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DESCRIPTION

CROSS-REFERENCE TO RELATED APPLICATION

[0001] This application claims priority back to U.S. Patent Application No. 13/516,407 filed on June 18, 2012, and U.S. Patent Application No. 61/639,952 filed on April 29, 2012.

BACKGROUND OF THE INVENTION

1. Field of the Invention.

[0002] The present invention relates generally to the field of wind energy, and more specifically, to a wind energy system and a method for using the wind energy system to store energy, mine metals, produce hydrogen and decontaminate water.

2. Description of the Related Art.

[0003] The majority of the existing wind turbines use horizontal axis turbines. These turbines drive an electrical machine typically through a high ratio gearbox. The extracted power is processed fully, as in the case of permanent magnet generators, or partially by means of slip recovery, as in the case of doubly fed induction generators. In both cases, the electrical machine, associated gearbox, coupling and clutch are located in the nacelle on top of the tower. This has the consequence of requiring a larger tower and associated structure.

[0004] In a conventional wind farm energy system, the electrical energy is generated by a cascade of units so that if one of these units fails, operation is interrupted immediately. In addition, the cost and complexity of maintenance action are significant due to the fact that the gearbox and generator are on the top of a fixed tower that cannot be lowered. Furthermore, the electrical power generated by the conventional wind turbine fluctuates with time as a function of the wind prevailing condition. In some instances, when the wind velocity falls below or rises above certain thresholds, energy production ceases. Because this availability of energy is fluctuating, it cannot be relied upon for sustained energy supply.

[0005] The present invention overcomes these and many other limitations of conventional wind energy systems, and it also provides significant advantages in terms of size, cost and ease of installation. Structural disadvantages of conventional wind energy systems include, but are not limited to, the following: (i) the turbines only turn to face the prevailing wind on a horizontal axis; (ii) they do not include a mechanism for reducing driveline mechanical drag relating to available wind speed; (iii) they do not provide a system for absorbing fluctuations in wind power so as to provide a constant level electrical power output; (iv) the rotor blades tend to vibrate excessively and suffer from asymmetrical torque effect, which increases driveline maintenance and limits placement options for the turbines; (v) they do not include an integrated energy storage system, which enables a controlled energy output without the loss of energy; (vi) the single generator and gearbox located in the nacelle are very heavy and difficult to maintain; (vii) the coupled driveline does not allow the generators to be driven independently of the rotor system; (viii) there is no hybrid power option for constant energy supply; (ix) they do not incorporate load sensors that automatically adjust the tower height based on load stress or wind speed, thereby avoiding the need to turn rotors off and cease energy production; and (x) the towers are not able to be lowered for maintenance. In addition to solving all of the above problems, the present invention incorporates a bat deterrence system that is not found in any existing wind energy systems.

[0006] Examples of patented prior art wind energy systems (or inventions relating to wind energy systems) include: U.S. Patent No. 3,932,723 (Browning, 1976) entitled "Windmills"; U.S. Patent No. 4,058,979 (Germain, 1977) entitled "Energy Storage and Conversion Technique and Apparatus"; U.S. Patent No. 4,274,010 (Lawson-Tancred, 1981) entitled "Electric Power Generation"; U.S. Patent No. 4,366,779 (Knecht, 1983) entitled "Wind Driven Heating System"; U.S. Patent No. 4,447,738 (Allison, 1984) entitled "Wind Power Electrical Generator System"; U.S. Patent No. 4,496,846 (Parkins, 1983) entitled "Power Generation From Wind"; U.S. Patent No. 4,496,847 (Parkins, 1995) entitled "Power Generation From Wind"; U.S. Patent No. 4,498,017 (Parkins, 1985) entitled "Generating Power From Wind"; U.S. Patent No. 4,648,801 (Wilson, 1987) entitled "Wind Turbines"; U.S. Patent No. 7,183,664 (McClintic, 2007) entitled "Methods and Apparatus for Advanced Wind Turbine Design"; U.S. Patent No. 7,418,920 (Harvey et al., 2008) entitled "Wind Turbine With Hydraulic Transmission"; U.S. Patent No. 7,436,086 (McClintic, 2008) entitled

"Methods and Apparatus for Advanced Wind Turbine Design"; U.S. Patent NO. 7,569,943 (Kovach et al. 2009) entitled "Variable Speed Wind Turbine Drive and Control System"; U.S. Patent No. 7,656,055 (Torres et al., 2010) entitled "Hydro-Wind Power Generating Turbine System and Retrofitting Method"; U.S. Patent No. 7,863,767 (Chapple et al., 2011) entitled "Turbine Drive Electric Power Production System and a Method for Control Thereof"; U.S. Patent No. 7,877,992 (Chen, 2011) entitled "Hydraulic Power Generation system Driven by Compression Air Produced by Fluid"; U.S. Patent No. 7,932,620 (Plant, Jr., 2011) entitled "Windmill Utilizing a Fluid Driven Pump"; and U.S. Patent No. 7,944,078 (Wang, 2011) entitled "Wind Turbine With Hydro-Transmission."

BRIEF SUMMARY OF THE INVENTION

[0007] the present invention is a wind energy system comprising a wind turbine comprising a cowling surrounded by a diffuser, a plurality of inner rotor blades located inside of the cowling, wherein the plurality of inner rotor blades rotates about an inner rotor hub; a plurality of outer rotor blades positioned between the diffuser and the cowling, wherein the plurality of outer rotor blades are counter-rotating relative to the plurality of inner rotor blades; a drive mechanism located within the inner rotor hub; a dynamic telescopic tower; any a tower support that connects the wind turbine to the dynamic telescopic tower. In a preferred embodiment, the invention further comprises a plurality of air guides located inside of the cowling and in front of the inner rotor blades. The outer rotors preferably rotate around the cowling on roller bearings.

[0008] In a preferred embodiment, the invention further comprising two horizontal wind speed sensors and two vertical wind speed sensors situated on an outer surface of the cowling forward of the diffuser, the two horizontal wind speed sensors are situated opposite one another on a horizontal plane, and the two vertical wind speed sensors are situated opposite one another on a vertical plane. Preferably, the cowling and diffuser each comprises an exhaust with an inner diameter and an inlet with an inner diameter, the inner diameter of the exhaust of the cowling is greater than the inner diameter of the inlet of the cowling, and the inner diameter of the exhaust of the diffuser is greater than the inner diameter of the inlet of the diffuser. Preferably, the cowling and diffuser each comprises a rear edge, the rear edges of the cowling and diffuser are roughly aligned vertically, the cowling extends a certain length from the rear edge of the cowling to a front edge of the cowling, the diffuser extends a certain length from the rear edge of the diffuser to a front edge of the diffuser, and the certain length of the diffuser is equal to roughly half the certain length of the cowling.

[0009] In one embodiment, the inner rotor blades are connected to a first drive shaft, the first drive shaft is connected to the inner rotor hub, wherein the first drive shaft rotates a first gear, the first gear is connected to a plurality of first variable displacement hydraulic pumps that pump a pressurized liquid through a high-pressure hydraulic circuit each of the plurality of first variable displacement hydraulic pumps is connected to the first gear by a first electromagnetic coupling, and the first electromagnetic coupling is controlled by a power control unit that processes information from a speed sensor located on the first drive shaft. In another embodiment, the inner rotor blades are connected to a first drive shaft, the first drive shaft is connected to the inner rotor hub, the first drive shaft rotates a first gear, the first gear is connected to a plurality of first variable displacement hydraulic pumps that pump a pressurized liquid through a high-pressure hydraulic circuit, each of the plurality of first variable displacement hydraulic pumps is connected to the first gear by a first electromagnetic coupling, and the first electromagnetic coupling is controlled by a power control unit that processes information from a torque sensor located on the first drive shaft.

[0010] In a preferred embodiment, the invention further comprises a ring gear that rotates when the plurality of outer rotor blades rotates, the ring gear engages an outer rotor drive gear, the outer rotor drive gear is connected to a second drive shaft, the second drive shaft is connected to a second gear, the second gear drives a plurality of second electromagnetic couplings, and each of the plurality of second electromagnetic couplings is connected to a second variable displacement hydraulic pump. In yet another preferred embodiment, the invention further comprises one or more sensors that monitor rotational speed of the first gear and second gear, the dynamic telescopic tower positions the wind turbine at a height, the dynamic telescopic tower comprises one or more load sensors, and a computer control unit automatically adjusts the height of the wind turbine based on data from the one or more sensors that monitor the rotational speed of the first gear and second gear and the one or more load sensors in the dynamic telescopic tower.

[0011] In one embodiment, the inner rotor blades are connected to a first drive shaft, the first drive shaft is connected to the inner rotor hub, the first drive shaft rotates a first gear, the first gear is connected to a plurality of first air compressors that pump a pressurized fluid through a high-pressure pneumatic circuit, each of the plurality of first air compressors is connected to the first gear by a first electromagnetic coupling, and the first electromagnetic coupling is controlled by a power control unit that processes information from a speed sensor located on the first drive shaft. In another embodiment, the inner rotor blades are connected to a first drive shaft, the first drive shaft is connected to the inner rotor hub, the first drive shaft rotates a first gear, the first gear is

connected to a plurality of first air compressors that pump a pressurized fluid through a high-pressure pneumatic circuit, each of the plurality of first air compressors is connected to the first gear by a first electromagnetic coupling, and the first electromagnetic coupling is controlled by a power control unit that processes information from a torque sensor located on the first drive shaft.

[0012] In a preferred embodiment, the invention further comprises a ring gear that rotates when the plurality of outer rotor blades rotates, the ring gear engages an outer rotor drive gear, the outer rotor drive gear is connected to a second drive shaft, the second drive shaft is connected to a second gear, the second gear drives a plurality of second electromagnetic couplings, and each of the plurality of second electromagnetic couplings is connected to a second air compressor. In yet another preferred embodiment, the invention further comprises one or more sensors that monitor rotational speed of the first gear and second gear, the dynamic telescopic tower positions the wind turbine at a height, the dynamic telescopic tower comprises one or more load sensors, and a computer control unit automatically adjusts the height of the wind turbine based on data from the one or more sensors that monitor the rotational speed of the first gear and second gear and the one or more load sensors in the dynamic telescopic tower.

[0013] In a preferred embodiment, energy is generated by wind with a mean direction, and the dynamic telescopic tower comprises an integrated three-dimensional yaw control that aligns the wind turbine with the mean direction of the wind. The three-dimensional yaw control preferably comprises a plurality of yaw horizontal drive motors attached to a horizontal yaw ring gear and a plurality of vertical yaw drives connected to a drive rail on a yaw control platform.

[0014] In one embodiment, the invention further comprises a bat deterrence system, the bat deterrence system comprises a microphone, a preamplifier, a low-pass filter, an analog-to-digital converter, a digital sound processor, a digital-to-analog converter, an amplifier, and a speaker, and the bat deterrence system is attached to the wind turbine. In further embodiment, the invention further comprises a bat deterrence system, the bat deterrence system comprises a microphone, a pre-amplifier, a low-pass filter, an analog-to-digital converter, a digital sound processor, a digital-to-analog converter, an amplifier, and a Speaker, and the bat deterrence system is attached to the dynamic telescopic tower.

[0015] In a preferred embodiment, the invention further comprises one or more hydraulic accumulators that compress an inert gas and use the compressed inert gas to force the pressurized liquid through a controlled release valve and through high-pressure pipes to drive a hybrid variable displacement hydraulic pump. In another preferred embodiment, the hybrid variable displacement pump drives one or more ground-based multiple permanent magnet electrical generators to create electricity. Each of the first variable displacement hydraulic pumps preferably comprises a solenoid-operated bypass valve that diverts fluid flow through the first variable displacement hydraulic pump when the first variable displacement pump is not in use.

[0016] In a preferred embodiment, the power control unit monitors data comprising wind speed, drive shaft speed and hydraulic pressure via electrical sensors and processes the data to determine how many first variable displacement hydraulic pumps need to be actuated at any moment in time. In another preferred embodiment, the power control unit monitors data comprising wind speed, drive shaft speed and hydraulic pressure via electrical sensors and processes the data to determine how many second variable displacement hydraulic pumps need to be activated at any moment in time. When wind speed reaches a certain velocity, the dynamic telescopic tower is preferably automatically lowered to a safe operating height without the inner and outer rotor blades being switched off.

[0017] In a preferred embodiment, rotational speed of the rotor blades changes as wind velocity changes. Preferably, the invention further comprises hydraulic accumulators that absorb fluctuating energy levels from wind, store excess energy, and supply a constant and controlled output to drive a plurality of permanent magnetic generators. The plurality of permanent magnetic generators are preferably housed in modular generator clusters. The modular generator clusters preferably switch on and off individually as and when demand is required.

[0018] In a preferred embodiment, each permanent magnetic generator is driven by a generator drive gear, and the generator drive gear turns a permanent magnetic generator coupling that spins a drive in the permanent magnetic generator without a direct mechanical linkage. Preferably, each permanent magnetic generator comprises a water jacket that cools the permanent magnetic generator by passing a cool liquid around heat-producing mechanical components. A computer control unit preferably monitors hydraulic pressure at a hydraulic motor that drives the generator drive gear, calculates how many permanent magnetic generators to activate to generate electricity, and switches individual permanent magnetic generator electromagnetic couplings on or off depending on available hydraulic pressure.

[0019] The invention is also a wind energy system comprising; a wind turbine comprising a cowling surrounded by a diffuser; a plurality of first inner rotor blades located inside of the cowling, wherein the plurality of inner rotor blades rotates about a first inner rotor hub; a plurality of second inner rotor blades located inside of the cowling and behind the plurality of first inner rotor

blades, wherein the plurality of second inner rotor blades rotates about a second inner rotor hub in the same direction as the plurality of first inner rotor blades; a plurality of outer rotor blades positioned between the diffuser and the cowling, wherein the plurality of outer rotor blades are counter-rotating relative to the plurality of first and second inner rotor blades; a drive mechanism located within the inner rotor hub; a dynamic telescopic tower; and a tower support that connects the wind turbine to the dynamic telescopic tower.

[0020] The invention is also a method of mining metals comprising: using the wind energy system described above to generate energy; passing a slurry through an electrochemical ion transfer desalination process to remove precious metals from the slurry and produce hydrogen gas and oxygen; producing potable water by removing metals and contaminants from the slurry; and storing the hydrogen gas and oxygen produced during the desalination process in pressurized containers.

BRIEF DESCRIPTION OF THE DRAWINGS

[0021]

Figure 1 is a schematic diagram of the wind energy system of the present invention.

Figure 2 is a schematic diagram of an alternate embodiment of the present invention in which pneumatic power is used in lieu of hydraulic power.

Figure 3 is a front perspective view of the ducted diffuser multiple rotor wind turbine and dynamic tower of the present invention.

Figure 4a is a front perspective view of the ducted diffuser multiple rotor wind turbine nacelle and diffuser of the present invention.

Figure 4b is a rear perspective view of the ducted diffuser multiple rotor wind turbine nacelle and diffuser of the present invention.

Figure 5a is a front perspective view of the ducted diffuser multiple rotor wind turbine nacelle and diffuser of the present invention with two sets of internal rotors.

Figure 5b is a rear perspective view of the ducted diffuser multiple rotor wind turbines nacelle and diffuser of the present invention with two sets of internal rotors.

Figure 6 is a side elevation view of the ducted diffuser multiple rotor wind turbine of the present invention.

Figure 7 is a from view of the ducted diffuser multiple rotor wind turbine of the present invention shown without the tower.

