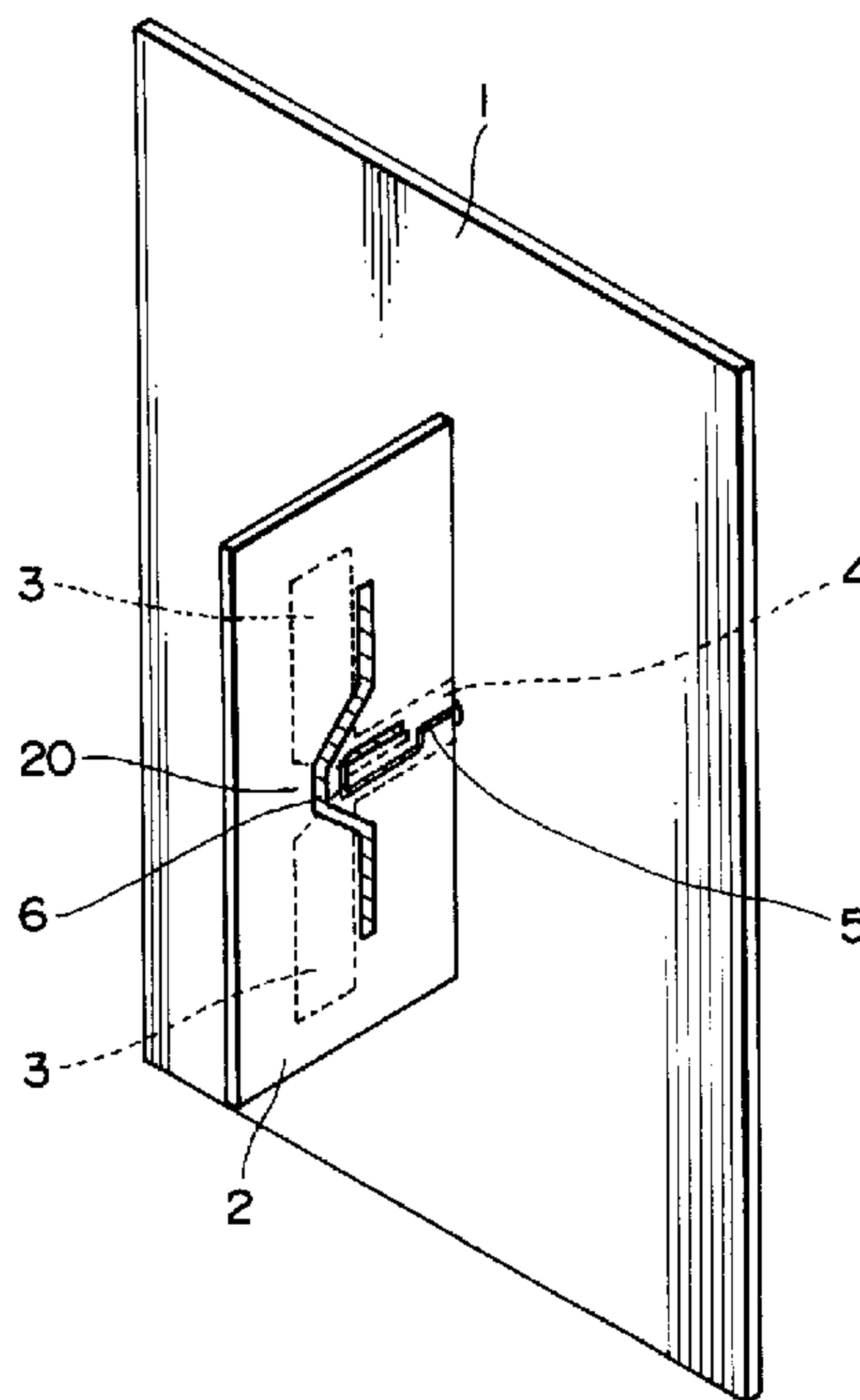




(72) ARAI, Hiroyuki, JP
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(51) Int.Cl.⁶ H01Q 19/10, H01Q 1/38
(54) **ANTENNE DIPOLE POURVU D'UN REFLECTEUR**
(54) **REFLECTOR-PROVIDED DIPOLE ANTENNA**



(57) To realize a reflector-provided dipole antenna showing an outstanding performance in a wide frequency range and allowing simultaneous transmission and reception at different frequencies. A dipole antenna element is provided at the back of a dielectric substrate set to the reflector surface. A parasitic element is provided on the front of the dielectric substrate, which is constituted by forming and protruding the central portion of a linear conductor forward like an almost trapezoidal shape, setting the pyramidal protruded portion to a position corresponding to the front of the feed point of the dipole antenna element and the both parts of the said parasitic element towards ends to positions corresponding to the rear of the dipole antenna element. A feed circuit provided on the face side of dielectric substrate is connected to a coaxial connector provided at the back of the reflector.

ABSTRACT OF THE DISCLOSURE

To realize a reflector-provided dipole antenna showing an outstanding performance in a wide frequency range and allowing simultaneous transmission and reception at different frequencies.

A dipole antenna element is provided at the back of a dielectric substrate set to the reflector surface. A parasitic element is provided on the front of the dielectric substrate, which is constituted by forming and protruding the central portion of a linear conductor forward like an almost trapezoidal shape, setting the pyramidal protruded portion to a position corresponding to the front of the feed point of the dipole antenna element and the both parts of the said parasitic element towards ends to positions corresponding to the rear of the dipole antenna element. A feed circuit provided on the face side of dielectric substrate is connected to a coaxial connector provided at the back of the reflector.

TITLE OF THE INVENTION

REFLECTOR-PROVIDED DIPOLE ANTENNA

BACKGROUND OF THE INVENTION

The present invention relates to a reflector-provided dipole antenna suitable for the antenna of a base station for mobile communication or the like for which broad-band characteristics and simultaneous transmission and reception are required.

For the base stations for mobile communication, particularly for cellular telephone system, the communication system with small radio zones is used. In such a system, the same frequency is reused in different radio zones in order to efficiently use the precious frequency resources and to cope with the extreme increase of subscribers.

In the cellular telephone system, the space diversity technique is generally used to improve the communication quality. As a result, however, the number of antennas installed at each base station increases. For decreasing the number of antennas, the same antenna is used in common for the transmission and reception in the uplink and downlink with different frequencies.

For this type of transmitting-receiving antenna, it is required to have as wide a frequency band as 810 to 960 MHz for the digital cellular telephone system, an example in Japan. Moreover, it is required that horizontal directivities for

transmission and reception are almost identical in the uplink and downlink so that the service quality in both links is kept equal.

FIG. 20 is a perspective view showing a reflector-provided dipole antenna having been used so far as an antenna meeting said requirement, in which symbol 1 denotes a reflector and 2 denotes a dielectric substrate.

Symbol 3 denotes a conductor for forming a dipole antenna element and 4 denotes an earth conductor which is perpendicularly attached to the central portion of the said conductor 3. Both 3 and 4 are provided on the back surface of the dielectric substrate 2.

FIG. 21(a) shows an essential portion of the back side of the dipole antenna element and feed circuit. A notch 20 is formed at one side of the central portion of the conductor 3, dividing the conductor 3 into two, and forms a dipole antenna element. From the vertex of the notch 20, a slot 21 is formed on and along the earth conductor 4 for forming a feed circuit for the said dipole antenna element. The intersection 22 of notch 20 and slot 21 is the feed point of the said dipole antenna element.

Fig. 21(b) shows the face side of substrate 2. Symbol 5 denotes a folded conductor for forming a feed circuit and 16 denotes a parasitic element. The folded conductor 5 forms a micro-strip line balance-unbalance conversion circuit (BALUN) associated with the branch conductor formed

by the divided portion of the earth conductor 4 provided on the back of the dielectric substrate 2.

The parasitic element 16 comprises a linear conductor having a length of a little shorter than $\lambda/2$, λ being the designed radiation wavelength, and is set a little separated from and in parallel with the conductor 3, which forms a dipole antenna element as shown in FIG. 20. Those elements such as 5 and 16 formed on the face side of substrate 2 can be formed on the back side, provided those such as 3 and 4 on the back side to be formed on the face side.

In FIG. 20, a coaxial connector (not shown in the figure) is provided on the back of the reflector 1. The inner conductor of the coaxial connector is made to pass through a hole provided on the reflector 1 and connected to the rear end of the folded conductor 5 so that it is not electrically connected with the reflector 1, and the outer conductor of the coaxial connector is connected to the rear end of the earth conductor 4 through the hole on the reflector 1.

In the case of this antenna, the resonance characteristics of the dipole antenna element comprising the conductor 3 is electromagnetically coupled with the resonance characteristics of the parasitic element 16 and broad-band characteristics are obtained based on the double-tuning principle.

FIG. 22 shows the frequency response of beam width (half power beam width) of the conventional antenna shown in FIGS. 20 and 21 in the magnetic field plane (in the horizontal plane

when the radiated wave is of vertical polarization) for the case where the distance between the feed point and the reflection surface of the reflector 1 is approximately 0.3λ , the length of the reflector 1 in the direction of electric field is approximately 1λ , and the length of the reflector 1 in the direction of magnetic field on the reflector surface is approximately 0.6λ .

In this figure, x-axis shows the frequency (MHz) of the radiated wave and y-axis shows the beam width (degree) in the magnetic field plane. From FIG. 22, it is found that there is a defect that the beam width changes greatly in accordance with the change of frequency of radiated wave.

In the case of the conventional antenna shown in FIGS. 20 and 21, the parasitic element 16 is made so that the length of the element 16 is a little shorter than that of the dipole antenna element. Therefore, the conventional antenna resonates at a frequency higher than that of the dipole antenna element. Thus, the beam width decreases when the frequency of radiation wave is low because the parasitic element 16 serves as a director. When the frequency of radiation wave is high, large current flows through the dipole antenna element serving as the radiation center and the large current flowing through the dipole antenna element moves to the parasitic element and the beam width increases.

That is, the parasitic element of a conventional antenna is effective to widen the band width of return loss but it is improper as a shared antenna for uplink and downlink having

different frequencies like an antenna of a base station for mobile communication because the beam width greatly changes against the frequency change of radiation wave.

Moreover, in the case of a conventional antenna, the parasitic element must be placed a little separated from the dipole antenna element for keeping the wide band characteristic, and the height of substrate 2 from the reflector 1 becomes large. Therefore, the outside diameter of a cylindrical radome for covering the antenna must be increased and thereby, difficulty arises in selecting the place for antenna installation due to the increased weight, size wind load of the radome.

SUMMARY OF THE INVENTION

It is an object of the present invention to eliminate disadvantages of a conventional antenna by realizing a reflector-provided dipole antenna comprising:

- a dipole antenna element set to the back (or face) side of a dielectric substrate perpendicularly provided on the surface of a reflector;

- a feed circuit provided on the dielectric substrate; and
- a parasitic conductive element provided on the face (or back) side of the said dielectric substrate and constituted by setting a pyramidal protrusion formed at the central portion of the parasitic element to a position corresponding to the front side of the feed point of the dipole antenna element and setting the linear portions of the parasitic

element, towards both ends, to a position corresponding to the rear side of the dipole antenna element.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 is an embodiment of the present invention;

FIGS. 2(a) and 2(b) are essential portions of an antenna of the present invention;

FIG. 3 is the frequency response of the beam width of an antenna of the present invention;

FIG. 4 is the frequency response of the return loss of an antenna of the present invention;

FIGS. 5(a) and 5(b) are essential portions of the optimum embodiment of the present invention;

FIGS. 6(a) and 6(b) are essential portions of another embodiment of the present invention;

FIGS. 7(a) and 7(b) are essential portions of still another embodiment of the present invention;

FIGS. 8(a) and 8(b) are essential portions of still another embodiment of the present invention;

FIGS. 9(a) and 9(b) are essential portions of still another embodiment of the present invention;

FIGS. 10(a) and 10(b) are essential portions of still another embodiment of the present invention;

FIGS. 11(a) and 11(b) are essential portions of still another embodiment of the present invention;

FIGS. 12(a) and 12(b) are essential portions of still another embodiment of the present invention;

FIGS. 13(a) and 13(b) are essential portions of still another embodiment of the present invention;

FIGS. 14(a) and 14(b) are essential portions of still another embodiment of the present invention;

FIGS. 15(a) and 15(b) are essential portions of still another embodiment of the present invention;

FIGS. 16(a) and 16(b) are essential portions of still another embodiment of the present invention;

FIG. 17 is an array antenna comprising an antenna of the present invention;

FIG. 18 is the frequency response of the beam width of an array antenna of the present invention;

FIG. 19 is the frequency response of the return loss of an array antenna of the present invention;

FIG. 20 is a conventional antenna;

FIGS. 21(a) and 21(b) are essential portions of a conventional antenna; and

FIG. 22 is the frequency response of the beam width of a conventional antenna.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

FIG. 1 is a perspective view showing an embodiment of the present invention, in which symbol 1 denotes a reflector and 2 denotes a dielectric substrate, and one edge of the dielectric substrate 2 is attached directly to the reflection surface of the reflector 1 or indirectly by means of a proper support so that the plane of the dielectric substrate 2

perpendicularly intersects with the reflection surface of the reflector 1. The conductor 3 for forming a dipole and the earth conductor 4 are provided on the back side of the dielectric substrate 2, on which, as shown in FIG. 2(a), a notch 20 is formed at the central portion of the front edge of the conductor 3.

Symbol 4 denotes an earth conductor which is perpendicularly attached to the central portion of the said conductor 3. Both 3 and 4 are provided on the back side of the dielectric substrate 2. FIG. 2(a) shows an essential portion of the back side of the dipole antenna element and feed circuit.

A notch 20 is formed at the front of the central portion of the conductor 3, dividing the conductor 3 into two, and forms a dipole antenna element. From the vertex of the notch 3 a slot 21 is formed on and along the earth conductor 4 for forming a feed circuit for said dipole antenna element. The intersection 22 of notch 20 and slot 21 is the feed point of said dipole antenna element.

FIG. 2(b) shows the face side of substrate 2. Symbol 5 denotes a folded conductor for forming a feed circuit and 16 denotes a parasitic element. As shown in FIG. 1 and FIG. 2(b), they are provided on the face surface of the dielectric substrate 2. The folded conductor 5 forms a micro-strip line balance-unbalance conversion circuit (BALUN) associated with the branch conductor formed by the divided portion of the earth conductor 4 provided on the back surface of the

dielectric substrate 2. The parasitic element 6 comprises linear conductors 25 towards the ends having a length a little shorter than $\lambda/2$, λ being a designed radiation wavelength, constituted by providing a pyramidal protruding 26 at the central portion of the conductor 6. The pyramidal protruded portion 26 is set to a position corresponding to the notch 20 in FIG. 1 formed at the central portion of the conductor 3 for forming a dipole antenna element. This position corresponds to the upper part (in FIG. 1) of the feed point of the dipole antenna element. The linear portions 25 towards both ends of conductor 6 is set to positions corresponding to the rear edge of the conductor 3 for forming the dipole antenna element on the back side.

In this explanation, FIG. 2(a) is the back side of the substrate 2 and FIG. 2(b) is the face side. The face and back side can be interchanged, if necessary, achieving the same performance.

Moreover, though not shown in the figure, a coaxial connector is provided on the back of the reflector 1. The inner conductor of the coaxial connector is made to pass through a hole provided on the reflector 1 and connected to the rear end of the conductor 5 for forming the balance-imbalance conversion circuit(BALUN) so that the inner conductor is not electrically connected with the reflector 1, and the outer conductor of the coaxial connector is connected to the rear end of the earth conductor 4 through the hole on the reflector 1.

FIG. 3 shows the frequency response of beam width (half power beam width) of the antenna of the present invention shown in FIGS. 1 and 2 in the magnetic field plane (in the horizontal plane when the radiated wave is of vertical polarization) when setting the distance between feed point, or the vertex of notch 20, of the dipole antenna element and the reflection surface of the reflector 1 to approximately 0.3λ , setting the length of the reflector 1 in the direction of electric field to approximately 1λ , and setting the length of the reflector in the direction of magnetic field to approximately 0.6λ . In this figure, x-axis shows the frequency (MHz) of radiated wave and y-axis shows the beam width (degree) in a magnetic field plane. From FIG. 3, it is found that the beam width is almost constant, independent of the frequency change of radiated wave. This is because, when the frequency of radiated wave is relatively high, a relatively large current is induced through the parasitic element 6 and the electrical distance (the distance in terms of radiated wavelength) between the reflection surface of the reflector 1 and the radiation center is kept almost constant.

Therefore, an antenna of the present invention is suitable for, for example, a transmitting-receiving antenna operating at different frequencies.

FIG. 4 shows the result of measurement of the reflection characteristics viewed from the coaxial connector (provided on the back side of the reflector 1 but not shown in the figure).

The measurement was made in terms of frequency response of return loss. The x-axis shows frequency (MHz) of radiated wave and y-axis shows return loss (dB) in the case of the antenna of the present invention shown in FIGS. 1 and 2. From FIG. 4, it is found that the relative band width of the voltage standing wave ratio (VSWR) at a value of 1.5 or less is approximately 20%. From this figure, it can be noted that the band widening is sufficiently achieved based on the double-tuning principle according to electromagnetic coupling between the resonance characteristics of a dipole antenna element formed by the conductor 3 and that of the parasitic element 6.

FIG. 5(a) and FIG. 5(b) are simplified version of FIG. 2(a) and FIG. 2(b), in which the parasitic element 6 is shown by a mere continuous line, where as it is shown by a shaded strip in FIGS. 2(a) and 2(b).

FIGS. 6(a) and 6(b) to FIGS. 15(a) and 15(b) are illustrations for explaining essential portions of other embodiments of the present invention (illustrations for explaining other embodiments of the parasitic element 6). The parasitic elements 6 in FIGS. 6 to 15 are shown in the same manner as the case of FIG. 5.

In the case of the parasitic elements 6 shown in FIGS. 6 to 11, shapes of the protruded portions formed at the central portion of parasitic element 6 are almost like a trapezoid similar to the case of the parasitic element 6 shown in FIG. 2. However, the shapes at the both ends of the parasitic

element 6 are different each other. The one in FIG. 6 is upward concave with relatively large curvature. In the case of FIG. 7, it is of a curved shape upward convex having a relatively large curvature. In FIG. 8, it is of a consecutive waves of relatively small curvature. In the case of FIG. 8, it is of consecutive. In the case of FIG. 9, it is a straight wedge shape.

As shown in FIG. 10, it is possible to make all corners of pyramidal protrusion of the parasitic element rounded.

FIG. 11 shows a case of properly extending outward the ends of all elements of the parasitic element 6.

FIG. 12 shows a case of forming the central portion of the parasitic element 6 into a pyramid shape and extending the both ends into straight lines. In the case of this embodiment similarly to those of the embodiments in FIGS. 6 to 9, it is also possible to embody the present invention by forming the both ends into a curved shape having a relatively large curvature and concave or upward convex, consecutive waves with a relatively small curvature, or straight lines and making all corners of the parasitic element 6 sharp or rounded.

FIG. 13 shows a case of forming the central portion of the parasitic element 6 into semi-circular shape and forming the both ends into straight lines linear shape. This embodiment also makes it possible to embody the present invention by forming the both ends into a curved shape having a relatively large curvature and concave or upward convex,

consecutive waves with a relatively small curvature, or a linear wedge shape and making all corners of the parasitic element 6 sharp or rounded.

FIG. 14 shows a case of forming the central portion of the parasitic element 6 into an multiple straight lines approximating a circle and forming the both ends into straight lines. In this embodiment it is also possible to embody the present invention by forming the both ends into a curved shape having a relatively large curvature, concave or upward convex, and a polygonal line, consecutive waves having a relatively small curvature and a polygonal line to make a waveform, or a linear wedge shape, and making all corners of the parasitic element 6 sharp or rounded.

FIG. 15 shows a case of forming the central portion of the parasitic element 6 into an almost rectangular shape and forming the both ends into straight lines. In this embodiment also makes it possible to embody the present invention by forming the both ends into a curved shape having a relatively large curvature and concave or upward convex, a consecutive wave shape having a relatively small curvature, or a linear wedge shape, and making all corners of the parasitic element 6 sharp or rounded.

In the case of any of the embodiments above described, the function of the parasitic element 6 is the same as that of the parasitic element 6 shown in FIGS. 1 and 2.

FIGS. 16(a) and 16(b) are also illustrations showing essential portions of another embodiment of the present

invention, in which FIG. 16(a) shows the back (or face) side of one essential portion and FIG. 16(b) shows the face (or back) side of the other essential portion.

