

(19) World Intellectual Property Organization
International Bureau



(43) International Publication Date
14 February 2008 (14.02.2008)

PCT

(10) International Publication Number
WO 2008/017860 A1

(51) International Patent Classification:
G01S 1/00 (2006.01)

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(21) International Application Number:
PCT/GB2007/003050

(81) Designated States (unless otherwise indicated, for every kind of national protection available): AE, AG, AL, AM, AT, AU, AZ, BA, BB, BG, BH, BR, BW, BY, BZ, CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PG, PH, PL, PT, RO, RS, RU, SC, SD, SE, SG, SK, SL, SM, SV, SY, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.

(22) International Filing Date: 10 August 2007 (10.08.2007)

(25) Filing Language: English

(26) Publication Language: English

(30) Priority Data:
0615930.5 10 August 2006 (10.08.2006) GB
0624516.1 8 December 2006 (08.12.2006) GB

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(84) Designated States (unless otherwise indicated, for every kind of regional protection available): ARIPO (BW, GH, GM, KE, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HU, IE, IS, IT, LT, LU, LV, MC, MT, NL, PL, PT, RO, SE, SI, SK, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

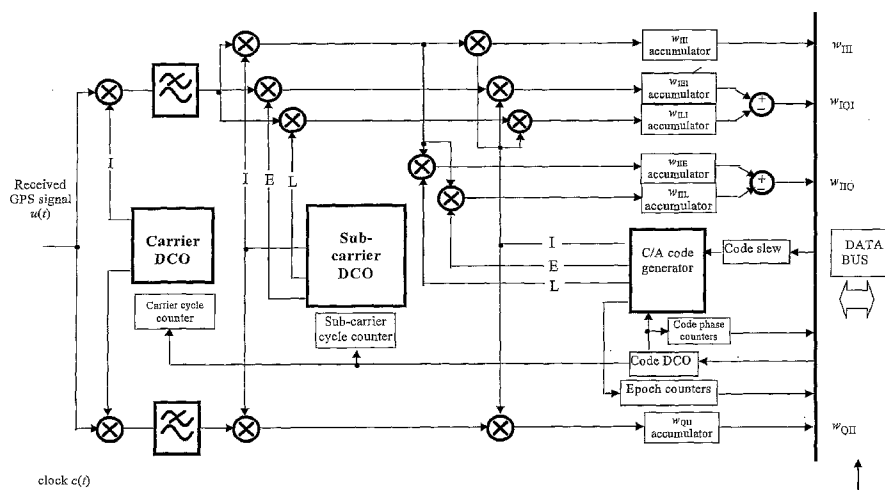
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Published:

— with international search report

(54) Title: A RECEIVER OF BINARY OFFSET CARRIER (BOC) MODULATED SIGNALS



(57) Abstract: Binary Offset Carrier (BOC) is the agreed modulation for signals of next generation Global Navigation satellite systems (GNSS). Compared to current phase shift keying (PSK) modulation by a code, there is a further modulation by a sub-carrier. There is a known major difficulty with BOC called 'false lock' where early/late gates settle on the wrong peak of the multi-peaked correlation function. This invention eliminates the problem by eliminating that correlation. Instead, a two dimensional correlation is tracked independently to realise a dual estimate. An unambiguous lower accuracy estimate derived from the code phase is used to make an integer correction to a higher accuracy but ambiguous independent estimate based on the sub-carrier phase. The actual receiver may adopt a triple loop, instead of the usual double loop, where carrier phase, sub-carrier phase and code phase are tracked independently but interactively.

A RECEIVER OF BINARY OFFSET CARRIER (BOC) MODULATED SIGNALS

Field of the Invention

The present invention relates to the reception of Binary Offset Carrier (BOC) modulated signals and similar such signals. One particular application of the invention is the reception of BOC modulated navigation signals in a Global Navigation Satellite System (GNSS).

Background to the Invention

In a GNSS, a receiver estimates delays τ in the navigation signals received from different satellites and uses this information, combined with information on the position of the satellites, to estimate its position. The more accurate the estimation of the delays τ , the more accurately the receiver can estimate its position.

The United States led Global Positioning System (GPS) is presently the GNSS in most common use. Navigation signals transmitted by GPS satellites are modulated using a Phase Shift Keying (PSK) modulation of a code onto a carrier signal having a designated carrier frequency. The modulation involves altering the phase of the carrier signal by fixed amounts (0 or π) at a code rate f_C , each symbol of the code having duration $T_C = 1/f_C$ and the code being repeated with time period T_G . A navigation signal received at a receiver from a satellite can therefore be represented by an equivalent bi-modal amplitude modulation function $a(t - \tau) \in (-1, +1)$ with period T_G , as shown in Figure 1.

The receiver estimates the delay τ by comparing the received signal to a locally generated reference signal. The reference signal consists of an in-phase and quadrature-phase (I and Q) carrier modulated with the same code as the input signal. The reference modulation can be represented mathematically as $a(t - \hat{\tau})$ where $\hat{\tau}$ is a trial delay. The comparison typically consists in multiplying the received signal by the I and Q reference to yield a demodulated signal. The demodulated signal is then integrated over a given time, usually the same as the period T_G of the code, to output a value known as a correlation. The correlation depends on the difference between the trial delay $\hat{\tau}$ of the reference signal and the true delay τ of the received signal and can be expressed as a correlation function $\Lambda(\hat{\tau} - \tau)$. As shown in

Figure 2, this correlation function for a PSK modulated signal is triangular and peaks when the trial delay $\hat{\tau}$ matches the true delay τ . The width of the correlation function is twice the symbol duration T_C , i.e. $2T_C$.

Calculating the entire correlation function $\Lambda(\hat{\tau} - \tau)$ over all $\hat{\tau}$ and analysing it to determine its peak and hence identify the delay τ of the received signal is a computationally time-consuming task. Most conventional GPS receivers therefore compute just three sampled correlations simultaneously, using three reference signals offset in time from one another. The three correlations are usually referred to as gate values of Early (E), Prompt (P) and Late (L) gates. The E and L gates are offset from one another by a time separation T_{DC} , so that they can be considered to have trial delays $\hat{\tau} - \frac{T_{DC}}{2}$ and $\hat{\tau} + \frac{T_{DC}}{2}$ respectively. The P gate can then be considered to have trial delay $\hat{\tau}$ half way between these trial delays of the E and L gates. So, as illustrated in Figure 2, when the E and L gate values are equal, the P gate value yields the peak value of the correlation function $\Lambda(\hat{\tau} - \tau)$ and the trial delay $\hat{\tau}$ is equal to the true delay τ .

An iterative algorithm can be used to arrive at this state. When the trial delay $\hat{\tau}$ is not equal to the true delay, the P gate will be offset from the peak of the correlation function $\Lambda()$, and there will be a difference in the values of the E and L gates. So, an error signal proportional to the difference between the trial delay $\hat{\tau}$ and the true delay τ can be generated by subtracting the L gate value from the E gate value. This can be used to iteratively adjust the trial delay $\hat{\tau}$ toward the true delay τ . A best estimate of the true delay is then deemed to be the value of the trial delay (of the P gate) when the E gate value is equal to the L gate value (as shown in Figure 2).

It is presently intended to improve the American GPS by adding new navigation signals to the system. The independent European Galileo system will use similar new navigation signals in both the same and new frequency bands. While some of the new navigation signals will continue to use PSK modulation, most of them will be modulated using the new Binary Offset Carrier (BOC) modulation.

Like PSK modulation, BOC modulation involves modulating a code onto a carrier. The code is similar to that used in PSK modulation, and the code in the received signal can again be represented by an equivalent bi-modal amplitude modulation function $a(t - \tau)$ having code rate f_C , symbol duration T_C and periodicity T_G . However, BOC modulation

involves further modulating the signal by a sub-carrier, which can be represented by a sub-carrier modulation function $s(t - \tau)$ having sub-carrier rate f_s and sub-symbol duration equivalent to a half-cycle $T_s = 1/(2f_s)$. As seen in Figure 3, the sub-carrier modulation function $s(t - \tau)$ is a simple periodic square waveform. The sub-carrier rate f_s is an integer multiple, or an integer-and-a-half multiple of the code rate f_c . The standard notation for BOC modulation reads $BOC(f_s, f_c)$. This figure shows what can be called 'sine-BOC' where the sub carrier has 0 deg phase shift relative to the code zero crossings. Also there is 'cosine -BOC' where the sub-carrier is phase shifted 90 deg relative to the code zero-crossings (not shown).

When a received BOC signal is correlated using a matching locally generated BOC reference signal the resulting correlation function $\mathbb{W}(\hat{\tau} - \tau)$ has multiple peaks. For example, referring to Figure 4, this correlation function of a sine-BOC signal modulated using $BOC(2f, f)$ has three positive peaks and four negative peaks. The central positive peak corresponds to a match of the true delay τ of the received signal with the trial delay of the reference signal. The other, secondary peaks are separated at intervals of the sub-symbol duration T_s . Importantly, the envelope (dashed line) of this correlation function $\mathbb{W}(\hat{\tau} - \tau)$ is the same as the correlation function $\Lambda(\hat{\tau} - \tau)$ of a PSK modulated signal having the same code rate f_c .

Because the central peak of the BOC correlation function $\mathbb{W}(\hat{\tau} - \tau)$ has steeper sides than the peak of the equivalent PSK correlation function $\Lambda(\hat{\tau} - \tau)$, BOC modulation has the potential to allow more accurate delay estimation. Specifically, when the E and L gates are located on either side of the central peak then the error signal generated from the difference between the L gate value and the E gate value can steer the P gate to the top of the central peak and hence the trial delay $\hat{\tau}$ to the true delay τ , as illustrated in the top part of Figure 4. There is however an inherent ambiguity in the delay estimate for a BOC signal provided by the conventional delay estimation technique, as described above. When the E and L gates reside on either side of one of the secondary peaks, the error signal will steer the P gate to the secondary peak (which can be negative). In that situation, the error signal will be zero, just as it is when the P gate is at the top of the central peak, and the iteration will have converged to a value of the trial delay $\hat{\tau}$ that does not correspond to the true delay τ . This is known as 'false lock' or 'slip', or 'false node tracking'.

A number of techniques have been proposed for overcoming this problem. One such technique, commonly referred to as ‘bump jumping’, is described in the paper “Tracking Algorithm for GPS Offset Carrier Signals”, P. Fine et al, Proceedings of ION 1999 National Technical Meeting, January 1999. This technique takes advantage of the knowledge that adjacent peaks of the BOC correlation function $\mathcal{W}(\hat{\tau} - \tau)$ are separated from one another by the known sub-carrier symbol duration T_s . Specifically, the technique tests for correct location of the P gate using a pair of gates, called Very Early (VE) and Very Late (VL) gates, having trial delays $\hat{\tau} - T_s$ and $\hat{\tau} + T_s$ respectively. These are offset from the trial delay $\hat{\tau}$ of the P gate by the sub-carrier symbol duration T_s . So, if the P gate has converged to the top of one of the peaks, e.g. the receiver is in lock, the VE, P and VL gates are located on three adjacent peaks. At this stage, the VE, P and VL gate values are compared. If the VE and VL gate amplitudes are less than the P gate amplitude, the P gate is known to lie on the central peak and the trial delay $\hat{\tau}$ corresponds to the true delay. However, if the VE or VL gate amplitude is higher than the P gate value, the P gate is on a secondary peak. In this event, the trial delay $\hat{\tau}$ is incremented by the sub-symbol duration T_s in the direction of whichever of the VE and VL gates has the higher (modulus) value. This action should cause the P gate to jump to the next peak toward the central peak. The comparison is then repeated to verify that the P gate is on the central peak or to cause repeated incrementing of the trial delay $\hat{\tau}$ until the P gate is located on the central peak.

Bump jumping allows a receiver to fully exploit the potential accuracy of BOC. However, there can be a significant waiting time before the delay estimate can be relied on. There is an elapsed time required to decide whether there is a false lock or not. This is longer for a low C/N_0 , when the VE, P and VL gate values must also be averaged over a significant time in order to be sure which of the three tested adjacent peaks has the highest amplitude. The required time to detect false lock also increases proportionally with the ratio of the sub-carrier rate to the code rate f_s/f_c , because the difference of amplitude between adjacent peaks relatively decreases. It may also be necessary to correct false lock several times over successive secondary peaks before the central peak is found, a problem which is exacerbated as the ratio of the sub-carrier rate to the code rate f_s/f_c increases, because the number of secondary peaks increases. Overall, the waiting time may range upwards to several seconds, which is certainly enough to have potentially disastrous consequences for a plane landing,

ship docking or such like. Worse, the receiver does not know that it has been in a false lock state until it actually jumps out of it. The bump jumping system therefore is not fail safe.

A further difficulty has now been realised since the launch of the first test satellite GIOVE-A transmitting BOC signals in December 2005. Non-linear and linear distortion in the transmitting chain can easily cause appreciable asymmetry in the actual correlation function $\hat{\Lambda}(\hat{\tau} - \tau)$ - where the corresponding secondary peaks on either side of the main peak are no longer equal in amplitude. This inevitably degrades performance, and in a worst case, the bump-jumping receiver simply does not work. "GIOVE-A in orbit testing results" M. Falcone, M. Lugert, M. Malik, M. Crisic, C. Jackson, E. Rooney, M. Trethey ION GNSS FortWorth Texas, September 2006.

The paper "Unambiguous Tracker for GPS Binary-Offset-Carrier Signals", Fante R., ION 59th Annual Meeting / CIGTF 22nd Guidance Test Symposium, 23 - 25 June 2003, Albuquerque, NM, describes another technique involving multiple sampling (gating) of the correlation function and then linear combination of these samples to synthesise a monotonic approximation to the PSK correlation function $\hat{\Lambda}(\hat{\tau} - \tau)$ having no multiple peaks. This solution certainly eliminates false locks. However, this technique relies on a very complex receiver design. More fundamentally, it fails to realise the potential accuracy conferred by BOC modulation, because the shallower PSK correlation peak is relied on to resolve the delay estimate. Similarly, the paper "BOC(x, y) signal acquisition techniques and performances", Martin et al., Proceedings of ION GPS 2003, September 2003, Portland, Oregon, describes a technique that exploits the fact that the BOC modulated signal has a mathematical equivalence to two PSK modulated signals centred on two separate carrier frequencies; where the higher frequency f_H is equal to the carrier frequency plus the sub-carrier frequency f_s while the lower frequency f_L is equal to the carrier frequency minus the sub-carrier frequency f_s . With appropriate processing the actual monotonic PSK correlation function $\hat{\Lambda}(\hat{\tau} - \tau)$ can be recovered. But this method is again complex to implement and more fundamentally fails to realise the potential accuracy conferred by BOC modulation.

The present invention overcomes these problems.

Summary of the Invention

According to a first aspect of the present invention, there is provided a receiver for receiving a navigation signal comprising a carrier modulated by a code modulation function

of a given code rate and further modulated by a sub-carrier modulation function having a sub-carrier rate different to the code rate, the receiver comprising processing means arranged to:

- generate a first estimate of delay based on the code modulation;
- generate a second estimate of delay based on the sub-carrier modulation; and
- determine an optimal delay estimate from the first and second delay estimates.

The essence of the invention is that it estimates the signal delay in two independent ways and then combines the estimates to arrive at a signal optimal delay estimate. The prior art correlates the modulation in the received signal with only a single modulation function, which is the combined code modulation and sub-carrier modulation. Up to now, dealing with the complex correlation function which results from this action has been considered unavoidable, because the combined modulation has been perceived to be intrinsic and inseparable. The invention contradicts this perception. It recognises that correlating the received signal with the sub-carrier modulation function and code modulation function can be done separately, so avoiding the need to contemplate the conventional correlation function.

