50%) of the light 174 to the output port 100 onto the second output fiber 102 as indicated by the line 104. Thus the couplers 66 and 98 act as optical combiners of the signals 62,142 to the output signal 72 and of the signals 94,174 to the output signal 104.

The coupler 120 and the gratings on the fibers 126,158 operate in precisely the same fashion as discussed hereinbefore regarding the coupler 20 and fiber gratings and PZT's attached thereto on the fibers 26,32. In general, when all the gratings on a given fiber are not stretched (or not "detuned"), all the wavelengths of the input signal 112 are reflected for that fiber.

Similarly, when one of the gratings is "detuned" so as not to reflect at the unstretched reflection wavelength for that grating, that wavelength will pass through all of the series gratings on that fiber. Additionally, the couplers 66,98 act effectively as optical combiners. In particular, the optical coupler 66 combines the optical passed signal 62 from the gratings 34,40,46 along the fiber 24 and the optical passed signal 142 from the gratings 128,130,132

on the fiber 126, to the output fiber 70 as the signal 72. This allows any of the wavelengths on the first input line 12 to be coupled to the output fiber 70 and/or any of the same wavelengths on the second input line 110 to be coupled to the output fiber 70, having a similar amount of signal loss for both channels.

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Similarly, the optical coupler 98 acts as an optical combiner to combine the passed optical signal 94 from the gratings 80,82,84 along the fiber 32, and the passed signal 174 from the fiber gratings 160,162,164 along the fiber 158, to be provided along the second output fiber 102. This allows any of the wavelengths on the first input line 12 to be coupled to the second
10 output line 102, and/or any of the wavelengths on the second input 110 to be coupled to the second output fiber 102. Thus, this configuration, which is also known as a crossbar configuration in electronic networking, provides an optical crossbar switching network which allows any wavelength or combination of wavelengths along any input to be routed to any output, in combination with any wavelengths from any other input.

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Referring generally now to Figs. 2a to 2c, an equalizer circuit is shown wherein Bragg gratings or elements are utilized in a controllable manner to attenuate a multiplexed input optical beam comprising three signals of three wavelengths, λ_1 , λ_2 , and λ_3 . In the drawing, the three signals on the left side are unequal in amplitude, λ_2 having the least intensity, then
20 λ_1 followed by λ_3 having the highest intensity. In many instances it is preferred to have the optical signals equalized, wherein their amplitudes are as close as possible to one another. One use of the equalizer of this invention is with rare-earth doped optical fiber amplifiers.

One limitation of any rare-earth doped optical fibre amplifier is unequal gain over a
25 range of frequencies or optical channels of interest, as well as for various input signal strengths (i.e. different saturation levels). Over a 35 nanometer gain bandwidth, erbium doped fibre amplifiers (EDFAs) typically exhibit a 10 to 15 dB small-signal gain variation. In long chains of cascaded EDFAs small spectral gain variation can result in unacceptable large

difference in received optical power and therefore, it is preferable to lessen even small spectral variation in gain.

To date, several gain equalization and flattening techniques have been proposed and described in a variety of prior art references. For example, gain clamping with enhanced inhomogeneous saturation is described by V.L. da Silva et al. in an article entitled, "Automatic gain flattening in Er-doped-fiber amplifiers," in Proc. OFC'93, paper THD2, P.174, 1993. One of the limitations of this method is the requirement that fibre be cooled to 77 K. The use of passive internal/external filters has been explored by M. Tachibana, et al., in an article entitled, "Erbium-Doped Fiber Amplifier With Flattened Gain Spectrum," in IEEE Photonics Technol. Lett. 3, no. 2, 118, 1991; by M. Wilkinson, et al., in an article entitled, "D-Fibre Filter For Erbium Gain Spectrum Flattening," in Electron. Lett. 28, no. 2, p. 131, 1992; and by Kashyap, et al., in an article entitled, "Wideband Gain Flattened Erbium Fibre Amplifier Using a Photosensitive Fibre Blazed Grating," in Electron. Lett. 29, no. 2, P.154, 1993, and as well by Grasso et al, in an article entitled, "980-nm diode pumped Er-doped fiber optical amplifiers with high gain-bandwidth product," in Proc. OFC'91, paper FA3, p. 195, 1991. Another attempt to provide a doped optical fibre amplifier that is suitable for use over a range of frequencies is described in U.S. patent 5,245,467 entitled, "Amplifier with a Samarium-erbium Doped Active Fibre," issued September 14, 1993 in the name of Grasso et al. Although the invention described in the patent works well at particular wavelengths and for particular signal strengths, it has been found to be limited at other wavelengths. However, a major limitation with most of these devices and methods is the requirement for bulk optics and non-standard components. The use of external active acousto-optic filters has been explored by S.F.Su et al. in an article entitled, "Gain Equalization in Multiwavelength Lightwave Systems Using Acoustooptic Tunable Filters," in IEEE Photonics Technol. Lett. 4, no. 3, p.269, 1992; the drawback with this proposal is that it requires bulk optics, and is complex in design.

