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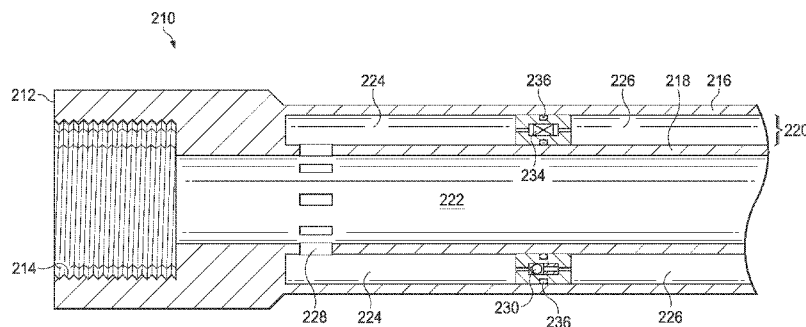


FIG. 2A

(57) **Abstract:** In accordance with some embodiments of the present disclosure, a high pressure regulation system for a ball valve used in a wellbore is disclosed. The high pressure ball valve includes an outer wall, an inner wall disposed in the outer wall, a tubing defined by an inner diameter of the inner wall, an annulus defined by an outer diameter of the inner wall and an inner diameter of the outer wall, a lower chamber formed in the annulus, and a relief valve fluidically coupled to the lower chamber. The relief valve is to control a pressure differential between a pressure in the lower chamber and a pressure in the tubing.

## HIGH PRESSURE REGULATION FOR A BALL VALVE

### TECHNICAL FIELD

5 The present disclosure relates generally to well drilling and hydrocarbon recovery operations and, more particularly, to regulating high pressure in a ball valve for use in a wellbore.

### BACKGROUND

10 During recovery operations in a wellbore, different stimulation techniques may be performed downhole, including nitrogen circulation, acidizing, fracturing, or a combination of acidizing and fracturing. Acidizing and nitrogen circulation are designed to clean up residues and skin damage in the wellbore in order to improve the flow of hydrocarbons. Fracturing is designed to create fractures in the formation surrounding the wellbore to allow hydrocarbons to flow from a reservoir into the wellbore. To enable the use of these stimulation techniques, perforations, or holes,  
15 may be created in a downhole casing in the wellbore. The perforations allow acid and other fluids to flow from the wellbore into the surrounding formation. The perforations may also allow hydrocarbons to flow into the wellbore from fractures in the formation created during fracturing techniques.

20 Recovery operations may also include using one or more ball valves to provide control of fluids to and from the formation. The ball valve isolates the portions of the formation downhole from the ball valve to prevent fluids from flowing into the formation from uphole and prevent fluids from flowing uphole from the formation during stimulation operations performed uphole from the formation.

### BRIEF DESCRIPTION OF THE DRAWINGS

25 For a more complete understanding of the present disclosure and its features and advantages, reference is now made to the following description, taken in conjunction with the accompanying drawings, in which:

FIGURE 1 illustrates an elevation view of an example embodiment of a subterranean operations system;

30 FIGURE 2A illustrates a detailed cross-sectional view of an uphole end of a high pressure ball valve;

FIGURE 2B illustrates a detailed cross-sectional view of a section of the high pressure ball valve of FIGURE 2A including a piston and ball mechanism that are located downhole from the components shown in FIGURE 2A; and

FIGURE 3 illustrates a flow chart of a method for performing a pressure cycle  
5 used to operate a high pressure ball valve;

FIGURE 4 illustrates a graph of a pressure cycle for a high pressure ball valve that includes regulation of a pressure differential using a relief valve.

#### DETAILED DESCRIPTION

A high pressure regulation system for a ball valve is disclosed. The ball valve  
10 may operate under high pressure conditions and includes a tubing defined by an inner wall and an annulus defined by the inner wall and an outer wall. The annulus includes a lower chamber. A check valve controls the flow of fluid between the tubing and the lower chamber. The check valve allows fluid to flow into the lower chamber and restricts the flow out of the lower chamber. A relief valve limits the pressure  
15 differential between the pressure in the lower chamber and the pressure in the tubing. By limiting the pressure differential, the pressure range of the operating window of the ball valve is decreased and the thickness of the inner wall and the amount of material used to produce the high pressure ball valve may be reduced, which decreases the manufacturing cost of the ball valve. Additionally, flexing of the inner  
20 wall caused by a high pressure differential may be reduced. Accordingly, a high pressure ball valve may be formed in accordance with the teachings of the present disclosure and may have different designs, configurations, and/or parameters according to a particular application. Embodiments of the present disclosure and its advantages are best understood by referring to FIGURES 1 through 4, where like  
25 numbers are used to indicate like and corresponding parts.

FIGURE 1 illustrates an elevation view of an example embodiment of a subterranean operations system. In the illustrated embodiment, subterranean operations system 100 may be associated with land-based subterranean operations. However, subterranean operations tools incorporating teachings of the present  
30 disclosure may be satisfactorily used with subterranean operations equipment located on offshore platforms, drill ships, semi-submersibles, and drilling barges.

Subterranean operations system 100 includes wellbore 102 that is defined in part by casing string 104 extending from well surface 106 to a selected downhole location. Uphole may be used to refer to a portion of wellbore 102 that is closer to well surface 106 and downhole may be used to refer to a portion of wellbore 102 that is further from well surface 106. Portions of wellbore 102 that do not include casing string 104 may be described as open hole.

Various types of fluid, such as oil, water, or gas, may be pumped from downhole to well surface 106 through wellbore 102. Additionally, other types of fluids, such as stimulation fluids and fracturing fluids, may be pumped from well surface 106 to areas of wellbore 102 near formation 108. As shown in FIGURE 1, wellbore 102 may be substantially vertical (*e.g.*, substantially perpendicular to the surface), substantially horizontal (*e.g.*, substantially parallel to the surface), or at an angle between vertical and horizontal.

Ball valve 110 may be positioned in wellbore 102 to prevent fluids from flowing to and from formation 108 when ball valve 110 is in a closed position. In some examples, ball valve 110 is installed in wellbore 102 to isolate formation 108 during completion operations performed on the portions of wellbore 102 uphole from ball valve 110. Completion operations include any suitable completion operations including installation of casing string 104, stimulation techniques, and pressure testing of wellbore 102. Ball valve 110 may be coupled to sections of production tubing 109 which may communicate fluids to and from ball valve 110. In some installations, ball valve 110 may be installed downhole from a packer (not expressly shown) that isolates the annular space in the wellbore such that any fluid flowing from formation 108 to well surface 106 flows through ball valve 110.

