



**Electroluminescent Devices With Color Adjustment  
Based on Current Crowding**

5                                    CROSS-REFERENCE TO RELATED APPLICATIONS

Reference is made to the following pending and/or commonly filed U.S. patent applications, the features of which can be incorporated into the embodiments presently disclosed: U.S. Application Serial No. 61/175,640, "Re-Emitting Semiconductor Construction With Enhanced Extraction Efficiency" (Attorney Docket No. 64759US002),  
10        filed May 5, 2009; U.S. Application Serial No. 61/175,632, "Semiconductor Devices Grown on Indium-Containing Substrates Utilizing Indium Depletion Mechanisms" (Attorney Docket No. 65434US002), filed May 5, 2009; U.S. Application Serial No. 61/175,636, "Re-Emitting Semiconductor Carrier Devices For Use With LEDs and Methods of Manufacture" (Attorney Docket No. 65435US002), filed May 5, 2009; and  
15        U.S. Application Serial No. 61/221,660, "White Light Electroluminescent Devices With Adjustable Color Temperature" (Attorney Docket No. 65330US002), filed on even date herewith.

FIELD OF THE INVENTION

20                    This invention relates generally to solid state semiconductor light sources.

BACKGROUND

A wide variety of semiconductor devices, and methods of making semiconductor devices, are known. Some of these devices are designed to emit light, such as visible or  
25        near-visible (e.g. ultraviolet or near infrared) light. Examples include electroluminescent devices such as light emitting diodes (LEDs) and laser diodes, wherein an electrical drive current or similar electrical signal is applied to the device so that it emits light. Another example of a semiconductor device designed to emit light is a re-emitting semiconductor construction (RSC).

30                    Unlike an LED, an RSC does not require an electrical drive current from an external electronic circuit in order to emit light. Instead, the RSC generates electron-hole pairs by absorption of light at a first wavelength  $\lambda_1$  in an active region of the RSC. These

electrons and holes then recombine in potential wells in the active region to emit light at a second wavelength  $\lambda_2$  different from the first wavelength  $\lambda_1$ , and optionally at still other wavelengths  $\lambda_2$ ,  $\lambda_3$ , and so forth depending on the number of potential wells and their design features. The initiating radiation or “pump light” at the first wavelength  $\lambda_1$  is typically provided by a blue, violet, or ultraviolet emitting LED coupled to the RSC. Exemplary RSC devices, methods of their construction, and related devices and methods can be found in, e.g., U.S. Patent 7,402,831 (Miller et al.), U.S. Patent Application Publications US 2007/0284565 (Leatherdale et al.) and US 2007/0290190 (Haase et al.), PCT Publication WO 2009/048704 (Kelley et al.), and pending U.S. Application Serial No. 61/075,918, “Semiconductor Light Converting Construction” (Attorney Docket No. 64395US002), filed June 26, 2008, all of which are incorporated herein by reference.

When reference is made herein to a light at a particular wavelength, the reader will understand that reference is being made to light having a spectrum whose peak wavelength is at the particular wavelength.

Of particular interest to the present application are light sources that are capable of emitting white light. In some cases, known white light sources are constructed by combining an electroluminescent device such as a blue-emitting LED with first and second RSC-based luminescent elements. The first luminescent element may, for example, include a green-emitting potential well that converts some of the blue light to green light, and transmits the remainder of the blue light. The second luminescent element may include a potential well that converts some of the green and/or blue light it receives from the first luminescent element into red light, and transmits the remainder of the blue and green light. The resulting red, green, and blue light components combine to allow such a device, which is described (among other embodiments) in WO 2008/109296 (Haase), to provide substantially white light output.

Other known white light sources are constructed by combining a blue-emitting LED with a layer of yellow phosphor, such as cerium-doped yttrium aluminum garnet (YAG:Ce). Some of the blue light is absorbed by the phosphor and re-emitted as yellow light, and some of the blue light passes through the phosphor layer. The transmitted blue light combines with the re-emitted yellow light to produce an output beam having an overall output spectrum that is perceived as nominally white light.

Device-to-device variations in phosphor layer characteristics and/or other design details give rise to device-to-device differences in the output spectrum and corresponding differences in perceived color, with some LED/phosphor devices providing a “cool” white color and others providing a “warm” white color, for example. A given “shade” of white may be plotted as an (x,y) color coordinate on a conventional CIE chromaticity diagram, and can be characterized by a color temperature as is known by those skilled in the art. U.S. Patent 7,387,405 (Ducharme et al.) discusses some of these aspects of LED/phosphor devices, and reports that some commercial LED/phosphor devices exhibit color temperatures of 20,000 degrees Kelvin (20,000K) while others exhibit color temperatures of 5750K. The ‘405 patent also reports that a single one of these LED/phosphor devices allows for no control of color temperature, and that a system with a desired range of color temperature cannot be generated with one device alone. The ‘405 patent goes on to describe an embodiment in which two such LED/phosphor devices are combined with an optical long-pass filter (a transparent piece of glass or plastic tinted so as to enable only longer wavelength light to pass through) that shifts the color temperature of the devices, and then a specific third LED (an Agilent HLMP-EL 18 amber LED) is added to these filtered LED/phosphor devices to provide a 3-LED embodiment with adjustable color temperature.

#### BRIEF SUMMARY

The present application discloses, *inter alia*, lighting systems that provide a system optical output as a function of an applied electrical signal. The system output, which in exemplary embodiments is or comprises white light, can be characterized by a color temperature or by any other suitable measure that represents in some fashion the color or output spectrum of the system optical output. Desirably, the lighting system is designed so that the color temperature changes as a function of the applied electrical signal. In exemplary embodiments, these changes in color temperature are at least in part a result of a phenomenon known as “current crowding”, which is normally considered to be undesirable in a solid state lighting device, and is described further below.

In exemplary embodiments, the system includes an electroluminescent device and a first light modifying material, such as an RSC or phosphor. The electroluminescent device is adapted to emit light in response to the applied electrical signal. The first light

modifying material is adapted to modify a first portion of the emitted light to provide a first light component. The lighting system combines the first light component with at least a second light component associated with a second portion of the emitted light, to produce the system optical output. The system may be characterized by a relative proportion of the first to the second light component, and the changes in color temperature may be associated with changes in the relative proportion.

In further exemplary embodiments, the emitted light is emitted from an output surface of the electroluminescent device, and the electroluminescent device is characterized in that a spatial distribution of the emitted light over the output surface changes as a function of the applied electrical signal, the changes in the spatial distribution being at least in part as a result of current crowding. The system may also include a second light modifying material that modifies the second portion of the emitted light to provide the second light component, the second light component having a second spectrum different from the first spectrum and from the emitted light spectrum. The first light modifying material may cover a first portion of the output surface, and the second light modifying material may cover a second portion of the output surface. For example, the electroluminescent device may include an electrical contact disposed on the output surface, and the first portion of the output surface may be disposed proximate the electrical contact, whereas the second portion of the output surface may be spaced apart from the electrical contact, for example.

Also disclosed are lighting systems that include an electroluminescent device and a first light converting material. The electroluminescent device is adapted to emit light from an output surface in response to an applied electrical current, the electroluminescent device being characterized in that a spatial distribution of the emitted light over the output surface changes as a function of the electrical current at least in part as a result of current crowding. The first light converting material covers a first portion of the output surface, and is adapted to convert a first portion of the emitted light to a first light component. The first light component combines with at least a second light component to provide a system output, and the second light component is associated with a second portion of the emitted light. The first light converting material is spatially distributed such that the changes in the spatial distribution of the emitted light over the output surface produce changes in a color of the system optical output.

In some cases, the second light component may not be associated with any light converting material. For example, the second light component may simply be or comprise the second portion of the emitted light, which may be emitted from a second portion of the output surface. Alternatively, the system may include a second light converting material that covers the second portion of the output surface, and that converts the second portion of the emitted light to the second light component. Note that in addition to including the first and second light components, the system optical output may also include other components such as light that is emitted by the electroluminescent device but not converted to other light by any light converting material. The system optical output may be or include white light, for example, and the changes in color may comprise changes in a color temperature of the system optical output.

Related methods, systems, and articles are also discussed.

These and other aspects of the present application will be apparent from the detailed description below. In no event, however, should the above summaries be construed as limitations on the claimed subject matter, which subject matter is defined solely by the attached claims, as may be amended during prosecution.

#### BRIEF DESCRIPTION OF DRAWINGS

FIGS. 1a-c are schematic sectional views of an electroluminescent device that exhibits the current crowding phenomenon;

FIG. 2a is a schematic top view and FIG. 2b is a schematic sectional view of a lighting system;

FIG. 3 is a CIE chromaticity diagram on which is plotted a line segment representative of a lighting system;

FIGS. 3a and 3b are graphs of the emission spectra of two components of the lighting system of FIG. 3;

FIG. 4 is a schematic sectional view of a lighting system;

FIG. 5 is a schematic sectional view of a lighting system with an associated graph of current density as a function of position;

FIGS. 6 and 7 are schematic top views of different lighting systems;

FIG. 8 is a schematic side view of a combination LED/RSC device; and

FIG. 9 is a schematic side view of an exemplary semiconductor layer stack that includes an RSC.

In the figures, like reference numerals designate like elements.

5                    DETAILED DESCRIPTION OF ILLUSTRATIVE EMBODIMENTS

Optoelectronic device manufacturers consider the phenomenon known as “current crowding” to be a problem that should be avoided, since it is generally associated with reduced quantum efficiency. See e.g. U.S. Patent 7,078,319 (Eliashevich et al.).

10           However, at least some of the lighting systems described herein are intentionally designed to exhibit current crowding, and to take advantage of it in order to produce color changes as a function of an applied electrical signal. Notwithstanding this, we emphasize that we do not wish to be bound by theory, and that any lighting system that is capable of changing a color of its system optical output based on an applied electrical signal, in a manner that is the same as or similar to any of the embodiments described herein, is  
15           intended to be encompassed by the present application even if such a lighting system does not in fact exhibit current crowding.