In all embodiments of the invention the delay in the BOC signal is estimated in two different and independent ways - in a double estimate. A first non-ambiguous lower accuracy estimate is used to resolve the ambiguities in a second higher accuracy estimate. This first estimate is derived only from the phase of the code modulation in the BOC signal; it treats the BOC modulation as a 'virtual' PSK and ignores the sub carrier. A second estimate is derived only from the phase of sub carrier modulation in the BOC signal and ignores the code. A three-loop receiver can be used for the optimal double estimate of the delay in a selected BOC transmission. In some embodiments an inner delay-locked loop (DLL) tracks the delay as embodied in the code phase; a middle sub-carrier locked loop (SLL) independently tracks the same delay as embodied in the sub-carrier phase, thus two independent delay estimates are calculated. A third outer loop may track and lock to the carrier phase and/or frequency of the particular satellite signal. All three loops may operate simultaneously, independently yet co-operatively. This implementation may be contrasted with a conventional receiver which uses only two loops, where the single delay estimate is derived from the tracking of the correlation function in a delay-locked loop (DLL) while in parallel and simultaneously the carrier phase and/or frequency is tracked by a second phase locked loop (PLL) or frequency locked loop (FLL).

By virtue of the dual estimate principle in this invention the BOC correlation function $\Lambda(\tau)$ with its secondary peaks does not exist and there are no secondary peaks on which a false lock would occur.

In some embodiments of a three-loop receiver the DLL locks to the peak of the same $\Lambda(\tau)$ -shaped function as the standard GPS, so ensuring a smooth and non-ambiguous acquisition of a delay estimate. The SLL however locks to the nearest peak of the continuous sub-carrier correlation function - which is a triangular function of periodicity of the sub-carrier. This loop estimate has higher accuracy but has an inherent ambiguity in integer multiples of sub-carrier half cycles. There is no 'wrong peak' in this concept however and this ambiguity is however acceptable. For, in a further step, the ambiguity in this SLL estimate is automatically and instantly resolved by comparison with the DLL estimate.

The combination of SLL and DLL estimate now provide the inherently higher accuracy due to BOC modulation on the signal (comparing with PSK on the basis of the same chip rate), with the ambiguity now resolved.

Simulations show smooth consistent operation of this joint estimation process even in conditions of poor signal to noise.

The three-loop receiver can be implemented with the same variety of options that are available to two loop receivers. The standard option is to track the phase of the carrier - as in so-called 'coherent DLL' where the outer loop is phase locked to the carrier, using a phase discriminator. An alternative is to track the frequency of the carrier - as in so-called 'incoherent DLL' where the outer loop is frequency locked to the carrier, using a frequency discriminator. Various possible phase and frequency discriminators can be used.

Various possible discriminators for the SLL can also be used. A variety of standard discriminators for the DLL loop can also be used. Known technologies and variants, including methods for reducing effect of multipath and currently used in two-loop system will transfer to the new three loop system without complication.

Preferred embodiments of the invention are now described, by way of example only, with reference to the accompanying drawings.

Brief Description of the Drawings

Figure 1 is a graphical illustration of a PSK modulated signal according to the prior art;

Figure 2 is a graphical illustration of a correlation function for the PSK modulated signal shown in Figure 1 according to the prior art;

Figure 3 is a graphical illustration of a basic sine-BOC modulated signal according to the prior art;

Figure 4 is a graphical illustration of a correlation function for the BOC modulated signal shown in Figure 3 according to the prior art, showing examples of both correct tracking and false tracking;

Figure 5 is a schematic illustration of the overall BOC receiver according to a first preferred embodiment of the invention;

Figure 6 is a general block diagram of the correlator means 9 of the receiver of Figure 5;

Figure 7 is a functional expansion of the correlator 9 from Figure 6 and also the signal processor 10;

Figure 8 is a functional expansion of a receiver according to a further embodiment of the invention;

Figure 9 is a graphical illustration of a two dimensional correlation function for the BOC modulated signal, which correlation function is used by the BOC receiver shown in Figure 5, 6, 7 and 8 ;

Figure 10 is a cross section in the sub-carrier trial delay dimension of the correlation function shown in the Figure 9;

Figure 11 is the nominal correlation in the sub-carrier trial delay dimension only;

Figure 12 is a cross section in the code delay dimension of the correlation function shown in Figure 9;

Figure 13 is the nominal correlation in the code delay dimension only;

Figure 14 is a discriminator function in the sub-carrier delay dimension only;

Figure 15 is a discriminator function in the code delay dimension only ;

Figures 16 and 17 are computer-generated syntheses illustrating operation of the BOC receiver shown in Figure 8; and

Figures 18 shows an example of the top-level operations and tasks of a GNSS software receiver.

Detailed Description of the Preferred Embodiments

Referring to Figure 5, a BOC receiver 1 according to a first preferred embodiment of the present invention is arranged to receive a BOC modulated signal via a right-hand circularly polarised antenna 2. The antenna 2 feeds the received signal to a pre-amplifier 3, which includes a filter for filtering the received signal, a circuit for blocking strong interfering signals and a Low Noise Amplifier (LNA) for amplifying the received signal. The LNA effectively sets the receiver's noise figure, normally around 2dB, and provides around 30dB gain. The pre-amplifier 3 feeds the filtered, amplified signal to a down-converter 4 for a first stage down-conversion of the signal to a suitable intermediate frequency (IF). The signal is down-converted in multiple stages and filtered to eliminate unwanted image signals.

The down-converter 4 feeds the down-converted signal to an Analogue to Digital Converter (ADC) 5 for converting the signal to the digital domain. The ADC 5 can quantise the signal to one, two or more bits. In this embodiment, because the ADC 5 uses multi-bit quantisation, the receiver 1 incorporates an automatic gain control (AGC) circuit 6 to maintain proper distribution of the signal across the quantisation levels. The output of the AGC circuit 6 feeds back to the down-converter 4 to enable control of the signal level input to the ADC 5 and hence maintain proper amplitude distribution of the signal output by the ADC 5. The ADC 5 is arranged to output the digital signal $u(t)$ to the dual-estimator 8. This has a correlator stage 9 and a processing stage 10. In this embodiment, the dual estimator 8 is implemented in hardware. So, the correlator stage 9 comprises an Application Specific Integrated Circuit/Field Programmable Gate-Array (ASIC/FPGA) and the processing stage 10 is a microprocessor. The dual estimator 8 estimates the delay τ between transmission and reception of the received signal and outputs the delay estimate via output 11. A clock signal $c(t)$ from reference oscillator at 7 is provided to the down-converter 4, ADC 6 and the dual estimator 8.

Figure 6 shows a first level of physical detail to the correlator 9. The input signal $u(t)$ splits into an upper in-phase and lower quadrature arm and is processed through three stages. The incoming signal is mixed with replica carrier, sub carrier and code waveforms, each generated by separate digitally controlled oscillators (DCO) 12, 17, 18. First there is multiplication by a phase or quadrature reference signal from the carrier DCO; then multiplication by a prompt, early or late reference signal from the sub-carrier DCO and finally multiplication by a prompt, early or late reference signal from the C/A code generator. The resulting signal combinations are accumulated over the code period and six correlation results

formed. The extreme right of the diagram shows the interaction through a data bus to the microprocessor 10.

Figure 7 provides a more detailed functional description. The correlator sub-block 9 is identified. The remainder is the processing stage 10.

The input signal $u(t)$ at 5 can be described (neglecting additive noise and other BOC signals simultaneously present) as

$$u(t) = A \times \cos(\omega_0 t + \phi) \times s(t - \tau) \times a(t - \tau) \times d \quad (1)$$

where A is amplitude, $\cos(\omega_0 t + \phi)$ represents the carrier signal after down conversion to an intermediate frequency (IF) ω_0 and phase ϕ , $s(t - \tau)$ is the sub-carrier modulation in the received signal comprising the sub-carrier modulation function $s(t)$ at delay τ , $a(t - \tau)$ is the code modulation in the received signal comprising the code modulation $a(t)$ at delay τ and $d \in (-1, +1)$ is a polarity.

The invention depends essentially on the fact that sub-carrier is half-periodic over a relatively short sub-chip width T_S and that expression (1) is mathematically identical to

$$u(t) = A \times \cos(\omega_0 t + \phi) \times s(t - \tau^*) \times a(t - \tau) \times d^* \quad (2)$$

where

$$\tau^* = \tau + nT_S \quad (3)$$

is a multi-valued offset delay which has a number of values each offset from the delay τ by a different integer shift n times the sub-chip width T_S . The equivalent polarity $d^* = d$ for even number of shifts and $d^* = -d$ for an odd integer shift. It should be understood that the actual sub-carrier delay and the code delay for any actually received signal are still the same τ . The receiver must always estimate this actual non-ambiguous delay τ in the code function $a(\cdot)$. It is however only necessary for the receiver to seek to estimate the ambiguous τ^* in the sub-carrier function $s(\cdot)$ and achieve the same result as if it were estimating the actual delay τ . Accordingly, the offset delay τ^* and delay τ are treated as independent quantities, without regard to (3), and two independent estimates may be generated. Only in a final correction stage is it admitted that an estimate of offset delay τ^* and delay τ are related as in (3), and the value of estimate $\hat{\tau}$ used to remove the ambiguities in the value of estimate $\hat{\tau}^*$.

Referring to Figure 7, the correlator stage 9 of the dual estimator 8 receives the digital signal $u(t)$ from the ADC 5 and the clock signal $c(t)$ from the reference oscillator 7. A carrier Digital Controlled Oscillator (DCO) 12 of the correlator stage uses the clock signal

$c(t)$ to generate In-phase (I) and Quadrature (Q) reference signals $r_I(t)$, $r_Q(t)$ at the IF ω_0 with trial phase $\hat{\phi}$, e.g.

$$r_I(t) = +\cos(\omega_0 t + \hat{\phi}) \quad (4)$$

and

$$r_Q(t) = -\sin(\omega_0 t + \hat{\phi}) \quad (5)$$

The I signal multiplier 13 then multiplies the digital signal $u(t)$ with I reference signal $r_I(t)$ and the I signal filter 14 filters the result to output an I signal $v_I(t)$ which represents the I component of the received signal; while the Q signal multiplier 15 multiplies the digital signal $u(t)$ with reference Q signal $r_Q(t)$ and the Q signal filter 16 filters the result to output Q signal $v_Q(t)$ which represents the Q component of the received signal.

The I and Q signals $v_I(t)$, $v_Q(t)$ can be described (neglecting additive noise and other BOC signals simultaneously present) as

$$v_I(t) = A \times \cos(\phi - \hat{\phi}) \times s(t - \tau^*) \times a(t - \tau) \times d \quad (6)$$

and

$$v_Q(t) = A \times \sin(\phi - \hat{\phi}) \times s(t - \tau^*) \times a(t - \tau) \times d \quad (7)$$

A sub-carrier DCO 17 uses the clock signal $c(t)$ and the sub-carrier modulation function $s(t)$ to generate Prompt (P), Early (E) and Late (L) gate sub-carrier reference signals $s(t - \hat{\tau}^*)$, $s(t - \hat{\tau}^* + T_{DS}/2)$ and $s(t - \hat{\tau}^* - T_{DS}/2)$ respectively, where $\hat{\tau}^*$ is a trial sub-carrier delay and T_{DS} is the total separation between E and L gates. The separation T_{DS} can be selected freely in the range $0 < T_{DS} < T_S$.

Similarly, a code DCO 18 uses the clock signal $c(t)$ and the code modulation function $a(t)$ to generate P, E and L gate code reference signal $a(t - \hat{\tau})$, $a(t - \hat{\tau} + T_{DC}/2)$ and $a(t - \hat{\tau} - T_{DC}/2)$, respectively, where $\hat{\tau}$ is a trial code delay and T_{DC} is the total separation between E and L gates. The separation T_{DC} can be selected freely in the range $0 < T_{DC} < T_C$.

The correlator stage 8 continues by multiplying the I and Q signals $v_I(t)$, $v_Q(t)$ with appropriate combinations of the P, E and L gate sub-carrier reference signals $s(t - \hat{\tau}^*)$, $s(t - \hat{\tau}^* + T_{DS}/2)$ and $s(t - \hat{\tau}^* - T_{DS}/2)$, and the P, E and L gate code reference signals $a(t - \hat{\tau})$, $a(t - \hat{\tau} + T_{DC}/2)$ and $a(t - \hat{\tau} - T_{DC}/2)$ in order to generate six demodulated signals:

an I sub-carrier P gate and I code P gate signal $v_{III}(t)$, an I sub-carrier E gate and I code P gate signal $v_{IEI}(t)$, an I sub-carrier L gate and I code P gate signal $v_{ILI}(t)$, and I sub-carrier P gate and I code E gate signal $v_{IIE}(t)$, an I sub-carrier P gate and I code L gate signal $v_{ILL}(t)$ and Q sub-carrier P gate and Q code P gate signal $v_{QII}(t)$, all of which can be expressed

$$v_{III}(t) = v_I(t) \times s(t - \hat{\tau}^*) \times a(t - \hat{\tau}) \quad (8)$$

$$v_{IEI}(t) = v_I(t) \times s(t - \hat{\tau}^* + T_{DS/2}) \times a(t - \hat{\tau}) \quad (9)$$

$$v_{ILI}(t) = v_I(t) \times s(t - \hat{\tau}^* - T_{DS/2}) \times a(t - \hat{\tau}) \quad (10)$$

$$v_{IIE}(t) = v_I(t) \times s(t - \hat{\tau}^*) \times a(t - \hat{\tau} + T_{DC/2}) \quad (11)$$

$$v_{ILL}(t) = v_I(t) \times s(t - \hat{\tau}^*) \times a(t - \hat{\tau} - T_{DC/2}) \quad (12)$$

$$v_{QII}(t) = v_Q(t) \times s(t - \hat{\tau}^*) \times a(t - \hat{\tau}) \quad (13)$$

These multiplications are implemented by first and second multipliers 19, 20 multiplying the I signal $v_I(t)$ with P gate sub-carrier reference signal $s(t - \hat{\tau}^*)$ and P gate code reference signal $a(t - \hat{\tau})$ to output first demodulated signal $v_{III}(t)$; third and fourth multipliers 21, 22 multiplying the I signal $v_I(t)$ with E gate sub-carrier reference signal and P gate code reference signal to output second demodulated signal $v_{IEI}(t)$; fifth and sixth multipliers 23, 24 multiplying the I signal $v_I(t)$ with L gate sub-carrier reference signal and P gate code reference signal to output third demodulated signal $v_{ILI}(t)$; first and seventh multipliers 19, 25 multiplying the I signal $v_I(t)$ with P gate sub-carrier reference signal and E gate code reference signal to output fourth demodulated signal $v_{IIE}(t)$; first and eighth multipliers 19, 26 multiplying the I signal $v_I(t)$ with P gate sub-carrier reference signal and L gate code reference signal to output fifth demodulated signal $v_{ILL}(t)$; and ninth and tenth multipliers 27, 28 for multiplying the Q signal $v_Q(t)$ with P gate sub-carrier reference signal and P gate code reference signal to output sixth demodulated signal $v_{QII}(t)$.

