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DESCRIPTION

TECHNICAL FIELD

[0001] Aspects of the present invention relate to an apparatus and method for determining icing risk in wind turbines, and more particularly to systems and methods for triggering the activation of de-icing systems for wind turbines in dependence on the determined icing risk.

BACKGROUND

[0002] Wind turbines that are to be installed in cold climates make up a large proportion of the global wind turbine market, as such climates tend to have high wind resources, particularly during the winter. However, due to the low temperatures experienced in these locations during the winter, the likelihood of ice build-up on the wind turbine blades is high. The build-up of ice on the turbine blades adversely affects the power production efficiency and forces on the rotor.

[0003] Various types of de-icing (and anti-icing) systems and methods have already been implemented in cold climate wind turbines. For example, a controlled blade acceleration/deceleration to shake off the ice is sometimes utilised. De-icing systems may additionally or alternatively involve the incorporation of built-in electric heating elements within the blades, or the provision of a heating unit in the hub which distributes hot air throughout the generally hollow blade interiors.

[0004] In such active solutions, it is important to ensure that the de-icing systems are triggered at an appropriate point in time, in order to make the most efficient use of them. Many of the currently-implemented de-icing systems comprise trigger mechanisms that are activated based on the degradation of the power curve, and specifically the de-icing system is triggered or activated when the measured output power reaches a particular threshold value.

[0005] These triggering or activation mechanisms typically require a substantial build-up of ice before the decrease in output power of the wind turbine is sufficient to satisfy the necessary threshold conditions, since a large amount of ice is required to have formed in order to cause the necessary drop in output power. However, in particularly cold conditions, even after the de-icing system is activated, the subsequent removal of ice may not occur at a sufficiently fast rate to counter the re-formation of the ice on the blades. One known system EP1906192 A2 discloses determining the risk of icing for the blades of a wind turbine based on environmental conditions.

[0006] It is against this background that the embodiments of the invention have been devised.

SUMMARY OF THE INVENTION

[0007] According to an embodiment of the present invention there is provided an apparatus for controlling a sub-system of a wind turbine. The apparatus comprises a cooling system comprising first and second heat exchangers, and a fluid circuit arranged to enable a coolant to flow between the first and second heat exchangers; and a processor. The processor is configured to: monitor one or more operational parameters of the cooling system; determine an icing risk based on the one or more operational parameters; and generate a control signal for output to the wind turbine sub-system in dependence on the determined icing risk.

[0008] Advantageously, the above configuration provides the ability to ascertain the icing risk of wind turbine blades using existing equipment that is already installed on the wind turbines, namely the cooling system of the wind turbine. This allows the associated method to be applied to all existing wind turbines without the need to retrofit any additional sensors. Such methods are therefore easier and cheaper to implement on a large scale.

[0009] Optionally, the first heat exchanger may be arranged to absorb thermal energy from an internal environment of the wind turbine. Preferably, the internal environment of the wind turbine corresponds to the internal environment of the wind turbine nacelle. Making use of the existing cooling system that has been installed in the wind turbine advantageously simplifies the implementation of the apparatus and associated method in existing wind turbines.

[0010] The second heat exchanger may be arranged to transfer thermal energy to an ambient environment external to the wind turbine. Optionally, at least a portion of the second heat exchanger is located on the nacelle of the wind turbine. An advantage of monitoring parameters of the portion of the heat exchanger located external to the wind turbine (e.g. on top of the nacelle) is that these parameters will accurately reflect the current conditions of the ambient environment around the wind turbine, without requiring any additional sensors to be retrofit.

[0011] The icing risk may be determined by comparing one of the operational parameters with a measured parameter of the external environment of the wind turbine. Such a configuration is advantageous as it makes use of the systems that are already installed on the wind turbine to determine the icing risk.

[0012] In some cases, the icing risk may be determined by comparing the one or more operational parameters to a pre-defined threshold value. Advantageously, this allows the determination of icing risk to be carried out in an automated manner, based on a threshold value that was defined based on prior knowledge and analysis.

[0013] One of the operational parameters to be monitored may correspond to an outlet temperature of the second heat exchanger. Optionally, the outlet temperature of the second heat exchanger is compared with an ambient temperature of the wind turbine external environment in order to determine the icing risk.

[0014] The outlet temperature (and its value relative to the ambient temperature of the external environment) indicates the efficiency of the wind turbine cooling system. The cooling system efficiency has a quantifiable relationship or correlation with the liquid water content of the air, and the liquid water content in turn is a key factor in the icing risk of the wind turbine blades - generally, the higher the liquid water content, the greater the icing risk. Monitoring the outlet temperature of the cooling system heat exchanger therefore allows easy inference of the liquid water content and the associated icing risk.

[0015] Preferably, the processor may be further configured to generate the control signal if a difference between the outlet temperature of the second heat exchanger and the ambient temperature of the wind turbine external environment is lower than a pre-defined threshold value. The difference between the two temperature values is indicative of the level of increase in the cooling system efficiency, and reflects an increased rate of evaporation of water off the heat exchanger due to an increased liquid water content in the surrounding air. The lower the difference between the two temperatures (i.e. the lower the outlet temperature), the greater the liquid water content and hence the greater the icing risk of the wind turbine blades. Setting a predefined threshold value for the temperature difference therefore allows the system to automatically ascertain whether the risk of icing is sufficiently high to affect power production.

[0016] Additionally or alternatively, the processor is further configured to generate the control signal if the outlet temperature of the second heat exchanger is lower than a pre-defined threshold value. Advantageously, if used on its own, such a configuration means that a determination of icing risk is only dependent on cooling system parameters, and therefore fewer sensors are required to monitor the surrounding conditions. If used in combination with the difference between ambient and outlet temperatures, this configuration provides a cross-check of the result determined solely from the cooling system, with the result obtained using current external conditions.

[0017] The pre-defined threshold value may be determined based on a model of how a liquid water content of the external environment of the wind turbine affects efficiency of the cooling system. Utilising a theoretically determined correlation between liquid water content and cooling system efficiency obviates the need for dedicated liquid water content sensors to be retrofit to existing wind turbines.

[0018] The wind turbine sub-system may correspond to a de-icing system, or an anti-icing system, and the processor may be further configured to generate the control signal to activate the de-icing or anti-icing system. Advantageously, this configuration provides an automated mechanism for sensing a high icing risk, and for taking action to counter the icing risk so as to increase (or prevent further decrease of) wind turbine power production.

[0019] The apparatus may further comprise a temperature sensor arranged to measure an ambient temperature of the wind turbine external environment. The processor may be configured to determine the icing risk and to generate the control signal based on the

measured ambient temperature as well as the operational parameters of the cooling system. Advantageously, this configuration ensures that the sub-system of the wind turbine (for example, the de-icing system) is only activated when the combination of a low ambient temperature and high liquid water content indicates a high icing risk, as there may be some situations in which a high liquid water content is present but the temperature is also sufficiently high as to prevent any ice from forming on the wind turbine blades.