Referring now to FIG. 1a, we see there a schematic sectional view of a semiconductor electroluminescent device **110** such as an LED, which is reproduced in FIGS. 1b and 1c. The reader will understand that the layer construction of the device **110**  
20           is depicted only schematically for purposes of illustration, that the constituent elements of the device are not necessarily drawn to scale, and that additional elements may be included or illustrated elements may be omitted or modified as desired. As shown, the device **110** includes a semiconductor base layer **112**, a light-emitting layer **114**, and a current spreading layer **116**. The base layer **112** may be or comprise, for example, p-type GaN, or  
25           other suitable semiconductor materials. Light-emitting layer **114** may be or comprise an active layer sandwiched between a p-type cladding layer and an n-type cladding layer (not shown), each of which may comprise, for example, AlGaInN-based materials, or other suitable semiconductor materials. Current spreading layer **116** may be or comprise, for example, an n-type semiconductor such as GaN-based material that is doped with a  
30           concentration of n-type dopant such as Si, or other suitable semiconductor materials.

Also provided are first and second electrodes **118a**, **118b** that make ohmic contact with the respective outer semiconductor layers so that an electrical drive current or similar

electrical signal supplied by an external electronic circuit can be applied to the device such that it emits light. The device **110** may be made with an asymmetrical design, as shown, in order to emit light preferentially from one of its major surfaces, e.g. outer surface **116a** of layer **116**. For this reason, first electrode **118a** can be made to cover only a portion of surface **116a**, whereas second electrode **118b** can be made to cover substantially all of the opposite major surface **112a**. If the second electrode **118b** is at least partially reflective, e.g. metallic, then some light generated within the device **110** that would otherwise escape via major surface **112a** can be reflected by the electrode **118b** so that it escapes via the side surfaces or the major surface **116a** of the device. Of course, semiconductor electroluminescent devices that may be used in the disclosed embodiments need not be asymmetric in the forward/backward characteristic of their light emission, or in the arrangement of their electrodes.

FIGS. 1b and 1c show in a qualitative, schematic fashion the behavior of the device **110** when an electrical signal is applied across the electrodes. In FIG. 1b, a first signal having a first magnitude is applied. In FIG. 1c, a second signal having a second magnitude is applied. The signal magnitudes may be characterized as desired, but, in view of the I-V (current-voltage) characteristics of most semiconductor diode devices, it is most logical to characterize the signal magnitude in terms of electric current. Alternatively, one can characterize the signal magnitude in terms of electric potential (voltage). In any case, the electric current distribution from electrode **118a** through the interior of the device **110** to the other electrode **118b** is depicted by arrows **120** for the first signal (FIG. 1b), and by arrows **122** for the second signal (FIG. 1c).

Recalling that the respective signals are being applied to the very same device **110**, the difference in current distributions exemplified by the different width or lateral dimension of the pattern of arrows **120** compared to that of arrows **122** is a result of the different magnitudes of the respective signals and the “current crowding” phenomenon. As is apparent from the figures, current crowding results in a narrower or more concentrated current distribution for the second signal (FIG. 1c) compared to the first signal (FIG. 1b). This current crowding phenomenon typically occurs at high current densities. That is, the second signal would typically have a greater signal magnitude, measured in electric current, than the first signal. In the case of device **110**, the current crowding may be the result of the p-n junction having a decreased electrical resistance at



the higher current levels. The decreased resistance tends to cause the current to flow in a more direct path from electrode **118a** to electrode **118b**, producing current “bunching” under the electrode **118a** compared to the current distribution of FIG. 1b.

The change in current distribution within the device for different signal magnitudes also has an effect on the spatial distribution of light generated by the device **110**. This is because the light emitting layer **114** will generate light only to the extent electric current is flowing through it. Portions of the light emitting layer in which the current density is low will generate less light than portions in which the current density is high, within limits. By specifying a cutoff value of generated light per unit volume, or per unit projected area (e.g., when viewing the device along an axis perpendicular to the major surface **116a**), one can define a high-intensity region of the light emitting layer **114**. The cutoff value may be, for example, a fraction of a reference light emission level, where the reference level may be a maximum light emission, or a spatially averaged light generation over the entire light emitting layer, and where the fraction may be selected as desired such as  $\frac{1}{2}$ ,  $1/10^{\text{th}}$ , or  $1/e$  of the reference value. Whichever of these parameters one selects, one can use the resulting cutoff value to provide a consistent way to characterize the spatial extent of the higher-intensity region of the light emitting layer. The higher-intensity region is identified by label **124** in FIG. 1b and by label **126** in FIG. 1c. As one would expect, the region **124** has a greater width or lateral dimension than region **126**. This may be the case even though region **124** may have greatly reduced overall light emission levels compared to region **126**, in view of the (typically) substantially greater electric current level used to produce region **126** compared to region **124**.

The differences in the lateral dimension or other spatial extent of the regions **124**, **126** give rise to corresponding differences in the spatial distribution of light emitted from the outer surface **116a** of the device. Thus, the relatively wide region **124** gives rise to a relatively wide spatial distribution of light emitted from the surface **116a**, compared to the relatively narrow region **126**, which gives rise to a narrower spatial distribution of light emitted from the surface **116a**. Stated differently, the spatial distribution of light emitted from surface **116a** using the second signal is more concentrated towards the electrode **118a** than that of the first signal. Just as with the regions **124**, **126**, the spatial distribution of light emitted from the surface **116a** may be characterized or measured in relative terms, e.g., as a fraction or percentage of a maximum or average value, for example. Thus,

assuming the second signal has a greater magnitude than the first signal, differences in their respective spatial distributions of emitted light from the surface **116a** are independent of the fact that the overall amount of light emitted from the surface **116a** may be greater for the second signal than for the first signal.

5           In large part, the degree of current crowding may be controlled by the sheet resistivity of the current-spreading layer. Mathematical models of such current crowding effects may be found in Chapter 8 of *Light-Emitting Diodes*, Second Edition, by E. Fred Schubert (Cambridge University Press).

10           Having now described the current crowding phenomenon, or certain aspects thereof, and its effect on the spatial distribution of light emitted from the surface of an electroluminescent device, we now go on to describe how this can be used to provide lighting systems whose optical output, e.g. white light, can be made to change color, e.g. color temperature, based on an applied electrical signal.

15           A lighting system **210** is shown in a schematic top view in FIG. 2a and in a schematic sectional view in FIG. 2b. The system comprises an electroluminescent device **212** adapted to emit light in response to an applied electrical signal. The electroluminescent device **212** includes a main body **214** to which first and second electrodes **216a**, **216b** have been applied at outer surfaces thereof. The main body **214** is drawn schematically, and may comprise any suitable stack of semiconductor layers (not shown individually) such as would be found in a semiconductor LED, for example. The main body may be in the form of an individual chip or die, as shown, or in the form of an entire semiconductor wafer prior to dicing. Significantly, the layers that make up the body **214** are designed so that the device **212** exhibits the current crowding phenomenon, or so that it otherwise exhibits a spatial distribution of emitted light that substantially changes as a function of a magnitude of the applied electrical signal. The electrical signal is applied, of course, across the electrodes **216a**, **216b**, where a thin wire **218** may connect to the electrode **216a** via a wire bond to help convey the signal from an external electrical driver or source to the device **212**. The light generated within the device **212** may escape or be emitted via the relatively small side surfaces or via the major surface **214a**, to which the first electrode **216a** is applied. Such emitted light may be referred to as pump light, and is labeled  $\lambda_p$  in the figure. The pump light may be or comprise blue, violet, or ultraviolet

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light, e.g., with a peak wavelength in a range from 350 to 500 nm, but other spectral characteristics of the pump light are also contemplated.

As a result of the design of the electroluminescent device, a spatial distribution of pump light  $\lambda_p$  that is emitted from the surface **214a** substantially changes as a function of a magnitude of the applied electrical signal. For example, a first electrical signal having a relatively small magnitude may provide pump light whose spatial distribution as emitted from the surface **214a** is relatively uniform, and a second electrical signal having a larger magnitude may provide pump light whose spatial distribution as emitted from the surface **214a** is concentrated in a smaller area such as an annulus surrounding the electrode **216a**.

In addition to the electroluminescent device **212**, the system **210** also includes first and second light modifying materials **220**, **222**. These materials may convert at least some of the pump light striking them into light components of other wavelengths. For example, first light modifying material **220** may be or comprise a phosphor that converts at least some of the pump light  $\lambda_p$  striking it into a first light component at another wavelength  $\lambda_1$ , typically longer than a wavelength of the pump light. The second light modifying material may be or comprise an RSC having at least one potential well that converts at least some of the pump light  $\lambda_p$  striking it into a second light component at another wavelength  $\lambda_2$  different from  $\lambda_1$ , and also typically longer than a wavelength of the pump light. One or both of light modifying materials **220**, **222** may also be partially transparent to the pump light, such that light propagating out of first light modifying material **220** may comprise a combination or mixture of the first light component at wavelength  $\lambda_1$  and the pump light  $\lambda_p$ , and/or light propagating out of second light modifying material **222** may comprise a combination or mixture of the second light component at wavelength  $\lambda_2$  and the pump light  $\lambda_p$ . Alternatively, both light modifying materials **220**, **222** may be substantially opaque to the pump light  $\lambda_p$ . In any case, light propagating out of the first light modifying material **220** may be characterized by a spectrum **S1**, which includes at least the first light component at wavelength  $\lambda_1$  and may also include the pump light, whereas light propagating out of the second light modifying material **222** may be characterized by a different spectrum **S2**, which includes at least the second light component at wavelength  $\lambda_2$  and may also include the pump light.

The light characterized by the spectra **S1** and **S2** combine, whether by free space propagation or via mechanisms such as optical diffusers, lenses, mirrors, or the like, and optionally with other light components, to produce a system optical output of lighting system **210** represented schematically by arrow **230**. The system optical output **230** thus includes some amount of the light of the first spectrum **S1** and some amount of the light of the second spectrum **S2**. Stated differently, the system optical output **230** includes some amount of the first light component at wavelength  $\lambda_1$  and some amount of the second light component at wavelength  $\lambda_2$ . The different spectra **S1**, **S2** are associated with different perceived colors, and their combination (optionally with other light components) produces yet another perceived color for the system optical output **230**. The perceived color (e.g. a color temperature) of the system optical output **230** can thus be adjusted or changed by changing the relative amounts of the first and second light components that are included in the system optical output **230**.

