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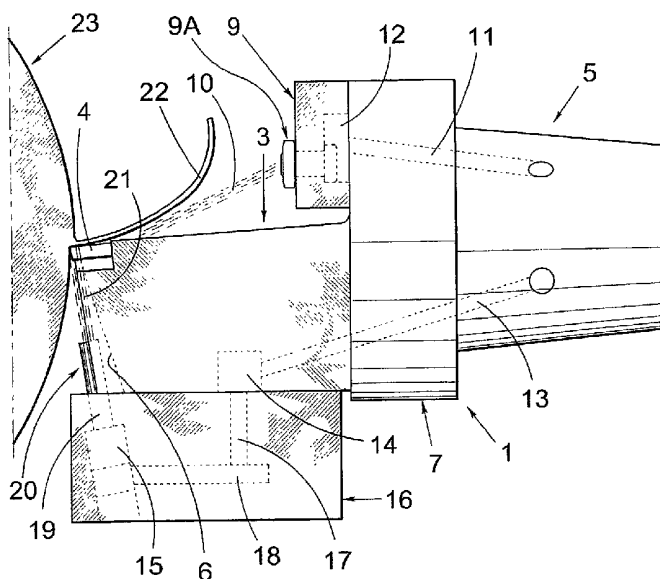
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For two-letter codes and other abbreviations, refer to the "Guidance Notes on Codes and Abbreviations" appearing at the beginning of each regular issue of the PCT Gazette.

(54) Title: CHIP REMOVING MACHINING OF A WORKPIECE WHILE APPLYING HIGH PRESSURE COOLING LIQUID



(57) Abstract: The chip removing machining of a workpiece is performed by a cutting tool (1, 1') which includes a cutting insert (4). In order to cool the cutting insert (4), one or more over-cooling nozzles (9A) is arranged for directing a jet of cooling liquid (10) downwardly toward a contact area between the workpiece (23) and a chip surface of the cutting insert (4). A sub-cooling nozzle (20) is arranged for directing a jet of cooling liquid (21) upwardly toward a contact area between the workpiece (23) and a flank surface of the cutting insert (4). A jet of cooling liquid can be emitted from only the over-cooling nozzle (9A), or from only the sub-cooling nozzle (20), or from both of those nozzles simultaneously.



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Chip removing machining of a workpiece while applying high pressure cooling liquidTechnical field of the invention

5 The present invention relates to a method for chip removing machining, wherein a so-called high pressure cooling is applied. At least one jet of cooling liquid under high pressure is directed towards the contact area between a cutting edge of a cutting insert for chip removing machining and the workpiece that the cutting insert machines. The invention also relates to a cutting tool for chip removing machining.

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Prior art

A cutting tool where one or more jets of cooling liquid under high pressure is sprayed in the area between the chip and the chip surface of the cutting insert is previously known from, for instance, SE 513 480 C. This type of cooling/chip control henceforth will be denominated as "over-cooling," because the jet is directed downwardly toward the cutting insert from above. The fact is that a jet of cooling liquid under high pressure according to SE 513 480 C not only provides cooling but also a certain degree of chip control.

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Certain types of materials are of the nature that the chips cannot be broken by means of the geometry of the cutting insert. For this reason, the chips leave the cutting edge in the form of long, tangled chips, which may cause interruptions in the machining process as well as also destroy the components being machined. An additional disadvantage is the subsequent chip handling, especially disposal of unwieldy chip tangles, which may mean a risk of injury for the operator.

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By supplying one or more jets of cooling liquid under high pressure in the zone between the chip and the chip surface of the cutting insert, a safe and reliable chip control can be obtained. The prerequisite for obtaining such a chip control is, however, that certain characteristics of the jet, i.e. flow, pressure (velocity) and point(s) of impact should be well adapted in relation to the current cutting criteria, i.e. cutting depth, feeding, cutting

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speed and material properties (hardness, strength and machinability). However, in this connection, it should be pointed out that the jet characteristics which provide an optimum chip control do not always ensure an optimum temperature control/cooling of the chip removing machining.