[0020] According to another embodiment of the present invention there is provided an apparatus for controlling a sub-system of a wind turbine. The apparatus comprises: a cooling system comprising first and second heat exchangers, and a fluid circuit arranged to enable a coolant to flow between the first and second heat exchangers; and a processor. The processor is configured to: monitor one or more operational parameters of the cooling system; estimate a liquid water content of an external environment of the wind turbine based on the operational parameters; measure an ambient temperature of the external environment; determine an icing risk of the wind turbine based on the liquid water content and the ambient temperature; and generate a control signal for output to the wind turbine sub-system in dependence on the determined icing risk.

[0021] According to another embodiment of the present invention there is provided a wind turbine comprising the apparatus as described herein for controlling a wind turbine sub-system.

[0022] According to another embodiment of the present invention there is provided a method for controlling a sub-system of a wind turbine. The method is implemented using a cooling system comprising first and second heat exchangers, and a fluid circuit arranged to enable a coolant to flow between the first and second heat exchangers. The method comprises: monitoring one or more operational parameters of the cooling system; determining an icing risk based on the one or more operational parameters; and generating a control signal for output to the wind turbine sub-system in dependence on the determined icing risk.

[0023] Within the scope of this application it is expressly intended that the various aspects, embodiments, examples and alternatives set out in the preceding paragraphs, in the claims and/or in the following description and drawings, and in particular the individual features thereof, may be taken independently or in any combination. That is, all embodiments and/or features of any embodiment can be combined in any way and/or combination, unless such features are incompatible. The applicant reserves the right to change any originally filed claim or file any new claim accordingly, including the right to amend any originally filed claim to depend from and/or incorporate any feature of any other claim although not originally claimed in that manner.

BRIEF DESCRIPTION OF THE DRAWINGS

[0024] One or more embodiments of the invention will now be described, by way of example

only, with reference to the accompanying drawings, in which:

Figure 1 shows a simplified diagram of a wind turbine in which embodiments of the present invention may be implemented;

Figure 2 shows a schematic diagram of a typical cooling system implemented in a nacelle of the wind turbine of Figure 1;

Figure 3 shows a schematic block diagram of a control system, for determining an icing risk and for controlling a sub-system of a wind turbine, according to an embodiment of the present invention;

Figure 4 is a flow chart showing an overview of a method for determining an icing risk and for controlling a sub-system of a wind turbine, according to an embodiment of the present invention;

Figure 5 is a flow chart showing an overview of a method utilised to determine reference values for use in controlling a sub-system of a wind turbine, according to an embodiment of the present invention.

DETAILED DESCRIPTION

[0025] A specific embodiment of the invention will now be described in which numerous specific features will be discussed in detail in order to provide a thorough understanding of the inventive concept as defined in the claims. However, it will be apparent to the skilled person that the invention may be put in to effect without the specific details and that in some instances, well known methods, techniques and structures have not been described in detail in order not to obscure the invention unnecessarily.

[0026] In order to place the embodiments of the invention in a suitable context, reference will firstly be made to **Figure 1**, which illustrates schematically a portion of a typical wind turbine in which an apparatus for determining icing risk and for controlling a sub-system of the wind turbine according to an embodiment of the present invention may be implemented.

[0027] The wind turbine 1 comprises a tower 2, a nacelle 4 rotatably coupled to the top of the tower 2, a rotating hub 6 mounted to the nacelle 4 and a plurality of wind turbine rotor blades 8 coupled to the hub 6.. Although not shown in these figures, it will be understood that the wind turbine further comprises a de-icing system and/or an anti-icing system which is arranged to remove ice from the blades 8, and to prevent the substantial build-up of ice on the wind turbine blades. Although de-icing and anti-icing systems do differ in terms of their functionality and operational parameters, such systems will simply be collectively referred to throughout this specification as 'de-icing systems' for simplicity. An example of such de-icing systems may be found in WO 2013/107457 (to the present applicant) which circulates heated air around the

interior of the blades 8 to remove ice that has formed on the blades.

[0028] The nacelle 4 houses all of the generating components of the wind turbine, including the generator, gearbox, drive train and brake assembly, as well as convertor equipment for converting the mechanical energy of the wind into electrical energy for provision to the grid. The nacelle 4 also necessarily contains a main shaft housing (not shown in Figure 1), which houses a main rotor shaft that is connected at a forward end to the hub 8 and rotor blades 10, and at a rear end to the generating components.

[0029] The nacelle 4 also contains a cooling system 10, a portion of which is located on the top of the nacelle 4 and is visible in Figure 1 which is arranged to cool the components housed within the nacelle 4, for example the generator, gearbox and other drive train components. Typically, the cooling systems utilised in wind turbine nacelles are liquid cooling systems, and therefore the subsequent methods focus on the features of such systems. However, it will be understood that alternative systems such as evaporative cooling systems may be implemented instead, and the methods described herein may equally be applied to such alternative cooling systems. The liquid cooling system that will be described hereafter is one in which the coolant remains a liquid throughout the system, and merely varies in temperature. However, it will be appreciated that other variants of liquid cooling system could also be suitable for use in a wind turbine - for example, a two-phase liquid cooling system in which the coolant transitions between the liquid and vapour phases.

[0030] Figure 2 shows a typical liquid cooling system 10 that is utilised in wind turbines. As the operation of such liquid cooling systems is generally well known to the person skilled in the art, only a brief description of how such a system works will be provided here to place the embodiments of the invention in context.

[0031] In general, the purpose of the liquid cooling system is to transfer thermal energy from an internal environment of the wind turbine, out to the external environment of the wind turbine. The cooling system comprises first and second heat exchangers, connected by a fluid circuit such that coolant is able to flow between the two heat exchangers. The first heat exchanger is usually located within the wind turbine (for example, within the nacelle 4) and is arranged to absorb thermal energy from the internal environment of the wind turbine, and from specific heat-generating components within the nacelle. The second heat exchanger is usually located such that a portion of it is exposed to the external environment, so as to enable the transfer of thermal energy out to the external environment of the wind turbine. In some cases, the cooling system also comprises one or more monitoring components arranged to monitor the operational parameters of the cooling system, and thereby ensure that the cooling system is functioning as intended.

[0032] A specific example of a liquid cooling system implemented in a wind turbine will now be described in greater detail.