Figure 8 is a side elevation cross-section view of the wind turbine of the present invention illustrating how air flows through the turbine.

Figure 9 is a schematic operating diagram of the wind turbine hydraulic drive system based in the nacelle of the present invention.

Figure 10 is a front perspective view of the center nacelle frame and drive shown without outer cladding or body panels.

Figure 11 is a rear perspective view of the center nacelle frame and drive shown without outer cladding or body panels.

Figure 12 is a perspective view of a section of the outer rotor system of the present invention.

Figure 13 is a front perspective view of the dynamic tower and wind turbine of the present invention shown in a raised position.

Figure 14 is a front perspective view of the dynamic tower and wind turbine of the present invention shown in at lowered position.

Figure 15 is a detail perspective view of the below-ground installation of the dynamic tower in the lowered position shown with the turbine nacelle yaw control and hydraulic pipe winding device located inside the base of the tower.

Figure 16 is a front perspective view of the dynamic tower on surface installation with cable support.

Figure 17A a perspective view of the three-dimensional yaw system of the present invention.

Figure 17B is a perspective view of the wind turbine of the present invention tilted forward.

Figure 17C is a perspective view of the wind turbine of the present invention tilted backward.

Figure 18 is a perspective view of the dynamic tower drive system used to raise and lower the tower during operation.

Figure 19 is a detail interior view of the electromagnetic drive of the dynamic tower of the present invention.

Figure 20 is a perspective view of the permanent magnet generator of the present invention shown in vertical orientation with a water jacket and an electromagnetic variable drive.

Figure 21 is a perspective view of the modular generator cluster and hydraulic drive system of the present invention shown with an installation frame.

Figure 22 is a schematic diagram of the bat deterrent system of the present invention.

REFERENCE NUMBERS

[0022]

- 1 Wind energy
- 2 Wind turbine
- 3 Dynamic tower
- 4 High-presure hose
- 5 Hydraulic pipe
- 6 High-pressure hose reel
- 9 Electrohydraulic servo valve
- 10 Hydraulic accumulator
- 12 Hybrid variable displacement hydraulic pump
- 15 Electrical permanent magnet generator
- 16 First heat exchanger
- 17 Steam generator
- 18 Electrical junction control switch
- 19 Water-based slurry
- 20 Water desalination system
- 21 Hydrogen electrolyzer
- 22 Desalinated water
- 23 Dryer
- 24 Compound
- 26 First pressurised storage container

27	Non-return valve
28	Three-way valve
29	Hydrogen fuel cell
30a	Tanker
30b	Commercial shipper
31	Second heat exchanger
32	Three-way electrical switch
33	DC to AC converter
34	Power transmission grid
35	Second pressurized storage container
36	Hybrid energy system
37	Computer control unit (CCU)
38	Wind speed
41	Third heat exchanger
45	Piping
52	Two-way pipe
53	Hybrid-driven air compressor
54	Hybrid air compressor heat exchanger
55	High-pressure air line
56	Air dryer
57	First air dividing valve
58	Compressed air storage vessel
59	Air release valve
60	One-way valve
61	Second dividing valve
62	High-speed pneumatic motor
80	Cowling
81	Diffuser
82	Air guide

83	Inner rotor blade
84	Outer rotor blade
85	Inner rotor hub
86	Tower support
87	Structure stave
88	Wind speed sensor (horizontal plane)
89	Wind speed sensor (vertical plane)
90	First gear
92	Variable displacement hydraulic pump
93	Torque/speed sensor
94a	First electronic shutoff valve
94b	Second electronic shutoff valve
96a	First electromagnetic coupling
96b	Second electromagnetic coupling
97	Pressure release valve
98	Hydraulic actuator
99	Power control unit (PCU)
100	Hydraulic line
110	Rotor hub
111	Rotor blade attachment base
112	Disc brake
113	First drive shaft
117	Tubular space frame
120	First bearing
121	Second bearing
131	Outer rotor assembly
132	Ring gear
133	Roller bearing
134	

	Second driver shaft
135	
	Second gear
136	
	Third electromagnetic coupling
140	
	Ground
141	
	Drive rail
142	
	Section (of dynamic tower)
143	
	Yaw control
144	
	Hydraulic hose reel
145	
	Service panel
146	
	Steel cable
147	
	platform
150	
	Yaw bearing
151	
	Yaw horizontal drive motor
152	
	Yaw control platform
153	
	Yaw tilt drive rail
154	
	Vertical yaw frame
155	
	Vertical yaw drive
156	
	Horizontal yaw drive gear
157	
	Horizontal yaw ring gear
160	
	Dynamic tower electromagnetic drive
162	
	DC rotor
163	
	Bevel gear
164	
	Dynamic tower roller guide
171	
	Generator drive gear
172	
	PMG electromagnetic coupling
173	
	Electrical cable
174	
	Outlet connector
175	
	Inlet connector
176	
	Fixing plate
180	

	Generator cluster drive gear
181	
	Hydraulic motor
182	
	Lifting hook
185	
	Generator cluster frame
186	
	Retaining bracket
191	
	Front area (of turbine)
192	
	Rear area (of turbine)
193	
	Wind turbine tilted down
194	
	Wind turbine tilted up
195	
	Rear inner rotor blade
196	
	Cowling outer surface
197	
	Cowling inner surface
198	
	Diffuser leading edge
199	
	Outer rotor drive gear
201	
	Microphone
202	
	Pre-amplifier
203	
	Low-pass filter
204	
	Digital signal
205	
	digital sound processor
206	
	Digital analog converter
207	
	Amplifier
208	
	Speaker

DETAILED DESCRIPTION OF INVENTION

[0023] Figure 1 is a schematic diagram of the wind energy system of the present invention. Specifically, Figure 1 shows the process by which the sustainable energy system (SES) of the present invention extracts energy from wind through a decoded multiple rotor ducted diffuser wind turbine by converting the energy from the prevailing wind into rotational energy of the rotor blades. The rotational energy captured by the rotor blades drives a series of hydraulic pumps that transfer the rotational energy into a pressurized fluid. The pressurized fluid transmits, balances and stores the captured energy in hydraulic accumulators, which retain the energy under pressure that can then be released through valves in a controlled manner.

[0024] The fluid pressure is maintained in the accumulators by a membrane bladder (diaphragm), steel piston or steel bellows.

Each of these options uses the hydraulic pressure to force the bladder, piston or bellows against an inert gas, which compresses under the pressure applied. The pressurized inert gas is used to force the pressurized fluid out through a controlled release valve and through high-pressure pipes to drive a hydraulic motor, which in turn drives the ground-based multiple permanent magnet electrical generators (PMGs) to create electricity. The SES uses high- and low-air pressure zones created by the aerodynamics of the ducted diffuser wind turbine to pull or suck air through the rotor systems. The creation of the low-pressure area at the rear of the wind turbine forces the air to accelerate through the rotors and, as such, create more wind energy than that of an open rotor wind turbine. The inner and outer rotors are counter-rotating to reduce vibration and asymmetrical effect.

[0025] A series of hydraulic pumps is connected to a number of drive shafts, one for each set of rotors, either through electromagnetic couplings that enable the SES to switch the individual hydraulic pumps on or off according to the wind speed or without electromagnetic couplings. When the SES is used without the electromagnetic couplings, variable displacement hydraulic pumps are used to enable the shutting down or switching off of unwanted hydraulic pumps without retaining unwanted mechanical drag associated with standard non-variable displacement hydraulic pumps. When switched off, the electromagnetic couplings have exceptionally low friction or drag on the system to improve the drive efficiency and maximize energy output. The multiple generators switch on or off through the same electromagnetic coupling system, to provide maximum efficiency. Because the motor drive is decoupled from the generators, the SES is able to use hybrid power sources to drive the generators when the wind speed is low or when additional energy is required to provide a constant on demand energy supply.

[0026] The electrical energy can be transmitted to an end user or an electricity transmission grid, or it can be used to power a mining process through electrochemical ion transfer for the extraction of metals such as gold, platinum and copper from slurry without the use of contaminant chemicals such as cyanide. During the mining procedure, the slurry goes through electrochemical ion transfer desalination process that produces hydrogen gas and oxygen as byproducts, and through the removal of the metals and contaminants, potable water is produced. The hydrogen and oxygen produced during the electrochemical ion transfer process is captured and stored separately in pressurised containers and can be used in the generation of energy through hydrogen fuel cell or by injecting the hydrogen and oxygen with natural gas into a gas turbine as a backup power supply to the SES. This enables the SES to provide self-sustainable energy at all times.

[0027] Referring to Figure 1, the wind energy **1** is harvested through the decoupled ducted diffuser multiple rotor wind turbine of wind turbines **2**. The ducted diffuser multiple rotor (DDMR) wind turbine **2** contains two or more separate decoupled rotor systems, and each of these rotor system collects the energy and transmits it through a series of hydraulic pumps.

[0028] The wind accelerates as it travels through the wind turbine, which allows the SES to exceed the energy levels depicted within Betz's Law (a theory developed in 1919 by German physicist Albert Betz about the maximum possible energy to be derived from the wind by an open rotor wind turbine). Betz's Law is used by those skilled in the art of designing wind energy systems to predict energy levels possible through an open rotor wind turbine. The DDMR aerodynamic encapsulated cowling and diffuser reduce rotor tip and tower bypass noise and recover the energy lost through the blade tips of an open rotor. Each of the counter-rotating rotor assemblies drives a large gear, which in turn drives multiple hydraulic pumps. The hydraulic pump gear mechanism contains an electromagnetic Coupling, which couples or decouples the hydraulic pump from the main gear drive, thereby allowing the hydraulic pumps to be individually turned on or off depending on the available wind speed or hydraulic pressure. The SES can be operated without the electromagnetic couplings but loses some efficiency through increased mechanical drag or friction.

[0029] By decoupling unwanted Variable displacement hydraulic pumps at low wind speeds, the operational drag of the energy transmission is reduced, and efficiency is improved, enabling the SES to produce energy in very low wind speeds. Each variable displacement hydraulic pump has a solenoid-operated bypass valve that diverts the fluid flow through the variable displacement hydraulic pump when not in use. The power control unit (PCU) monitors the wind speed **38**, drive shaft speed and hydraulic pressure via electrical sensors and then processes this data to determine how many variable displacement hydraulic pumps need to be activated at any moment in time.

[0030] In low wind speeds, the PCU will activate a small number of the variable displacement hydraulic pumps, (for example, one to four) to reduce the energy required to drive the hydraulics and thus maximize the energy efficiency from the given wind speed. At higher wind speeds, the PCU will automatically increase the number of variable displacement hydraulic pumps to extract further energy from the wind. In a preferred embodiment, the SES hydraulic drive can contain from six to thirty variable displacement hydraulic pumps, depending on the output size of the individual hydraulic pumps and the rotor diameter of The wind turbine.

[0031] The SES outer rotor uses the same hydraulic energy recovery system as the inner rotor (or rotors), although the drive mechanism is different. The drive on the outer rotor is supplied by a ring gear, which, turns a drive shaft at the bottom of the outer rotor. The drive shaft turns a number of variable displacement hydraulic pumps, as shown in Figure 12. The pressurized fluid from the variable displacement hydraulic pumps or pneumatic compressors passes down from the wind turbine **2** to the base of the

dynamic tower **3** via a high-pressure hose **4** at an operating pressure of up to 5000 psi. In a preferred embodiment, the high-pressure hydraulic hose is the Gates EFG6K manufactured by Gates Corporation of Denver, Colorado. The dynamic tower (shown as reference number **3** in Figures 13 and 14) of the present invention allows variable tower height sittings during operation and maintenance, The high-pressure hose is retracted or extracted from the reel depending on the direction of the height adjustment of the dynamic tower through a computer-controlled hose reel at the base of the dynamic, tower.

[0032] The high-pressure hose reel **6** at the base of the tower collects the hose when the SES is operating at a reduced height or during maintenance. The motor-driven hose reel **6** and dynamic tower **3** operate in unison during the height adjustment of the dynamic tower and are controlled by the SES computer control unit (CCU) **37**. The hose reel and dynamic tower hare an additional manual winding system for fail-safe backup. The dynamic tower is raised and lowered by electric motors built into the frame structure that alter the height of the dynamic tower and look the dynamic tower in place. The motors are controlled by the CCU **37**, which monitors data sent via structural sensory that are built into the dynamic tower (not shown) and the wind speed data from the wind turbine **2**. The structural sensors are standard industry bad sensor such as the SM63 made by Sensor Techniques Ltd. of Cowbridge, South Glamorgan, Wales, United Kingdom. If the wind speed reaches excessively high velocities, the tower will automatically lower to a safe operating height without the need to switch off the rotor drives, thereby enabling the SES to continue producing energy.

[0033] The pressurized fluid generated by the wind turbine rotor and hydraulic drive systems exits the hose reel and travels along a fixed hydraulic pipe **5** through a four-way electrohydraulic servo valve **9** to the ground-located hydraulic accumulators **10**. The valve **9** controls the flow of the pressurised liquid back and forth from the accumulators **10**. As the velocity of the prevailing wind continually changes, so does the rotational speed of the rotor blades. With the present invention, the problem of dealing with continually changing energy input is eliminated due to the use of inline hydraulic accumulators **10** that absorb the fluctuating energy levels store the excess energy, and supply a constant and controlled output to drive the generators.

[0034] The accumulator stores the hydraulic energy under pressure against an inert gas housed in the accumulator in a separate partition, and the increase in hydraulic pressure compresses the gas behind a diaphragm, piston or steel bellows which retains the energy as pressure for later release. The pressure exerted on the inert gas is then used to force the liquid back out of the accumulator and to either the remote ground-based electrical PMG's **15** or back to the wind turbine **2** to recover energy from the rotor braking system in extreme wind conditions. The hydraulic accumulator releases energy at a precise and constant pressure through the hydraulic line **5** and inline hydraulic filter **11** to the hydraulic motor **181** (Figure 21) that drives the PMGs **15**.

[0035] In general, before electricity can be parsed into an electricity transmission grid, it has to be balanced so as not to affect the energy transmission, In prior art system, the balancing of the electricity is usually done by expensive electrical systems that remove the spikes in power, to the present invention, the accumulators **10** store the spikes of energy and filter out the disruption that can be caused by the fluctuation of the energy production from the wind. This system enables energy to be retained and stored rather than lost by being earthed into the ground, which is what happens with prior art systems.

[0036] Each generator cluster houses multiple permanent magnetic generators (usually six per cluster), as shown in Figure 1, and these clusters are modular so that any number may be added to the SES system, A single hydraulic motor rotates a generator drive gear, which in turn drives a series of smaller gears attached to each generator to produce the electrical energy output, Each generator has an electromagnetic coupling that switches on or off depending on the hydraulic pressure received by the hydraulic motor. This enables a reduced number of generator to operate in low wind speeds and higher numbers of generators in high wind speeds. The PMGs **15** can be driven by numerous wind turbines enabling a wind farm to haye a single centrally located PMG assembly that houses numerous permanent magnetic generators powered by multiple wind turbines.

[0037] The direct current (DC) electrical energy is transmitted from the PMGs to an electrical junction control switch **18**. From here, the DC electrical energy output can be split to power more than one end user, In the example shown in Figure 1, the electricity is used to power a water desalination system **20** for the electrochemical mining of metals from Water-based slurry and to power a hydrogen electrolyzer **21** for the production of hydrogen from the desalinated water. Alternately, the electrical energy can be used for numerous applications, including, but not limited to, being fed directly into a power transmission grid **34**.