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Among those skilled in the art, different opinions are found as to what is to be regarded as "low" and "high" fluid pressure, respectively. However, generally the classification should be made in the following intervals:

- 10 Low pressure < 10 bar
Intermediate pressure 10 - 100 bar
High pressure > 100 bar

Aims and features of the invention

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A primary aim of the present invention is to provide a method and a device of the kind mentioned in the introduction where a satisfactory chip control is provided at the same time as a satisfactory temperature control/cooling is provided. Thereby, an increased, but above all a more predictable, service life of the cutting insert is obtained.

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Yet another aim of the present invention is to obtain an improved surface profile on the machined workpiece in comparison to conventional cooling.

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One aspect of the invention relates to a method for the chip removing machining of a workpiece. The method utilizes a cutting tool which comprises a cutting insert, an over-cooling nozzle arranged for directing a jet of cooling liquid downwardly toward a contact area between the workpiece and a chip surface of the cutting insert, and a sub-cooling nozzle arranged for directing a jet of cooling liquid upwardly toward a contact area between the workpiece and a flank surface of the cutting insert. The method

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comprises the steps of:

- A. effecting relative movement between the workpiece and the cutting insert for cutting chips from the workpiece, and
- B. emitting, during step A, a jet of cooling liquid from at least the sub-cooling nozzle
5 toward the second contact area.

The method can also be practiced by simultaneously emitting jets of cooling liquid from the over-cooling nozzle and the sub-cooling nozzle.

- 10 Another aspect of the invention pertains to a cutting tool for the chip removing machining of a workpiece. The tool comprises a seat for a cutting insert, an over-cooling nozzle, and a sub-cooling nozzle. The over-cooling nozzle is arranged for directing a jet of cooling liquid downwardly toward the seat (and thus toward a chip surface of a cutting insert). The sub-cooling nozzle is arranged for directing a jet of
15 cooling liquid upwardly toward the seat (and thus toward a flank surface of a cutting insert).

Brief description of the drawings

- 20 Below, two preferred embodiments of the invention will be described, reference being made to the accompanying drawings, where:

Fig 1 shows a schematic side view of a device for chip removing machining according to a first embodiment of the invention, the supply of cooling liquid being carried out via
25 a cone-shaped holder part.

Fig 2 shows a schematic side view of an alternative device for chip removing machining according to a second embodiment of the invention, the supply of cooling liquid being carried out by a flange intake.

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Fig 3 is a cross sectional view through an over-cooling nozzle.

Fig 4 is a rear view of the nozzle depicted in Fig. 3, i.e., a view looking from right-to-left in Fig. 3.

Detailed description of preferred embodiments of the invention

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The cutting tool 1 illustrated in fig 1 for chip removing machining comprises a front part 3, which has a cutting seat for a replaceable indexable insert 4. A rear part 5 of the cutting tool 1 is formed as a male part, which is intended to be received in a holder (not shown) of a machine tool. The rear part 5 may be of any suitable shape. For instance, in 10 Fig 1 the rear part 5 has the shape of a truncated cone. Between the front part 3 and the rear part 5, a flange 7 is arranged, said flange forming a stop face against the holder and can be formed with members for effecting automatic tool exchange.

As is seen in Fig 1, the cutting tool 1 is provided with a plate-shaped nozzle carrier 9, 15 which is applied on the side of the flange 7 facing the front part 3. In the nozzle carrier 9, one or more first or upper nozzles 9A (only one shown) is mounted, whereby said first nozzle sprays a first jet of liquid 10, with high pressure, obliquely from above towards the replaceable indexable insert 4.

20 The first nozzle 9A is preferably of the adjustable type, i.e. the direction of the jet which exits from the nozzle is adjustable. One way of adjusting the direction of the jet is shown in Fig. 3 and described in U.S. Serial No. 09/654,989, the disclosure of which is incorporated by reference herein. That is, the nozzle 9A is made to be rotatable about its longitudinal axis, and an outlet 9A' of the jet is non-parallel to the axis, whereby the 25 direction of the jet changes in response to rotation of the nozzle 9A. Alternatively, or additionally, the nozzle outlet could be offset from the axis.