The exemplary circuit shown in Fig. 2a in conjunction with the responses shown Figs. 3b and 3c can be used to offset the unequalized gain over a wavelength region exhibited from commercially available erbium doped amplifiers; or, can be used to vary or offset the relative strengths of particular wavelengths prior to amplification so as to obtain a relatively
5 equalized signal after amplification. Although only three Bragg gratings 102, 104, and 106 are shown, other gratings can be included and chained in series tuned to other wavelengths of interest.

Referring specifically now to Fig. 2a, a circuit is shown wherein three Bragg gratings
10 102, 104, and 106 are shown in series written into an optical fiber 101. Tuning means in the form of individually controllable piezo-electric transducers 102a, 104a, and 106a are coupled to the respective gratings each for changing the period of a grating in dependence upon a control signal. A tuning control circuit 108 can be preprogrammed or programmed in real-time for issuing appropriate control signals to the transducers. Each of the Bragg gratings
15 102, 104, and 106 are designed to have a different period, and are consequently designed to affect a different channel. In one embodiment, the gratings are chirped, appodized gratings having a sloped or inclined reflectivity response as shown in Fig. 3b. Therefore the refractive index difference Δn between adjacent regions within each of the gratings varies along the length of the chirped grating so as to provide a sloped reflectivity response over a
20 predetermined wavelength region. Of course, other methods of forming reflective/transmissive elements having a variable reflectively response can be envisaged. One way of fabricating the grating is to provide a standard linear chirp using a mask; when exposing the fibre an amplitude mask can be utilized so that one side of the grating is exposed more so than the other, resulting in a periodicity that varies in refractive index rather
25 than in distance, providing a variable masked chirp. The effective Δn can be varied by varying the width of Δn sections. Another means of providing a sloped region is by using a very short hydrogen loaded grating, for example one having a 2nm bandwidth, can be utilized; by providing such a grating, tuning can be achieved by utilizing the falling or rising

edge of the gratings reflectivity response. By tuning or wavelength shifting these gratings a variable reflectivity response and consequently a variable amount of attenuation is provided. Another means of achieving a chirp in a grating is by stretching or bending a grating having a non-varying period in non-uniform manner. For example, a grating shown in prior art Fig. 4 is shown being bent over a form having non-uniform bend radius. By doing so, the period of the grating is changed in such a manner as to vary it along its length, thereby chirping the grating. The authors of this prior art reference, Variable- spectral response optical waveguide Bragg grating filters for optical signal processing by K. O. Hill et al., Optics Letters / Vol. 20, No. 12, June 15, 1995 disclose the usefulness of non-uniformly bending a grating, in relation to signal processing applications, for example for dispersion compensation; however, we have found a particularly useful feature that is less related to the processing of optical signals. The advantage of such a scheme is as follows; a substantially long grating with a uniform period typically has a very narrow reflectivity response; thus, when the grating is un-bent, it can be hidden or stored between adjacent channels essentially "tucked away". In the instance where an adjacent channel or wavelength range is to be attenuated, the grating can be bent and thereby chirped so that range of reflectivity broadens, in a manner similar to an opening curtain. Of course by stretching or compressing the grating its effective wavelength range shifts. Thus the grating response can be compressed, expanded, and/or shifted.

Standards and specifications are provided by the telecommunications industry regarding the minimum allowable or acceptable channel spacing between two transmission channels. In some instances where it is desired to have a plurality of channels within a small wavelength region, this spacing labeled G on Fig. 3a, is relatively small. In order to provide a grating having reflectivity response that conveniently lies within this space G in one mode of operation, and that can be shifted to have a reflectivity response that coincides with the wavelength or channel of interest λ_1 , λ_2 , or λ_3 in a variable manner so as to attenuate a particular channel by predetermined amount, the grating must have predetermined characteristics. For example, the grating of interest must be designed to have a slope of the reflectivity response that is suitable for a particular application. Fig. 3c shows an embodiment

wherein grating couplets are provided, each grating of a couplet of gratings, being tunable over substantially the same range, and wherein the couplet can share a same space G for convenient storage when no attenuation is required. In another embodiment compressive actuation means are also or alternatively coupled to each grating, or each other grating; in this arrangement one grating of a couplet can be used to attenuate an adjacent higher wavelength, while the other grating of a couplet can be utilized to attenuate an adjacent lower wavelength signal, by stretching of the gratings and compressing the other of the gratings a predetermined amount. It should be noted, that although the gratings shown are preferably impressed within an optical fibre, other optical waveguide structures can conveniently be utilized; for example a plurality of gratings can be written into a slab waveguide wherein heating elements can be used to control the wavelength reflectivity response of the gratings.

Turning now to Fig. 2b, a circuit is shown for equalizing an input beam of light. The circuit is similar in many respects to that of Fig. 2a, however includes a feedback circuit for providing information relating to the input beam after it has been attenuated. A tap, 112 taps, for example, 5% of the attenuated beam and couples this light to a circuit 116 for further processing. The tapped light is wavelength demultiplexed into three channels. The intensity of signals representing a 5% portion of wavelengths λ_1 , λ_2 , and λ_3 are measured by circuit 116 and converted to electrical signals by photodetectors (not shown). A tuner control circuit 114 in response to these electrical signals continuously and dynamically varies the response of the gratings 102, 104, and 106 by providing an appropriate voltage to the actuators 102a, 104a, and 106a. The circuit of Fig. 2c operates in a similar manner, however the tuner 124 provides appropriate voltages to six Bragg gratings, 102, 102b, 104, 104b, 106, and 106b.