Once isolation of formation 108 is complete, for example when completion operations in the uphole portions of wellbore 102 are finished, ball valve 110 is opened to allow fluids to flow to and from formation 108. Ball valve 110 may be opened by applying pressure cycles to ball valve 110, as explained in further detail with respect to FIGURES 2–4. For example, drilling fluid or water may be pumped downhole to increase the pressure in ball valve 110. Once the pressure in ball valve 110 is increased, the drilling fluid or water may be pumped uphole to decrease the pressure in ball valve 110. The increase and decrease of the pressure in ball valve 110

may create a pressure differential that causes a mechanism in the ball valve to operate and open the ball valve. A pressure cycle may include one increase in pressure in ball valve 110 and the subsequent decrease in pressure in ball valve 110. Ball valve 110 may be designed to open after a predetermined number of pressure cycles. For example, each pressure cycle causes an axial movement of a piston in ball valve 110. The distance the piston moves axially during a single pressure cycle is referred to as the stroke length. When a piston has moved the complete distance of the travel path of the piston, a latch in the ball valve may become unsupported and allow springs to push ball valve 110 open. The predetermined number of pressure cycles used to open ball valve 110 may be calculated by dividing the total movement distance of the piston by the stroke length of the piston.

After completion of a pressure cycle, some amount of residual pressure remains in an annulus of ball valve 110, as described in further detail with respect to FIGURES 2–4, creating a pressure differential between the pressure of the interior of ball valve 110 and the pressure in the annulus of ball valve 110. The amount of residual pressure remaining in the annulus of ball valve 110 is based on the amount of pressure applied to ball valve 110 during the pressure cycle. Ball valve 110 may be designed to isolate formation 108 under high pressure conditions. For example, ball valve 110 may be designed to withstand pressures of greater than 10,000 pounds per square inch and the pressure applied to ball valve 110 during a pressure cycle may be also be greater than approximately 10,000 pounds per square inch. Therefore, to reduce the amount of pressure differential between the pressure of the interior of the ball valve and the pressure in the annulus of the ball valve after the application of a high pressure cycle, ball valve 110 may include a relief valve (not expressly shown) to reduce the residual pressure in the annulus of ball valve 110. The reduction in the pressure differential allows portions of ball valve 110 to be designed using thinner materials and reduces the amount of deformation of ball valve 110 that may occur during high pressure conditions. Therefore, a high pressure ball valve designed according to the present disclosure reduces the cost and increases the reliability and performance of the high pressure ball valve.

FIGURE 2A illustrates a cross-sectional view of an uphole end of a high pressure ball valve. FIGURE 2B illustrates a cross-sectional view of the high pressure

ball valve of FIGURE 2A including a piston and ball mechanism that are located downhole from the components shown in FIGURE 2A. High pressure ball valve 210 is attached to uphole completion equipment at end 212. The uphole completion equipment may be production tubing, wellbore testing equipment, or any other suitable equipment used in a wellbore completion operation. End 212 may be coupled to uphole completion equipment by threads 214 or any other suitable coupling mechanism such as a press fit, an interference fit, welding, crimp rings, or a combination thereof.

High pressure ball valve 210 includes outer wall 216 and inner wall 218. Annulus 220 is defined by the outside diameter of inner wall 218 and the inside diameter of outer wall 216. Tubing 222 is defined by the inside diameter of inner wall 218. Annulus 220 may be divided into multiple segments including upper chamber 224 and lower chamber 226. Lower chamber 226 may be filled with a compressible fluid, such as silicon oil other liquid or gas. Upper chamber 224 may be fluidically coupled to tubing 222 by inlets 228 such that fluids from tubing 222 flow into upper chamber 224 through inlets 228.

As described with respect to FIGURE 3, during a pressure cycle a fluid, such as drilling fluid or water, is pumped downhole to high pressure ball valve 210. The fluid fills tubing 222 and enters upper chamber 224 through inlets 228. The fluid is pumped into tubing 222 until the pressure in tubing 222 reaches a predetermined level. For example, the pressure in tubing 222 of high pressure ball valve 210 may reach a level of 10,000 pounds per square inch, 15,000 pounds per square inch, or greater. The predetermined level may be the maximum differential rating of ball valve 210. As the pressure in tubing 222 increases, the pressure in upper chamber 224 also increases. Check valve 230 may allow fluid from upper chamber 224 to flow into lower chamber 226. The flow of fluid into lower chamber 226 increases the pressure in lower chamber 226. Check valve 230 may be a valve that allows fluid to flow in only one direction. For example, check valve 230 allows fluid to flow from upper chamber 224 to lower chamber 226 but not from lower chamber 226 to upper chamber 224. Therefore, because tubing 222, upper chamber 224, and lower chamber 226 are fluidically coupled, the pressures in tubing 222, upper chamber 224, and

lower chamber 226 increase to the same pressure at the same rate during a pressure cycle, as described in further detail with respect to FIGURE 4.

Once the pressure in tubing 222 reaches the predetermined level, the pressure in tubing 222 may be rapidly decreased by pumping the fluid from tubing 222. The pressure in tubing 222 may return to a pressure at or near atmospheric pressure. Initially, the pressure in upper chamber 224 may decrease at approximately the same rate as the pressure decreases in tubing 222 as the fluid flows from upper chamber 224 through inlets 228. However, once the pressure in lower chamber 226 reaches a predetermined percentage of the maximum pressure of the pressure cycle, for example approximately 60–90 percent, and check valve 230 act to trap the remaining pressure in lower chamber 226 and allow the pressure to slowly decrease. The trapped pressure creates a pressure differential between the pressure in lower chamber 226 and the pressure in tubing 222. The pressure differential may cause piston 240, shown in FIGURE 2B, to move.