In the case of this embodiment, a dipole antenna is formed with a conductor 3_F for forming a folded dipole antenna and its function is the same as that of the dipole antenna shown in FIGS. 1 and 2. In the case of the folded dipole antenna of this embodiment, however, it is possible to make the input impedance large compared to the case of the dipole antenna shown in FIGS. 1 and 2. Therefore, the structure using folded dipole antenna is suitable for an antenna for constituting an array antenna to be described later.

In this embodiment it is also possible to embody the present invention by forming the parasitic element 6 into any one of the shapes described in FIGS. 6 to 15.

In FIG. 16, symbols and structures other than conductor 3_F are the same as those in FIG. 2.

FIG. 17 is a perspective view showing an array antenna comprising an antenna of the present invention, in which symbol 11 denotes a common reflector and 12 denotes a common dielectric substrate. In the case of this embodiment, the plane of the common dielectric substrate 12 is set so as to be parallel with the reflection surface of the common reflector 11.

To keep the parallel relation between the common reflector 11 and the common dielectric substrate 12, for example, a proper solid dielectric is inserted between the

common reflector 11 and the common dielectric substrate 12 or the common reflector 11 and the common dielectric substrate 12 are united into one body by setting a spacer made of a proper material between them.

Then, symbols 3_1 and 3_2 denote conductors for forming first and second dipole antenna elements and 14 denotes a common earth conductor for forming a feed circuit. They are provided on the back (or face) side of the common dielectric substrate 12. The conductors 3_1 and 3_2 are provided symmetrically to the central point of the common dielectric substrate 12 and the center of the common earth conductor 14 is approximately set to the central point of the common dielectric substrate 12.

On the common earth conductor 14, longitudinal slots 210 and 211 are provided to which the vertexes of notch 200 and 201 are mated. In other words, two substrates 2, on both of which a dipole antenna element is formed as show in FIG 1, FIG. 2(a) and FIG. 2(b), are connected back-to-back. The two earth conductors 4 of each substrate 2 become now one-piece earth conductor 14.

The intersections of slot 210 and vertex 200, and slot 211 and vertex 201 are the feed points of the first dipole antenna element and the second dipole antenna element, respectively.

Symbols 5_1 and 5_2 denote folded conductors for forming a feed circuit and 6_1 and 6_2 denote parasitic elements. They are provided on the face (or back) side of the common

dielectric substrate 12 so as to be symmetric to the central point of the common dielectric substrate 12.

The folded conductor 5_1 forms a micro-strip line balance-unbalance conversion circuit (BALUN) associated with a part of the branch conductor formed by the divided portion of the earth conductor 14 provided on the back surface of the dielectric substrate 12.

The folded conductor 5_2 dose the same function of BALUN with another part of the branch conductor formed by the divided portion of the earth conductor 14.

The parasitic elements 6_1 and 6_2 have the same shape as the parasitic element 6 shown in FIGS. 1 and 2. The mechanical arrangement relation between the conductor 3_1 for forming a dipole antenna element and parasitic element 6_1 and the mechanical arrangement relation between the conductor 3_2 for forming a dipole antenna element and parasitic element 6_2 are formed similarly to the mechanical arrangement relation between the conductor 3 for forming the dipole antenna element and parasitic element 6 in FIGS. 1 and 2.

Though not shown in the figure, a coaxial connector is provided at the central portion of the back of the common dielectric substrate 12, the inner conductor of the coaxial connector is inserted into a hole provided on the common dielectric substrate 12 and connected to the middle point of the conductors 5_1 and 5_2 for forming the BALUN so that it is not electrically connected with the common earth conductor

14, and the outer conductor of the coaxial connector is connected to the common earth conductor 14.

Moreover, a coaxial cable connected to the coaxial connector is led to the back of the common reflector 11 through a hole provided at the central portion of the common reflector 11.

FIG. 18 is an illustration showing the frequency response of the beam width of the array antenna of the present invention shown in FIG. 17, in which x-axis and y-axis are the same as the case of FIG. 3, the solid line shows the response of the array antenna of the present invention shown in FIG. 17. The broken line shows the response of an array antenna obtained by replacing the parasitic elements 6_1 and 6_2 in FIG. 17 with linear parasitic elements having a length a little smaller than the length of a dipole antenna element, which is of the same configuration as a conventional reflector-provided antenna as shown in FIG. 20. In the case of the array antenna of the present invention (shown by the solid line), the beam width in a magnetic field plane is kept relatively narrow in a radiated frequency range of approximately 800 to approximately 960 MHz. In the case of the response shown by the broken line, however, the beam width in a magnetic field plane, is considerably increased in the same frequency range.

This is caused by the fact that the linear parasitic element provided in front of each dipole antenna element (outside of each dipole antenna element when viewed from the

central point of dielectric substrate) serves as a director when the frequency of radiated wave is low, but serves as a reflector when the frequency of radiated wave is high, and in either case, the beam is narrowed in the plane parallel with the dielectric substrate.

That is, in a plane vertical to the dielectric substrate (magnetic field plane), it tends that the beam becomes wider and the gain become lower. This trend becomes more prominent as the frequency lowers.

Even in the case of the array antenna of the present invention (shown by the solid line), the trends of wider beam width and lower gain exist. However, the trends for wider beam and lower gain are improved by setting the parasitic elements 6_1 and 6_2 inside of the dipole antenna elements 3_1 and 3_2 respectively.

In the case of an array antenna having the same shape and same setting position of a parasitic element as the conventional way, it is necessary to increase the area of the reflector and to increase the distance between the reflector and the dipole antenna element and the distance between dipole antenna elements in order to make the beam width and gain equal to those of an array antenna of the present invention. Therefore, it cannot be avoided that the entire size of an array antenna increases.

On the contrary, when it is permitted to keep the beam width and gain of an array antenna of the present invention

equal to those of a conventional antenna, it is possible to decrease the entire size of the array antenna.

FIG. 19 shows the result of measurement of return loss to illustrate the reflection characteristics of the array antenna of the present invention shown in FIG. 17 viewed from the coaxial connector (not shown though it is set to the back of the common dielectric substrate 12). The x-axis and y-axis are the same as the case of FIG. 4. From FIG. 19, it is found that a relative band width is approximately 18% at the voltage standing wave ratio (VSWR) of approximately 1.5 or less and that the band width is widened almost equally to the case of the antenna of the present invention shown in FIG. 1.

By arranging a proper number of array antennas of the present invention shown in FIG. 17 in the directions of electric field and magnetic field, it is possible to constitute an array antenna having a required radiation characteristics.

In the same manner, by arranging a proper number of antennas of the present invention shown in FIG. 1 in the direction of electric field and magnetic field, it is possible to constitute an array antenna having a required radiation characteristics. Furthermore, in the case of the antenna of the present invention shown in FIG. 1, it is possible to constitute an array antenna by setting another dielectric substrate same as the dielectric substrate 2 on the front surface of the reflector 1 in parallel with the dielectric

substrate 2 at a proper separation and providing another antenna element same as the antenna element provided on the dielectric substrate 2 on the above dielectric substrate.

Also in the case of the array antenna of the present invention shown in FIG. 17, it is possible to replace the dipole antenna elements 3_1 and 3_2 with the folded dipole antenna element shown in FIG. 16 and the parasitic elements 6_1 and 6_2 with any one of the parasitic elements explained in FIGS. 6 to 15.

Because the reflector-provided dipole antenna of the present invention shows an outstanding performance over a wide frequency range and allows simultaneous transmission and reception at different frequencies, the antenna is suitable for a base station for mobile communication. Moreover, by folding and protruding the central portion of the parasitic element, it is possible to set the parasitic element at a position almost same as that of the dipole antenna element. For this reasons, particularly, when storing the antenna of the present invention shown in FIG. 1 in a cylindrical radome, it is possible to reduce the diameter of radome. Therefore, there is an advantage in selecting the site to install the antenna of the present invention, since it is not restricted by the size, weight and wind load.

Claims:

1. A dipole antenna having a reflector, said antenna comprising:

a dielectric substrate having a first and second face, the dielectric substrate being provided at a surface of said reflector;

a dipole antenna element located on said first face of said dielectric substrate;

a feed circuit provided on said dielectric substrate; and

a parasitic element provided on said second face of said dielectric substrate, said parasitic element having a pyramidal middle section and first and second end sections;

wherein the pyramidal middle section overlays the center of said dipole antenna element and the first and second end sections overlay each of the end sections of the dipole antenna element.

2. The dipole antenna of claim 1, wherein the dielectric substrate is located in a plane that is perpendicular to said reflector.

3. The dipole antenna of claim 1, wherein the dielectric substrate is located in a plane that is parallel to said reflector.

4. A dipole antenna having a reflector, said antenna comprising:

a plurality of dielectric substrates each having a first and second face, the plurality of dielectric substrates being provided at a common surface of said reflector;

a dipole antenna element located on said first face of each of said plurality of dielectric substrates;

a feed circuit provided on each of said plurality of dielectric substrates;

a parasitic element provided on said second face of each of

said plurality of dielectric substrates, each said parasitic element having a pyramidal middle section and first and second end sections;

wherein the pyramidal middle section overlays the center of the dipole antenna element and the first and second end sections overlay each of the end sections of the dipole antenna element below the feed point; and

a common feed circuit connected to said feed circuit for each-of said plurality of dielectric substrates.

5. A dipole antenna having a reflector, said antenna comprising:

a dielectric substrate having a first and second face, the dielectric substrate being provided at a front common surface of said reflector and located in a plane parallel with said common surface of said reflector;

first and second dipole antenna elements located on said first face of said dielectric substrate and located symmetrically about a center line on said substrate;

first and second feed circuits provided on said dielectric substrate;

first and second parasitic elements provided on said second face of said dielectric substrate, each said parasitic element having a pyramidal middle section and first and second end sections;

wherein the pyramidal middle section of the first parasitic element overlays the center of the first dipole antenna element and the first and second end sections overlay each of the end sections of the first dipole antenna element and wherein the pyramidal section of the second parasitic element overlays the center of the second dipole antenna element and the first and second end sections overlay each of the end sections of the second dipole antenna element; and

a common feed circuit connected to said first and second feed circuits for said first and second dipole antenna elements.

6. The dipole antenna of claim 1, 4 or 5, wherein said pyramidal middle section is substantially trapezoidal and wherein said first and second end sections are straight lines.

7 The dipole antenna of claim 1, 4 or 5, wherein said pyramidal middle section is substantially curved and wherein said first and second end sections are curved lines.

8. The dipole antenna of claim 1, 4 or 5, wherein said pyramidal middle section is a true pyramidal shape and wherein said first and second end sections are straight lines.

9. The dipole antenna of claim 1, 4 or 5, wherein said pyramidal middle section is a true pyramidal shape and wherein said first and second end sections are curved lines.

10. The dipole antenna of claim 1, 4 or 5, wherein said pyramidal middle section is substantially a semi-circle and wherein said first and second end sections are straight lines.

11. The dipole antenna of claim 1, 4 or 5, wherein said pyramidal middle section is substantially a semi-circle and wherein said first and second end sections are curved lines.

12. The dipole antenna of claim 1, 4 or 5, wherein said pyramidal middle section is substantially a semi-circle approximating a polygonal line and wherein said first and second end sections are straight lines.

13. The dipole antenna of claim 1, 4 or 5, wherein said pyramidal middle section is substantially a semi-circle approximating a polygonal line and wherein said first and second end sections are curved lines.

14. The dipole antenna of claim 1, 4 or 5, wherein said

pyramidal middle section is substantially rectangular and wherein said first and second end sections are straight lines.

15. The dipole antenna of claim 1, 4 or 5, wherein said pyramidal middle section is substantially rectangular and wherein said first and second end sections are curved lines.

FIG. 1

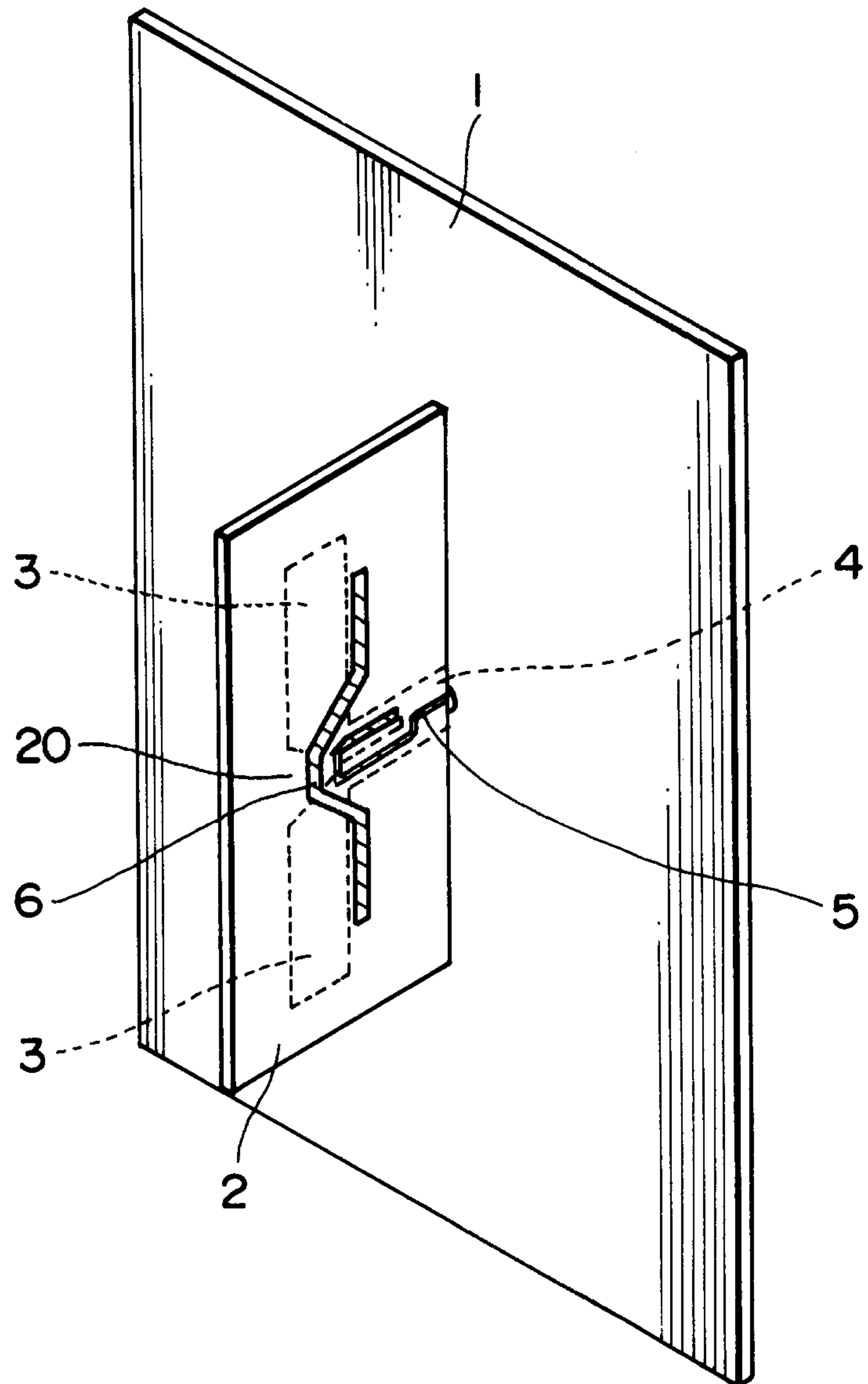


FIG. 2(a)

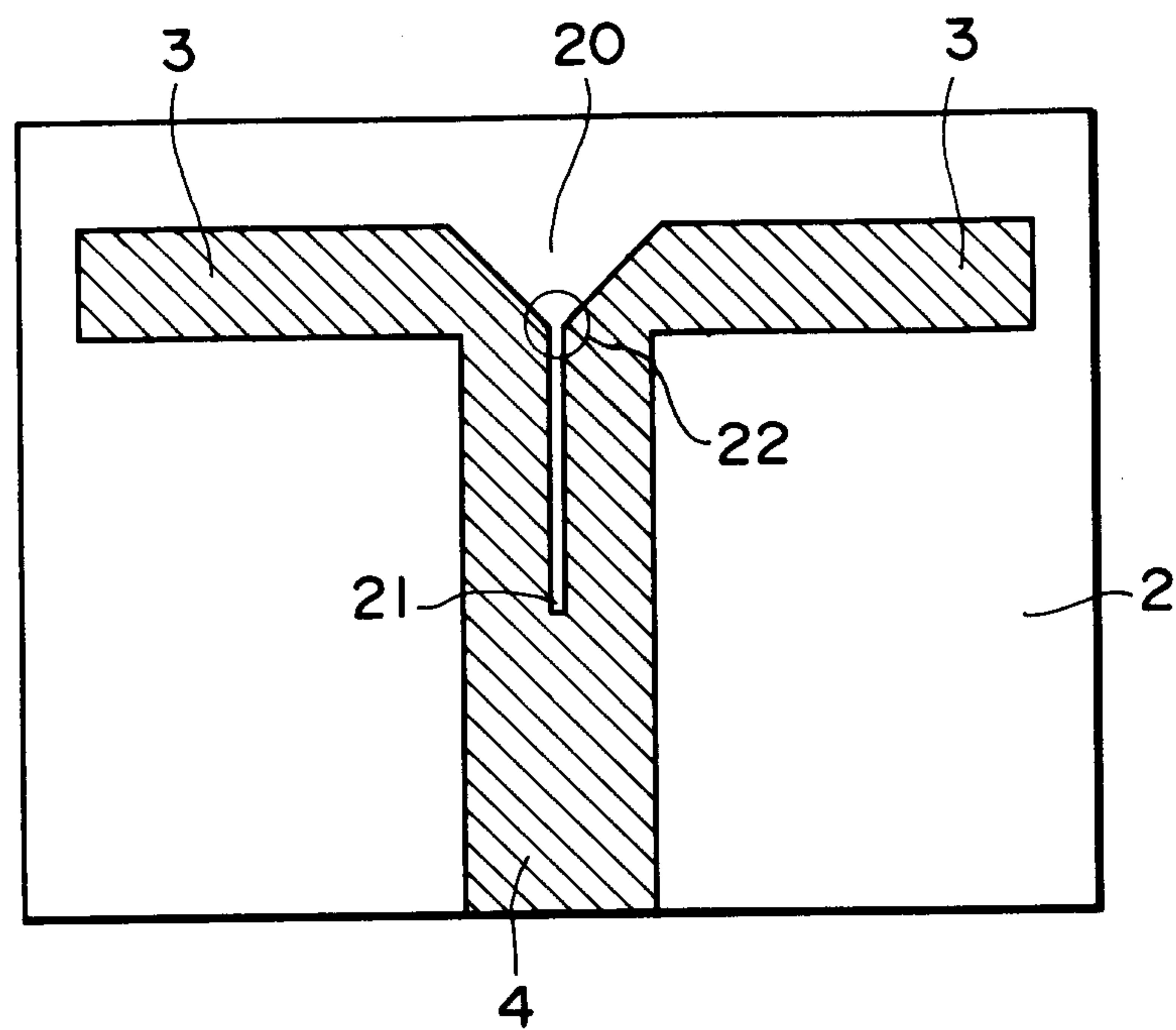


FIG. 2(b)