Of course, numerous other embodiments may be envisaged, without departing from the spirit and scope of the invention.

Claims

What we claim is:

1. An attenuator capable of controllably attenuating at least two wavelengths of light
5 independently, comprising:
an optical waveguide section having a plurality of Bragg grating elements disposed therein in series, at least two Bragg grating elements having a sloped reflectivity response within a predetermined wavelength range that is determined at least in part by refractive index variations of the grating elements;
10 and means for so applying at least to one grating element of the optical waveguide section an external influence to modify a periodicity of the at least one grating element to shift its central wavelength within a predetermined wavelength range to vary the attenuation of a wavelength of light.
- 15 2. An attenuator as defined in claim 1, wherein the at least two Bragg grating elements have a refractive index difference between two adjacent locations denoted as Δn , and wherein Δn varies substantially linearly along each grating element increasing from one end to the other.
3. An attenuator as defined in claim 1, wherein the at least two Bragg grating elements are
20 chirped Bragg gratings and wherein the refractive index difference between two adjacent regions of a grating element Δn varies increasing from one end of a grating element to the other.
4. An attenuator as defined in claim 3, wherein two of the at least two Bragg grating elements
25 having a substantially same central reflectivity wavelength band of light centered at a predetermined central wavelength, and wherein their wavelength reflectivity responses are oppositely sloped.

5. An attenuator as defined in claim 1, wherein the means to apply the external influence to modify the period of the grating effectively chirp the grating by stretching or compressing at least a portion of the grating non-uniformly.

5 6. An attenuator as defined in claim 5, wherein said means to apply the external influence includes bending means.

7. A wavelength selective optical attenuator for attenuating an input signal having a predetermined wavelength, comprising:

10 an optical waveguide having an input port and an output port;
at least one optical reflective element located along said optical waveguide between the input port and the output port, said reflecting element for reflecting a predetermined wavelength band of light centered at a predetermined central wavelength, said central wavelength being at a base wavelength when said reflective element is not detuned, said base wavelength
15 including a predetermined offset corresponding to the predetermined wavelength of said input signal, said optical reflective element having a reflectivity along its length that varies such that one end of the reflective element is substantially more reflective than another end; tuning means, attached to said reflective element for detuning said central wavelength away from said base wavelength and towards the wavelength of the input signal so as to attenuate
20 said input signal.

8. A wavelength selective optical attenuator as defined in claim 7, wherein the optical reflective element is in the form of a Bragg grating having a plurality of hi and low index regions adjacent to one another each adjacent hi and low index region having a refractive
25 index difference Δn , and wherein Δn varies substantially linearly along the grating increasing from one end to the other.

9. A wavelength selective optical attenuator as defined in claim 8, comprising a plurality of Bragg gratings connected in series for attenuating at least two input signals having different

wavelengths, at least two of the Bragg gratings reflecting different predetermined wavelengths of light, the at least two Bragg gratings having a refractive index difference Δn which varies substantially linearly along each grating increasing from one end to the other, and comprising tuning means for tuning each of said Bragg gratings independent of the other.

5

10. A wavelength selective optical attenuator as defined in claim 9, wherein at least two Bragg gratings have an oppositely sloped reflection response and have a same base wavelength.

10 11. A wavelength selective optical attenuator as defined in claim 9 including means for detecting the intensity of at least a portion of the at least two input signals that have passed through the at least two Bragg gratings.

12. A wavelength selective optical attenuator as defined in claim 9 wherein the optical
15 waveguide is a planar waveguide.

13. A wavelength selective optical attenuator as defined in claim 11, including feedback means for controlling the tuning means in dependence upon a detected intensity of the at least a portion of the at least two input signals.

20

14. A wavelength selective optical attenuator as defined in claim 13, wherein the optical waveguide is in the form of an optical fibre.

15. An attenuator capable of controllably, variably, attenuating a wavelength of light
25 independently, comprising:

an optical waveguide section having a Bragg grating element disposed therein, said Bragg grating element having reflectivity response that varies in such a manner as to provide more than two levels of reflectivity within a predetermined wavelength range that is determined at

least in part by at least one of an effective periodicity and refractive index variations of the grating element;

and means for so applying to the grating element of the optical waveguide section an external influence to modify the periodicity of the at least one grating element to shift its central
5 wavelength within a predetermined wavelength range, so that at least a section of the varied reflectivity response may be coincident with the wavelength of light to thereby only partially attenuate said wavelength of light.

16. An attenuator comprising an optical waveguide having a tunable Bragg grating disposed
10 within, said grating having a reflectivity response over a predetermined wavelength range that varies between at least three different levels, and means for tuning the Bragg fibre grating so as to shift its response over that predetermined wavelength range.

17. An attenuator as defined in claim 16 including means for modifying the Bragg grating
15 along the length of the grating so as to controllably increase or decrease the bandwidth of the grating.

