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(54) TEMPERATURE DEPENDENT ELECTRICALLY RESISTIVE YARN

(76) Inventors: **Alfred R. DeAngelis**, Spartanburg, SC (US); **Earle Wolynes**, Spartanburg, SC (US)

Correspondence Address:
Jeffery E. Bacon
Milliken & Company
Legal Department, M-495
PO Box 1926
Spartanburg, SC 29304 (US)

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(57) **ABSTRACT**

A positive variable resistive yarn having a core, a sheath, and an insulator. The sheath includes distinct electrical conductors intermixed within a thermal expansive low conductive matrix. As the temperature of the yarn increases, the resistance of the sheath increases.

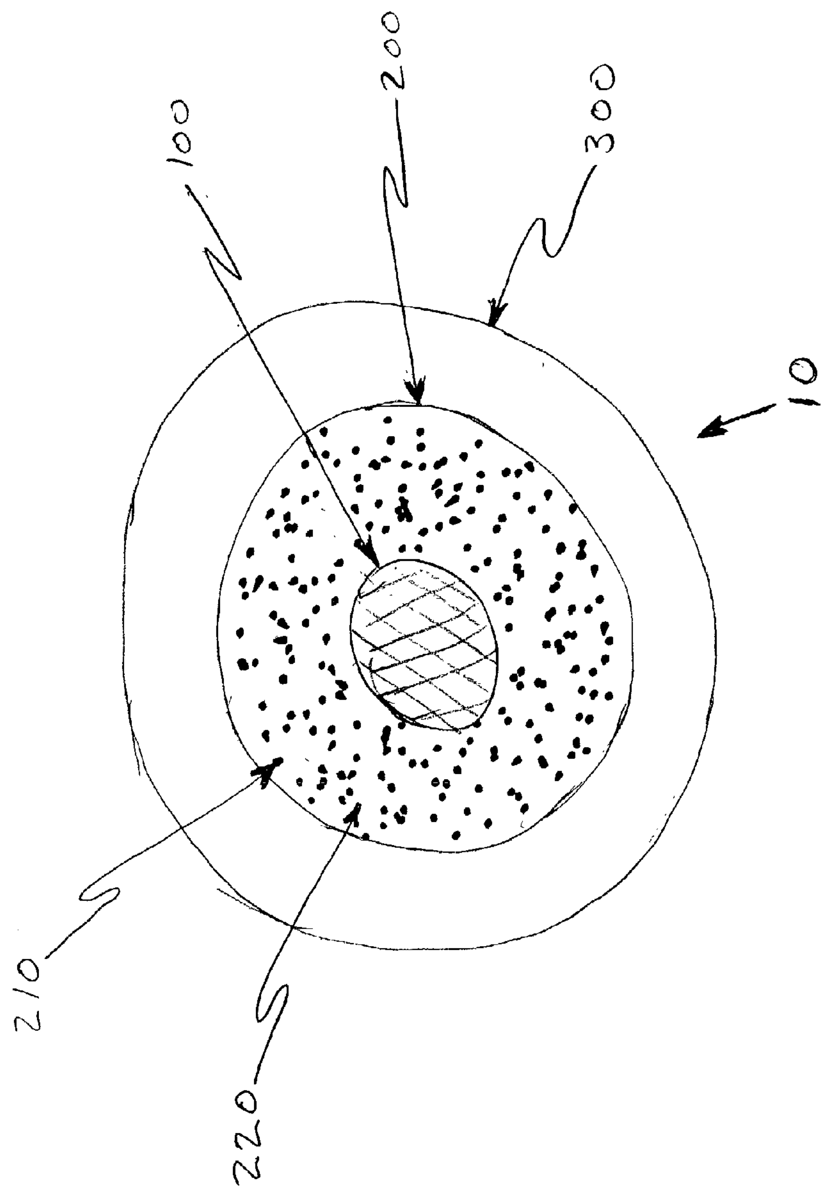

FIGURE 1

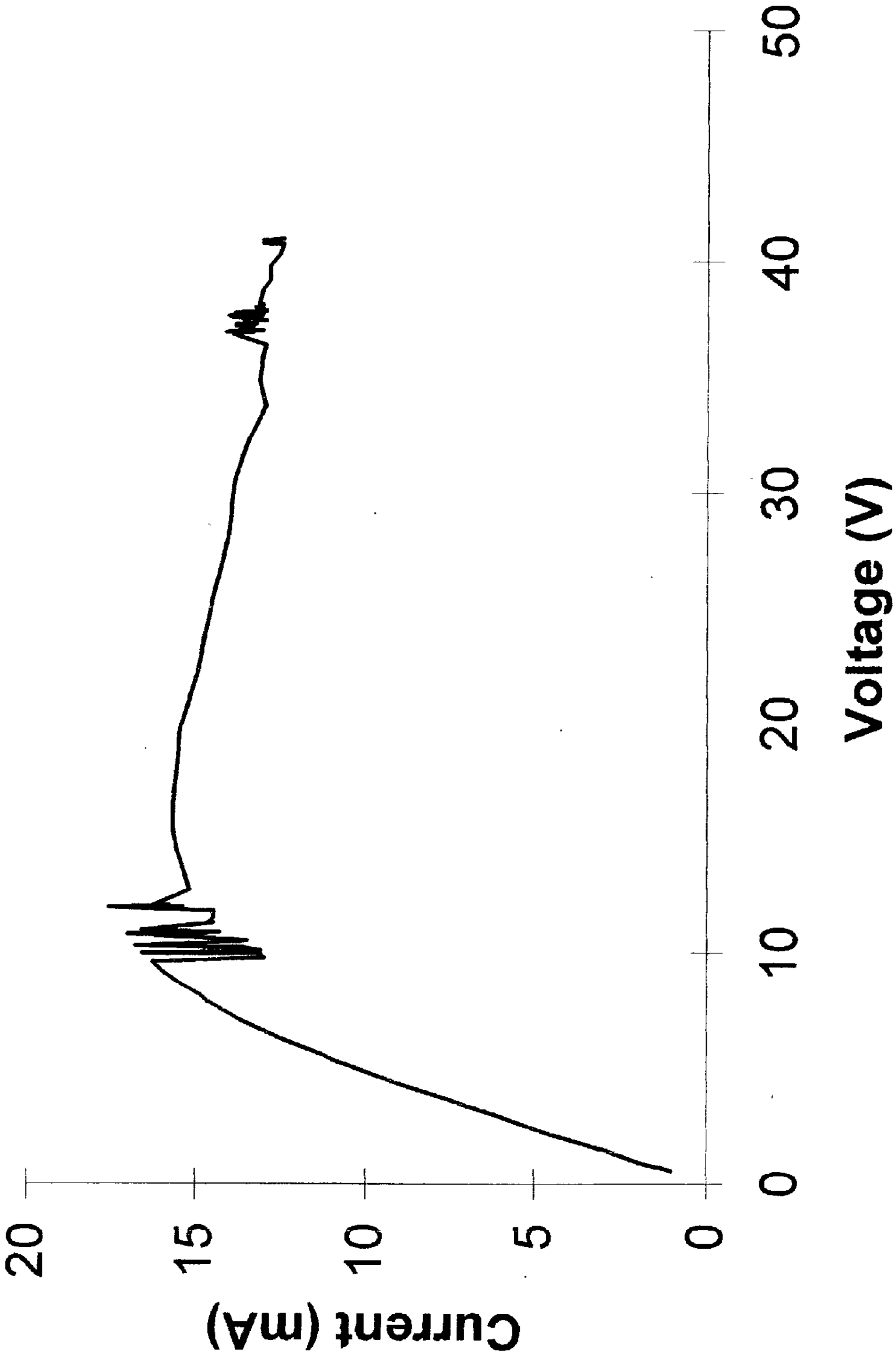

FIGURE 2

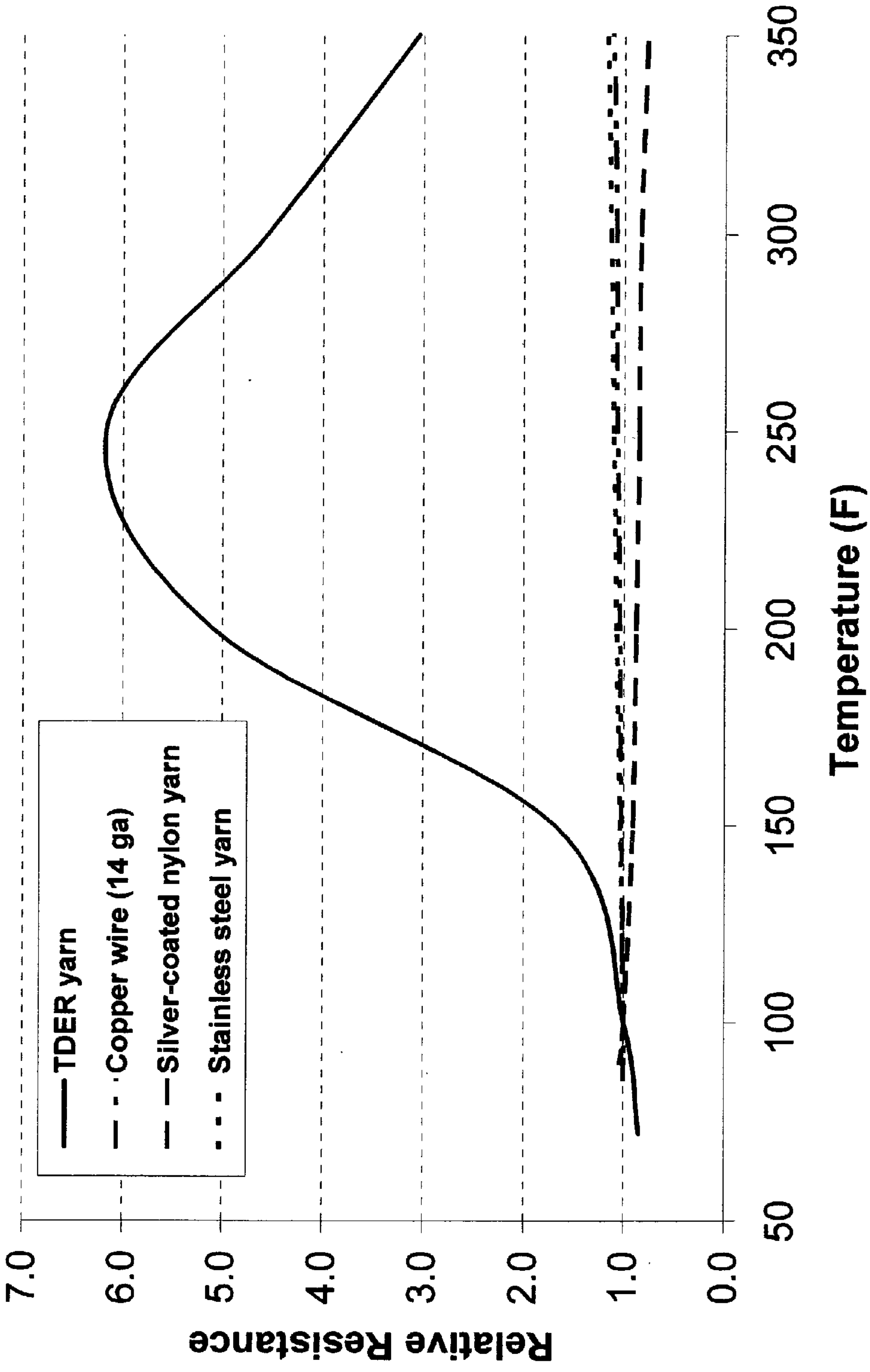
Relative Resistance
7.0
6.0
5.0
4.0
3.0
2.0
1.0
0.0
50
100
150
200
250
300
350
Temperature (F)
TDER yarn
Copper wire (14 ga)
Silver-coated nylon yarn
Stainless steel yarn

FIGURE 3

TEMPERATURE DEPENDENT ELECTRICALLY RESISTIVE YARN

BACKGROUND

[0001] The present invention relates generally to electrically conductive yarns, and in particular, to electrically conductive yarns providing a resistance that is variable with temperature.

[0002] Electrically conductive elements have been used as heating elements in textiles such as knit or woven fabrics. The electrically conductive elements are incorporated into the textile, and electricity is passed though the electrically conductive elements. Therefore, there is a need for electrically conductive elements, such as yarns for use in items such as textiles.

