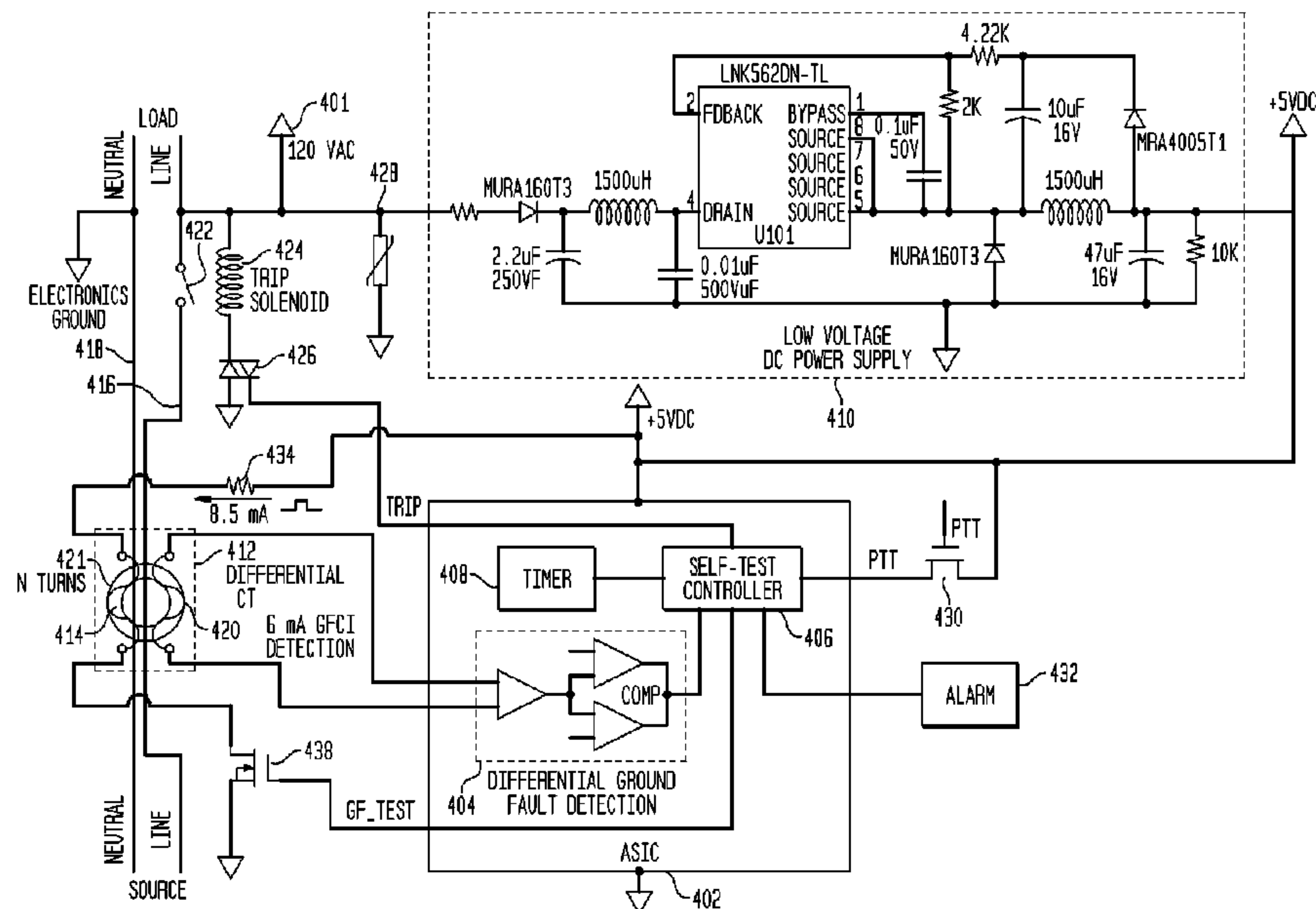




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DEVICE



(57) **Abrégé/Abstract:**

An apparatus and method for a supervisory circuit for a ground fault detection device or ground fault circuit interrupt (GFCI) device is disclosed in which a test stimulus signal for a self test of the GFCI device is generated on a second secondary winding on a toroid of a differential current transformer. The GFCI device includes line and neutral conductors configured to connect an AC power source and a load. A differential current transformer includes a toroid, through which the line and neutral conductors pass, a first secondary winding wound on the toroid to generate a current in response to an imbalance of magnetic flux in the toroid, and a second secondary winding wound on the toroid. A differential ground fault detector is electrically connected to the first secondary winding of the differential current transformer to compare current generated in the secondary winding to a trip threshold. A controller is configured to control a test stimulus signal to be generated in the second secondary winding wound on the toroid of the differential current transformer.





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(57) Abstract: An apparatus and method for a supervisory circuit for a ground fault detection device or ground fault circuit interrupt (GFCI) device is disclosed in which a test stimulus signal for a self test of the GFCI device is generated on a second secondary winding on a toroid of a differential current transformer. The GFCI device includes line and neutral conductors configured to connect an AC power source and a load. A differential current transformer includes a toroid, through which the line and neutral conductors pass, a first secondary winding wound on the toroid to generate a current in response to an imbalance of magnetic flux in the toroid, and a second secondary winding wound on the toroid. A differential ground fault detector is electrically connected to the first secondary winding of the differential current transformer to compare current generated in the secondary winding to a trip threshold. A controller is configured to control a test stimulus signal to be generated in the second secondary winding wound on the toroid of the differential current transformer.

54106-1204

METHOD AND APPARATUS FOR SUPERVISORY CIRCUIT FOR GROUND
FAULT CIRCUIT INTERRUPT DEVICE

[0001] This application claims the benefit of U.S. Provisional Application No. 61/313,889, filed March 15, 2010.

BACKGROUND OF THE INVENTION

[0002] The present invention relates to ground fault detection circuits and more particularly, to testing a ground fault detection circuit using a stimulus signal on a second winding added to a differential current transformer of a ground fault detection circuit.

[0003] Ground Fault Circuit Interrupt (GFCI) devices detect the presence of ground current faults and grounded neutral faults, and interrupt power in AC power systems if such faults are detected. Accordingly, GFCI devices provide protection from electrocution and are typically used in receptacles in kitchens, bathrooms, and outdoor receptacles where there may be water or moisture that can pose a risk of electrocution. GFCI devices are also used in circuit breakers that protect these same areas of residential buildings. GFCI devices and other devices that detect ground faults and interrupt AC power systems may also be referred to generally as "ground fault detectors". Ground fault detectors typically have supervisory circuits or test circuits that check the functionality of the ground fault detection circuit.

[0004] Ground fault detectors disconnect a circuit when current leakage is detected. Current leakage occurs when current flowing through a line, or "hot" conductor, from a source load is diverted to ground without returning to the source. This leakage may result from an accidental short circuit, such as from a defective load attached to the line. If a person touches the load, the leakage current may pass through the person's body to ground, leading to an electric shock. Consequently, ground fault detectors, or GFCIs, act as safety devices and are designed to detect line-to-ground shorts and disconnect the distribution circuit.

[0005] Ground fault detectors also need to act quickly. While a typical circuit breaker interrupts a circuit at 20 amperes, it only takes approximately 100

milliamperes to electrocute a person. Therefore, for added safety, ground fault detectors should be able to detect current flow between a line and ground at current levels as little as 6 milliamperes and trip a breaker at the receptacle or at the breaker panel to remove the shock hazard. Ground fault detectors are typically required for receptacles in bathrooms and other areas exposed to water in order to prevent deadly ground fault situations from occurring.

[0006] In two-line systems, GFCIs typically detect current leakage by comparing the current flowing in the line and returning in the neutral. A difference in current levels implies that some current has leaked from the circuit and a ground fault exists. GFCIs typically use a differential transformer to detect a difference in the current levels in the line and the neutral. The differential transformer is often a toroidal core that has as its primary windings the line and neutral conductors of the distribution circuit being protected, which are encircled by the core. The secondary windings of the transformer are wrapped around the core. During normal conditions, the current flowing in one direction through the line conductor will return in the opposite direction through the neutral conductor. This balance produces a net current flow of zero through the differential transformer, and the multi-turn winding provides no output. If a fault exists, current leaks from the line conductor to ground and the current flowing back through the line and neutral conductors in the differential transformer will not be equal. This current imbalance will produce uncanceled flux in the differential transformer's core, resulting in an output from the multi-turn secondary winding. Detection circuitry identifies the output from the differential transformer and opens the circuit breaker contacts.

BRIEF SUMMARY OF THE INVENTION

[0007] The present invention provides an apparatus and method for a supervisory circuit in a ground fault detection device, such as a ground fault circuit interrupt (GFCI) device. Embodiments of the present invention utilize a stimulus on a second winding added to a differential current transformer for a self test of a GFCI device. This reduces the amplitude of the test current needed to test the GFCI device and simplifies assembly of the GFCI device.

[0008] In one embodiment of the present invention, a GFCI device includes line and neutral conductors configured to connect an AC power source and

54106-1204

a load. A differential current transformer includes a toroid, through which the line and neutral conductors pass, a first secondary winding wound on the toroid to generate a current in response to an imbalance of magnetic flux in the toroid, and a second secondary winding wound on the toroid. A differential ground fault detector is
5 electrically connected to the first secondary winding of the differential current transformer to compare current generated in the first secondary winding to a trip threshold. A controller is configured to control a test stimulus signal to be generated in the second secondary winding wound on the toroid of the differential transformer. A low voltage DC power supply can be electrically connected to the second secondary
10 winding to generate the test stimulus signal.

[0009] According to another embodiment of the present invention, in a method of performing a self test by a GCFI device, a test stimulus signal is generated in a second secondary winding wound on a toroid of a differential current transformer. It is then determined whether a differential current greater than a trip threshold is detected
15 in a first secondary winding wound on the toroid.

[0009a] According to one aspect of the present invention, there is provided a ground fault detection device comprising: line and neutral conductors configured to connect an AC power source and a load; a differential current transformer comprising: a toroid, through which the line and neutral conductors pass, a first
20 secondary winding wound on the toroid configured to generate a current in response to an imbalance of magnetic flux in the toroid, and a second secondary winding wound on the toroid; a differential ground fault detector electrically connected to the first secondary winding of the differential current transformer and configured to compare the current generated in the first secondary winding to a predetermined
25 threshold; a controller configured to control a test stimulus signal to be generated in the second secondary winding; and a DC power supply electrically connected to the second secondary winding wound on the toroid of the differential current transformer, wherein the controller is configured to control the DC power supply to generate the test stimulus signal in the second secondary winding.

54106-1204

[0009b] According to another aspect of the present invention, there is provided a method of performing a self test by a ground fault detection device having a differential current transformer including a toroid, a first secondary winding wound on the toroid, and a second secondary winding wound on the toroid, comprising:

- 5 generating a test stimulus signal in the second secondary winding wound on the toroid of the differential current transformer from a low voltage DC power supply; and determining whether a differential current greater than a predetermined threshold is detected in the first secondary winding wound on the toroid.

- [0009c]** According to still another aspect of the present invention, there is
10 provided a ground fault detection device comprising: means for generating a low voltage DC test stimulus signal in a secondary winding wound on a toroid of a differential current transformer; and means for determining whether a differential current greater than a predetermined threshold is detected in another secondary winding wound on the toroid.

- 15 **[0010]** These and other advantages of the invention will be apparent to those of ordinary skill in the art by reference to the following detailed description and the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

- [0011]** FIG. 1 illustrates a GFCI device with a supervisory test circuit that
20 utilizes a low voltage DC power supply to generate a test stimulus signal;

[0012] FIG. 2 illustrates a signal timing diagram of the push-to-test self test for the GFCI device of FIG. 1;

[0013] FIG. 3 illustrates a signal timing diagram of an automatic self test for the GFCI device of FIG. 1;

- 25 **[0014]** FIG. 4 illustrates a GFCI device according to an embodiment of the present invention;

54106-1204

[0015] FIG. 5 illustrates a signal timing diagram of the push-to-test self test for the GFCI device of the embodiment of FIG. 4;

[0016] FIG. 6 illustrates a signal timing diagram of an automatic self test for the GFCI device according to the embodiment of FIG. 4;

[0017] FIG. 7 illustrates a GFCI device according to another embodiment of the present invention;

[0018] FIG. 8 illustrates a signal timing diagram of the push-to-test self test for the GFCI device of the embodiment of FIG. 7;

[0019] FIG. 9 illustrates a signal timing diagram of an automatic self test for the GFCI device according to the embodiment of FIG. 7;

[0020] FIG. 10 illustrates a GFCI device according to another embodiment of the present invention;

[0021] FIG. 11 illustrates a GFCI device according to another embodiment of the present invention;

[0022] FIG. 12 illustrates a GFCI device according to another embodiment of the present invention; and

[0023] FIG. 13 illustrates a method of performing a self test by a GFCI device according to an embodiment of the present invention.

DETAILED DESCRIPTION

[0024] The present invention relates to a supervisory circuit for testing Ground Fault Circuit Interrupt (GCFI) devices. Many GFCI devices have a "test" button for verifying the health of a device. Test methods may create a small imbalance by passing a stimulus signal current through the core of the differential transformer. For example, pressing the test button may cause the 120 volt AC power supply to be drawn across a 15 K resistor along a test wire that passes through the differential transformer. In this example, a current of 8 mA (milliamperes rms), which is greater than the 6 mA leakage current detection requirement for GFCI circuits, passes through the differential transformer. The differential transformer and detection circuitry in a properly functioning device would detect the test current as an imbalance and cause the circuit to trip. The tester interprets this result as meaning the circuit breaker device is working safely and correctly. If the circuit breaker does not trip, the tester may assume the circuit has a problem that may be dangerous and require a specialist's attention and possible replacement of the device. Some GFCI devices also include a reset button for resetting the breaker after it has tripped.

54106-1204

[0025] In the near future, many GFCI devices may also include auto self test functions that are initiated internally at periodic intervals to verify the health of the device. Such devices consist of a timer and an electromechanical or an electronic switch that electrically connects the 120 volt AC power supply across a resistor along a test wire that passes through the differential transformer.