Due to the high pressure reached at the peak of the pressure cycle and the rapid decrease in the pressure in tubing 222, there may be a large pressure differential between the pressure in tubing 222 and the pressure in lower chamber 226. A large pressure differential between tubing 222 and lower chamber 226 may cause inner wall 218 to flex towards the center of tubing 222 such that the volume of lower chamber 226 increases. An increase in the volume of lower chamber 226 causes a decrease in the pressure in lower chamber 226. Over a number of pressure cycles, the flexing of inner wall 218 may impede the movements of the components of ball valve 210 due to the volume and pressure of lower chamber 226 deviating from the original design of lower chamber 226. For example, the flexing of inner wall 218 may displace the mechanical components of ball valve mechanism such that the alignment between the components changes and impedes the movement of the components.

Therefore, to reduce the flexing of inner wall 218, high pressure ball valve 210 may additionally include relief valve 234 that limits the differential pressure between tubing 222 and lower chamber 226. Relief valve 234 may be any type of relief valve suitable for use in hydraulic components under the conditions present in the wellbore environment. For example, relief valve 234 may be a spring operated valve, that opens when the force created by the differential pressure compresses the spring to

open a nozzle on relief valve 234. Relief valve 234 may be designed to open at a predetermined pressure differential between the pressure of tubing 222 and the pressure of lower chamber 226. For example, when the pressure differential exceeds the predetermined pressure, the pressure may force relief valve 234 open. The  
5 predetermined pressure differential may be set to a value above the pressure differential required to operate ball mechanism 242 of high pressure ball valve 210, referred to as the minimum cycling pressure. While one relief valve 234 is shown in FIGURE 3A, high pressure ball valve 210 may include multiple relief valves 234. Using multiple relief valves 234 may allow the pressure differential to be controlled  
10 in a quicker manner by allowing fluid to exit lower chamber 226 at a faster rate.

High pressure ball valve may additionally include sealing element 236 which prevents fluid from leaking between upper chamber 224 and lower chamber 226 at check valve 230, relief valve 234, or a combination thereof. Sealing element 236 may be any suitable sealing element, such as an O-ring, an X-ring, a D-ring, or a lip seal.  
15 The particular type of sealing element 236 may be selected to have an operating range corresponding to the maximum pressure differential between lower chamber 226 and tubing 222. The decrease in the pressure differential provided by relief valve 234 may decrease the operating range of sealing element 236 and allow a less expensive sealing element 236 to be used on high pressure ball valve 210 and reduce the  
20 likelihood of failure of sealing element 236.

High pressure ball valve 210 may additionally include piston 240 coupled to ball mechanism 242, as shown in FIGURE 2B. Piston 240 may be fluidically coupled to lower chamber 226 such that during the pressure cycle, the pressure differential between lower chamber 226 and tubing 222 may apply a force on end 246 of piston  
25 240 to cause piston 240 to move downhole.

During each pressure cycle, as the pressure in lower chamber 226 decreases, the force acting on piston 240 may decrease and the movement of piston 240 may stop. During the next pressure cycle, the pressure in lower chamber 226 may again apply a force to end 246 of piston 240 and move piston 240 downhole by another  
30 incremental amount. Each incremental movement of piston 240 may act on mechanical components of ball mechanism 242 which cause ball mechanism 242 to rotate from a closed position to an open position. Once piston 240 has moved its full



length, piston 240 is no longer supporting a latch (not expressly shown) in ball mechanism 242. When supported, the latch compresses a spring (not expressly shown). When piston 240 moves such that the latch is not supported, the spring moves downward to exert a force on ball mechanism 242 to cause ball mechanism 242 to rotate from a closed to an open position. This process may continue through each pressure cycle until piston 240 has fully activated ball mechanism 242 to open the ball valve, thus allowing flow through high pressure ball valve 210.

FIGURE 3 illustrates a flow chart of a method for performing a pressure cycle used to operate a high pressure ball valve. The steps of method 300 may be performed by an operator (*e.g.*, a person or automation equipment located at the well site) that is configured to operate downhole tools during a subterranean operation, a component of the high pressure ball valve, or both. The components of the high pressure ball valve discussed with respect to FIGURE 3 are described in more detail with respect to FIGURES 2A–B.

Method 300 may begin at step 302 where the operator may apply a tubing pressure to a tubing of a high pressure ball valve, such as tubing 222 shown in FIGURES 2A–2B while the ball valve is in a closed position. The tubing pressure may be applied by pumping a fluid, such as drilling fluid or water, downhole to the high pressure ball valve. Because the ball valve is closed, the fluid is trapped in the ball valve and the pressure in the tubing increases.

At step 304, the flow of fluid downhole to the high pressure ball valve may increase a chamber pressure in a lower chamber of the high pressure ball valve, such as lower chamber 226 shown in FIGURES 2A–2B. The lower chamber may be formed in an annular space between the tubing and the outer wall of the ball valve, as described in further detail with respect to FIGURES 2A–B. The pressure in the lower chamber increases due to fluid flowing from the tubing, into the annular space, and into the lower chamber. A check valve, such as check valve 230 shown in FIGURE 2A, may be used to allow fluid to flow into the lower chamber, but prevent the flow of fluid from the lower chamber.

At step 306, the operator may decrease the tubing pressure by pumping the fluid uphole from the high pressure ball valve. As the tubing pressure decreases, a pressure differential may be created between the chamber pressure and the tubing

pressure due to the check valve preventing the release of fluid and pressure from the lower chamber.

Steps 308 through 312 may be performed at any point during the pressure cycle when a pressure differential exists between the chamber pressure and the tubing pressure. At step 308, the relief valve, such as relief valve 234 shown in FIGURE 2A may determine whether the pressure differential between the chamber pressure and the tubing pressure is above a threshold. The threshold may be a predetermined value that is greater than the minimum cycling pressure of the high pressure ball valve. If the pressure differential is above the threshold, method 300 may proceed to step 310. If the pressure differential is below the threshold, method 300 may proceed to step 312.

At step 310, the relief valve may open to reduce the pressure in the lower chamber. At step 312, the relief valve may close. The relief valve closes when the pressure differential falls below the threshold such that the pressure differential stays above the minimum cycling pressure of the ball valve. By opening and closing the relief valve, the relief valve may limit the pressure differential between the chamber pressure and the tubing pressure while maintaining the pressure differential above the minimum cycling pressure such that the ball valve mechanism is still activated. By limiting the pressure differential, the relief valve limits the range of pressures in the operating window used to operate the ball valve. Therefore, the thickness and flexing of the walls of the tubing may be reduced, thus reducing the cost and increasing the performance and reliability of the ball valve.