[0038] The water-based slurry **19** is made from mined ore that is broken down through series of crushers to particle sizes of approximately twenty (20) herons or less; the broken down ore is then added to water to create slurry. The slurry is pumped through a series of ion transfer modules, such as those manufactured by FET Group of Bristol, United Kingdom. The modules perform specific actions depending on the metals being mined and extracted through electrochemical ion transfer a specific material from the slurry in a single pass; the metals are then dried **23** and pat into separate compounds **24**. Some of the processes involved in the water desalination and metal, specially the process to remove alkaline metals, create hydrogen and

oxygen gases as a byproduct, and these two gases are stored under pressure in containers **26** and **35**.

[0039] The desalinated water then optionally passes through a hydrogen electrolyzer **21** to produce additional hydrogen. This process takes the energy required for the electrolysis process from the electrical junction switch **18**. The electrolyzer converts the water into hydrogen and oxygen, which are then pumped to the pressurized storage cylinders for hydrogen **26** and for oxygen **35**. The hydrogen from the pressurized storage cylinders **26** is pumped through a non-return valve **27** to a three-way valve **28** and directed to either a hydrogen fuel cell **29**, a tanker for shipping **30a**, or injected into a gas turbine **36** as a hybrid power source. The oxygen stored in the pressurized storage cylinders **35** can either be pumped via **44** to a gas turbine **36** as hybrid reserve power to the SES to improve burning efficiency of the natural gas or shipped out for commercial use **30c**. The desalinated water **22** can be further processed for drinking water, put back into the water system (river), or recycled and pumped back for the slurry process. The water could also be commercially shipped **30b**.

[0040] The hydrogen fuel cell **29** supplies energy when required through a three-way electrical switch **32** to the electrical junction switch **18** for use in the SES mining process should the wind energy be low or, if there is an increase of demand for electrical energy, elsewhere in the system. The energy from the fuel cell can also be fed directly into a power transmission grid **34** of demand. The energy can be converted from DC to AC before entering a transmission grid through a DC to AC converter **33**. The invention requires a single electrical DC to AC inverter **33** per system and not per wind turbine as with prior art systems. The three-way electrical switch **32** is controlled to distribute the electrical energy to an external transmission or end user either directly from the PMGs **15** or from the hydrogen fuel cell **29** or both.

[0041] The wind turbine decoupled rotor and drive of the invention enables additional hybrid energy systems **36** to be plugged into the hydraulic circuit through the hybrid variable displacement hydraulic pump **12** to drive the PMGs **15** when required. The hybrid power can come from any form of power supply, including solar, photovoltaic, geothermal, gas, steam, coal, hydrogen, fuel cell, diesel, oil and biomass. The hybrid power source drives the hybrid variable displacement hydraulic pump **12** to supply fluid to the hydraulic accumulators **10** to produce energy when the wind speed is low or an increase in energy is required.

[0042] A series of heat exchangers throughout the SES recover energy from the heat produced from anywhere in the system, including the electrical generators **16**, the hydrogen electrolyzer **41**, and the hydrogen fuel cell **31**. The heat exchangers convert the heat into steam that is pumped by **42** and **14** through pipe **45** into a steam generator **17** that powers the hybrid hydraulic pump **12**. The PMGs **15** have water jackets that remove excess heat created during operation and transfer the heat energy to the steam generator.

[0043] The SES has electrical sensors to monitor wind speed, wind direction, hydraulic operating and pump pressures, dynamic tower height and load stresses (vertical and horizontal), generator electrical output, accumulator energy reserves, mechanical operating temperatures, rotor speed, rotor shaft load and climatic conditions. The sensors are linked directly to the CCU **37** where the data is processed and stored before being fed back into the SES active units to adjust such elements as wind turbine direction and angle, dynamic tower height, and the number of hydraulic pumps or generators to activate. The CCU calculates the information and reacts accordingly to preset criteria. Specific information is sent and received by the SES via data communications **39** to allow reprogramming of software or to alert of an impending mechanical issue.

[0044] Figure 2 is a schematic diagram of an alternate embodiment of the present invention in which pneumatic power is used in lieu of hydraulic power. The pneumatic system shown in Figure 2 operates in much the same way as the hydraulic energy transmission, although it uses compressed air storage **58** to balance and store the excess energy. The wind energy **1** is harvested through the wind turbine **2**. In Figure 2, the wind energy is converted into pneumatic energy rather than hydraulic via multiple air compressors housed in the wind turbine in lieu of the hydraulic pumps of the first embodiment. The air compressors are connected to the two rotor drives through the same electromagnetic couplings used in the hydraulic version of the wind turbine **2**.

[0045] The compressed air passes from the wind turbine and through pressurized pipe **55** and through an air dryer **56** to remove moisture from the system. Once it has travelled through the dryer **56**, the compressed air passes through a dividing valve **57** to split the air into numerous high-pressure air storage vessels **58**. The high-pressure air storage vessels **58** balance the energy produced and store the excess energy produced in the form of air pressure ready for controlled pressure release through air release valves **59**. The pressurized air passes through a one-way valve **60** and through a second dividing valve **61** to drive high-speed pneumatic motors **62**. The high-speed pneumatic motors **62** power the generators to produce the electricity. The excess heat is recovered from the pressurized air through heat exchangers in the SES and through the hybrid-driven compressor **53** through heat exchanger **54**. This excess heat is converted into steam and piped through a two-way pipe **52** to power a steam generator **17**. The energy created by the steam generator **17** is used to drive the hybrid variable displacement hydraulic pump to provide additional energy for the SES.

[0046] Figure 3 is a front perspective view of the ducted diffuser multiple rotor wind turbine and dynamic tower of the present invention. This figure shows the ducted diffuser multiple rotor wind turbine **2** and dynamic tower **3** at the highest point setting of the dynamic tower **3** with the wind turbine forward facing into the prevailing wind. The separate stages of the telescopic dynamic tower **3** are also shown. Because the rotor blades of the wind turbine **2** are enclosed and not an open rotor or propeller, they produce a small radar footprint, which makes the present invention particularly suited for installations close to radar installation. The removal of the gearbox from the energy system and the fact that the generators are located at ground level means that the present invention is less likely to attract lightning strikes than conventional wind turbines.

[0047] Figure 4a is a front perspective view of the ducted diffuser multiple rotor wind turbine of the present invention. The cowling **80** creates a Venturi jet effect through the steep incline interior surface shape of the cowling **80**, which works against the outer shape of the cowling. The narrowing of the internal surface accelerates and compresses the air passing through the wind turbine to provide an increase in energy when compared to an open rotor wind turbine of comparable size. The cowling **80** stabilises the wind speed and consistency over an open rotor wind turbine. Below is the Venturi flow rate formula:

$$Q = A_1 \sqrt{\frac{2(p_1 - p_2)}{\rho \left(\left(\frac{A_1}{A_2} \right)^2 - 1 \right)}} = A_2 \sqrt{\frac{2(p_1 - p_2)}{\rho \left(1 - \left(\frac{A_2}{A_1} \right)^2 \right)}}$$

[0048] The airflow enters through the front of the wind turbine **2** and through the air guides **82**. The air guides direct and straighten the airflow through the front section of the wind turbine and into inner rotor blades **83**, which rotate inside the cowling **80** at the point of highest air pressure and velocity. The inner rotor hub **85** of the wind turbine houses the wind turbine drive mechanism, and the aerodynamically shaped lower support **86** connects the turbine to the dynamic tower **3** (not shown). The air flow, which travels around the outside of the cowling **30** and under the diffuser **81**, is drawn onto counter - rotating outer rotor blades **84**.

[0049] The counter-rotating outer rotor blades **84** achieve three objectives: first, they remove wind energy from the airflow around the outside of the cowling **80**; second, they create an area of low pressure behind the wind turbine; and third, they reduce vibration and asymmetrical torque effect and improve wind direction stability by rotating in opposite direction to the inner rotors **83**. The diffuser **81** deflects the airflow away from the rear of the wind turbine to create an area of low pressure behind the wind turbine. The area of low pressure at the rear of the wind turbine draws the air through the wind turbine cowling **80** from the high pressure area at the front of the wind turbine. The air accelerating from the high pressure at the front of the wind turbine and through the inside of the cowling **80** compresses the air. It is the combination of the air compression and increased air speed that enables the wind turbine to exceed Betz's Law. Because of the combination of the wind turbine **2** aerodynamic cowling **80**, the diffuser **81** and the outer rotor **84**, the air speed that reaches the inner rotors **83** can be over three times the wind speed.

[0050] The wind turbine **2** has four wind speed sensors **88** and **89** located on the outside of the front of the cowling **80**. The wind speed sensors work in two pairs on adjacent sides of the cowling-the two of the horizontal level **88** are one pair, and the two on the vertical plane **89** are the other pair. The wind speed sensors are monitored by the CCU **37** (see Figure 1), which compares the wind speed registered by each one of the sensors in each pair. The CCU compares the two sensors **88** on the horizontal plane, and if one sensor is showing a highest wind speed than the other, the wind turbine is turned via the three-dimensional yaw control **143** (see figure 15) towards the wind speed sensor recording the lower wind speed (*i.e.* left to right or right to left). The software algorithm that processes the wind speed data removes wind gusts from the data, and the mean wind direction is calculated to hold the wind turbine in position and to stop continual direction hunting from left to right.

[0051] The vertical pair of wind speed sensors **89** (top and bottom locations) are controlled in exactly the same process as described for the wind speed sensors **88** except that the field of movement is up and down rather than left to right. The wind sometimes moves at angles rather just parallel to the ground, especially around objects such as buildings or on hills. Through the use of horizontal and vertical sensors, the invention controls the direction and angle of the wind turbine in a three-dimensional plane and is better able to accommodate wind moving at an angle to the ground than prior art systems that move the turbine in only two dimensions (left and right). Open rotor wind turbines used in wind farms rely on a low number of weather stations in front of the wind farm to determine wind direction and turn all of the wind turbines towards the data received by the weather station, which can be over a mile away. In the present invention, each wind turbine is optimized individually to its own space in a three-dimensional environment without the need for weather stations, radar or sonar devices.

[0052] Figure 4b is a rear perspective view of the ducted diffuser multiple rotor wind turbine cowling **80** and diffuser **81** of the

present invention. As shown in this figure, the exhaust of the cowling **80** and diffuser **81**, where the air exits the wind turbine, is of a larger diameter than the that nit the inlet at then front of both the cowing **80** and diffuser **81** (see Figure 4), where the air enters the wind turbine. This difference in size between the exhaust and the inlet generates a low-pressure area at the rear of the wind turbine. The four structural staves **87** at the rear of the wind turbine support the diffuser **81** and the cowling **88**.

[0053] Figure 5a is a from perspective view, and Figure 5b is a rear perspective view, of the present invention with two sets of internal rotors **83**, **95**. The rear inner rotor blades **195** are positioned directly behind the front inner rotor blades **83** and capture energy from the air that passes through the inner rotor blades **83**. Approximately thirty percent (30%) of the wind energy that hits the front inner rotor blades **83** remains available after the wind has passed through the front inner rotor blades **83**, and the remaining energy is used to rotate the rear inner rotor blades **195**. The wind energy that rotates the rear inner rotor blades **195** is captured in the same manner as for the front inner rotor blades **83**.

[0054] The rear inner rotor blades **195** are counter-rotating rotors, which mean that they notate in the oppose direction as the front inner rotor blades **83**. When there low wind speed, the mass of the air flowing through the inner rotor blades usually causes a tangential or rotational air flow to be created by the spinning blades. The energy or this tangential pair flow is wasted in a single-propeller design. The placement of a second propeller behind the first takes advantage of the disturbed airflow. The tangential air flow can cause the wind turbine to yaw left or right, depending of the direction of rotor rotation.

[0055] The rear inner rotor blades **195** counter the asymmetrical torque effect of the front inner rotor blades **83**. Counter-rotating propellers can be up to sixteen percent (16%) more efficient than normal propellers. The rear inner rotor blades **195** shown in Figure 5a have the same number of rotor blades as the front inner rotor blades **83**, but the number of rotor blades in the front and rear sets of rotor blades may vary. For example, there could be five rotor blades on the front inner rotor blades **83** and six rotor blades on the rear inner rotor blades **195**.

[0056] The installation of the rear inner rotor blades 195 is optional and would have considerable benefits in areas of very high wind speeds that average over thirty-five miles per hour. The use of the rear inner rotor blades 195 would enable smaller and stronger diameter wind turbines to be used to extract the energy from the higher wind speeds, and the system would still have benefits at low wind speeds.

[0057] Figure 6 is a aide elevation view of the ducted diffuser multiple rotor wind turbine of the present invention. As shown in this figure, the diffuser **81** is positioned around the cowling **80** with the front of the diffuser **81** extending approximately half the length of the cowing from the front of the cowling **80**. The figure clearly illustrates the comparative size differential between the inlet and outlets of the wind turbine.

[0058] Figure 7 is a front view of the ducted diffuser multiple rotor wind turbine of the present invention shown without the dynamic tower. This figure shows the cowling **80** and the diffuser **81** with the wind turbine tower support **86**.

[0059] Figure 8 is a side elevation cross-section view of the wind turbine of the present invention illustrating how air flows through the wind turbine. This figure illustrates the airflow through the wind turbine and the acceleration of air through the cowling **80**. The wind **1** enters through the front of the wind turbine **80**. The inner surface **197** of the cowling **80** illustrates how the inside diameter of the cowing decreases quickly to form an inlet shape that curves in a smooth, deep incline before leveling out at the point where the inner rotor blades **83** are located. The inside diameter of the cowling **80** then gradually increases to the rear or exhaust of the cowling **192**. The exhaust **192** of the cowling **80** has a larger diameter aperture than the inlet aperture **191**; the larger the diameter of the exhaust, the quicker the air dissipates from the wind, turbine, thereby creating a low-pressure area. The low-pressure area at the rear of the turbine works with the aerodynamics of the cowling **80** and the diffuser **81** to create the suction through the center of the wind turbine cowling.

[0060] The outer surface **196** of the cowling **80** has a reduced curve in the opposite direction to the inner surface **197** of the cowling **80**; the outer curved surface **196** increases the air speed traveling through the inside of the cowling **80** and into the inner rotor blades **83**. The acceleration in the air speed through the cowling **80** increases the energy available to be taken from the wind by the inner rotor blades **83**. The air speed decreases once it has passed through the inner rotor blades **83** because a large proportion of the energy has been removed by the rotor blades and transferred into the drive system of the wind turbine. The reduction in wind energy at the rear of the wind turbine **192** cremates an area of lower air pressure than at the front of the wind turbine **191**, and this differential in air pressure sacks the air through from the front to the rear. An additional set of rear inner rotor blades **195** can be installed behind the inner rotors **83** toward the rear of the wind turbine to extract further energy from the wind. The rear inner rotor blades **195** are preferable in high wind velocity areas where a smaller rotor system is advisable due to the rotational stresses applied to a larger rotor blade in very high wind speeds.

[0061] The diffuser **81** guides the airflow at the rear of the wind turbine out and away, which has the effect of pulling the exiting air from the cowling outwards **80**. Because, the air speed is faster over the outer edge of the diffuser **81** than at the rear of the cowling **80**, the slower air is pulled away from the back of the wind turbine to further reduce the air pressure at the rear. There is a gap between the leading edge **198** of the outer diffuser **81** and the outer surface **196** of the cowling **80** through which air passes. The counter-rotating outer rotor blades **84** use the energy from the air passing through this gap to rotate, and this energy is then harvested by the energy transmission system. The removal of the wind energy by the outer rotor **84** increases the effect of the diffuser **81** and helps to reduce the air pressure at the rear of the wind turbine **192**, thereby increasing the pressure differential between the front and the rear of the wind turbine. The outer rotor blades **84** rotate in the opposite direction to that of the inner rotor blades **83** to reduce the asymmetrical torque effect and vibration.