[0033] The liquid cooling system 10 comprises a cooler 12 (i.e. the first heat exchanger) in

thermal contact with a heat source 14 that is to be cooled (for example, the generator or various other electronic components located within the nacelle). In some cases, the cooler 12 may take the form of a cold plate or cooling coils that are placed in direct or close proximity to the heat source 14, such that the coolant entering the cooler 12 absorbs thermal energy from the heat source 14. The liquid cooling system 10 also comprises a condenser 16 (i.e. the second heat exchanger) that receives heated coolant from the cooler 12 and enables the thermal energy from the coolant to be dissipated. The 'condenser' is generally referred to as such in those embodiments where the coolant is heated to a sufficient temperature to enable it to be vaporized, as the dissipation of thermal energy from the coolant by the condenser results in the recondensation of the hot vaporized coolant into cooler liquid form. However, for simplicity and to avoid confusion between the two heat exchangers in the cooling system, the term 'condenser' will be used hereafter to refer generically to the second heat exchanger which is arranged to dissipate thermal energy to the external environment. The liquid cooling system 10 also comprises an accumulator 18 or coolant storage component arranged to receive and store cold liquid coolant from the heat exchanger. A pipe network 20 provides a fluid circuit and fluid connections between the various components, and a circulation pump 22 is also provided to drive circulation of coolant around the liquid cooling system 10 via the pipe network 20.

[0034] In use, as previously mentioned, the first heat exchanger - the cooler 12 - is located within the nacelle 4 and in close proximity to the heat source 14 that is to be cooled. For example, as previously discussed, the cooler 12 may be placed directly under or next to the generator component. Alternatively, the cooler 12 may take the form of an air conditioning unit that blows cool air through the nacelle and across the hot components. The cooler 12 may also take the form of cooling fins projecting from various components to radiate thermal energy away from those components. In order to function efficiently, the second heat exchanger - the condenser 16 - should be exposed to the outside air, and may be located on the roof of the nacelle 4 for example. Cold coolant is pumped from the accumulator 18 (where it is stored) to the cooler; the thermal energy from the heat source 14 is absorbed by the cold coolant which heats up. The hot coolant flows away from the cooler 12, carrying the thermal energy away, and enters the condenser 16 where the thermal energy is dissipated. The now cold coolant is then returned to the accumulator 18 to begin the cycle again.

[0035] Figure 3 shows an apparatus for determining an icing risk of a wind turbine, and also places the apparatus in its intended context for controlling a sub-system (such as the de-icing system) of the wind turbine according to an embodiment of the present invention.

[0036] The apparatus 30 comprises a control processor 32 arranged and configured to carry out various comparison and analysis steps in order to determine an icing risk of the wind turbine, and to ascertain whether the de-icing system of the wind turbine should be activated. The control processor 32 comprises an input 34 arranged to receive information that will be used during the subsequent analyses, and an output 36 arranged to provide a control signal to the de-icing system in dependence on the results of the analyses. In the present embodiment, the control processor 32 is arranged to receive information directly relating to properties of the

external environment around the wind turbine, and in particular measurements of the meteorological conditions, for example the ambient air temperature around the wind turbine (received for example from an external temperature sensor 38), as well as the wind speed (received for example from an external wind speed sensor 40 or anemometer).

[0037] In addition, the control processor 32 is also arranged to receive information relating to properties of certain internal systems within the wind turbine, which properties indirectly reflect certain external environmental conditions. In particular, the control processor 32 is arranged to receive information relating to the efficiency of the condenser 16 provided as part of the wind turbine liquid cooling system 10; specifically, the control processor 32 is arranged to receive measurements of an outlet temperature of the condenser 16, or the temperature difference across the condenser 16, from one or more temperature sensors 42 associated with the condenser 16.

[0038] The control apparatus 30 also comprises a data store 44, in operative communication with the control processor 32, which stores a plurality of rules 46 specifying relationships between the various pieces of received information, and specifically between the various measureable properties of the external and internal environments of the wind turbine. These rules 46 are referred to by the control processor 32 when carrying out the analyses to determine whether the de-icing system should be activated. The rules 46 may require the comparison of received or measured data with pre-determined values 48 which are also stored in the data store 44. The control processor 32 is arranged to carry out its analyses of the received data, based on the rules 46 and values 48 stored in the associated data store 44, to determine the icing risk of the wind turbine. If the icing risk (i.e. the risk of ice formation and build-up on the wind turbine blades 8) is significant, the control processor 32 is configured to output a control signal to activate the de-icing system (for example, via a de-icing system controller component 50).

[0039] It will be appreciated that whilst the above functionality has been described with respect to separate functional blocks, this is merely for clarity purposes and the functionality could instead be incorporated into the de-icing controller.

[0040] **Figure 4** shows a flow chart illustrating a method for determining an icing risk of a wind turbine, and for subsequently controlling activation of the wind turbine de-icing system according to an embodiment of the present invention. In particular, the method involves an analysis of the meteorological conditions around the wind turbine in order to ascertain the risk of ice forming on the wind turbine blades 8 - if it is deemed that there is a high risk of ice formation, the de-icing system will be activated.

[0041] In summary, the method involves the control processor 32 receiving measurements of operational parameters of the nacelle cooling system 10, determining an icing risk based on these received operational parameters, and subsequently generating a control signal for output to the de-icing system if the icing risk is determined to be sufficient to warrant activation of the de-icing system.

[0042] To begin with, the theory underpinning this method needs to be considered before the method itself is described in detail.

[0043] The meteorological conditions that give a good indication of the risk of ice formation are the ambient temperature and the liquid water content of the air - a combination of low ambient temperature and high liquid water content of the surrounding air will result in a high risk of ice formation. At present, many wind turbine designs already incorporate sensors that measure the ambient air temperature; however, the majority of wind turbines are not fitted with standard sensors (or even any sensors at all) for measuring the liquid water content of the surrounding air as there is little or no need for such measurements during the majority of normal operations. Therefore, for all existing cold climate wind turbines to be retrofitted with the same or standard sensors designed with the express purpose of measuring the liquid water content of the surrounding air would be extremely costly and difficult to achieve.

[0044] However, the present applicant has appreciated that rather than retrofitting dedicated liquid water content sensors to existing wind turbine designs, various properties of the nacelle cooling system may be utilised instead in order to estimate the liquid water content of the surrounding (outside) air. In this approach, no dedicated additional components would need to be utilised; instead, the provision of some simple updates to the processing systems and methods that are currently in place in wind turbines is all that would be required.

[0045] Specifically, the present applicant has appreciated that there is a correlation between the efficiency of the condenser 16 (i.e. the heat flow out of the condenser 16) in the nacelle cooling system, and the risk of ice formation on the wind turbine blades 8. In particular, the heat flow out of the condenser 16 is highly dependent on the same two main environmental factors as the risk of ice formation - namely the ambient temperature and the liquid water content of the surrounding air. Other factors, such as the humidity (otherwise known as the water vapour content) of the surrounding air, have less of an effect on the efficiency of the condenser 16, and can be largely ignored in the subsequent calculations.