In view of the current-crowding characteristics of the electroluminescent device **212** described above, such a change in the relative amounts of light provided by the first and second light modifying materials can be achieved by simply changing the magnitude of the applied electrical signal, provided the first and second light modifying materials **220**, **222** are spatially distributed in a way that is synergistic with the changes in the spatial distribution of the pump light that is emitted from the surface **214a**. For example, if a change in the applied electrical signal results in more pump light emitted from a first portion of the surface relative to a second portion, and if the first light modifying material is disposed at the first portion while the second light modifying material is disposed at the second portion, then the change in the applied electrical signal may provide relatively more of the first light component (or of the light of spectrum **S1**) and relatively less of the second light component (or of the light of spectrum **S2**) in the system optical output **230**, thus changing the perceived color of the system optical output.

In the embodiment of FIGS. 2a-b, the first light modifying material **220** is disposed in a circle or an effective annulus proximate the electrode **220**. The second light modifying material **222** is disposed on the remainder of the surface **214a**, i.e., spaced apart from the electrode **220**. This spatial arrangement of light modifying materials **220**, **222** is synergistic with the changes in the spatial distribution of the pump light resulting from the current crowding phenomenon. At low electrical current levels, a relatively uniform

distribution of pump light is emitted from surface **214a**, which produces an initial or baseline proportion of the light of spectrum **S1** to the light of spectrum **S2** in the system optical output. At a higher electrical current, at which current crowding confines the spatial distribution of emitted pump light to a smaller area such as an annulus surrounding the electrode **216a**, the system optical output **230** will include relatively more of the light of spectrum **S1** and relatively less of the light of spectrum **S2**, thus yielding a different proportion of such light components and a different perceived color of the system optical output **230**. The first and second light modifying materials may be selected as appropriate so that the change in color of the system optical output for an increase in magnitude of the applied electrical signal corresponds to an increase in color temperature of a nominally white light output. Alternatively, the light modifying materials may be selected to produce an opposite effect, wherein the change in color of the system optical output for an increase in magnitude of the applied electrical signal corresponds to a decrease in color temperature of a nominally white light output.

In alternative embodiments to that shown in FIGS. 2a-b, the first light modifying material **220** may be omitted, or the second light modifying material **222** may be omitted, such that only one light modifying material is included in the lighting system. Thus, for example, if the first light modifying material **220** is omitted, then the light of spectrum **S1** may include only pump light of wavelength  $\lambda_p$  that is emitted from the annular region of the surface **214a** surrounding the electrode **216a**. Alternatively, if the second light modifying material **222** is omitted, then the light of spectrum **S2** may include only pump light of wavelength  $\lambda_p$  that is emitted from the portion of surface **214a** outside of such annular region.

In still other alternative embodiments, additional light modifying materials such as a third, fourth, etc. light modifying material, may be provided and spatially arranged with the other light modifying materials in patterns that are synergistic with the changes in the spatial distribution of the pump light resulting from the current crowding phenomenon, so that a color of the system optical output changes based on a magnitude of the applied electrical signal. Note that a given light modifying material may convert pump light at wavelength  $\lambda_p$  to a light component that is characterized by only a single peak (having e.g. a Gaussian or bell-shaped spectral distribution) at one peak wavelength, or to a light component that is characterized by multiple peaks at multiple peak wavelengths,

depending on the design of the light modifying material. An RSC, for example, may comprise only one potential well, or may comprise multiple potential wells of the same or similar design, such that the spectrum of the converted light is characterized by only a single peak. Alternatively, an RSC may comprise multiple potential wells of substantially different design, such that the spectrum of the converted light is characterized by a plurality of peaks.

Those skilled in the art will be familiar with a tool or standard used to characterize and quantify perceived colors, in particular, the well-known 1931 CIE chromaticity diagram, promulgated by the Commission Internationale de l'Eclairage (International Commission on Lighting) or "CIE". The color (or "chromaticity" or "chromaticity coordinates") of a light source or article can be precisely measured or specified by a point or region expressed in terms of one or more chromaticity coordinates (x,y) on the CIE chromaticity diagram, using the CIE 1931 standard colorimetric system.

Such a chromaticity diagram is shown in FIG. 3. Those skilled in the art will recognize curve **310** as the "Planckian locus", i.e., the color of an ideal blackbody source over a range of temperatures measured in degrees Kelvin, which temperature is referred to as "color temperature"  $T_c$ .

Points **312** and **314** represent the color coordinates of the light of spectrum **S1** and the light of spectrum **S2**, respectively, for one embodiment of the lighting system **210** of FIGS. 2a-b. The spectra of these points are plotted as a function of optical wavelength in FIGS. 3a and 3b, respectively. That is, FIG. 3a plots the spectrum **S1** corresponding to point **312** in FIG. 3, and FIG. 3b plots the spectrum **S2** corresponding to point **314** in FIG. 3. Spectrum **S1** has two main components: a relatively narrow spectral peak **S1a** corresponding to pump light at wavelength  $\lambda_p$  that is transmitted through first light modifying material **220**, and a broader spectral peak **S1b** corresponding to the first light component at wavelength  $\lambda_1$  produced by the first light modifying material, e.g., YAG:Ce phosphor. Spectrum **S2** also has two main components: a relatively narrow first spectral peak **S2a** and a relatively narrow second spectral peak **S2b**. These two peaks can be produced by a blue-LED-pumped RSC that has at least one potential well capable of converting the blue pump light to light at the first peak **S2a** and at least another potential well capable of converting the pump light to light at the second peak **S2b**. Note by the absence of any peak at the pump wavelength  $\lambda_p$  in spectrum **S2** that the second light

converting material, i.e., the RSC, absorbs or otherwise effectively blocks all pump light of wavelength  $\lambda_p$  incident upon it in this particular embodiment.

The line segment **316** in FIG. 3, whose endpoints are points **312** and **314**, represents the set of all possible lighting system optical outputs for systems whose outputs are composed of a linear combination of light of spectrum **S1** and light of spectrum **S2**. Thus, for example, a lighting system whose optical output is composed of equal parts of the light of spectrum **S1** and light of spectrum **S2** is represented by a point that bisects line segment **316**. If the proportion of the light of spectrum **S1** is increased, the system point moves along line segment **316** towards point **312**. If instead the proportion of the light of spectrum **S2** is increased, the system point moves along line segment **316** towards point **314**.

By judicious selection of the position (color) of points **312** and **314**, the line segment **316** can be made to closely approximate a portion of the Planckian locus **310**, e.g., the portion of the locus **310** over a range of color temperatures from 2500K to 5000K, or from 3000K to 5000K, for example. In such a case, a system point on line segment **316** that moves towards point **312** corresponds to a color shift towards higher color temperatures, or a “cooler” (higher blue content) white light source. If instead a system point moves towards point **314**, it corresponds to a color shift towards lower color temperatures, or a “warmer” (higher red content) light source. Note that the lighting system **210** of FIGS. 2a-b, utilizing the light modifying materials described in connection with FIGS. 3, 3a, and 3b, generates a system optical output that shifts from lower to higher color temperatures (along the line segment **316** towards point **312**) as the magnitude of the applied electrical signal is increased.

The particular shapes of the spectra **S1** and **S2**, when plotted as a function of wavelength, not only determine the positions of their respective points **312**, **314** on the CIE chromaticity diagram, but also determine a characteristic known as the “color rendering index” of the resulting system light. The color rendering index (CRI) is a parameter that may be important to a lighting system designer if the designer is concerned not only with the appearance or color of the system optical output as it is perceived by direct observation with the eye, but also with the appearance of objects or articles that are viewed for example in reflected light using the system optical output. Depending on the reflectivity spectrum of the objects or articles, their appearance may be very different

when illuminated with a first nominally white light source than when illuminated with a second nominally white light source, even though the first and second white light sources may have identical color coordinates on the CIE chromaticity diagram. This is a consequence of the fact that a particular color coordinate on the CIE chromaticity diagram may be associated with numerous optical spectra that may differ substantially from each other. A common illustration demonstrating the effect of color rendering is the sometimes very different appearance that colored objects have when illuminated with sunlight as compared to illumination with a fluorescent office lights for example, or as compared to illumination with a gas discharge street lamp, even though all of these illumination sources may appear to be nominally white when viewed directly.

The color rendering index of a given source can be measured using the method described in the CIE publication 13.3-1995, "Method of Measuring and Specifying Colour Rendering Properties of Light Sources". The color rendering index in general ranges from a low of 0 to a high of 100, with higher values generally being desirable. Furthermore, numerical techniques and software are available from the CIE, that are capable of calculating the color rendering index of a given spectrum representing a given light source, based on the CIE 13.3-1995 publication.

When such software is used to calculate the color rendering index of system optical outputs composed of a linear combination of the spectra **S1** and **S2** shown in FIGS. 3a and 3b, the result is a color rendering index of at least 80 over a color temperature range (corresponding to different proportions of the spectra **S1** and **S2**) from 2500K to 5000K. In exemplary embodiments, the color rendering index is at least 60, or at least 70, or at least 80, over a color temperature range from 2500K to 5000K, or from 3000K to 5000K, for example. In order to achieve high color rendering index values, it is desirable to ensure that each of the constituent spectra (**S1**, **S2**) that make up the system optical output is characterized by at least two distinct spectral peaks, e.g. the peaks **S1a**, **S1b** of FIG. 3a or the peaks **S2a**, **S2b** of FIG. 3b, which peaks may be separated from each other by at least 10 nm, for example. Further reference in this regard is made to commonly filed U.S. Application 61/221,660, "White Light Electroluminescent Devices With Adjustable Color Temperature" (Attorney Docket No. 65330US002), which is incorporated herein by reference.