At step 314, the pressure differential may operate a piston, such as piston 240 shown in FIGURE 2B. The piston may be fluidically coupled to the lower chamber such that the pressure in the lower chamber exerts a force on the piston and causes the piston to move. As the piston moves, the pressure in the lower chamber is reduced.

At step 316, the movement of the piston may activate the ball valve, such as ball valve 242 shown in FIGURE 2B. The activation of the ball valve may move the ball valve from a closed position to an open position.

At step 318, the operator may determine whether the ball valve is open. The operation of the piston in step 314 and the activation of the ball valve mechanism in step 316 may be incremental, such that several pressure cycles may be completed

before the piston has moved by an amount sufficient to open the ball valve. Therefore, if the ball valve is not open, method 300 may return to step 302 to perform the next pressure cycle which may activate the ball valve mechanism by the next increment. If the ball valve is open, method 300 may be complete.

- 5           The steps of method 300 may be completed in any order and some steps may be omitted or performed simultaneously with other steps. For example, the relief valve may be opened and closed at the same time the tubing pressure is decreasing and while the piston operates to activate the ball valve mechanism.

FIGURE 4 illustrates a graph of a pressure cycle for a high pressure ball valve that includes regulation of a pressure differential using a relief valve. Line 402 of graph 400 is the pressure in the tubing, such as tubing 222 shown in FIGURES 2A–B, and line 404 is the pressure in the lower chamber, such as lower chamber 226 shown in FIGURES 2A–B. The pressure cycle begins when tubing pressure is applied to the high pressure ball valve and the pressure in the tubing increases. The pressure in the lower chamber also increases at approximately the same rate as the increase in the pressure in the tubing. Once the pressure reaches a predetermined level, such as the maximum pressure differential rating of the high pressure ball valve, the pressure momentarily stabilizes. In FIGURE 4, the maximum pressure differential rating of the high pressure ball valve is approximately 10,000 pounds per square inch.

- 20           The pressure in the tubing may then be rapidly decreased to atmospheric pressure. Initially, the pressure in the lower chamber decreases at the same rate as the decrease in the pressure in the tubing. However, once the pressure in the lower chamber reaches a predetermined percentage of the maximum pressure of the pressure cycle, for example approximately 60–90 percent, a check valve act to trap the remaining pressure in the lower chamber. The trapped pressure creates a pressure differential between the pressure in the lower chamber and the pressure in the tubing. The pressure differential may cause a piston to move, as described with respect to FIGURES 2A–3.

- 30           When the difference between the pressure in the lower chamber and the pressure in the tubing exceeds the predetermined pressure differential setting of a relief valve included in the high pressure ball valve, the relief valve may open to control the pressure differential and allow the pressure in the lower chamber to

decrease. In FIGURE 4, the relief valve opens at point 406. The relief valve may remain open until the pressure differential between the pressure in the lower chamber and the pressure in the tubing falls below the predetermined pressure differential setting of the relief valve. At this point, shown as point 408 in FIGURE 4, the relief valve may close and the pressure in the lower chamber may remain constant.

In this way, the relief valve acts to limit the maximum pressure differential (e.g., the maximum retained pressure in the lower chamber) to reduce flexing of an inner wall of the high pressure ball valve. The reduced flexing of the inner wall may allow the inner wall to be thinner and thus reduce the cost associated with manufacturing the high pressure ball valve.

Embodiments disclosed herein include:

A. A high pressure ball valve including an outer wall; an inner wall disposed in the outer wall; a tubing defined by an inner diameter of the inner wall; an annulus defined by an outer diameter of the inner wall and an inner diameter of the outer wall; a lower chamber formed in the annulus; and a relief valve fluidically coupled to the lower chamber, the relief valve to control a pressure differential between a pressure in the lower chamber and a pressure in the tubing.

B. A method for operating a high pressure ball valve including applying a tubing pressure to a tubing of a high pressure ball valve by pumping a fluid downhole to the tubing; increasing a chamber pressure in a lower chamber of the high pressure ball valve through fluid flow from the tubing to the lower chamber; decreasing the tubing pressure by pumping the fluid uphole from the tubing; and opening a relief valve fluidically coupled to the lower chamber if a pressure differential between the chamber pressure and the tubing pressure exceeds a predetermined threshold.

C. A subterranean operation system including a production tubing disposed in a wellbore; and a high pressure ball valve coupled to the production tubing. The high pressure ball valve including an outer wall; an inner wall disposed in the outer wall; a tubing defined by an inner diameter of the inner wall; an annulus defined by an outer diameter of the inner wall and an inner diameter of the outer wall; a lower chamber formed in the annulus; and a relief valve fluidically coupled to the lower chamber, the relief valve to control a pressure differential between a pressure in the lower chamber and a pressure in the tubing.

Each of embodiments A, B, and C may have one or more of the following elements in any combination: Element 1: further comprising a sealing element preventing a fluid flow between the upper chamber and the lower chamber at the relief valve. Element 2: further comprising a fluid disposed in the lower chamber.

5 Element 3: wherein the fluid is a compressible fluid. Element 4: wherein the fluid is a silicone oil. Element 5: further comprising an inlet fluidically coupling the tubing, the annulus, and the lower chamber. Element 6: further comprising a check valve fluidically coupling the tubing and the lower chamber such that the check valve allows a fluid to flow into the lower chamber and prevents the fluid from flowing out

10 of the lower chamber. Element 7: further comprising closing the relief valve when the pressure differential falls below the predetermined threshold. Element 8: further comprising operating a piston fluidically coupled to the lower chamber; and activating a mechanism to open the high pressure ball valve.

Although the present disclosure and its advantages have been described in

15 detail, it should be understood that various changes, substitutions and alterations can be made herein without departing from the spirit and scope of the disclosure as defined by the following claims. For example, while the disclosure is described with respect to ball valves, aspects of the present disclosure may be adapted for use in other downhole tools activated based on cyclic pressure such as disappearing plugs.