[0026] The present inventors have recognized the following problems with conventional supervisory test circuits, whether the test circuit is closed using mechanical switch or an electronic switch. First, conventional test circuits are directly exposed to noise that exists on the line conductor of the AC power supply, which can possibly interfere with the test. Second, the AC power supply can fluctuate in voltage resulting in a rather large variance of stimulus signal current creating test escape conditions. Third, the test circuit dissipates about 1 watt of power when exercised from a 120 volt AC supply.

[0027] With automatic self tests and the use of an electronic switch, the power dissipation of the test circuit becomes more of a problem. Another problem using electronic switches is direct exposure to high voltages on the line conductor of the AC supply. Components with higher rated power and higher rated voltage are larger in size and cost more than components with lower rated power and lower rated voltages.

[0028] U.S. Patent Application No. 13/041,704, filed March 7, 2011, entitled "Method and Apparatus for Supervisory Circuit for Ground Fault Circuit Interrupt Device", describes a supervisory circuit to test ground fault detection circuits by implementing a low voltage DC power supply from which to directly generate a test stimulus signal, typically a current, instead of directly from the line conductor of the 120 volt supply. A low voltage DC power supply provides filtering of any noise present on the line conductor of the 120 volt supply, thus preventing interference with the test from the test stimulus signal itself.

[0029] A low voltage DC power supply is typically regulated to within approximately 100 millivolts to provide a constant DC output voltage, thus eliminating any problems caused by large fluctuations in voltage of the AC supply. As a result, the test stimulus signal's current amplitude does not need to be set 15 to 20 percent higher than the rated trip threshold of the ground fault detection circuit to ensure sufficient amplitude, such as when the 120 volt AC supply is 85 percent

below rated voltage. This is a test requirement in Underwriters Laboratories (UL) 943 that governs GFCI devices in residential homes. Using a low voltage DC power supply, the test stimulus signal amplitude can be set to closer to the 6 mA rated trip threshold, thus resulting in more consistent repeatable tests that eliminate any possible test escape of a degrading trip threshold.

[0030] Power dissipation is reduced in embodiments of the present invention by using a highly efficient switching DC power supply. Power dissipated in the test circuit using a 120 volt AC power supply is approximately 1 watt ($120 \text{ volts} \times 8 \text{ mA} = 0.96 \text{ watts}$) every time the test circuit is exercised. If an 80 percent efficient switching DC power supply is implemented supplying 5 volts DC and 8.5 milliamperes of DC current (peak amplitude of 6 mA rms sinusoid), then the power dissipated in the test circuit is approximately 53 milliwatts ($5 \text{ volts} \times 8.5 \text{ mA} / 0.80$) every time the test circuit is exercised. Accordingly, components with lower rated power may be utilized in the supervisory test circuit with increased reliability due to lower electrical stress. This may not be much of a concern for devices with push to test only since the test circuit may only be exercised approximately 240 times over the life of the device if the test circuit is exercised once per month as recommended. However, for devices with auto self test, the test circuit may be exercised over 50,000 times over the life of the device.

[0031] Electronic switches in test circuits that generate the test signal stimulus directly from the line conductor of a 120 volt AC supply are subjected to transient voltages as high as 400 to 500 volts on the line conductor of a 120 volt AC supply, even with properly designed transient protection circuits that include components such as a transorb or metal-oxide varistor. These transient voltages can be reduced to just a few volts using a DC power supply to generate the test stimulus signal. Hence, an electronic switch and any other components with a much lower voltage rating may be utilized in the supervisory test circuit with increased reliability.

[0032] Many ground fault detection devices already utilize a low voltage DC power supply to provide power for the ground fault detection electronic circuits. According to various embodiments of the present invention, it may be convenient to use the same low voltage DC power supply to directly provide the stimulus signal for the test circuit instead of the line conductor of the 120 volt AC supply. Accordingly, since an addition of a low voltage DC power supply is not required for

many devices, the use of the low voltage DC power supply to provide the stimulus signal can be implemented with little or no extra cost or size to the device. The size and cost of the device can likely be reduced because various components with lower rated power and lower rated voltages can be used as compared with components used in conventional devices. Components with lower rated power and lower rated voltage are generally smaller in size and cost less than components with higher rated power and higher rated voltage. Further, an electronic switch with lower rated voltage, and a resistor that sets the current amplitude of the test stimulus signal with a lower power rating could be integrated into a CMOS detection ASIC, saving both size and cost. This can be implemented without adding an extra pin to the ASIC by reusing the pin for the control signal to the electronic switch.

[0033] The use of a low voltage DC power supply to generate the stimulus signal solves many common problems prevalent in conventional GFCI devices. However, the present inventors have recognized that the use of the low voltage DC power supply to generate the stimulus signal may introduce additional problems that need to be addressed. First, the DC power supply should be able to source additional current for a few milliseconds during a self test in addition to the current drawn by the other electronic circuits in the device. For GFCI devices that have a rated trip current of 6 milliamperes rms, this may not be an issue. However, for ground fault devices with much higher rated trip currents, such as 30 milliamperes rms and 50 milliamperes rms, this increasingly becomes an issue. Second, components from the supervisory circuit integrated into a CMOS ASIC must meet size and reliability requirements to supply a test current of 8.5 mA DC for GFCI device, or up to 71 mA DC for a 50 milliamperes rms rated ground fault detection device. Third, integrating the resistor that sets the amplitude of the test current into the ASIC limits the flexibility of the ASIC design to adapt to different rated ground fault detection devices.

[0034] Embodiments of the present invention add a second multi-turn winding on the differential current transformer in ground fault detection devices. This second winding can be used in the supervisory test circuit to provide a means to create a sufficient imbalance in the differential current transformer for successful self test purposes while reducing the current draw from the power supply, whether it is a 120 volts AC supply or a low voltage DC supply. The current drawn from the power supply is reduced by the number of turns on the winding. Hence,

54106-1204

embodiments of the present invention also reduce power dissipation in the supervisory circuit.

[0035] Embodiments of the present invention greatly reduce any additional burden placed on the low voltage DC power supply due to the generation of the test stimulus signal. Integrating components of the supervisory circuit into the low voltage ground fault detection ASIC can easily be done using standard cells without much concern about reliability issues. In addition, integrating the resistor into the ASIC does not limit flexibility of the ASIC design to adapt to different rated ground fault detection devices. The number of turns of the second winding used in the supervisory test circuit can be altered for various rated ground fault detection devices.

[0036] Embodiments of the present invention also advantageously eliminate the need to route a third wire for the supervisory test circuit through the toroid of the differential current transformer. Thus, the assembly process for routing the wire and soldering or welding the wire to a printed circuit board or terminal post can be eliminated in the factory, reducing both assembly time and cost.

[0037] Ground fault detection devices with supervisory test circuits are not just found in GFCI outlets or GFCI circuit breakers in residential buildings. These devices also have applications in protecting commercial and industrial electrical circuits. These devices may be combined with other devices such as AFCI (Arc Fault Circuit Interrupter) detection devices. Ground fault detection devices may be used in any electrical power delivery system or in any electrical equipment. Accordingly, embodiments of the present invention may be implemented in any type of ground fault detection device.

[0038] FIG. 1 illustrates a GFCI device 100 with a supervisory test circuit that uses a low voltage DC power supply 110 to directly generate a test current stimulus signal, as described in related U.S. Patent Application No. 13/041,704, filed March 7, 2011, entitled "Method and Apparatus for Supervisory Circuit for Ground Fault Circuit Interrupt Device".

As illustrated in FIG. 1, the GFCI device 100 includes an ASIC 102, which includes a differential ground fault detection circuit 104 and circuitry for a self test, such as a self test controller 106 and a timer 108. The GFCI device 100 further includes a DC power supply 110 to power the ASIC 102 and to directly generate the test current stimulus signal. A differential current transformer 112 is built on a toroid 114, with

the line conductor 116 and the neutral conductor 118 passing through the toroid 114 and a secondary winding 120 wound on the toroid 114. A main mechanical contact switch 122 is provided in the line conductor 116, and a trip solenoid 124 and accompanying electrical switch 126 are used to trip the main mechanical contact switch 122. A high current transient voltage suppressor component 128 is electrically connected from the line conductor 116 to the neutral conductor 118, which in this case is also an electronics ground. A PTT (Push-To-Test) button 130 can be pushed by an operator to initiate a self test. An alarm 132 alerts the operator of an automatic self test failure. The supervisory test circuit of the GFCI device 100 is comprised of a resistor 134, a third wire 136 passing through the toroid 114 of the transformer 112, and an electronic switch 138.

[0039] Basic function of the GFCI device 100 of FIG. 1 is as follows. Current leaking from the line conductor 116 on the load side of the main mechanical contact switch 122 of the device back to ground, or to neutral on the source side of the device through some path other than the neutral conductor 118, creates an imbalance of magnetic flux in the toroid 114 of the differential current transformer 112, causing a current to flow in the secondary windings 120. The terminals of the secondary winding 120 are electrically connected to input pins of the differential ground fault detection circuit 104 contained in an ASIC 102. The detection circuit 104 may amplify the input current signal and compare the amplitude to a predetermined trip threshold. In devices that have automatic self test, the self test controller 106 allows or inhibits the output signal of the detector 104 to pass through to an output pin of the ASIC 102. In particular, if an automatic self test is not being performed, the self test controller 106 allows the output signal to pass through to the output pin of the ASIC 102. The output pin of the ASIC 102 is electrically connected to a control pin of the electronic switch 126, and the output signal (TRIP) is transmitted to the electronic switch 126. One terminal of the electronic switch 126 is electrically connected to the electronics ground. The other terminal of the electronic switch 126 is electrically connected to one terminal of the trip solenoid 124. The other terminal of the trip solenoid 124 is electrically connected to the line conductor 116 of an AC power supply 101 on the load side of main contact switch 122. Trip solenoid 124 is mechanically located to activate a trip armature that opens the main contact switch 122 in the line conductor 116 when energized.

[0040] During normal ground fault detection mode, the self test controller 106 allows the output signal of the detector 104 to pass through to an output pin of the ASIC 102. In the case that the detected differential current exceeds the predetermined trip threshold, the output signal (TRIP) turns on or closes the electronic switch 126 which energizes the trip solenoid 124. The trip solenoid 124 activates the trip armature that opens the main contact 122 which interrupts delivery of the AC power supply 101 in the line conductor 116 to the load.

[0041] The supervisory test circuit serves to test the health of the ground fault detection device 100. A test may be initiated by the operator by pressing the push-to-test button 130 or may be initiated automatically at periodic time intervals triggered by the timer 108. The self test controller 106 monitors the push-to-test pin of the ASIC 102 and the timer 108. One terminal of the PTT button 130 is electrically connected to the push-to-test pin of the ASIC 102. The other terminal of the PTT button 130 is electrically connected to the DC power supply 110 (+5VDC). The PTT circuit can alternatively be configured such that the other terminal is connected to electronics ground for an active PTT. The control circuit outputs a signal (GF_TEST) on a pin of the ASIC 102 which is electrically connected to the control pin of electronic switch 138. One terminal of the electronic switch 138 is electrically connected to an electronics ground. The other terminal of the electronic switch 138 is electrically connected to one terminal of resistor 134 using a wire conductor 136 that is routed through the toroid 114 of the differential current transformer 112. The other terminal of the resistor 134 is electrically connected to the low voltage DC power supply 110.

[0042] In the case in which the test is initiated by an operator pressing the push-to-test button 130, the self test controller 106 transmits a signal (GF_TEST) to turn on or close the electronic switch 138. According to an advantageous implementation, the electronic switch 138 in FIG. 1 can be implemented as SI1902, a dual N-channel MOSFET manufactured by Vishay Siliconix. Turning on or closing the electronic switch 138 causes a current signal to flow directly from the low voltage DC power supply 110 through resistor 134 and wire 136 which is routed through the toroid 114 of the transformer 112, and through the electronic switch 138 to electronics ground. The amplitude of the test current stimulus signal is set by resistor 134 to a value at that is slightly above the trip threshold of the differential ground fault detection circuit 104 in the ASIC 102. For a GFCI device which has a

rated trip current of 6 milliamperes rms, or 8.5 milliamperes peak, the amplitude of the test current is set to just above 8.5 milliamperes DC. Since the test current is directly generated from the low voltage DC power supply 110, the amplitude of the test current stimulus signal remains constant when the line conductor 116 of the 120 volts AC power supply 101 drops to 85%. Accordingly, there is no need to set the amplitude of the test current stimulus signal at least 30% above the trip threshold of the differential ground fault detection circuit 104 in the ASIC 102, as in the conventional GFCI device, to guarantee detection with margin when the line conductor of the 120 volts AC supply drops to 85%.

[0043] The amount of momentary power dissipated in the supervisory circuit is reduced from 960 milliwatts (in a conventional GFCI device) to 43 milliwatts in the GFCI device 100 of FIG. 1. This allows one to use lower power rated components for the resistor 134 and the electronic switch 138 and still improve component reliability. This is important for devices that include automatic self test since the supervisory test circuit will be exercised periodically over 50,000 times over a lifetime of 20 years. Intentionally passing the stimulus current through the toroid 114 of the transformer 112 creates an imbalance of magnetic flux in the toroid 114 of the differential current transformer 112, causing a current to flow in the secondary windings 120. The current in the secondary windings 120 is detected by the ground fault detector circuit 104 in the ASIC 102.

[0044] During a push-to-test self test, the self test controller 106 can allow the output signal of the detector 104 to pass through to an output pin of the ASIC 102. The test current stimulus signal generated by the supervisory test circuit results in a detected differential current that exceeds the predetermined trip threshold. The detector output signal (TRIP) turns on or closes electronic switch 126 which energizes the trip solenoid 124. The trip solenoid 124 activates a trip armature that opens the main contact switch 122, which interrupts delivery of the 120 volts AC power supply 101 in the line conductor 116 to the load. Typically, a mechanical switch arm moves from the ON position to a TRIP position, indicating to the operator that the push-to-test has passed. Otherwise, there is no tripping action, indicating to the operator that the push-to-test has failed.