Turning now to FIG. 4, we see there a schematic sectional view of another solid state lighting system **410** capable of exhibiting a substantial color shift as a function of a magnitude of an applied electrical signal, at least in part as a result of current crowding. The system **410** includes a two-terminal semiconductor electroluminescent device **412**,  
5 such as an LED. The device is mounted on a metal header **414** having a first conductive post **416** electrically coupled to a base electrode of the device **412**. A second conductive post **418**, electrically insulated from the header **414**, electrically couples to a top electrode of the device via a thin wire **420** and wire bond **422**. The posts **416**, **418** form the two terminals of the system **410**, across which the electrical signal is applied to energize the  
10 device. The top electrode of the device is smaller than the base electrode, and offset to one side of an output surface **412a** of the electroluminescent device **412**.

An RSC **424** covers a first portion of the output surface **412a**, which first portion may as shown be spatially arranged to be spaced apart from the top electrode. The RSC **424** is operable to convert the emitted or pump light generated within the  
15 electroluminescent device into a first light component having a spectrum **S3**, e.g., characteristic of amber light. The spectrum **S3** may comprise or consist essentially of a distinct first and second spectral peak, e.g., the same as or similar to the spectrum **S2** of FIG. 3b. The spectrum **S3** may optionally include a distinct third spectral peak corresponding to residual pump light transmitted by the RSC **424**, or it may contain no  
20 such third spectral peak in the case that RSC **424** substantially blocks such pump light.

A phosphor **426** covers a second portion of the output surface **412a**, the second portion being different from the first portion, and including areas or zones that are proximate the top electrode. The phosphor **426** is operable to convert at least some of the pump light into a second light component, e.g., yellow light having a spectral peak similar  
25 to peak **S1b** of FIG. 3a, to result in emitted light having spectrum **S4**. The light having spectrum **S4** may include not only yellow light generated by the phosphor **426**, but also residual pump light transmitted by the phosphor, e.g. as shown in the spectrum **S1** of FIG. 3a. The light of spectrum **S3** and the light of spectrum **S4** are combined, optionally with other light components, to provide system optical output **428**, e.g., white light, whose  
30 color temperature is dependent upon the relative amounts or proportion of the first and second light components included in the system output.

Changes in color temperature of the system output with a changing magnitude of the applied electrical signal are achieved by ensuring that the electroluminescent device **412** exhibits current crowding, i.e., that the spatial distribution of the pump light emitted over the output surface **412a** substantially changes as a function of such magnitude, and further by ensuring that such changes in the spatial distribution of emitted light are synergistic with the spatial distributions of the RSC **424** and phosphor **426** so that the relative amounts or proportion of the first and second light components included in the system output change in a corresponding fashion. In particular, by offsetting the top electrode to one side of the electroluminescent device, opposite the RSC **424**, the effects of the current crowding phenomenon are promoted.

FIG. 5 shows a schematic sectional view of a lighting system **510** similar to system **410**, along with an associated graph of current density as a function of position. The system **510** includes an electroluminescent device **512** having an output surface **512a** from which pump light generated within the device is emitted. The device **512** also includes a top electrode **514**, a base electrode **516**, and constituent semiconductor layers **518**, **520**, **522**, which layers may be or comprise a current spreading layer, a p-n junction layer, and a substrate layer respectively. The current spreading layer may comprise, for example, AlGaInN, or other suitable semiconductor material; the p-n junction may comprise, for example, GaInN, or other suitable semiconductor material; and the substrate layer may comprise, for example, silicon, or other suitable semiconductor material. A first light modifying material **524**, which may be substantially the same as RSC **424** of FIG. 4, covers a first portion of the output surface **512a** and receives a first portion of the pump light. A second light modifying material **526**, which may be substantially the same as phosphor **426** of FIG. 4, covers a second portion of the output surface **512a** and receives a second portion of the pump light. Light emitted from the first light modifying material, having a spectrum **S5**, and light emitted from the second light modifying material, having a spectrum **S6** different from **S5**, combine to form a system optical output **528**.

Due to the geometry or layout of the electrodes **514**, **516**, and one or more electrical properties of one or more constituent layers of the electroluminescent device **512** that change in response to a magnitude of the electrical signal applied across the electrodes, a substantial current crowding phenomenon is observed. For example, the thickness and/or conductivity of the n-GaN layer can be designed to provide a controlled

amount of current crowding at high currents. In this regard, a graph of an expected current density through the p-n junction layer **520**, as a function of lateral position along the p-n junction layer, is provided in the figure. Curve **530** is representative of a first electrical current applied across electrodes **514**, **516**, and curve **532** is representative of a second electrical current greater than the first current. The curves assume that the resistivity of the p-n junction layer **520** is lower for the second electrical current than for the first electrical current. Although both curves exhibit a plateau or maximum at positions corresponding to the top electrode **514**, and taper off with increasing distance from that electrode, curve **532** is more heavily weighted or concentrated at positions close to the electrode, while curve **528** more nearly approximates a uniform spatial distribution. These differences in current density result in corresponding differences in the spatial distribution of pump light emitted from output surface **512a**, which, in combination with the different spatial distributions of the first and second light modifying materials, result in different relative amounts of the light of spectrum **S5** and light of spectrum **S6** in the system optical output **528**, thus producing changes in the color or color temperature of the output **528**.

The composition of the first and second light modifying materials, and their respective layout or spatial distribution on the output surface **512a** (e.g., the size of the gap between the electrode **514** and the first light modifying material **524**), may if desired be chosen to provide a system optical output having a nominally white light output that at low applied currents exhibits a particular color temperature, e.g., 2500K or 3000K, and which at higher applied currents exhibits a color temperature that increases. The increase in color temperature with increasing current may be designed to approximate the change in color temperature associated with an incandescent light source, for example.

FIGS. 6 and 7 show schematic top views of other lighting systems capable of providing a system optical output whose color or color temperature changes as a function of an applied electrical signal. For brevity, details of the design of the electroluminescent device are not shown, but reference is made in that regard to the discussion above. Instead, FIGS. 6 and 7 illustrate alternative designs of the top electrode and spatial distributions of the first and second light modifying materials that can be used to produce the desired color-changing effects.

In FIG. 6, a lighting system **610** includes a top electrode **612** disposed as shown on an output surface of an electroluminescent device. A first light modifying material **614** is

spatially arranged or disposed to be proximate the electrode **612**. A second light modifying material **616** is spatially arranged or disposed to be spaced apart from the electrode **612**. Current crowding may result in more light associated with the first light modifying material, relative to light associated with the second light modifying material, to be present in the system optical output as a magnitude of the electrical signal is increased.

In FIG. 7, a lighting system **710** includes a top electrode **712** disposed as shown on an output surface of an electroluminescent device. A first light modifying material **714** is spatially arranged or disposed to be proximate the electrode **712**. A second light modifying material **716** is spatially arranged or disposed to be spaced apart from the electrode **712**. A zone or area **718** of the output surface is not covered with any light modifying material, such that pump light generated in the electroluminescent device is emitted from this area without modification. Current crowding may result in more light associated with the first light modifying material, relative to light associated with the second light modifying material, to be present in the system optical output as a magnitude of the electrical signal is increased.

FIG. 8 shows an illustrative device **800** that combines an RSC **808** and an LED **802**. The LED has a stack of LED semiconductor layers **804**, sometimes referred to as epilayers, on an LED substrate **806**. The layers **804** may include p- and n-type junction layers, light emitting layers (typically containing quantum wells), buffer layers, and superstrate layers. The layers **804** may be attached to the LED substrate **806** via an optional bonding layer **816**. The LED has an upper surface **812** and a lower surface, and the upper surface is textured to increase extraction of light from the LED compared to the case where the upper surface is flat. Electrodes **818**, **820** may be provided on these upper and lower surfaces, as shown. When connected to a suitable power source through these electrodes, the LED emits light at a first wavelength  $\lambda_1$ , which may correspond to blue or ultraviolet (UV) light. Some of this LED light enters the RSC **808** and is absorbed there.

The RSC **808** is attached to the upper surface **812** of the LED via a bonding layer **810**. The RSC has upper and lower surfaces **822**, **824**, with pump light from the LED entering through the lower surface **824**. The RSC also includes a quantum well structure **814** engineered so that the band gap in portions of the structure is selected so that at least some of the pump light emitted by the LED **802** is absorbed. The charge carriers

generated by absorption of the pump light diffuse into other portions of the structure having a smaller band gap, the quantum well layers, where the carriers recombine and generate light at the longer wavelength. This is depicted in FIG. 8 by the re-emitted light at the second wavelength  $\lambda_2$  originating from within the RSC **808** and exiting the RSC to provide output light.

FIG. 9 shows an illustrative semiconductor layer stack **910** comprising an RSC. The stack was grown using molecular beam epitaxy (MBE) on an indium phosphide (InP) wafer. A GaInAs buffer layer was first grown by MBE on the InP substrate to prepare the surface for II-VI growth. The wafer was then moved through an ultra-high vacuum transfer system to another MBE chamber for growth of II-VI epitaxial layers used in the RSC. Details of the as-grown RSC are shown in FIG. 9 and summarized in Table 1. The table lists the thickness, material composition, band gap, and layer description for the different layers associated with the RSC. The RSC included eight CdZnSe quantum wells **930**, each having a transition energy of 2.15 eV. Each quantum well **930** was sandwiched between CdMgZnSe absorber layers **932** having a band gap energy of 2.48 eV that could absorb blue light emitted by an LED. The RSC also included various window, buffer, and grading layers.