[0062] The tips of each set of rotor blades **83** and **84** rotate within a distance of less than two inches from, the inner surface **197** of the cowling **80** (in the case of the inner rotors **83**) or the diffuser **81** (in the case of the outer rotor **84**). A traditional open rotor system or propeller loses energy from the tips of the blades as the energy is deflected up and away, whereas the motor blades in the present invention retain this energy. The ducted rotor system of the present invention reduces noise levels over an open rotor wind turbine due to the encapsulated environment created by the cowling **80** and the diffuser **81**.

[0063] Figure 9 is a schematic operating diagram of the wind turbine hydraulic drive system based in the wind turbine **2** of the present invention. This figure illustrates how the present invention converts the wind energy extracted by the inner rotor blades **83** and transmits that energy via a pressurized fluid for further conversion into electricity. The wind energy passing through the wind turbine causes the inner rotor blades **83** to rotate. The energy exerted in this rotation is removed from the wind and passed down the first drive shaft **113** connected to the rotor hub. The first drive shaft **113** routes a first gear **90** inside the of the wind turbine. Connected to the first gear **90** are numerous first hydraulic pumps **92** that pump a pressurized liquid through a high-pressure hydraulic circuit. Each of the first hydraulic pumps **92** is connected to the first gear **90** through the first electromagnetic coupling **96a**, **96b**, which switches the pumps on or off depending on the information received by the first electromagnetic couplings **96a**, **96b** from the PCU **99**, as described in connection with Figure 1.

[0064] The PCU processes information received from either a driveshaft speed or a torque sensor **93** on the drive shaft **113** and/or from the hydraulic pressure and evaluates whether to switch the pump on or off. With the first electromagnetic coupling **96a** switched on and the second electromagnetic coupling **96b** switched off, the first gear **90** rotates without the drag of the variable displacement hydraulic pump **92** on the hydraulic system, which enables a greater percentage of the wind energy captured to be used for energy conversion. The PCU also controls the first and second electronic shutoff valves **94a**, **94b**, which open and close in line with the first and second electromagnetic couplings **96a**, **96b**, so that the variable displacement hydraulic pumps **92** become isolated to reduce pressure losses throughout the hydraulic system. The first and second electromagnetic couplings **96a**, **96b** are connected to the PCU, which controls not only the switching on and off of the electromagnetic couplings but also the speed and force at which the individual electromagnetic couplings are activated.

[0065] The benefit of this design is that each variable displacement hydraulic pump can be introduced into the system gradually as the electromagnetic coupling can be slipped in the same way that a torque converter would on a gearbox. This design eliminates any sudden increase in hydraulic pressure into the system, thus protecting hydraulic seals and pipes from mechanical failure. The hydraulic fluid then passes through an electrohydraulic servo valve **9** and a hydraulic actuator **98** to control the fluid pressure and dampen the fluctuating pressure from the pump. The system is protected through pressure release valves **97** on either side of the actuator **98**.

[0066] In high wind speeds, the PCU **99** will activate a high number of the hydraulic pumps to maximize the energy extracted from the wind. The variable displacement hydraulic pumps can work individually or in clusters; for instance in large wind turbines of one megawatt (MW) output, the hydraulic pumps would work in six clusters with four pumps in each cluster and each cluster connected to a separate hydrate line. The hydraulic lines **100** exit the wind turbine and extend down the dynamic tower through a centrally portioned coupling.

[0067] The first and second electromagnetic couplings **96a**, **96b** are separated from the hydraulic pumps **92** by a four-millimeter gap of air and do not have a mechanical connection. This eliminates the vibration that is usually created through a direct driveline and parsed into the bearings and seals. The vibration in a typical open rotor wind turbine can load to the breakdown of major driveline components such as the gearbox and generator through bearing and seal breakages and excessive heat generation. In the present invention, the decoupled hydraulic drive (the hydraulic drive is decoupled in the sense that the rotors can turn without driving the generators, and the generators work without having to turn the rotors) and electromagnetic couplings eliminate these problems while gaining operational efficiency and energy output.

[0068] Figure 10 is a front perspective view of the center of the wind turbine frame and drive shown without outer cladding or body panels. As shown in this figure, the wind turbine is constructed from a tubular space frame **117** that creates a strong and light support structure that is simple to repair or maintain. The inner rotor blades (see Figure 4, reference number **83**) bolt into the rotor hub **110** through the separate rotor blade attachment housing **111**. The rotor hub **110** is preferably constructed from metal or carbon composites. The rotor hub **110** is attached to a steel or carbon composite first drive shaft **113** that rotates with the rotor blades when the wind blows, thereby driving the large gear **90**. The rotating gear **90** drives a series of electromagnetic couplings **96a, 96b**, which in turn drive the hydraulic pumps **92** (not shown) to transmit the energy from the rotor blades. The disc brake **112** is attached to the first drive shaft **113** and is used to slow the drive shaft rotation under extreme conditions or to lock the drive shaft still during maintenance. The PCU **99** controls the activation of the hydraulic pumps, the yaw control for the rotor blades (not shown), and the disc braking system.

[0069] Figure 11 is a rear perspective view of the center of the wind turbine frame illustrating the drive system shown without outer cladding or body panels for clarity. This view shows the location of the hydraulic pumps **92** and the directional shut-off valves **94a, 94b**. The first drive shaft **113** bolts onto the rotor hub **110** and is supported by the two large bearings **120** and **121**.

[0070] Figure 12 is a perspective view of a section of the outer rotor system of the present invention. The outer rotor **84** is constructed in sections for easy transportation and on site assembly. The outer rotor assembly **131** rotates around the cowling **80** on roller bearings **133** built into the assembly **131**. The outer rotor blades **84** are attached to the outside of the assembly. Attached to the outer rotor assembly is a ring gear **132** that drives an outer rotor drive gear **199** and the second drive shaft **134**. Attached to the end of the second drive shaft **134** is the second gear **135**, which drives a series of second electromagnetic couplings **136** that are individually connected to the variable displacement hydraulic pumps **92**.

[0071] The second electromagnetic coupling **136** and variable displacement hydraulic pumps **92** operate in the same way as the inner rotor drive described in Figure 9. If the wind velocity is low, only one hydraulic pump will be activated, and in high wind velocities, all of the variable displacement hydraulic pumps **92** will be activated. The pressurized fluid enters and exits through the high pressure hydraulic pipes **45**. Because the second electromagnetic couplings **136** do not drive the variable displacement hydraulic pumps **92** through a mechanical connection, little or no vibration is carried through the wind turbine. The reduction in vibration improves reliability and reduces maintenance.

[0072] Figure 13 is a front perspective view of the dynamic tower **3** and the wind turbine **2** of the present invention shown in a raised position. The dynamic tower **3** is an automated motorized active or dynamic telescopic tower that automatically adjusts the height of the wind turbine **2** depending upon operational conditions or requirements determined by the PCU **99**, which monitors the conditions through sensors on the dynamic tower **3** and the wind turbine **2**. The dynamic tower **3** uses built-in, high-power DC motors (shown in Figure 18) to power the electromagnetic drives (**160** in Figure 18) to raise and lower the dynamic tower and also to lock the dynamic tower in position. Sensors for vertical and horizontal loads measure the stress being applied to the dynamic tower, and speed sensors monitor the rotational speed of first gear **90** and second gear **135** (not shown). These sensors send information to the CCU **37**, which acts on the information (together with additional information from the wind turbine such as rotor speed) according to preprogrammed criteria.

[0073] If the load sensors in the dynamic tower **3** detect movement in the dynamic structure due to high, wind speeds or excessive rotor speed from the wind turbine, then the dynamic tower **3** will automatically lower to a safe operating height for either load stress or wind speed so that the wind turbine can continue to operate rather than switch off and cease energy production, as open rotor wind turbines do. The dynamic tower enables the wind turbine **2** to be assembled at a low level and then raised once the assembly is complete without the need for large cranes. The dynamic tower can be lowered for routine maintenance, which is considerably safer and more economic than maintenance procedures currently employed with open wind turbines.

[0074] Figure 13 shows the dynamic tower **3** fully extended with the base of the dynamic tower **3** sunk in to the ground **140**. In this illustration, the dynamic tower **3** is shown without a cover or cladding. Each section of the dynamic tower is preferably fabricated from steel, although it is also possible to use carbon composite materials, which are especially suited to mobile or temporary applications and installations close to radar systems because they reduce the radar interference. The dynamic tower **3** construction is hexagonal in shape, and all of the sections fit tightly together to add strength to the construction while maintaining ease of build.

[0075] Figure 14 is a front perspective view of the dynamic tower **3** and wind turbine **2** of the present invention shown in a lowered position. This figure clearly shows the height differential between the extreme raised and lowered positions.

[0076] Figure 15 is a detail perspective view of the below-ground installation of the dynamic tower in the lowered position shown with the wind turbine yaw control **143** and hydraulic pipe winding device **144**. The dynamic tower raises and lowers through a

dynamic tower electromagnetic drive (see Figure 18, reference number **160**) and drive rail **141** that are integrated into each individual section of the dynamic tower **142**. The dynamic tower has an integrated three-dimensional yaw control **143**, which aligns the wind turbine **2** onto the mean direction of the wind. By integrating the yaw control into the tower, the manufacturing and assembly of the SES becomes considerably easier and safer than an open rotor wind turbine, which has the yaw control separate from the tower.

[0077] When the dynamic tower is lowered, the hydraulic hose used in the SES energy transmission is wound automatically onto a reel **144** located at the base of the dynamic tower structure **3**. (In an alternate embodiment, the reel **144** is located above ground.) The reel **144** is motorized and works in conjunction with the dynamic tower electromagnetic motor drive (see Figure 18, reference number **160**) to synchronize the movement of the dynamic tower. A manually operational service panel **145** is located next to the base of the dynamic tower to enable the dynamic tower to be operated manually during maintenance and installation procedures. The manually operational service panel contains a manual override and electrical power point so that an external power source can be added to power the dynamic tower electromagnet drive system during maintenance or repair.

[0078] Figure 16 is a front perspective view of the dynamic tower **3** installed on the surface of the ground through the use of steel cables **146** and a platform base support **147**. This figure shows the dynamic tower **3** in the lowered position; the installation is above ground in this example for use as a temporary installation or on contaminated ground. The tower is held in place through the use of steel cables **146** and a wider platform base support **147**, and the hydraulic hose reel **144** and manually operated service panel **145** are installed on the surface of the ground. The steel cables **146** support the dynamic tower and are pinned to the ground with steel slakes **148**.

[0079] Figure 17A is a perspective view of the three-dimensional yaw control system of the present invention with the facing panels removed to illustrate the two drive systems. The three-dimensional yaw control is integrated with the dynamic tower **3** to position the wind turbine into the mean direction of the wind on both horizontal and vertical planes. The main components of the three-dimensional yaw control are a yaw bearing **150**, which rotates the wind turbine left or right, and a central horizontal platform **153** to tilt the wind turbine forward or backward, as shown in Figures 17B and 17C. For the horizontal movement (left and right), a series of electric yaw horizontal drive motors **151** are attached to a horizontal yaw ring gear **157** inside the three-dimensional yaw control system. When power is supplied to the electric yaw horizontal drive motors **151**, they rotate the three-dimensional yaw control left or right via a horizontal yaw drive gear **156**, which turns the system by driving on the horizontal yaw ring gear **157**. When the electrical power is removed from the electric yaw horizontal drive motors **151**, they become fixed in place and act as the braking mechanism to hold the wind turbine in place. This system enables precise positioning of the wind turbine to obtain the optimum wind speed and direction. The drive and positioning can be done with the use of hydraulics in place of the electrical system described.

[0080] The vertical positioning of the wind turbine is controlled by the vertical yaw drives **156**, which are incorporated within the structure **154** and are connected to the drive rail **153** on the platform **152**. The vertical yaw drives **155** tilt the yaw control platform up or down by driving the curved yaw tilt rail **153**. As the vertical yaw drives **155** rotate on either side of the structure **154**, the vertical yaw drives **155** lock into the drive rail **153** on the platform **152** to tilt the angle of the wind turbine (see Figure 3, reference number **2**). The vertical yaw drives **155** (see Figure 18) lock in place and act as the holding brake when the electrical power is removed, thereby acting as a safety mechanism and saving on energy usage. The position of the wind turbines is determined by the CCU (see Figure 1, reference number **37**), which receives data from wind speed sensors **88** and **89** (see Figure 4) that provide the mean wind direction and remove the intermittent gusts of wind. In this manner, the position of the wind turbine can be fine-tuned in a three-dimensional field to extract the optimum available wind energy.

[0081] In a wind farm where multiple wind turbines are positioned close together, the efficiency of the wind farm is enhanced because each wind turbine is individually optimized to the wind conditions local to the wind turbine rather than all of the wind turbines working from a central wind data point. The three-dimensional yaw control of the present invention has considerable benefits in urban areas and on skyscrapers where the wind becomes turbulent. The air exiting the wind turbine can be directed up or down, enabling the wind turbines to be grouped closer together.

[0082] The three-dimensional yaw control system of the present invention controls the wind flow through the wind turbine. (see Figure 3, reference number **2**) to extract the maximum wind energy available, and it also controls the wind speed through the wind turbine in extreme wind speeds by either tilting or turning the wind turbine away from the prevailing wind to reduce the speed of the wind reaching the rotor blades. The ability to control the angle of the wind turbine against the prevailing wind, combined with the ability of the CCU (see Figure 1, reference number **37**) to control the height of the dynamic tower (see Figure 3, reference number **3**), enabled the SES to operate in very high wind speeds angling the wind turbine into the wind without the need to brake and stop the rotors from turning to avoid damage to the wind turbine. Open motor wind turbines would usually cease rotating in

wind speeds of fifty-five (55) miles per hour, whereas the present invention will operate in wind speeds up to eighty (80) miles per hour.

[0083] Figure 17B is a perspective view of the wind turbine **2** of the present invention tilted forward on the three-dimensional yaw control system at an angle of ten degrees (10°) **193**. Figure 17C is a perspective view of the wind turbine **2** of the present invention tilted backward **194** at an angle of ten degrees (10°). The wind turbine **2** can be tilted up to an angle of thirty-five degrees (35°) in either direction, up or down.

[0084] Figure 18 is a perspective view of the dynamic tower drive system used to raise and lower the dynamic tower during operation. The dynamic tower (see Figure 3, reference number **3**) is assembled in a number of sections **142** with each section **142** fitting inside the lower section of the dynamic tower. Incorporated within the hexagon frame of the dynamic tower are a series of electromagnetic drives **160** that control the movement of each section of the tower. The electromagnetic drives **160** work in pairs on opposite sides of the hexagonal frame structure, and each hexagonal section **142** has a dynamic tower electromagnetic drive **160** and a dynamic tower roller guide **164**, which is the same as the dynamic tower electromagnetic drive but without a power drive. Each lifting section **142** of the dynamic tower has at least two pairs of electromagnetic drives **160**, each pair being capable of lifting the designed lift capability of the dynamic tower section **142**. There are two electrical circuits per dynamic tower, and each pair of electromagnetic drives **160** per lower section operates off either of the two electrical circuits so that failure to one electrical circuit still enables the dynamic tower to operate.