BRIEF DESCRIPTION OF THE DRAWINGS

[0003] **FIG. 1** shows an enlarged cross-sectional view of an embodiment of the present invention, illustrated as a temperature variable resistive yarn;

[0004] **FIG. 2** shows a graph of current as a function of voltage through one inch of one embodiment of the yarn in the present invention; and

[0005] **FIG. 3** shows a graph illustrating the different temperature dependence of the electrical resistance of one embodiment of a yarn made according to the present invention, and "conventional" conducting materials that might be put into a fabric.

DETAILED DESCRIPTION

[0006] Rearing to **FIG. 1**, there is shown a temperature dependent electrically resistive yarn **10** illustrating one embodiment of the present invention. The yarn **10** generally comprises a core yarn **100** and a positive temperature coefficient of resistance (PTCR) sheath **200**. The yarn **10** can also include an insulator **300** over the PTCR sheath **200**. As illustrated, the temperature variable resistive yarn **10** is a circular cross section; however, it is anticipated that the yarn **10** can have other cross sections which are suitable for formation into textiles, such as oval, flat, or the like.

[0007] The core yarn **100** is generally any material providing suitable flexibility and strength for a textile yarn. The core yarn **100** can be formed of synthetic yarns such as polyester, nylon, acrylic, rayon, Kevlar, Nomex, glass, or the like, or can be formed of natural fibers such as cotton, wool, silk, flax, or the like. The core yarn **100** can be formed of monofilaments, multifilaments, or staple fibers. Additionally, the core yarn **100** can be flat, spun, or other type yarns that are used in textiles. In one embodiment, the core yarn **100** is a non-conductive material.

[0008] The PTCR sheath **200** is a material that provides increased electrical resistance with increased temperature. In the embodiment of the present invention, illustrated in **FIG. 1**, the sheath **200** generally comprises distinct electrical conductors **210** intermixed within a thermal expansive low conductive (TELC) matrix **220**.

[0009] The distinct electrical conductors **210** provide the electrically conductive pathway through the PTCR sheath **200**. The distinct electrical conductors **210** are preferably particles such as particles of conductive materials, conductive-coated spheres, conductive flakes, conductive fibers, or the like. The conductive particles, fibers, or flakes can be formed of materials such as carbon, graphite, gold, silver, copper, or any other similar conductive material. The coated spheres can be spheres of materials such as glass, ceramic, copper, which are coated with conductive materials such as carbon, graphite, gold, silver, copper or other similar conductive material. The spheres are microspheres, and in one embodiment, the spheres are between about 10 and about 100 microns in diameter.

[0010] The TELC matrix **220** has a higher coefficient of expansion than the conductive particles **210**. The material of the TELC matrix **220** is selected to expand with temperature, thereby separating various conductive particles **210** within the TELC matrix **220**. The separation of the conductive particles **210** temperature to provide a built-in "fuse" that will cut off the conductivity of the TELC matrix **220** at the location of the selected temperature.

[0011] The insulator **300** is a non-conductive material which is appropriate for the flexibility of a yarn. In one embodiment, the coefficient of expansion is close to the TELC matrix **220**. The insulator **300** can be a thermoplastic, thermoset plastic, or a thermoplastic that will change to thermoset upon treatment, such as polyethylene. Materials suitable for the insulator **300** include polyethylene, polyvinylchloride, or the like. The insulator **300** can be applied to the PTCR sheath **200** by extrusion, coating, wrapping, or wrapping and heating the material of the insulator **300**.

[0012] A voltage applied across the yarn **10** causes a current to flow through the PTCR sheath **200**. As the temperature of the yarn **10** increases, the resistance of the PTCR sheath **200** increases. The increase in the resistance of the yarn **10** is obtained by the expansion of the TELC matrix **220** separating conductive particles **210** within the TELC matrix **220**, thereby removing the micropaths along the length of the yarn **10** and increasing the total resistance of the PTCR sheath **200**. The particular conductivity-to-temperature relationship is tailored to the particular application. For example, the conductivity may increase slowly to a given point, the rise quickly at a cutoff temperature.