[0045] During an automatic self test, the self test controller 106 inhibits the output signal of the detector 104 from passing through to an output pin of the ASIC 102. The test current stimulus signal generated by the supervisory test circuit

results in a detected differential current that exceeds the predetermined trip threshold. The detector output signal is inhibited by the self test controller 106, preventing the electronic switch 126 from closing and energizing the trip solenoid 124. Instead, normal operation is resumed. Otherwise, if no differential current is detected that exceeds the predetermined trip threshold after a predetermined elapsed period of time, the control circuit sends a signal to the alarm circuit 132 to alert the operator that the ground fault device is defective and needs to be replaced.

[0046] FIG. 2 illustrates a signal timing diagram of the push-to-test self test for the GFCI device 100 of the embodiment of FIG. 1. In particular, FIG. 2 shows the line conductor signal 210 of the 120 volts AC power supply 201, the push-to-test signal 220, the self test timer signal 230, the GF_TEST signal 240, the test current 250 from the low voltage DC power supply 110, the TRIP signal 260, and the ALARM signal 270 for the case in which the GFCI device 100 performs a push-to-test self test. Referring to FIGS. 1 and 2, the push-to-test signal 220 is initiated by an operator pushing the PTT button 130 at a random phase of the line conductor signal 210. The GF_TEST signal 240 is then generated by the self test controller 106 which closes the electronic switch 138 of the supervisory test circuit resulting in a test current stimulus signal 250 (e.g., 8.5 milliamperes) on wire 136 from the low voltage DC power source 110. The GF_TEST signal 240 should be present for at least one complete cycle (e.g., 16.33 milliseconds) of the line conductor signal 210 to guarantee that a test current stimulus signal 250 will be generated that exceeds the trip threshold to test the ground fault detection circuit in case there is any minimal leakage of ground fault current (less than 6 milliamperes rms, 8.5 milliamperes peak) during the negative half cycle. Once the test current signal 250 exceeds the detection threshold of the ground fault detector 104, the detector 104 outputs the TRIP signal 260 to trip the circuit breaker (e.g., switch 126).

[0047] FIG. 3 illustrates a signal timing diagram of an automatic self test for the GFCI device 100 according to the embodiment of FIG. 1. In particular, FIG. 3 shows the line conductor signal 310 of the 120 volts AC power supply 101, the push-to-test signal 320, the self test timer signal 330, the GF_TEST signal 340, the test current 350 from the low voltage DC power supply 110, the TRIP signal 360, and the ALARM signal 370 for the case in which the GFCI device 100 performs an automatic self test. Referring to FIGS. 1 and 3, the self test timer 108 transmits a

self test timer signal 330 initiating a self test at a random phase of the line conductor signal 310. The GF_TEST signal 340 is then generated by the self test controller 106 and closes the electronic switch 138 resulting in a test current stimulus signal 350 (e.g., 8.5 milliamperes) on wire 136 from the low voltage DC power source 110. The GF_TEST signal 340 should be present for at least one complete cycle (e.g., 16.33 milliseconds) of the line conductor signal 310 to guarantee that a test current stimulus signal 350 will be generated that exceeds the trip threshold to test the ground fault detection circuit in case there is any minimal leakage of ground fault current (less than 6 milliamperes rms, 8.5 milliamperes peak) during the negative half cycle. Once the test current signal 350 exceeds the detection threshold of the ground fault detector 104, the detector 104 outputs a signal 362 that is inhibited by the self test controller 106 from reaching the TRIP signal output. However, the self test controller 106 utilizes this signal 362 as a self test pass indicator. At the end of self test period, if the self test passed, the self test controller 106 resets the self test timer 108 and again enables the output of the ground fault detector 104 to the output pin of the ASIC. It is also possible that the self test timer 108 automatically starts over at zero without a reset. Otherwise, if the self-test fails, the self-test controller 106 outputs an ALARM signal 370 to the alarm circuit 132 to alert the operator of a self test failure.

[0048] FIG. 4 illustrates a GFCI device 400, according to an embodiment of the present invention, that uses an additional secondary winding 421 on the toroid 414 of the differential current transformer 412 to generate the test current stimulus signal. As illustrated in FIG. 4, the GFCI device 400 includes an ASIC 402, which includes a differential ground fault detection circuit 404 and circuitry for a self test, such as a self test controller 406 and a timer 408. The GFCI device 400 further includes a DC power supply 410 to power the ASIC 402 and to directly generate the test current stimulus signal. A differential current transformer 412 is built on a toroid 414, with the line conductor 416 and the neutral conductor 418 passing through the toroid 414, a first secondary winding 420 wound on the toroid 414 for differential current detection, and a second secondary winding 421 wound on the toroid 414 for utilization by the supervisory circuit. A main mechanical contact switch 422 is provided in the line conductor 416, and a trip solenoid 424 and accompanying electrical switch 426 are used to trip the main mechanical contact switch 422. A high current transient voltage suppressor component 428 is electrically connected

from the line conductor 416 to the neutral conductor 118, which in this case is also an electronics ground. A PTT (Push-To-Test) button 430 can be pushed by an operator to initiate a self test. An alarm 432 alerts the operator of an automatic self test failure. The supervisory test circuit of the GFCI device 400 is comprised of a resistor 434 and an electronic switch 438, which are electrically connected to the second secondary winding 421 of the differential current transformer 412.

[0049] According to an embodiment of the present invention, basic function of the GFCI device 400 of FIG. 4 is as follows. Current leaking from the line conductor 416 on the load side of the main mechanical contact switch 422 of the device back to ground, or to neutral on the source side of the device through some path other than the neutral conductor 418, creates an imbalance of magnetic flux in the toroid 414 of the differential current transformer 412, causing a current to flow in the secondary windings 420. The terminals of the first secondary winding 420 are electrically connected to input pins of the differential ground fault detection circuit 404 contained in the ASIC 402. The detection circuit 404 may amplify the input current signal and compare the amplitude to a predetermined trip threshold. In devices that have automatic self test, the self test controller 406 allows or inhibits the output signal of the detector 404 to pass through to an output pin of the ASIC 402. In particular, if an automatic self test is not being performed, the self test controller 406 allows the output signal to pass through to the output pin of the ASIC 402. The output pin of the ASIC 402 is electrically connected to a control pin of the electronic switch 426, and the output signal (TRIP) is transmitted to the electronic switch 426. One terminal of the electronic switch 426 is electrically connected to the electronics ground. The other terminal of the electronic switch 426 is electrically connected to one terminal of the trip solenoid 424. The other terminal of the trip solenoid 424 is electrically connected to the line conductor 416 of an AC power supply 401 on the load side of main contact switch 422. Trip solenoid 424 is mechanically located to activate a trip armature that opens the main contact switch 422 in the line conductor 416 when energized.

[0050] During normal ground fault detection mode, the self test controller 406 allows the output signal of the detector 404 to pass through to an output pin of the ASIC 402. In the case that the detected differential current exceeds the predetermined trip threshold, the output signal (TRIP) turns on or closes the electronic switch 426 which energizes the trip solenoid 424. The trip solenoid 424

activates the trip armature that opens the main contact 422 which interrupts delivery of the AC power supply 401 in the line conductor 416 to the load.

[0051] The supervisory test circuit serves to test the health of the ground fault detection device 400. A test may be initiated by the operator by pressing the push-to-test button 430 or may be initiated automatically at random or periodic time intervals triggered by the timer 408. The self test controller 406 monitors the push-to-test pin of the ASIC 402 and the timer 408. One terminal of the PTT button 430 is electrically connected to the push-to-test pin of the ASIC 402. The other terminal of the PTT button 430 is electrically connected to the DC power supply 110 (+5VDC). The PTT circuit can alternatively be configured such that the other terminal is connected to electronics ground for an active PTT. The control circuit outputs a signal (GF_TEST) on a pin of the ASIC 402 which is electrically connected to the control pin of electronic switch 438. One terminal of the electronic switch 438 is electrically connected to an electronics ground. The other terminal of the electronic switch 438 is electrically connected to one terminal of the second secondary winding 421 on the toroid 414 of the differential current transformer 412. The other terminal of the second secondary winding 421 is electrically connected to one terminal of the resistor 434. The other terminal of the resistor 434 is electrically connected to the low voltage DC power supply 410. Hence, this embodiment of the present invention eliminates the third wire (136 of FIG. 1) routed through the toroid of the differential current transformer, along with the assembly process of soldering or welding the wire to a printed circuit board or terminal post. The cost of adding an additional winding and pins into a packaged assembly of a differential transformer is small compared to the time and cost savings resulting from eliminating the third wire and the associated assembly process in the factory.

[0052] In the embodiment of FIG. 4, the low voltage DC power supply 410 supplies +5 VDC, but the present invention is not limited thereto. For example, the low voltage DC power supply 410 can alternatively supply a negative voltage. The low voltage DC power supply 410 can be a bridge rectifier or half wave rectifier that converts AC power from the AC power supply 401 to DC power 402. The low voltage DC power supply 410 can be implemented as a half wave rectifier, as shown in FIG. 4, but the present invention is not limited thereto. The low voltage DC power supply 410 filters the high voltage transients as well as other low voltage noise on the line conductor 416 that could potentially interfere with the self test.

[0053] In the case in which the test is initiated by an operator pressing the push-to-test button 430, the self test controller 406 transmits a signal (GF_TEST) to turn on or close the electronic switch 438. According to an advantageous implementation, the electronic switch 438 in FIG. 4 can be implemented as SI1902, a dual N-channel MOSFET manufactured by Vishay Siliconix. The part was selected by the present inventors based on a much lower voltage rating requirement of 10 to 20 volts to withstand any transient voltages that leaked through the low voltage DC power supply 410 from the line conductor of the 120 volts AC supply 401, and comes in a very small package type SOT-363, which is 2.1 millimeters by 2 millimeters. The SI1902 electronic switch behaves like a normal switch in that it is on or closed when there is gate voltage, and is off or open when the gate voltage is removed. It is to be understood that the present invention is not limited to the use of the SI1902 electronic switch, and the above description of the SI1902 electronic switch illustrates that in embodiments of the present invention in which the stimulus signal is generated from a low voltage DC power supply, an electronic switch can be used that has a lower voltage rating, cheaper price, and smaller package, as compared with the conventional GFCI device that has automatic self test capabilities.

[0054] Turning on or closing the electronic switch 438 causes a current signal to flow directly from the low voltage DC power supply 410 through resistor 434 and the second secondary winding 421 on the differential current transformer 412, and through the electronic switch 438 to electronics ground. The amplitude of the test current stimulus signal is set by resistor 434. It can be noted that any component that provides a resistance can be used as the resistor 434 to set the amplitude of the test current stimulus signal. For example, in place a traditional resistor, a field-effect transistor (FET) biased in the linear region to form a resistance could be used as the resistor 434 to set the amplitude of the test current stimulus signal. The amplitude necessary for the test current stimulus signal to create a current imbalance large enough to overcome the trip threshold can be determined based on the number of turns (N) of the second secondary winding 421 on the transformer 412. The second secondary winding 421 on the transformer 412 effectively multiplies the magnetic flux generated in the toroid 414 by the number of turns (N) of the second secondary winding 421. Therefore, the amplitude of the test current stimulus signal can be reduced by a factor of the number of turns (N) and

still create the same imbalance in magnetic flux in the toroid 414 as in the example of FIG. 1, and thus create the same amount of current flowing in the differential detection winding (first secondary winding 420) of the transformer 412. Accordingly, the amplitude of the test current stimulus signal can be set to a value such that this value multiplied by the number of turns (N) on the second secondary winding 421 results in a current in the first secondary winding 420 with an amplitude at just above the trip threshold of the differential ground fault detection circuit 404 in the ASIC 402. This can be expressed as: Test Current Amplitude X N > Trip Threshold Amplitude.

[0055] Hence, embodiments of the present invention significantly reduce the amount of current draw needed from the power supply for the self test. For example, for a GFCI device which has a rated trip current of 6 milliamperes rms, or 8.5 milliamperes peak, the example of FIG. 1 required that the test current amplitude be set just above 8.5 milliamperes DC. In an embodiment of the present invention, in which the GFCI device 400 includes a differential transformer 412 that has an additional secondary winding 421 of 10 turns used in the supervisory test circuit, the amplitude of the test current can be set to just above 0.85 milliamperes DC (8.5 milliamperes DC / 10). This can be accomplished by setting the value of the resistor 434 to 5.6 kilohms, assuming a 5 Volt DC power supply. Intentionally passing the stimulus current through the second secondary winding 421 of the transformer 412 creates an imbalance of magnetic flux in the toroid 414 of the differential current transformer 412, causing a current to flow in the first secondary winding 420 and to be detected by the ground fault detector circuit 404 in the ASIC 402.

[0056] Embodiments of the present invention significantly reduce the amount of momentary power dissipated in the supervisory circuit. In the above example in which the number of turns (N) of the second secondary winding 421 is 10, the amount of power dissipated in the supervisory test circuit is reduced from 43 milliwatts in the GFCI device 100 of FIG. 1 to 4.3 milliwatts in the GFCI device 400 of FIG. 4. This allows the utilization of even lower power rated components for the resistor 434 and the electronic switch 438 than those of the GFCI device of FIG. 1 or conventional GFCI devices, further improving component reliability. This is important for devices that include automatic self test since the supervisory test circuit will be exercised periodically over 50,000 times over a lifetime of 20 years.

[0057] During a push-to-test, the self test controller 406 can allow the output signal of the detector 404 to pass through to an output pin of the ASIC 402. The test current stimulus signal generated by the supervisory test circuit results in a detected differential current that exceeds the predetermined trip threshold. The detector output signal (TRIP) turns on or closes electronic switch 426 which energizes the trip solenoid 424. The trip solenoid 424 activates a trip armature that opens the main contact switch 422, which interrupts delivery of the 120 volts AC power supply 401 in the line conductor 416 to the load. Typically, a mechanical switch arm moves from the ON position to a TRIP position, indicating to the operator that the push-to-test has passed. Otherwise, there is no tripping action, indicating to the operator that the push-to-test has failed.

[0058] During an automatic self test, the self test controller 406 inhibits the output signal of the detector 404 from passing through to an output pin of the ASIC 402. The test current stimulus signal generated by the supervisory test circuit results in a detected differential current that exceeds the predetermined trip threshold. The detector output signal is inhibited by the self test controller 406, preventing the electronic switch 426 from closing and energizing the trip solenoid 424. Instead, normal operation is resumed. Otherwise, if no differential current is detected that exceeds the predetermined trip threshold after a predetermined elapsed period of time, the control circuit sends a signal to the alarm circuit 432 to alert the operator that the ground fault device is defective and needs to be replaced.