Preferably, the nozzle carrier 9 is also provided with conventional flow stabilisers 15, normally one for each first nozzle. The flow stabiliser 15, which is depicted in Figs. 3 30 and 4, and also described in the aforementioned Serial No. 09/654,989, functions to divide the flow of liquid into a number of partial flows. Thus, the stabilizer can comprise a generally cylindrical insert having a series of radial wings 15' which divide

the nozzle interior into separate passages 15" (e.g., four passages in Fig. 4). By dividing the flow in that manner, the tendency of the liquid to become turbulent is counteracted.

This type of high pressure cooling is denominated "over-cooling", since the cooling jet is directed downwardly toward the insert. A first channel 11 is arranged for the supply of liquid to the nozzle carrier 9, said channel extending between the envelope surface of the rear part 5 and a first cavity 12 in the nozzle carrier 9. The first channel 11 thus passes through the flange 7. One of the ends of the first channel 11 ports in the front surface of the flange 7, more precisely in the cavity 12 behind and at a distance from the first nozzle 9A. As to how cooling liquid is supplied to the first channel 11, how cooling liquid is transferred from the first front end of the channel 11 to the first nozzle, (via the cavity 12), and how cooling liquid is sprayed out through the first nozzle towards the indexable insert 4, reference is made to the afore mentioned U.S. Serial No. 09/654,989, which also shows how a plurality of the first nozzles can be provided.

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The cutting tool according to the present invention also comprises a second channel 13, which extends from the envelope surface of the rear part 5 to a second cavity 14 at the bottom of the front part 3. In the embodiment according to Fig 1, one of the afore described stabilizers 15 is arranged, which is included in a housing 16, which is applied at the bottom of the front part 3. A third channel 17, a fourth channel 18 and a fifth channel 19 are also arranged in the housing 16. The third channel 17 extends from the second cavity 14 to one end of the fourth channel 18, the other end of which joins to the flow stabilizer 15. The fifth channel 19 is situated downstream of the flow stabilizer 15, said fifth channel 19 extending from the outlet of the flow stabilizer 15 to a second nozzle 20, by means of which cooling liquid is sprayed upwardly towards the indexable insert 4.

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In the embodiment illustrated in fig 1, the nozzle 20 is applied in a groove 6 on the front part 3. In that connection, the nozzle 20 is partly countersunk in the groove 6. Normally, said nozzle 20 is fixed, i.e. the direction of the second liquid jet leaving the second nozzle 20 under high pressure is not adjustable. The second liquid jet leaving the nozzle 20 is schematically illustrated in fig 1 and has been given the reference designation 21.

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This type of high pressure cooling is denominated "sub-cooling" because the cooling liquid is directed upwardly from below the cutting insert. Supply of cooling liquid to the second channel 13 is carried out in principally the same way as the supply of cooling liquid to the first channel 11.

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The cutting tool 1 described in fig 1 works principally in the following way. When the cutting tool 1 is mounted in a holder (not shown), chip removing machining may be carried out by means of the indexable insert 4 by establishing relative rotary movement between the insert and the workpiece. As shown schematically in fig 1, a chip 22 is about to be separated from a workpiece 23. In doing so, heat will be generated, i.e. there is a need for supplying cooling liquid, which may take place by means of the first and second nozzles 9A, 20 of the above-described cutting tool 1.

As is apparent from the description above, the cutting tool 1 according to the present invention permits the cooling liquid to be directed toward the point of cutting in respective directions from above and below the insert. In so doing, cooling liquid is supplied to the first channel 11 and the second channel 13, the cooling medium being supplied from the first channel 11 further to the first cavity 12 and then, by means of high pressure, out through the first nozzle 9A to effect cooling and chip control. Cooling liquid under high pressure is also supplied further through the second channel 13, through the second cavity 14, the third channel 17, the fourth channel 18, the flow stabilizer 15 and the fifth channel 19. Then, liquid under high pressure is sprayed out through the second nozzle 20, the liquid meeting the point of cutting from below and guaranteeing cooling of the point of cutting as well as also a certain chip control of the chip 22 released from the workpiece 23.

