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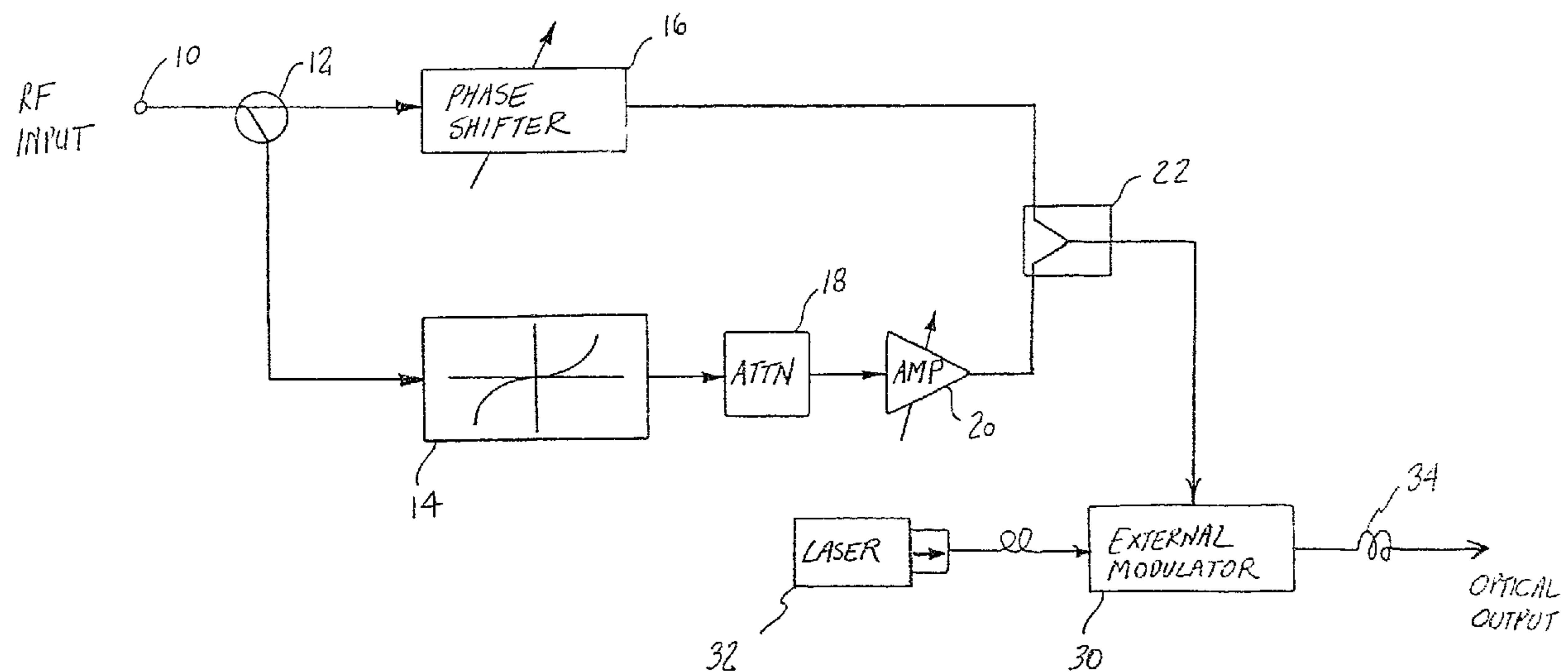
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(54) **DISPOSITIF ET METHODE POUR LINEARISER LE
FONCTIONNEMENT D'UN MODULATEUR OPTIQUE
EXTERNE**

(54) **APPARATUS AND METHOD FOR LINEARIZING THE
OPERATION OF AN EXTERNAL OPTICAL MODULATOR**



(57) A modulating signal is predistorted to linearize the output of an optical intensity modulator. The modulating signal is split into first and second paths. In the first path, the signal is phase shifted. In the second path, distortion components are introduced. The phase shifted signal from the first path is then combined with the distorted signal from the second path to provide a predistorted signal for use in modulating a light source. The distortion generator can comprise a diode pair coupled with opposite polarities in parallel. Both diodes are forward biased, and the pair is coupled in series with the input signal to provide the desired predistortion.

ABSTRACT OF THE DISCLOSURE

A modulating signal is predistorted to linearize the output of an optical intensity modulator. The modulating signal is split into first and second paths. In the first path, the signal is phase shifted. In the second path, distortion components are introduced. The phase shifted signal from the first path is then combined with the distorted signal from the second path to provide a predistorted signal for use in modulating a light source. The distortion generator can comprise a diode pair coupled with opposite polarities in parallel. Both diodes are forward biased, and the pair is coupled in series with the input signal to provide the desired predistortion.