18. An attenuator as defined in claim 17, wherein said means includes bending means for bending the grating non-uniformly.

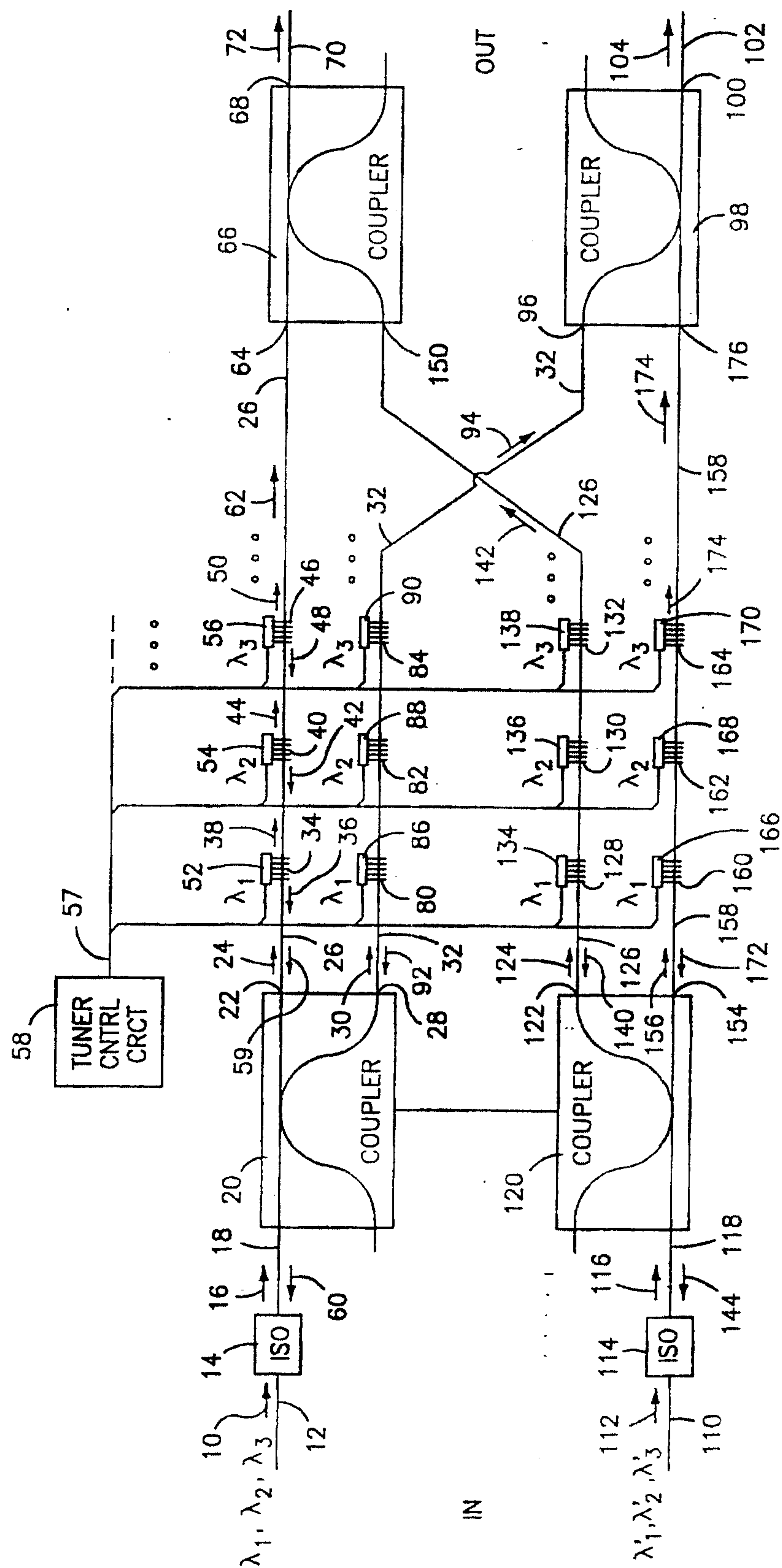


FIG-1 PRIOR ART

Fig. 2a

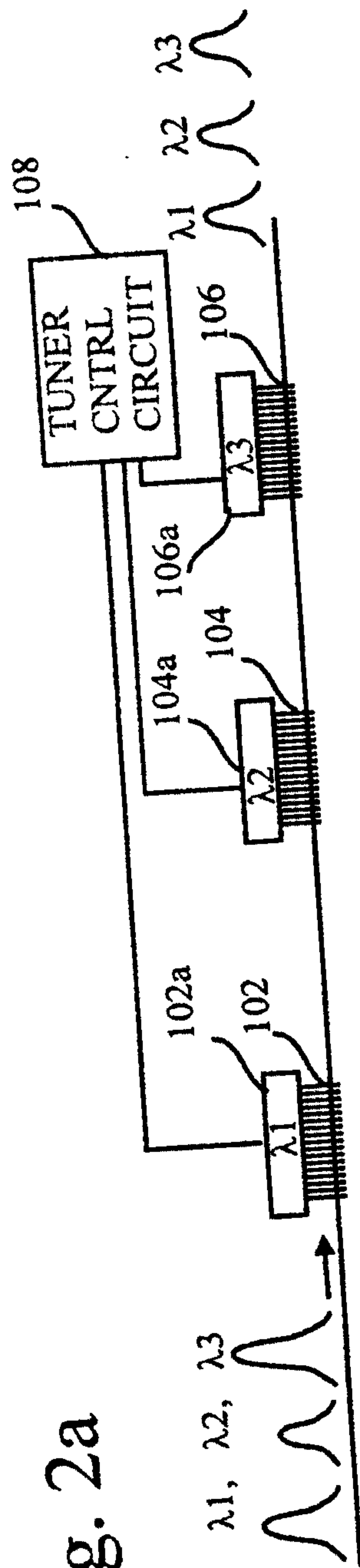


Fig. 2b