[0085] The dynamic tower electromagnetic drive gear **160** locks into the drive rail **141**, and as the electromagnetic drive rotates, it moves the dynamic tower section **142** either up or down. The electromagnetic drive **160** is also the braking mechanism for the dynamic tower. Without an electrical supply the electromagnetic drive gear **160** locks in place and only becomes operational with electrical power, which means the dynamic tower automatically locks if all power is lost.

[0086] Figure 19 is a detail interior view of the dynamic tower electromagnetic drive **160** of the present invention. This figure shows the electromagnetic drive **160** with the high-power DC motor **162** installed in the dynamic tower **142**. The DC motor **162** is fitted in the frame structure of the dynamic tower and is accessible through panels on either side of the tower frame. The DC motor **162** drives the electromagnetic drive gear **160** through a bevel gear **163** to take the output from a vertical axis to a horizontal axis. The electromagnetic drive **160** is recessed into the frame of the structure and only protrudes out of the frame to link into the drive rail **141** (see Figure 18). This configuration enables each section of the dynamic tower **142** to fit securely inside the section immediately below, thereby eliminating any lateral movement from the dynamic tower section **142**.

[0087] Each set of electromagnetic drives is capable of operating the dynamic tower movement. When the electrical current is switched off, the electromagnetic gear drive automatically locks in position to hold the dynamic tower in place, which acts as a safety mechanism and saves energy when the height of the tower does not need to be adjusted.

[0088] In addition to the electromagnetic drive **160** and DC motor **162**, each section of the tower has roller gears that keep the sections of the tower tight against the inserted telescopic section inside and provide strength in the tower mast similar to a rigid unit. The roller gears are the same as the electromagnetic gear drive **160** but without the DC motor **162** to power the gear in movement. As with the dynamic tower electromagnetic drive, the roller gears lock when the electrical power supply is removed to hold the mast in position. Both of the electrical circuits in the dynamic tower have a plugin backup system at the base of the tower through the manually operational service panel **145** (see Figure 15) that can be used by trained maintenance personnel to release the electromagnetic lock for repair and general maintenance.

[0089] Figure 20 is a perspective view of the permanent magnet generator **15** of the present invention shown in vertical orientation with a water jacket and PMG electromagnetic coupling **172**. As shown in this figure, a single PMG **15** is used to turn the wind energy into a high-voltage direct current electrical output. The PMG **15** operates in clusters of identical generators that switch on and off individually as and when the demand is required. In a preferred embodiment, the PMG **15** is a 200-kilowatt version that measures one meter twenty centimeters (four feet) in height and 15 centimeters (six inches) in diameter and weighs 200 kilograms (440 pounds). The total weight of the PMG **15** for a 2-MW wind turbine is two tons compared to thirty (30) tons for a standard induction generator used in an open rotor wind turbines. The PMG **15** can be manufactured in output capacity from ten kilowatts to multiple megawatts.

[0090] The PMG **15** is driven by a generator drive gear **171** at the top of the assembly that is turned by either a hydraulic or pneumatic motor at a set geared speed of 5000 rpm. The generator drive gear **171** turns the PMG electromagnetic coupling **172**, which turns the generator enclosed in the PMG **15** outer casing and water jacket. The PMG electromagnetic coupling spins the drive in the PMG **15** without a direct mechanical linkage, which significantly reduces the vibration carried through a drive system and enables the generator to be detached from the gear drive **171** when required. The electricity generated by the PMG is

transmitted through the electrical table **173** at the bottom of the generator,

[0091] In operation, the PMG **15** generates heat from the mechanical movement, as is true of any similar generator. The PMG **15** has a water jacket incorporated in the casing of the FMG **15** that cools the generator by passing a cool liquid around the outside of the heat-producing mechanical components. The cool liquid enters the PMG **15** through the inlet connector **175** and exits the system through the outlet connector **174**, where the now hot liquid is passed through a heat exchanger to remove the heat energy and recycle the liquid back through the water jacket incorporated within the casing of the PMG **15**. In this manner, the heat energy extracted by, the heat exchanger is recovered back into the SES system. The PMG **15** is installed into a frame and anchored, in position via the fixing plate **176**.

[0092] Figure 21 in a perspective view of the modular generator cluster and hydraulic drive system of the present invention shown with an installation frame. This figure illustrates how a cluster of multiple PMGs **15** operates and how the individual PMGs are fitted into the generator cluster frame **185**. In this example, the PMGs are driven by a single large hydraulic motor **181** at the top of the generator cluster frame **185**,

[0093] The hydraulic motor **181** rotates the generator cluster drive gear **180** on the underside of the top action of the frame **185**. The generator cluster drive gear **180** spins and in turn rotates the PMG generator electromagnetic couplings **172** at the top of the PMG **15**. The CCU (see Figure 1, reference number **37**) monitors the hydraulic pressure at the hydraulic motor **181** and calculates how many of the PMGs **15** can be activated to generate electricity. The CCU switches the individual PMG electromagnetic couplings **172** on or depending on the available hydraulic pressure. When the electromagnetic coupling **172** is switched off, the drag or friction from the PMG **15** is removed completely from the drive system to improve the efficiency of the energy output from the available hydraulic pressure. When the Available energy to drive the generators is low, the CCU activates a small number of generators, and when the available energy is high, the CCU activates all of the PMGs in the cluster.

[0094] The PMG switching system enables the individual generators **15** to be replaced or serviced without the need to shut down the SES, thereby avoiding any down time. The generator cluster frame **185** is designed to allow any individual generator to be removed any replaced as quickly as possible. Each PMG **15** has a separate retaining bracket **186** that is held in place by two bolts, and the bottom of the PMG **15** is bolted to the lower section of the frame **187**. The PMG cluster is designed to be modular so that additional units may be added or subtracted as energy demand is increased or decreased.

[0095] Prior art large wind turbine of 500 kilowatts to three megawatts in size generally produce their optimum energy output at a wind speed of 35 miles per hour. Once the wind turbine reaches its optimum operating speed, it will then produce the same electrical output up to the wind speed at which it switches off, which is generally between 50 and 55 miles per hour in the case of a 3-MW wind turbine, so that a 3-MW wind turbine produces 3MW at 35 miles per hour and 3MW aft 50 miles per hour. The present invention does not cease to produced excess energy at any given wind speed; instead, it produces at higher electrical output at higher wind speeds. For example, the wind turbine of the present invention will produce three megawatts of electrical output at a wind, speed of 35 miles per hour, six megawatts of electrical energy at 45 miles per hour, and 12 megawatts of electrical energy at 55 miles per hour. This is because the present invention does not require the rotor blades to be braked or slowed down until the wind speed is in excess of fifty-five (55) miles, per hour and also because the SES uses multiple generators to capture all of the available wind energy. Because the available energy from the wind increases by two-fold with each 10-mile-per-hour increase in wind speed, a prior art wind turbine that produces three megawatts at thirty (30) miles per hour should produce six megawatts at forty-five (45) miles per hour but actually only produces three megawatts. This means that prior art wind turbines can waste as much energy as they produce in wind speeds above forty (40) miles per hour.

[0096] At the top of each frame are four lifting hooks **182** to allow complete generator clusters to lifted and moved. Because the high-voltage direct current generators are decoupled from the wind turbines, they can be driven by additional forms of power such as photovoltaic, natural gas or coal.

[0097] Figure 22 is a schematic diagram of the bat deterrence system of the present invention. Bats are frequently killed by open rotor wind turbines either from colliding with the rotor blades or flying into the area of low pressure behind the rotor blades. The sudden drop in air pressure can cause the lungs of the bat to collapse, killing the animal. A bat uses echolocation to navigate by emitting ultrasonic sounds that bounce off solid objects to create an echo. By comparing the outgoing pulse with the returning echo, the bat's brain and auditory nervous system produce an image of the bat's surrounding, for navigation Each bat produces its own unique sonic pulse signal that allows it to identify its own signal even in a cave containing thousands of other bats.

[0098] The bat deterrence system shown in Figure 22 is preferably attached to the areas of the turbine **2** that bats need to avoid (specifically, the tear areas of the turbine **2**). This system captures the bat's unique signal and fires it back at the bat, making it

believe that there is a large solid object in its immediate path and it must change direction to avoid it. The signal can be delayed and timed to go in between the natural reflecting pulses of at, existing solid object (such as the wind turbine) to make the object appear closer to the bat or simply tired back in rapid succession to make an empty section of air appear solid to the bat. In this manner, the area of low pressure behind the wind turbine can be kept clear of bats to avoid harm falling upon the animal.

[0099] The unique sonic bat signal **200** is received by the microphone **201** and passed through a pre-amplifier **202** to boost the signal. The signal is then passed though a low-pass filter **203** to remove unwanted frequencies, leaving only the bat sonic frequencies, before being converted from an analog signal into a digital signal **204**. A digital sound processor **205** amends the signal to the required output (in this example, to make the bat believe the empty low-pressure ares behind the turbine is solid) before passing it through a digital-to-analog converter **206** to turn the signal back into an analog sound. The sound is then put through an amplifier **207** to boost the signal ready for transmission through the speaker **208**. The bat deterrence system can be used in any application than has a requirement to keep bats away from a location without inflicting harm on the bats.

[0100] Although the preferred embodiment of the present invention has been shown and described, it will be apparent to those skilled in the art that many changes and modifications may be made without departing from the invention in its broaden aspects. The appended claims are therefore intended to define the scope of protection.

REFERENCES CITED IN THE DESCRIPTION

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P A T E N T K R A V

1. Vindenergisystem, omfattende

- 5 (a) en vindturbine (2), der omfatter en motorskærm (80) omgivet af en diffusor (81);
- (b) en flerhed af første indre rotorblade (83), der er placeret inde i motorskærmen (80), hvor flerheden af indre rotorblade (83) roterer om et første indre rotornav (85);
- 10 (c) en flerhed af ydre rotorblade (84), der er anbragt mellem diffusoren (81) og motorskærmen (80), hvor flerheden af ydre rotorblade (84) roterer modsat i forhold til flerheden af indre rotorblade (83), og hvor de ydre rotorblade (84) er fastgjort på ydersiden af en ydre rotorindkapsling (131), der roterer om motorskærmen (80) på rullelejer (133), der er indbygget i
- 15 indkapslingen (131);
- (d) en drivmekanisme, der er placeret inde i det indre rotornav (85);
- (e) et dynamisk teleskoptårn (3);
- (f) og en tårnstøtte (86), der forbinder vindturbinen (2) med det dynamiske teleskoptårn (3).

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2. Vindenergisystem ifølge krav 1, der endvidere omfatter en flerhed af luftstyringer (82), der er placeret inde i motorskærmen (80) og foran de indre rotorblade (83).

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3. Vindenergisystem ifølge krav 1, der endvidere omfatter to horisontale vindhastighedssensorer (88) og to vertikale vindhastighedssensorer (89), der er beliggende på en ydre flade af motorskærmen (196) foran diffusoren (81), hvor de to horisontale vindhastighedssensorer (88) er beliggende over for hinanden på et horisontalt plan, og de to vertikale vindhastighedssensorer (89) er beliggende

30 over for hinanden på et vertikalt plan.

4. Vindenergisystem ifølge krav 1, hvor motorskærmen (80) og diffusoren (81) hver især omfatter en udstødning med en indre diameter og en indsugning med en indre diameter, og hvor den indre diameter af motorskærmens (80) udstødning er større end den indre diameter af motorskærmens (80) indsugning, og den indre diameter af diffusorens (81) udstødning er større end den indre diameter af diffusorens (81) indsugning.

5. Vindenergisystem ifølge krav 1, hvor motorskærmen (80) og diffusoren (81) hver især omfatter en bagkant, hvor motorskærmens (80) og diffusorens (81) bagkanter ligger omtrent på linje vertikalt, hvor motorskærmen (80) strækker sig en bestemt længde fra motorskærmens (80) bagkant til en forkant af motorskærmen (80), hvor diffusoren (81) strækker sig en bestemt længde fra diffusorens (81) bagkant til en forkant af diffusoren (81), og hvor den bestemte længde af diffusoren (81) er lig med omtrent halvdelen af den bestemte længde af motorskærmen (80)

6. Vindenergisystem ifølge krav 1, hvor de indre rotorblade (83) er forbundet med en første drivaksel (113), hvor den første drivaksel (113) er forbundet med det indre rotornav (85), hvor den første drivaksel (113) roterer et første tandhjul (90), hvor det første tandhjul (90) er forbundet med en flerhed af første regulerbare hydrauliske fortrængningspumper (92), der pumper en tryksat væske gennem et hydraulisk højtryksskredsløb, hvor hver især af flerheden af første regulerbare hydrauliske fortrængningspumper (92) er forbundet med det første tandhjul (90) ved hjælp af en første elektromagnetisk kobling (96a), og hvor den første elektromagnetiske kobling (96a) styres af en effektstyringsenhed (99), der behandler information fra en hastighedssensor (93), der er placeret på den første drivaksel (113).

7. Vindenergisystem ifølge krav 1, hvor de indre rotorblade (83) er forbundet med en første drivaksel (113), hvor den første drivaksel (113) er forbundet med det indre rotornav (85), hvor den første drivaksel (113) roterer et første tandhjul

(90), hvor det første tandhjul (90) er forbundet med en flerhed af første regulerbare hydrauliske fortrængningspumper (92), der pumper en tryksat væske gennem et hydraulisk højtryksskredsløb, hvor hver især af flerheden af første regulerbare hydrauliske fortrængningspumper (92) er forbundet med det første tandhjul (90) ved hjælp af en første elektromagnetisk kobling (96a), og hvor den første elektromagnetiske kobling (96a) styres af en effektstyringsenhed (99), der behandler information fra en momentsensor (93), der er placeret på den første drivaksel (113).

8. Vindenergisystem ifølge krav 6 eller 7, der endvidere omfatter en tandkrans (132), der roterer, når flerheden af de ydre rotorblade (84) roterer, hvor tandkransen (132) griber ind i et ydre rotordrivhjul (199), hvor det ydre rotordrivhjul (199) er forbundet med en anden drivaksel (134), hvor den anden drivaksel (134) er forbundet med et andet tandhjul (135), hvor det andet tandhjul (135) driver en flerhed af elektromagnetiske koblinger (96b), og hvor hver især af flerheden af andre elektromagnetiske koblinger (96b) er forbundet med en anden regulerbar hydraulisk fortrængningspumpe (92).

9. Vindenergisystem ifølge krav 8, der endvidere omfatter en eller flere sensorer, der overvåger rotationshastigheden af det første tandhjul (90) og det andet tandhjul (135), hvor det dynamiske teleskoptårn (3) positionerer vindturbinen (2) i en højde, hvor det dynamiske teleskoptårn (3) omfatter en eller flere belastningssensorer, og hvor en computerstyringsenhed (37) automatisk justerer højden af vindturbinen (2) baseret på data fra en eller flere sensorer, der overvåger rotationshastigheden af det første tandhjul (90) og det andet tandhjul (135) og den ene eller flere belastningssensorer i det dynamiske teleskoptårn (3).

10. Vindenergisystem ifølge krav 1, hvor de indre rotorblade (83) er forbundet med en første drivaksel (113), hvor den første drivaksel (113) er forbundet med det indre rotornav (85), hvor den første drivaksel (113) roterer et første tandhjul (90), hvor det første tandhjul (90) er forbundet med en flerhed af første luftkom-

5 pressorer, der pumper en tryksat fluid gennem et pneumatisk højtryksskredsløb, hvor hver især af flerheden af første luftkompressorer er forbundet med det første tandhjul (90) ved hjælp af en første elektromagnetisk kobling (96a), og hvor den første elektromagnetiske kobling (96a) styres af en effektstyringsenhed (99), der behandler information fra en hastighedssensor (93), der er placeret på den første drivaksel (113).