[0013] The present invention can be further understood by reference to the following examples:

EXAMPLE 1

[0014] A temperature dependent electrically resistance yarn was formed from a core yarn of 500 denier multifilament polyester with a PTCR sheath of fifty percent (50%) carbon conducting particles and fifty percent (50%) EEA. The average yarn size was about 40 mils. with a denier of 8100. Prior to extruding the PTCR sheath onto the core yarn, the material for the PTCR sheath was predried at 165F for at least twenty four (24) hours. The yarn was formed by extrusion coating the TELC material onto the core yarn at a temperature of increases the electrical resistance of the PTCR sheath **200**. The TELC matrix **220** is also flexible to the extent necessary to be incorporated into a yarn. In one embodiment, the TELC matrix **220** is an ethylene ethylacrylate (EEA) or a combination of EEA with polyethylene. Other materials that might meet the requirements for a material used as the TELC matrix **220** include, but are not limited to, polyethylene, polyolefins, halo-derivitaves of polyethylene, thermoplastic, or thermoset materials.

[0015] The PTCR sheath **200** can be applied to the core **100** by extruding, coating, or any other method of applying a layer of material to the core yarn **100**. Selection of the particular type of distinct electrical conductors **210** (e.g. flakes, fibers, spheres, etc.) can impart different resistance-to-temperature properties, as well as influence the mechanical properties of the PTCR sheath **200**. The TELC matrix **220** can be formed to resist or prevent softening or melting at the operating temperatures. It has been determined that useful resistance values for the yarn **10** could vary anywhere within the range of from about 0.1 Ohms/inch to about 2500 Ohms/inch, depending on the desired application.

[**0016**] A description of attributes of a material that could be suitable as the PTCR sheath **200** can also be found in U.S. Pat. No. 3,243,753, issued on Mar. 29, 1966 to Fred Kohler, which is hereby incorporated herein in its entirety by specific reference thereto. A description of attributes of another material that could be suitable as the PTCR sheath **200** can also be found in U.S. Pat. No. 4,818,439, issued on Apr. 4, 1984 to Blackledge et al., which is also hereby incorporated herein in its entirety by specific reference thereto.

[**0017**] One embodiment of the present invention, the TELC matrix **220** can be set by cross-linking the material, for example through radiation, after application to the core yarn **100**. In another embodiment, the TELC matrix **220** can be set by using a thermosetting polymer as the TELC matrix **220**. In another embodiment, TELC matrix **220** can be left to soften at a specific about 430F through an orifice of about 47 mils. at a pressure of about 6600 psi. The coated core yarn was quenched in water at a temperature of about 85F. The resistance of the yarn was about 350 Ohms/inch at about 72F. The final yarn had a tenacity of about 9.3 lbs and an elongation at breaking of about 12%, giving a stiffness of 4.3 grams/denier %

EXAMPLE 2

[**0018**] The yarn of Example 1 was coated with an insulation layer of polyethylene. The polyethylene was Tenite 812A from Eastman Chemicals. The polyethylene was extruded onto the yarn at a temperature of about 230F. at a pressure of about 800 psi, and was water quenched at a temperature of about 75F. The final diameter of the insulated yarn was about 53 mils. and had a denier of about 13,250. The resistance of the insulated yarn was about 400 Ohms/Inch at about 75F.

EXAMPLE 3

[**0019**] The yarn of Example 1 was coated with an insulation layer of polyethylene, the polyethylene being Dow 9551 from Dow Plastics. The polyethylene was extruded onto the yarn at a temperature of about 230F at a pressure of about 800 psi, and was water quenched at a temperature of about 75F. The final diameter of the insulated yarn was about 53 mils. and had a denier of about 13,250. The resistance of the insulated yarn was about 400 Ohms/inch at about 75F.

EXAMPLE 4

[**0020**] A temperature dependent electrically resistance yarn was formed from a core yarn of 500 denier multifilament polyester with a PTCR sheath of fifty percent (50%) carbon conducting particles and fifty percent (50%) EEA. The average yarn size was about 46 mils. Prior to extruding the PTCR sheath onto the core yarn, the material for the PTCR sheath was predried at 165F for at least twenty four (24) hours. The yarn was formed by extrusion coating the TELC material onto the core yarn at a temperature of about 430F through an orifice of about 59 mils. at a pressure of about 5600 psi. The coated core yarn was quenched in water at a temperature of about 70F. The resistance of the yarn was about 250 Ohms/Inch at about 72F.