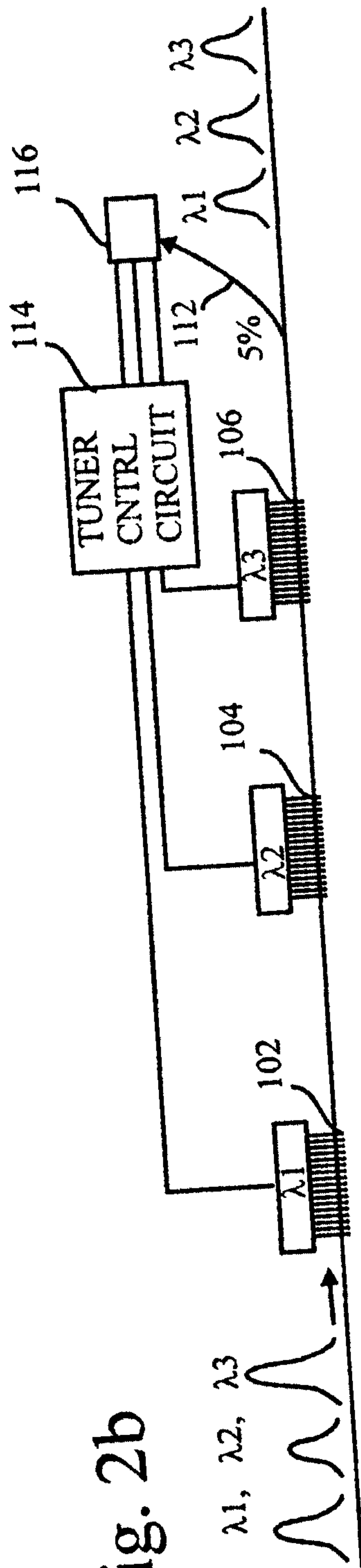


Fig. 2c

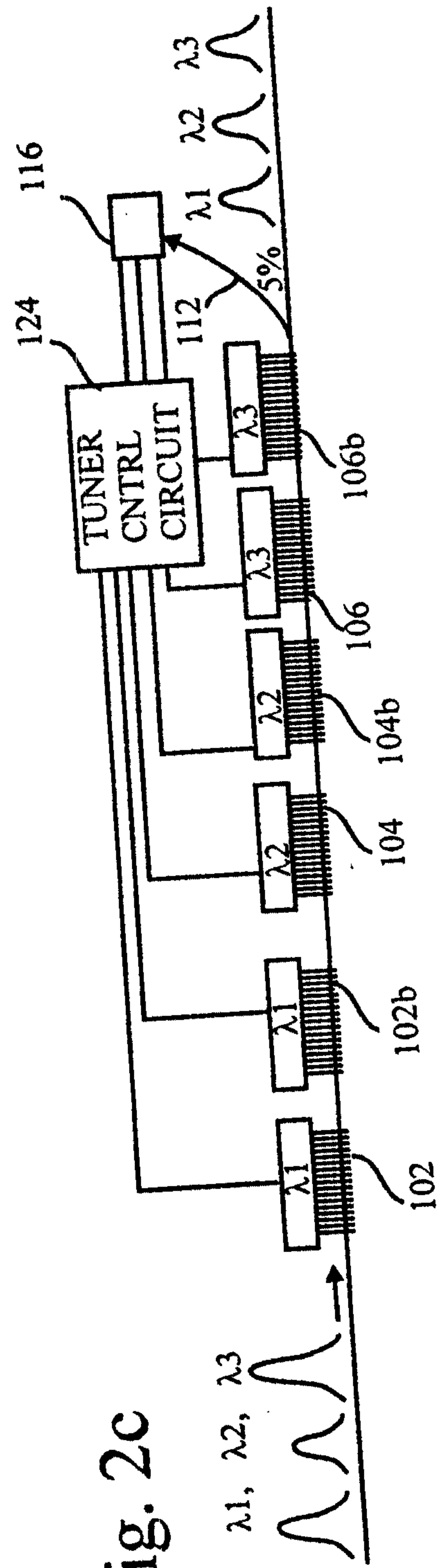


Fig. 3a