10 11. Vindenergisystem ifølge krav 1, hvor de indre rotorblade (83) er forbundet med en første drivaksel (113), hvor den første drivaksel (113) er forbundet med det indre rotornav (85), hvor den første drivaksel (113) roterer et første tandhjul (90), hvor det første tandhjul (90) er forbundet med en flerhed af første luftkompressorer, der pumper en tryksat fluid gennem et pneumatisk højtryksskredsløb, hvor hver især af flerheden af luftkompressorer er forbundet med det første tandhjul (90) ved hjælp af en første elektromagnetisk kobling (96a), og hvor den første elektromagnetiske kobling (96a) styres af en effektstyringsenhed (99), der behandler information fra en momentsensor (93), der er placeret på den første drivaksel (113).

20 12. Vindenergisystem ifølge krav 10 eller 11, der endvidere omfatter en tandkrans (132), der roterer, når flerheden af ydre rotorblade (84) roterer, hvor tandkransen (132) griber ind i et ydre rotordrivhjul (199), hvor det ydre rotordrivhjul (199) er forbundet med en anden drivaksel (134), hvor den anden drivaksel (134) er forbundet med et andet tandhjul (135), hvor det andet tandhjul (135) driver en flerhed af andre elektromagnetiske koblinger (96b), og hvor hver især af flerheden af andre elektromagnetiske koblinger (96b) er forbundet med en anden luftkompressor.

30 13. Vindenergisystem ifølge krav 12, der endvidere omfatter en eller flere sensorer, der overvåger rotationshastigheden af det første tandhjul (90) og det andet tandhjul (135), hvor det dynamiske teleskoptårn (3) positionerer vindturbinen (2) i en højde, hvor det dynamiske teleskoptårn (3) omfatter en eller flere belastnings-

sensorer, og hvor en computerstyringsenhed (37) automatisk justerer højden af vindturbinen (2) baseret på data fra en eller flere sensorer, der overvåger rotationshastigheden af det første tandhjul (90) og det andet tandhjul (135) og den ene eller flere belastningssensorer i det dynamiske teleskoptårn (3).

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14. Vindenergisystem ifølge krav 1, hvor energien frembringes af vind med en middelretning, og hvor det dynamiske teleskoptårn (3) omfatter en integreret tredimensionel giringsstyring (143), der stiller vindturbinen (2) på linje med vindens middelretning.

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15. Vindenergisystem ifølge krav 14, hvor den tredimensionelle giringsstyring (143) omfatter en flerhed af horisontale giringsdrivmotorer (151), der er fastgjort på en horisontal giringstandkrans (157) og en flerhed af vertikale giringsdrev (155) forbundet med en drivskinne (141) på en giringsstyreplatform (152).

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16. Vindenergisystem ifølge krav 1, der endvidere omfatter et flagermusafskrækkelsessystem, hvor flagermusafskrækkelsessystemet omfatter en mikrofon (201), en forforstærker (292), et lavpasfilter (203), en analog-digital-konverter (204), en digital lydbehandlingsenhed (205), en digital-analog-konverter (206), en forstærker (207) og en højttaler (208), og hvor flagermusafskrækkelsessystemet er fastgjort på vindturbinen (2).

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17. Vindenergisystem ifølge krav 1, der endvidere omfatter et flagermusafskrækkelsessystem, hvor flagermusafskrækkelsessystemet omfatter en mikrofon (201), en forforstærker (292), et lavpasfilter (203), en analog-digital-konverter (204), en digital lydbehandlingsenhed (205), en digital-analog-konverter (206), en forstærker (207) og en højttaler (208), og hvor flagermusafskrækkelsessystemet er fastgjort på det dynamiske teleskoptårn (3).

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18. Vindenergisystem ifølge krav 6 eller 7, der endvidere omfatter en eller flere hydrauliske akkumulatorer (10), der komprimerer en inert gas og anvender den

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komprimerede inerte gas til at tvinge den tryksatte væske gennem en styret overtryksventil og gennem højtryksrør for at drive en regulerbar hydraulisk hybrid fortrængningspumpe (12).

5 19. Vindenergisystem ifølge krav 18, hvor den regulerbare hybride fortrængningspumpe (12) driver en eller flere jordbaserede elektriske generatorer (15) med multiple permanentmagneter for at frembringe elektricitet.

10 20. Vindenergisystem ifølge krav 7 eller 8, hvor hver især af de første regulerbare hydrauliske fortrængningspumper (92) omfatter en solenoiddrevet bypassventil, der omdirigerer fluidstrømmen gennem den første regulerbare hydrauliske fortrængningspumpe (92), når den første regulerbare fortrængningspumpe (92) ikke er i brug.

15 21. Vindenergisystem ifølge krav 6 eller 7, hvor effektstyringsenheden (99) overvåger data omfattende vindhastighed (38), drivakselhastighed og hydraulisk tryk via elektriske sensorer og behandler dataene for at bestemme, hvor mange første regulerbare hydrauliske fortrængningspumper (92) behøver at blive aktiveret på et hvilket som helst tidspunkt.

20 22. Vindenergisystem ifølge krav 8, hvor effektstyringsenheden (99) overvåger data omfattende vindhastighed (38), drivakselhastighed og hydraulisk tryk via elektriske sensorer og behandler dataene for at bestemme, hvor mange andre regulerbare hydrauliske fortrængningspumper (92) behøver at blive aktiveret på
25 et hvilket som helst tidspunkt.

30 23. Vindenergisystem ifølge krav 1, hvor det dynamiske teleskoptårn (3) automatisk sænkes til en sikker driftshøjde, uden at de indre (83) og ydre rotorblade (84) frakobles, når vindhastigheden (38) når en bestemt hastighed.

24. Vindenergisystem ifølge krav 1, hvor rotorbladenes rotationshastighed æn-

drer sig, efterhånden som vindhastigheden ændrer sig.

25. Vindenergisystem ifølge krav 1, der endvidere omfatter hydrauliske akkumulatorer (19), der absorberer skiftende energiniveauer fra vind, lagrer overskudsenergi og leverer et konstant og kontrolleret output for at drive en flerhed af generatorer (15) med permanentmagneter.

26. Vindenergisystem ifølge krav 25, hvor flerheden af generatorer (15) med permanent magneter rummes i modulære generatorklynger.

27. Vindenergisystem ifølge krav 26, hvor de modulære generatorklynger kobles til og fra individuelt, efterhånden som og når der er behov.

28. Vindenergisystem ifølge krav 25, hvor hver generator (15) med permanentmagneter drives af et generatordrivhjul, og hvor generatordrivhjulet drejer en kobling til generatoren med permanentmagneter, der roterer et drev i generatoren (15) med permanentmagneter uden en direkte mekanisk forbindelse.

29. Vindenergisystem ifølge krav 25, hvor hver generator (15) med permanentmagneter omfatter en vandkappe, der køler generatoren (15) med permanentmagneter ved at lede en kølig væske om varmefrembringende mekaniske komponenter.

30. Vindenergisystem ifølge krav 28, hvor en computerstyringsenhed (37) overvåger det hydrauliske tryk ved en hydraulisk motor, der driver generatordrivhjulet (171), beregner hvor mange generatorer (15) med permanentmagneter, der skal aktiveres for at frembringe elektricitet, og til- eller afkobler individuelle elektromagnetiske koblinger (172) til generatoren med permanentmagneter i afhængighed af det til rådighed stående hydrauliske tryk.

31. Vindenergisystem ifølge krav 1, der endvidere omfatter:

en flæthed af andre indre rotorblade (83), der er placeret inde i motorskærmen (80) og bag flætheden af første indre rotorblade (83), hvor flætheden af andre indre rotorblade (83) roterer om et andet indre rotornav (85) i samme retning som flætheden af første indre rotorblade (83).

5

32. Anvendelse af et vindenergisystem ifølge krav 1 i en fremgangsmåde til brydning af metal, omfattende:

(a) at anvende vindenergisystemet til at frembringe energi;

10

(b) at lede en slam gennem en elektrokemisk ionoverføringsafsaltningssproces for at fjerne ædle metaller fra slammen og frembringe brintgas og ilt;

(c) at frembringe drikkevand ved at fjerne metaller og forurenende stoffer fra slammen; og

15

(d) at lagre brintgassen og ilten frembragt under afsaltningssprocessen i tryksatte beholdere.

DRAWINGS

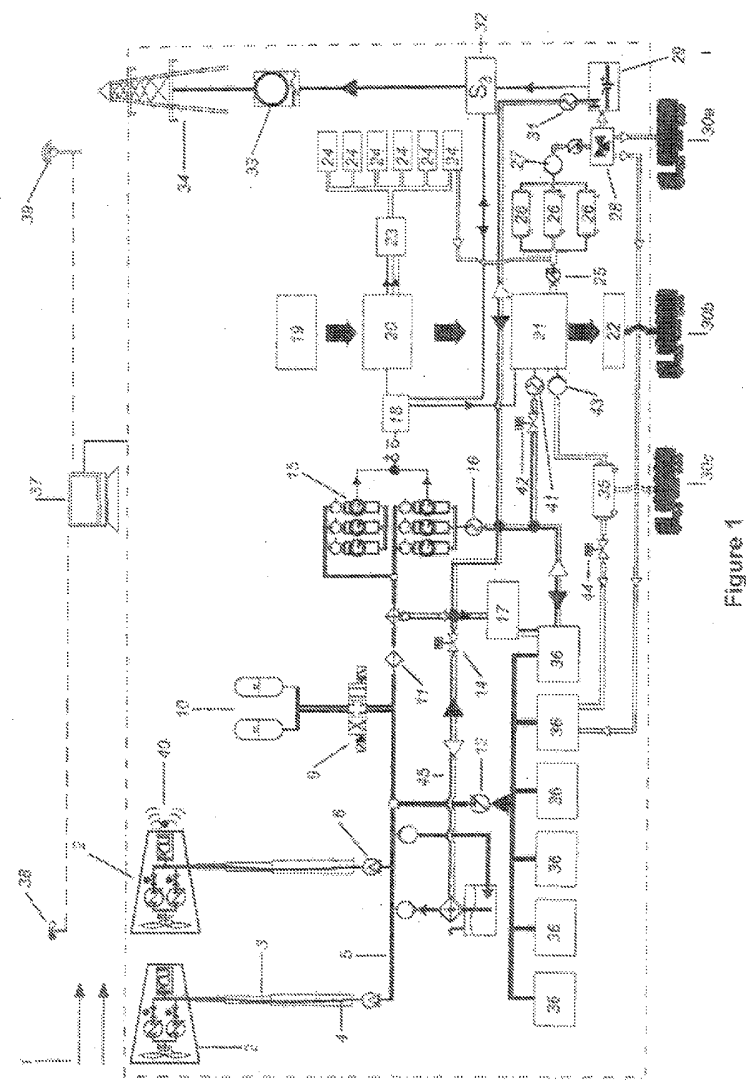
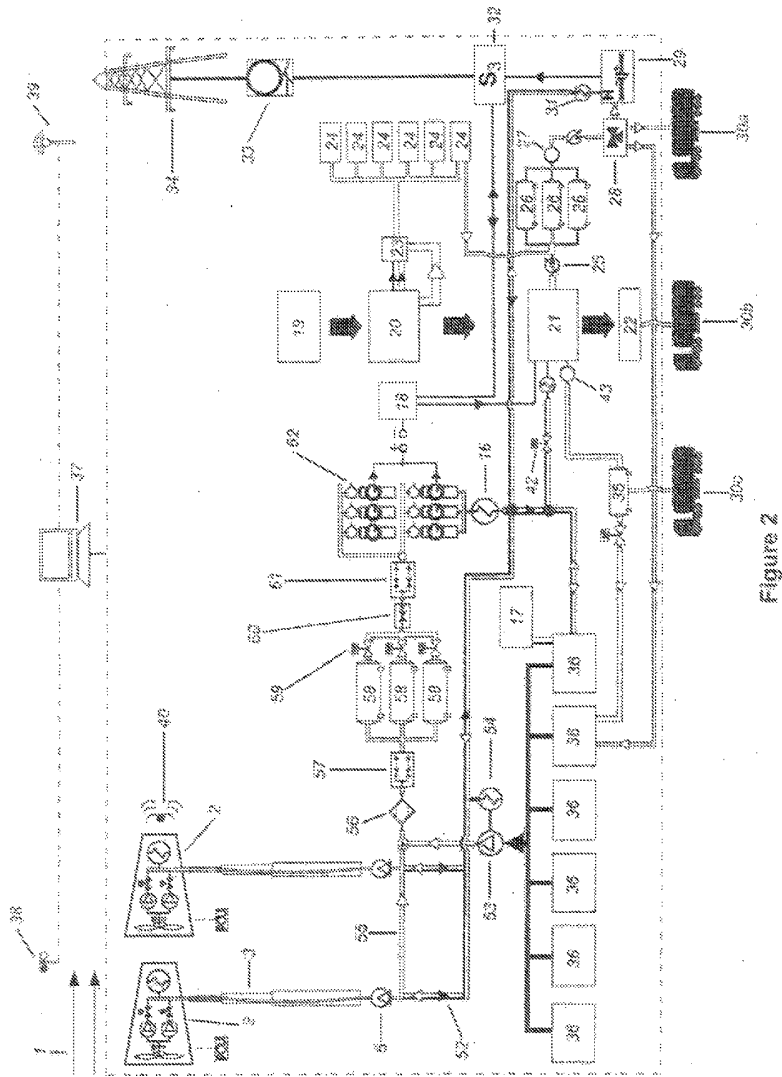