WHAT IS CLAIMED IS:

1. A high pressure ball valve, comprising:  
an outer wall;  
an inner wall disposed in the outer wall;  
5 a tubing defined by an inner diameter of the inner wall;  
an annulus defined by an outer diameter of the inner wall and an inner  
diameter of the outer wall;  
a lower chamber formed in the annulus; and  
a relief valve fluidically coupled to the lower chamber, the relief valve to  
10 control a pressure differential between a pressure in the lower chamber and a pressure  
in the tubing.
2. The high pressure ball valve of claim 1, further comprising a sealing  
element preventing a fluid flow between the upper chamber and the lower chamber at  
15 the relief valve.
3. The high pressure ball valve of claim 1, further comprising a fluid  
disposed in the lower chamber.
- 20 4. The high pressure ball valve of claim 3, wherein the fluid is a  
compressible fluid.
5. The high pressure ball valve of claim 3, wherein the fluid is a silicone  
oil.  
25
6. The high pressure ball valve of claim 1, further comprising an inlet  
fluidically coupling the tubing, the annulus, and the lower chamber.

7. The high pressure ball valve of claim 1, further comprising:  
a check valve fluidically coupling the tubing and the lower chamber such that the check valve allows a fluid to flow into the lower chamber and prevents the fluid from flowing out of the lower chamber.

5

8. A method for operating a high pressure ball valve, comprising:  
applying a tubing pressure to a tubing of a high pressure ball valve by pumping a fluid downhole to the tubing;  
increasing a chamber pressure in a lower chamber of the high pressure ball  
10 valve through fluid flow from the tubing to the lower chamber;  
decreasing the tubing pressure by pumping the fluid uphole from the tubing;  
and  
opening a relief valve fluidically coupled to the lower chamber if a pressure differential between the chamber pressure and the tubing pressure exceeds a  
15 predetermined threshold.

9. The method of claim 8, further comprising closing the relief valve when the pressure differential falls below the predetermined threshold.

20 10. The method of claim 8, further comprising:  
operating a piston fluidically coupled to the lower chamber; and  
activating a mechanism to open the high pressure ball valve.

25 11. The method of claim 8, wherein the lower chamber is filled with a fluid.

12. The method of claim 9, wherein the fluid is a compressible fluid.

13. The method of claim 9, wherein the fluid is a silicone oil.

30

14. A subterranean operation system, comprising:  
a production tubing disposed in a wellbore; and  
a high pressure ball valve coupled to the production tubing, the high pressure ball valve including:
- 5 an outer wall;  
an inner wall disposed in the outer wall;  
a tubing defined by an inner diameter of the inner wall;  
an annulus defined by an outer diameter of the inner wall and an inner diameter of the outer wall;
- 10 a lower chamber formed in the annulus; and  
a relief valve fluidically coupled to the lower chamber, the relief valve to control a pressure differential between a pressure in the lower chamber and a pressure in the tubing.
- 15 15. The subterranean operation system of claim 14, the high pressure ball valve further including sealing element preventing a fluid flow between the upper chamber and the lower chamber at the relief valve.
- 20 16. The subterranean operation system of claim 14, the high pressure ball valve further including a fluid disposed in the lower chamber.
- 25 17. The subterranean operation system of claim 16, wherein the fluid is a compressible fluid.
18. The high pressure ball valve of claim 17, wherein the fluid is a silicone oil.
- 30 19. The subterranean operation system of claim 14, the high pressure ball valve further including an inlet fluidically coupling the tubing, the annulus, and the lower chamber.



20. The subterranean operation system of claim 14, the high pressure ball valve further including:

- 5 a check valve fluidically coupling the tubing and the lower chamber such that the check valve allows a fluid to flow into the lower chamber and prevents the fluid from flowing out of the lower chamber.