The demodulated signals $v_{III}(t)$, $v_{IEI}(t)$, $v_{ILI}(t)$, $v_{IIE}(t)$, $v_{ILL}(t)$ and $v_{QII}(t)$ are then integrated by integrators 29 to 34 respectively. These integrators run over a fixed time, which in this embodiment is the same as the code period T_G . In other embodiments, the integration time T can be an integer multiple of this code period, so that the integration time is typically of the order of a few milliseconds in total. The output of each of the integrators 29 to 34 is

sampled by the processing stage 10 at the end of each fixed time and then the integrators 29 to 34 reset to zero. The outputs of the integrators 29 to 34 can be described by a set of six correlations $w_{\text{III}}[k]$, $w_{\text{IEI}}[k]$, $w_{\text{ILI}}[k]$, $w_{\text{IEE}}[k]$, $w_{\text{ILL}}[k]$ and $w_{\text{QII}}[k]$ for each sample $k=1,2,3\dots$. The values of these correlations depend of the difference between the trial phase $\hat{\phi}$ and the true phase ϕ , the difference between the trial sub-carrier delay $\hat{\tau}^*$ and the offset sub-carrier delay τ^* , and the difference between the trial code delay $\hat{\tau}$ and the true code delay τ . The I sub-carrier P gate and code P gate correlation $w_{\text{III}}[k]$ can be expressed

$$w_{\text{III}}[k] = A \times \cos(\phi - \hat{\phi}) \times \chi(\hat{\tau}^* - \tau^*, \hat{\tau} - \tau) \times d^* \quad (14)$$

where $\chi(\cdot)$ is a two-dimensional correlation function, as shown in Figure 9. The two-dimensional correlation function $\chi(\cdot)$ has multiple peaks when the trial code delay $\hat{\tau}$ equals the true code delay τ

$$\hat{\tau} = \tau \quad (15)$$

and the trial sub-carrier delay $\hat{\tau}^*$ is equal to any of the multiple values of the sub-carrier code delay τ^* , i.e. the true code delay τ plus a positive or negative integer n multiple of the sub-carrier symbol duration T_s

$$\hat{\tau}^* = \tau + nT_s \quad (16)$$

For explanatory purposes, the I sub-carrier P gate and code P gate correlation $w_{\text{III}}[k]$ can be approximated by the expression

$$w_{\text{III}}[k] \approx A \times \cos(\phi - \hat{\phi}) \times \text{trc}(\hat{\tau}^* - \tau^*) \times \Lambda(\hat{\tau} - \tau) \times d^* \quad (17)$$

where $\text{trc}(\cdot)$ is a continuous triangular cosine of periodicity $2T_s$ and $\Lambda(\cdot)$ is the correlation function of a PSK modulated signal having the same code rate as the received signal. The acceptability of this approximation can be appreciated from Figures 10 to 13, where it can be seen that the continuous triangular cosine function $\text{trc}(\cdot)$ shown in Figure 11 is very similar to a view of the two-dimensional function $\chi(\cdot)$ just in the dimension of the difference between the trial sub-carrier delay $\hat{\tau}^*$ and true sub-carrier delay τ^* as shown in Figure 10; while the PSK correlation function $\Lambda(\cdot)$ shown in Figure 13 is very similar to a view of the two-dimensional function $\chi(\cdot)$ just in the dimension of the difference between the trial code delay $\hat{\tau}$ and true code delay τ as shown in Figure 12.

The other correlations $w_{\text{IEI}}[k]$, $w_{\text{ILI}}[k]$, $w_{\text{IEE}}[k]$, $w_{\text{ILL}}[k]$ and $w_{\text{QII}}[k]$ are likewise sufficiently well approximated mathematically by

$$w_{\text{IEI}}[k] \approx A \times \cos(\phi - \hat{\phi}) \times \text{trc}(\hat{\tau}^* - \tau^* - T_{\text{DS}}/2) \times \Lambda(\hat{\tau} - \tau) \times d^* \quad (18)$$

$$w_{\text{ILI}}[k] \approx A \times \cos(\phi - \hat{\phi}) \times \text{trc}(\hat{\tau}^* - \tau^* + T_{\text{DS}}/2) \times \Lambda(\hat{\tau} - \tau) \times d^* \quad (19)$$

$$w_{\text{IEE}}[k] \approx A \times \cos(\phi - \hat{\phi}) \times \text{trc}(\hat{\tau}^* - \tau^*) \times \Lambda(\hat{\tau} - \tau - T_{\text{DC}}/2) \times d^* \quad (20)$$

$$w_{\text{ILL}}[k] \approx A \times \cos(\phi - \hat{\phi}) \times \text{trc}(\hat{\tau}^* - \tau^*) \times \Lambda(\hat{\tau} - \tau + T_{\text{DC}}/2) \times d^* \quad (21)$$

$$w_{\text{QII}}[k] \approx A \times \sin(\phi - \hat{\phi}) \times \text{trc}(\hat{\tau}^* - \tau^*) \times \Lambda(\hat{\tau} - \tau) \times d^* \quad (22)$$

It can be appreciated that, when the I sub-carrier P gate and I code P gate correlation $w_{\text{III}}[k]$ peaks, this is because the I sub-carrier E gate and I code P gate correlation $w_{\text{IEI}}[k]$ has the same amplitude as the I sub-carrier L gate and I code P gate correlation $w_{\text{ILI}}[k]$, i.e.

$w_{\text{IEI}}[k] = w_{\text{ILI}}[k]$, where the E and L gates for the sub-carrier reference signal have the same value, as seen in Figure 11. It is also because the I sub-carrier P gate and I code E gate correlation $w_{\text{IEE}}[k]$ has the same amplitude as the I sub-carrier P gate and I code L gate correlation $w_{\text{ILL}}[k]$, i.e. $w_{\text{IEE}}[k] = w_{\text{ILL}}[k]$, where the E and L gates for the code reference signal have the same value, as shown in Figure 13. Inspection of these equations further shows that in a tracking state the phase estimate $\hat{\phi}$ must be the same as the true phase ϕ plus or minus an integer number of carrier half cycles. This condition is known to exist when the Q sub-carrier P gate and Q sub-carrier P gate correlation $w_{\text{QII}}[k]$ is zero, i.e. $w_{\text{QII}}[k] = 0$, because the sine function in expression (22) is zero, signifying the case of carrier lock.

Any difference between the I sub-carrier E gate and I code P gate correlation $w_{\text{IEI}}[k]$ and the I sub-carrier L gate and I code P gate correlation $w_{\text{ILI}}[k]$ is proportional to the difference between the sub-carrier trial delay $\hat{\tau}^*$ and the nearest multi-value of the sub-carrier delay τ^* . Consequently, the processing stage 10 carries out a subtraction step 35 that subtracts the I sub-carrier E gate and I code P gate correlation $w_{\text{IEI}}[k]$ from the I sub-carrier L gate and I code P gate correlation $w_{\text{ILI}}[k]$ to give a sub-carrier difference correlation $w_{\text{IQI}}[k]$. This can then be expressed

$$w_{\text{IQI}}[k] \approx A \times \cos(\phi - \hat{\phi}) \times \text{Trs}(\tau^* - \hat{\tau}^*) \times \Lambda(\hat{\tau} - \tau) \times d^* \quad (23)$$

where $\text{Trs}(\cdot)$ is a trapezium sine discriminator function depending on the difference between the trial sub-carrier delay $\hat{\tau}^*$ and the multivalued sub-carrier delay τ^* , and which therefore decreases in magnitude as $\hat{\tau}^*$ approaches τ^* as shown in Figure 14.

Similarly, any difference between the I sub-carrier P gate and I code E gate correlation

$w_{IE}[k]$ and the I sub-carrier P gate and I code L gate correlation $w_{IL}[k]$ is proportional to the difference between the trial code delay $\hat{\tau}$ and the true code delay τ . Consequently, the processing stage 10 carries out a subtraction step 36 that subtracts the I sub-carrier P gate and I code E gate correlation $w_{IEI}[k]$ from the I sub-carrier P gate and I code L gate correlation $w_{ILI}[k]$ to give a code difference correlation $w_{IIQ}[k]$. This can then be expressed

$$w_{IIQ}[k] \approx A \times \cos(\phi - \hat{\phi}) \times \text{trc}(\hat{\tau}^* - \tau^*) \times \sqrt{\Lambda}(\tau - \hat{\tau}) \times d^* \quad (24)$$

where $\sqrt{\Lambda}(\cdot)$ is a discriminator function shown in fig 15.

NB It should be noted that in this account an E gate is subtracted from an L gate in order to ensure correct polarity of loop correction in terms of a code and sub-carrier delay estimate. In an equivalent description an L gate is subtracted from an E gate, in order to ensure correct polarity of loop correction in terms of a code and sub-carrier = phase estimate.

Finally, any non-zero value of the Q sub-carrier P gate and Q sub-carrier P gate correlation $w_{QII}[k]$ is approximately proportional to the difference between the trial phase $\hat{\phi}$ and the true phase ϕ .

Error signals $e_{\phi}[k]$, $e_{\tau}[k]$ and $e_{\tau}[k]$ are generated from the correlations in order to steer the trial phase $\hat{\phi}$, trial sub-carrier delay $\hat{\tau}^*$ and trial code delay $\hat{\tau}$ respectively toward the true phase ϕ , true sub-carrier delay τ^* and true code delay τ . The processing stage 10 carries out a limiter step 37 to estimate the sign of the I sub-carrier P gate and code P gate correlation $w_{III}[k]$ (which may be either positive or negative). Expressed mathematically this reads

$$\hat{d} \leftarrow \text{sgn}(w_{III}) \quad (25)$$

where the 'sgn' function delivers either +1 or -1 depending on the polarity of the correlation.

Every T s, notated here as an event by a unit increment in count k , the processing stage 10 then computes the three feed-back error signals $e_{\phi}[k]$, $e_{\tau}[k]$ and $e_{\tau}[k]$ at multiplication steps 38, 39, 40 by multiplying the respective Q sub-carrier P gate and Q code P gate correlation $w_{QII}[k]$, sub-carrier difference correlation $w_{IQI}[k]$ and code difference correlation $w_{IIQ}[k]$ by the $\text{sgn}(\cdot)$ signal $\hat{d}[k]$. So, the error signals $e_{\phi}[k]$, $e_{\tau}[k]$ and $e_{\tau}[k]$ can be expressed

$$e_{\phi} \leftarrow w_{QII} \times \hat{d} \quad (26)$$

$$e_{\tau^*} \leftarrow w_{\text{IQI}} \times \hat{d} \quad (27)$$

$$e_{\tau} \leftarrow w_{\text{IIQ}} \times \hat{d} \quad (28)$$

The count notation ' $[k]$ ' is deliberately omitted since in the actual algorithm this count need not be recorded

The processing stage then filters the error signals $e_{\phi}[k]$, $e_{\tau}[k]$ and $e_{\tau^*}[k]$ at loop filter steps 41, 42, and 43 respectively to increment or decrement the trial phase $\hat{\phi}$, sub-carrier trial delay $\hat{\tau}^*$ and code trial delay $\hat{\tau}$. These actions can be expressed iteratively as

$$f_{\phi} \leftarrow f_{\phi} + e_{\phi} \quad (29a)$$

$$\hat{\phi} \leftarrow \hat{\phi} + k_1 f_{\phi} + k_2 e_{\phi}$$

$$\hat{\tau}^* \leftarrow \hat{\tau}^* + k_{\tau^*} e_{\tau^*} \quad (29b)$$

$$\hat{\tau} \leftarrow \hat{\tau} + k_{\tau} e_{\tau} \quad (29c)$$

Again, the count notation ' $[k]$ ' is deliberately omitted since in the actual algorithm this count need not be recorded

In this embodiment the carrier phase correction is implemented by a second order loop, where phase error e_{ϕ} increments an integrated phase error f_{ϕ} , which direct and integrated errors update a current phase estimate via two gain constants k_1 and k_2 . The SLL time estimate implements a first order loop via a gain constant k_{τ^*} , and the DLL time estimate implements a first order loop via a gain constant k_{τ}

With increasing count and in the realistic presence of noise these errors go to zero on average i.e. $e_{\phi}[k] \rightarrow 0$, $e_{\tau}[k] \rightarrow 0$ and $e_{\tau^*}[k] \rightarrow 0$

Finally, in this first embodiment of the correction stage a subtractor 44 computes the instantaneous difference between the code trial delay and the sub-carrier trial delay:

$$\Delta\hat{\tau} = \hat{\tau} - \hat{\tau}^* \quad (30)$$

Provided noise is not excessive then dividing by T_S will automatically find the correct integer offset n between $\hat{\tau}^*$ and $\hat{\tau}$. The calculation, performed every correlation interval, to a best estimate is then

$$\hat{\tau}^+ = \hat{\tau}^* + \text{round}\left(\frac{\hat{\tau} - \hat{\tau}^*}{T_S}\right) \times T_S \quad (31)$$

In this final stage it is admitted that the estimates $\hat{\tau}^*[k]$ and $\hat{\tau}[k]$ are necessarily linked, because the difference between them, after rounding, should be an integer multiple of

the sub chip width T_S , assuming that both loops are locked (converged) and the input C/N_0 is sufficiently high. This best combination of the two estimates is updated every correlation interval.

The system as described above with reference to figs 5 -15 eliminates the possibility of slip or false node tracking in a BOC receiver while fully exploiting the potential of BOC modulation. This calculation automatically combines the low error of the SLL estimate with the non-ambiguous DLL estimate to get the best of both worlds.

As an essential qualification is noted that the system fails if the loops lose lock . But this is true of all loop-based systems. The system also fails if the difference of estimates falls randomly outside the bounds

$$\left(n - \frac{1}{2}\right)T_S < \Delta\hat{\tau} < \left(n + \frac{1}{2}\right)T_S \quad (32)$$

which in principle can occur because of excessive noise in the DLL estimate, even if the loops are in lock, for too low an input carrier to noise density ratio (CNDR) and /or too high a loop bandwidth B_L . Theory finds however that this restriction on the allowed range of CNDR and B_L is not practically onerous. In this basic embodiment the value of the DLL gate width T_{DC} , which controls the DLL discriminator action is a compromise. It must be chosen somewhere in the range $T_S \leq T_{DC} \leq T_C$. Setting T_{DC} equal to chip width T_C gives the fastest response of the DLL in the initial tracking. Setting T_{DC} equal to the BOC sub-chip width T_S will however minimise the noise in the DLL estimate and extend the basic performance envelope. Such a failure condition is however fail safe since the receiver can always measure for itself when this condition has arisen.

Practical Implementation

The correlator architecture of a GNSS BOC receiver requires relatively few changes compared to a GNSS PSK receiver in order to implement the dual estimate in a triple loop technique. A general schematic of a correlator channel of the dual-estimate triple-loop receiver was shown in Figure 6. The incoming signal is mixed with, i.e. multiplied by, replica carrier, sub carrier and code waveforms each derived from separate digitally controlled oscillators (DCO). The resulting signal combinations are accumulated over the code period and the six correlation results formed, every correlation interval.

The correlator is arranged to produce an interrupt at least once every code epoch to instruct the processor to read the new accumulator values. New estimates of carrier, sub carrier and

code phase are then calculated and all three DCOs are updated. Each of the carrier, sub carrier and code DCOs are updated in three independent tracking loops. Provided that lock is achieved and maintained on the incoming signal the navigational data can be demodulated and processed. This process is equivalent in both hardware and software receivers.

Figure 18 shows an example of the top-level operations and tasks of a GNSS software receiver according to a further embodiment of the invention. The initialisation involves setting up the software and starting the correlator channels running. After initialisation the software enables the software interrupts. Typically two types of interrupt are used; a fast rate ($\approx 1\text{ms}$) interrupt for the tracking task which takes the highest priority and a slower rate ($\approx 100\text{ms}$) interrupt for the measurement task which is given a lower priority. The tracking task reads the accumulator values, estimates the navigational data state and updates all three loops with new estimates of carrier, sub carrier and code phase. The measurement task provides the detailed measurements required to form the navigation solution such as reading the carrier, sub carrier and code DCO values and necessary counters in the correlator. Under these essential tasks priority can be given to the various navigational tasks.