TABLE 1

| Reference No. | Material  | Thickness (nm) | Band Gap/ Transition (eV) | Comment         |
|---------------|---|----------------|---------------------------|-----------------|
| 930           | $\text{Cd}_{0.48}\text{Zn}_{0.52}\text{Se}$   | 3.1            | 2.15                      | quantum well    |
| 932           | $\text{Cd}_{0.38}\text{Mg}_{0.21}\text{Zn}_{0.41}\text{Se}$   | 8              | 2.48                      | absorber        |
| 934           | $\text{Cd}_{0.38}\text{Mg}_{0.21}\text{Zn}_{0.41}\text{Se}:\text{Cl}$   | 92             | 2.48                      | absorber        |
| 936           | $\text{Cd}_{0.22}\text{Mg}_{0.45}\text{Zn}_{0.33}\text{Se}$   | 100            | 2.93                      | window          |
| 938           | $\text{Cd}_{0.22}\text{Mg}_{0.45}\text{Zn}_{0.33}\text{Se} \rightarrow \text{Cd}_{0.38}\text{Mg}_{0.21}\text{Zn}_{0.41}\text{Se}$ | 250            | 2.93 – 2.48               | grading         |
| 940           | $\text{Cd}_{0.38}\text{Mg}_{0.21}\text{Zn}_{0.41}\text{Se}:\text{Cl}$   | 46             | 2.48                      | absorber        |
| 942           | $\text{Cd}_{0.38}\text{Mg}_{0.21}\text{Zn}_{0.41}\text{Se} \rightarrow \text{Cd}_{0.22}\text{Mg}_{0.45}\text{Zn}_{0.33}\text{Se}$ | 250            | 2.48 – 2.93               | grading         |
| 944           | $\text{Cd}_{0.39}\text{Zn}_{0.61}\text{Se}$   | 4.4            | 2.24                      | II-VI buffer    |
| 946           | $\text{Ga}_{0.47}\text{In}_{0.53}\text{As}$   | 190            | 0.77                      | III-V buffer    |
| 924           | InP   | 350,000        | 1.35                      | III-V substrate |

Further details of this and other RSC devices can be found in PCT Publication WO 2009/048704 (Kelley et al.).

- 5 An exemplary semiconductor stack comprising an RSC capable of simultaneously emitting light having a spectrum that includes two peak wavelengths, similar to the spectrum shown in FIG. 3b, is set forth below in Table 2. The stack includes one green-emitting (555 nm) quantum well, producing a green spectral peak, and one red-emitting (620 nm) quantum well, producing a red spectral peak. The relative intensities of the
- 10 green and red peaks are principally controlled by the thicknesses of the absorber layers associated with the respective quantum wells. By using relatively thin absorber layers adjacent the green-emitting quantum well, more of the pump light will pass through these layers and be absorbed in the absorbing layers adjacent the red-emitting quantum well. This can result in the emission of more red light than green light. The ratio of green light
- 15 to red light may also be somewhat influenced by the presence of any light-extraction features, e.g., where such features are etched into or attached to the outer surface of the cyan blocker.

TABLE 2

| Layer type   | Material  | Thickness (nm) | Band gap/ emission energy (eV) | Band gap/ emission wavelength (nm) |
|--------------|---|----------------|--------------------------------|------------------------------------|
| cyan blocker | $\text{Cd}_{0.38}\text{Mg}_{0.21}\text{Zn}_{0.41}\text{Se}$ | 1000           | 2.48                           | 500                                |
| barrier      | $\text{Cd}_{0.23}\text{Mg}_{0.43}\text{Zn}_{0.34}\text{Se}$ | 20             | 2.88                           | 430                                |
| absorber     | $\text{Cd}_{0.34}\text{Mg}_{0.27}\text{Zn}_{0.39}\text{Se}$ | 150            | 2.58                           | 480                                |
| quantum well | $\text{Cd}_{0.72}\text{Zn}_{0.28}\text{Se}$                 | ~ 4            | 2.00                           | 620                                |
| absorber     | $\text{Cd}_{0.34}\text{Mg}_{0.27}\text{Zn}_{0.39}\text{Se}$ | 150            | 2.58                           | 480                                |
| barrier      | $\text{Cd}_{0.23}\text{Mg}_{0.43}\text{Zn}_{0.34}\text{Se}$ | 20             | 2.88                           | 430                                |
| absorber     | $\text{Cd}_{0.34}\text{Mg}_{0.27}\text{Zn}_{0.39}\text{Se}$ | 30             | 2.58                           | 480                                |
| quantum well | $\text{Cd}_{0.47}\text{Zn}_{0.53}\text{Se}$                 | ~ 3            | 2.23                           | 555                                |
| absorber     | $\text{Cd}_{0.34}\text{Mg}_{0.27}\text{Zn}_{0.39}\text{Se}$ | 30             | 2.58                           | 480                                |
| window       | $\text{Cd}_{0.23}\text{Mg}_{0.43}\text{Zn}_{0.34}\text{Se}$ | 500            | 2.88                           | 430                                |

The person skilled in the art will understand how to tailor the composition of the CdMgZnSe alloys to achieve the listed band gap energies for the various layers. For example, the band gap energies of the CdMgZnSe alloys are primarily controlled by the Mg content. Emission wavelengths (or energies) of the quantum wells are controlled both by the Cd/Zn ratio, and the precise thickness of the quantum well.

Unless otherwise indicated, all numbers expressing quantities, measurement of properties, and so forth used in the specification and claims are to be understood as being modified by the term “about”. Accordingly, unless indicated to the contrary, the numerical parameters set forth in the specification and claims are approximations that can vary depending on the desired properties sought to be obtained by those skilled in the art utilizing the teachings of the present application. Not as an attempt to limit the application of the doctrine of equivalents to the scope of the claims, each numerical parameter should at least be construed in light of the number of reported significant digits and by applying ordinary rounding techniques. Notwithstanding that the numerical ranges and parameters setting forth the broad scope of the invention are approximations, to the extent any numerical values are set forth in specific examples described herein, they are reported as

precisely as reasonably possible. Any numerical value, however, may well contain errors associated with testing or measurement limitations.

Various modifications and alterations of this invention will be apparent to those skilled in the art without departing from the spirit and scope of this invention, and it  
5 should be understood that this invention is not limited to the illustrative embodiments set forth herein. For example, the reader should assume that features of one disclosed embodiment can also be applied to all other disclosed embodiments unless otherwise indicated. It should also be understood that all U.S. patents, patent application  
10 publications, and other patent and non-patent documents referred to herein are incorporated by reference, to the extent they do not contradict the foregoing disclosure.



## CLAIMS

1. A lighting system, comprising:

5           an electroluminescent device adapted to emit light in response to an applied  
            electrical signal; and  
            a first light modifying material adapted to modify a first portion of the emitted  
            light to provide a first light component;  
            wherein the lighting system combines the first light component with at least a  
10           second light component associated with a second portion of the emitted light to  
            produce a system optical output;  
            wherein the system optical output has a color temperature that changes based on  
            the applied electrical signal; and  
            wherein the changes in color temperature are at least in part a result of current  
15           crowding.

2. The system of claim 1, wherein the system optical output is characterized by a relative  
proportion of the first to the second light component, and wherein the changes in color  
temperature are associated with changes in the relative proportion.

20

3. The system of claim 1, wherein the emitted light is emitted from an output surface of  
the electroluminescent device, and wherein the electroluminescent device is characterized  
in that a spatial distribution of the emitted light over the output surface changes as a  
function of the applied electrical signal, the changes in the spatial distribution being at  
25           least in part as a result of current crowding.

25

4. The system of claim 3, wherein the emitted light has an emitted light spectrum and the  
first light component has a first spectrum different from the emitted light spectrum.

30

5. The system of claim 4, further comprising a second light modifying material that  
modifies the second portion of the emitted light to provide the second light component, the

second light component having a second spectrum different from the first spectrum and from the emitted light spectrum.

5 6. The system of claim 5, wherein the first light modifying material covers a first portion of the output surface and the second light modifying material covers a second portion of the output surface.

10 7. The system of claim 6, further comprising a third light modifying material covering a third portion of the output surface, the third light modifying material being adapted to modify a third portion of the emitted light to provide a third light component that has a third spectrum different from the first, second, and emitted light spectra.

15 8. The system of claim 4, wherein the first light modifying material covers a first portion of the output surface, wherein a second portion of the output surface is characterized by an absence of any light modifying material, and wherein the second light component has a second spectrum that is substantially the same as the emitted light spectrum.

20 9. The system of claim 4, wherein the emitted light spectrum has a peak at a wavelength  $\lambda_p$  and the first spectrum has a peak at a wavelength  $\lambda_1$ , and wherein  $\lambda_1 > \lambda_p$ .

10. The system of claim 1, wherein the first light modifying material comprises a phosphor.

25 11. The system of claim 1, wherein the first light modifying material comprises a first re-emitting semiconductor construction that includes a first potential well.

30 12. The system of claim 11, further comprising a second light modifying material that modifies the second portion of the emitted light to provide the second light component, the second light modifying material comprising a second re-emitting semiconductor construction that includes a second potential well.

13. The system of claim 6, wherein the electroluminescent device includes an electrical contact disposed on the output surface, wherein the first portion of the output surface is disposed proximate the electrical contact, and wherein the second portion of the output surface is spaced apart from the electrical contact.

5

14. The system of claim 1, wherein the color temperature changes as a function of a magnitude of the applied electrical signal.

10

15. The system of claim 14, wherein the color temperature increases with increasing magnitude of the applied electrical signal.

16. A lighting system, comprising:

an electroluminescent device adapted to emit light from an output surface in response to an applied electrical current, the electroluminescent device being characterized in that a spatial distribution of the emitted light over the output surface changes as a function of the electrical current at least in part as a result of current crowding; and

15

a first light converting material covering a first portion of the output surface and adapted to convert a first portion of the emitted light to a first light component; wherein the first light component combines with at least a second light component to provide a system optical output, the second light component being associated with a second portion of the emitted light; and

20

wherein the first light converting material is spatially distributed such that the changes in the spatial distribution of the emitted light over the output surface produce changes in a color of the system optical output.