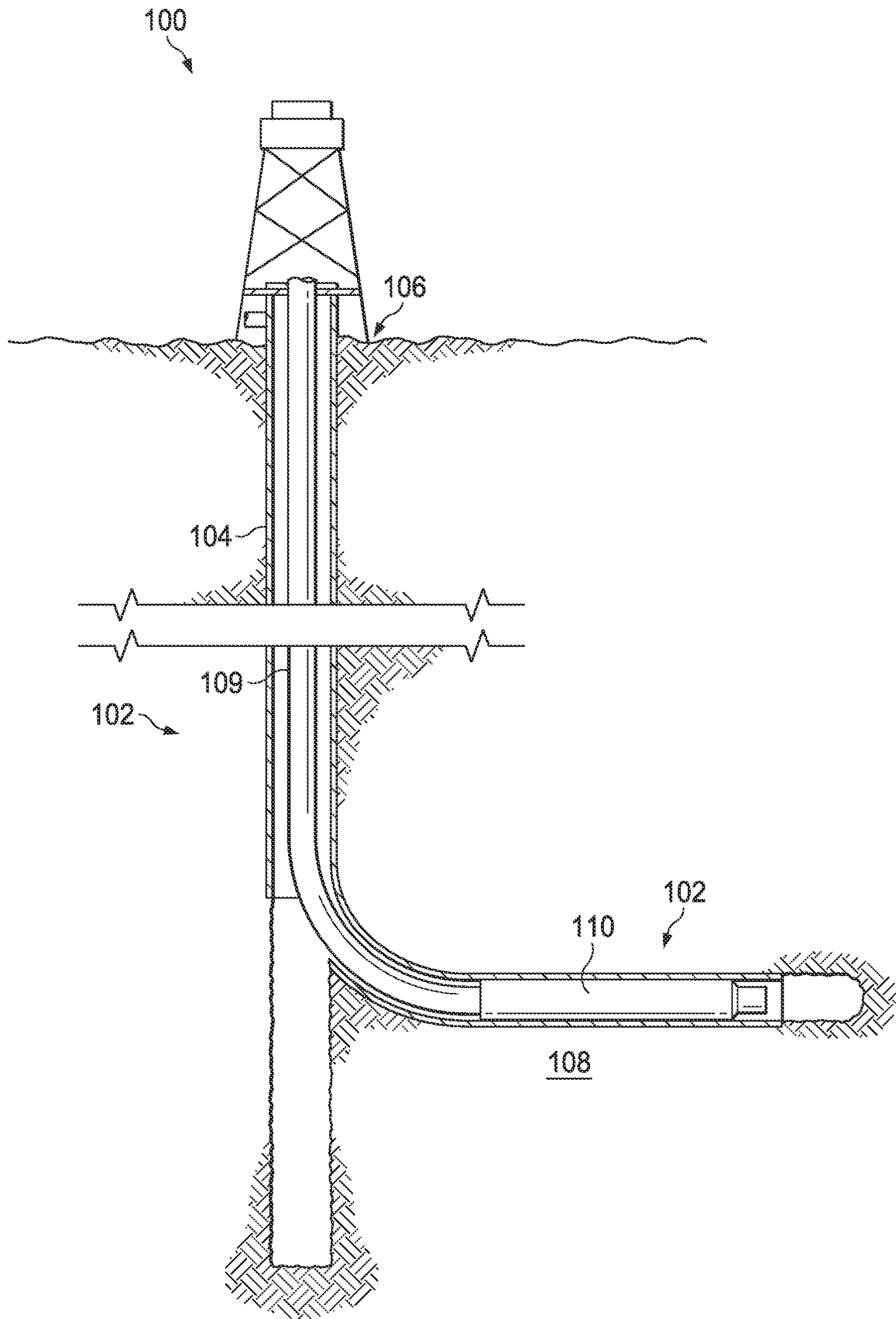


FIG. 1

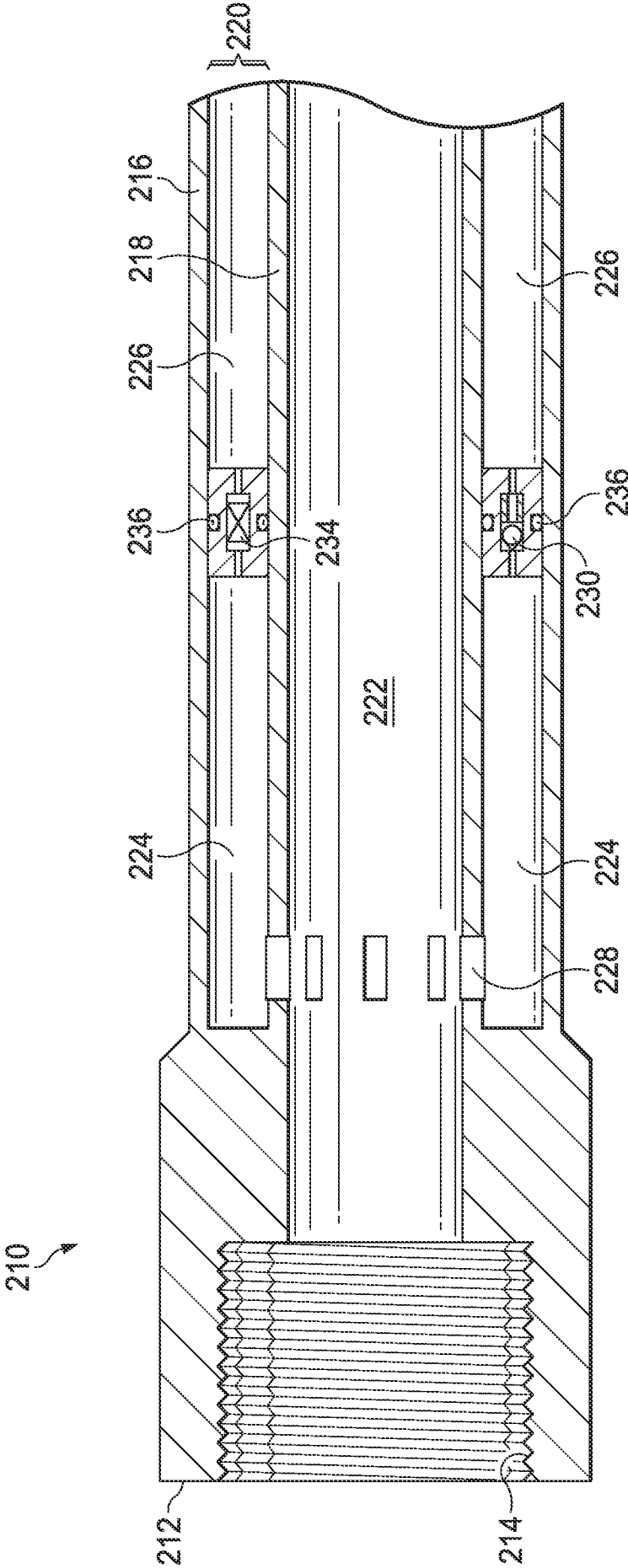
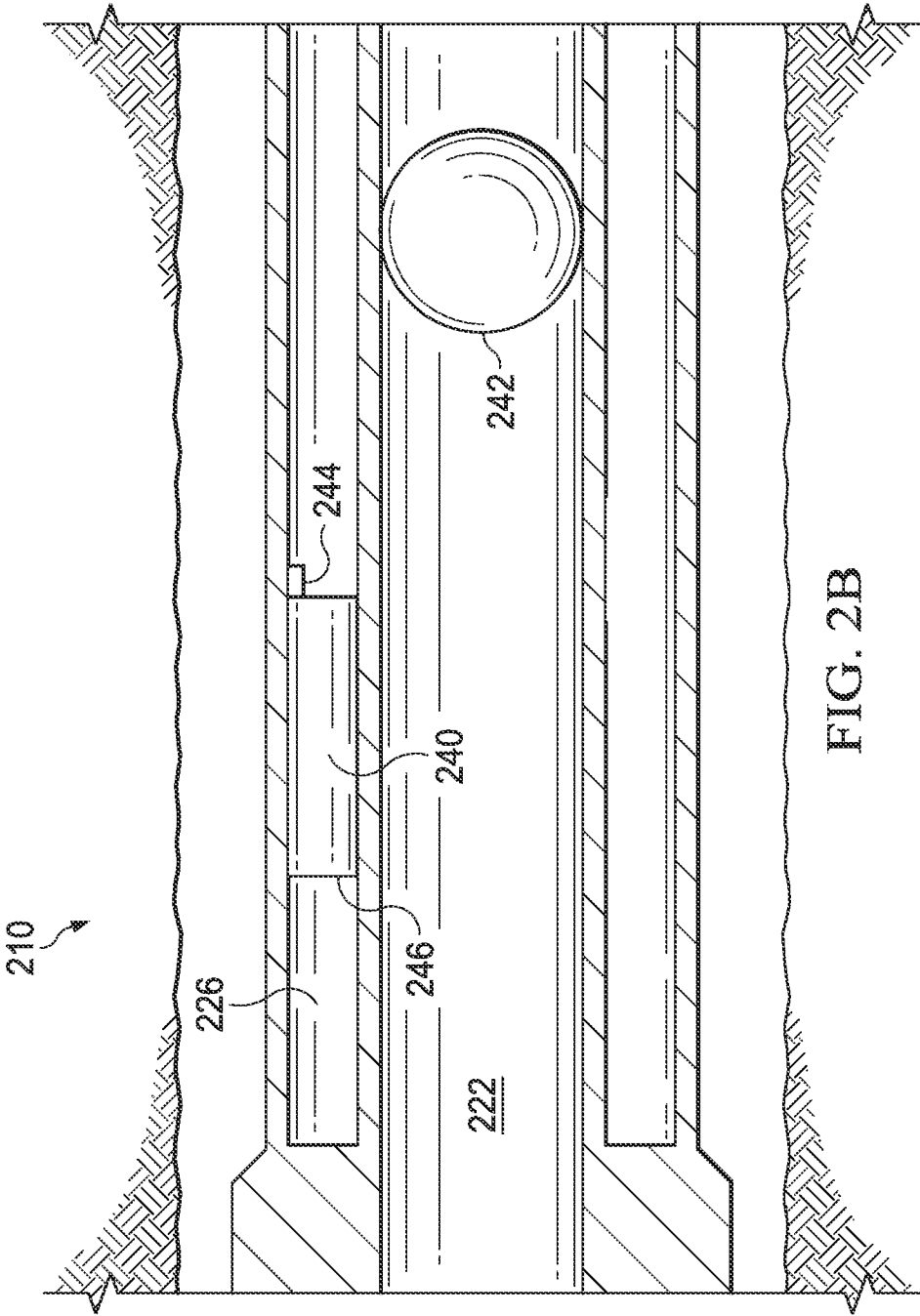