5 The present invention relates to analog optical transmission systems, and more particularly to an apparatus and method for predistorting a modulation signal to provide linear operation of an external optical modulator.

10 Optical transmission systems are currently being implemented for use in various communication applications. For example, telephone systems are now in use that utilize optical fiber technology to transmit voice and data signals over long distances. Similarly, cable television networks are now 15 available where an optical fiber technology is used for the transmission of both analog and digital signals.

20 Prior to the implementation of optical transmission networks, cable television programs were carried as radio frequency ("RF") signals over electrical coaxial cables. In such systems, it is usually necessary to transmit signals over long distances. Since the strength of transmitted signals decreases in proportion to the length of the 25 cable over which the signals are transmitted, amplification at repeated intervals along the cable is necessary to maintain adequate signal strength.

The electronic amplifiers used for this purpose inherently distort the signals as they are being amplified. Harmonic distortion, in particular, results from nonlinearities in the amplifier that 5 cause harmonics of the input frequencies to appear in the output. Other components in the communication network can similarly introduce distortion components.

One solution to the distortion problem in 10 coaxial cable RF communication systems has been to use "feedforward" amplifiers to amplify the signals at repeated intervals along the cable. Feedforward amplifiers are described, for example, in Blumenkranz U.S. Patent No. 4,472,725 entitled "LC 15 Delay Line for Feedforward Amplifier", Tarbutton et al U.S. Patent No. 4,617,522 entitled "Temperature Regulated Feedforward Amplifier", Mannerstrom U.S. Patent No. 4,625,178 entitled "Feedforward Gain Block with Mirror Image Error Amplifier", and 20 Blumenkranz et al U.S. Patent No. 4,792,751 entitled "Apparatus for Field Testing the Performance of a Feedforward Amplifier".

In the operation of a feedforward amplifier, a 25 signal component representative of the distortion introduced by the amplifier is extracted from the amplified signal. That component is then typically phase inverted and the phase inverted distortion component is combined with the amplified signals. The phase inverted component cancels the distortion

component in the amplified signal, leaving a relatively distortion free amplified signal for transmission along the cable.

Optical transmission systems provide a new problem in coping with distortion. In particular, harmonic distortion is a major limitation in analog amplitude modulated optical communication transmission systems. In order to maintain a desired carrier-to-noise ratio of at least 58 dB in a cable television communication system, for example, it is preferable to use external modulators to modulate an optical carrier with the communication signal. However, currently available external modulators, such as Mach Zehnder intensity modulators are nonlinear, due to the phase to intensity conversion process. Nonlinearities of the modulator result in odd order harmonic distortions, of which the third order components are most significant.

It would be advantageous to provide an apparatus and method for reducing harmonic distortion in an analog optical transmission system using an external modulator. Such an apparatus and method would have particular application in an AM cable television supertrunk distribution system. It would be further advantageous to provide such an apparatus and method that is economical, readily manufacturable, and reliable. The present invention provides such an apparatus and method.

In accordance with the present invention, a method and apparatus are provided for linearizing the output of an external analog optical modulator.

5 The phase of a modulating signal is adjusted to compensate for phase shifts introduced by an external optical modulator and a distortion generator used to predistort the signal. The modulation signal is predistorted with odd order distortion components similar to but opposite in polarity than distortion components introduced by the modulator. The predistorted, phase shifted modulation signal is coupled to a modulating signal input of the external modulator.

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15 In one embodiment of the invention, means are provided for splitting an input signal into first and second paths. Phase shift means are coupled to the first path for shifting the input signal phase. Distortion generator means are coupled to the second path for introducing distortion components into the input signal. The phase shifted input signal from the first path is combined with the distorted input signal from the second path to provide a predistorted signal for use in modulating a light source.

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25 A variable gain amplifier is coupled to amplify the distortion components in the predistorted signal to a desired level. The phase shift means may also be adjustable to provide a desired phase delay. The variable gain amplifier for amplifying the distortion components is coupled

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in the second path between the distortion generator means and the combining means. An attenuator may be coupled to the input of the amplifier.

In an alternate embodiment, the variable gain
5 amplifier is coupled to amplify the predistorted signal provided by the combining means. In this embodiment, the combining means can subtract the phase shifted input signal from the distorted input signal to provide a predistorted signal that
10 primarily comprises the distortion components. The amplified, predistorted signal from the combining means is then summed with the input signal to provide a modulation signal for the light source. The input signal may also be amplified prior to
15 summation with the amplified predistorted signal.

In either embodiment, the light source can comprise a solid state laser. The external modulator can comprise a Mach Zehnder modulator. The distortion generator means provide odd order
20 distortion components that are opposite in polarity to the odd order distortion components introduced by the external modulator.