[0059] FIG. 5 illustrates a signal timing diagram of the push-to-test self test for the GFCI device 400 of the embodiment of FIG. 4. In particular, FIG. 5 shows the line conductor signal 510 of the 120 volts AC power supply 401, the push-to-test signal 520, the self test timer signal 530, the GF_TEST signal 540, the test current 550 from the low voltage DC power supply 410 on the second secondary winding 421, the TRIP signal 560, and the ALARM signal 570 for the case in which the GFCI device 400 performs a push-to-test self test. Referring to FIGS. 4 and 5, the push-to-test signal 520 is initiated by an operator pushing the PTT button 430 at a random phase of the line conductor signal 510. The GF_TEST signal 540 is then generated by the self test controller 406 which closes the electronic switch 438 of the supervisory test circuit resulting in a test current stimulus signal 550 from the low voltage DC power source 410 on the second secondary winding 421 of the differential current transformer 420. The GF_TEST signal 540 should be present

for at least one complete cycle (e.g., 16.33 milliseconds) of the line conductor signal 510 to guarantee that a test current stimulus signal 550 will be generated that exceeds the trip threshold to test the ground fault detection circuit in case there is any minimal leakage of ground fault current (less than 6 milliamperes rms, 8.5 milliamperes peak) during the negative half cycle. Once the test current signal 550 multiplied by the number of turns of the second secondary winding 421 exceeds the detection threshold of the ground fault detector 404, the detector 404 outputs the TRIP signal 560 to trip the circuit breaker (e.g., switch 426).

[0060] FIG. 6 illustrates a signal timing diagram of an automatic self test for the GFCI device 400 according to the embodiment of FIG. 4. In particular, FIG. 6 shows the line conductor signal 610 of the 120 volts AC power supply 401, the push-to-test signal 620, the self test timer signal 630, the GF_TEST signal 640, the test current 650 from the low voltage DC power supply 410 on the second secondary winding 421 of the differential current transformer 412, the TRIP signal 660, and the ALARM signal 670 for the case in which the GFCI device 400 performs an automatic self test. Referring to FIGS. 4 and 6, the self test timer 408 transmits a self test timer signal 630 initiating a self test at a random phase of the line conductor signal 610. The GF_TEST signal 640 is then generated by the self test controller 406 and closes the electronic switch 438 resulting in a test current stimulus signal 650 from the low voltage DC power source 410 on the second secondary winding 421 of the differential current transformer 412. The GF_TEST signal 640 should be present for at least one complete cycle (e.g., 16.33 milliseconds) of the line conductor signal 610 to guarantee that a test current stimulus signal 650 will be generated that exceeds the trip threshold in case there is any minimal leakage of ground fault current (less than 6 milliamperes rms, 8.5 milliamperes peak) during the negative half cycle. Once the test current signal 650 multiplied by the number of turns of the second secondary winding 421 exceeds the detection threshold of the ground fault detector 404, the detector 404 outputs a signal 662 that is inhibited by the self test controller 406 from reaching the TRIP signal output. However, the self test controller 406 utilizes this signal 662 as a self test pass indicator. At the end of the complete cycle self test period, if the self test passed, the self test controller 406 resets the self test timer 408 and again enables the output of the ground fault detector 404 to the output pin of the ASIC. Otherwise,

if the self-test fails, the self-test controller 406 outputs an ALARM signal 670 to the alarm circuit 432 to alert the operator of a self test failure.

[0061] FIG. 7 illustrates a GFCI device 700, according to another embodiment of the present invention. In the embodiment of FIG. 7, the required duration of the test current stimulus signal can be reduced from a complete cycle (e.g., 16.33 milliseconds) of the line conductor 716 of the AC power supply 701 to a few milliseconds by synchronizing the test current stimulus signal to the line conductor of 716 of the AC power supply 701. The components 701-738 of the GFCI device 700 of FIG. 7 operate similarly to the respective components 401-438 of the GFCI device 400 of FIG. 4 described above, other than the following differences described hereinafter.

[0062] The GFCI device 700 of FIG. 7 is similar to the GFCI device 400 of FIG. 4, but includes a resistor 742 that electrically couples the line conductor voltage of the AC power supply 701 to the ASIC 702. The ASIC 702 includes a line synchronizer circuit 740 to synchronize the test current stimulus signal to the line conductor of the AC power supply 701. One terminal of resistor 742 is electrically connected to the LINE conductor of the 120 volt AC supply 701. The other terminal is electrically connected to a pin of the ASIC 702 that is input into the line synchronizer circuit 740. The line synchronizer circuit 740 outputs a signal to the self test controller 706 when the amplitude exceeds a predetermined threshold during the positive half cycle of the line conductor of the 120 volt AC power supply 701. It is to be understood, that the line synchronizer circuit 740 can output the signal to the self test controller 706 when the amplitude exceeds a predetermined threshold during the negative half cycle of the line conductor of the 120 volt AC power supply 701, in a case in which the low voltage DC test stimulus signal is routed through the second secondary winding 721 in the opposite direction. The self test controller 706 utilizes this signal to determine when to generate the GF_TEST signal during a self test. In the embodiment of FIG. 7, the push-to-test self test and the automatic self test operate in a similar manner as described above with respect to FIG. 4. However, the timing diagram is different with the self test controller 706 utilizing the output signal from the line synchronizer circuit 740, as in the embodiment of FIG. 7.

[0063] FIG. 8 illustrates a signal timing diagram of the push-to-test self test for the GFCI device 700 of the embodiment of FIG. 7. In particular, FIG. 8 shows

the line conductor signal 810 of the 120 volts AC power supply 701, the push-to-test signal 820, the self test timer signal 830, the GF_TEST signal 840, the test current 850 from the low voltage DC power supply 710 on the second secondary winding 421 of the differential current transformer 412, the TRIP signal 860, and the ALARM signal 870 for the case in which the GFCI device 700 performs a push-to-test self test. Referring to FIGS. 7 and 8, the push-to-test signal 820 is initiated by an operator pushing the PTT button 730 at a random phase of the line conductor signal 810. The GF_TEST signal 840 is then generated by the self test controller 706 which closes the electronic switch 738 of the supervisory test circuit resulting in a test current stimulus signal 850 from the low voltage DC power source 710 on the second secondary winding 721 of the differential current transformer 712. The self test controller 706 gates the output signal from the line synchronizer circuit 740 so that the GF_TEST signal is present for only a few milliseconds during the positive half cycle of the line conductor signal 810 of the AC power supply 701. This is the optimal time to generate the test current stimulus signal 850. It is to be understood that in an alternative embodiment, the GF_Test signal could be present during the negative half cycle of the line conductor signal, in a case in which the low voltage DC stimulus signal is routed through the wire conductor 736 in the opposite direction. Once the test current signal 850 multiplied by the number of turns in the second secondary winding 721 exceeds the detection threshold of the ground fault detector 704, the detector 704 outputs the TRIP signal 860 to trip the circuit breaker (e.g., switch 726).

[0064] FIG. 9 illustrates a signal timing diagram of an automatic self test for the GFCI device 700 according to the embodiment of FIG. 7. In particular, FIG. 9 shows the line conductor signal 910 of the 120 volts AC power supply 701, the push-to-test signal 920, the self test timer signal 930, the GF_TEST signal 940, the test current 950 from the low voltage DC power supply 710 on the second secondary winding 421 of the differential current transformer 412, the TRIP signal 960, and the ALARM signal 970 for the case in which the GFCI device 700 performs an automatic self test. Referring to FIGS. 7 and 9, the self test timer 708 transmits a self test timer signal 930 initiating a self test at a random phase of the line conductor signal 910. The GF_TEST signal 940 is then generated by the self test controller 706 and closes the electronic switch 738 resulting in a test current stimulus signal 950 from the low voltage DC power source 710 on the second

secondary winding 721 of the differential current transformer 712. The self test controller 706 gates the output signal from the line synchronizer circuit 740 so that the GF_TEST signal is present for only a few milliseconds during the positive half cycle of the line conductor signal 910 of the AC supply 701. This is the optimal time to generate the test current stimulus signal 950. It is to be understood that in an alternative embodiment, the GF_Test signal could be present during the negative half cycle of the line conductor signal, in a case in which the low voltage DC stimulus signal is routed through the wire conductor 736 in the opposite direction. Once the test current signal 950 multiplied by the number of turns of the second secondary winding 721 exceeds the detection threshold of the ground fault detector 704, the detector 704 outputs a signal 962 that is inhibited by the self test controller 706 from reaching the TRIP signal output. However, the self test controller 706 utilizes this signal 962 as a self test pass indicator. At the end of the self test period, if the self test passed, the self test controller 706 resets the self test timer 708 and again enables the output of the ground fault detector 704 to the output pin of the ASIC 702. It is also possible, that the self-test timer can automatically start over at zero without a reset. Otherwise, if the self-test fails, the self-test controller 706 outputs an ALARM signal 970 to the alarm circuit 732 to alert the operator of a self test failure.

[0065] FIG. 10 illustrates a GFCI device 1000, according to another embodiment of the present invention. It is to be understood that the components 1001-1042 of the GFCI device 1000 of FIG. 10 operate similarly to the respective components 701-742 of the GFCI device 700 of FIG. 7 described above. The elements the supervisory circuit including the electronic switch 1038, the second secondary winding 1021 on the toroid 1014 of the differential current transformer 1012, and the resistor 1034 that sets the amplitude of the test current stimulus signal are connected electrically in series. These elements can be electrically connected in any order. For example, the embodiment of FIG. 10 swaps the order of the electronic switch 1038 and the second secondary winding 1021 on the toroid 1014 of the differential current transformer 1012, as compared with the electronic switch (438, 738) and second secondary winding (421, 721) in the previous embodiments.

[0066] FIG. 11 illustrates a GFCI device 1100, according to another embodiment of the present invention. It is to be understood that the components

1101-1142 of the GFCI device 1100 of FIG. 11 operate similarly to the respective components 701-742 of the GFCI device 700 of FIG. 7 described above. The embodiment of FIG. 11 swaps the order of the electronic switch 1138 and resistor 1134, as compared with the electronic switch 1038 and resistor 1034 in the embodiment of FIG. 10.

[0067] FIG. 12 illustrates a GFCI device 1200, according to another embodiment of the present invention. It is to be understood that the components 1201-1242 of the GFCI device 1200 of FIG. 12 operate similarly to the respective components 701-742 of the GFCI device 700 of FIG. 7 described above. In the embodiment of FIG. 12, the electronic switch 1238 and the resistor 1234 are integrated into the ASIC 1202. As described above, various embodiments of the present invention enable a low voltage rated components to be used for the electronic switch 1238 and the resistor 1234. This allows the electronic switch 1238 and the resistor 1234 to be integrated into a low power, low voltage CMOS ASIC 1202, which can reduce cost and board space. In addition, the integration of the electronic switch 1238 and the resistor 1234 into the ASIC 1202 can be done without adding any additional pins to the ASIC 102 by reusing the pin for the GF_TEST signal. As shown in FIG. 12, in this embodiment, the DC test stimulus signal is generated inside the ASIC 1202 from the DC power supplied to the ASIC 1202. Furthermore, although FIG. 12 shows the DC power supply 1210 being separate from the ASIC 1202, the present invention is not limited thereto. In another possible embodiment, the DC power supply circuitry can be included inside the ASIC instead of separate from the ASIC.

[0068] One problem with the GFCI device 100 of FIG. 1 is the relatively high amplitude of the test current that needs to be generated for the self test. Components of the supervisory circuit integrated into a CMOS ASIC must meet size and reliability requirements to supply a test current of 8.5 mA DC for 6 milliamperes rms rated GFCI device, 43 mA DC for a 30 milliamperes rms rated ground fault detection device, or up to 71 mA DC for a 50 milliamperes rms rated ground fault detection device. Another problem with the GFCI device 100 of FIG. 1 is integrating the resistor that sets the amplitude of the test current into the ASIC would limit the flexibility of the ASIC design to adapt to different rated ground fault detection devices. Embodiments of the present invention reduce the amplitude of the test current required to be supplied by the components integrated into a CMOS ASIC,

thus enabling the use of standard size cells in silicon for these components and improving reliability. Embodiments of the present invention also allow flexibility for the ASIC 1202 to adapt to different rated ground fault devices when integrating the resistor 1234 into the ASIC 1202 since the test current can also be adjusted by changing the number of turns (N) of the second secondary winding 1221 of the differential current transformer 1212.

[0069] In the GFCI device 100 of FIG. 1, if the resistor 134 and the electronic switch 138 were to be integrated into the ASIC 102, the ASIC 102 would be required to source 8.5 mA DC for the supervisory test circuit of a 6 mA rms rated GFCI device. In the embodiment of FIG. 12, the components (resistor 1234 and electronic switch 1238) integrated into the ASIC 1202 would only be required to source 8.5 mA DC divided by the number of turns (N) of the second secondary winding 1221 on the differential current transformer 1212 for the supervisory test circuit of a 6 mA rms rated GFCI device. Hence, if the number of turns (N) is 10, then the components 1234 and 1238 integrated into the ASIC 1202 would only be required to source 0.85 mA DC. If the number of turns (N) is 20, then the components integrated 1234 and 1238 into the ASIC 1202 would only be required to source 0.425 mA DC.

[0070] Suppose the integrated resistor 1234 is set to a fixed value such that the circuit generates 0.85 mA DC. The ASIC 1202 with the integrated components for the supervisory test circuit can still be used to generate a test current stimulus signal for rated ground fault detection devices other than 6 mA rms GFCI device by simply increasing the number of turns (N) of the second secondary winding 1221 on the differential current transformer 1212. For example, a 30 mA rms rated ground fault detection device would ordinarily require 43 mA DC. If the number of turns (N) is 50, then the ASIC 1202 with the resistor 1234 set to a fixed value such that the circuit generates 0.85 mA DC would be sufficient to test a 30 mA rms rated ground fault device. Similarly, a 50 mA rms rated ground fault device would ordinarily require 71 mA DC. If the number of turns (N) is 83, then the ASIC 1202 with the resistor 1234 set to a fixed value such that the circuit generates 0.85 mA DC would be sufficient to test a 50 mA rms rated ground fault detection device.