Table T1 shows the hardware requirements of each correlator channel based on receiver architecture designed to operate at an intermediate frequency IF of 11.38MHz, with a 50MHz sampling rate, 100ms measurement interval (TIC period) and 2-bit quantisation. The hardware requirements of the triple loop receiver as detailed in Table 1 are easily achievable (12 channels or more) with most modern ASIC and FPGA designs.

Components	Size	Number required per channel
Multipliers	4x1	8
	2x2	4
	2x4	2
Digitally Controlled Oscillators (DCO)	31 bits (frequency resolution = 23.03 mHz)	3 (Carrier, Sub carrier and Code DCOs)
Accumulators	19 bits	8
Counters	21 bits (carrier cycles in 100ms)	1
	20 bits (sub carrier cycles up to 10.23MHz)	1
	20 bits (code chips up to 10.23Mcps)	1

	11 bits (epoch counter 1ms epochs)	1
Registers	31 bits (phase register)	3 (Carrier, Sub carrier and Code DCO phase)

Table 1 Hardware requirements of triple loop architecture per channel.

Extensions and improvements

Faster dynamic response with max sensitivity

A significant extension and improvement to the above basic system is shown in Fig 8, compared to fig 7. In this embodiment the blocks and processes 42 43 44, 45 and 46 are replaced by a block 47 whose content and function will be described and also summarised in pseudo code. Execution of this block is synchronised to every correlation and is updated every correlation interval T

The same two timing errors $e_{\tau^*}[k]$ and $e_{\tau}[k]$ which were output from multipliers 38 and 39 respectively are now input to 47. The aim is again to generate two independent timing estimates to drive the sub-carrier DCO (17) and the code DCO 18 within an SLL and DLL respectively. The three different timing estimates, $\hat{\tau}^*[k]$, $\hat{\tau}[k]$ and $\hat{\tau}^+[k]$ in the basic system are however reduced to two: the same unambiguous lower accuracy $\hat{\tau}[k]$, generated by the DLL but now the single potentially ambiguous but higher accuracy estimate $\hat{\tau}^+[k]$ generated by the SLL is automatically integer corrected by the DLL. In this embodiment within block 47 error signals first update these two estimates (lines 33-1. 33-2). The filtered difference $\Delta\hat{\tau}$ between SLL estimate $\hat{\tau}^+[k]$ and the DLL estimate was evaluated on previous iteration (previous integer k value). If the magnitude of this difference is now found to have exceeded half a sub-chip width (line 33-3) then the high accuracy estimate is deemed to have slipped and is appropriately incremented or decremented (line 33-4) and the difference $\Delta\hat{\tau}$ reset to zero (line 33-5). Further, in line 33-6 the DLL gate width is suddenly expanded from whatever is its current narrower width (T_{DC}) to a full chip width T_C . The purpose of this manoeuvre is to speed up acquisition because it is likely that the DLL is in the process of acquiring lock. A typical simulation in the lower graph of fig 16 for the dotted line shows this effect at around count 65.

Otherwise the filtered difference between the two estimates has not exceeded half a sub-chip width (line 33-7). In which case a first order difference filter updates filtered $\Delta\hat{\tau}$ in

line 33-8 using the newly available updates $\hat{\tau}^+[k]$ and $\hat{\tau}[k]$ from lines 33-1 and 33-2 respectively. A gain term K_F controls the response time of this difference filter. Further, the gate width T_{DC} is reduced by a gate controller line 33-9, and in due course, over a sufficient number of iterations this width will continue to reduce asymptotically to a minimum value - made here to be equal to the sub-chip width T_S . This effect can be seen in lower graph dotted line from around count 120 in fig 16. The settling time of this asymptotic reduction is determined by a controller gain K_D .

The point of controlling the DLL gate downwards to this minimum is in order to minimise the noise in the DLL loop, which if excessive could trigger a false decision in line 33-3. In this way the operating range of the receiver is extended downwards to the lowest possible carrier to noise density ratio C/N_0 for a given loop bandwidth B_L . In this embodiment the DLL gate width $T_{DC}[k]$ therefore becomes a dynamic variable over the range $T_S \leq T_{DC} \leq T_C$ - as indicated by an arrow 48 pointing from block 47 to the DCO generator 18. Within block 47 a possible extension written in pseudo-code

$\rightarrow e_{\tau}, e_{\tau*}, \Delta\hat{\tau}, \hat{\tau}^+, \hat{\tau}, T_{DC}$

$$\hat{\tau}^+ \leftarrow \hat{\tau}^+ + k_{\tau*} e_{\tau*} \quad \text{SLL update} \quad (33-1)$$

$$\hat{\tau} \leftarrow \hat{\tau} + k_{\tau} e_{\tau} \quad \text{DLL update} \quad (33-2)$$

$$\text{If } |\Delta\hat{\tau}| > T_S/2 \quad (33-3)$$

$$\hat{\tau}^+ \leftarrow \hat{\tau}^+ + \text{sgn}(\Delta\hat{\tau}) \times T_S \quad (33-4)$$

$$\Delta\hat{\tau} \leftarrow 0 \quad (33-5)$$

$$T_{DC} \leftarrow T_C \quad (33-6)$$

$$\text{otherwise} \quad (33-7)$$

$$\Delta\hat{\tau} \leftarrow K_F \times (\hat{\tau} - \hat{\tau}^+ - \Delta\hat{\tau}) + \Delta\hat{\tau} \quad (33-8)$$

$$T_{DC} \leftarrow K_D \times (T_S - T_{DC}) + T_{DC} \quad (33-9)$$

$$\leftarrow \Delta\hat{\tau}, \hat{\tau}^+, \hat{\tau}, T_{DC}$$

Additional correlations for out of lock conditions

Not shown in either Figure 7 or figure 8 are potential improvements and alternatives, obtainable from computing further processing the down converted signals

$$v_{IEE}(t) = v_I(t) \times s(t - \hat{\tau}^* + T_{DS/2}) \times a(t - \hat{\tau} + T_{DC/2}) \quad (35)$$

$$v_{ILE}(t) = v_I(t) \times s(t - \hat{\tau}^* - T_{DS/2}) \times a(t - \hat{\tau} + T_{DC/2}) \quad (36)$$

$$v_{IEL}(t) = v_I(t) \times s(t - \hat{\tau}^* + T_{DS/2}) \times a(t - \hat{\tau} - T_{DC/2}) \quad (37)$$

$$v_{ILL}(t) = v_I(t) \times s(t - \hat{\tau}^* - T_{DS/2}) \times a(t - \hat{\tau} - T_{DC/2}) \quad (38)$$

$$v_{QEI}(t) = v_Q(t) \times s(t - \hat{\tau}^* + T_{DS/2}) \times a(t - \hat{\tau}) \quad (39)$$

$$v_{QLI}(t) = v_Q(t) \times s(t - \hat{\tau}^* - T_{DS/2}) \times a(t - \hat{\tau}) \quad (40)$$

$$v_{QIE}(t) = v_Q(t) \times s(t - \hat{\tau}^*) \times a(t - \hat{\tau} + T_{DC/2}) \quad (41)$$

$$v_{QIL}(t) = v_Q(t) \times s(t - \hat{\tau}^*) \times a(t - \hat{\tau} - T_{DC/2}) \quad (42)$$

from which may be integrated to corresponding correlations every T seconds to $w_{IEE}[k]$, $w_{ILE}[k]$, $w_{IEL}[k]$, $w_{ILL}[k]$, $w_{QEI}[k]$, $w_{QLI}[k]$, $w_{QIE}[k]$, $w_{QIL}[k]$ respectively. Further, there may be extracted correlation differences

$$w_{IQQ} = (w_{ILL} - w_{IEL}) - (w_{ILE} - w_{IEE}) \quad (43)$$

$$w_{QQI} = w_{QLI} - w_{QEI} \quad (44)$$

$$w_{QIQ} = w_{QIL} - w_{QIE} \quad (45)$$

These correlations may be used to enhance and generalise operation of the invention in many different ways.

For example from (24) it can be realized that, when the estimating process is far from lock i.e. when $\hat{\tau}^*$ is far away from τ^* , then because of the relatively small amplitude to $\text{trc}(\)$ the correction gain to τ^* will be small because the amplitude of $\text{trc}(\)$ is relatively small. The consequence is a slow updating of $\hat{\tau}^*$. To deal with this an additional term (ii) can be added to (28) for updating the DLL error, which now reads

$$e_{\tau} \leftarrow \underset{\text{i}}{w_{IIQ} \times \hat{d}} + \underset{\text{ii}}{B \times w_{IQQ} \times w_{IQI}} \quad (46)$$

where B is an appropriate scaling constant. This action can be seen to be beneficial because

$$\begin{aligned} w_{IQQ} &\approx A \times \cos(\phi - \hat{\phi}) \times \text{Trs}(\tau^* - \hat{\tau}^*) \times \sqrt{\Lambda}(\tau - \hat{\tau}) \times d^* \\ w_{IQI} &\approx A \times \cos(\phi - \hat{\phi}) \times \text{Trs}(\tau^* - \hat{\tau}^*) \times \Lambda(\tau - \hat{\tau}) \times d^* \end{aligned} \quad (47)$$

the trapezium sine function $\text{Trs}(\)$ will have greater amplitude than $\text{trc}(\)$ when $\hat{\tau}^*$ is sufficiently far from τ^* . Compare (17) and (24)

The aim here is to provide a boost to DLL acquisition if and when the SLL is far off lock and the correlation term w_{IIQ} has a temporarily small value

Improvement from carrier aiding

The invention admits the standard technique of carrier aiding - the technique of importing into the delay estimate a correction proportional to the Doppler frequency. The equations (29) can be modified accordingly to read

$$\hat{\tau}^* \leftarrow \hat{\tau}^* + k_{\phi*} f_{\phi} + k_{\tau*} e_{\tau*} \quad (48)$$

$$\hat{\tau} \leftarrow \hat{\tau} + k_{\phi} f_{\phi} + k_{\tau} e_{\tau} \quad (49)$$

Term f_{ϕ} is the same as in the PLL equations (29a) and is interpreted as a scaled Doppler shift estimate (either positive or negative depending on the sign of the relative motion). Constants k_{ϕ} and $k_{\phi*}$ are pre-calculated to provide the necessary open loop correction of Doppler shift appropriately scaled down to the code rate and sub-carrier rate respectively

Alternative embodiments of error discriminators

The computation to error sequences according to (26)(27) and (28) utilised only one of many possible discriminators. The standard alternatives available in the dual-loop single- estimate conventional PSK receivers may be adopted here, after appropriate modification

PLL discriminators

From (25) and (26) the equivalent formulation is

$$e_{\phi} \leftarrow w_{QII}[k] \times \text{sgn}(w_{III}) \quad (50)$$

Dispensing with $\text{sgn}()$ operation gives

$$e_{\phi} \leftarrow w_{QII}[k] \times w_{III} \quad (51)$$

Expressing this as a ratio gives

$$e_{\phi} \leftarrow \frac{w_{QII}}{w_{III}} \quad (52)$$

To improve tracking when SLL is not yet in lock one can adopt

$$e_{\phi} \leftarrow w_{QII} \times \text{sgn}(w_{III}) + w_{QOI} \times \text{sgn}(w_{IOI}) \quad (53)$$

from which removing $\text{sgn}()$ gives

$$e_{\phi} \leftarrow w_{QII} \times w_{III} + w_{QOI} \times w_{IOI} \quad (54)$$

SLL discriminator

From (25) and (27) the equivalent formulation is

$$e_{\tau^*} \leftarrow w_{IOI} \times \text{sgn}(w_{III}) \quad (55)$$

Dispensing with the $\text{sgn}(\)$ operation gives

$$e_{\tau^*} \leftarrow w_{IOI} \times w_{III} \quad (56)$$

Expressing this as a ratio gives

$$e_{\tau^*} \leftarrow \frac{w_{IOI}}{w_{III}} \quad (57)$$

DLL discriminator

From (25) and (28) the equivalent formulation is

$$e_{\tau} \leftarrow w_{IIQ} \times \text{sgn}(w_{III}) \quad (58)$$

Removing the $\text{sgn}(\)$ operation gives

$$e_{\tau} \leftarrow w_{IIQ} \times w_{III} \quad (59)$$

Improved convergence when SLL is not yet in lock

$$e_{\tau} \leftarrow w_{IIQ} \times \text{sgn}(w_{III}) + w_{IOQ} \times \text{sgn}(w_{IOI}) \quad (60)$$

or even hybrid

$$e_{\tau} \leftarrow w_{IIQ} \times \text{sgn}(w_{III}) + B \times w_{IOQ} \times w_{IOI} \quad (61)$$

Incoherent DLL embodiment

It has been claimed that an incoherent DLL receiver is more effective for standard PSK GNSS. A representative paper is "Theory and Performance of narrow correlation spacing in a GPS receiver", A.J. Van Dierendonck et al ION National Technical Meeting San Diego CA Jan 1992. This concept requires a frequency locked loop (FLL) instead of a PLL. This type of system is readily incorporated into the dual estimate concept for BOC-GNSS requiring however some of the additional correlations identified from (35) to (42)

The implementation of an FLL requires only that the difference between the phase and the phase estimate

$$\Delta\phi = \phi - \hat{\phi} \quad (62)$$

be made to settle at some arbitrary constant rather than zero . The aim however with the control of the time estimates in the two loops is again that $\hat{\tau}^* \rightarrow \tau + nT_s$ and $\hat{\tau} \rightarrow \tau$. But effective tracking of the SLL sub carrier phase (to yield estimate $\hat{\tau}^*$) and the DLL (to yield estimate $\hat{\tau}$) must generate an error signal which is indifferent to an arbitrary constant offset between $\hat{\phi}$ and ϕ

It is necessary then to realise a frequency discriminator from the correlations and/or correlation differences, and to ensure that the SLL and DLL discriminators are indifferent to carrier phase error

FLL discriminators

First we can compute a frequency error from current and previous correlations and correlation differences

$$e_{\omega QI} \leftarrow w_{QII} \operatorname{sgn}(w_{III}^-) - w_{III} \operatorname{sgn}(w_{QII}^-) \quad (63)$$

where the notation w_{III}^- and w_{QII}^- stands for correlation in the previous correlation (earlier by T) One can also form

$$e_{\omega II} \leftarrow w_{III} \operatorname{sgn}(w_{III}^-) + w_{QII} \operatorname{sgn}(w_{QII}^-) \quad (64)$$

which allows a 2-quadrant computation

$$e_{\omega} = \frac{\langle e_{\omega QI} \rangle}{\langle e_{\omega II} \rangle} \approx \tan(\Delta\omega) \quad (65)$$

Alternatively a 4 quadrant computation

$$e_{\omega} = \arctan 2(\langle e_{\omega QI} \rangle, \langle e_{\omega II} \rangle) \quad (66)$$

More robust acquisition can be used which allows for SLL not in lock as in previous embodiments:

$$\begin{aligned} e_{\omega Q} \leftarrow & w_{QII} \operatorname{sgn}(w_{III}^-) - w_{III} \operatorname{sgn}(w_{QII}^-) \\ & + w_{QQI} \operatorname{sgn}(w_{IQI}^-) - w_{IQI} \operatorname{sgn}(w_{QQI}^-) \end{aligned} \quad (67)$$

Similarly

$$\begin{aligned} e_{\omega I} \leftarrow & w_{III} \operatorname{sgn}(w_{III}^-) + w_{QII} \operatorname{sgn}(w_{QII}^-) \\ & + w_{IQI} \operatorname{sgn}(w_{IQI}^-) + w_{QQI} \operatorname{sgn}(w_{QQI}^-) \end{aligned} \quad (68)$$

which allows a 2-quadrant computation

$$e_{\omega} = \frac{\langle e_{\omega Q} \rangle}{\langle e_{\omega I} \rangle} \approx \tan(\Delta\omega) \quad (69)$$

Alternatively a 4 quadrant computation

$$e_{\omega} = \arctan 2(\langle e_{\omega Q} \rangle, \langle e_{\omega I} \rangle) \approx \Delta\omega \quad (70)$$

Another alternative is to dispense with sgn functions as in (63) so that

$$e_{\omega QI} \leftarrow w_{QII} w_{III} - w_{III} w_{QII} \quad (71)$$

and one can also form

$$e_{\omega II} \leftarrow w_{III} w_{III} + w_{QII} w_{QII} \quad (72)$$

which again allows a 2-quadrant computation or a 4 quadrant comparison.