EXAMPLE 5

[**0021**] A temperature dependent electrically resistance yarn was formed from a core yarn of 1000 denier multifilament Kevlar with a PTCR sheath of fifty percent (50%) carbon conducting particles and fifty percent (50%) EEA. The average yarn size was about 44 mils. Prior to extruding the PTCR sheath onto the core yarn, the material for the PTCR sheath was predried at 165F for at least twenty four (24) hours. The yarn was formed by extrusion coating the TELC material onto the core yarn at a temperature of about 415F through an orifice of about 47 mils. at a pressure of about 3900 psi. The coated core yarn was quenched in water at a temperature of about 70F. The resistance of the yarn was about 390 Ohms/Inch at about 72F.

EXAMPLE 6

[**0022**] A temperature dependent electrically resistance yarn was formed from a core yarn of 1000 denier multifilament Kevlar with a PTCR sheath of fifty percent (50%) carbon conducting particles and fifty percent (50%) EEA. The average yarn size was about 32 mils. Prior to extruding the PTCR sheath onto the core yarn, the material for the PTCR sheath was predried at 165F for at least twenty four (24) hours. The yarn was formed by extrusion coating the TELC material onto the core yarn at a temperature of about 415F through an orifice of about 36 mils. at a pressure of about 3700 psi. The coated core yarn was quenched in water at a temperature of about 70F. The resistance of the yarn was about 1000 Ohms/Inch at about 72F.

[**0023**] Referring now to **FIG. 2**, there is show a graph of current as a function of voltage through one inch of the yarn from Example 1. A 4-probe resistance setup was used to apply a steadily increasing DC voltage to the yarn in ambient air. The voltage across and current through a 1-inch length of yarn was monitored and plotted in **FIG. 2**. **FIG. 2** shows that the yarn of this invention can be used to limit the total current draw. The limitation on current draw both controls heat generation and helps prevent thermal stress to the yarn, reducing the possibility of broken heating elements. As shown the current draw for a yarn from Example 1 was limited to about 15 mA per yarn. A larger yarn would pass more current, as would a more conductive yarn. Conversely, a smaller or less conductive yarn would pass less current.

[**0024**] Referring now to **FIG. 3**, there is show a graph illustrating the different temperature dependence of the electrical resistance of a yarn made according to the present invention, and "conventional" conducting materials that might be put into a fabric. "TDER yarn" is the yarn from Example 1. "Copper wire" is a commercially available 14 gage single-strand wire. "Silver-coated nylon" is a 30 denier nylon yarn coated with silver, available from Instrument Specialties—Sauquoit of Scranton, Pa. "Stainless steel yarn" is a polyester yarn with 4 filaments of stainless steel twisted around the outside, available from Bekaert Fibre Technologies of Marietta, Ga. In **FIG. 3**, the Relative Resistance is the resistance of the material relative to its value at 100F. The three conventional materials all show very small temperature coefficients, whereas the resistance of the TDER yarn changes by more than a factor of 6 at 250F. As is typically the case for polymer-based PTCR materials, further heating will reduce the resistance. In actual use, products can be designed so they do not reach this temperature range during operation.

[0025] Table 1 below lists the temperature coefficients for each material in the range of 150F-200F. From the last column we see that the TDER yarn has 50 or more times the temperature coefficient of other typically available conductive materials suitable for construction of a textile.

TABLE 1

Material	Temperature coefficient (ohm/ohm/C)	Coefficient relative to TDER yarn
Copper wire:	0.00067	0.0092
Silver-coated nylon yarn:	−0.0012	−0.016
Stainless steel yarn:	0.0015	0.021
TDER yarn:	0.073	—

What is claimed is:

1. A temperature dependent electrically resistance yarn comprising:

a core yarn;

a sheath having a positive temperature coefficient of resistance, said sheath including:

a matrix material

a plurality of distinct electrical conductors intermixed throughout the matrix.

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