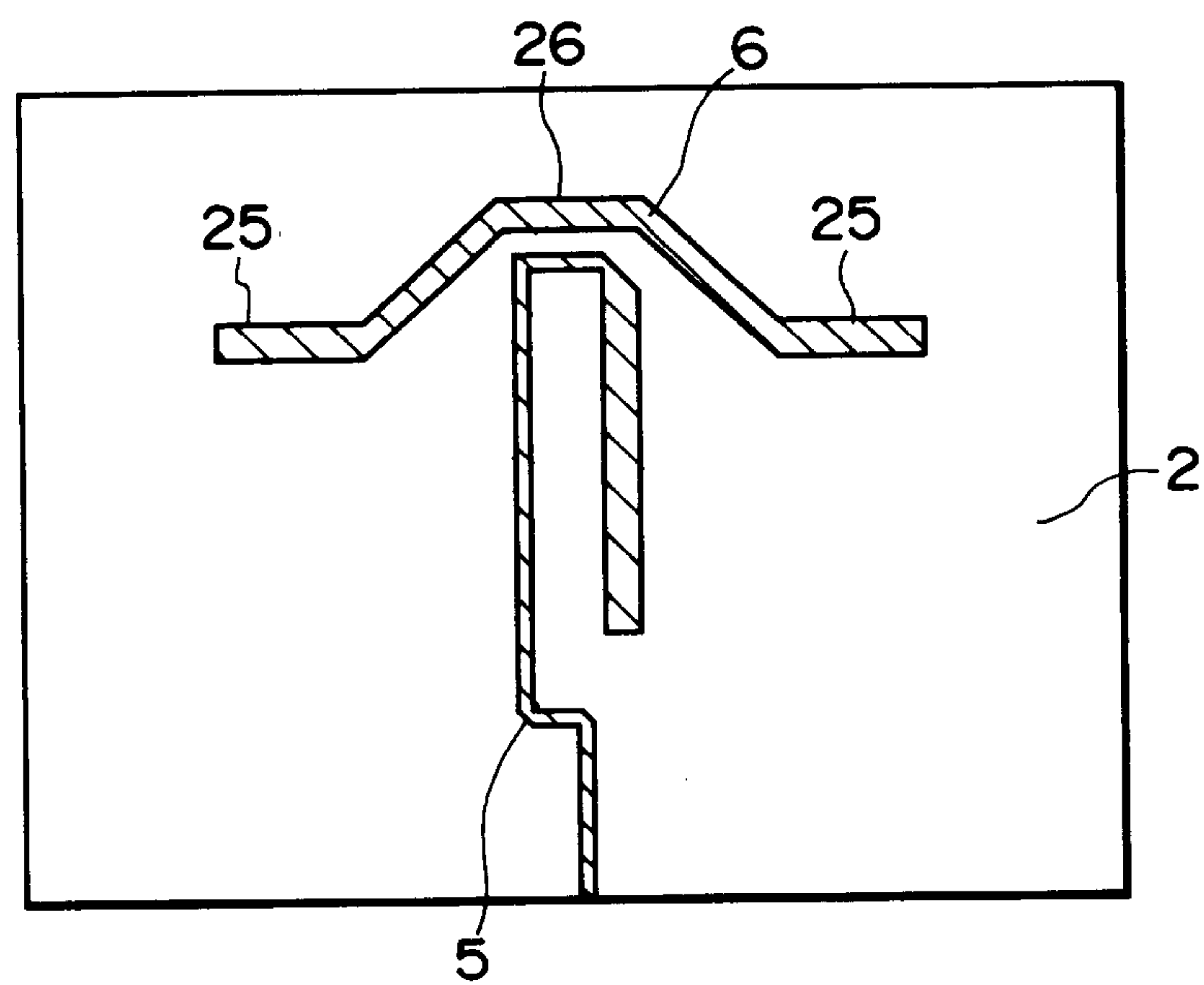


FIG. 3

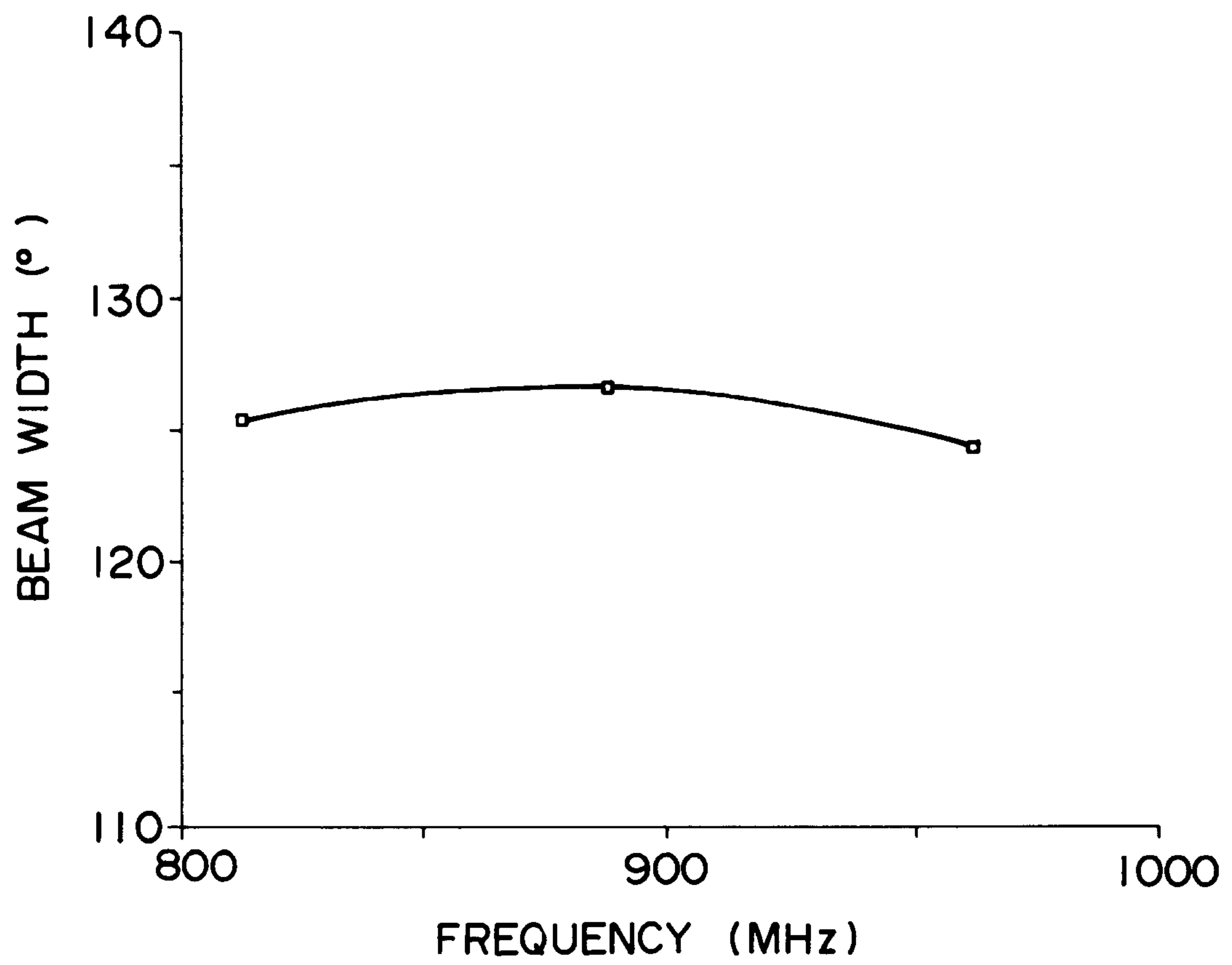


FIG. 4

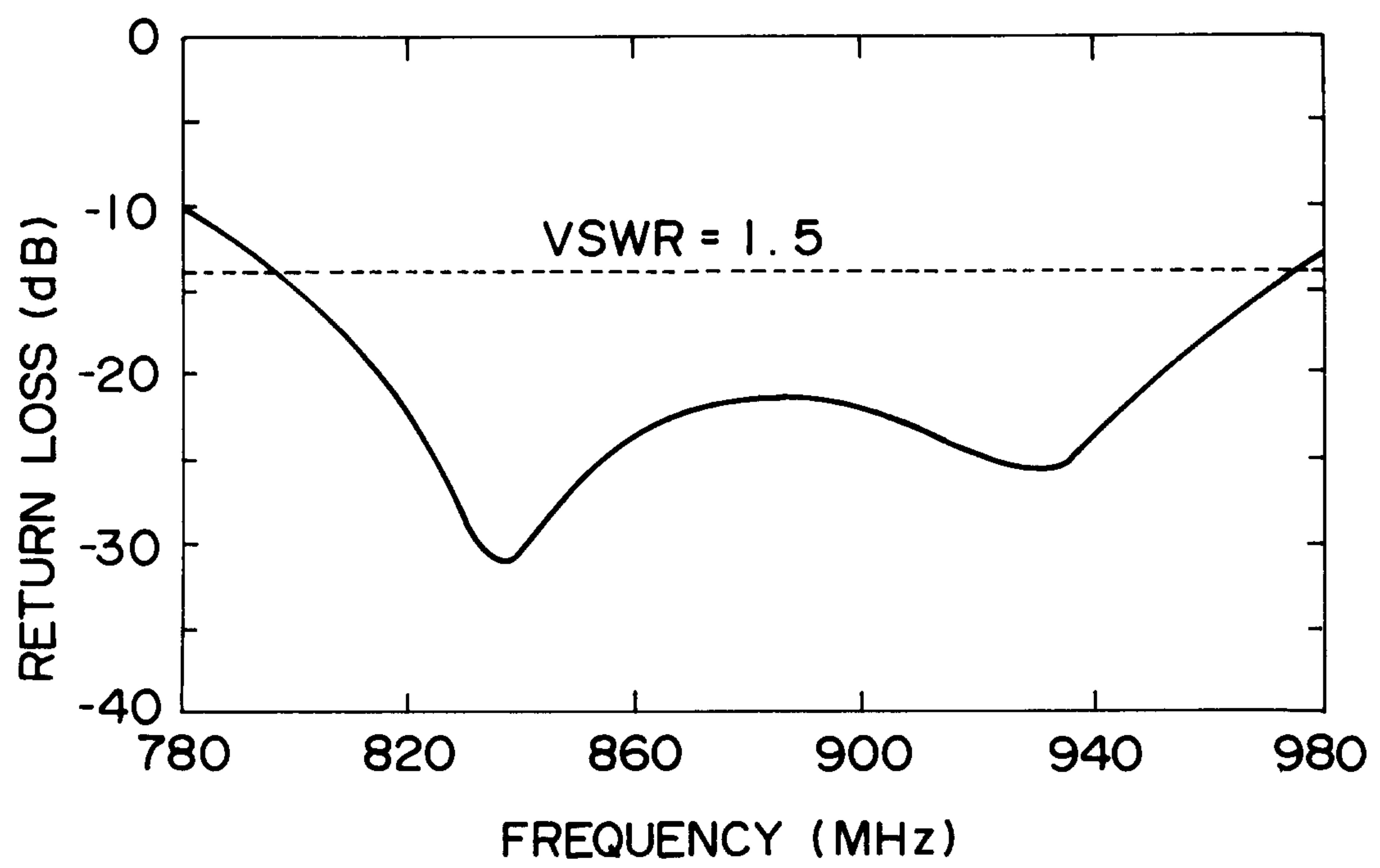


FIG. 5(a)

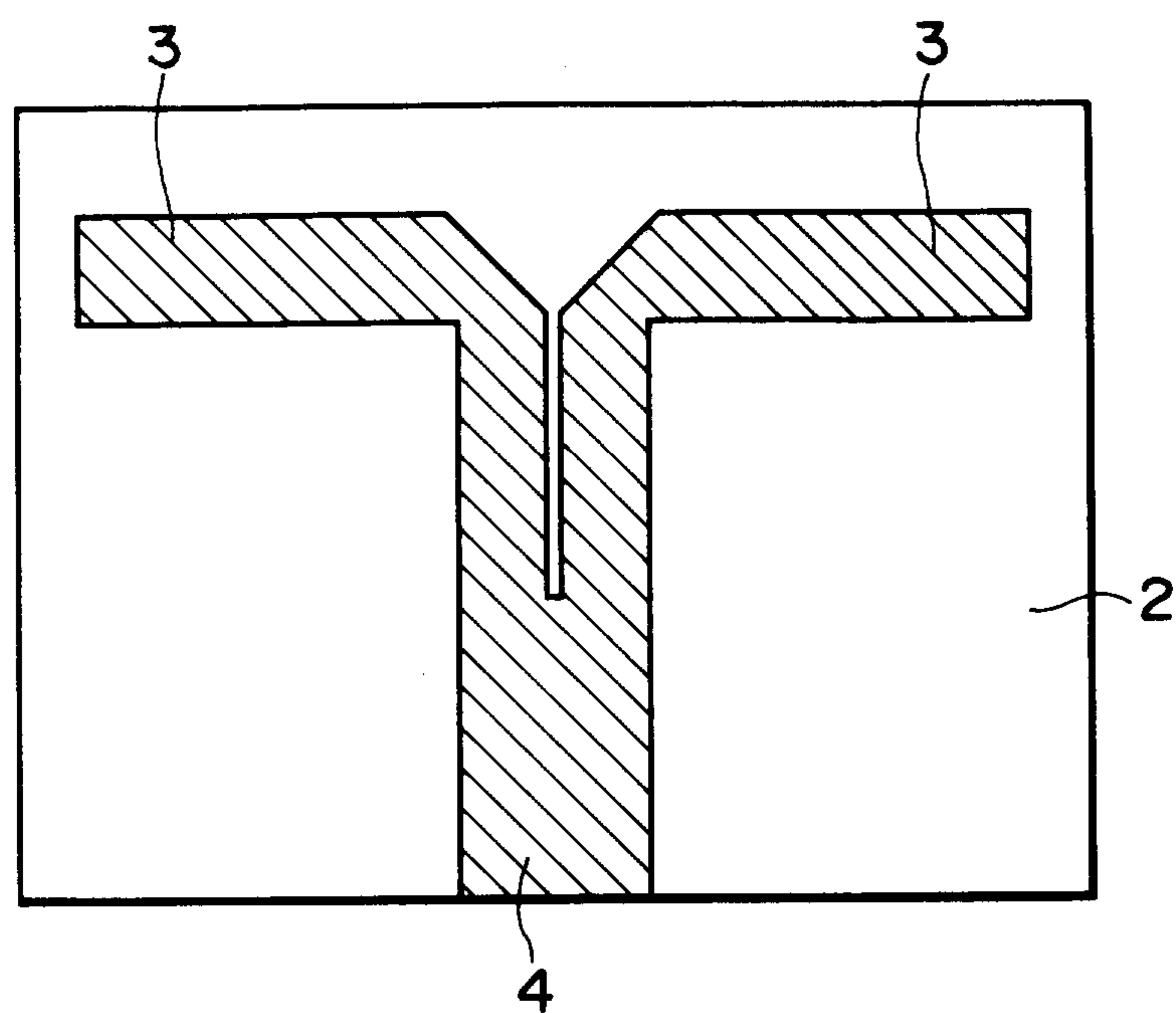


FIG. 5(b)

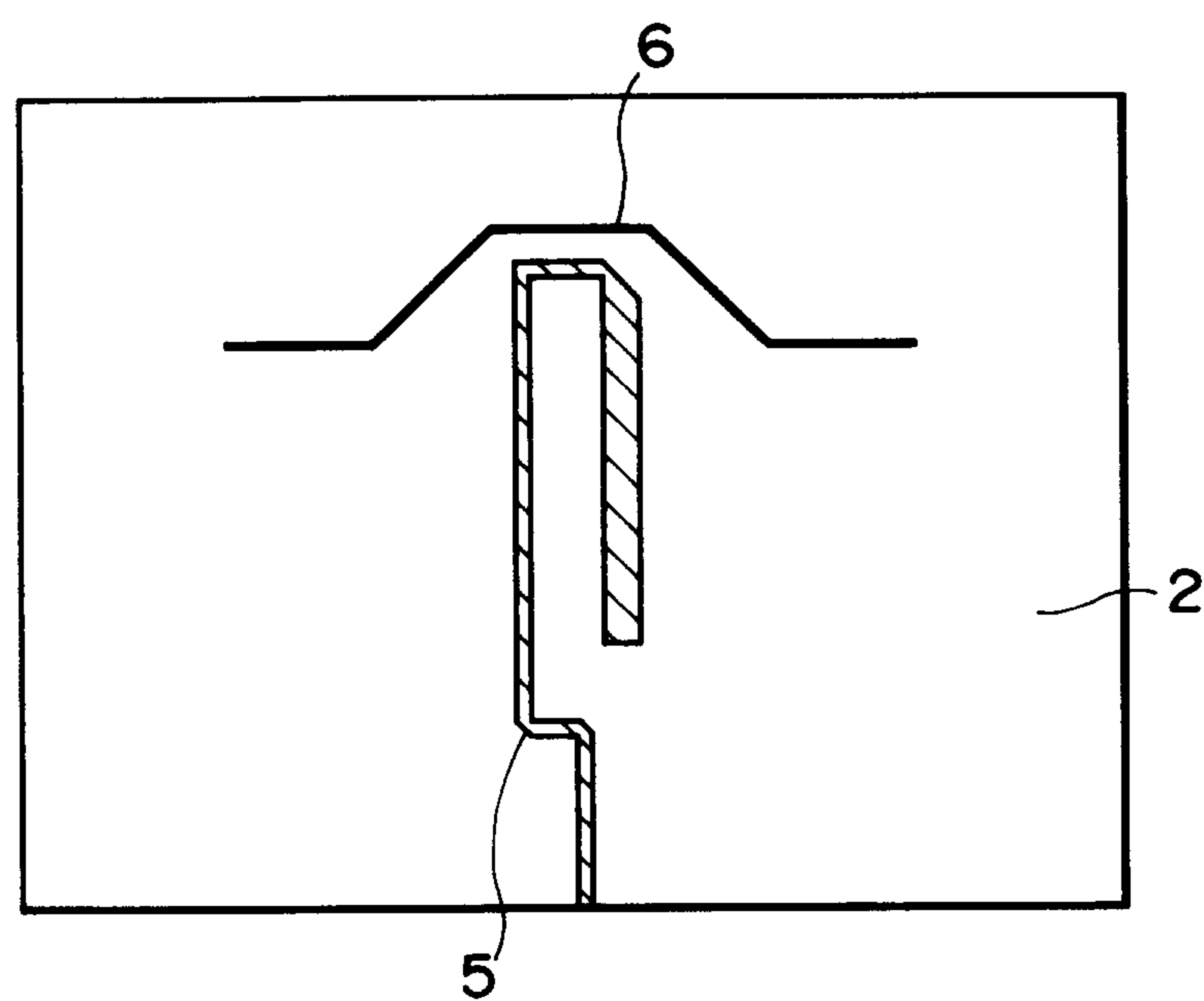


FIG. 6(a)

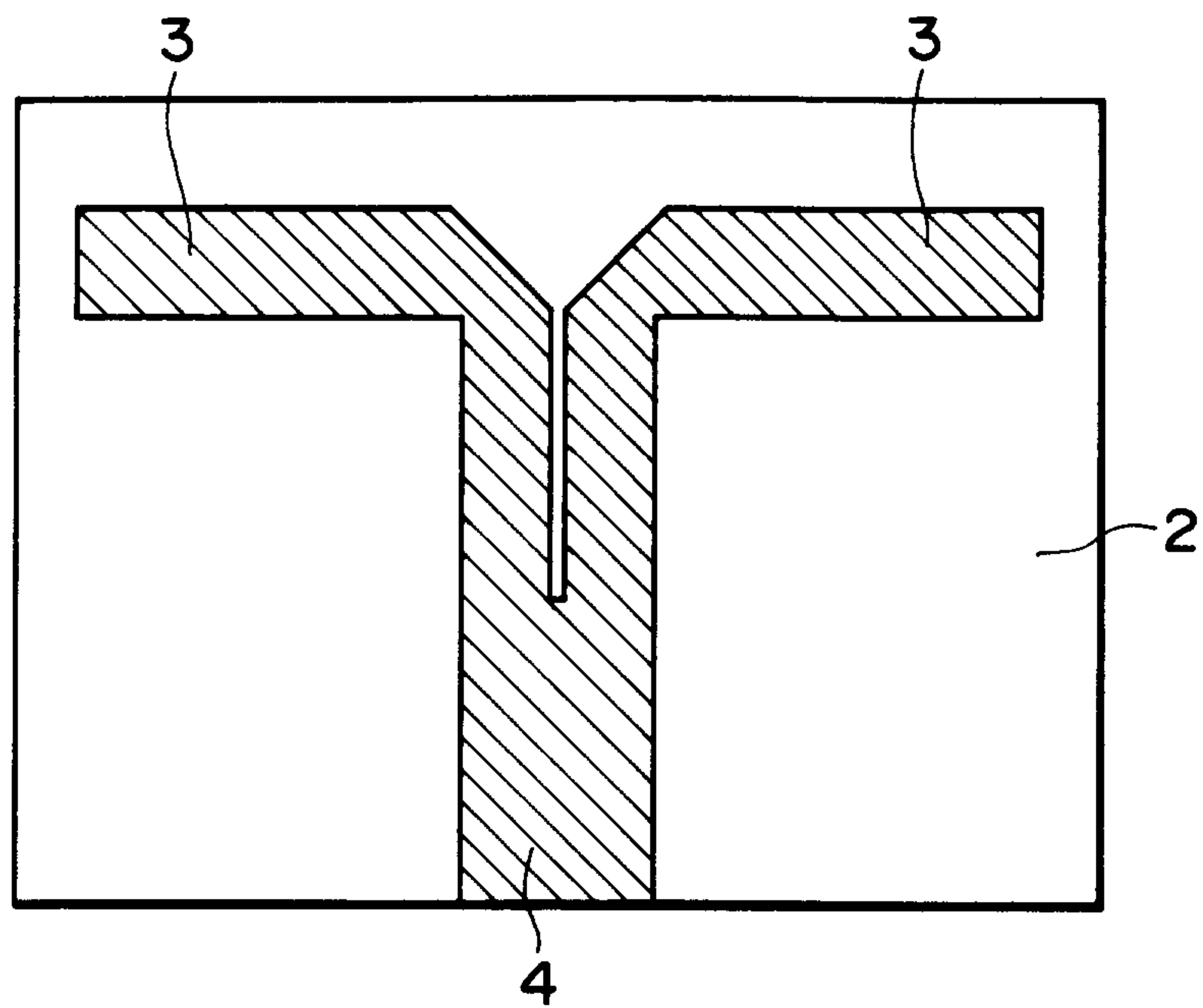


FIG. 6(b)