Figure 1



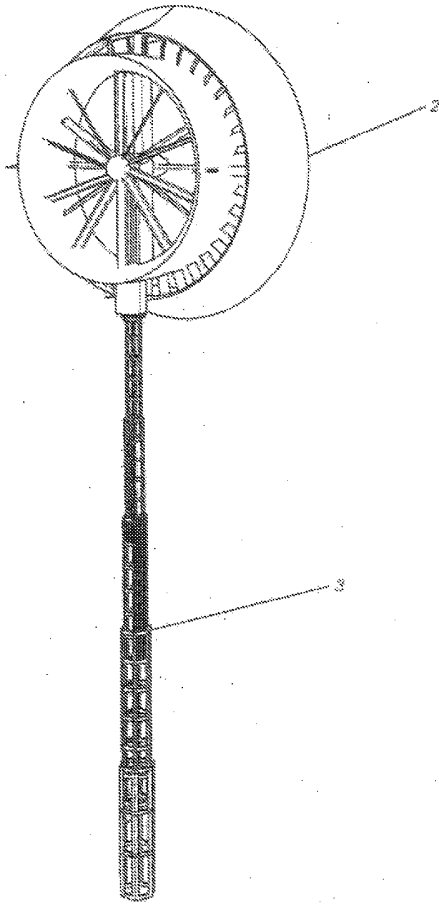


Figure 3

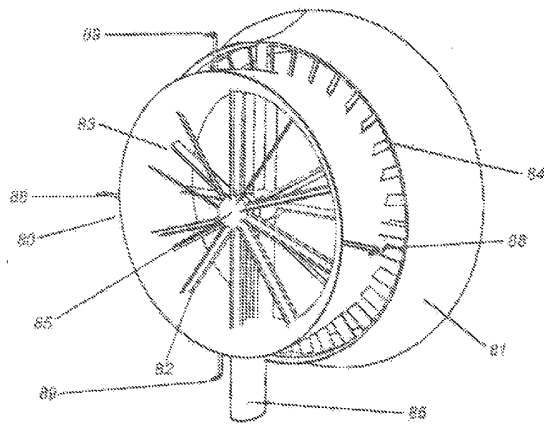


Figure 4a

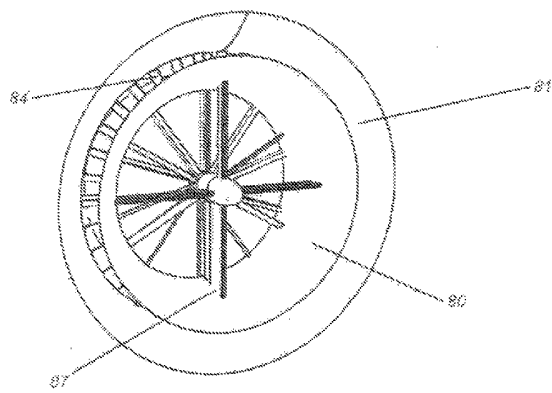


Figure 4b

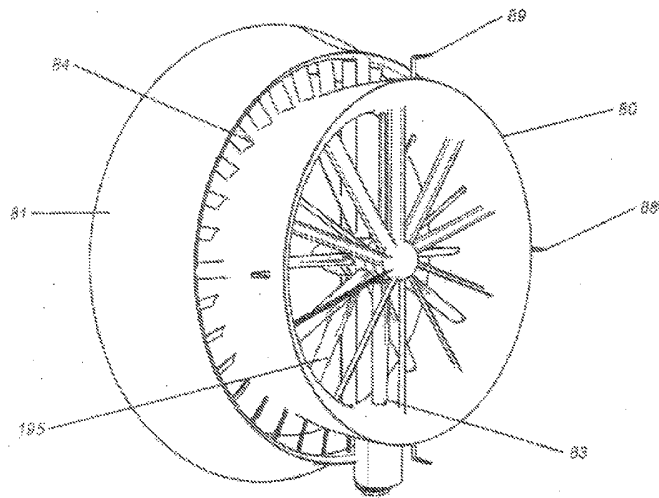


Figure 5a

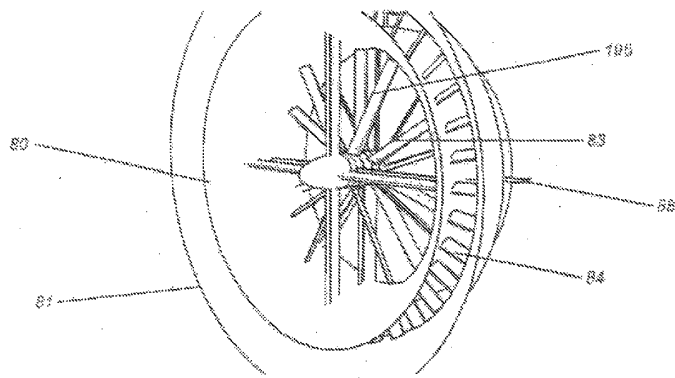


Figure 5b

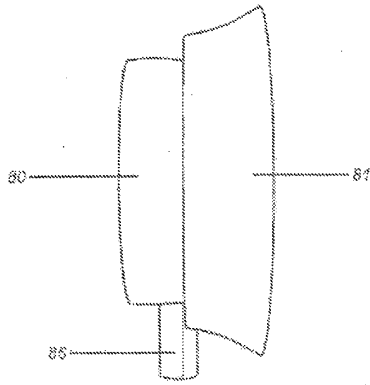


Figure 6

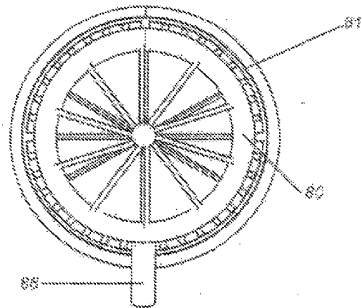


Figure 7

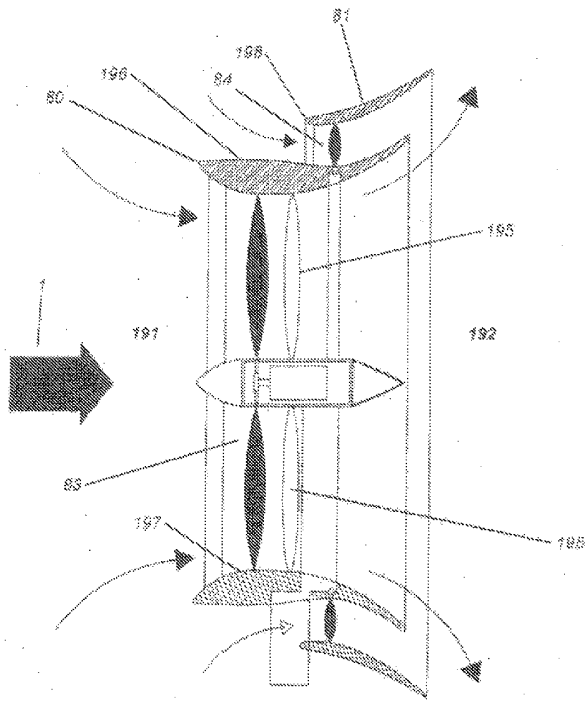


Figure 8

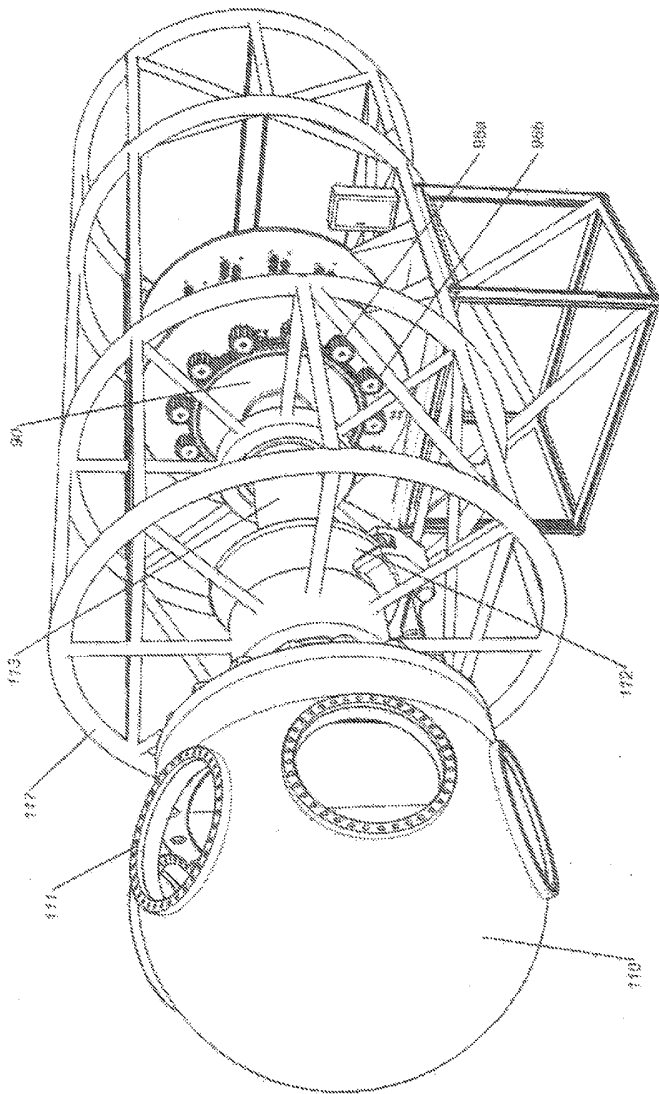


Figure 10

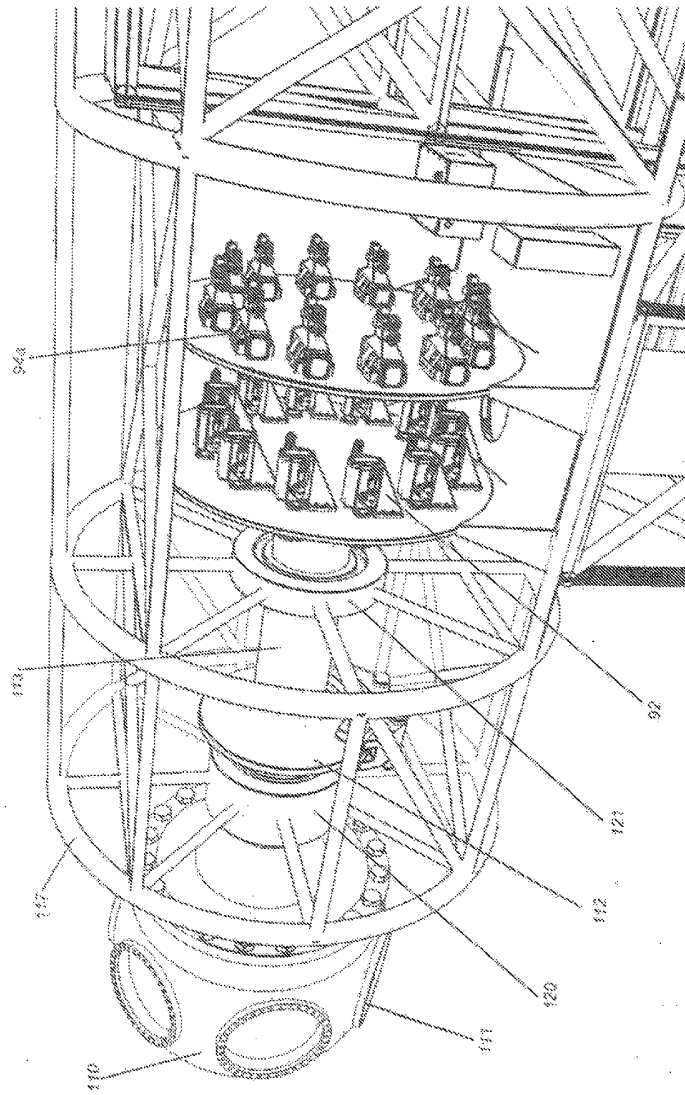


Figure 11

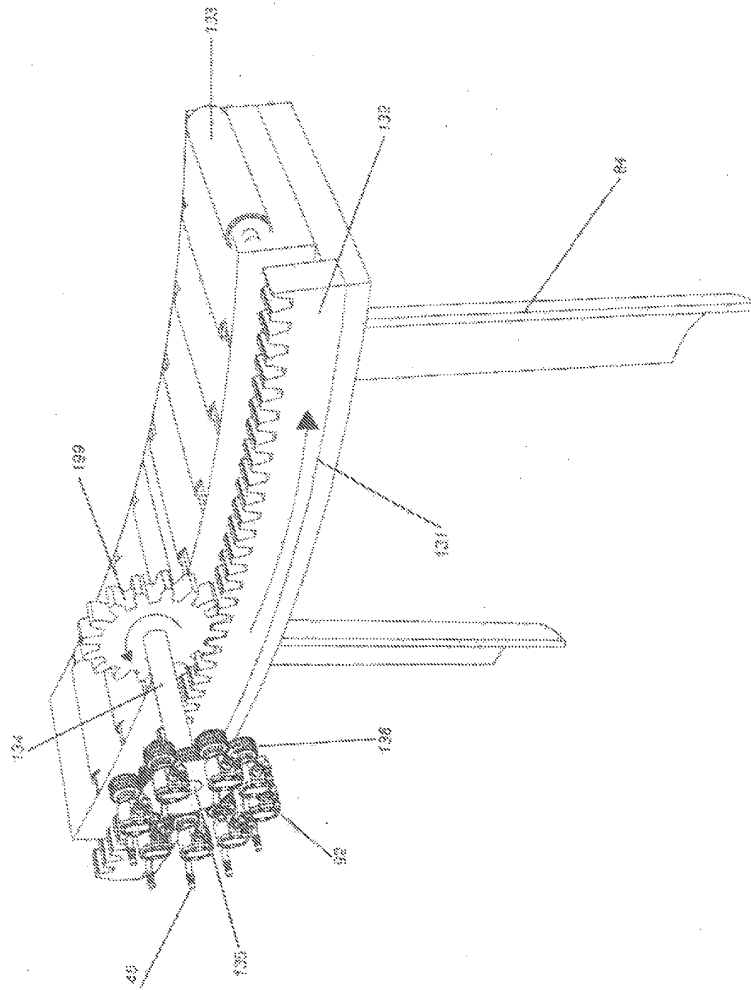


Figure 12

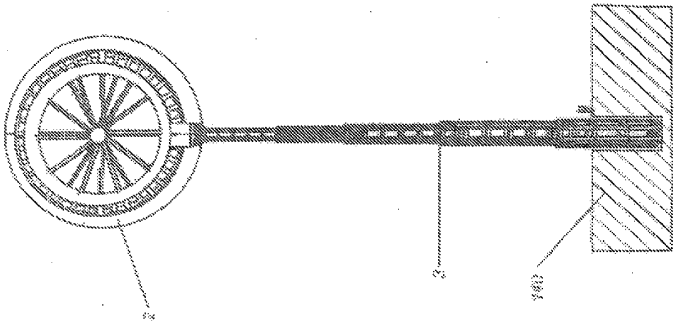