[0071] FIG. 13 illustrates a method of performing a self test by a GFCI device according to an embodiment of the present invention. The method of FIG. 13 can be performed by the GFCI devices illustrated in FIGS. 4, 7, 10, 11, and 12.

The self-test can be an automatic self test or a "push-to-test" self test. As illustrated in FIG. 13, at step 1302 the self test is initiated. In the case of the push-to-test self test, the self test is initiated by a user pressing the push-to-test button, which causes the push-to-test signal to be sent to the self test controller. In the case of an automatic self test, the self test timer sends a signal to the self test controller to initiate the self test. At step 1304, a test stimulus signal is generated in the second secondary winding on the toroid of the differential current transformer. According to an advantageous implementation, the test stimulus signal is generated on the second secondary winding from a low voltage DC power supply. In particular, the self-test controller can control the electronic switch electrically connected to the second secondary winding and the low voltage power supply to close causing the test stimulus signal to flow from the low voltage power supply through the second secondary winding, and a resistor can control the amplitude of the test stimulus signal from the low voltage power supply. The amplitude of the test stimulus signal can be set such that the amplitude multiplied by the number of turns of the second secondary winding is greater than a trip threshold of a differential ground fault detection circuit. At step 1306, it is determined whether a differential current exceeding the trip threshold is detected by the differential ground fault detector. At step 1308, if a differential current exceeding the trip threshold is detected at step 1306, the self test passes. In the case of the push-to-test self test, when the differential current exceeding the trip threshold is detected, the TRIP signal is sent to an electronic switch which energizes a trip solenoid that activates the trip armature to open the main contact which interrupts delivery of the AC power in the line conductor. In the case of an automatic self test, when the differential current exceeding the trip threshold is detected, the TRIP signal is suppressed by the self test controller, and the self test timer is reset. At step 1310, if a differential threshold exceeding the trip threshold is not detected at step 1306, the self test fails. In the push-to-test self test, when the self test fails, no TRIP signal is generated and the main contact is not opened, which alerts the user that the test has failed. In the automatic self-test, an alarm signal is sent to the alarm circuit to alert a user that the test has failed.

[0072] The foregoing Detailed Description is to be understood as being in every respect illustrative and exemplary, but not restrictive, and the scope of the invention disclosed herein is not to be determined from the Detailed Description, but

54106-1204

rather from the claims as interpreted according to the full breadth permitted by the patent laws. It is to be understood that the embodiments shown and described herein are only illustrative of the principles of the present invention and that various modifications may be implemented by those skilled in the art without departing from the scope of the invention. Those skilled in the art could implement various other feature combinations without departing from the scope of the invention.

54106-1204

CLAIMS:

1. A ground fault detection device comprising:

line and neutral conductors configured to connect an AC power source and a load;
- 5 a differential current transformer comprising:

a toroid, through which the line and neutral conductors pass,

a first secondary winding wound on the toroid configured to generate a current in response to an imbalance of magnetic flux in the toroid, and

a second secondary winding wound on the toroid;
- 10 a differential ground fault detector electrically connected to the first secondary winding of the differential current transformer and configured to compare the current generated in the first secondary winding to a predetermined threshold;

a controller configured to control a test stimulus signal to be generated in the second secondary winding; and
- 15 a DC power supply electrically connected to the second secondary winding wound on the toroid of the differential current transformer, wherein the controller is configured to control the DC power supply to generate the test stimulus signal in the second secondary winding.
2. The ground fault detection device of claim 1, further comprising:
- 20 an application specific integrated circuit (ASIC), wherein the differential ground circuit fault detector and the controller are included on the ASIC.
3. The ground fault detection device of claim 2, wherein:

54106-1204

the DC power supply is electrically connected to the ASIC to supply power to the ASIC.

4. The ground fault detection device of claim 1, further comprising:

an electronic switch electrically connected to the second secondary
5 winding and the controller, wherein the controller is configured to control the test stimulus signal to be generated on the second secondary winding by transmitting a signal to the electronic switch to close the electronic switch.

5. The ground fault detection device of claim 4, wherein the controller is configured to transmit the signal to the electronic switch to close the electronic switch
10 for at least one complete cycle of the AC power on the line conductor.

6. The ground fault detection device of claim 4, further comprising:

a line synchronizer electrically connected to the line conductor and the controller and configured to synchronize the controller with the line conductor, wherein the controller is configured to transmit the signal to the electronic switch to
15 close the electronic switch during a positive half cycle of the AC power on the line conductor.

7. The ground fault detection device of claim 4, further comprising:

a line synchronizer electrically connected to the line conductor and the controller and configured to synchronize the controller with the line conductor,
20 wherein the controller is configured to transmit the signal to the electronic switch to close the electronic switch during a negative half cycle of the AC power on the line conductor.

8. The ground fault detection device of claim 4, further comprising:

a resistor electrically connected to the second secondary winding,
25 wherein the resistor is configured to set an amplitude of the test stimulus signal.

54106-1204

9. The ground fault detection device of claim 8, further comprising:

an application specific integrated circuit (ASIC), wherein the differential ground circuit fault detector, the controller, the electronic switch, and the resistor are included on the ASIC.

5 10. The ground fault detection device of claim 9, wherein the ASIC further includes the DC power supply electrically connected to at least one of the electronic switch and the resistor.

11. The ground fault detection device of claim 8, wherein the amplitude of the test stimulus signal multiplied by a number of turns in the second secondary
10 winding is greater than the predetermined threshold.

12. The ground fault detection device of claim 1, further comprising:

a push-to-test button, electrically connected to the controller and configured to transmit a signal to the controller in response to a user pressing the push-to-test button, wherein the controller is configured to control the test stimulus
15 signal to be generated in the second secondary winding in response to receiving the signal from the push-to-test button.

13. The ground fault detection device of claim 12, further comprising:

a main contact switch provided in the line conductor, wherein the controller is configured to trip the main contact switch in response to detection of the
20 differential current greater than the predetermined threshold in the toroid.

14. The ground fault detection device of claim 1, further comprising:

a self test timer electrically connected to the controller and configured to automatically transmit a signal to the controller, wherein the controller is configured to control the test stimulus signal to be generated in the second secondary winding in
25 response to receiving the signal from the self-test timer.

54106-1204

15. The ground fault detection device of claim 1, wherein the differential ground fault detector is configured to transmit a predetermined signal to the controller in response to detecting that the current on the first secondary winding is greater than the predetermined threshold.

5 16. The ground fault detection device of claim 15, further comprising:
 an alarm circuit electrically connected to the controller and configured to alert a user that the ground fault circuit interrupt device is defective, wherein the controller is configured to transmit an alarm signal to the alarm circuit when the test current stimulus signal is generated in the second secondary winding and the trip
 10 signal is not received from the differential ground fault detector.

17. A method of performing a self test by a ground fault detection device having a differential current transformer including a toroid, a first secondary winding wound on the toroid, and a second secondary winding wound on the toroid, comprising:

15 generating a test stimulus signal in the second secondary winding wound on the toroid of the differential current transformer from a low voltage DC power supply; and

determining whether a differential current greater than a predetermined threshold is detected in the first secondary winding wound on the toroid.

20 18. The method of claim 17, further comprising:

receiving push-to-test signal from a push-to-test button, wherein the step of generating a test stimulus signal is performed in response to receiving the push-to-test signal.

19. The method of claim 18, further comprising:

54106-1204

if the differential current greater than the predetermined threshold is detected, tripping a main contact switch of the ground fault circuit interrupt device.

20. The method of claim 17, further comprising:

receiving a self test timer signal from a self test timer, wherein the step
5 of generating a test stimulus signal is performed in response to receiving the self test timer signal.

21. The method of claim 20, further comprising:

if the differential current greater than the predetermined threshold is detected, suppressing a trip signal that trips a main contact switch of the ground fault
10 circuit interrupt device and resetting the self test timer; and

if the differential current greater than the predetermined threshold is not detected, generating an alarm to alert a user that the ground fault circuit interrupt device is defective.

22. The method of claim 17, wherein the generating a test stimulus signal in
15 the second secondary winding wound on the toroid of the differential current transformer comprises:

generating the test stimulus signal in the wire conductor from the low voltage DC power supply during a portion of a positive half cycle of an AC power signal in a line conductor of the ground fault circuit interrupt device.

20 23. The method of claim 17, wherein the generating a test stimulus signal in the second secondary winding wound on the toroid of the differential current transformer comprises:

generating the test stimulus signal in the wire conductor from the low voltage DC power supply during a portion of a negative half cycle of an AC power
25 signal in a line conductor of the ground fault circuit interrupt device.

54106-1204

24. A ground fault detection device comprising:

means for generating a low voltage DC test stimulus signal in a secondary winding wound on a toroid of a differential current transformer; and

5 means for determining whether a differential current greater than a predetermined threshold is detected in another secondary winding wound on the toroid.

25. The ground fault detection device of claim 24, wherein the means for generating a low voltage DC test stimulus signal in a secondary winding wound on a toroid of a differential current transformer comprises:

10 means for generating the low voltage DC stimulus signal in response to receiving a push-to-test signal from a push-to-test button.

26. The ground fault detection device of claim 25, further comprising:

means for tripping a main contact switch in response to detection of the differential current greater than the predetermined threshold in the toroid.

15 27. The ground fault detection device of claim 24, wherein the means for generating a low voltage DC test stimulus signal in a secondary winding wound on a toroid of a differential current transformer comprises:

means for generating the low voltage DC test stimulus signal in response to receiving a self test timer signal from a self test timer.

20 28. The ground fault detection device of claim 27, further comprising:

means for suppressing a trip signal that trips a main contact switch in response to detection of the differential current greater than the predetermined threshold in the toroid; and

54106-1204

means for generating an alarm to alert a user that the ground fault circuit interrupt device is defective in response to no detection of the differential current greater than the predetermined threshold in the toroid.

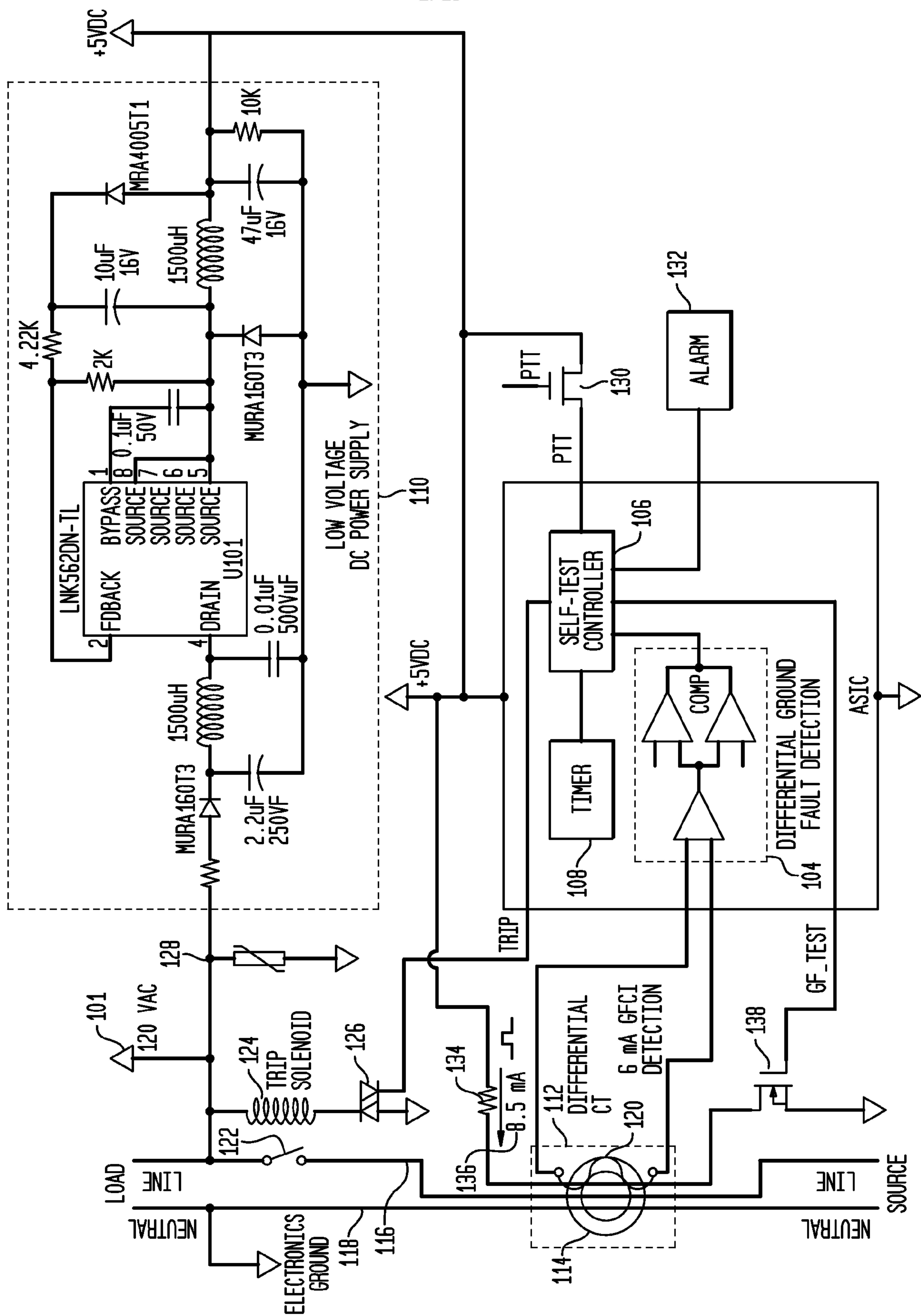
29. The ground fault detection device of claim 24, wherein the means for
5 generating a low voltage DC test stimulus signal in a secondary winding wound on a toroid of a differential current transformer comprises:

means for generating a low voltage DC test stimulus signal in the secondary winding during a portion of a positive half cycle of an AC power signal in a line conductor of the ground fault circuit interrupt device.