[0046] When there is sufficient liquid water content in the surrounding air, this water may be deposited onto the condenser 16, and in particular, on those portions of the condenser 16 that are located on the nacelle roof and are therefore exposed to the surrounding environment. As the condenser 16 absorbs thermal energy from the coolant passing through it, and radiates this thermal energy to the surrounding environment, the liquid water that is deposited on the condenser 16 is able to absorb this thermal energy and evaporate back into the air. This causes evaporative cooling of the condenser 16, and increases the efficiency of the condenser 16.

[0047] As a result of this increased efficiency, the coolant passing through the condenser 16 is cooled to a greater degree and emerges from the condenser 16 at a much lower temperature than would normally be observed. The temperature at the outlet of the condenser 16 is therefore decreased when the liquid water content of the outside air is higher.

[0048] A normally efficient condenser 16 will typically have an outlet temperature that is up to a few degrees higher than the ambient temperature of the surrounding air. However, where there is an increase in the efficiency of the condenser 16, and hence a corresponding decrease in the outlet coolant temperature, the difference between the outlet temperature and the ambient air temperature decreases. In other words, the gap between the two temperatures decreases when there is an increase in the liquid water content in the surrounding air. In some cases, the evaporative cooling effect is even sufficient to cause the outlet temperature to drop below the ambient temperature. The detection of such changes using sensors that are already incorporated within the wind turbine design lies at the heart of the present invention.

[0049] Furthermore, it will be appreciated that the methods proposed herein may be utilised with many different types of cooling system, as long as it is possible to measure the efficiency of the cooling system and compare this measured value to the expected efficiency of the cooling system, with and without liquid water content in the air.

[0050] Returning now to a description of **Figure 4**, the method 100 of the present invention begins at Step 105 with the control apparatus 30 receiving measurements of the outlet temperature of the nacelle cooling system condenser 16, as well as receiving at Step 110 measurements of the ambient air temperature around the wind turbine. The control processor 32 is configured to calculate in Step 115 the difference between the two measured temperatures, and to subsequently compare in Step 120 this difference to a pre-defined threshold value. If the difference between the two temperatures is less than this pre-defined threshold value, then this is deemed to be an indication of sufficiently high liquid water content in the surrounding air to indicate a high ice-formation risk. In the event that such a risk is deemed to exist, the control processor 32 is subsequently configured to output at Step 125 a control signal to the controller 50 of the de-icing system in order to trigger or activate the de-icing system.

[0051] Various other criteria may be used in combination with, or instead of, these threshold values to trigger the activation of the de-icing system. For example, if the absolute ambient temperature is also determined to be lower than a particular pre-defined threshold value, the combination of these two criteria being fulfilled may also be used to trigger activation of the de-icing system. Furthermore, it will also be appreciated that it is not strictly necessary for the pre-defined threshold value to correspond to a threshold temperature difference. Instead, the threshold value could simply correspond to a pre-defined minimum outlet temperature, below which it is determined that there is a significant risk of ice formation. It will be appreciated that the exact values, and the specific criteria (or combination of criteria) used to assess the risk of ice formation may be tailored to suit the meteorological conditions and wind turbine requirements in specific geographical locations.

[0052] A description of how the pre-defined threshold value used to trigger activation of the de-icing system may be obtained will now be provided with reference to **Figure 5**.

[0053] To begin with, in method 200, a temperature difference across the condenser 16 is

obtained in Step 205 based on a measurement of the inlet and outlet temperatures (i.e. the temperature difference between the incoming and outgoing coolant). Next, the mass flow rate through the condenser 16 needs to be determined in Step 210. This may be done directly using a flow rate sensor associated with the condenser 16 itself, or it may be done indirectly using a sensor or other measurement means to monitor the activity of the circulation pump 22.

[0054] The expected heat flow out of the condenser 16 can subsequently be determined in Step 215 by multiplying the obtained flow rate through the condenser 16 with the obtained temperature difference between the inlet and outlet of the condenser 16. Given the correlation between liquid water content and efficiency of the condenser 16, the liquid water content of the surrounding air can then be calculated in Step 220 for a given ambient temperature. A brief discussion of the theory underpinning this calculation, as well as a couple of different methods by which this calculation could be carried out, will now be provided.

[0055] In summary, computing or modelling the expected efficiency of the cooling system (given a set of known/measured environmental conditions), and comparing this expected efficiency to the measured efficiency, yields a residual value (i.e. a difference) which is assumed to result entirely from liquid water content in the surrounding air. Based on this assumption, an estimate of the liquid water content can therefore be computed.

[0056] A first method that may be used to estimate the expected efficiency of the system is referred to as a 'first principle approach' and is based on the basic engineering knowledge and principles of the cooling system 10. During the turbine design phase the efficiency of the condenser 16 (and hence of the cooling system 10 as a whole) has been calculated or tabularised using the engineering models made to scale the cooling system 10. It is therefore expected that a function expressing the expected heat flow Q_{model} through the condenser 16, which is dependent on ambient temperature (T), fluid flow (F) and wind speed (V), would be available. Such a function would take the following form: $Q_{\text{model}}(F, T, V)$.

[0057] As previously mentioned, the actual or measured heat flow is calculated based on the difference between the inlet (T_{in}) and outlet (T_{out}) temperatures of the condenser 16, as well as the volume flow of coolant (F) through the condenser 16. A function expressing the measured heat flow Q_{meas} through the condenser 16 could therefore be computed as follows: $Q_{\text{meas}} = (T_{\text{in}} - T_{\text{out}}) FC$, where C is a constant that is dependent on the density and the heat capacity of the cooling fluid flowing through the cooling system 10.

[0058] By comparing the measured heat flow to the actual heat flow, a residual or difference can be computed: $Q_{\text{res}} = Q_{\text{meas}} - Q_{\text{model}}$. Assuming any discrepancy between the models is due to liquid water evaporation, it then follows that the liquid water being evaporated per second M_{LW} (i.e. the rate of liquid water evaporation off the exposed surface of the condenser 16) can be calculated as $M_{\text{LW}} = Q_{\text{res}}/L_{\text{water}}$, where L_{water} is the specific latent heat for water at a given ambient temperature.

[0059] Based on the dimensions and design of the condenser 16, it is then possible to relate the amount of water being evaporated from the surface of the condenser 16 with the liquid water content in the air. For example, this relation could be determined experimentally in a test stand. It is further noted that the latent heat of evaporating water (expressed in units of Joules per gram of water) can be approximated by a polynomial in temperature: $L(T) = a - bT + cT^2 - dT^3$ J/g, where T is the ambient temperature. That means that the efficiency of the cooling will rise with $L(T)$ J/s per gram of water evaporated per second.