SLL discriminator

The discriminator must work for an arbitrary phase difference $\Delta\phi$

Discriminator (27) does not work in this case, so we need to extend to

$$e_{\tau^*} \leftarrow w_{IQI} \text{sgn}(w_{III}) + w_{QOI} \text{sgn}(w_{QII}) \quad (73)$$

One can dispense with sgn() to obtain

$$e_{\tau^*} \leftarrow w_{IQI} w_{III} + w_{QOI} w_{QII} \quad (74)$$

DLL discriminator

The discriminator must work for an arbitrary phase difference $\Delta\phi$

Discriminator (28) does not work in this case, so we need to extend to

$$e_{\tau} \leftarrow w_{IIQ} \text{sgn}(w_{III}) + w_{QIQ} \text{sgn}(w_{QII}) \quad (75)$$

One can dispense with sgn() to obtain

$$e_{\tau} \leftarrow w_{IIQ} w_{III} + w_{QIQ} w_{QII} \quad (76)$$

Computing the difference of power direct from early and late correlations gives

$$e_{\tau} \leftarrow w_{IIL}^2 + w_{QIL}^2 - w_{IIE}^2 - w_{QIE}^2 \quad (77)$$

which one may enhance with further correlations to obtain

$$e_{\tau} \leftarrow (w_{IIL}^2 + w_{QIL}^2 + w_{IQL}^2 + w_{QQL}^2) - (w_{IIE}^2 + w_{QIE}^2 + w_{IQE}^2 + w_{QQE}^2) \quad (78)$$

Computing the difference of amplitude direct from early and late correlations gives

$$e_{\tau} \leftarrow \sqrt{w_{IIL}^2 - w_{QIL}^2} - \sqrt{w_{IIE}^2 - w_{QIE}^2} \quad (79)$$

and computing the normalised difference gives

$$e_{\tau} \leftarrow \frac{\sqrt{w_{\text{IIL}}^2 - w_{\text{QIL}}^2} - \sqrt{w_{\text{IIE}}^2 + w_{\text{QIE}}^2}}{\sqrt{w_{\text{IIL}}^2 - w_{\text{QIL}}^2} - \sqrt{w_{\text{IIE}}^2 + w_{\text{QIE}}^2}} \quad (80)$$

Loop Operations

An appropriate modification for ‘incoherent DLL’ can be expressed in pseudo code as:

$$\begin{aligned} e_{\phi} &\leftarrow e_{\phi} + e_{\omega I} \\ f_{\phi} &\leftarrow f_{\phi} + e_{\phi} \quad] \text{ FLL} \\ \hat{\phi} &\leftarrow \hat{\phi} + k_1 f_{\omega} + k_2 e_{\phi} \\ \hat{\tau}^* &\leftarrow \hat{\tau}^* + k_{\tau^*} e_{\tau^*} \quad] \text{ SLL} \\ \hat{\tau} &\leftarrow \hat{\tau} + k_{\tau} e_{\tau} \quad] \text{ DLL} \end{aligned} \quad (81)$$

which can be extended by carrier aiding

AltboC formulation

An original feature of the proposed Galileo GNSS is the proposal to include up to four different codes in the same transmission. Proposed extensions to BOC now put additional codes into the one structure.

Half AltboC

The modulation can be written, instead of the usual complex variable formulation, in terms of in-phase and quadrature sub-carrier modulations. Initially for just two codes

$$\begin{aligned} u_{\text{BOC}}(t) = A \times [a_1(t - \tau) + a_2(t - \tau)] \times s(t - \tau) \times \cos(\omega_C t + \phi) + \\ A \times [a_1(t - \tau) - a_2(t - \tau)] \times \tilde{s}(t - \tau) \times \sin(\omega_C t + \phi) \end{aligned} \quad (82)$$

Here $a_1(t)$ and $a_2(t)$ are the two different codes.

For simplicity the possible further modulation by data is omitted. The in-phase sub-carrier modulation $s(\cdot)$ may be a square sine wave (sqs($\cdot$)) in which case the quadrature sub-carrier modulation $\tilde{s}(\cdot)$ is a square cosine wave (sqc($\cdot$)). Alternatively the in-phase sub-carrier modulation $s(\cdot)$ may be a square cosine wave (sqc($\cdot$)) in which case the quadrature sub-carrier modulation $\tilde{s}(\cdot)$ is a square sine wave (sqs($\cdot$)).

It can be shown mathematically that the upper and lower sidebands individually are modulated by the separate codes.

In the embodiment of a dual estimator a reference is generated again according to (4) and (5) in order to create parallel I signal $v_I(t)$ and Q signal $v_Q(t)$ (in phase and quadrature). The mathematical structure of the two products after filtering may be described as

$$v_I(t) = A \times \cos(\phi - \hat{\phi}) \times s(t - \tau) \times [a_1(t - \tau) + a_2(t - \tau)] \\ + A \times \sin(\phi - \hat{\phi}) \times \tilde{s}(t - \tau) \times [a_1(t - \tau) - a_2(t - \tau)] \quad (83)$$

$$v_Q(t) = A \times \sin(\phi - \hat{\phi}) \times s(t - \tau) \times [a_1(t - \tau) + a_2(t - \tau)] \\ - A \times \cos(\phi - \hat{\phi}) \times \tilde{s}(t - \tau) \times [a_1(t - \tau) - a_2(t - \tau)] \quad (84)$$

where $\hat{\phi}$ is the trial tracking phase.

The user has a choice in tracking either the sum or the difference of the codes. If intending to track the sum of the codes and not the difference of codes a further four waveform functions are created by multiplying test v_I and v_Q by a selection from analysing functions. There are early, prompt, and late formulations of sub-carrier $s(t - \hat{\tau}^*)$, and early, prompt and late formulations of code sum $a_1(t - \hat{\tau}^*) + a_2(t - \hat{\tau}^*)$

$$v_{III}(t) = v_I(t) \times s(t - \hat{\tau}^*) \times [a_1(t - \hat{\tau}) + a_2(t - \hat{\tau})] \quad (85)$$

$$v_{QII}(t) = v_Q(t) \times s(t - \hat{\tau}^*) \times [a_1(t - \hat{\tau}) + a_2(t - \hat{\tau})] \quad (86)$$

$$v_{IEI}(t) = v_I(t) \times s(t - \hat{\tau}^* + T_{DS}/2) \times [a_1(t - \hat{\tau}) + a_2(t - \hat{\tau})] \quad (87)$$

$$v_{ILI}(t) = v_I(t) \times s(t - \hat{\tau}^* - T_{DS}/2) \times [a_1(t - \hat{\tau}) + a_2(t - \hat{\tau})] \quad (88)$$

$$v_{IIE}(t) = v_I(t) \times s(t - \hat{\tau}^*) \times [a_1(t - \hat{\tau} + T_{DC}/2) + a_2(t - \hat{\tau} + T_{DC}/2)] \quad (89)$$

$$v_{IIL}(t) = v_I(t) \times s(t - \hat{\tau}^*) \times [a_1(t - \hat{\tau} - T_{DC}/2) + \tilde{a}_2(t - \hat{\tau} - T_{DC}/2)] \quad (90)$$

where $\hat{\tau}^*$ and $\hat{\tau}$ are again trial delay estimates. These waveforms are individually integrated and then sampled i.e. correlated to exactly the same functions as given from (17) to (22) and will ignore the right hand terms in (83) and (84) which are modulated by the code difference. The reason is that the difference of codes is orthogonal to the sum of the codes and therefore will not contribute to any correlation.

Correlations are computed in the same manner as for ordinary BOC and appropriate correlation differences. All proceeds after in the same way as for ordinary BOC. It is equally possible to process appropriate demodulated waveforms with difference of codes

Full Altboc

The concept of 'altboc' supports up to 4 modulations. The simplest formulation reads , and again without recourse to complex variable notation

$$\begin{aligned}
 u(t) = & A_1 \times [a_1(t-\tau) + a_2(t-\tau)] \times s(t-\tau) \times \cos(\omega_C t + \phi) + \\
 & A_1 \times [a_1(t-\tau) - a_2(t-\tau)] \times \tilde{s}(t-\tau) \times \sin(\omega_C t + \phi) + \\
 & A_2 \times [a_3(t-\tau) + a_4(t-\tau)] \times \tilde{s}(t-\tau) \times \cos(\omega_C t + \phi) + \\
 & A_2 \times [a_3(t-\tau) - a_4(t-\tau)] \times s(t-\tau) \times \sin(\omega_C t + \phi)
 \end{aligned} \tag{91}$$

which compared with (82) is seen to have two more terms embodying sum and difference of two more code functions $a_3(t)$ and $a_4(t)$. After multiplication by the carrier the down converted signals are

$$\begin{aligned}
 v_I(t) = & A_1 \times \cos(\phi - \hat{\phi}) \times s(t-\tau) \times [a_1(t-\tau) + a_2(t-\tau)] \\
 & + A_1 \times \sin(\phi - \hat{\phi}) \times \tilde{s}(t-\tau) \times [a_1(t-\tau) - a_2(t-\tau)] \\
 & A_2 \times \cos(\phi - \hat{\phi}) \times \tilde{s}(t-\tau) \times [a_3(t-\tau) + a_4(t-\tau)] \\
 & + A_2 \times \sin(\phi - \hat{\phi}) \times s(t-\tau) \times [a_3(t-\tau) - a_4(t-\tau)]
 \end{aligned} \tag{92}$$

$$\begin{aligned}
 v_Q(t) = & A_1 \times \sin(\phi - \hat{\phi}) \times s(t-\tau) \times [a_1(t-\tau) + a_2(t-\tau)] \\
 & - A_1 \times \cos(\phi - \hat{\phi}) \times \tilde{s}(t-\tau) \times [a_1(t-\tau) - a_2(t-\tau)] \\
 & + A_2 \times \sin(\phi - \hat{\phi}) \times \tilde{s}(t-\tau) \times [a_3(t-\tau) + a_4(t-\tau)] \\
 & - A_2 \times \cos(\phi - \hat{\phi}) \times s(t-\tau) \times [a_3(t-\tau) - a_4(t-\tau)]
 \end{aligned} \tag{93}$$

The ALTBOC signal may be tracked again with the sum or difference of $a_1()$ and $a_2()$.

Alternatively it may be tracked with sum or difference of $a_3()$ and $a_4()$

Computer generated simulation

Figs 16 and 17 show a simulation of the triple loop- dual estimator in action according to the embodiment of fig 8, and as described in earlier section. The chosen parameters are exactly the same in the two figures but without and with additive noise respectively. The aim here is not only to demonstrate the anti-slip fail safe nature of the triple loop but also to show a typical acquisition process. There is assumed to have been an initial search - just as in standard PSK-CDMA - which brings the code delay estimate within $\pm T_C$ of the actual input delay and therefore within range of the DLL discriminator.

Simulation values are deliberately chosen for the most stringent test of possible operation. The $C/N_0 = 250$ Hz is equivalent to 24dBHz and is the very low value chosen in the already cited paper by Fine and Wilson. This carrier to noise density ratio is significantly

lower than usual test conditions for GNSS signals. The BOC modulation is the most demanding highest proposed rate BOC(6f, f). Correlation interval $T = 20$ ms gives 10 dB signal to I channel noise ratio. Normalised chip width $T_C = 1$. Normalised sub-chip width $T_S = 1/12$. The loop bandwidth of $B_L = 0.5$ Hz (an equivalent settling time $T_L = 1$ s) is the highest allowed for this low value of C/N_0 and highest rate ratio $f_S / f_C = 6$. The test here shows that the algorithm will simultaneously acquire both estimates and instantaneously correct the SLL estimate from the DLL estimate while the loops are locking up. Tracking performance depends on the difference the actual code delay and the initial setting of the loop estimates after an initial search. The example synthesised actual delay $\tau = \tau_0 = 4.45/12$ or $4.45 \times T_S$ which is near a worst-case start up condition with the DLL and SLL loops originally initialised in this example with $\hat{\tau}^* = 0$ and $\hat{\tau} = 0$. Filter gains $K_F = 0.5$ and $K_D = 0.02$ were chosen empirically as a result of these tests.

The rising dotted curve in the upper graph is the DLL estimate. Acquisition starts relatively slowly but speeds up on an automatic opening of the DLL gate at around count 65 in fig 16 (as confirmed by dotted curve in lower graph). The stepped continuous curve in upper graph is the corrected SLL estimate $\hat{\tau}^+$. The step occur whenever the filter difference $\Delta\hat{\tau}$ between this and the DLL estimate exceeds half a sub chip width. The whole point and purpose of the invention is demonstrated here: namely when the loops are active (and the signal to noise is high enough) it is impossible for the higher -accuracy lower noise SLL estimate to slip more than $\pm T_S/2$ out of alignment with the lower accuracy higher error DLL estimate. The dotted curve depicts filtered difference $\Delta\hat{\tau}$ tracking between these limits.

Acquisition is complete on a step at around 120 counts of 2.4 s which compares favourably with the nominal loop settling time $T_L \approx 1$ sec. The simulation also monitors the tracking of the third carrier tracking loop which here is a 2nd order PLL. An input true carrier phase of $\phi = 30$ deg was adopted arbitrarily. The continuous track on the lower graph is the phase estimate and shows the characteristic overshoot of a second order loop.

Similar but random results with additive electrical noise actually present are shown in example from fig 17. The acquisition time is accordingly a random variable. It can take longer (as here); or it can be shorter. The much higher quality of the SLL estimate compared to the DLL is evident.

The advantage of some embodiments of the present invention over the prior art may include the following: the method can realise the potential accuracy of BOC - as does the

bump-jumping method described in the prior art but without the inherent delay in that process. Discounting loop settling time (common to all systems) the correct estimate is essentially instantaneous. By contrast the bump-jumping algorithm can be waiting for hundreds of milliseconds to several seconds before it 'knows' that it has locked onto the wrong peak, or 'false node'. The present invention avoids locking on a wrong peak (false node), provided uncritical requirements on input carrier to noise density ratio and loop bandwidth are met, since there is no multi-peaked correlation function in the first place. It is therefore fail safe. It is also insensitive to non-linear amplitude/ frequency conversion that may be present in the transmission chain.

The described embodiments of the invention are only examples of how the invention may be implemented. Modifications, variations and changes to the described embodiments will occur to those having appropriate skills and knowledge. These modifications, variations and changes may be made without departure from the scope of the invention defined in the claims and its equivalents.