In an alternative embodiment of a cutting tool 1' according to the present invention illustrated in fig 2, said cutting tool has a so-called flange intake, i.e. the first and second channels 11', 13' extend through the flange 7' of the cutting tool 1', but not through the male part 5'. This means that the male part 5' of the cutting tool 1' is not intersected by channels for cooling liquid under high pressure. As for the design of the plate-shaped nozzle carrier 9, it is made in principally the same way as in the embodiment according

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to Fig 1, however, cooling liquid passes to the first channel 11' connecting to the first cavity 12 through the flange 7'.

The channels, the cavity, the flow stabilizer and the nozzle for sub-cooling are made in
5 principally the same way as in the embodiment according to Fig 1. However, cooling
liquid passes to the second channel 13' connected to the second cavity 14 through the
flange 7'. In this connection, it should be pointed out that when the male part 5' of the
cutting tool 1' according to Fig 2 is mounted in a female part of a holder, the flange 7'
will abut against a stop face of the holder. The stop face is intersected by a number of
10 channels corresponding to the number of first and second channels 11', 13' in the flange
7'. When the male part 5' is received in the female part, the flange 7' abuts against the
stop face. When liquid under high pressure is to be transferred to the flange 7', the same
will be exposed to an axial force aiming to separate the flange 7' from the stop face of
the holder, which in such a case makes the effective pressure of the liquid leaving the
15 nozzles drop. The axial force acting on the flange 7' is proportional to the pressure of
the liquid that is to pass between the flanges. In the embodiment illustrated in Fig 2,
there normally is a limitation in this pressure.

In accordance with the present invention, a cutting operation can be performed using the
20 over-cooling jet alone, or the sub-cooling jet alone. However, in many types of cutting
operations, the simultaneous use of the over-cooling jet and the sub-cooling jet is
necessary in order to obtain an optimum chip control in combination with an optimum
cooling/temperature control.

25 Feasible modifications of the invention

The cooling liquid, which is used in the present invention, is normally a conventional
cooling liquid. However, it is feasible within the scope of the invention also to use water
as a cooling liquid, if so, a corrosion inhibitor is added.

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In the above-described embodiments, only one second nozzle 20 is arranged to
guarantee sub-cooling. However, it is feasible within the scope of the invention also to

provide a plurality of second nozzles, whereupon the number of connecting channels and other auxiliary equipment must be adjusted to the number of second nozzles. Of course, also the number of first nozzles may be varied within the scope of the present invention.

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The male part 5; 5' included in the above-described embodiments is of truncated conical shape, the same preferably consisting of a male part of a tool coupling which is marketed under the trademark COROMANT CAPTO[®]. However, within the scope of the present invention alternative designs of the holder for the cutting tool are
10 conceivable, in an exemplifying and not limiting purpose, the KM[®] coupling may be mentioned.

In the two above-described embodiments, flow stabilizers are arranged adjacent to respective the over-cooling nozzle 9A and the sub-cooling nozzle 20. However, it is
15 feasible within the scope of the invention that the cutting tool according to the present invention entirely lacks flow stabilizers or that only the over-cooling nozzle or only the sub-cooling nozzle is provided with a flow stabilizer.

In the above-described embodiments, the over-cooling nozzle 9A is adjustable to vary
20 the direction of the jet, while the jet of the sub-cooling nozzle 20 is fixed (non-adjustable). The reason for this is that a precisely directed jet flow is normally not required for the nozzle 20 since the sub-cooling is not intended to have a mechanical effect on the chip released from the workpiece. However, it is feasible within the scope of the invention for all nozzles to be fixed or that all nozzles be adjustable.

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An additional feasible alternative is that the sub-cooling nozzle 20 could be fixed, but the housing 16, which carries the nozzle 20, could be somewhat axially adjustable.