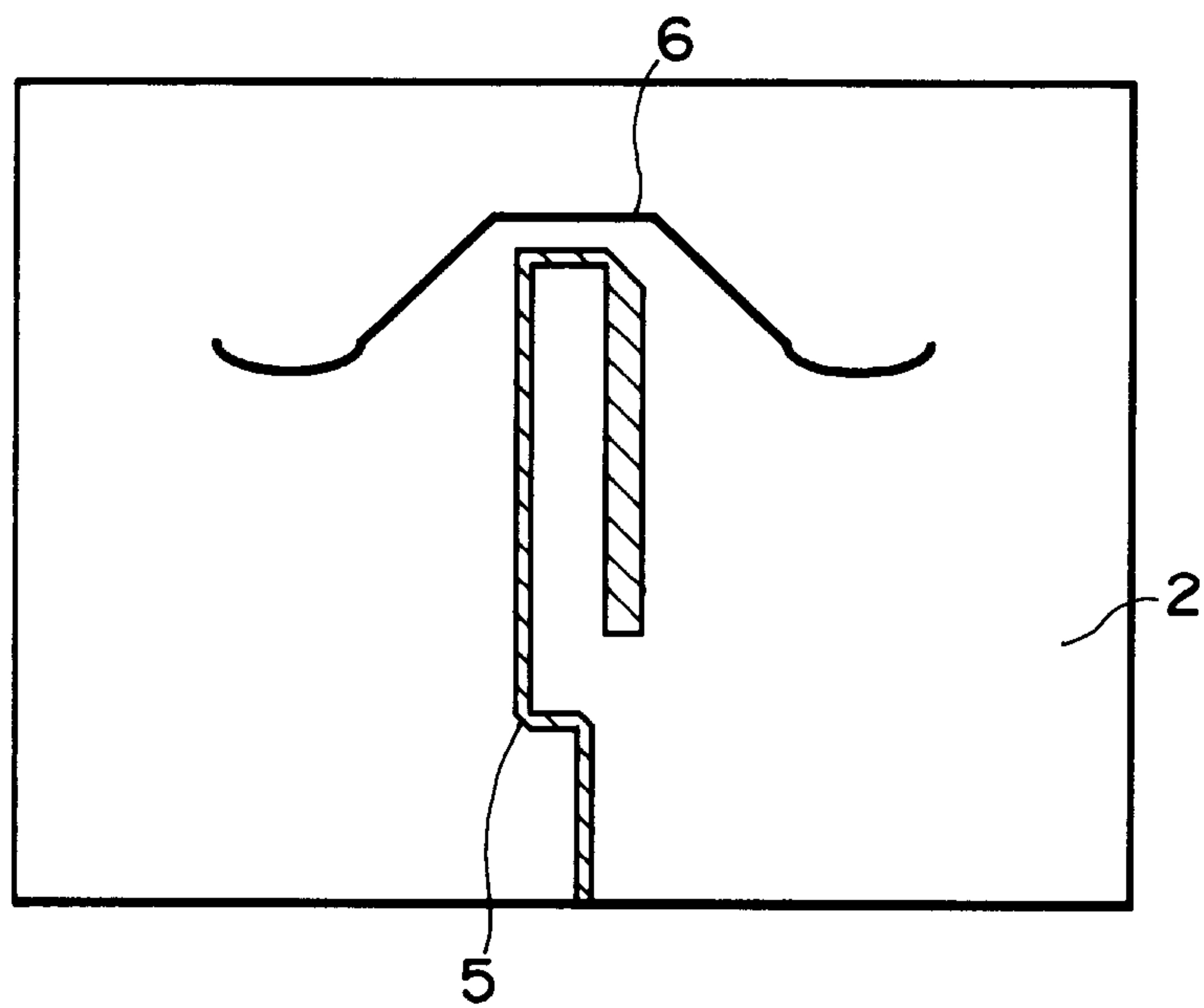


FIG. 7(a)

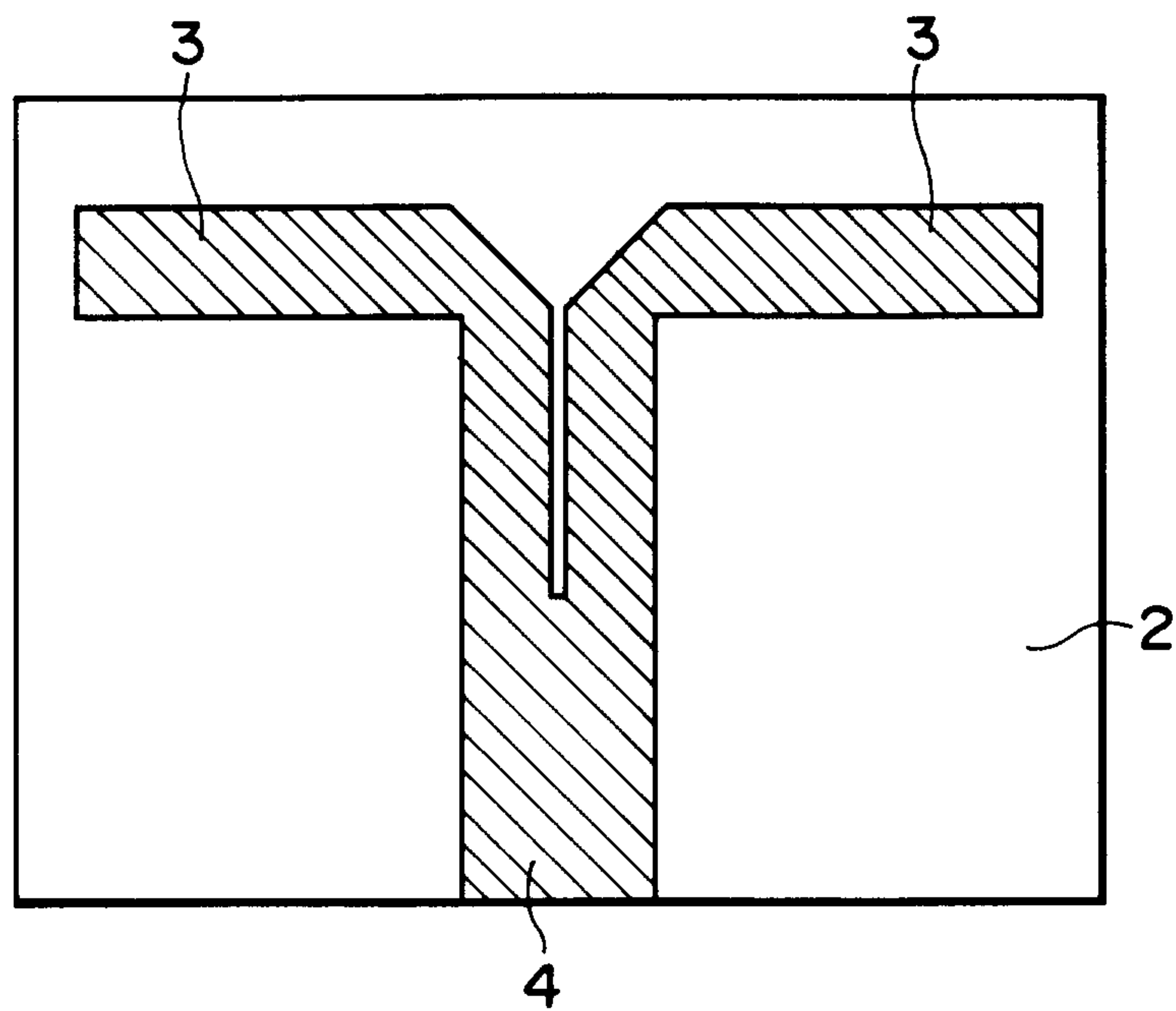


FIG. 7(b)

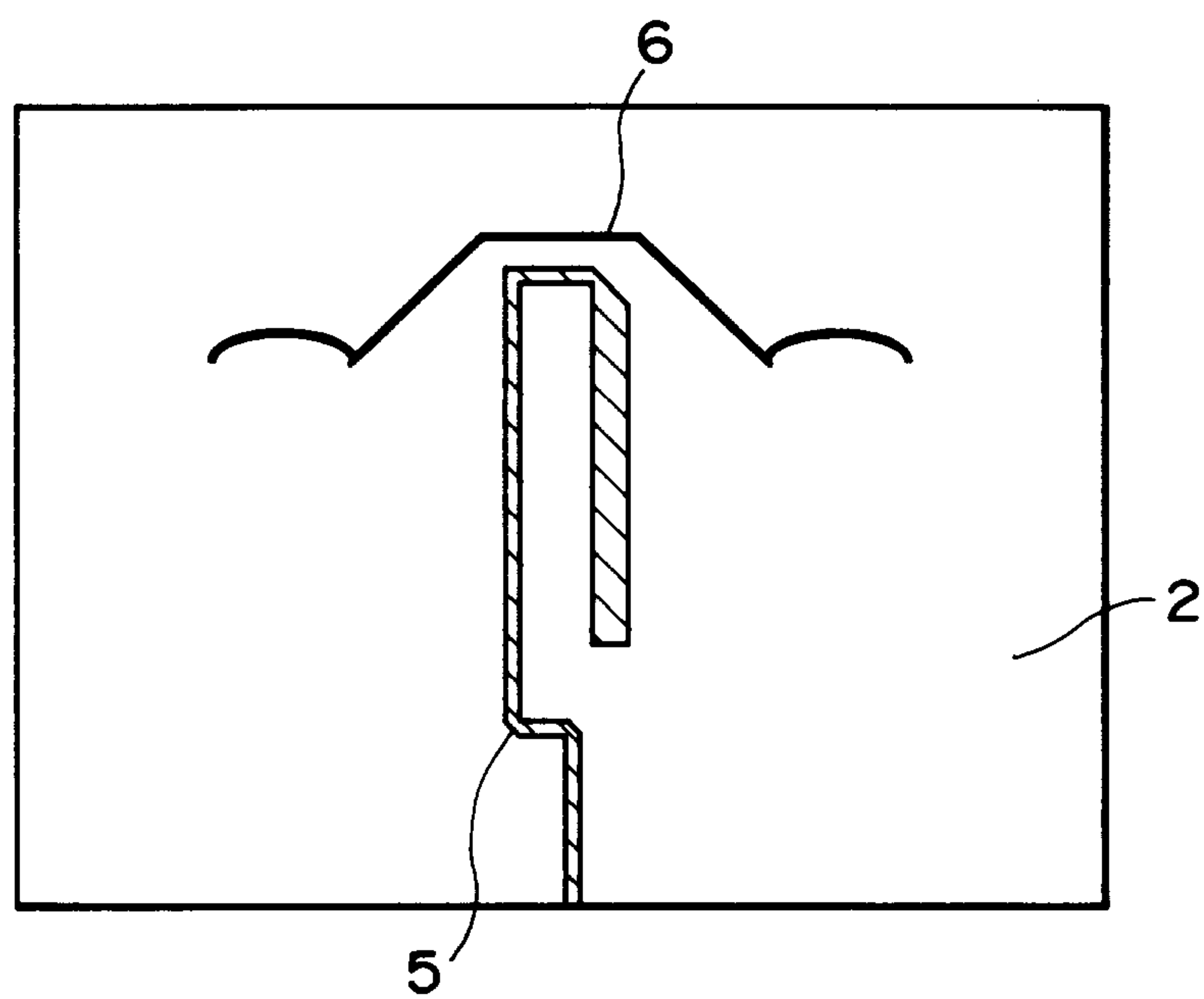


FIG. 8(a)

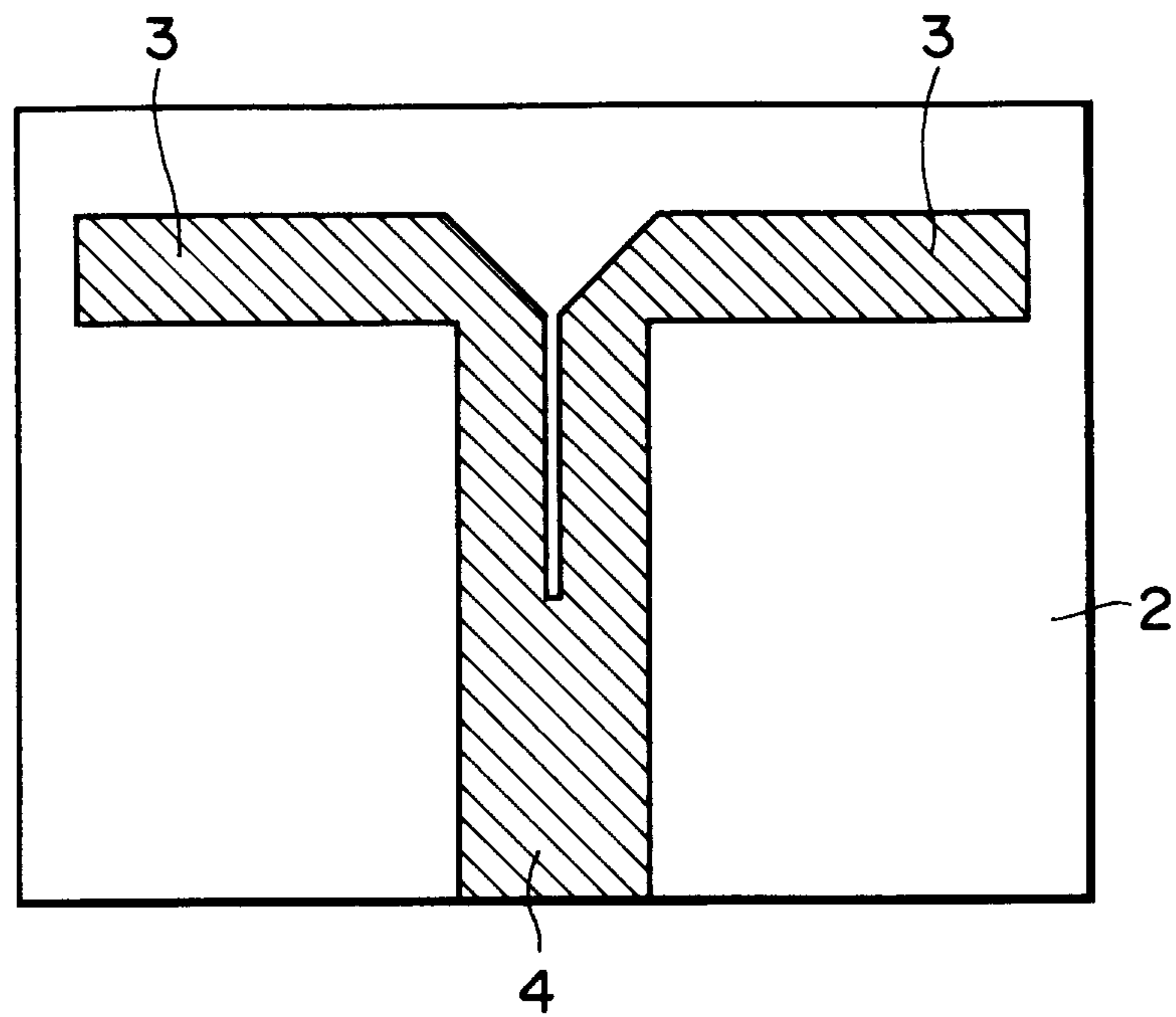


FIG. 8(b)

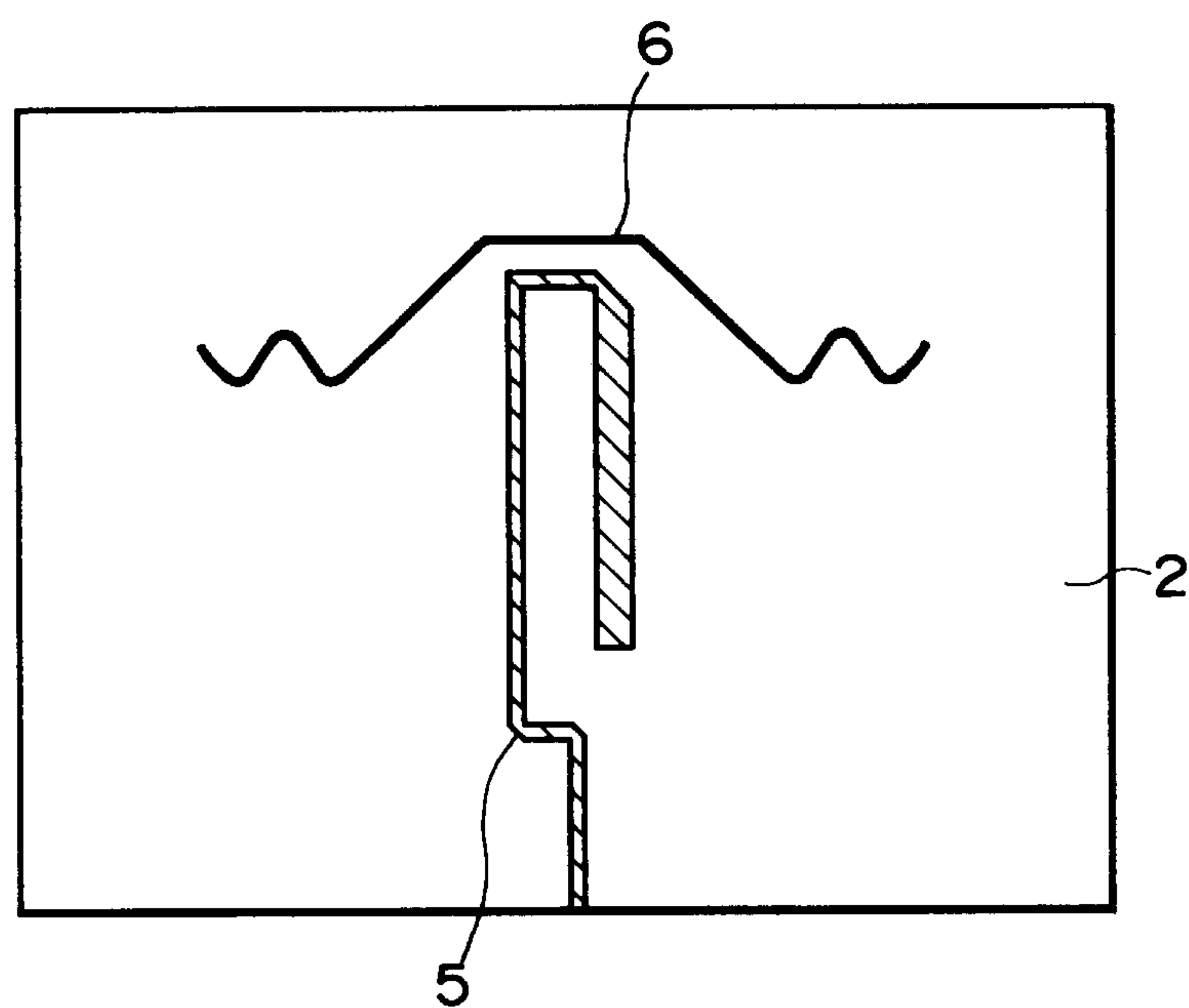


FIG. 9(a)