CLAIMS

1. A receiver for receiving a navigation signal comprising a carrier modulated by a code modulation function of a given code rate and further modulated by a sub-carrier modulation function having a sub-carrier rate different to the code rate, the receiver comprising processing means arranged to:
 - generate a first estimate of delay based on the code modulation;
 - generate a second estimate of delay based on the sub-carrier modulation; and
 - determine an optimal delay estimate from the first and second delay estimates.
2. A receiver according to claim 1 wherein the processing means is arranged in determining the optimal delay, to shift the second estimate by an integer number of half cycles to bring it towards the first estimate.
3. A receiver according to claim 1 or claim 2 wherein the processing means is arranged in determining the optimal delay estimate, to calculate a delay difference as the difference between the first and second estimates rounded to an integer number of sub-carrier half cycles.
4. A receiver according to claim 3 wherein the processing means is arranged, in determining the optimal delay estimate, to add the delay difference to the second estimate of delay.
5. A receiver according to any foregoing claim wherein the processing means is arranged to update the first and second estimates iteratively and to calculate the delay difference and add it to the second estimate repeatedly.
6. A receiver according to any of claims 1 to 4 wherein the processing means is arranged to update the first and second estimates iteratively until they converge towards respective final values and to calculate the delay difference and the optimal delay from the final values.
7. A receiver according to any foregoing claim wherein the processing means includes:
 - a reference code signal generator arranged to generate at least one reference code signal using the first estimate of delay;
 - a reference sub-carrier signal generator arranged to generate at least one reference sub-carrier signal using the second estimate of delay; and
 - correlation means arranged to generate correlations based on the reference signals and at least one component of the received signal.

8. A receiver according to claim 7 wherein the processing means is arranged to use the correlations to generate error estimations for the delay estimates, and to update the delay estimates based on the error estimations.
9. A receiver according to claim 7 or claim 8 wherein the at least one reference sub-carrier signal includes an early reference sub-carrier signal and a late reference sub-carrier signal separated by a gate width time difference.
10. A receiver according to any of claims 7 to 9 wherein the at least one reference code signal includes an early reference code signal and a late reference code signal separated by a gate width time difference.
11. A receiver according to claim 9 or claim 10 wherein the gate width time difference is variable.
12. A receiver according to claim 11 wherein the processing means is arranged to vary the gate width time difference as the trial sub-carrier delay is updated.
13. A receiver according to claim 12 when dependent on claim 3 wherein the processing means is arranged to detect a slip condition in the updating of the trial sub-carrier delay corresponding to a change in the estimated value of the integral number, and to increase the gate width time difference in response to the slip condition.
14. A receiver according to any of claims 7 to 13 wherein the correlation means is arranged to generate a plurality of correlations that vary in different ways as the trial delay approaches an actual delay and to combine them to determine the error estimation.
15. A receiver according to claim 14 wherein the processing means is arranged to combine the correlations in a manner which varies as the delay approaches the actual delay to determine the error estimations.