Figure 13

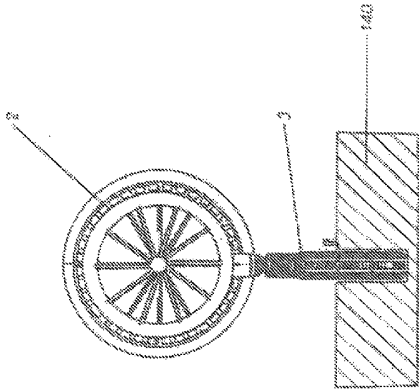


Figure 14

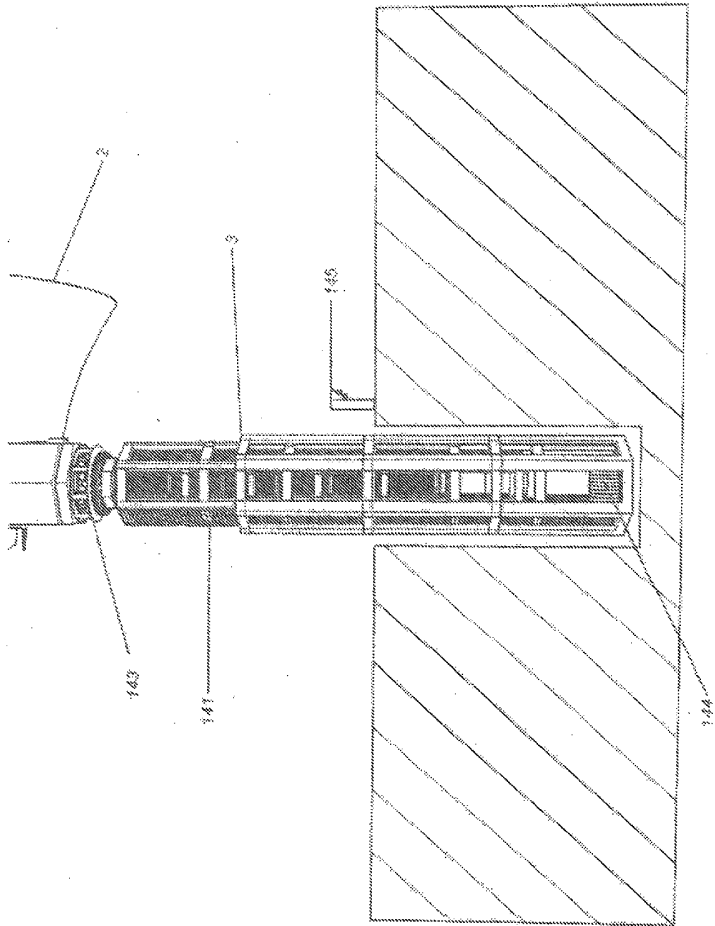


Figure 15

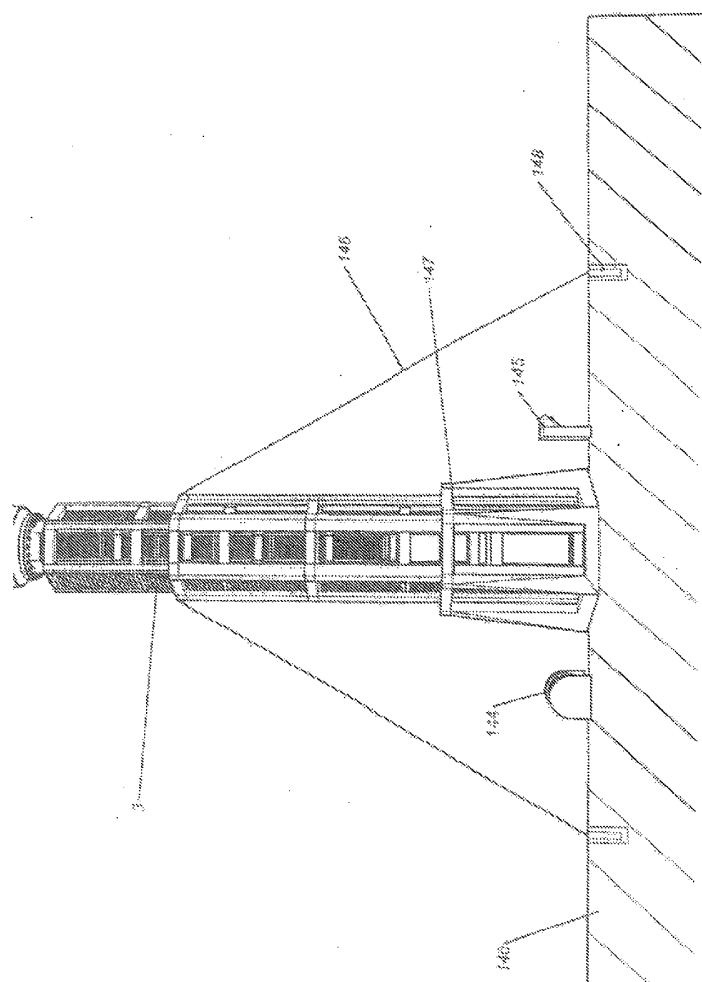


Figure 16

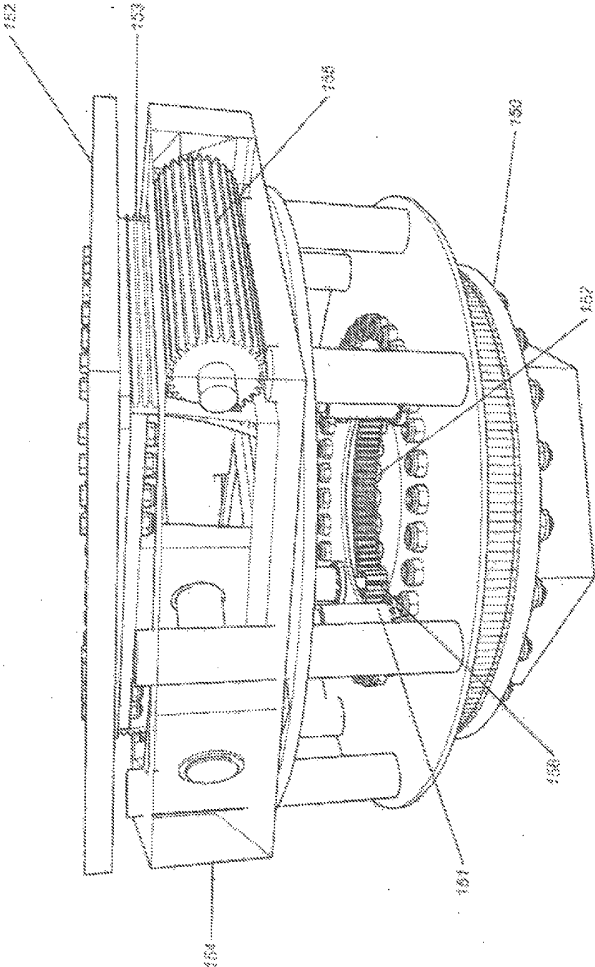


Figure 17A

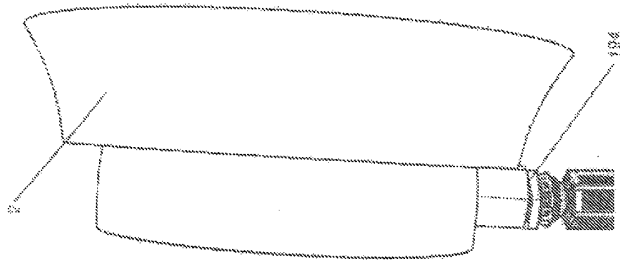


Figure 17C

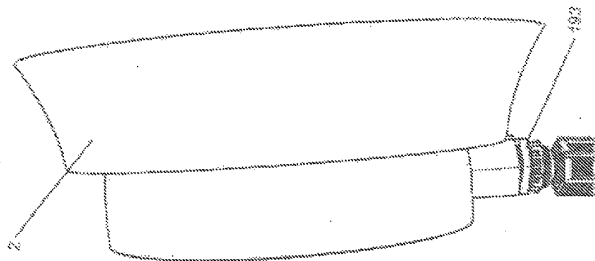


Figure 17B

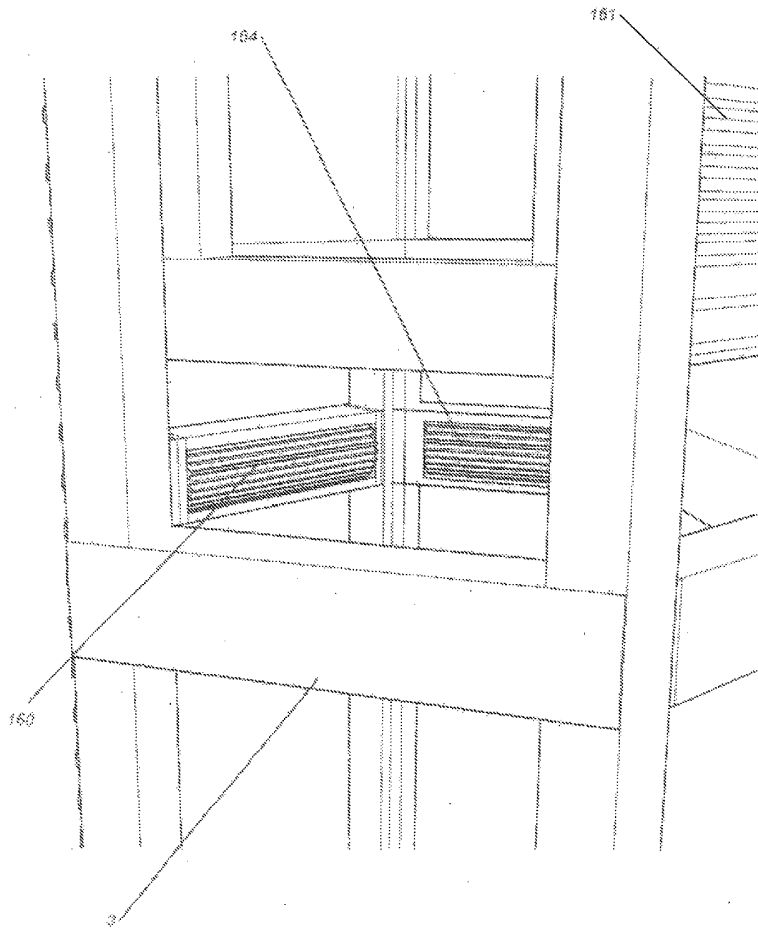


Figure 18

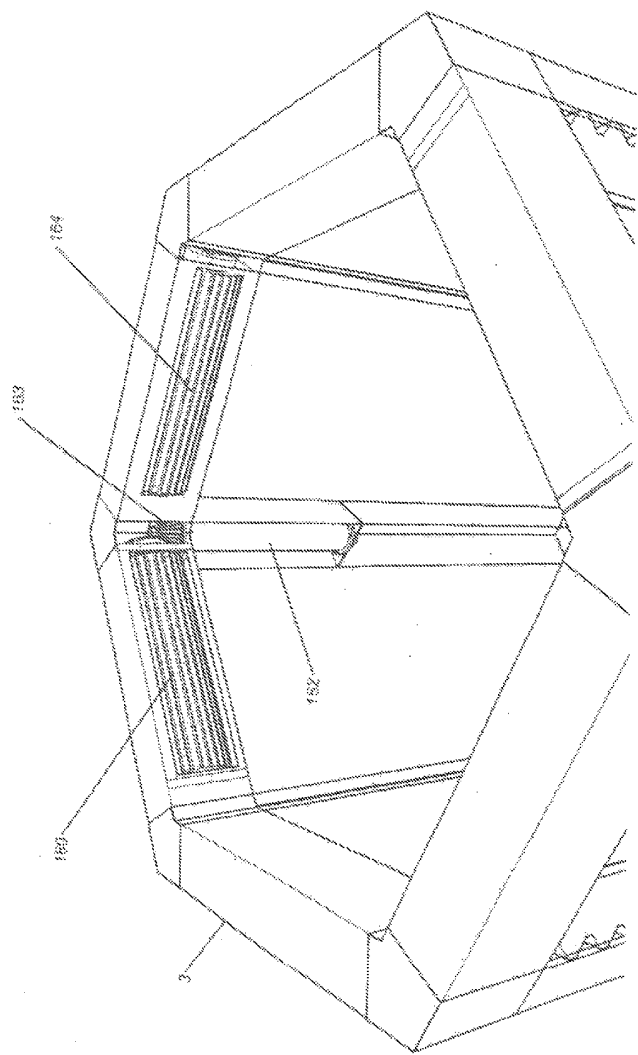


Figure 19

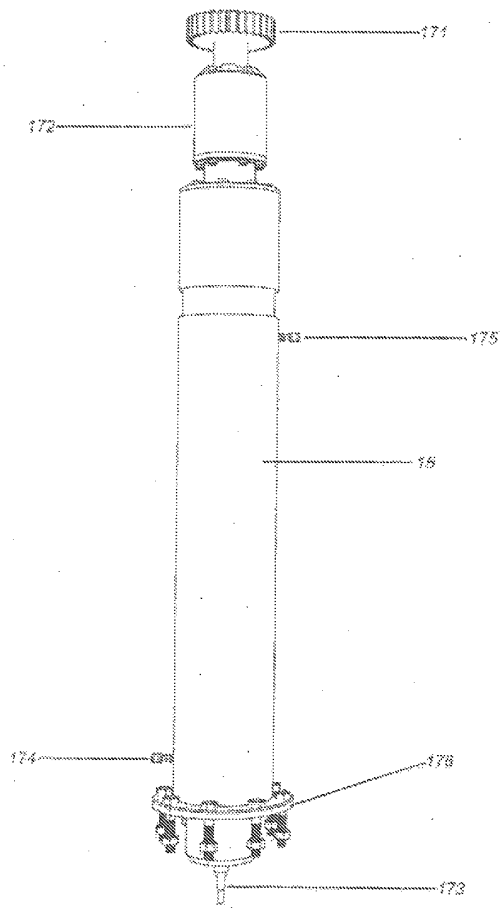


Figure 20

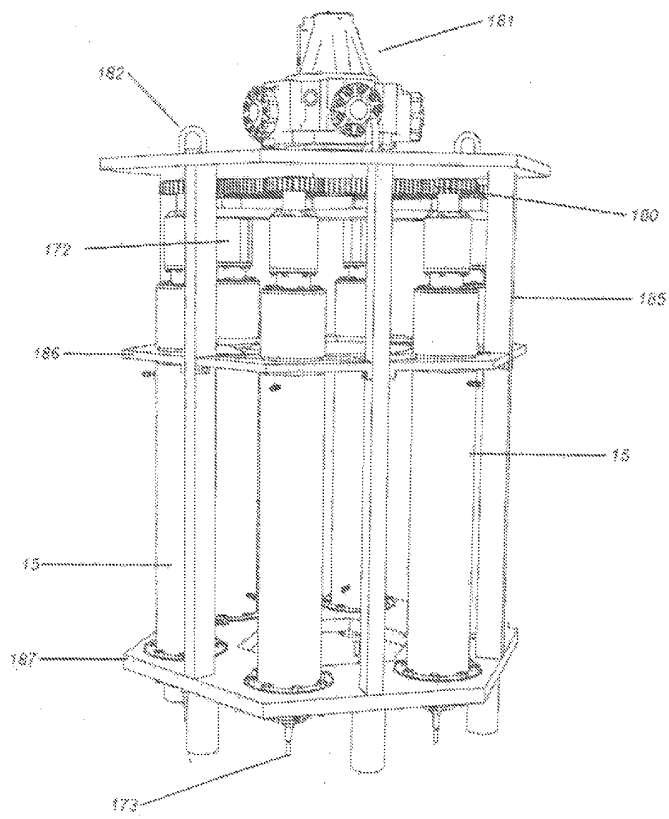


Figure 21

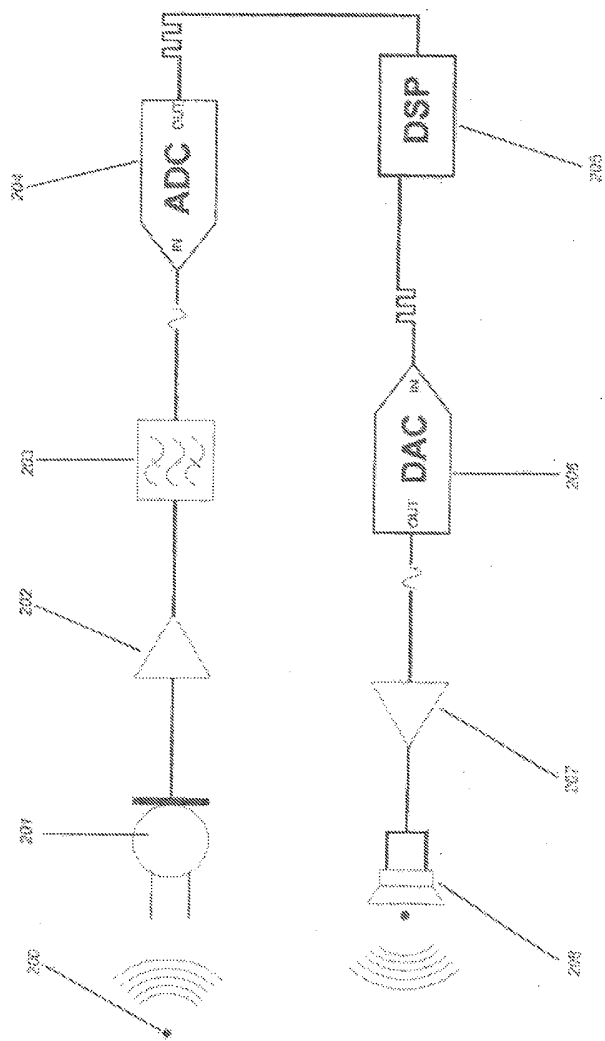


Figure 22