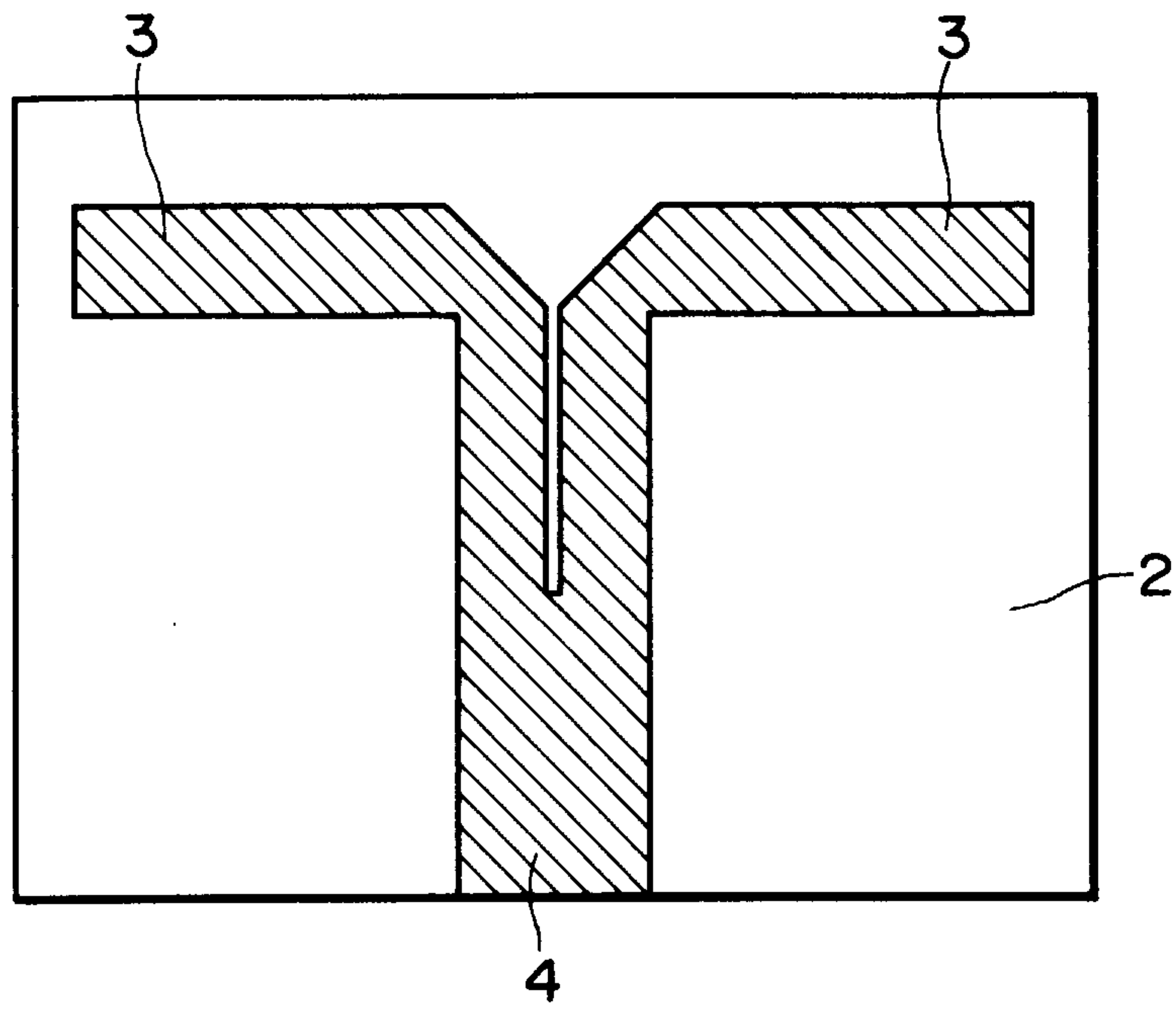


FIG. 9(b)

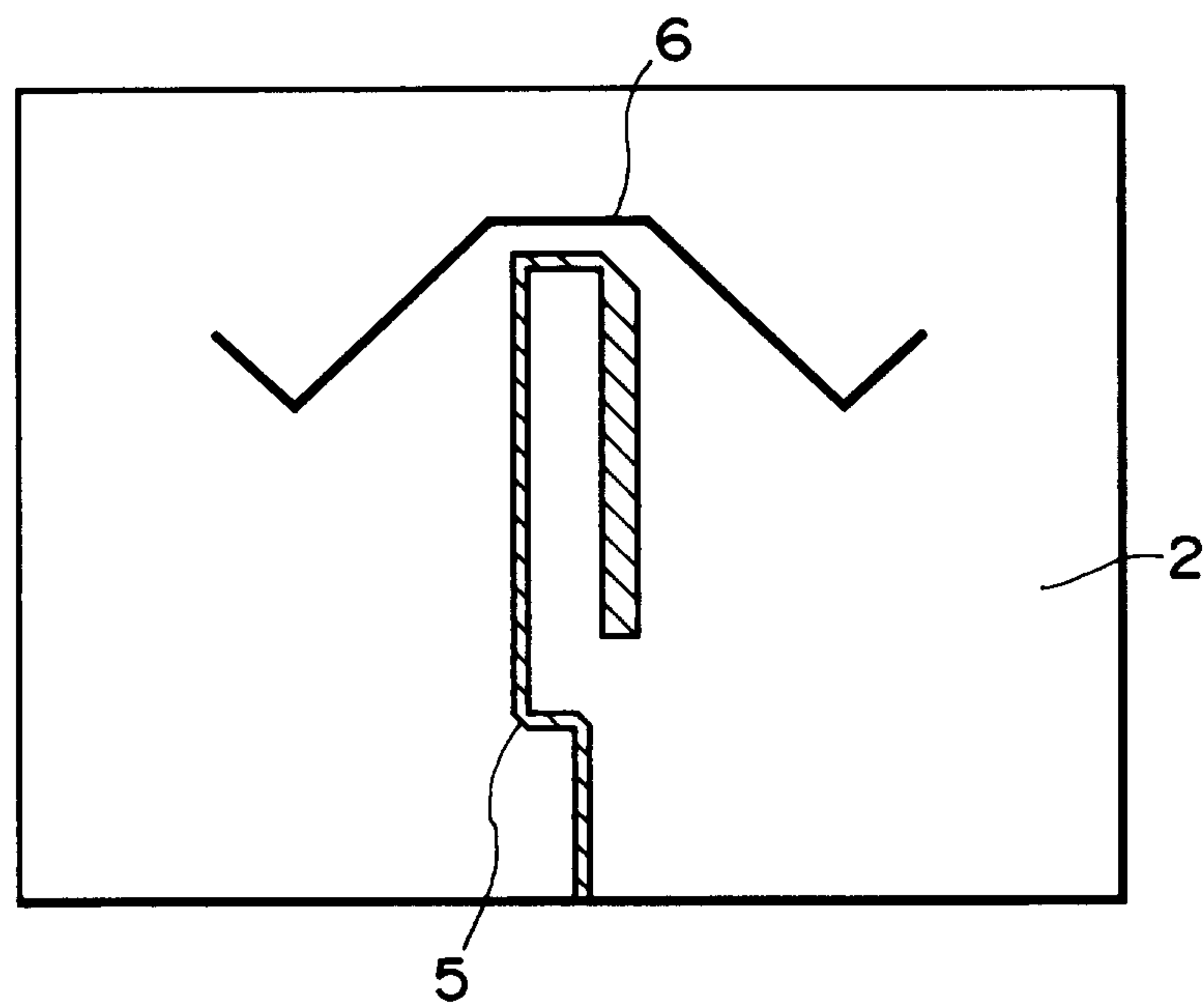


FIG. 10(a)

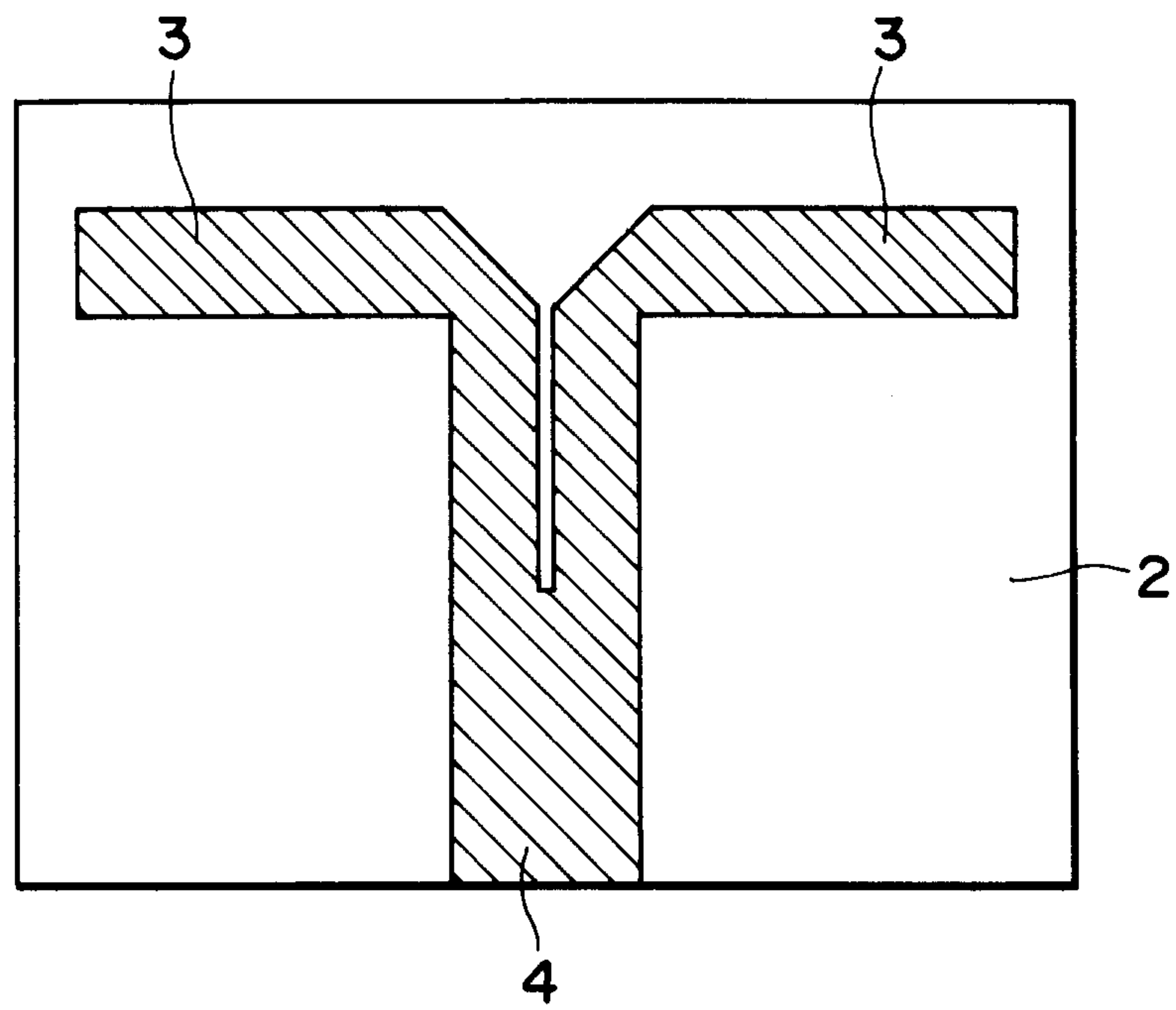


FIG. 10(b)

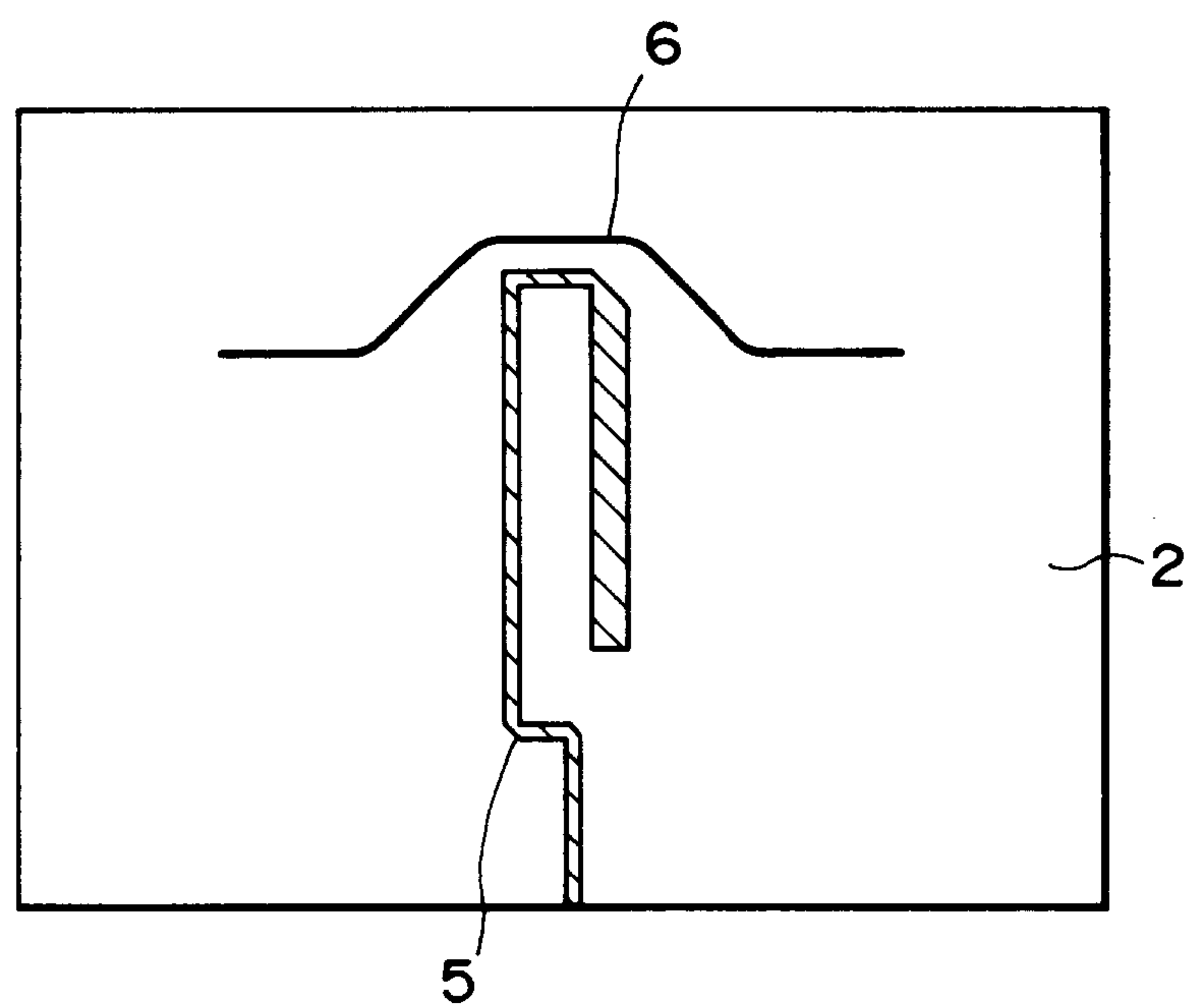


FIG. 11(a)

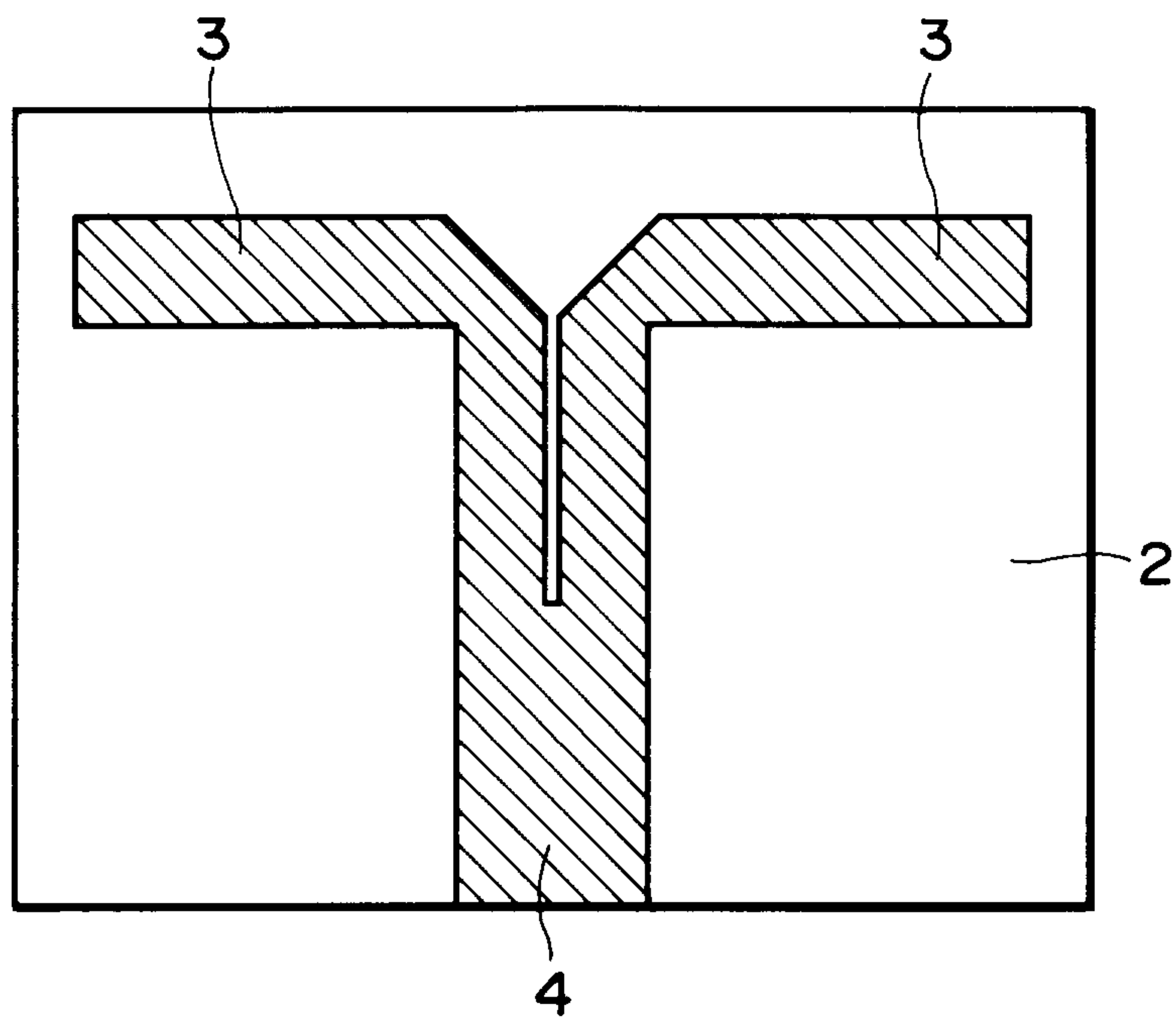


FIG. 11(b)

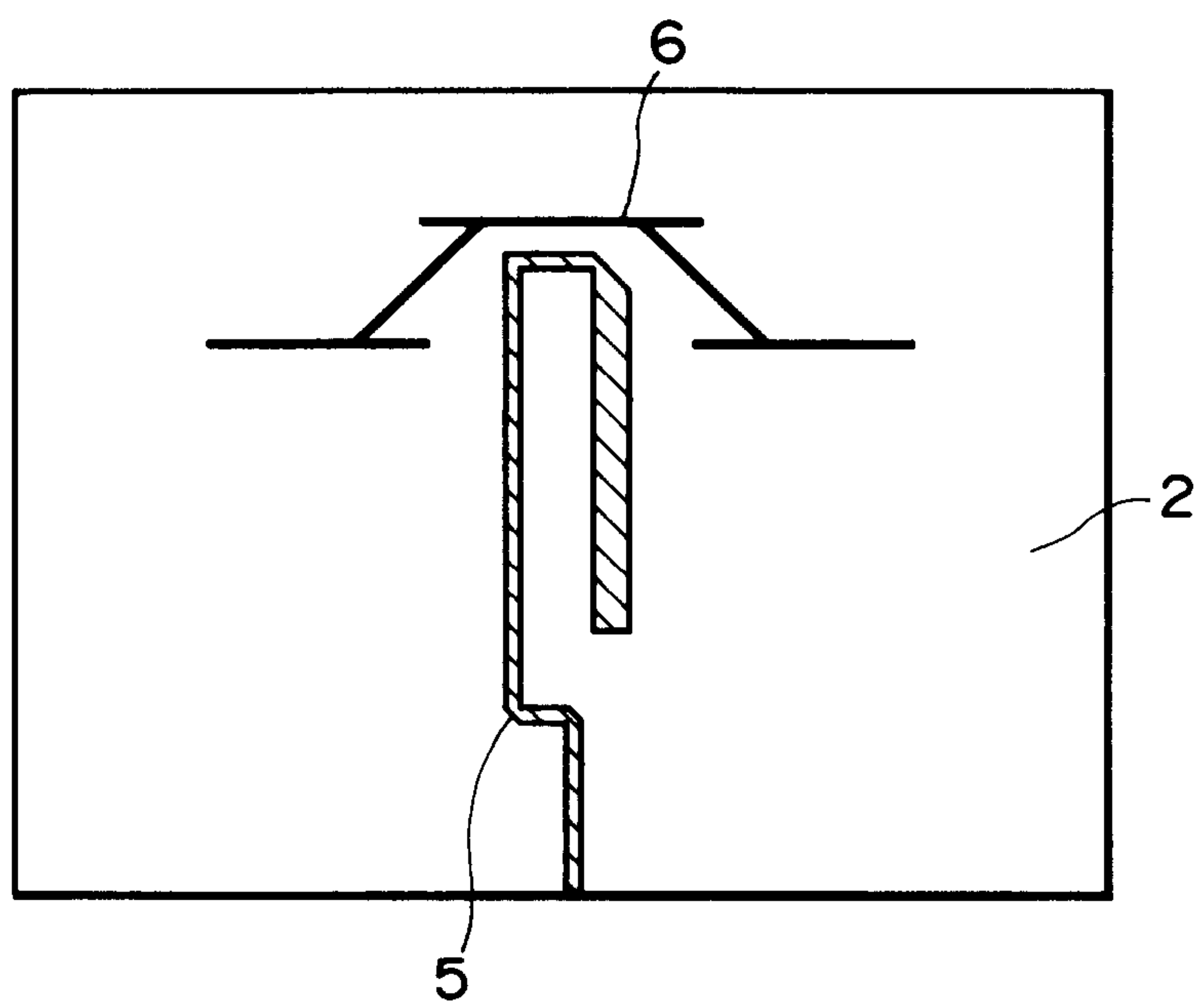


FIG. 12(a)