25

17. The system of claim 16, wherein the second light component is not associated with any light converting material.

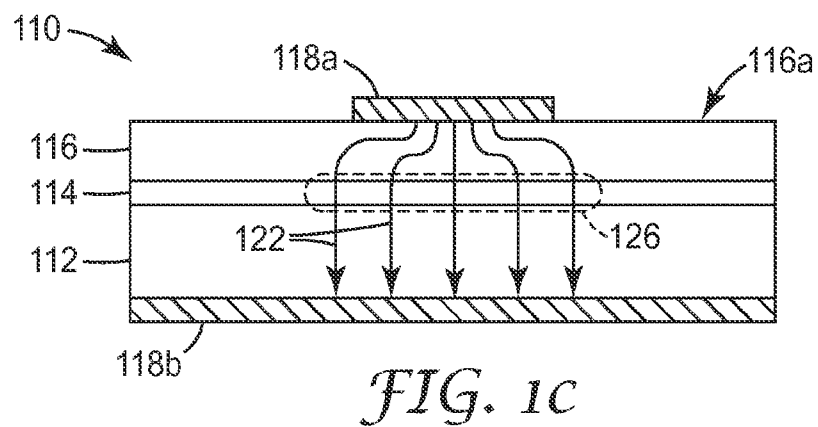
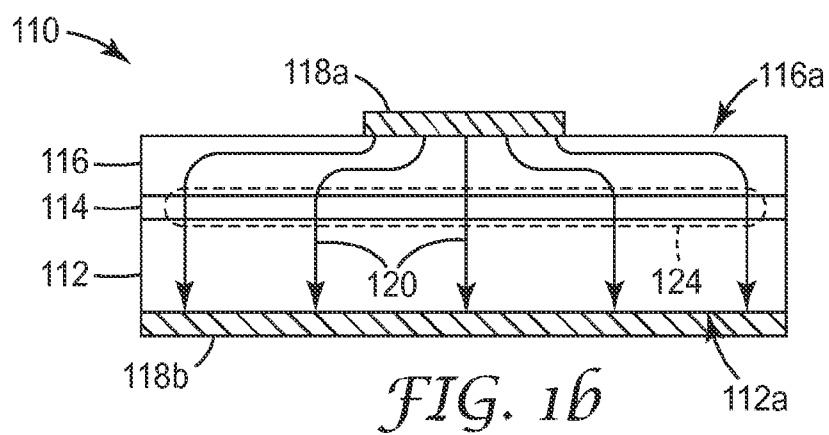
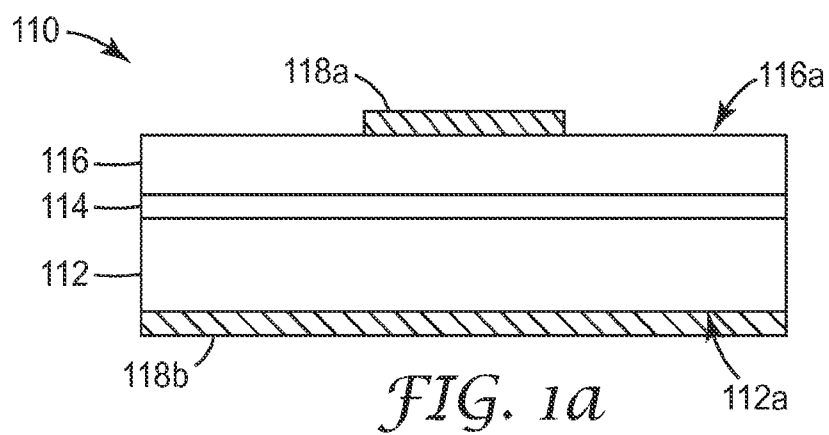
30

18. The system of claim 16, further comprising a second light converting material covering a second portion of the output surface, the second light converting material being adapted to convert the second portion of the emitted light to the second light component.

19. The system of claim 16, wherein the electroluminescent device includes an electrical contact disposed on the output surface, wherein the first portion of the output surface is generally proximate the electrical contact, and wherein the output surface includes a  
5 second portion generally spaced apart from the electrical contact.

20. The system of claim 16, wherein the system optical output comprises white light, and wherein the changes in the color comprise changes in a color temperature of the system optical output.  
10

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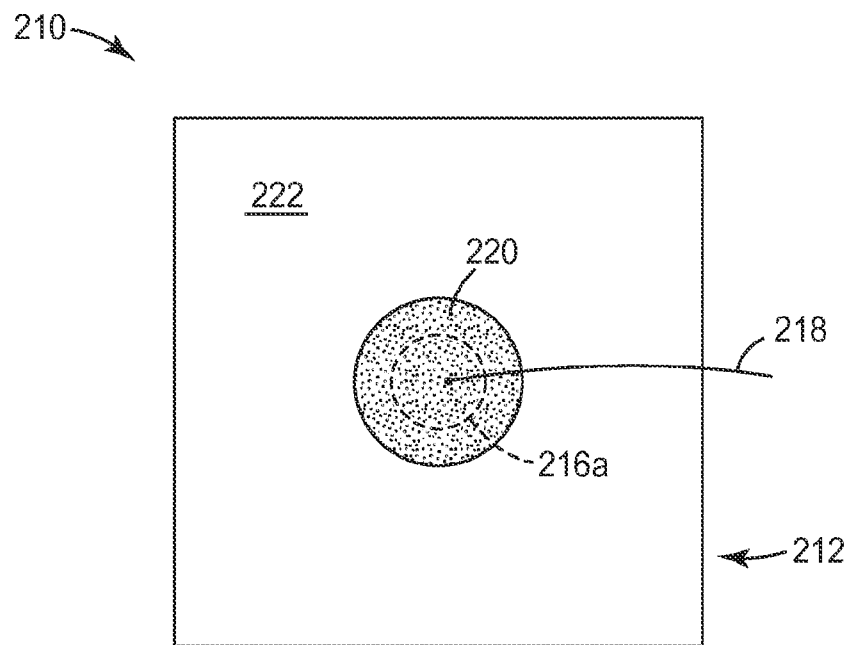