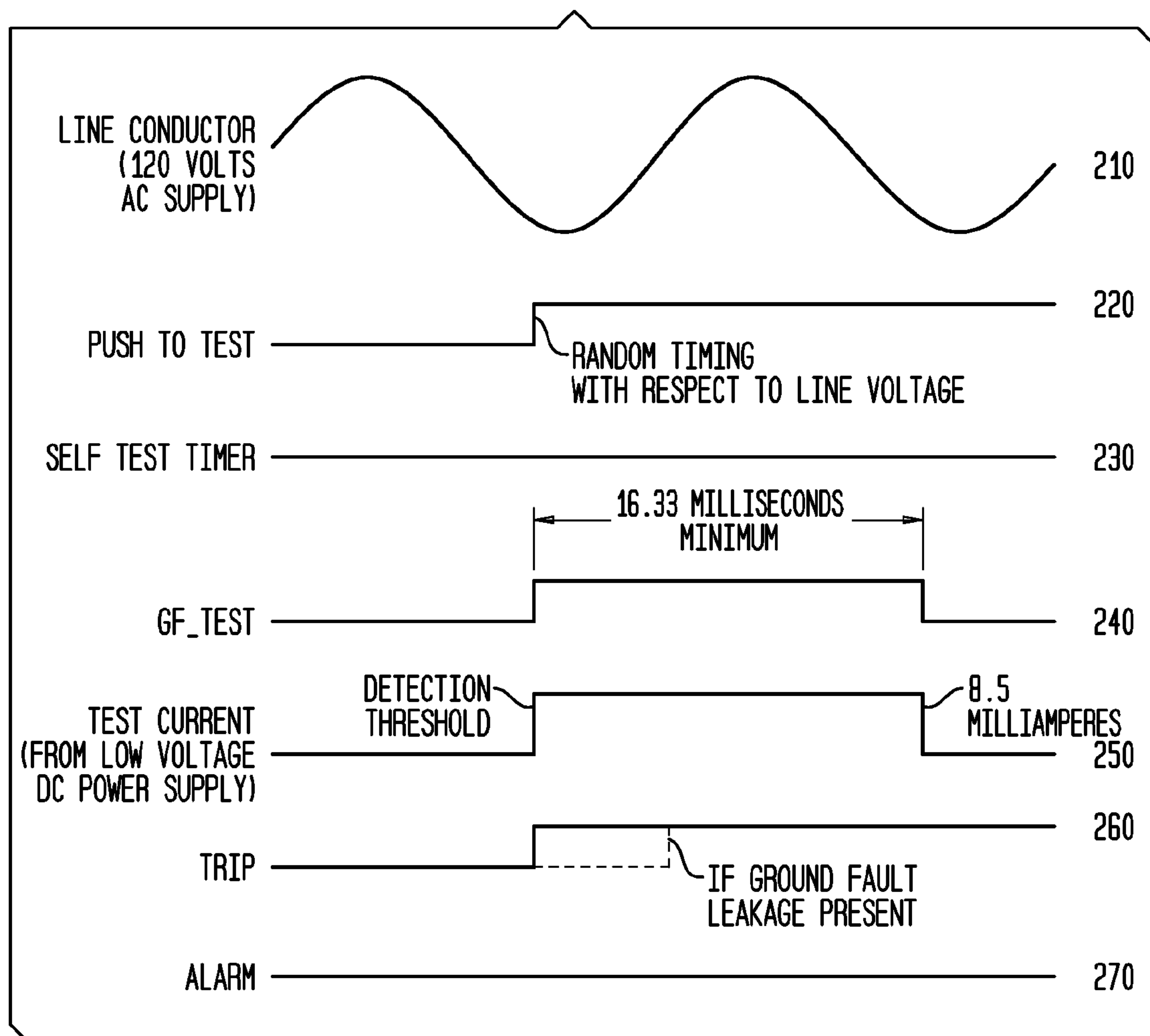
- 10 30. The ground fault detection device of claim 24, wherein the means for generating a low voltage DC test stimulus signal in a secondary winding wound on a toroid of a differential current transformer comprises:

means for generating a low voltage DC test stimulus signal in the secondary winding during a portion of a negative half cycle of an AC power signal in
15 a line conductor of the ground fault circuit interrupt device.

FIG. 1



2/13

FIG. 2

3/13

FIG. 3

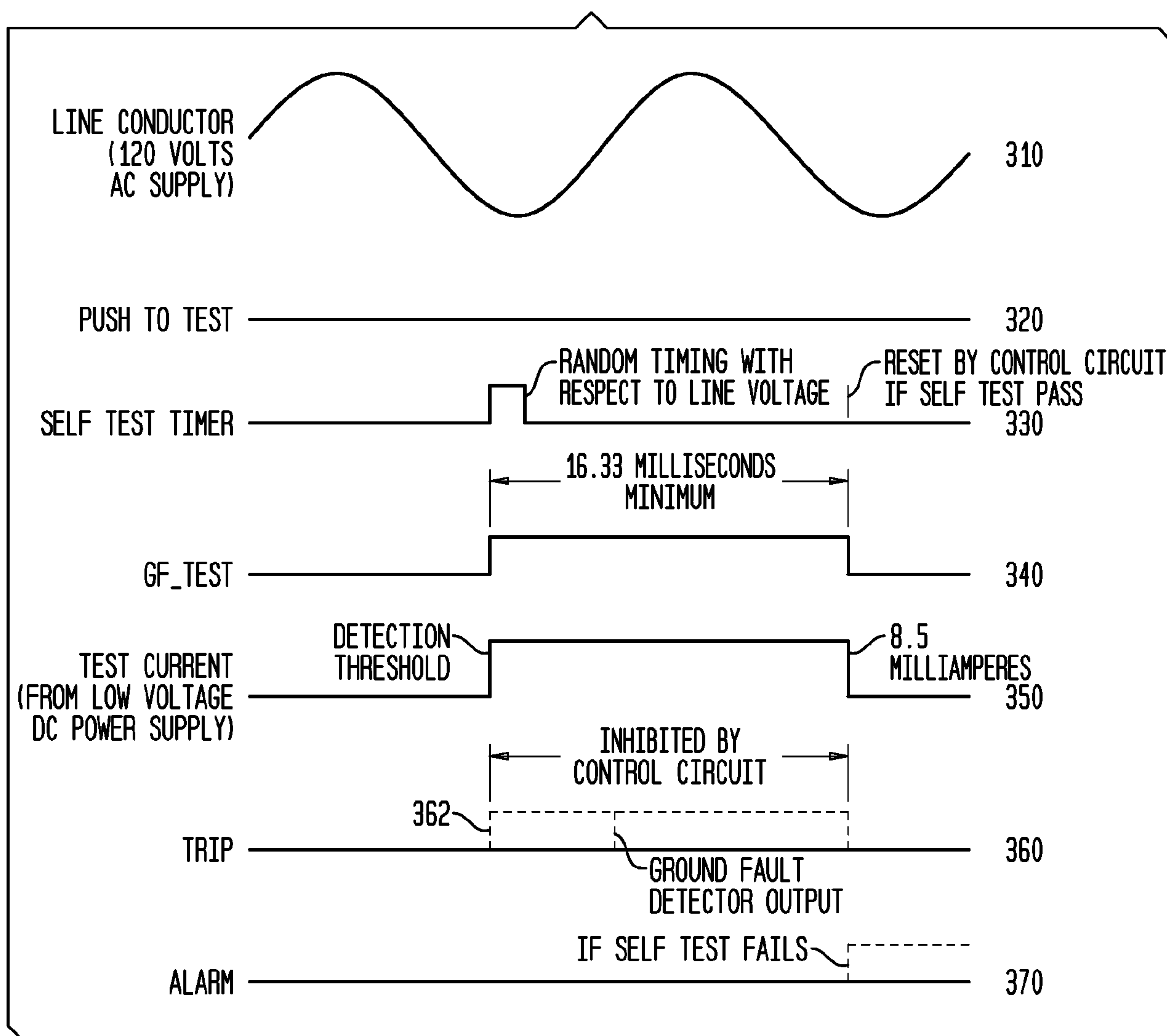
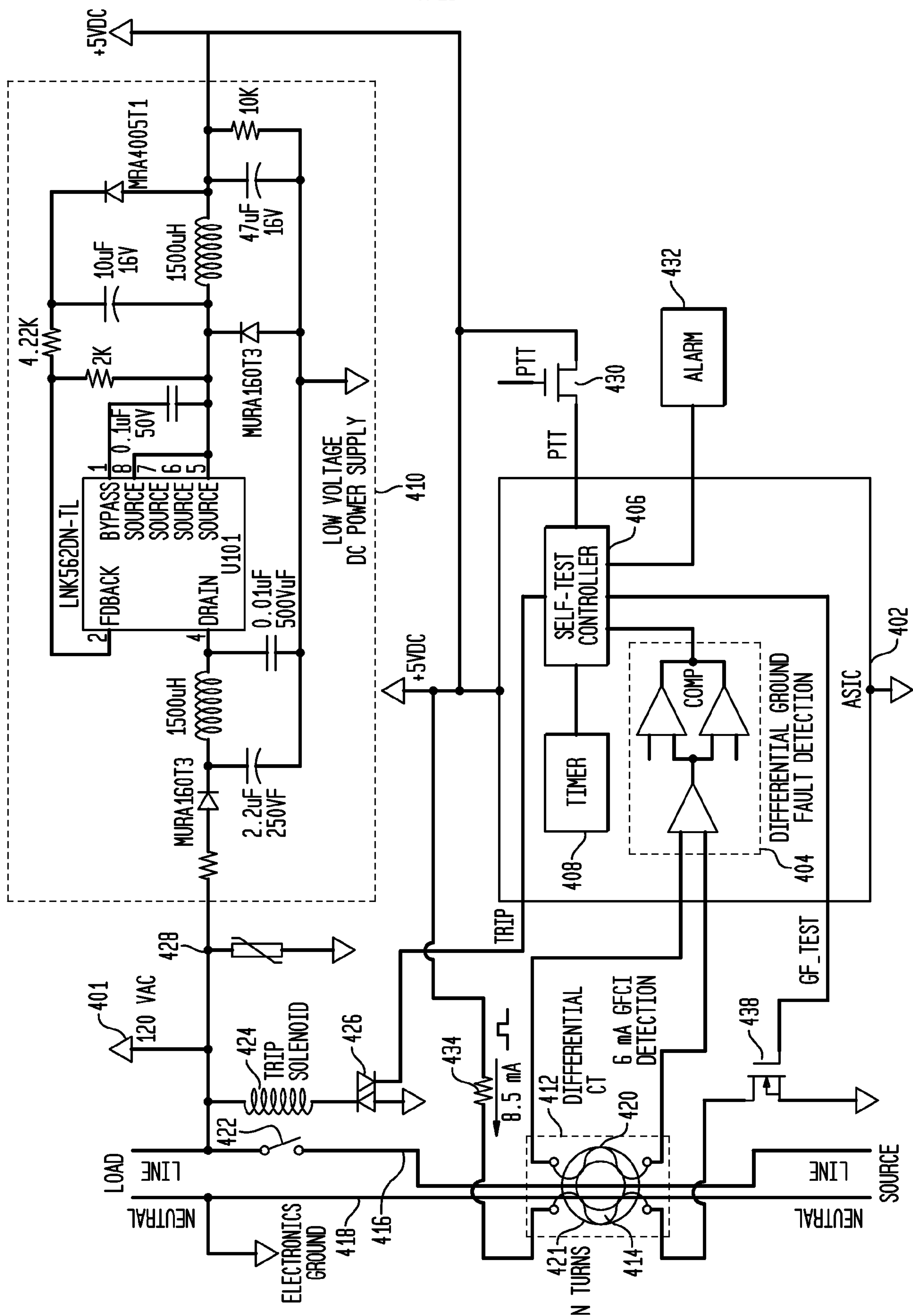
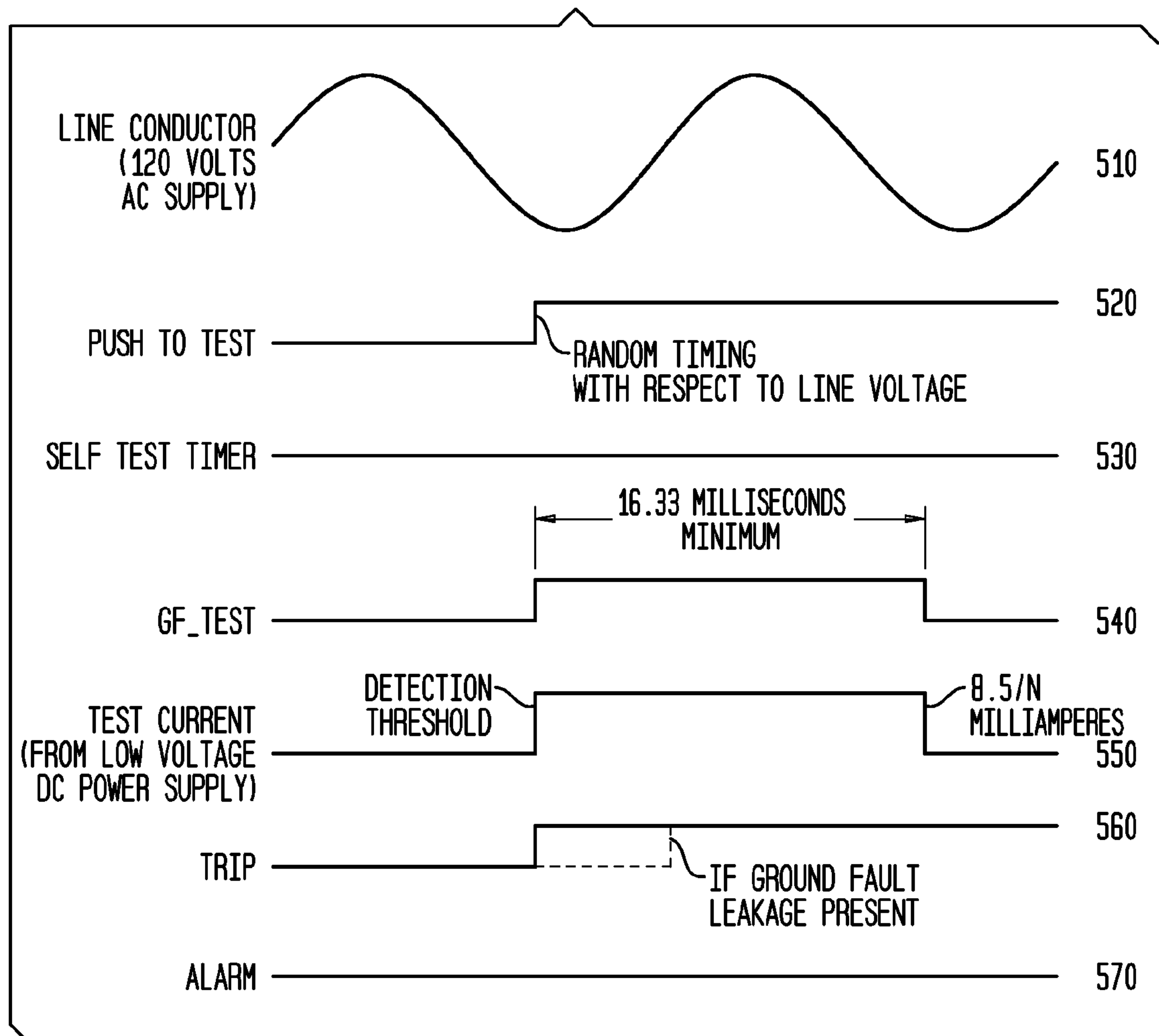