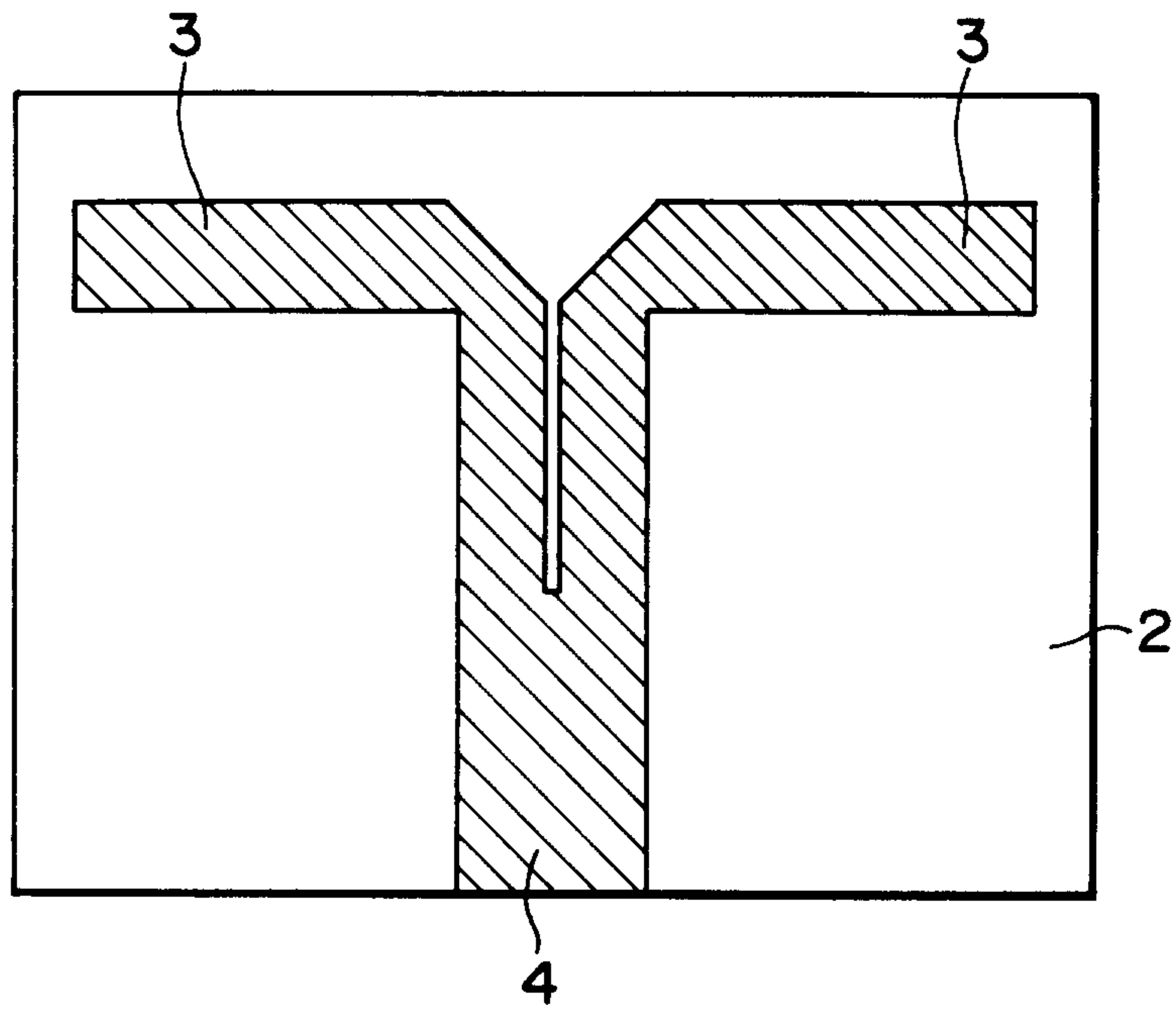


FIG. 12(b)

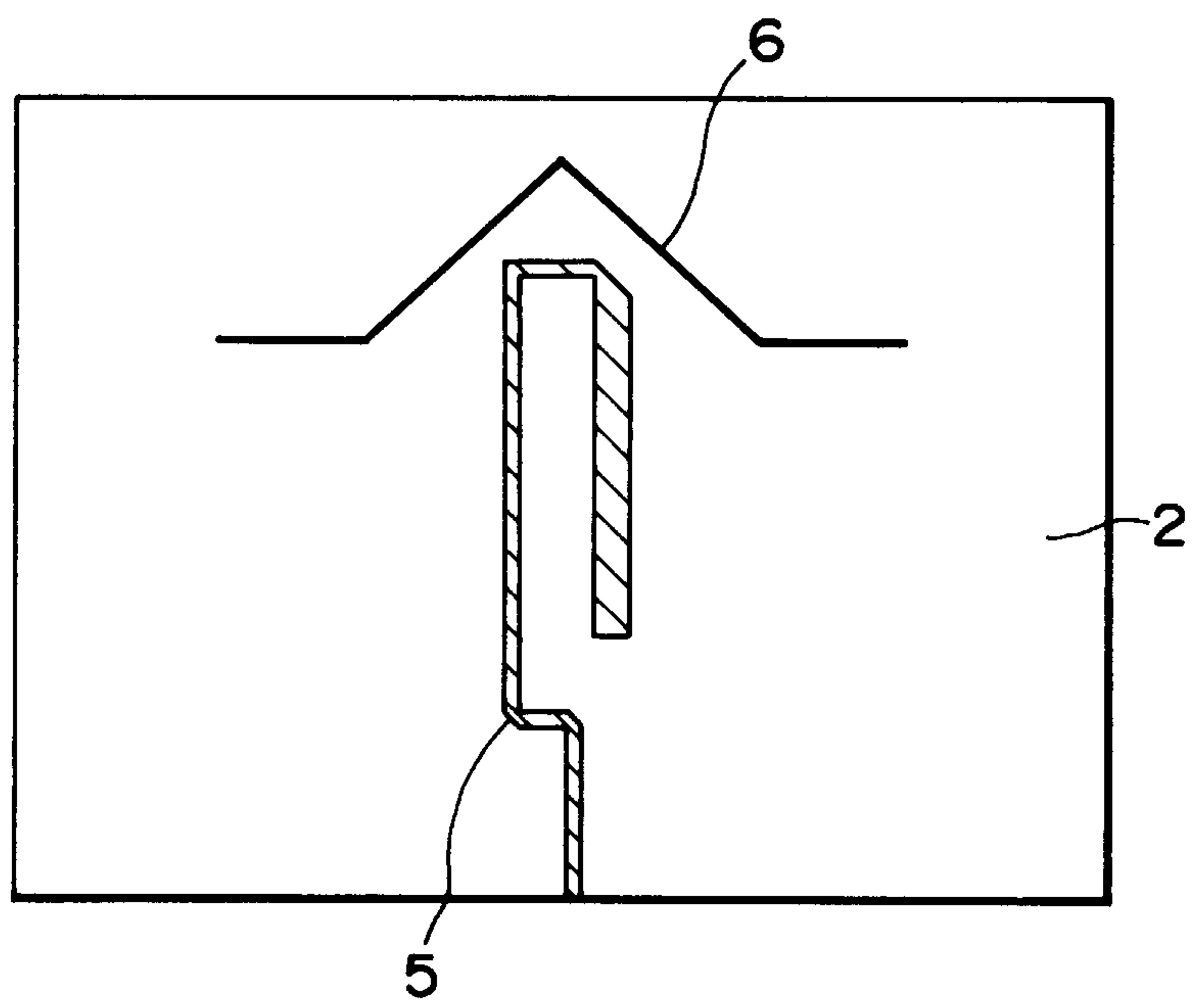


FIG. 13(a)

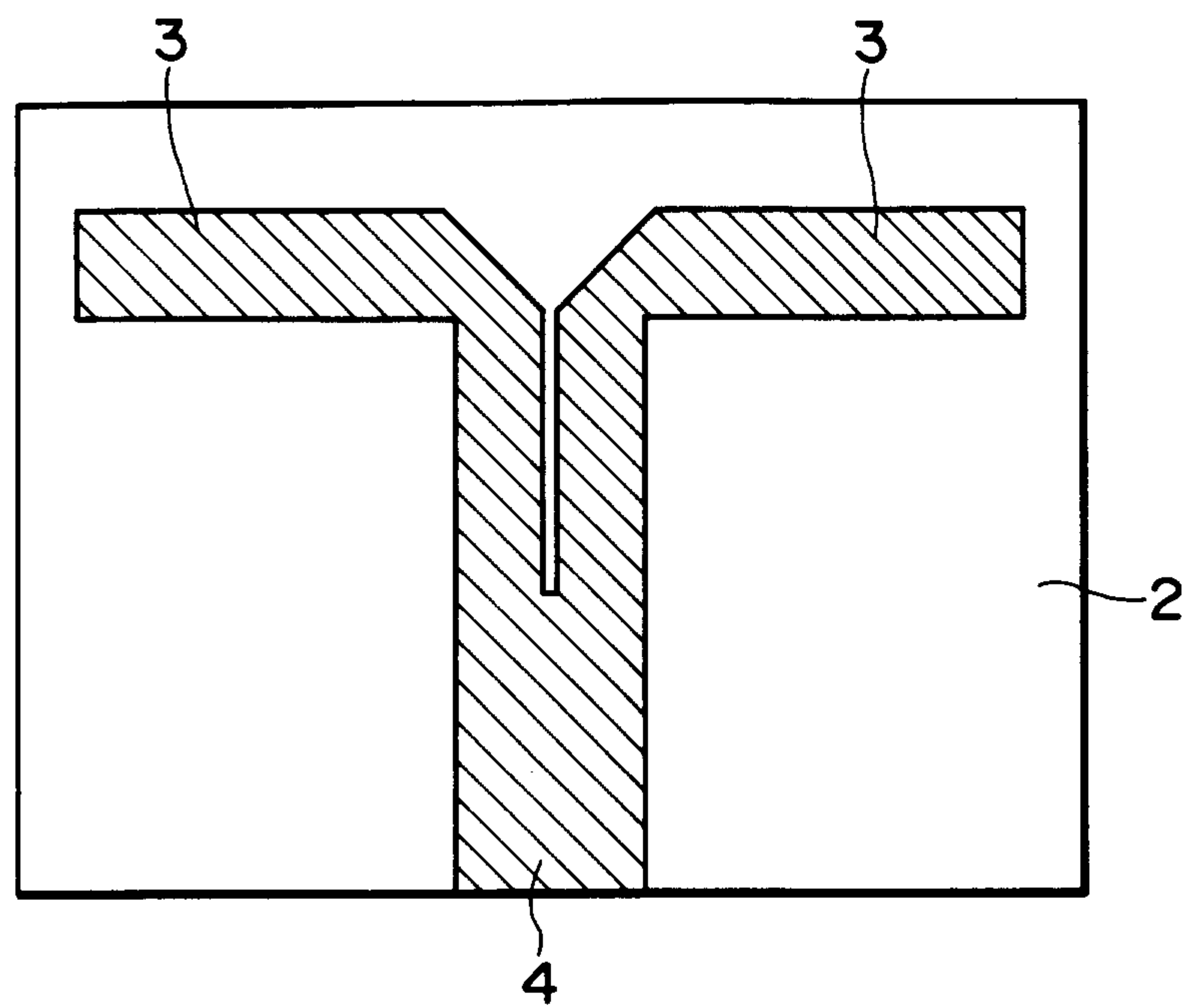


FIG. 13(b)

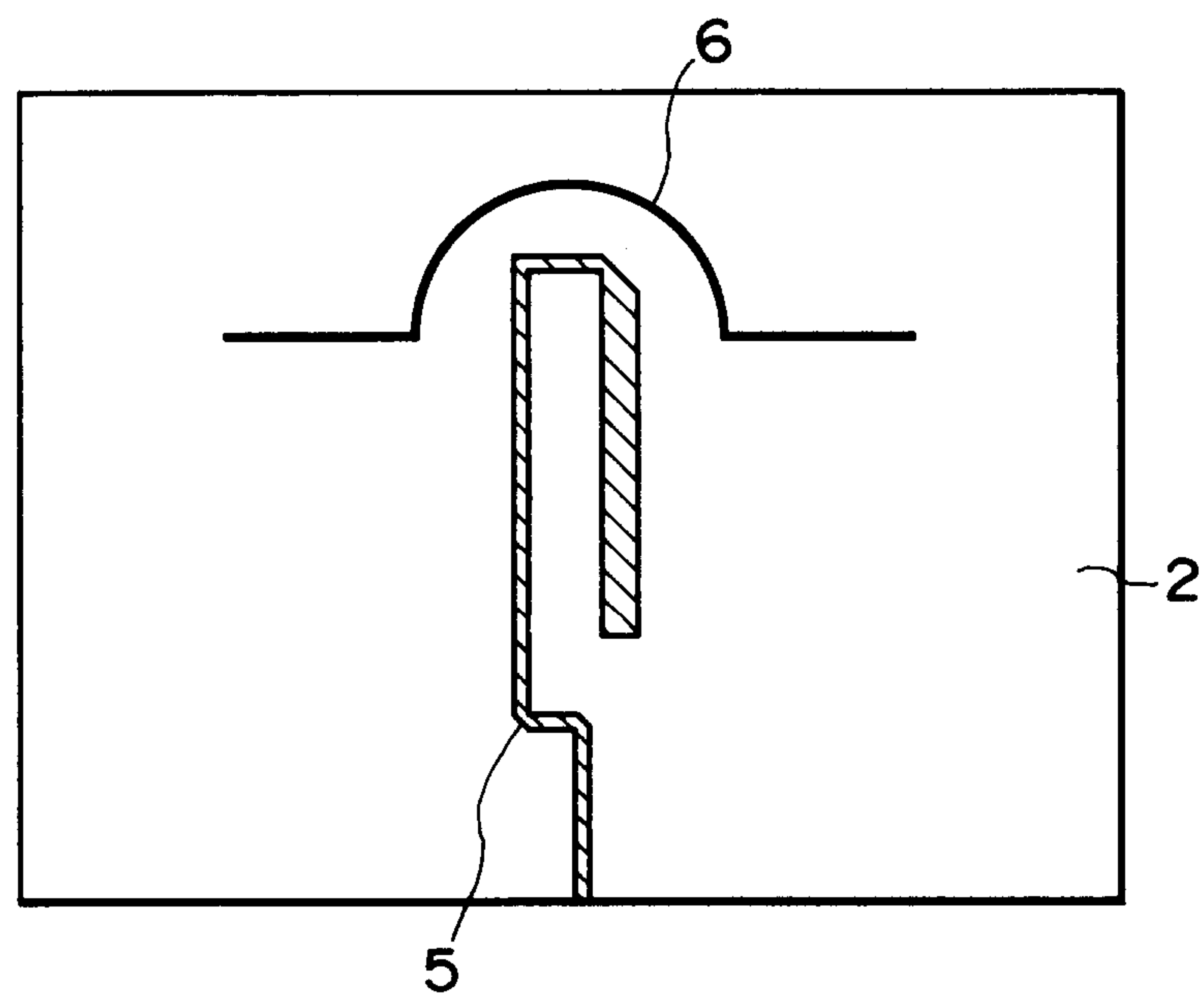


FIG. 14(a)

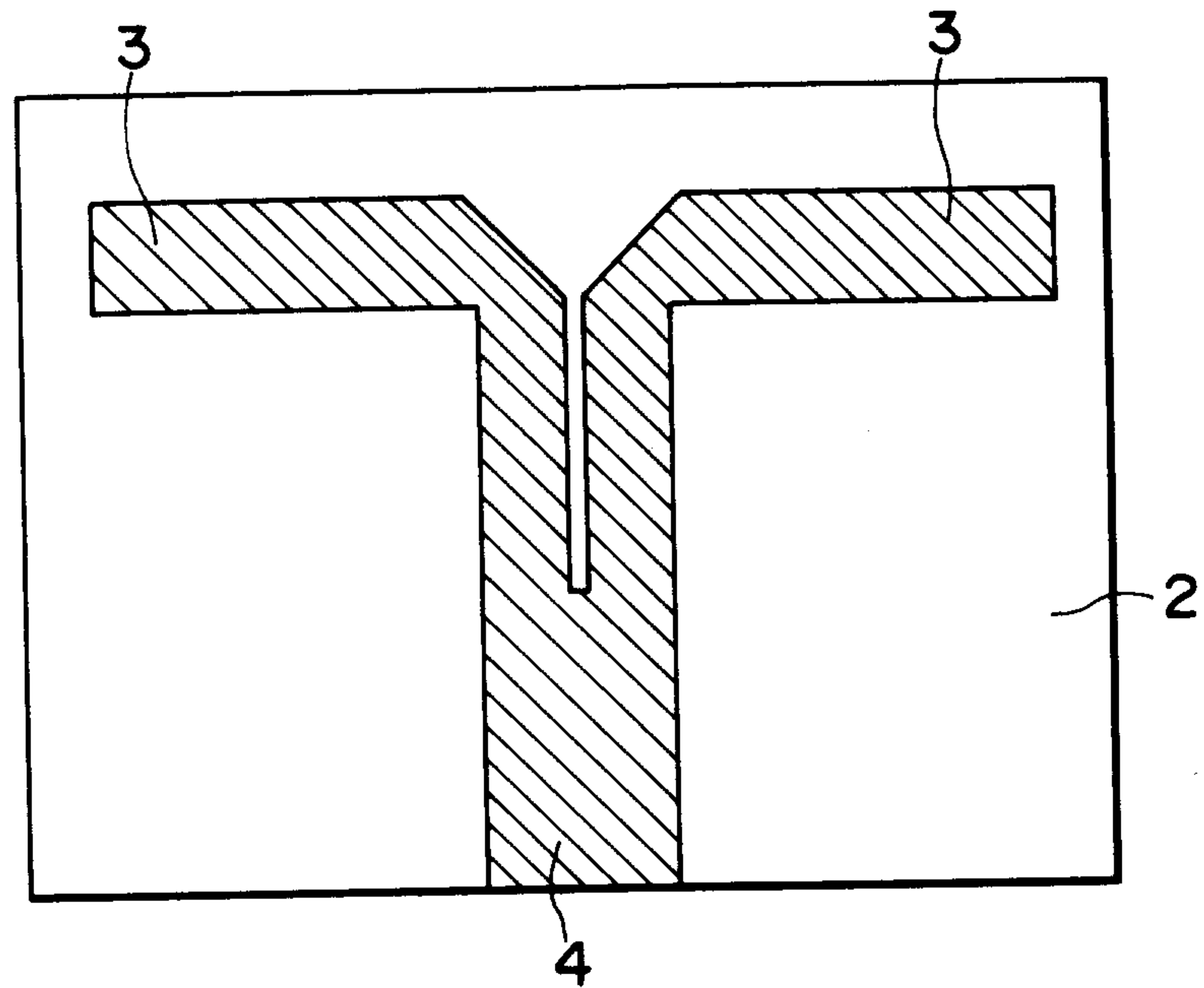


FIG. 14(b)