FIG. 2a

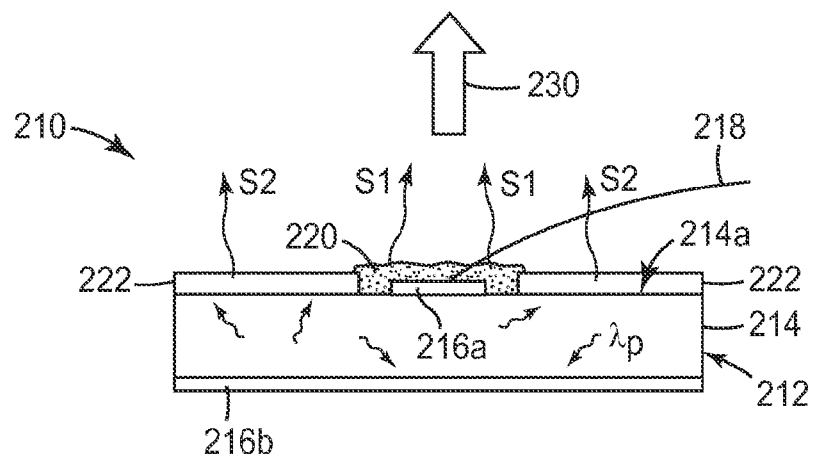


FIG. 2b

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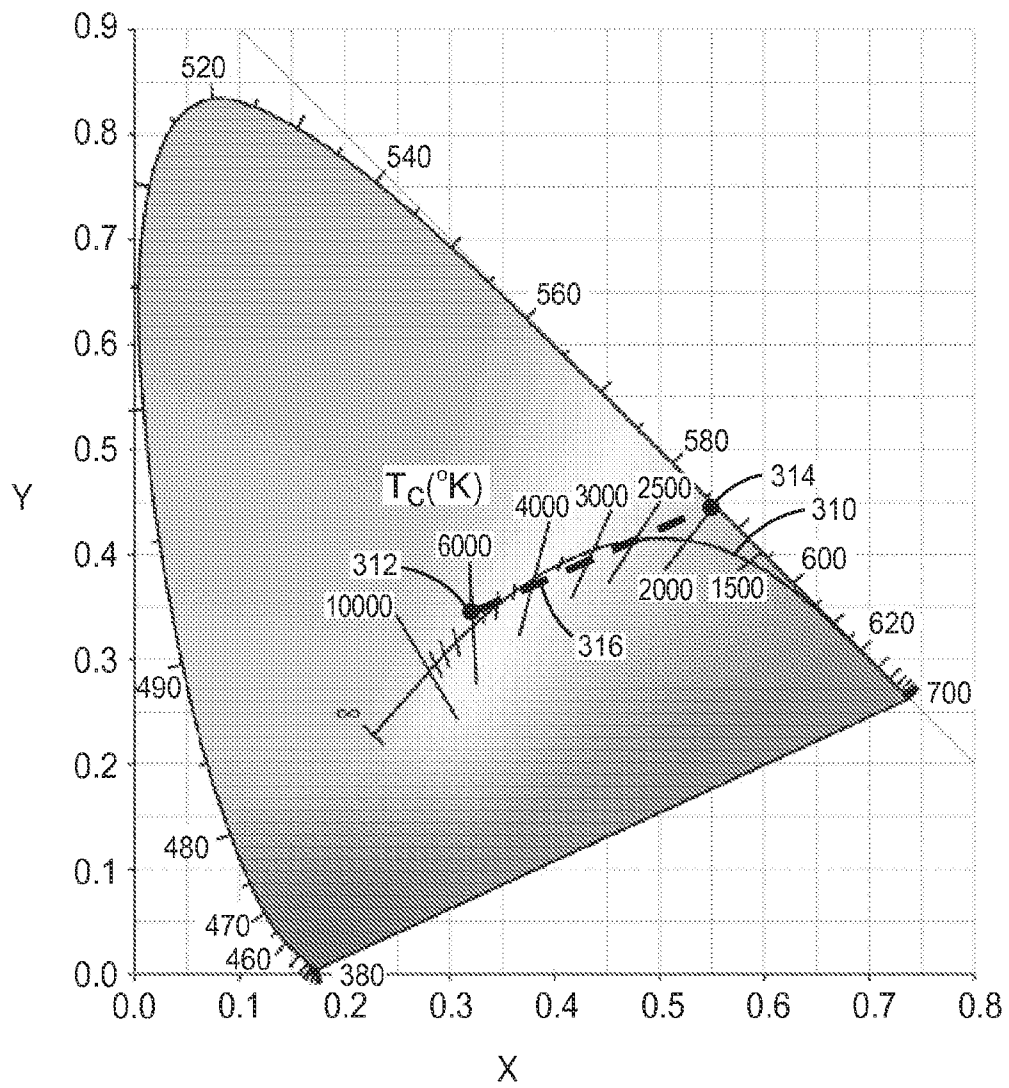
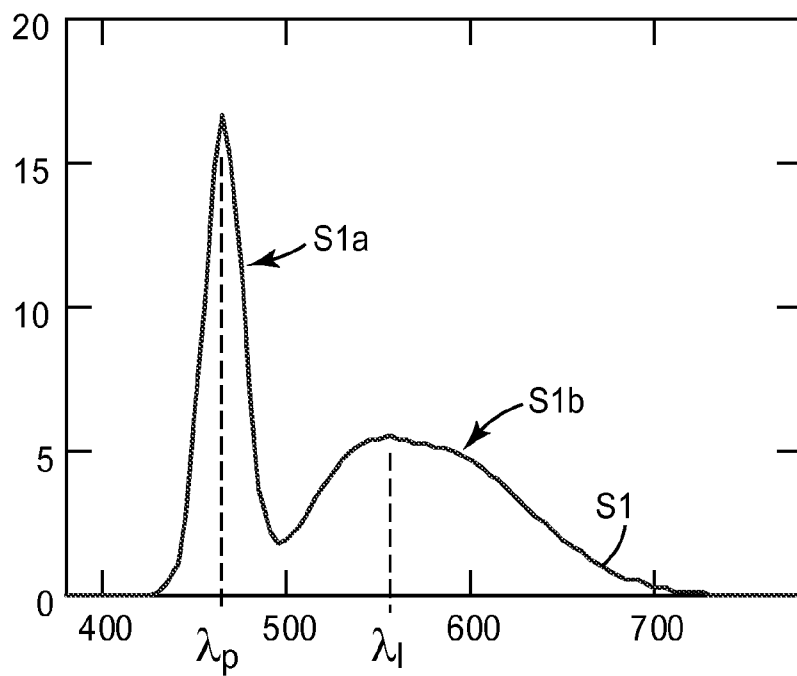
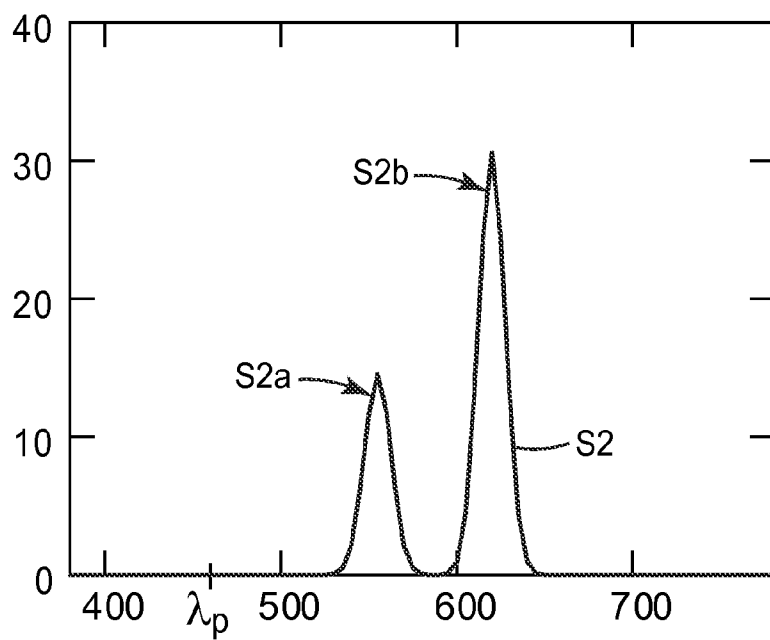


FIG. 3

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*FIG. 3a**FIG. 3b*



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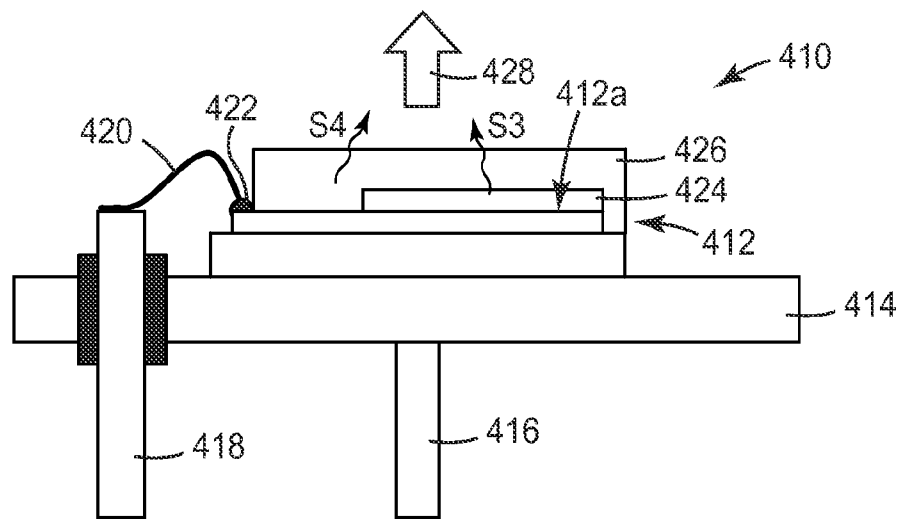


FIG. 4

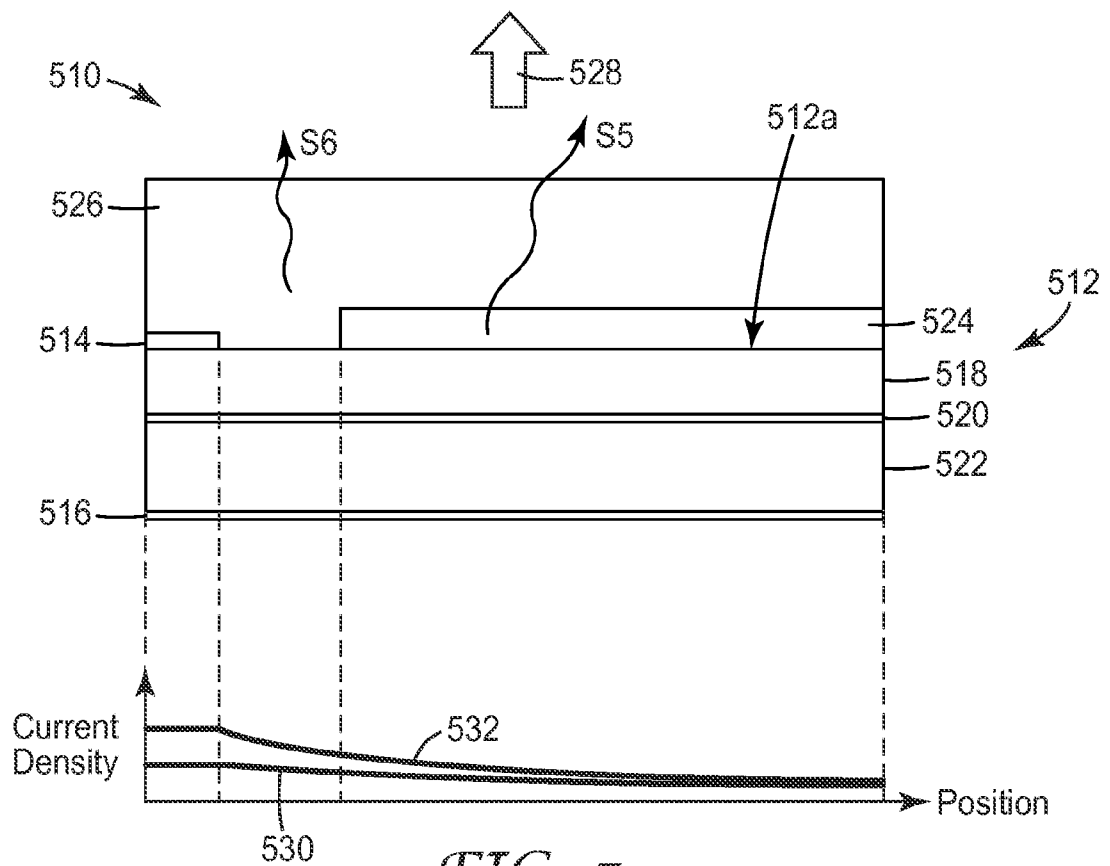


FIG. 5

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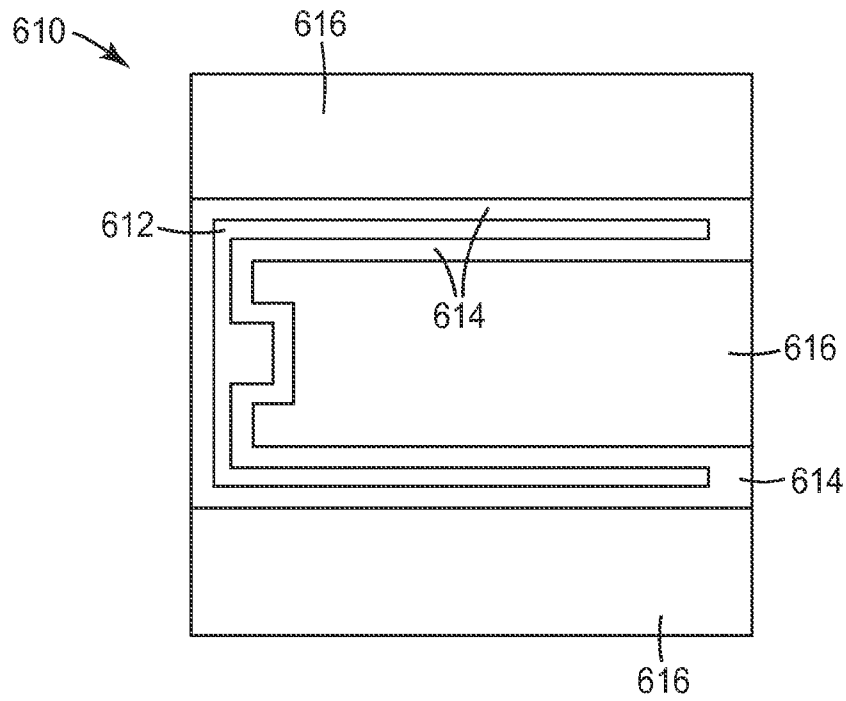