FIG. 4



5/13

FIG. 5

6/13

FIG. 6

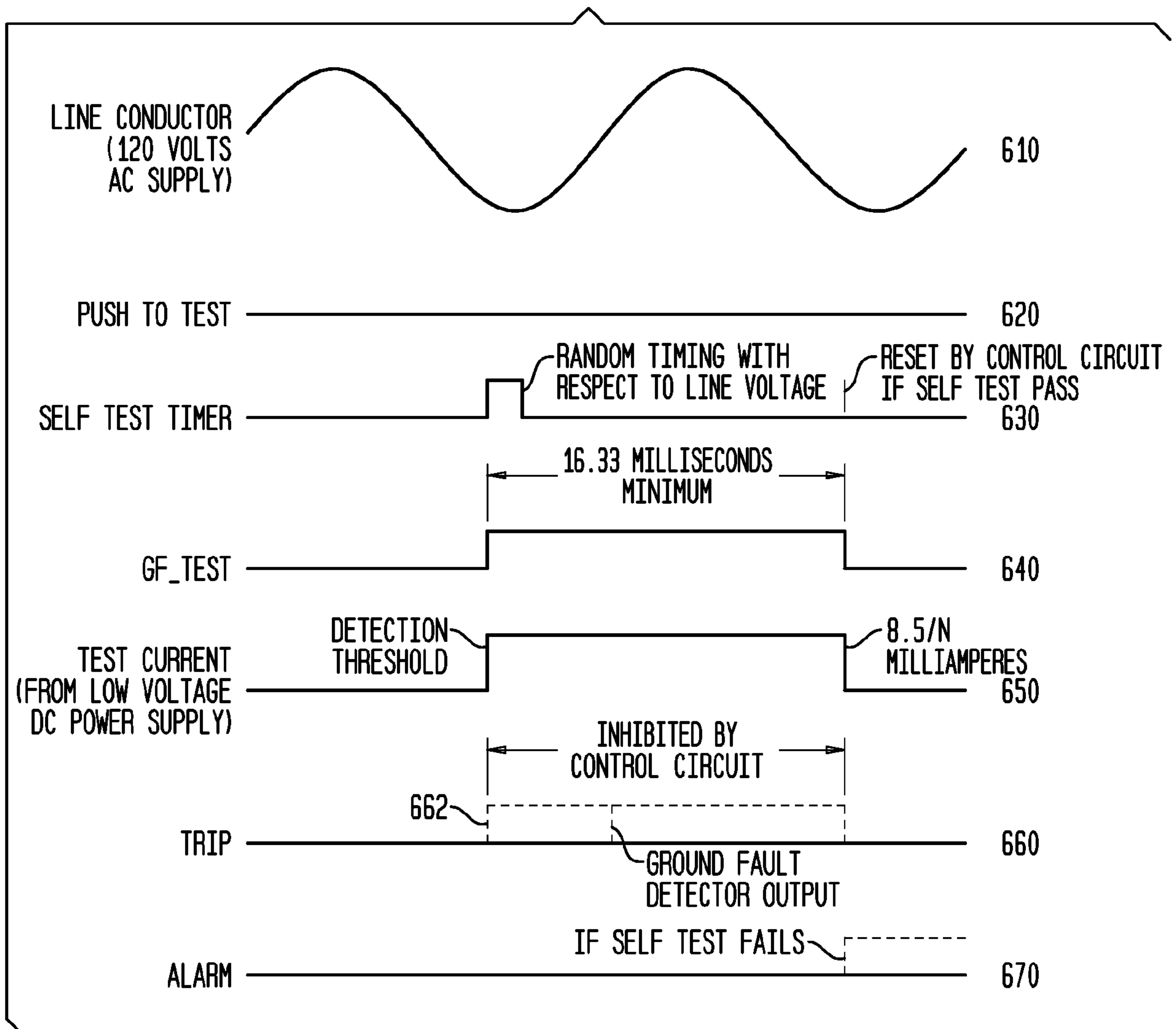
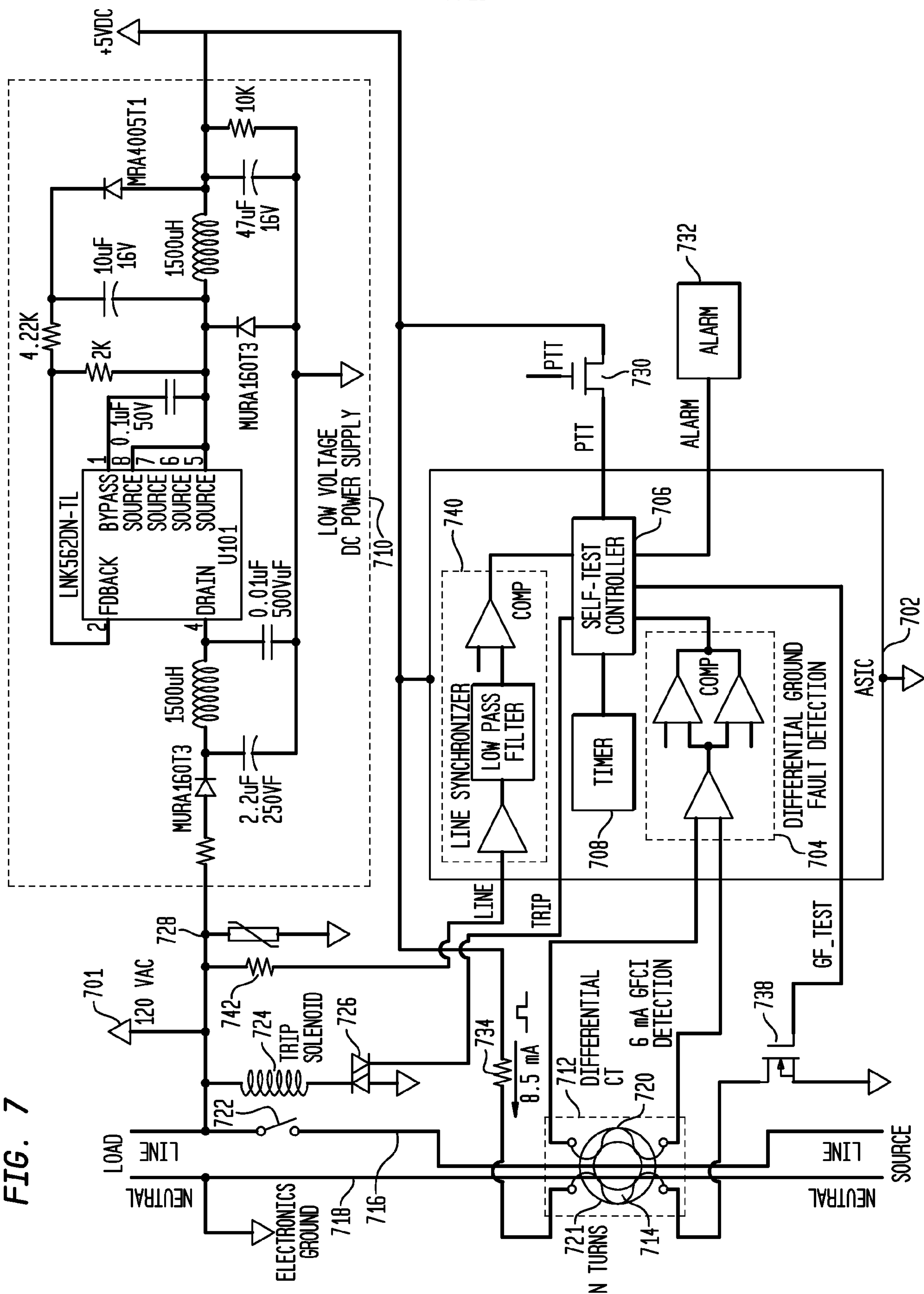
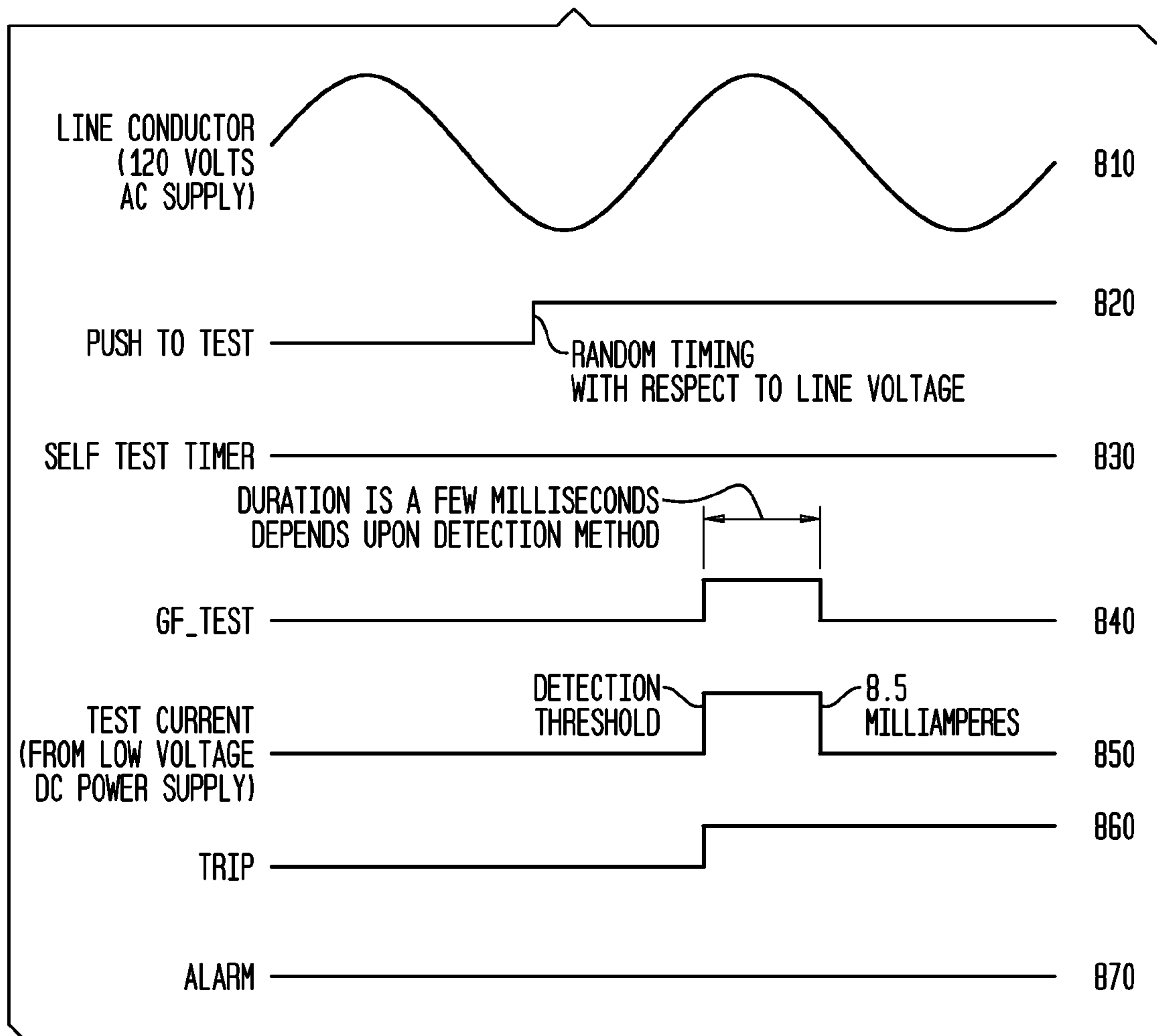