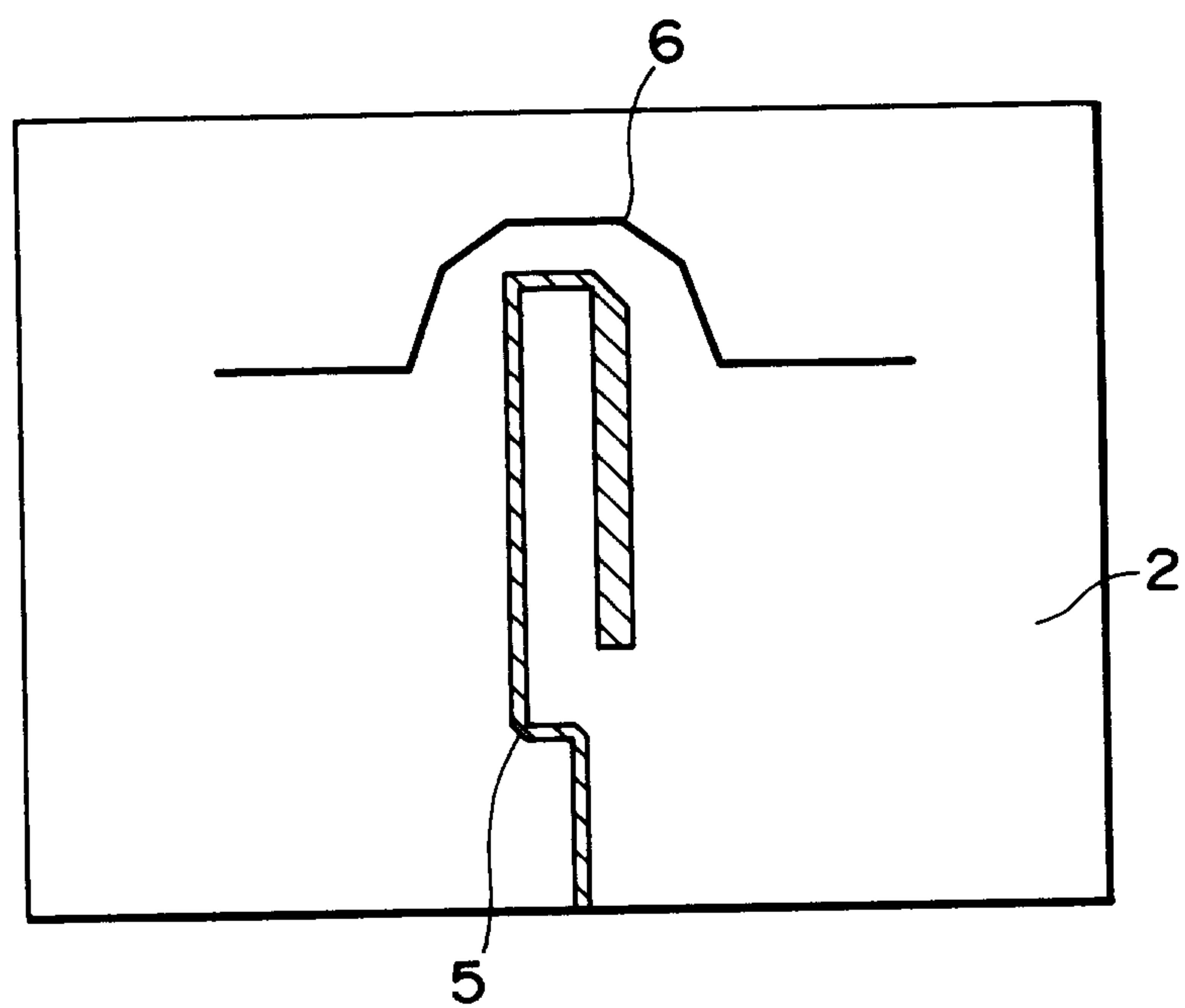


FIG. 15(a)

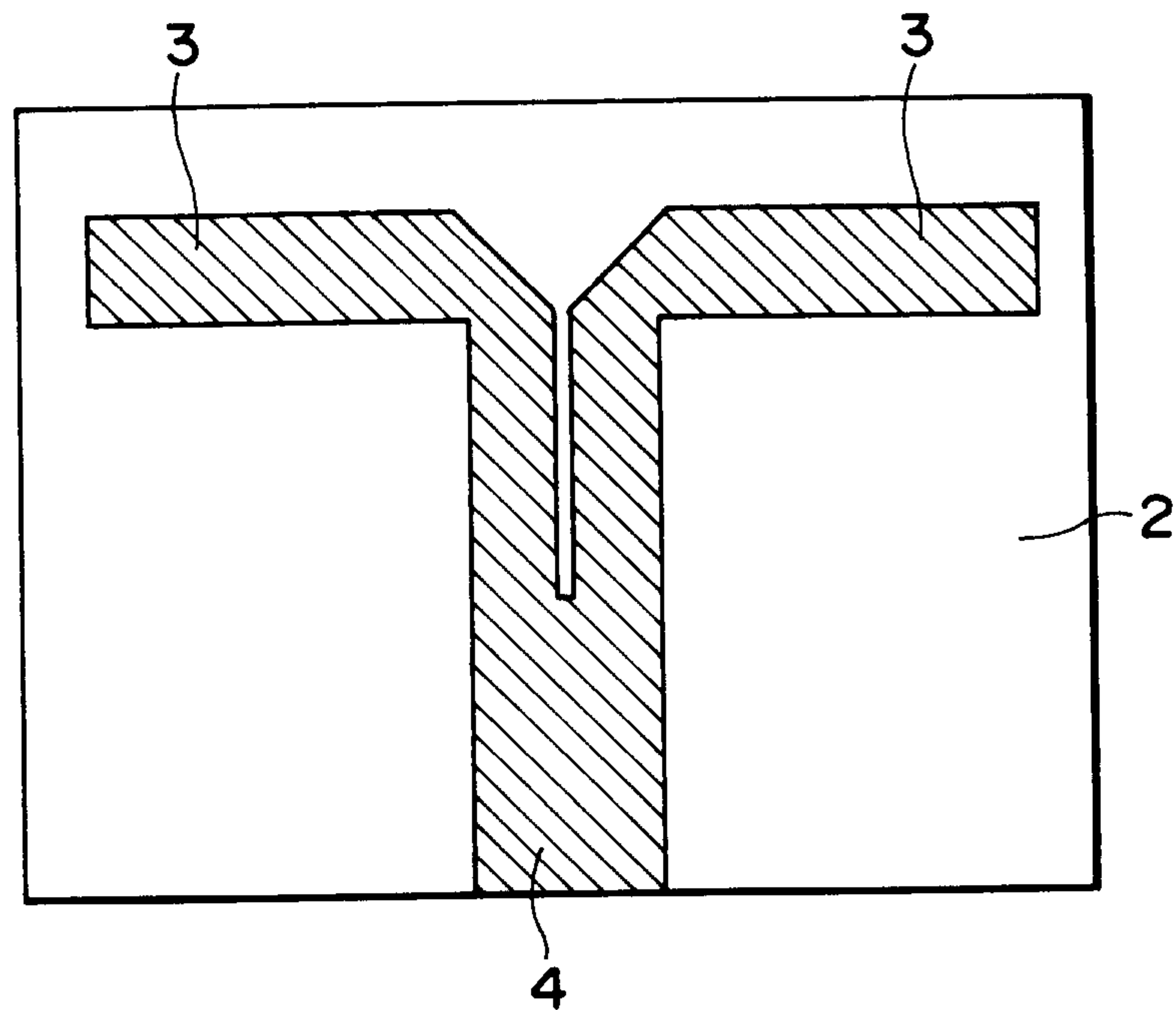


FIG. 15(b)

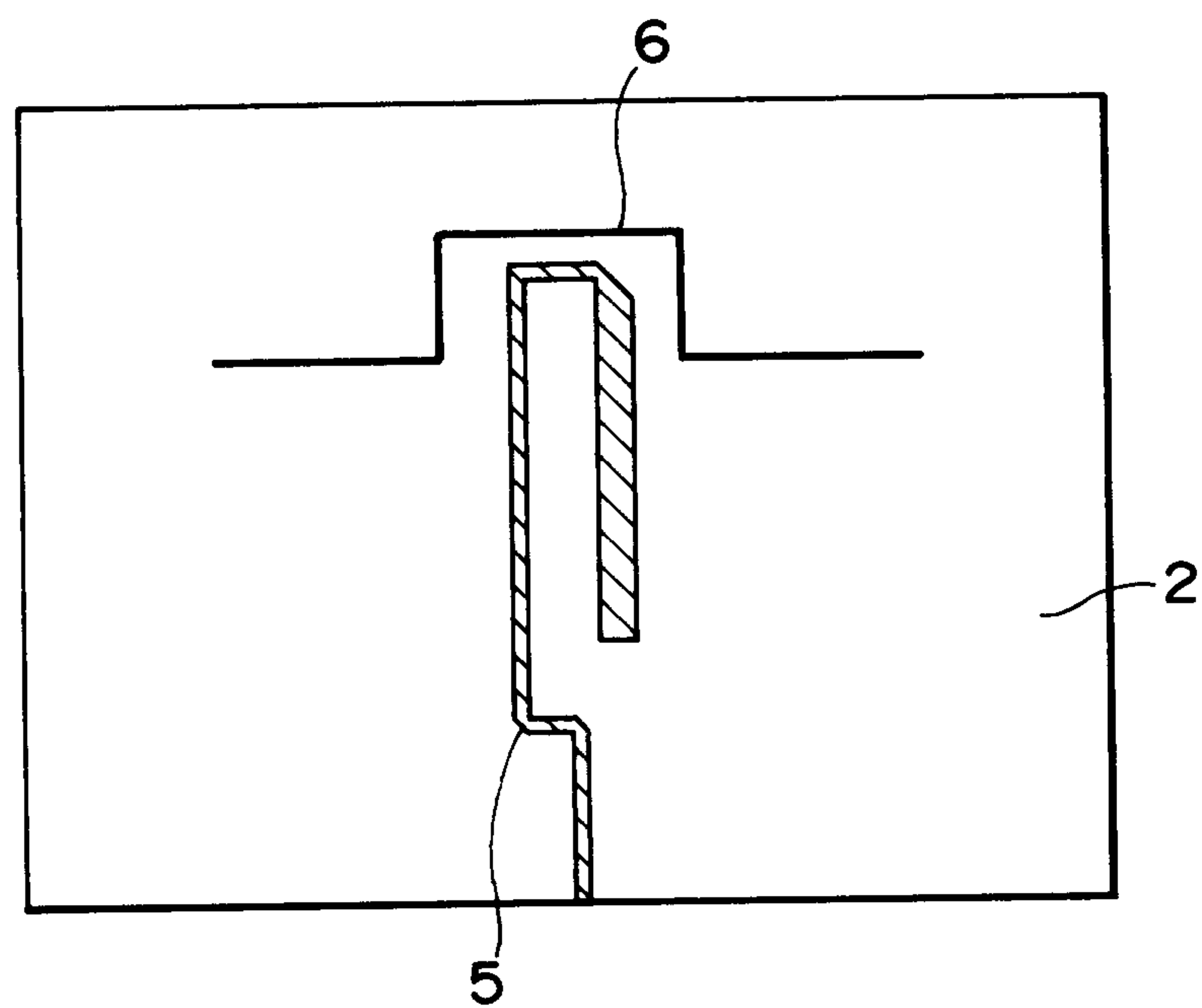


FIG. 16(a)

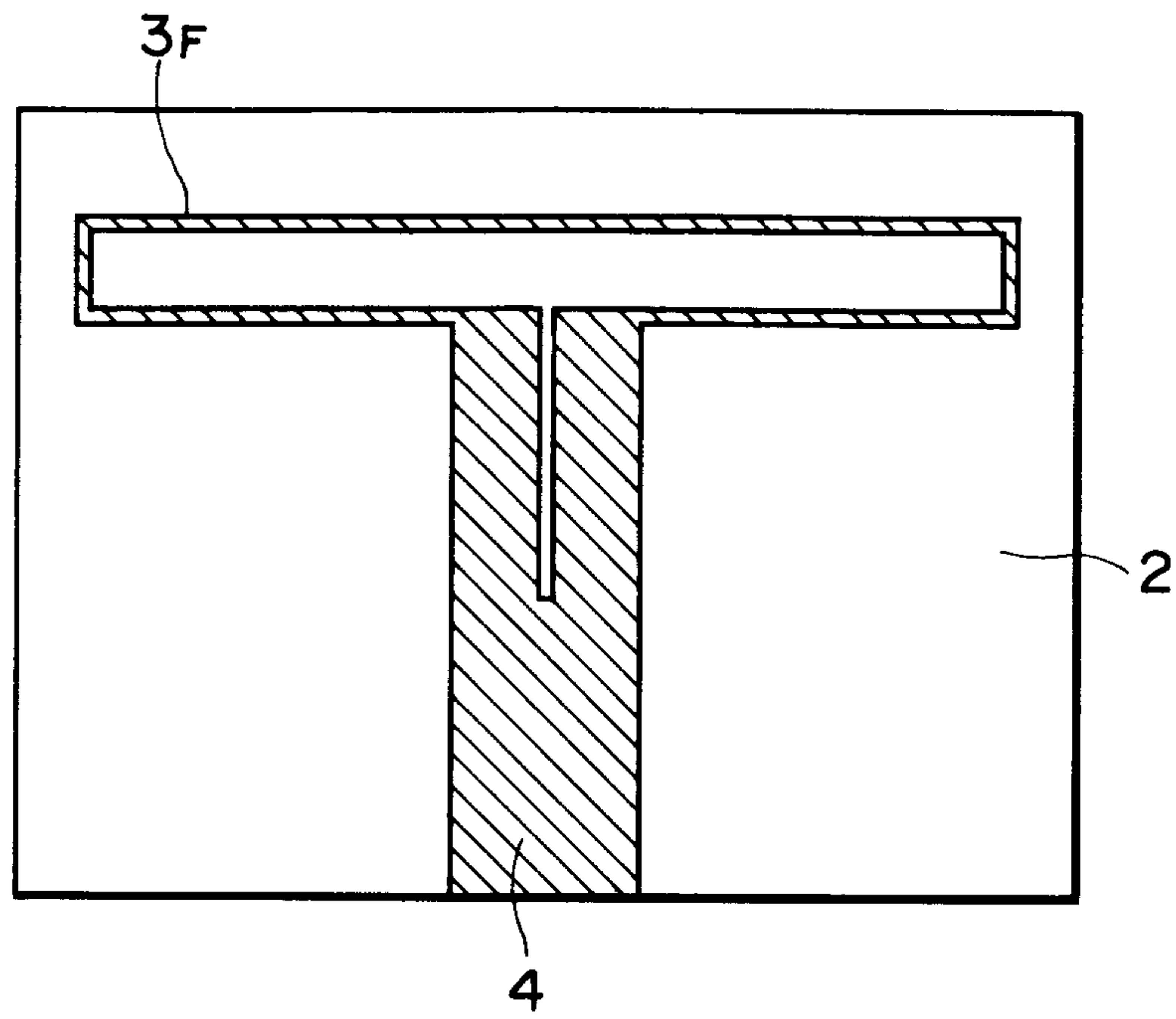


FIG. 16(b)