FIG. 6

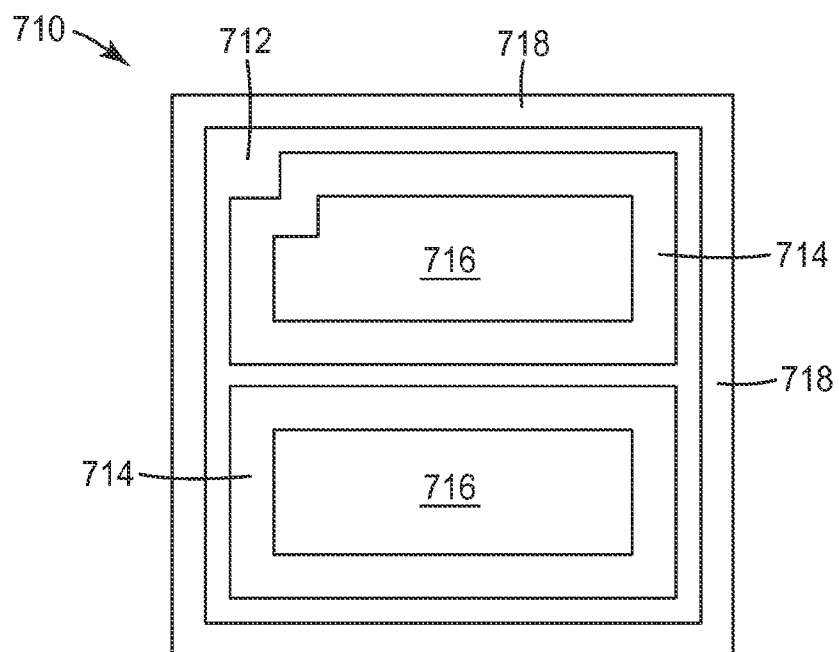
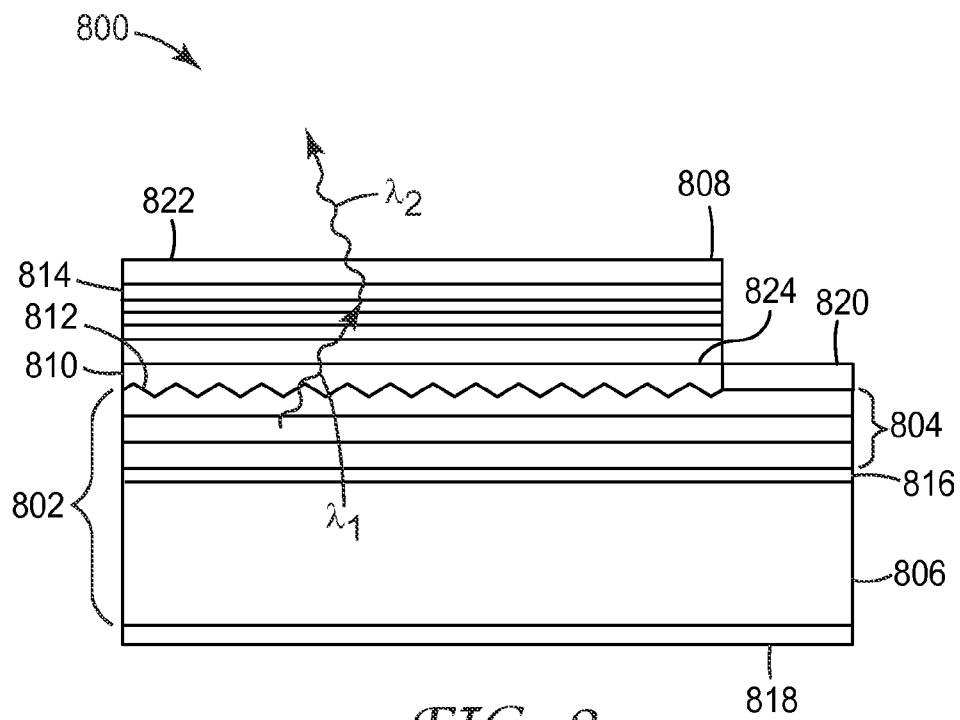


FIG. 7

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*FIG. 8*

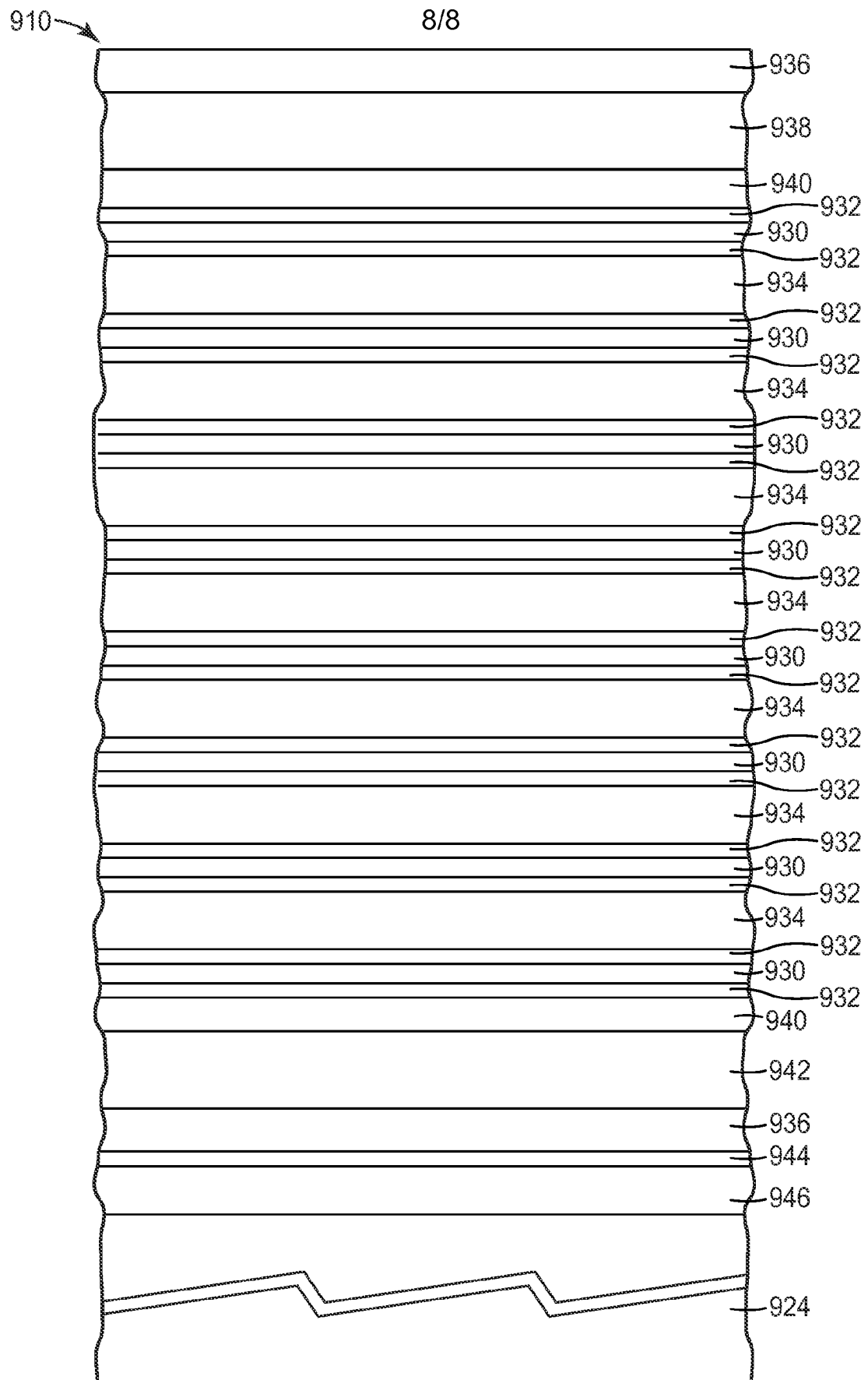


FIG. 9

# INTERNATIONAL SEARCH REPORT

International application No  
PCT/US2010/040009

## A. CLASSIFICATION OF SUBJECT MATTER

INV. H01L33/50  
ADD. H01L33/38

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)  
H01L

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EP0-Internal

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

| Category* | Citation of document, with indication, where appropriate, of the relevant passages   | Relevant to claim No. |
|-----------|--|-----------------------|
| X         | WO 2007/034367 A1 (KONINKL PHILIPS ELECTRONICS NV [NL]; JALINK CORNELIS J [NL]; VAN TARTW)<br>29 March 2007 (2007-03-29)<br>page 5, lines 11-14<br>page 7, line 7 - page 8, line 28; figures 1,2 | 1-10,<br>14-18,20     |
| X         | US 2008/230795 A1 (DIAS ERIC W B [IN])<br>25 September 2008 (2008-09-25)<br>paragraphs [0012] - [0015]; figure 1A<br>paragraph [0020]; figure 2A<br>-----<br>-/--                                | 1-6,8,<br>10-20       |

☒ Further documents are listed in the continuation of Box C.

☒ See patent family annex.

### \* Special categories of cited documents :

"A" document defining the general state of the art which is not considered to be of particular relevance  
"E" earlier document but published on or after the international filing date  
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)  
"O" document referring to an oral disclosure, use, exhibition or other means  
"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention  
"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone  
"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.  
"&" document member of the same patent family

Date of the actual completion of the international search

22 September 2010

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International application No  
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| A  | US 2009/108269 A1 (NEGLEY GERALD H [US] ET AL) 30 April 2009 (2009-04-30) paragraphs [0179], [0181]; figures 10,11   | 5,6,<br>8-10,18                |

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