Normally, the supply of cooling liquid is carried out under high pressure from a
30 common pressure source, i.e. the pressure in the jets of liquid is mainly the same irrespective of whether they are performing over-cooling or sub-cooling. However, the pressure in the jet or jets of liquid which carry out over-cooling need not be the same as

the pressure in the jet or jets of liquid which carry out sub-cooling. If different pressures are to be provided, this may be effected by means of a pressure regulator. The jet or jets of liquid which carry out over-cooling have a pressure which is in the high-pressure range, i.e. higher than 100 bar. This is in principle necessary if a mechanical effect is to be made on the chip released from the work piece. As for the jet or jets of liquid which carry out sub-cooling, these may have a pressure which is in the intermediate pressure range, i.e. higher than 10 bar but lower than 100 bar, or in the high pressure range, i.e. higher than 100 bar. It should however be advantageous if the jet or jets of liquid which carry out sub-cooling have a pressure within the high pressure range, whereby the risk for a vapour barrier being formed in the area between the release side of the cutting insert 4 and the workpiece 23 is reduced.

List of reference designations

	1; 1'	Cutting tool
	3; 3'	Front part
5	4	Indexable insert
	5; 5'	Rear part
	7; 7'	Flange
	9	Nozzle carrier
	9A	First nozzle
10	9A'	Outlet
	10	First liquid jet
	11; 11'	First channel
	12	First cavity
	13; 13'	Second channel
15	14	Second cavity
	15	Flow stabiliser
	15'	Radial wing
	15''	Passage
	16	Housing
20	17	Third channel
	18	Fourth channel
	19	Fifth channel
	20	Second nozzle
	21	Second liquid jet
25	22	Chip
	23	Workpiece

What is claimed is:

1. A method for the chip removing machining of a workpiece, utilizing a cutting tool (1) comprising a cutting insert (4), an over-cooling nozzle (9A) arranged for directing a jet of cooling liquid (10) downwardly toward a first contact area between the workpiece (23) and a chip surface of the cutting insert (4), and a sub-cooling nozzle (20) arranged for directing a jet of cooling liquid (21) upwardly toward a second contact area between the workpiece (23) and a flank surface of the cutting insert (4), characterized in, that the method comprises the steps of first effecting relative movement between the workpiece (23) and the cutting insert (4) for cutting chips from the workpiece (23), and secondly emitting, during said first step a jet of cooling liquid (21) from at least the sub-cooling nozzle toward the second contact area.
2. The method according to claim 1, wherein the second step comprises simultaneously emitting jets of cooling liquid (10, 21) from the over-cooling nozzle (9A) and the sub-cooling nozzle (20).
3. The method according to claim 2, wherein the jet of cooling liquid (10) from the over-cooling nozzle (9A) is emitted at a pressure greater than 100 bar, and the jet of cooling liquid (21) from the sub-cooling nozzle (20) is emitted at a pressure lower than 100 bar.
4. The method according to claim 2, wherein each of the jets of cooling liquid (10, 21) from the over-cooling (9A) and sub-cooling nozzles (20) are emitted at a pressure greater than 100 bar.
5. A cutting tool (1) for the chip removing machining of a workpiece (23), characterized in, that it comprises a seat for a cutting insert (4), an over-cooling nozzle (9A) arranged for directing a jet of cooling liquid (10) downwardly toward the seat; and a sub-cooling nozzle (20) arranged for directing a jet of cooling liquid (21) upwardly toward the seat.

6. The cutting tool (1) according to claim 5, characterized in, that it includes a cutting insert (4) mounted in the seat; wherein the over-cooling nozzle (9A) is arranged to direct its jet (10) toward a chip surface of the insert (4), and the sub-cooling jet (21) is arranged to direct its jet toward a flank surface of the insert (4).

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7. The cutting tool (1) according to claim 6, characterized in, that it comprises a tool body on which the cutting insert (4), the over-cooling nozzle (9A), and the sub-cooling nozzle (20) are mounted; the cutting insert (4) mounted on a front portion of the tool body (3, 3'); the tool body including a rear mounting portion (5, 5') adapted for mounting the tool; the rear mounting portion (5, 5') including channels (11, 13) formed therein and arranged to conduct cooling liquid for the over-cooling nozzle (9A) and the sub-cooling nozzle (20), respectively.