[0060] An alternative method of modelling the expected efficiency of the cooling system 10, and hence the liquid water content in the air, is referred to as the 'data driven method'. This method assumes no prior knowledge of the physical relations between cooling efficiency and the liquid water content of the air. Instead, a model is created by e.g. a machine learning technique where the dedicated liquid water content measurement on the wind turbine 1 is used as a reference and the model is then fitted until it can accurately predict the directly measured liquid water content. An example of such techniques is 'Deep Learning', which makes use of neural networks to model the physics of heat flow.

[0061] Regardless of the method by which it is obtained, the calculated liquid water content value may be stored for subsequent use (for example in the data store 44), or it may be transmitted to another sub-system, either periodically or on demand, for use in decisioning processes that are carried out by that sub-system.

[0062] Subsequently, a risk assessment step 225 may be carried out to ascertain the risk of ice formation on the wind turbine blades 8 for the calculated liquid water content and at the given ambient temperature. For example, the percentage likelihood that substantial ice formation will occur can be ascertained. This could be carried out in a laboratory environment (for example, in a testbed under carefully controlled conditions), using simulations, or even simply by analysing existing data. Alternatively, state of the art ice detection systems, which comprise cameras or other image sensors that are coupled with dedicated liquid water content sensors, could be used to carry out such investigations on existing wind turbines, if these detection systems are already installed or are retrofit. These investigations would provide initial ice formation data which could form the basis for some initial thresholds to be defined. These initial thresholds would subsequently be adjusted based on learning algorithms after a sufficient number of wind turbines with this liquid water content detection apparatus have been investigated. A threshold percentage likelihood may therefore be determined in Step 230 that would necessitate activation of the de-icing system. This threshold percentage likelihood will correspond to a particular threshold outlet temperature value, below which the risk of ice formation is sufficiently high so as to warrant activation of the de-icing system.

[0063] A different threshold value may be calculated for each set of external and internal environmental conditions - for example, certain combinations of values (or ranges of values) of wind speed and ambient air temperature, as well as coolant flow rate, will correspond to particular threshold values. These values are stored by the control processor in the associated data store and are retrieved when the method of Figure 4 is carried out.

[0064] Many modifications may be made to the above examples without departing from the scope of the present invention as defined in the accompanying claims.

REFERENCES CITED IN THE DESCRIPTION

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Patent documents cited in the description

- EP1906192A2 [0005]
- WO2013107457A [0027]

Patentkrav

1. Apparat til styring af et subsystem af en vindmølle, hvilket apparat omfatter:

et kølesystem omfattende første og anden varmevekslere (12,16) og et
fluidkredsløb (10) indrettet til at muliggøre et kølemiddel at strømme
5 mellem de første og anden varmevekslere; og **kendetegnet ved**
en processor (32) konfigureret til:

at overvåge et eller flere driftsparametre af kølesystemet;
at bestemme en isdannelsesrisiko baseret på det ene eller flere
driftsparametre; og
10 at generere et styresignal for output til vindmøllesubsystemet (50)
afhængigt af den bestemte isdannelsesrisiko.

2. Apparatet ifølge krav 1, hvor den første varmeveksler er indrettet til at
absorbere termisk energi fra et indre miljø af vindmøllen.

15

3. Apparatet ifølge krav 2, hvor det indre miljø af vindmøllen svarer til det indre
miljø af vindmøllenacellen.

4. Apparatet ifølge et hvilket som helst foregående krav, hvor den anden
20 varmeveksler er indrettet til at overføre termisk energi til et omgivende miljø
uden for vindmøllen.

5. Apparatet ifølge krav 5, hvor mindst en del af den anden varmeveksler er
lokaliseret på nacellen af vindmøllen.

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6. Apparatet ifølge et hvilket som helst foregående krav, hvor processoren er
yderligere konfigureret til at bestemme isdannelsesrisikoen ved at sammenligne et
af driftsparametrene med et målt parameter af det udvendige miljø af vindmøllen.

7. Apparatet ifølge et hvilket som helst foregående krav, hvor processoren er yderligere konfigureret til at bestemme en isdannelsesrisiko ved at sammenligne det ene eller flere driftsparametre med en foruddefineret tærskelværdi.

5 **8.** Apparatet ifølge et hvilket som helst foregående krav, hvor et af driftsparametrene, som skal overvåges, svarer til en udløbstemperatur af den anden varmeveksler.

9. Apparatet ifølge krav 8, hvor processoren er yderligere konfigureret til at
10 sammenligne udløbstemperaturen af den anden varmeveksler med en omgivende temperatur af det udvendige miljø af vindmøllen for således at bestemme isdannelsesrisikoen.

10. Apparatet ifølge krav 9, hvor processoren er yderligere konfigureret til at
15 generere styresignalet, hvis en forskel mellem udløbstemperaturen af den anden varmeveksler og den omgivende temperatur af det udvendige miljø af vindmøllen er lavere end en foruddefineret tærskelværdi.

11. Apparatet ifølge et hvilket som helst af kravene 8 til 10, hvor processoren er
20 yderligere konfigureret til at generere styresignalet, hvis udløbstemperaturen af den anden varmeveksler er lavere end en foruddefineret tærskelværdi.

12. Apparatet ifølge krav 10 eller krav 11, hvor den foruddefinerede tærskelværdi er bestemt baseret på en model af hvordan et flydende vandindhold af det
25 udvendige miljø af vindmøllen påvirker effektiviteten af kølesystemet.

13. Apparatet ifølge et hvilket som helst foregående krav, hvor vindmøllesubsystemet svarer til et afisningssystem eller et antiisningssystem, og processoren er yderligere konfigureret til at generere styresignalet for at aktivere
30 afisningssystemet eller anti-isningssystemet.

14. Apparatet ifølge et hvilket som helst foregående krav yderligere omfattende en temperatursensor indrettet til at måle en omgivende temperatur af det udvendige miljø af vindmøllen, og hvor processoren er konfigureret til at bestemme isdannelsesrisikoen og til at generere styresignalet baseret på den målte omgivende temperatur samt driftsparametrene af kølesystemet.

15. Apparat til styring af et subsystem af en vindmølle, hvilket apparat omfatter:
et kølesystem omfattende første og anden varmevekslere (12,16) og et fluidkredsløb (10) indrettet til at muliggøre et kølemiddel at strømme mellem de første og anden varmevekslere; og **kendetegnet ved**
en processor (32) konfigureret til:

at overvåge et eller flere driftsparametre af kølesystemet;
at estimere et flydende vandindhold af et udvendigt miljø af vindmøllen baseret på driftsparametrene;
at måle en omgivende temperatur af det udvendige miljø;
at bestemme en isdannelsesrisiko af vindmøllen baseret på det estimerede flydende vandindhold og den målte omgivende temperatur; og
at generere et styresignal for output til vindmøllesubsystemet (50) afhængigt af den bestemte isdannelsesrisiko.