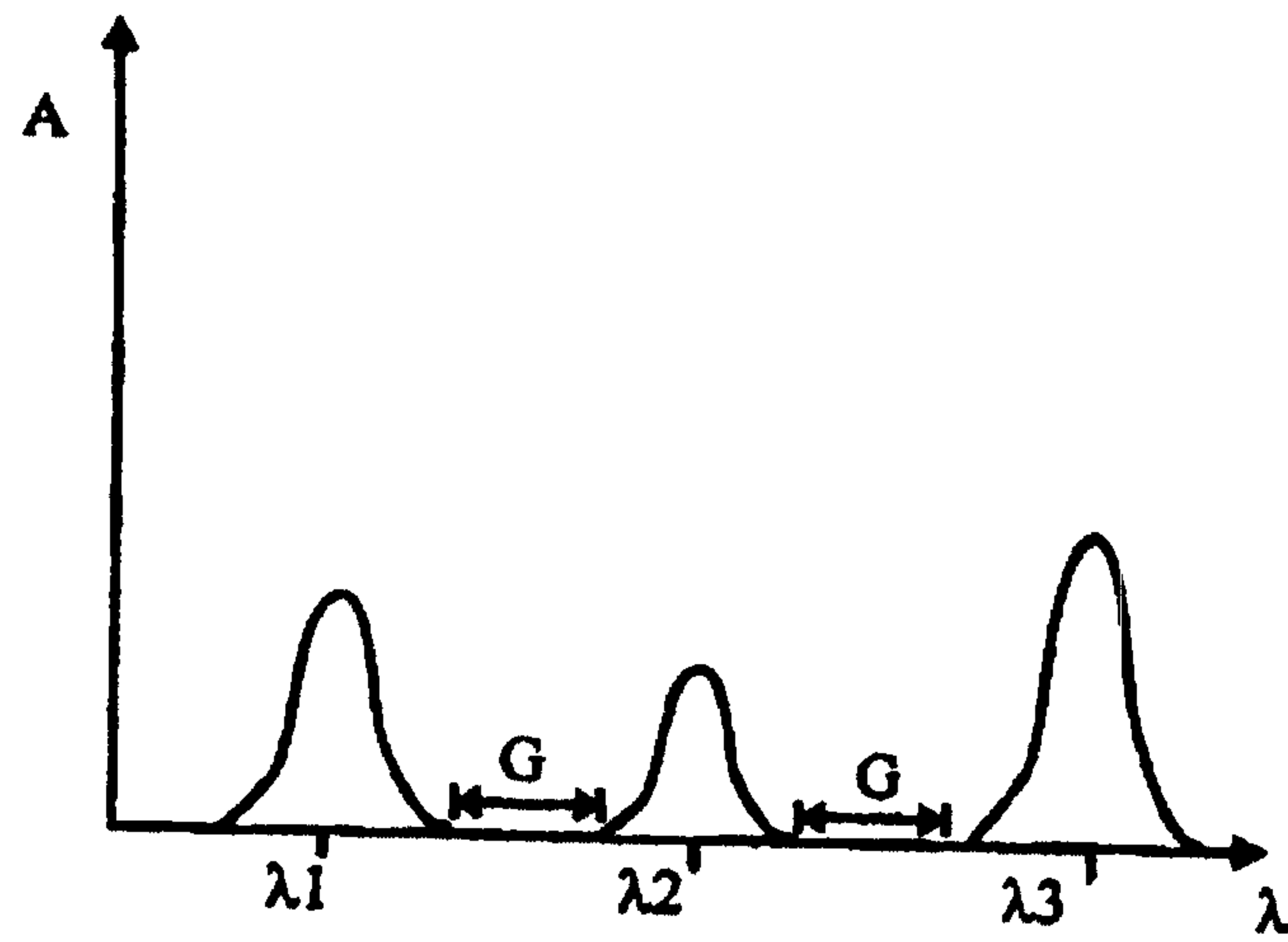


Fig. 3b

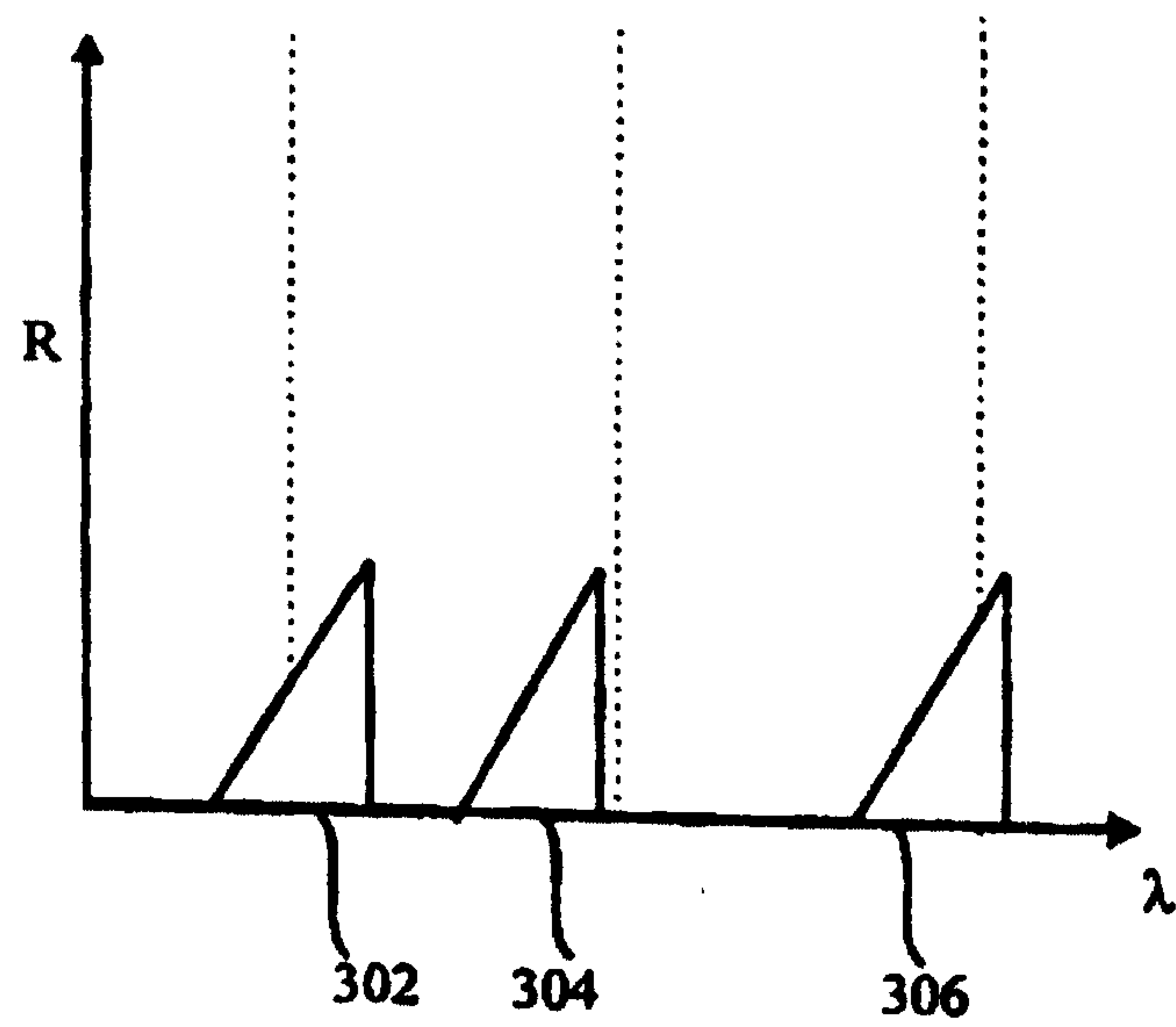
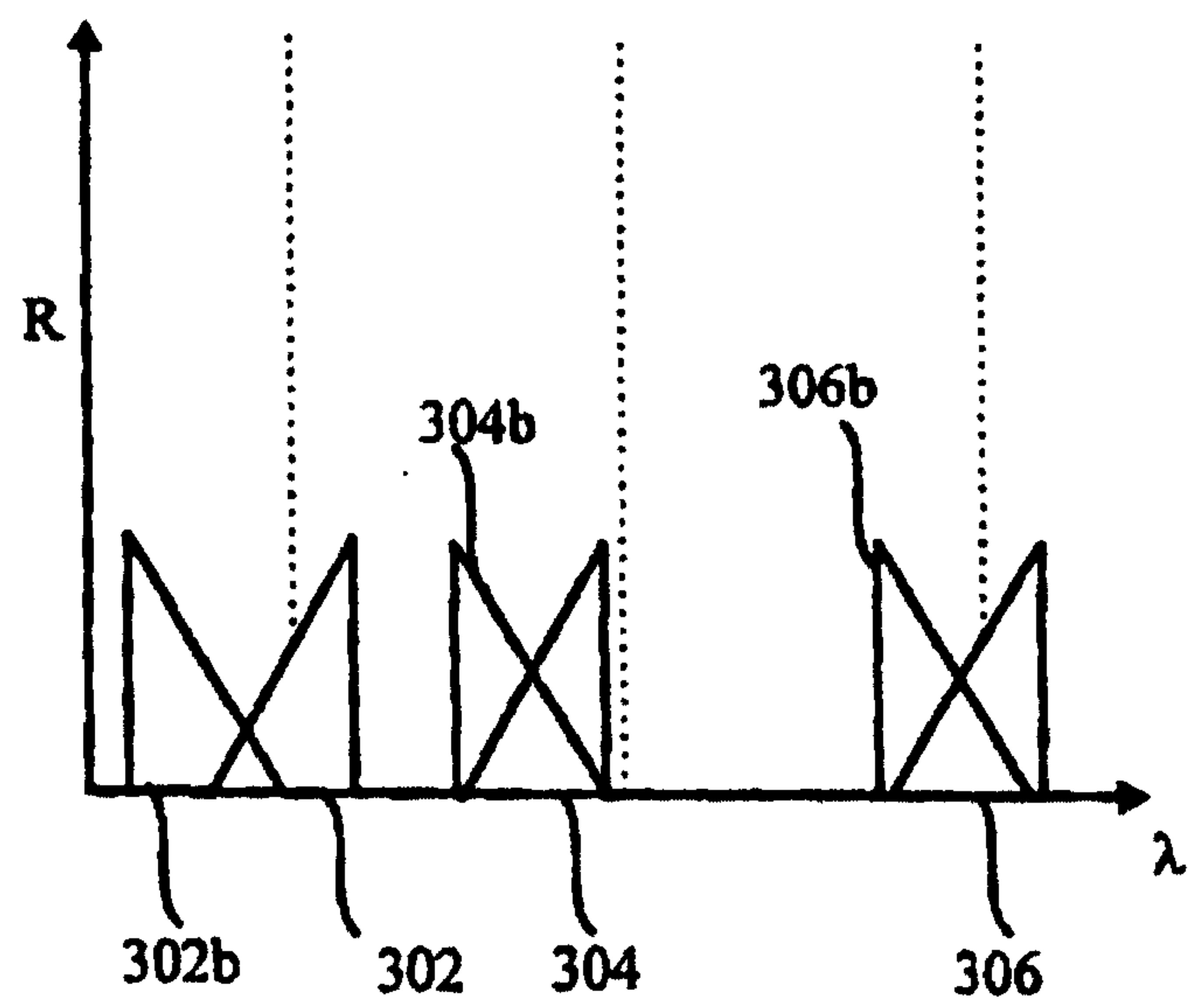