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8. The cutting tool (1) according to claim 6, characterized in, that it comprises a tool body on which the cutting insert (4), the over-cooling nozzle (9A), and the sub-cooling nozzle (20) are mounted, the cutting insert (4) mounted on a front portion (5, 5') of the tool body; the tool body including a rear mounting portion (5, 5') adapted for mounting the tool; the tool body including a flange (7, 7') disposed between the front portion (5, 5') and the mounting portion; the flange (7, 7') including channels (11, 13) formed therein and arranged to conduct cooling liquid for the over-cooling nozzle (9) and the sub-cooling nozzle (20), respectively; the mounting portion being free of liquid-conducting channels.

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9. The cutting tool (1) according to claim 5, wherein the over-cooling nozzle (9A) is adjustable to vary a direction of the cooling jet (10) emitted therefrom.

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10. The cutting tool (1) according to claim 9, wherein the sub-cooling nozzle (20) is fixed.

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11. The cutting tool (1) according to claim 9, wherein the sub-cooling nozzle (20) is adjustable to vary a direction of the cooling jet (21) emitted therefrom.

12. The cutting tool (1) according to claim 5, characterized in, that it includes a flow stabilizer (15) disposed upstream of the over-cooling nozzle (9A).

13. The cutting tool (1) according to claim 12, characterized in, that it
5 includes a flow stabilizer (15) disposed upstream of the sub-cooling nozzle (20).

14. The cutting tool (1) according to claim 5, characterized in, that it includes a flow stabilizer (15) disposed upstream of the sub-cooling nozzle (20).

AMENDED CLAIMS

[received by the International Bureau on 07 August 2002 (07.08.02);
original claims 1-14 replaced by new claims 1-8 (1 page)]

1. Method for chip removing machining, in which a so-called high pressure cooling is applied, where over-cooling is carried out by at least one first jet (10) of cooling liquid under high pressure being supplied to the contact area between a chip surface of a cutting insert (4) for chip removing machining and a chip (22) which is being separated from the workpiece (23) being machined by the cutting insert (4), characterized in that sub-cooling is carried out by at least one second jet (21) of cooling liquid under high pressure or intermediate pressure being supplied to the contact area between a flank surface of the cutting insert (4) and the workpiece (23) and that over-cooling and sub-cooling are carried out at the same time.
2. Method according to claim 1, characterized in that the direction of the first jets of liquid (10) which carry out over-cooling is adjustable.
3. Method according to any one of claims 1 or 2, characterized in that the jets (10, 21) of cooling liquid are flow stabilised.
4. Cutting tool (1; 1') for chip removing machining with high pressure cooling, which comprises a front part (3) which has at least one cutting insert (4) as well as a rear part (5; 5') which is detachably fixed in a holder of a machine tool, the cutting tool (1; 1') comprising at least one first nozzle included in the nozzle member (9) for over-cooling, as well as members (11-12; 11'-12) in order to supply cooling liquid under high pressure to said nozzle, included in the nozzle member (9), characterized in that at least one second nozzle (20) is arranged in order to guarantee sub-cooling, as well as members (13-19; 13'-19) in order to supply cooling liquid under high pressure or intermediate pressure to said second nozzle (20).
5. Cutting tool (1) according to claim 4, characterized in that one or more channels (11, 13), included in the members for the supply of cooling liquid, are arranged in a male part (5), which constitutes the rear part.
6. Cutting tool (1') according to claim 4, characterized in that one or more channels (11', 13'), included in the members for the supply of cooling liquid, are arranged in a flange (7'), which is situated between the front part (3') and the rear part (5').
7. Cutting tool (1; 1') according to any one of claims 4-6, characterized in that the nozzles, included in the nozzle member (9), for over-cooling are adjustable, i.e. the direction of the jet (10) of cooling liquid exiting under high pressure from the nozzles, included in the nozzle member (9), is adjustable.
8. Cutting tool (1; 1') according to any one of claims 4-7, characterized in that the nozzle (20) for sub-cooling is not adjustable.