FIG. 7



8/13

FIG. 8

9/13

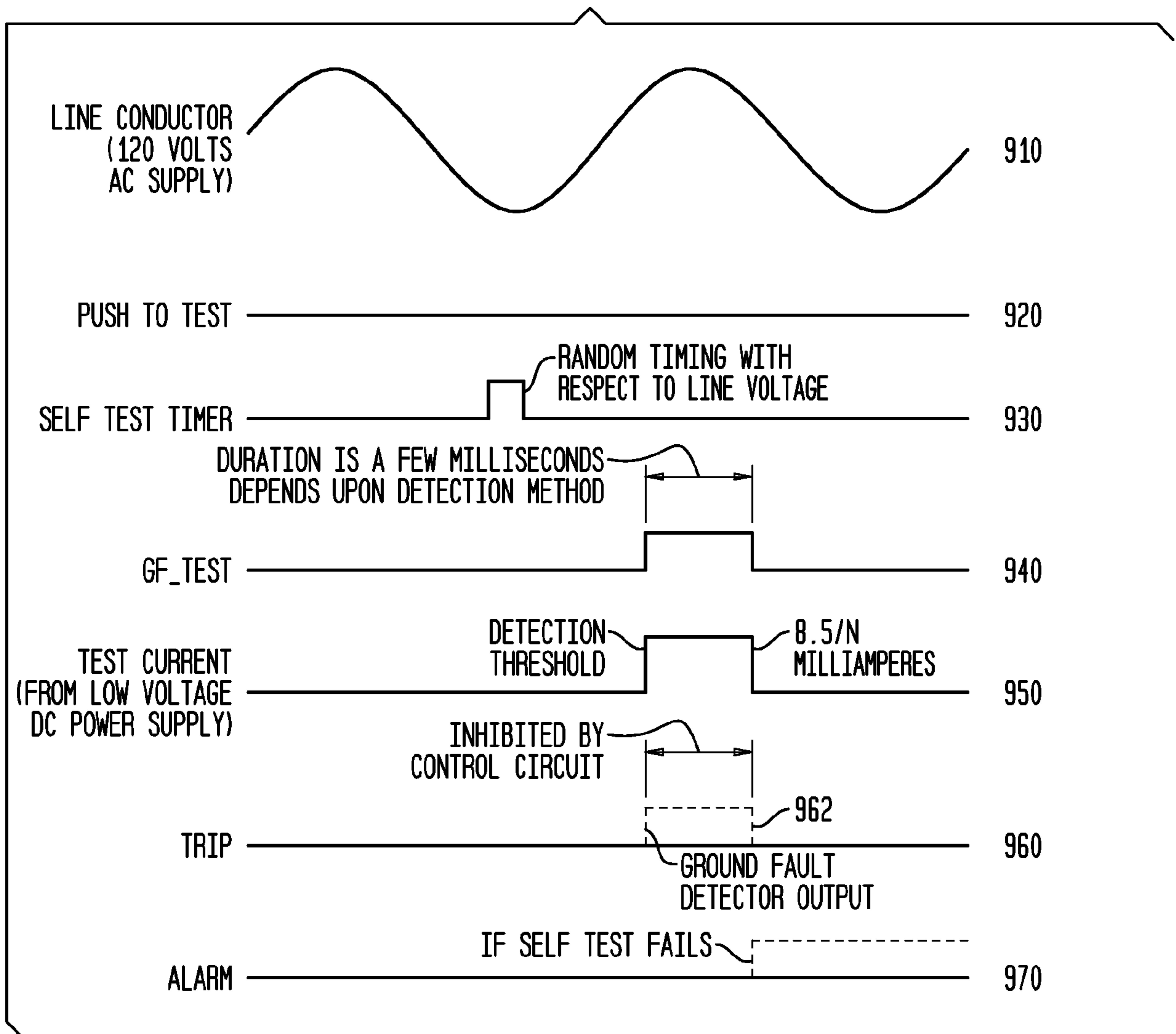
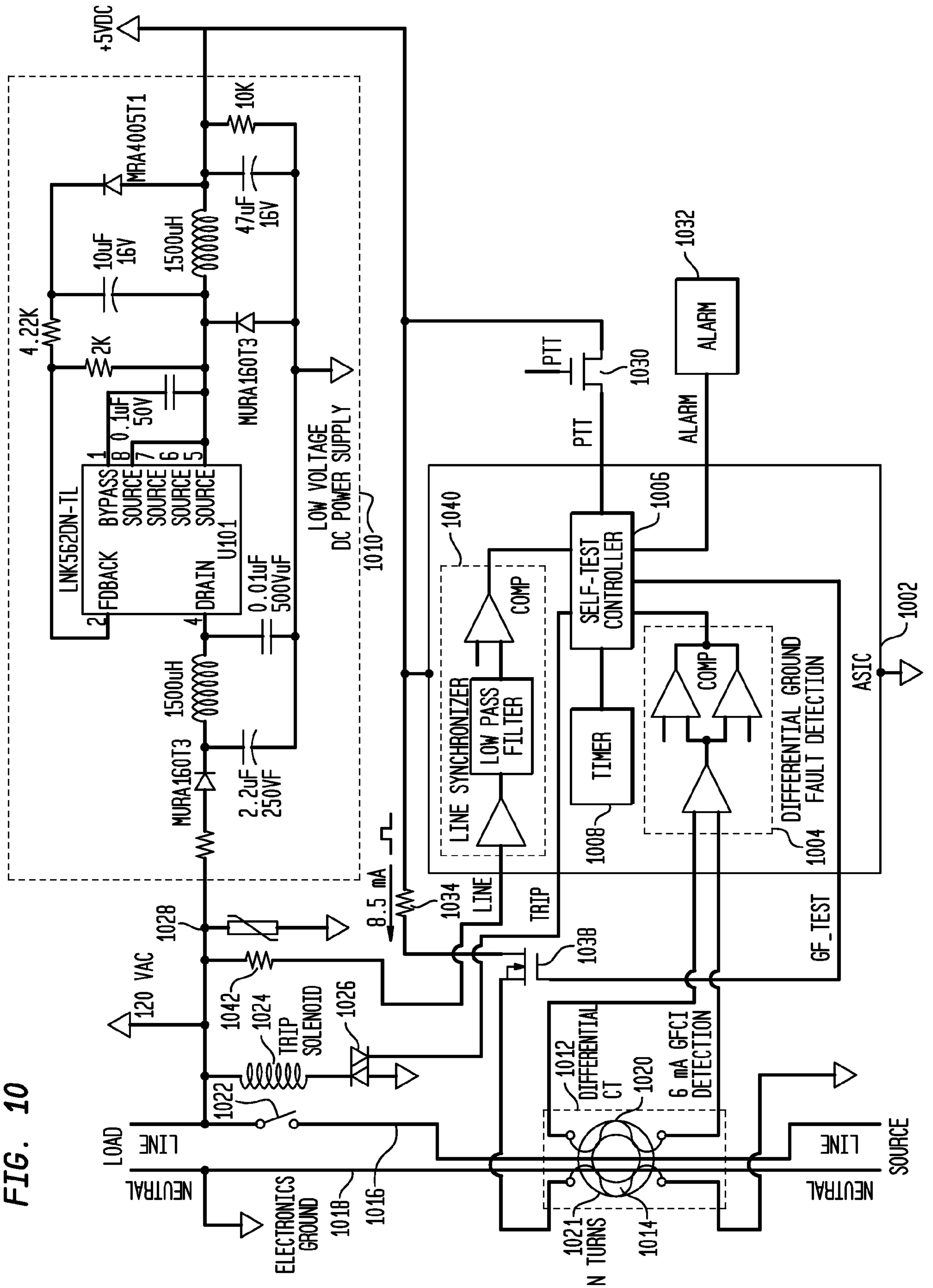
FIG. 9

FIG. 10



11/13

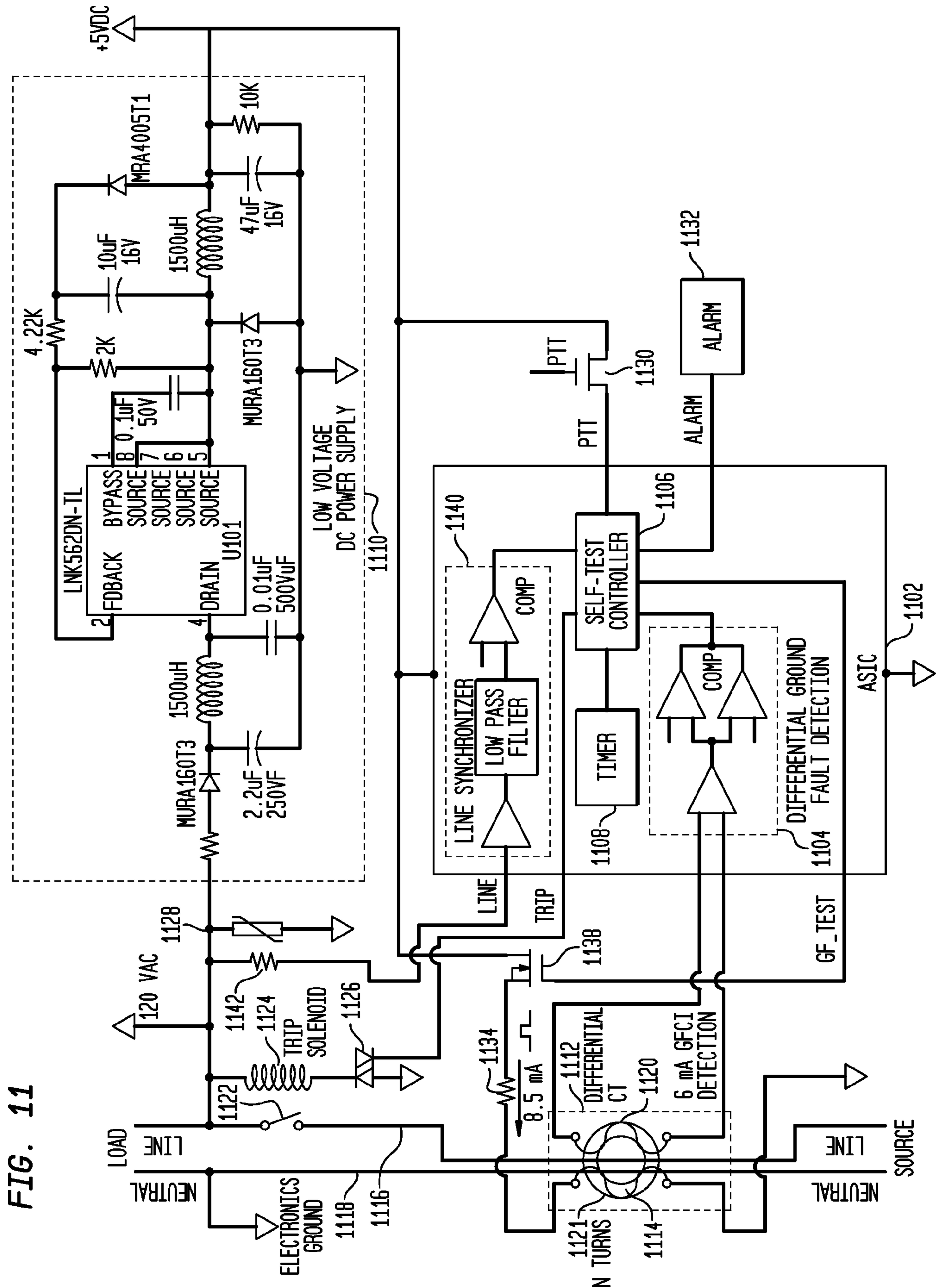
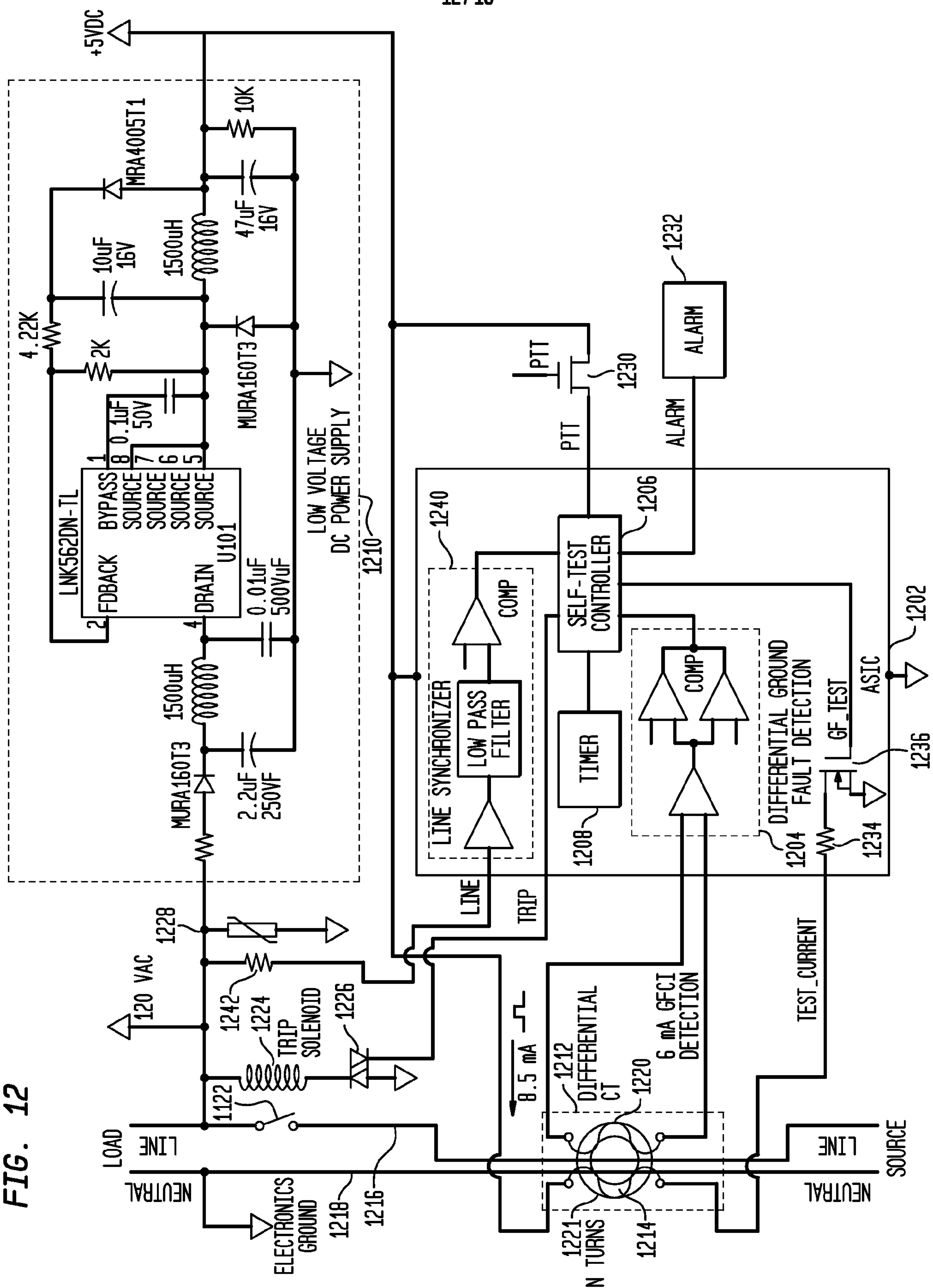


FIG. 12



13/13

FIG. 13