Fig. 3c



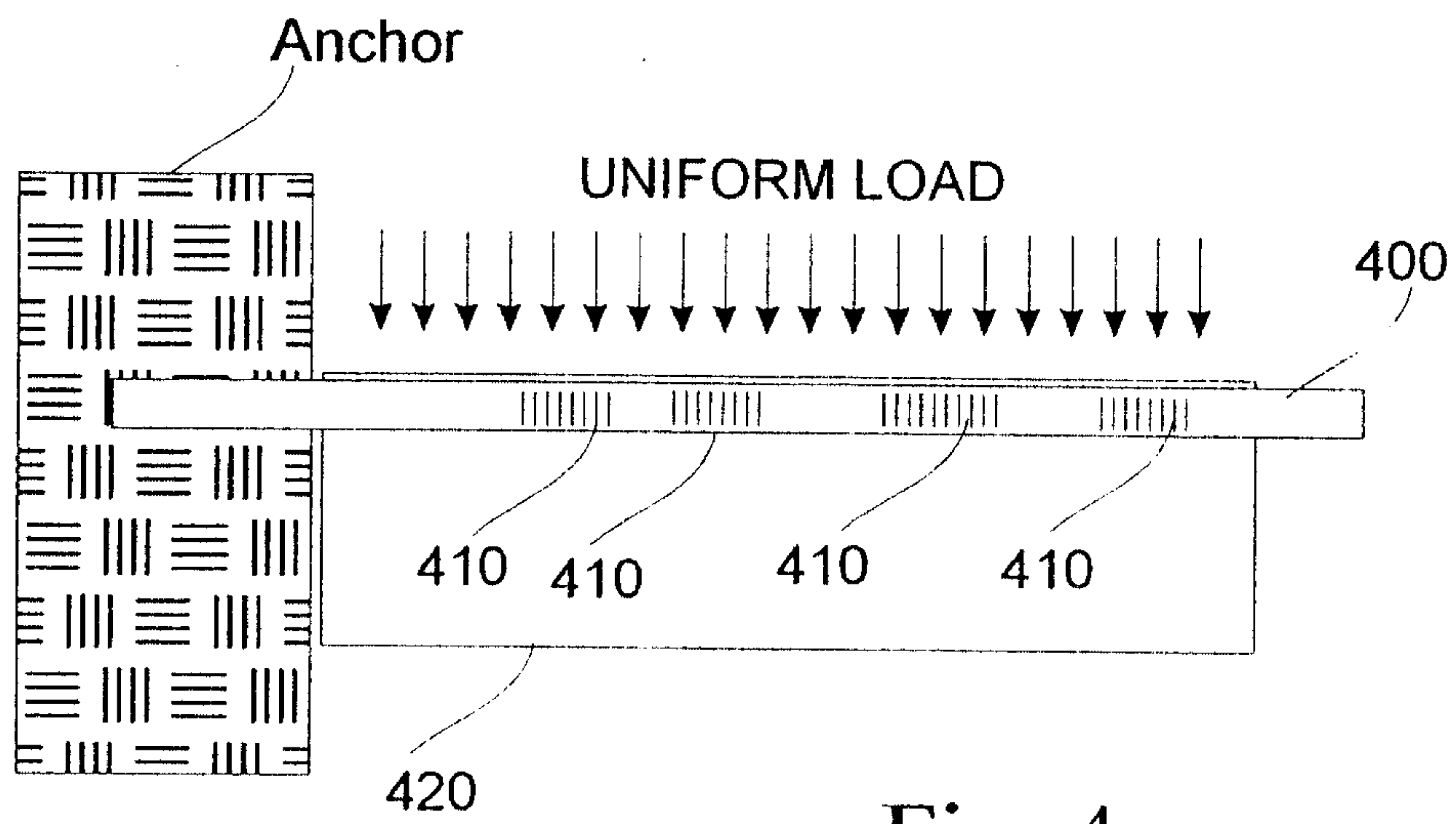


Fig. 4
PRIOR ART