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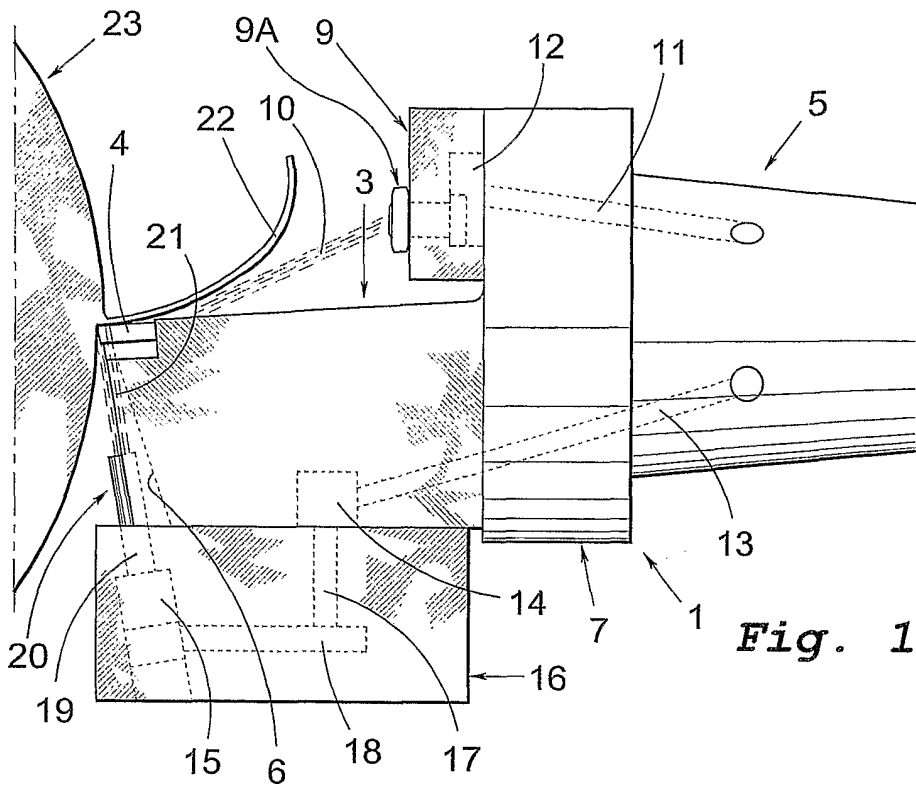