16. Vindmølle omfattende et apparat til styring af et vindmøllesubsystem ifølge et hvilket som helst foregående krav.

17. Fremgangsmåde til styring af et subsystem af en vindmølle, hvilken fremgangsmåde implementeres under anvendelse af et kølesystem omfattende første og anden varmevekslere (12,16) og et fluidkredsløb (10) indrettet til at muliggøre et kølemiddel at strømme mellem de første og anden varmevekslere, hvilken fremgangsmåde omfatter:

overvågning af et eller flere driftsparametre af kølesystemet;

4

bestemmelse af en isdannelsesrisiko baseret på det ene eller flere driftsparametre; og

generering af et styresignal for output til vindmøllesubsystemet (50) afhængigt af den bestemte isdannelsesrisiko.

5

DRAWINGS

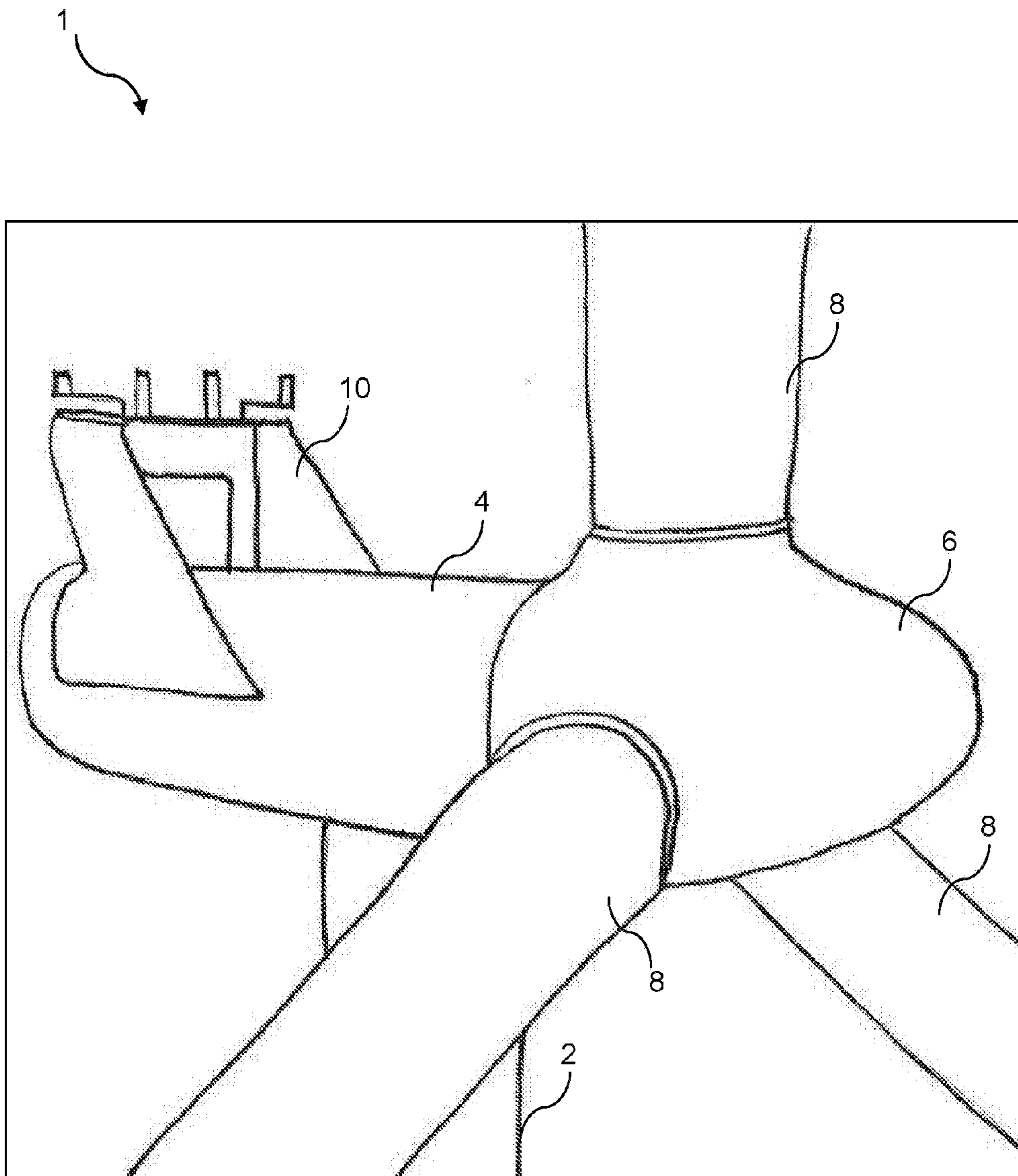


Figure 1

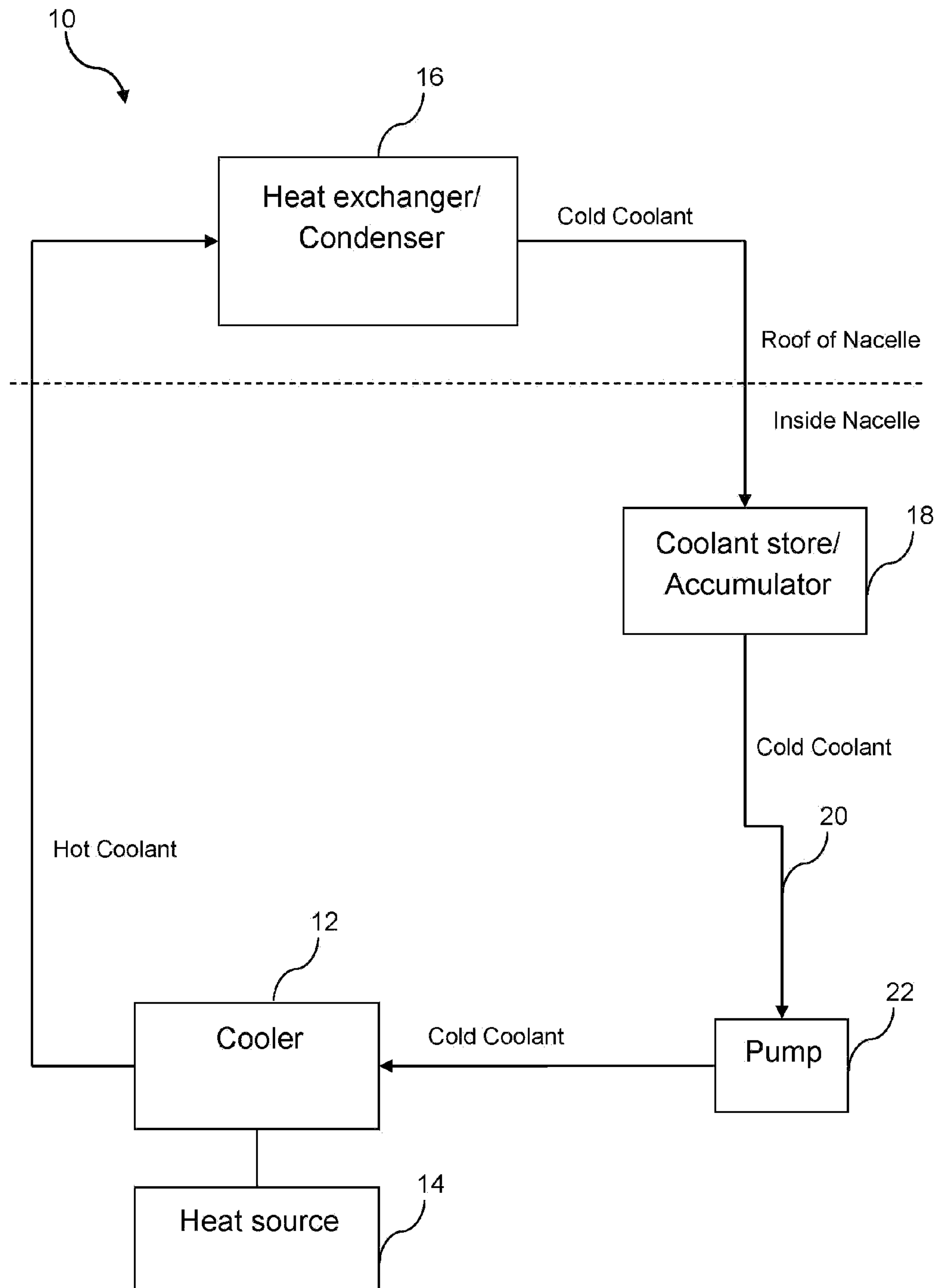


Figure 2

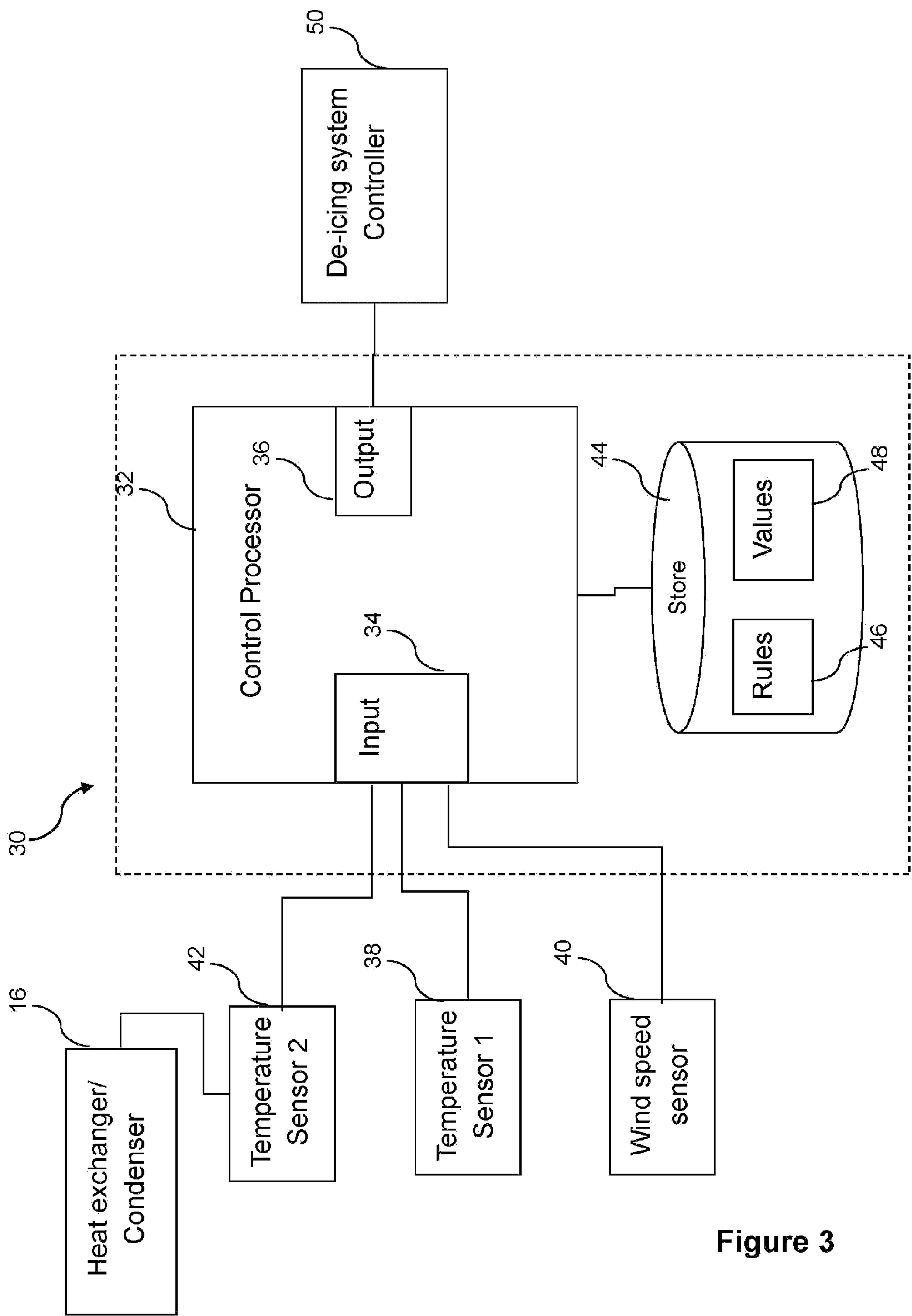


Figure 3

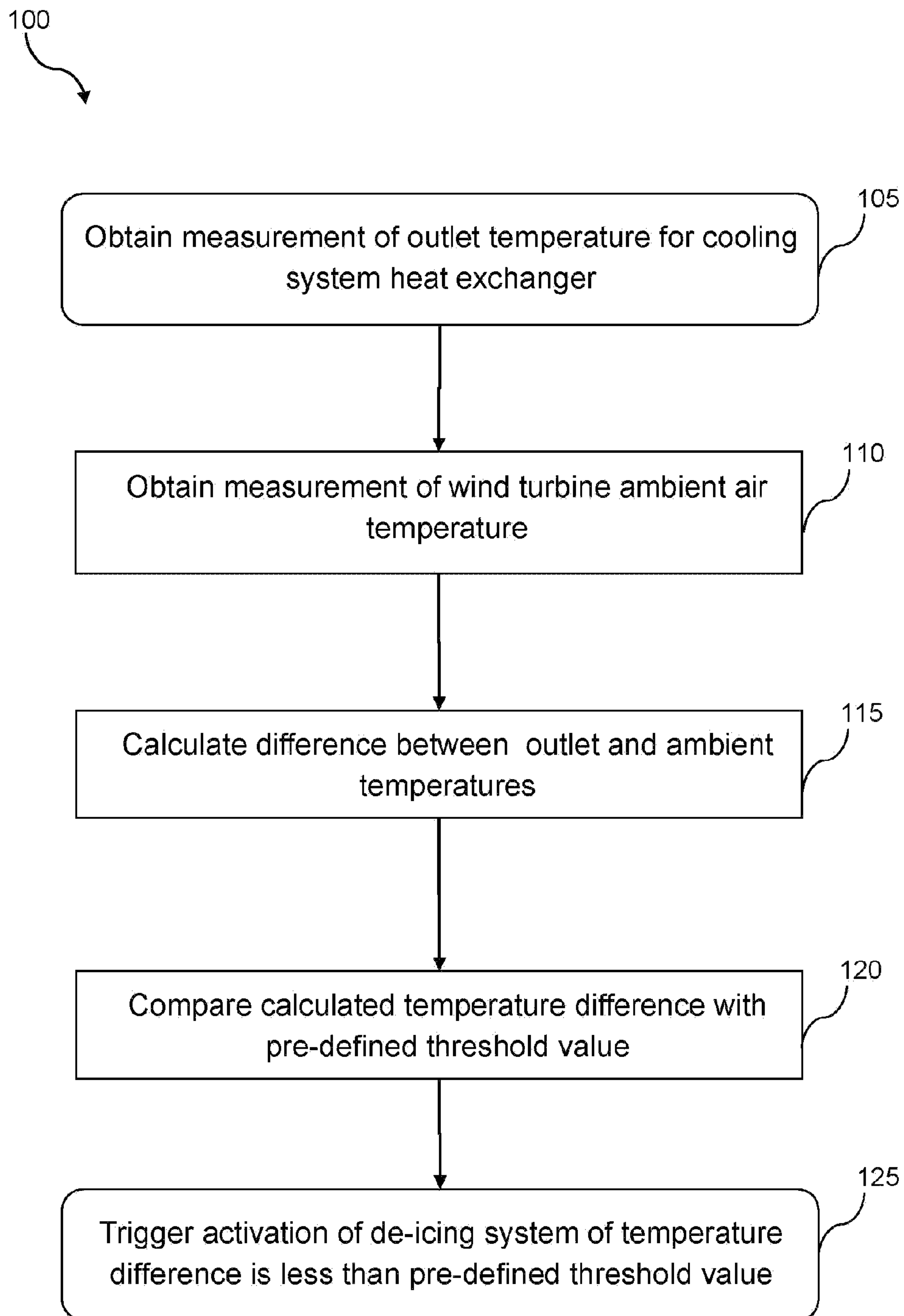


Figure 4

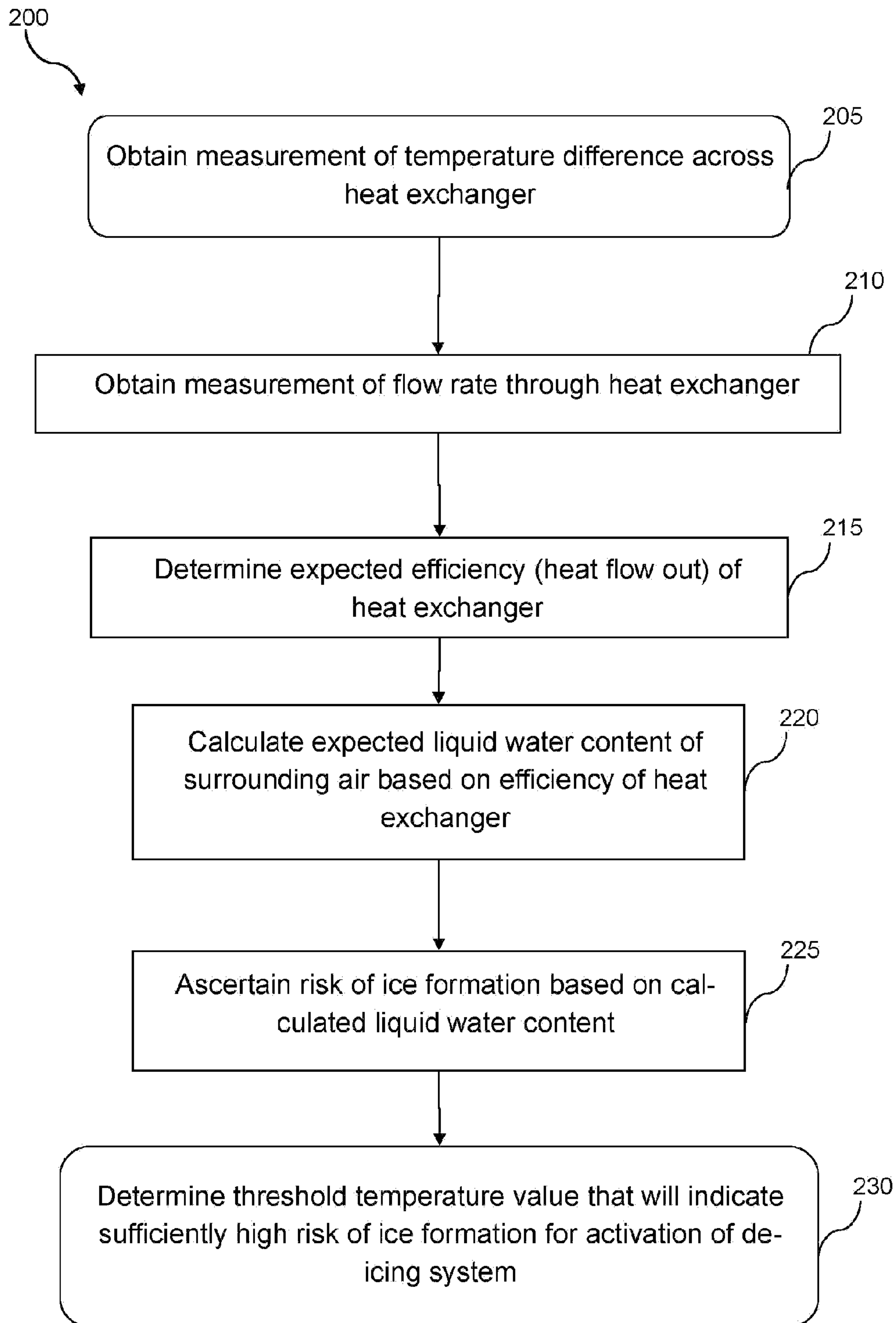


Figure 5