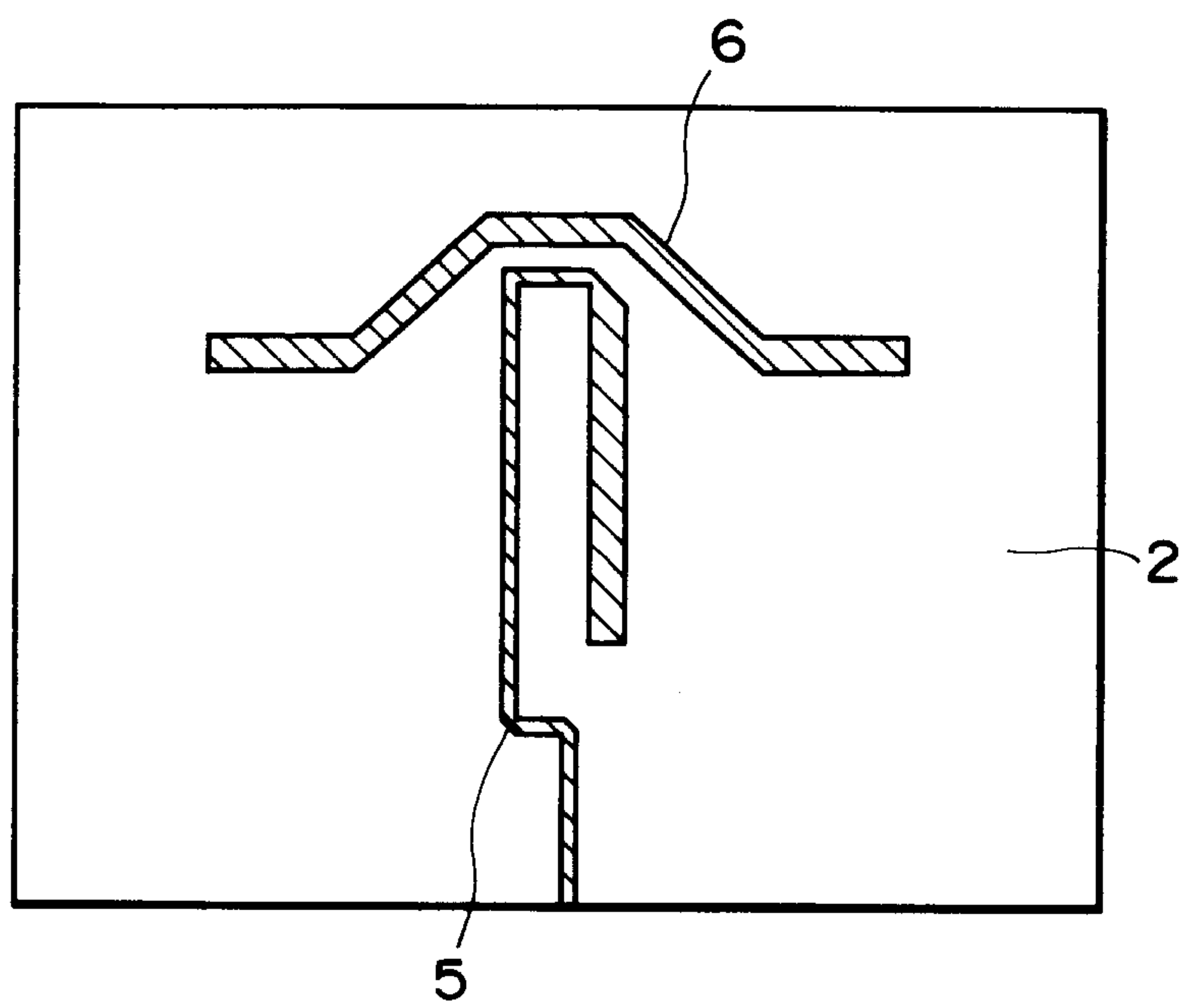


FIG. 17

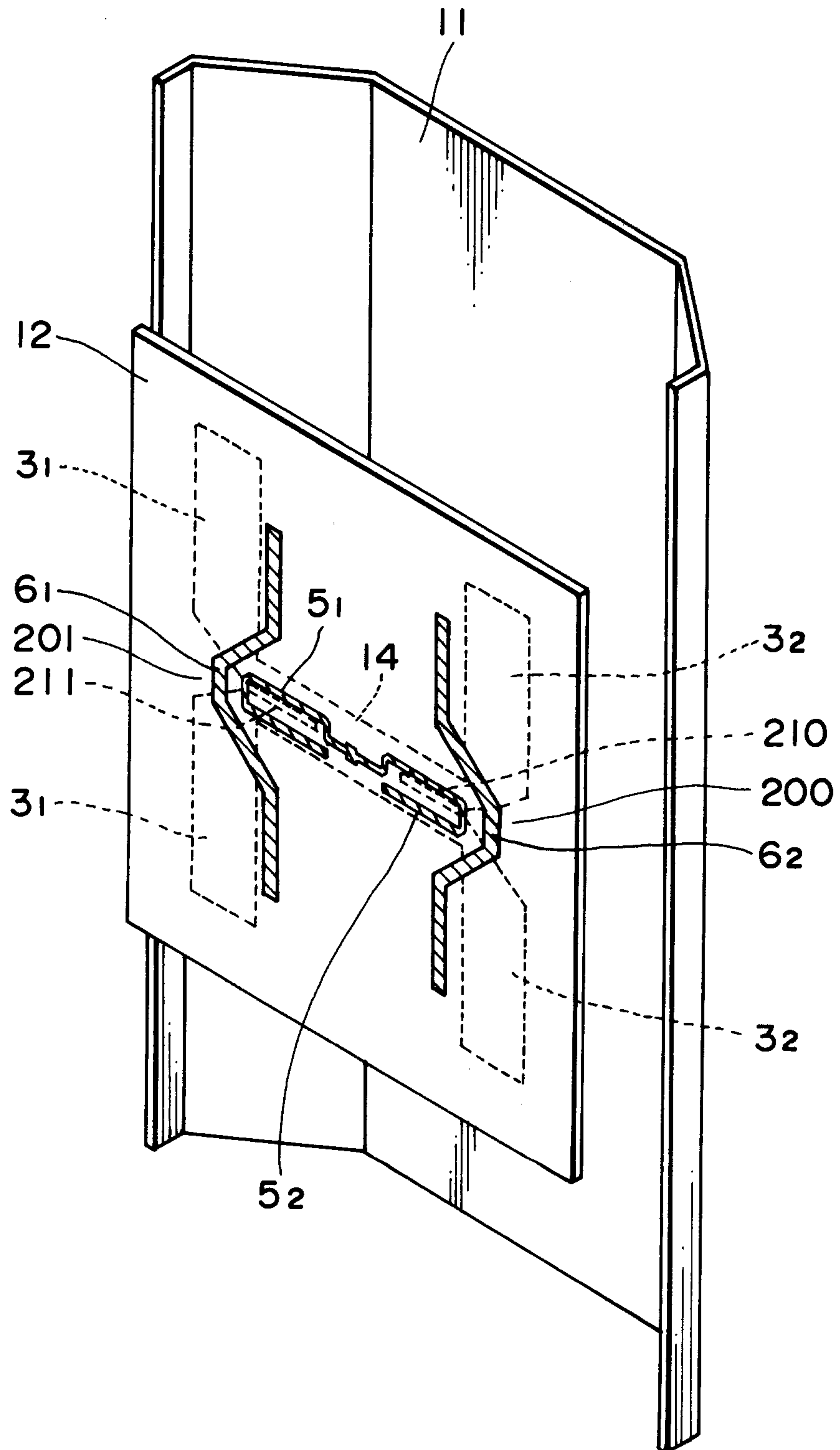


FIG. 18

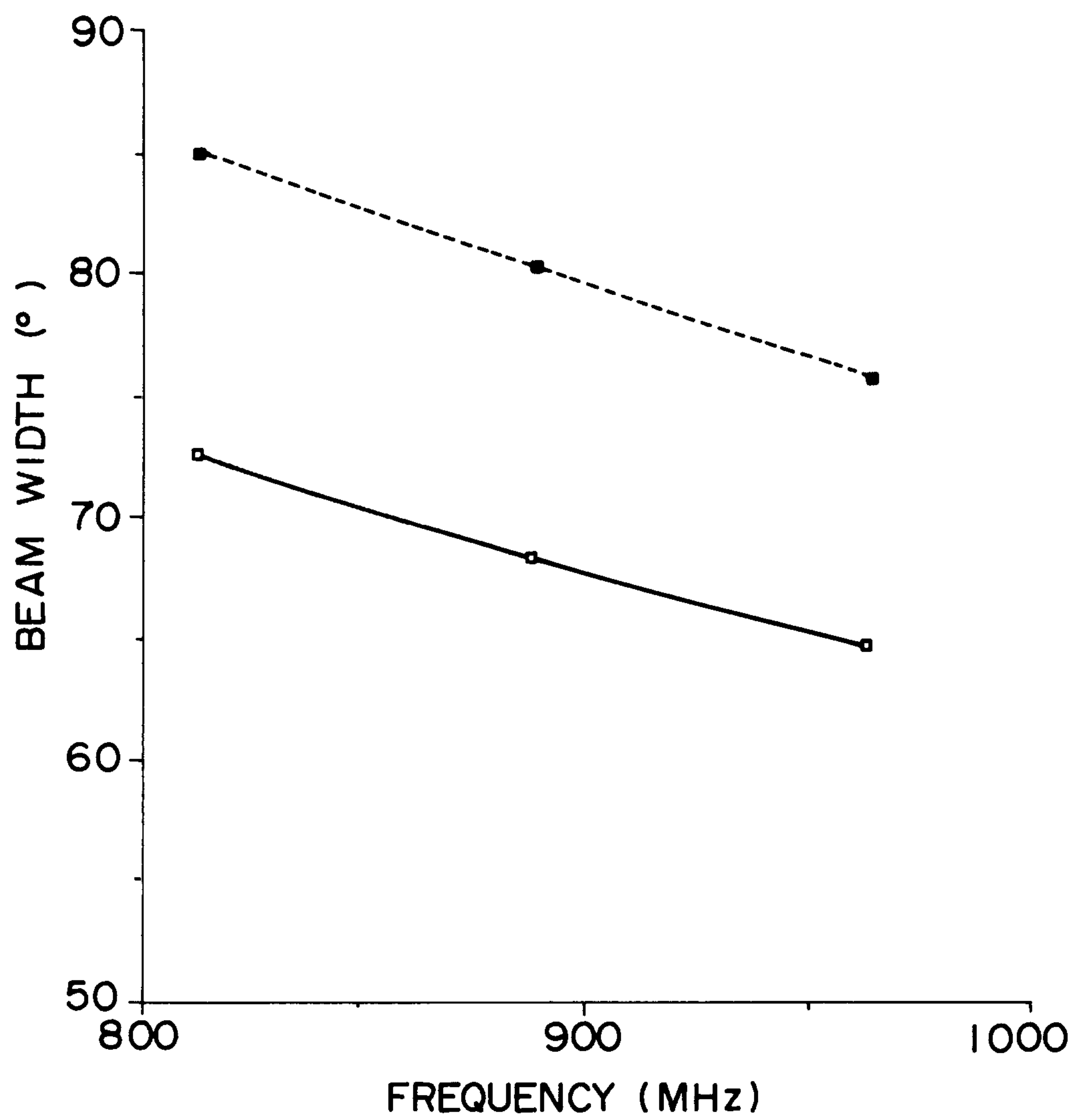


FIG. 19

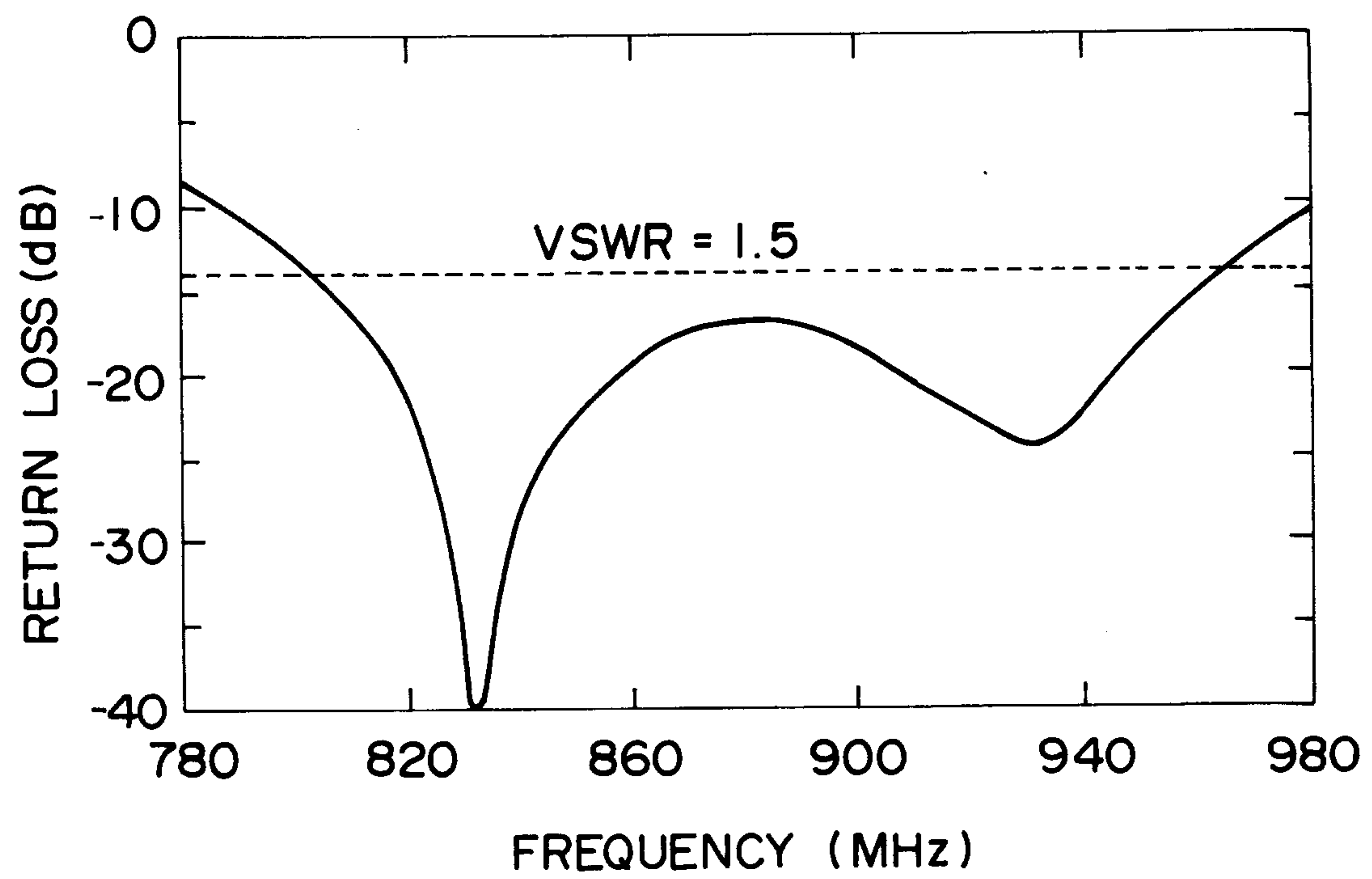


FIG. 20

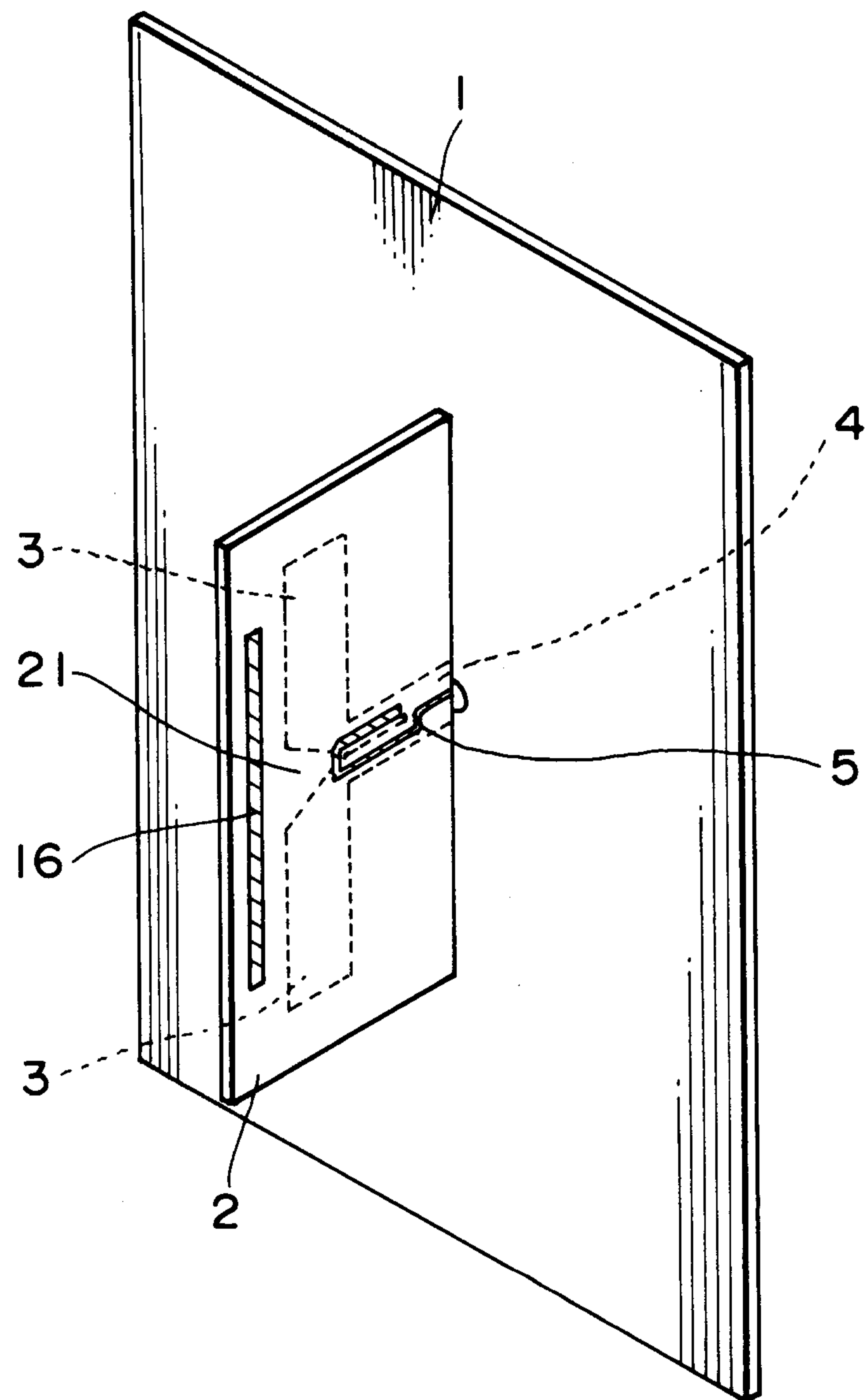


FIG. 21(a)

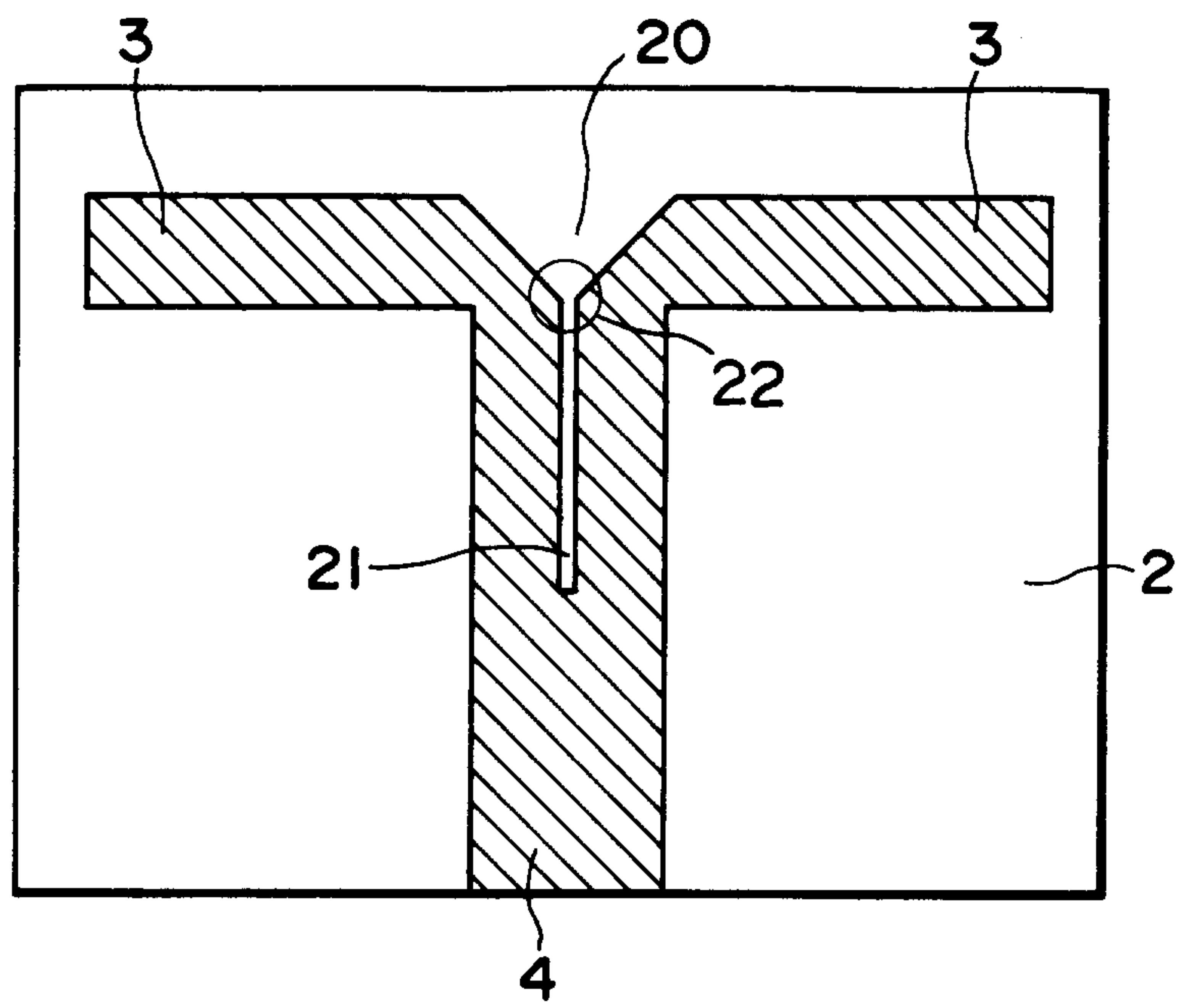


FIG. 21(b)

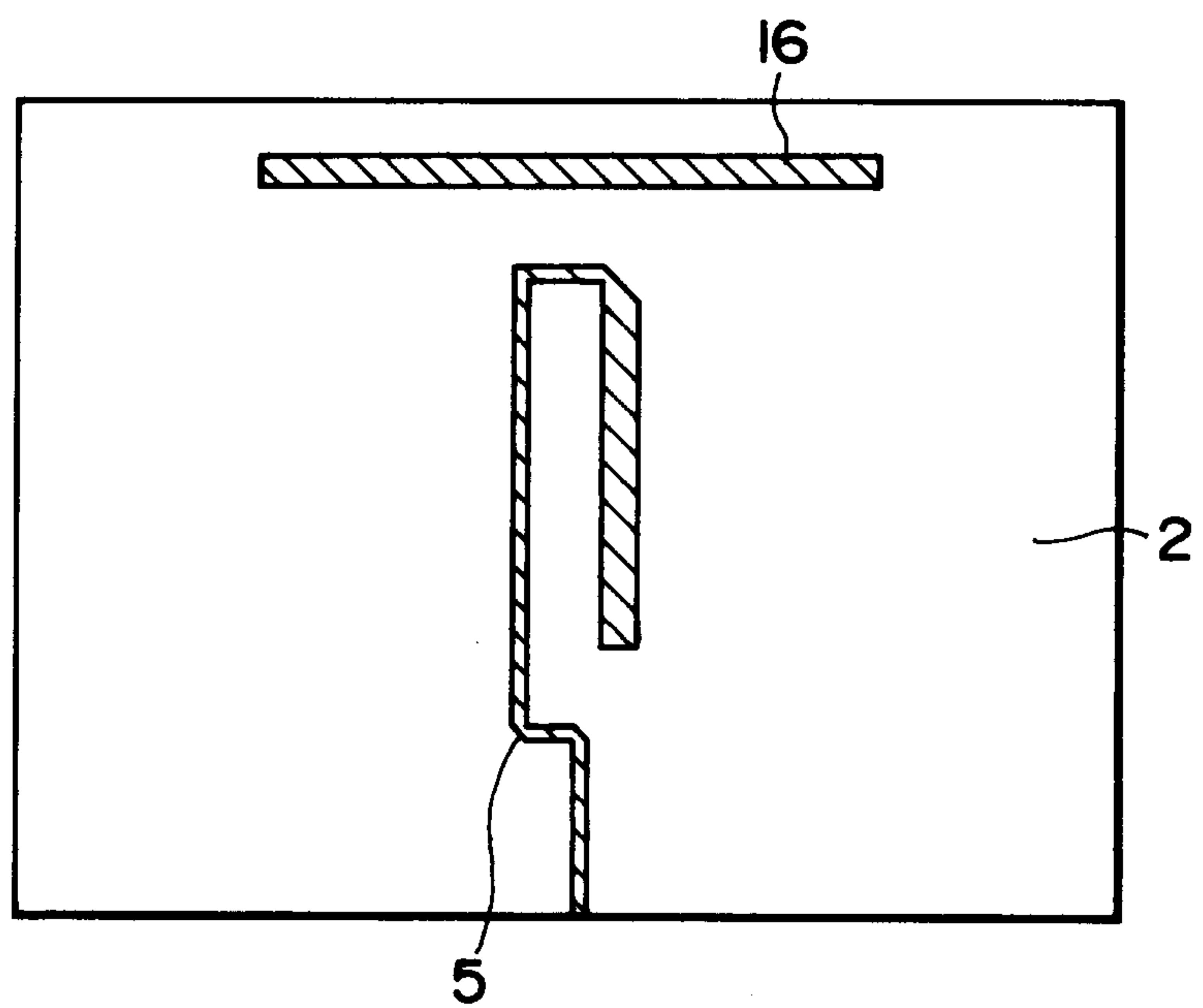


FIG. 22