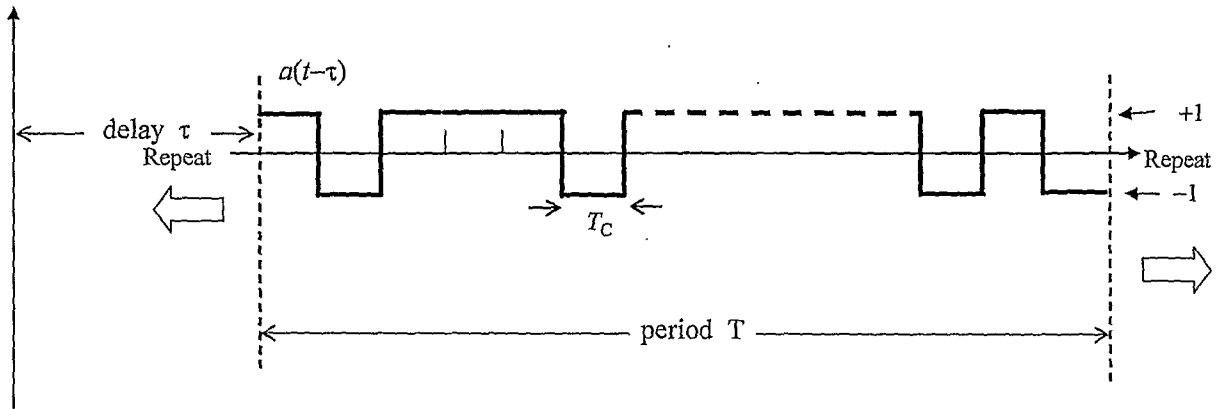
Drawings

Fig 1

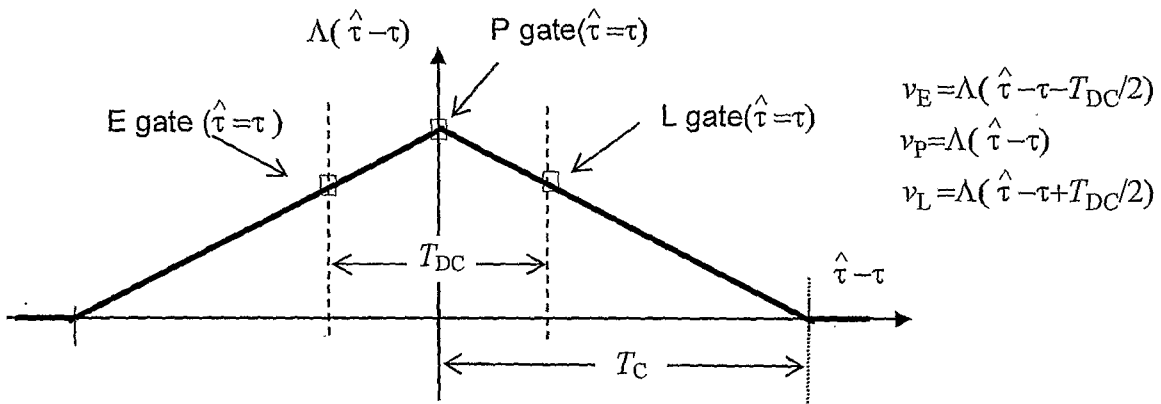


Fig 2

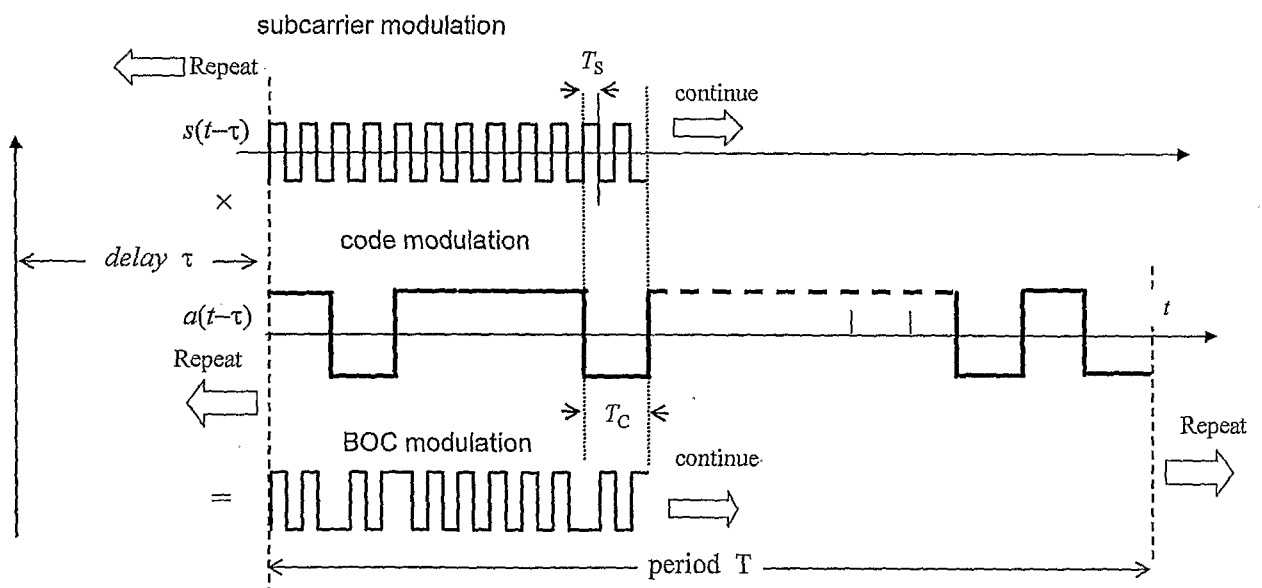


Fig 3

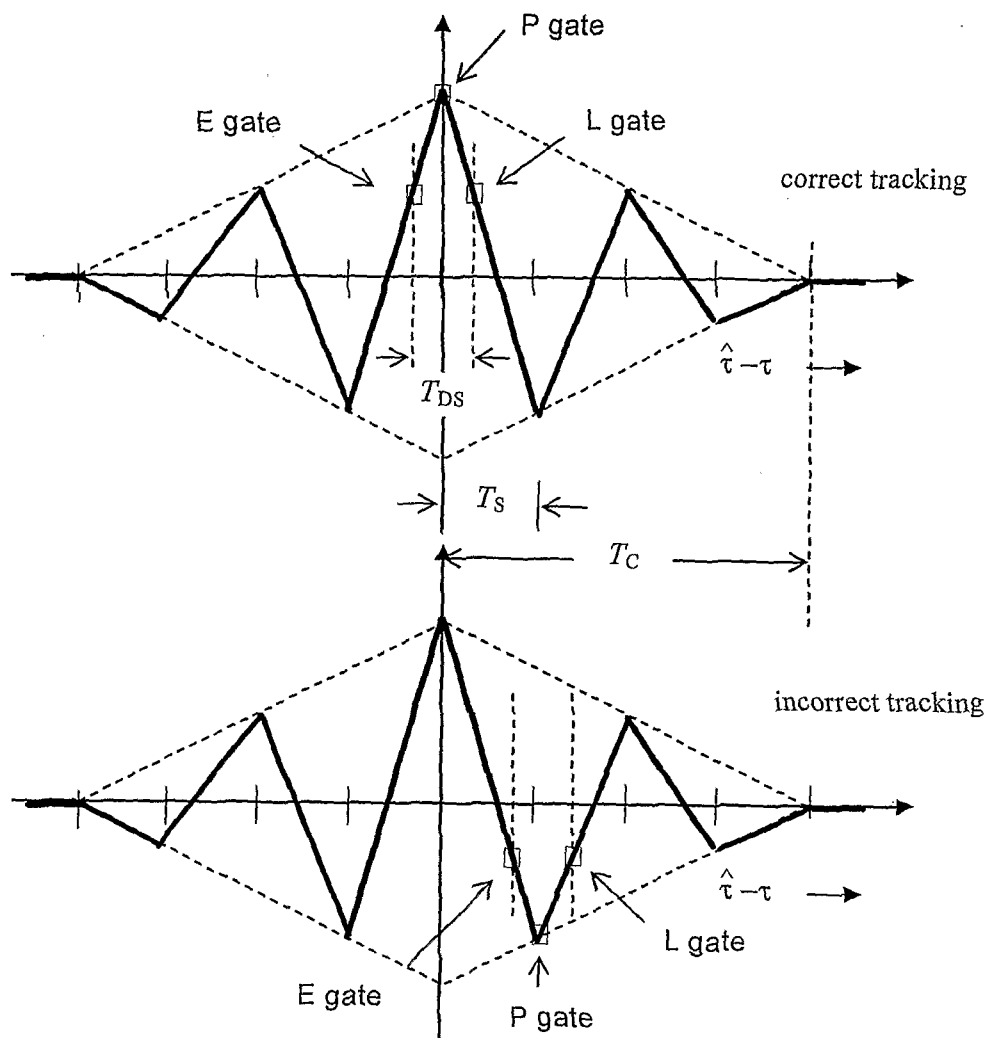


Fig 4

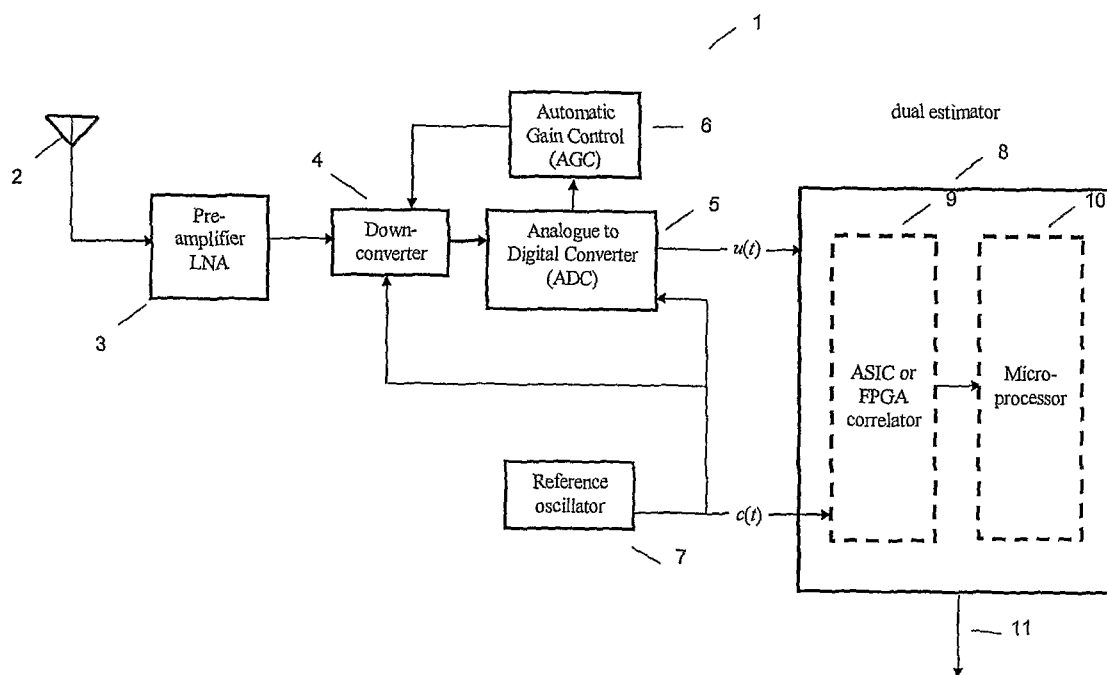


Fig 5

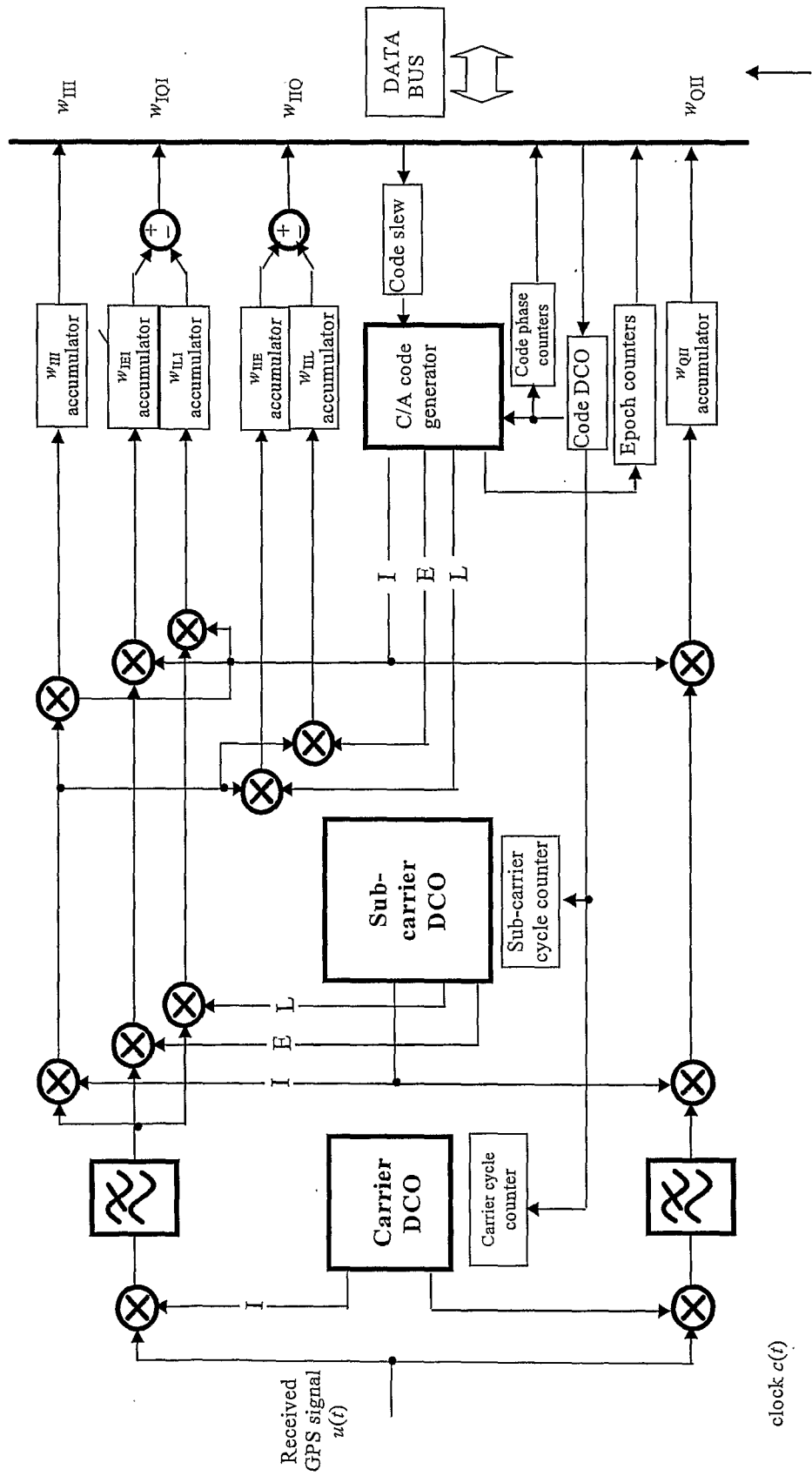


Fig 6

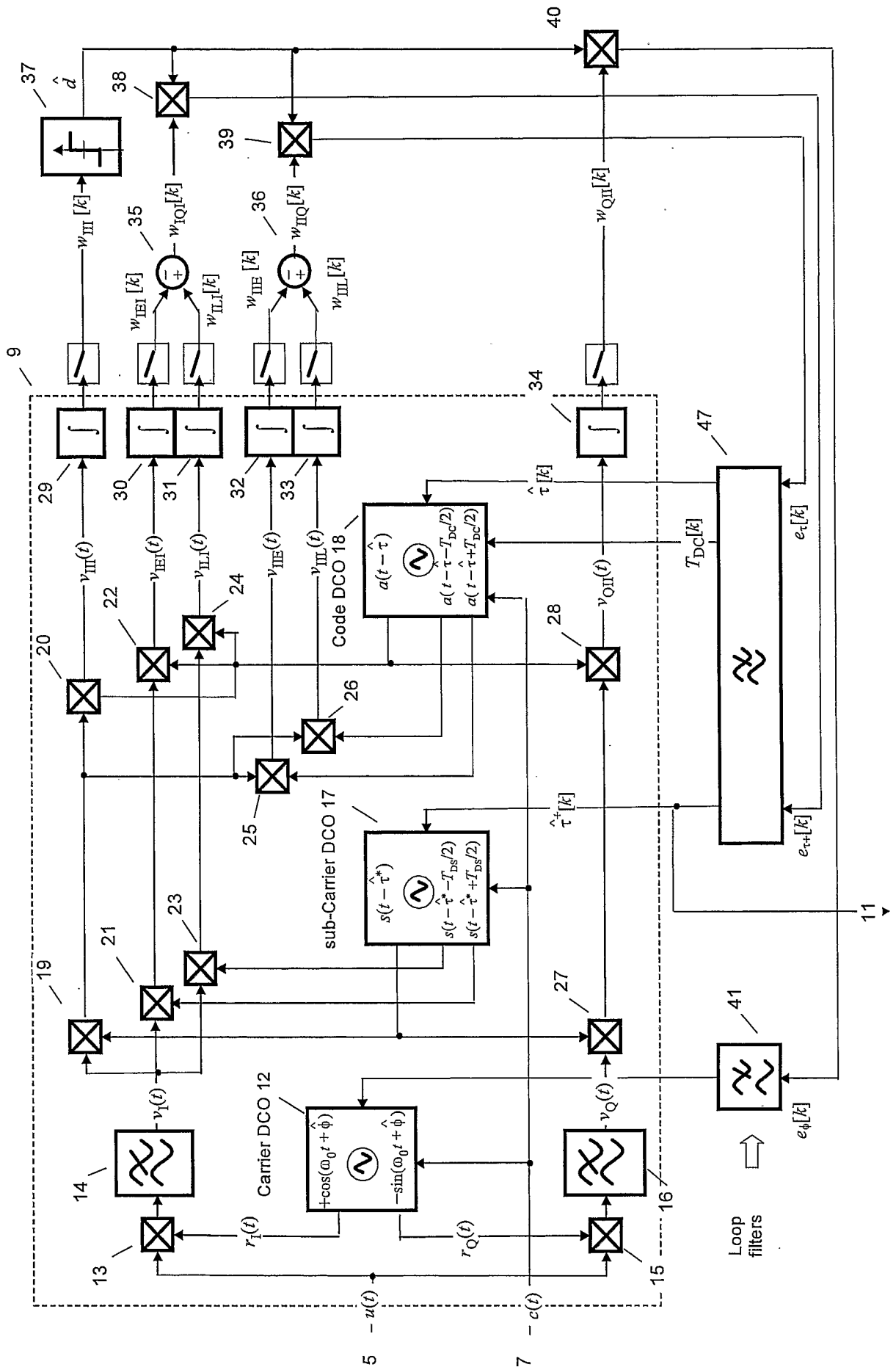


Fig 8

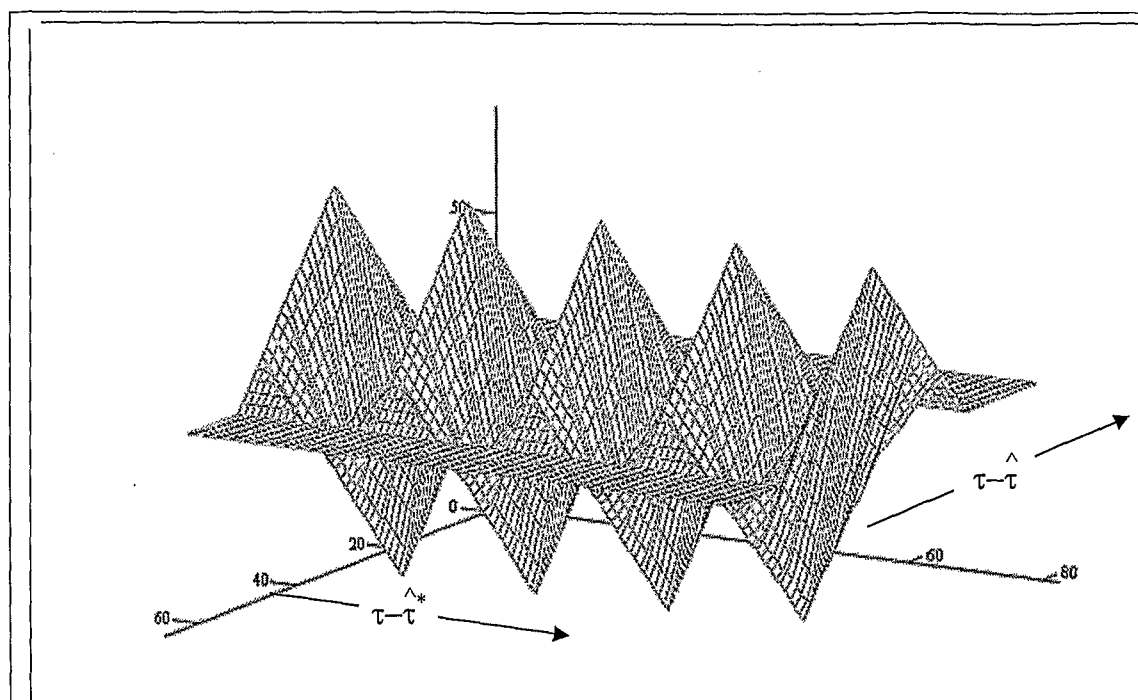


Fig 9

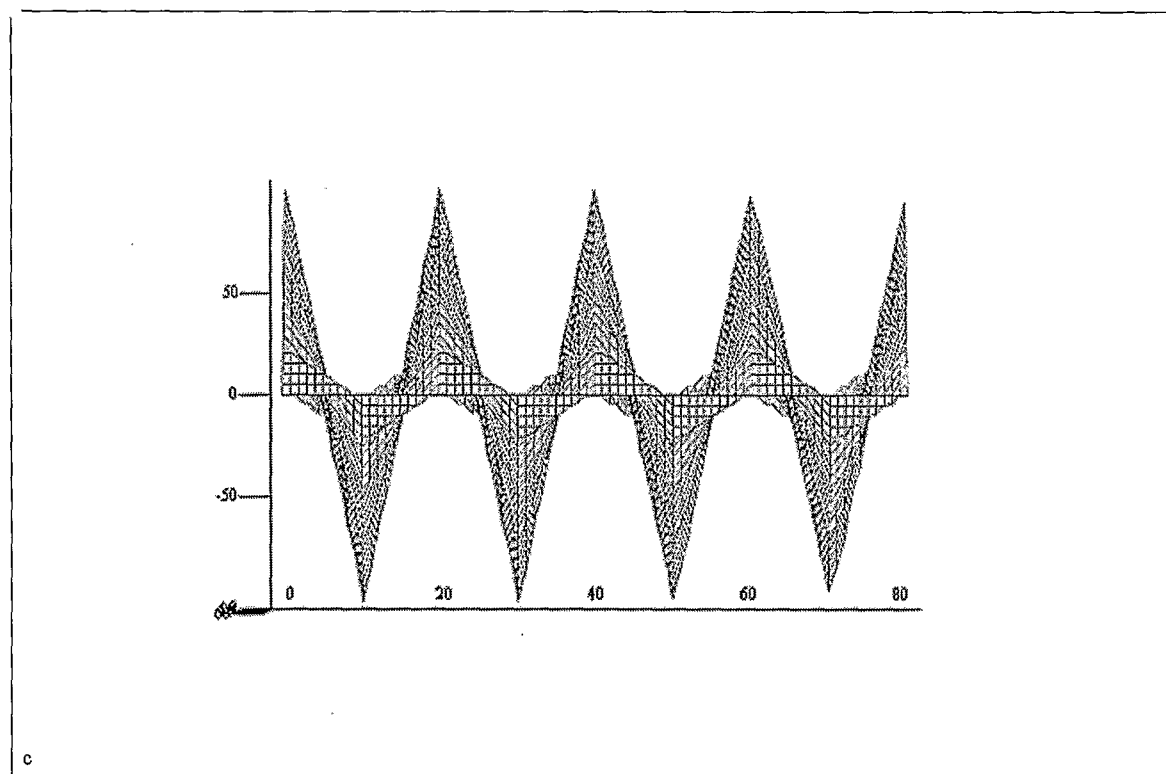


Fig 10

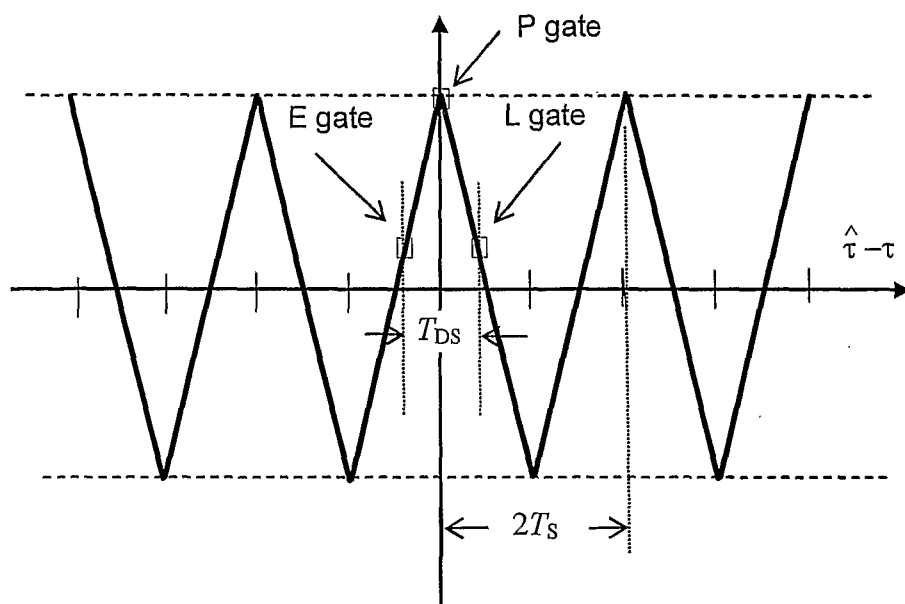


Fig 11

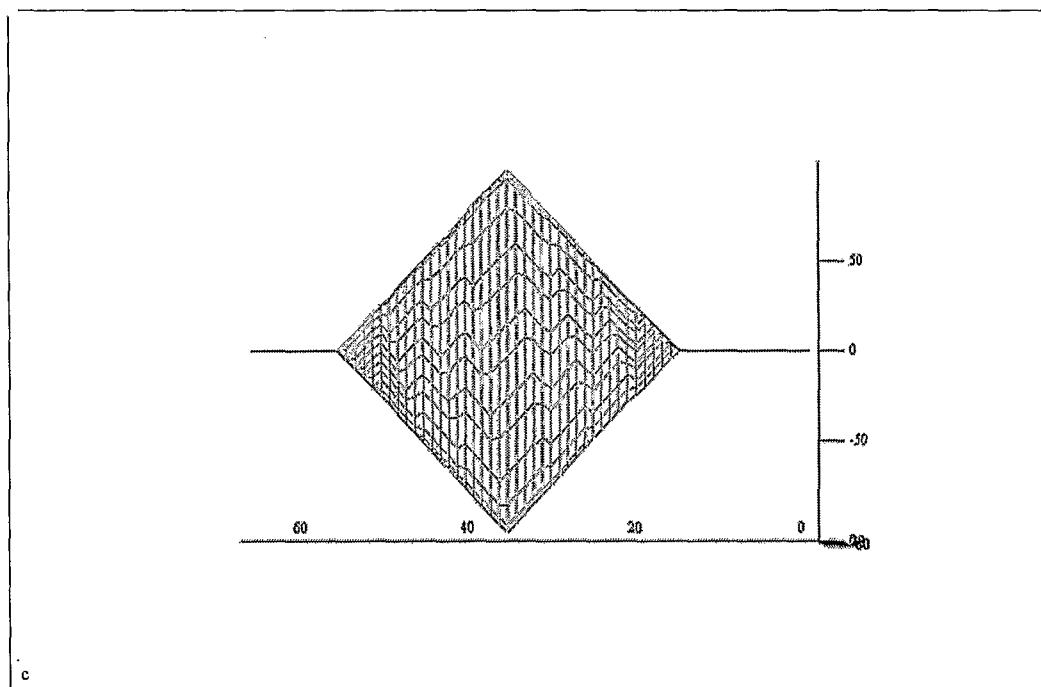


Fig 12

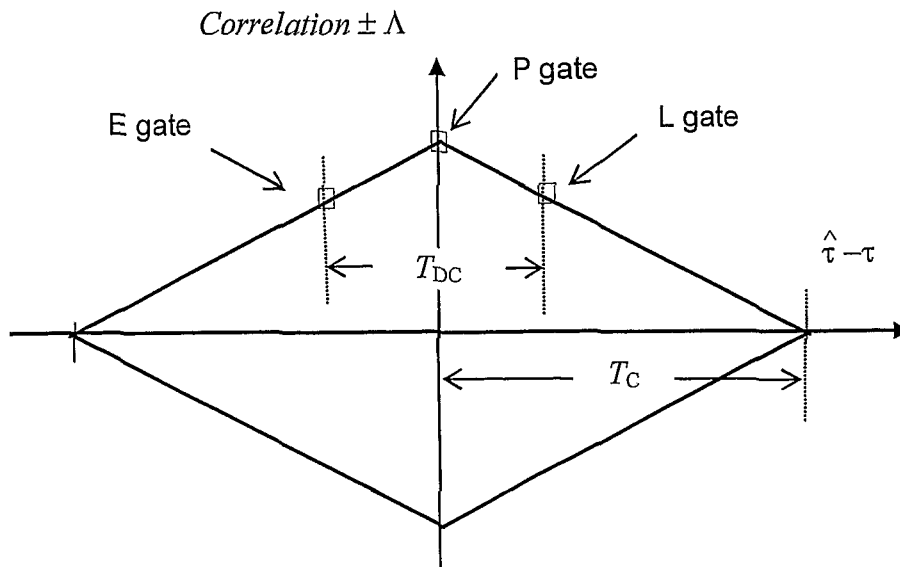


Fig 13

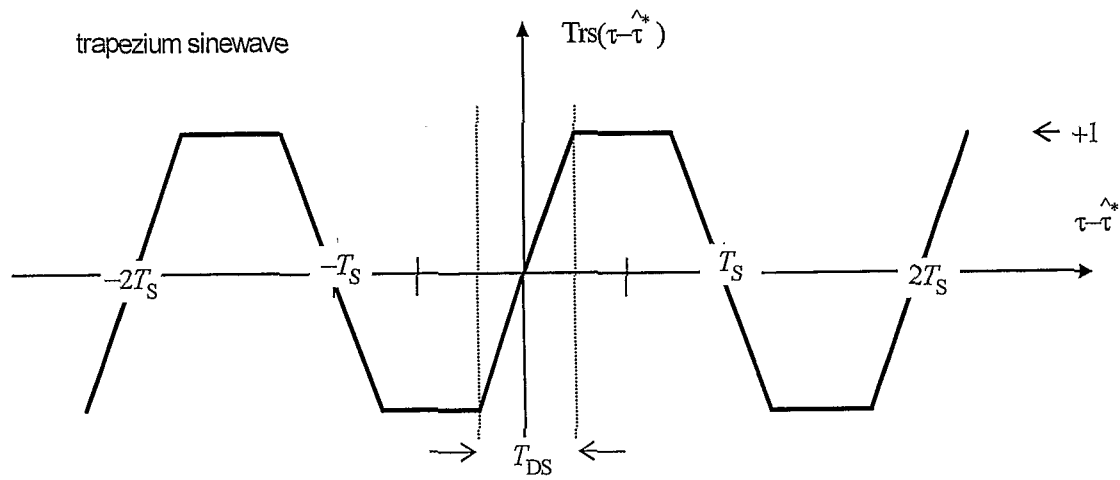


fig 14

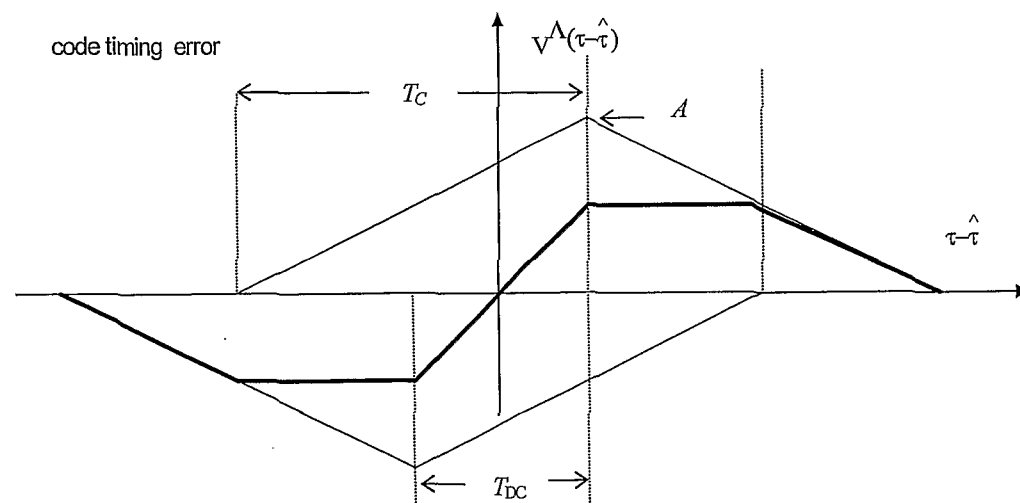


fig 15

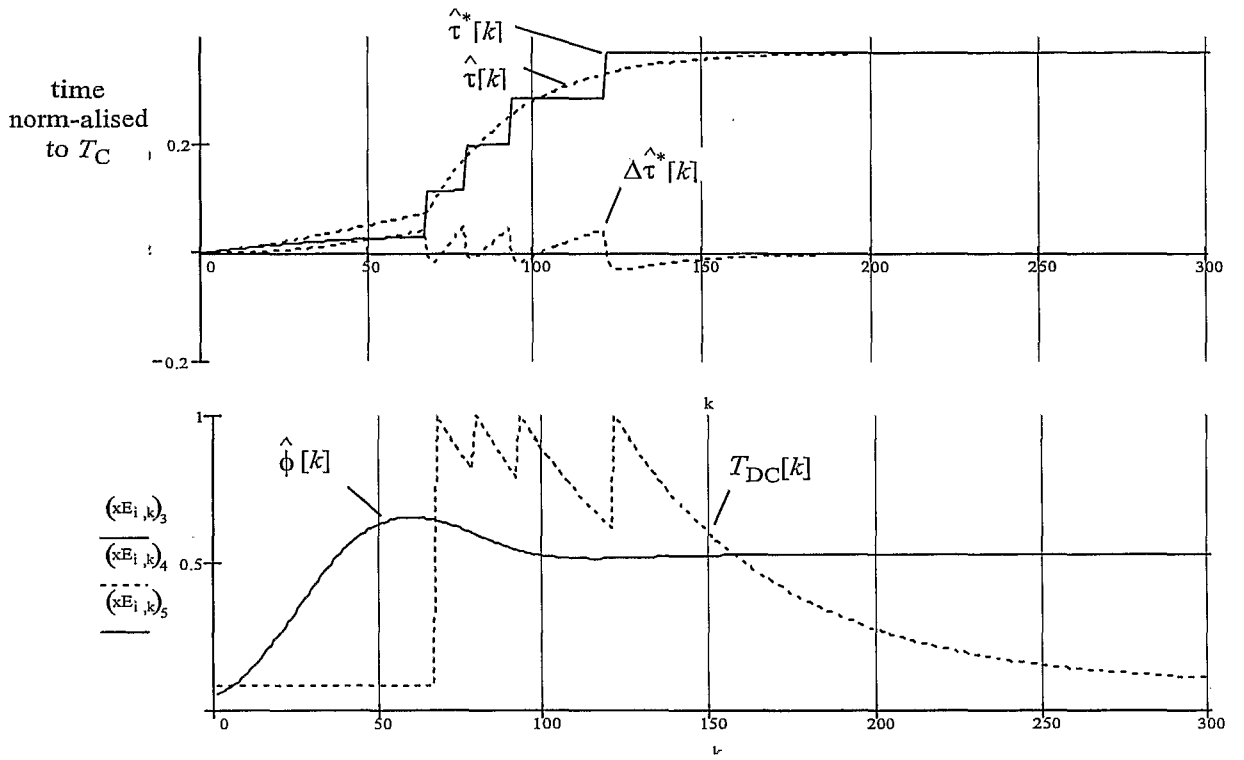


fig 16

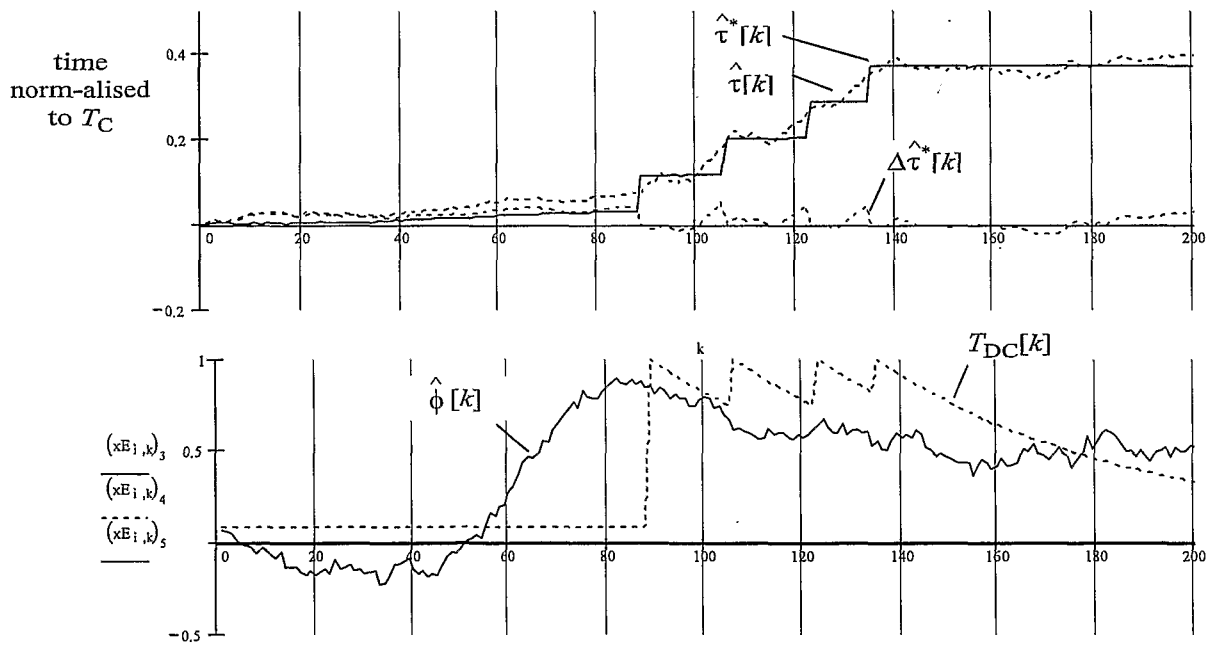


fig 17

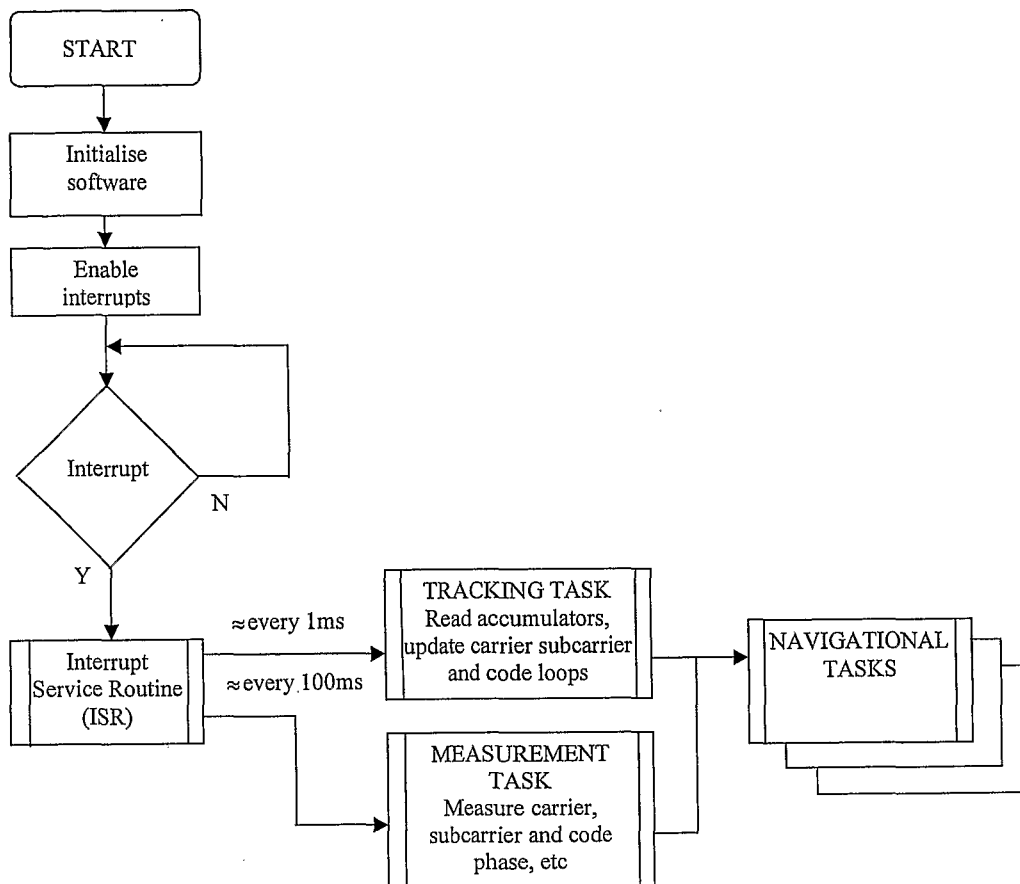


fig 18

INTERNATIONAL SEARCH REPORT

International application No
PCT/GB2007/003050

A. CLASSIFICATION OF SUBJECT MATTER

INV. G01S1/00

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

G01S

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, WPI Data, INSPEC

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	EP 1 598 677 A (UNIV TECHNOLOGIES INT [CA]) 23 November 2005 (2005-11-23) paragraphs [0034] - [0040], [0076] - [0088]; figures 5,6,7A,7B	1,5-12, 14,15
X	FABIO DOVIS, PAOLO MULASSAIO, LETIZIA LO PRESTI: "A Novel Algorithm for the Code Tracking of BOC(n,n) Modulated Signals" ION GNSS 18TH INTERNATIONAL TECHNICAL MEETING, 15 September 2005 (2005-09-15), pages 152-155, XP002458766 Long Beach CA Section 3 page 154; figure 5	1

☒ Further documents are listed in the continuation of Box C.

☒ See patent family annex.

* Special categories of cited documents :