FIG. 2A



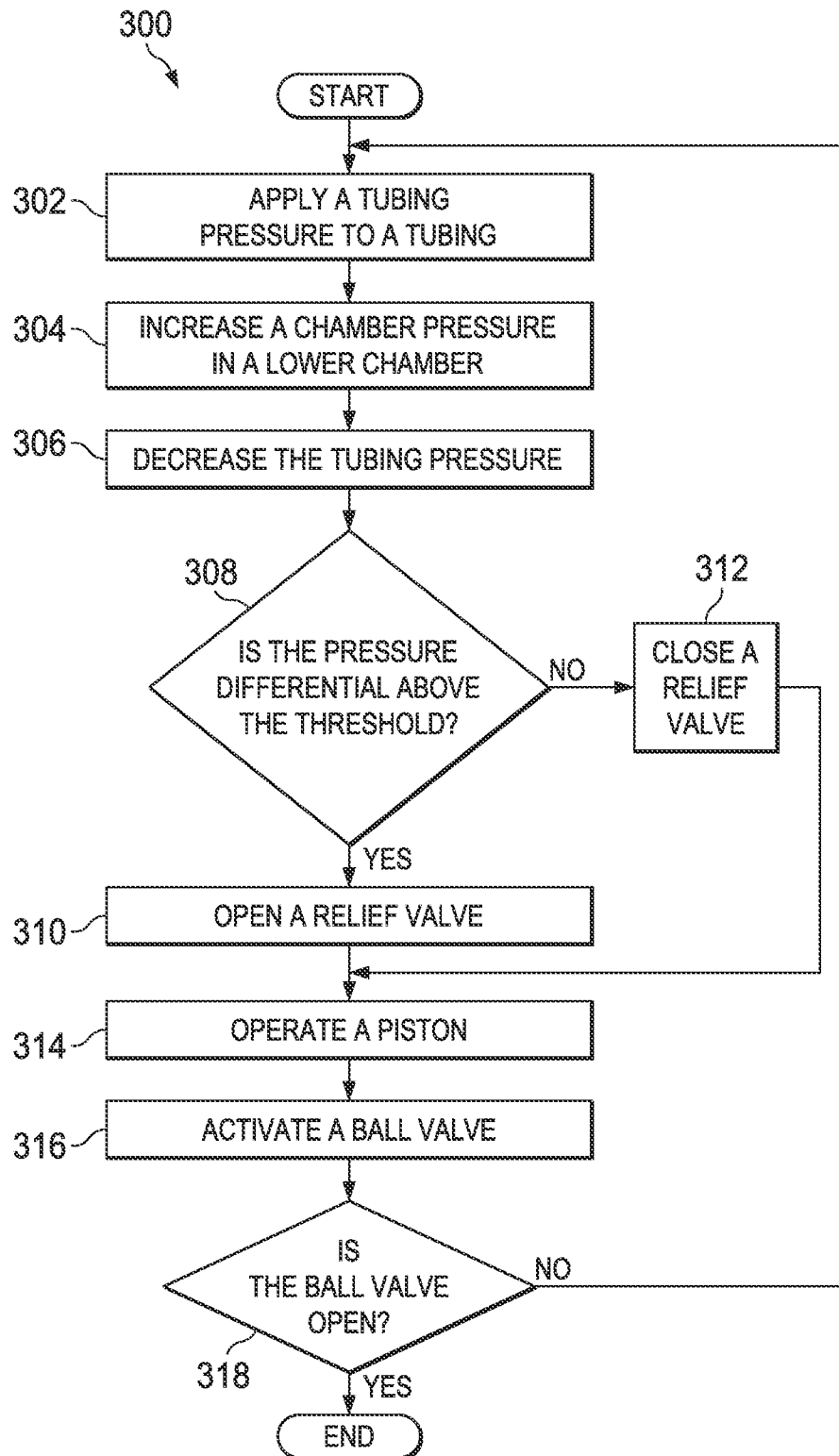
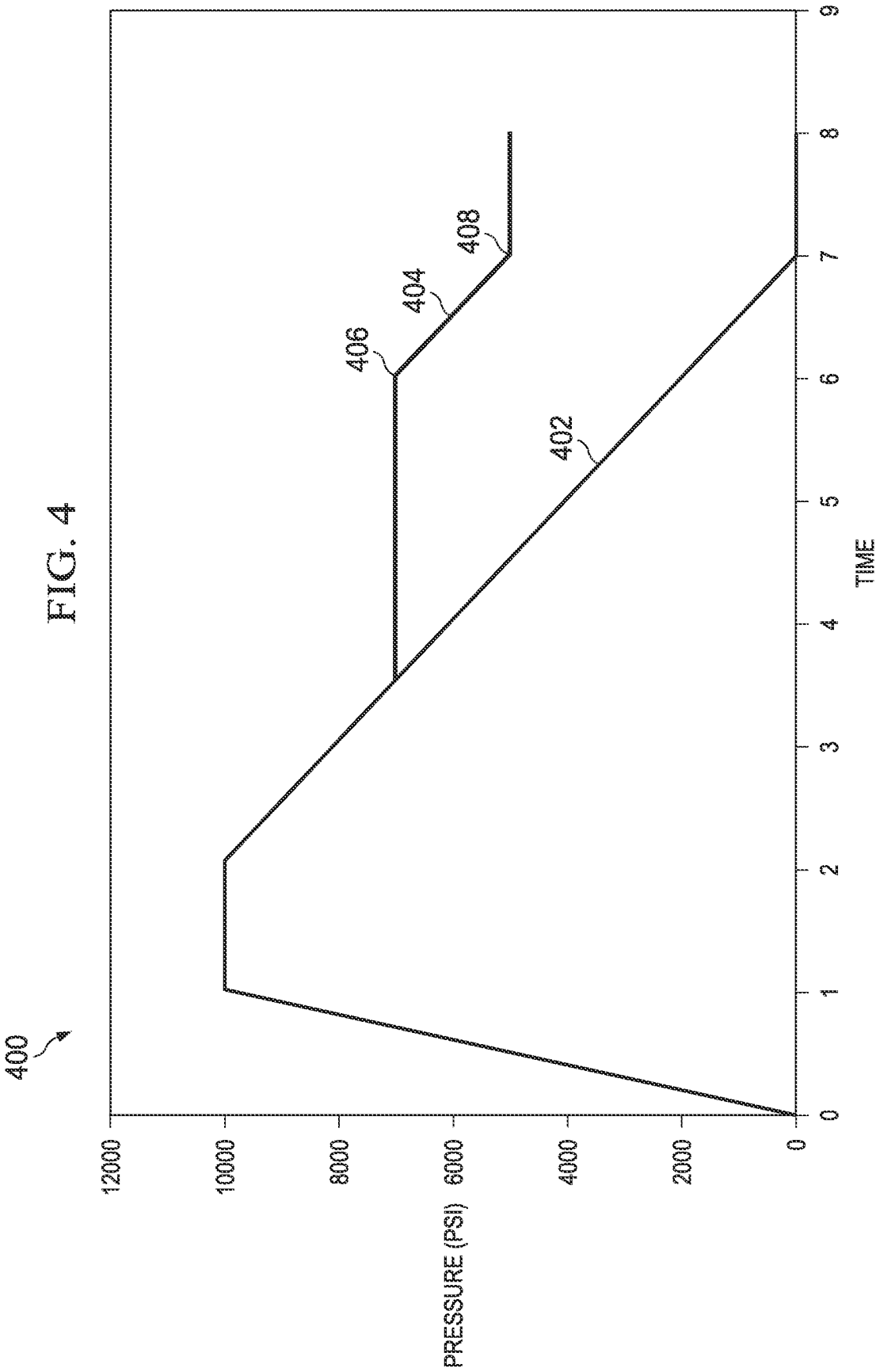