Fig. 1

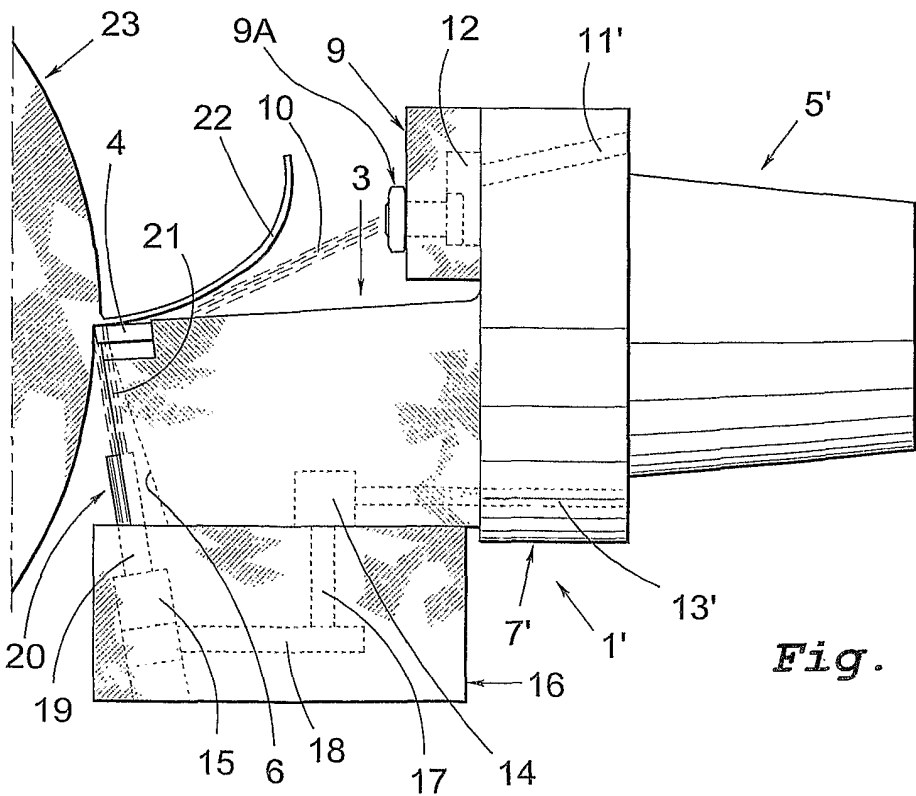


Fig. 2

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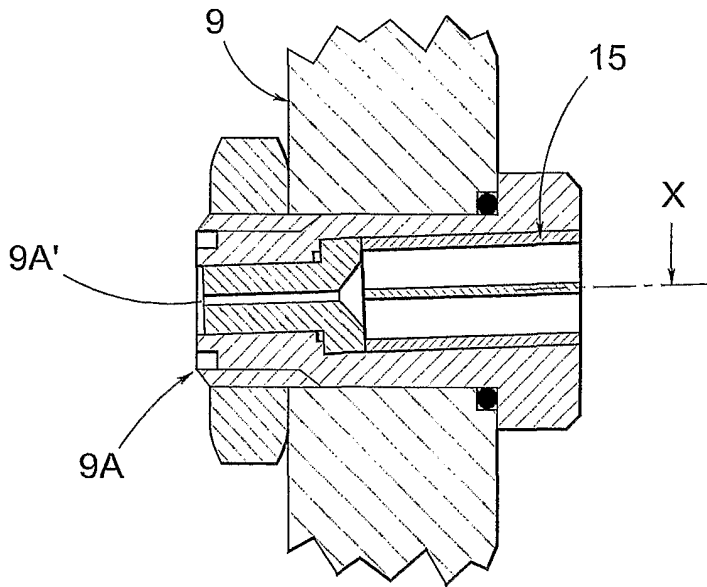


Fig. 3

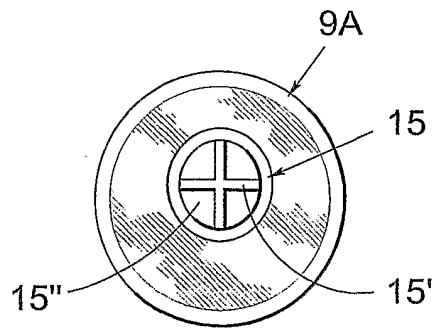


Fig. 4

INTERNATIONAL SEARCH REPORT

International application No.

PCT/SE 02/00329

A. CLASSIFICATION OF SUBJECT MATTER

IPC7: B23B 27/10

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC7: B23B, B23C

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

SE,DK,FI,NO classes as above

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	File WPI, Derwent accession no 2000-067348 Nissan Motor Co Ltd: "Cutting tool for machining" JP,A,11320213, 19991124, DW200006, fig 5, abstract --	1-14
Y	WO 9939852 A1 (SANDVIK AKTIEBOLAG), 12 August 1999 (12.08.99), page 2, line 5 - line 15, figures 1-10, abstract --	1-14
P,X	EP 1142669 A2 (SKF SVERIGE AB), 10 October 2001 (10.10.01), figures 1,2, claims 1-9, abstract	1,2,5,6
P,A	--	3-4,7-14

 Further documents are listed in the continuation of Box C.
 See patent family annex.

* Special categories of cited documents:

- "A" document defining the general state of the art which is not considered to be of particular relevance
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Date of the actual completion of the international search

29 May 2002

Date of mailing of the international search report

14 -06- 2002

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INTERNATIONAL SEARCH REPORT

International application No.

PCT/SE 02/00329

C (Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	EP 0534450 A2 (ISCAR LTD), 31 March 1993 (31.03.93), figures 1,2, abstract --	1-14
A	DE 3004166 A1 (SANDVIK AB), 21 August 1980 (21.08.80), figure 2 --	1-14
A	US 5775854 A (WERTHEIM), 7 July 1998 (07.07.98), figure 1, abstract -- -----	1-14

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No.

PCT/SE 02/00329

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