- *A* document defining the general state of the art which is not considered to be of particular relevance
- *E* earlier document but published on or after the international filing date
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- *O* document referring to an oral disclosure, use, exhibition or other means
- *P* document published prior to the international filing date but later than the priority date claimed

- *T* later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
- *X* document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
- *Y* document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.
- *Z* document member of the same patent family

Date of the actual completion of the international search

15 November 2007

Date of mailing of the international search report

27/11/2007

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INTERNATIONAL SEARCH REPORT

International application No

PCT/GB2007/003050

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	LIN V S ET AL: "Study of the Impact of False Lock Points in Subcarrier Modulated Ranging Signals and Recommended Mitigation Approaches" ION ANNUAL MEETING, XX, XX, 23 June 2003 (2003-06-23), pages 156-165, XP002338822 the whole document -----	1-15
A	WARD P W: "A DESIGN TECHNIQUE TO REMOVE THE CORRELATION AMBIGUITY IN BINARY OFFSET CARRIER (BOC) SPREAD SPECTRUM SIGNALS" PROCEEDINGS OF THE ION NATIONAL TECHNICAL MEETING, THE INSTITUTE OF NAVIGATION, US, 26 January 2004 (2004-01-26), pages 886-896, XP001207302 the whole document -----	1-15

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/GB2007/003050

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
EP 1598677	A	23-11-2005	AT
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