FIG. 3



## INTERNATIONAL SEARCH REPORT

International application No.  
**PCT/US2015/040284****A. CLASSIFICATION OF SUBJECT MATTER****E21B 34/06(2006.01)i, E21B 17/00(2006.01)i**

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)

E21B 34/06; E21B 47/10; B23P 11/00; E21B 21/10; E21B 10/02; F17D 1/16; E21B 17/00

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Korean utility models and applications for utility models

Japanese utility models and applications for utility models

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

eKOMPASS(KIPO internal) &amp; Keywords:ball-valve, relief-valve, control, fluid, silicon, tubing, string, flow, check valve and one-way valve

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US 2013-0118758 A1 (SCHLUMERGER TECHNOLOGY CORPORATION) 16 May 2013 See paragraphs [0019]-[0035] and figures 1-4.	1-20
A	US 2013-0341011 A1 (HALLIBURTON ENERGY SERVICE, INC.) 26 December 2013 See paragraphs [0011]-[0039] and figures 1-2F.	1-20
A	US 2013-0206417 A1 (HALLIBURTON ENERGY SERVICE, INC.) 15 August 2013 See paragraphs [0013]-[0028] and figures 1-3C.	1-20
A	US 2013-0000917 A1 (SLACK et al.) 03 January 2013 See paragraphs [0040]-[0060] and figures 1-4B.	1-20
A	US 2012-0234607 A1 (KINSELLA, DOUGLAS) 20 September 2012 See paragraphs [0018]-[0041] and figures 1A-3C.	1-20



Further documents are listed in the continuation of Box C.



See patent family annex.

\* Special categories of cited documents:

"A" document defining the general state of the art which is not considered to be of particular relevance

"E" earlier application or patent but published on or after the international filing date

"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art

"&amp;" document member of the same patent family

Date of the actual completion of the international search

20 March 2016 (20.03.2016)

Date of mailing of the international search report

**21 March 2016 (21.03.2016)**

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**INTERNATIONAL SEARCH REPORT**

Information on patent family members

International application No.

**PCT/US2015/040284**

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 2013-0118758 A1	16/05/2013	AU 2012-339874 A1 GB 201408613 D0 GB 2511952 A US 9074438 B2 WO 2013-074392 A1	29/05/2014 25/06/2014 17/09/2014 07/07/2015 23/05/2013
US 2013-0341011 A1	26/12/2013	CN 103890311 A EP 2764199 A1 US 2013-0081806 A1 US 8522883 B2 US 8714267 B2 WO 2013-052038 A1	25/06/2014 13/08/2014 04/04/2013 03/09/2013 06/05/2014 11/04/2013
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