In particular, the distortion generator means can comprise a diode pair coupled with opposite polarities in parallel. Each diode is forward biased with a respective current source. The biased diode pair is coupled in series with the second path to distort the input signal.
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Figure 1 is a block diagram of a first embodiment of the present invention;

5 Figure 2 is a schematic diagram of a parallel diode distortion generator that can be used in connection with the present invention;

Figure 3 is an equivalent circuit of the distortion generator of Figure 2;

10 Figures 4a-4c are spectral patterns of the distortion introduced by a predistortion circuit, an external modulator, and the combination thereof; and

Figure 5 is a block diagram of a second embodiment in accordance with the present invention.

External modulators, such as Mach Zehnder modulators are useful in modulating an optical carrier, such as a laser beam, with a communication signal for analog transmission. External modulation is desirable for analog lightwave distribution because a high powered diode pump laser can be used to achieve good power budget. In addition, intermodulation distortion is independent of frequency.

One problem with external modulators is that they are nonlinear, and the level of nonlinearities vary from device to device. The present invention provides a universal predistortion circuit for linearizing an optical intensity modulator. Both phase and amplitude adjustment of the modulating signal are provided to enable the circuit to adapt to any external modulator.

Figure 1 illustrates one embodiment of a predistortion circuit in accordance with the present invention. An RF input signal, such as a cable television ("CATV") signal is input at terminal 10. The signal is split into two paths at a conventional directional coupler 12. In the first path, the phase of the signal is shifted by an adjustable phase shifter 16. In the second path, the signal is distorted by a distortion generator 14 that can comprise a pair of diodes coupled with opposite polarities in parallel. The current-voltage characteristic of such a diode pair is illustrated

within box 14. The distorted signal output from distortion generator 14 is input to an attenuator 18, and an adjustable gain amplifier 20.

5 The phase shifted signal from the first path and distorted signal from the second path are combined in a conventional coupler 22 to produce a modulation signal for external modulator 30. Modulator 30, which can be a Mach Zehnder modulator or other optical modulator, modulates a coherent 10 light beam from a laser 32 for transmission over an optical fiber 34.

15 The circuit illustrated in Figure 1 provides an adaptive harmonic distortion generator. It is designed to produce distortion components that are similar, but opposite in phase to those produced by 20 external modulator 30. Phase shifter 16 and amplifier 20 are adjusted (e.g., by trial and error) to provide a phase delay and amplitude that result in an optimal linearization of the output from modulator 30. Amplifier 20 serves to set the level 25 of distortion according to the modulation depth used to modulate optical modulator 30.

It should be appreciated that the level of 25 distortion components introduced by distortion generator 14 do not have to be exactly the same as those produced by modulator 30. The only requirement on the distortion generator is to generate harmonic distortion components that have a similar order as those produced by the external

modulator. Since external modulators generally introduce odd order harmonics, distortion generator 14 also generates odd order harmonics.

Figure 2 is a schematic diagram of a diode pair distortion generator that can be used in connection with the present invention. An input signal is coupled via terminal 40 to the anode of diode 44 and the cathode of diode 46. Resistor 42 provides a proper input impedance. Diode 46 is forward biased by a current source generally designated 80. The current source includes a conventional transistor pair 48, 50 with a potentiometer 60 to enable adjustment of the output current. Current is applied through a choke 56 that blocks AC components of the input signal from feeding back into the current source.

A similar current source 82 is used to forward bias diode 44. This source includes transistor pair 52, 54 with potentiometer 62 that is used to adjust the output current. A choke 58 prevents AC components of the input signal from feeding back into the current source. Capacitors 64, 66 block the DC bias currents from feeding through with the distorted signal to output terminal 70. The output impedance of the circuit is established by resistor 68.

Figure 3 is a simplified diagram of the circuit of Figure 2. Similarly numbered components provide the functions described above in connection with Figure 2.

The response of the diode pair circuit can be expressed mathematically as:

$$V_o = 2R_L I_B [V_T V_{IN} / (1 + 2V_T I_B (R_S + R_L)) + (V_T V_{IN})^3 / 6 (1 + 2V_T I_B (R_S + R_L))^4 + \dots]$$

Where: V_o = Output Voltage
 5 R_L = Load Impedance
 I_B = Diode Bias Current
 V_T = Diode Threshold Voltage (Q/kT)
 R_S = Input Impedance
 V_{IN} = Input Voltage

10 Similarly, the response of an external optical modulator can be expressed as:

$$P_o = P_B [(KV_M - (KV_M)^3 / 8) \sin \omega t + ((KV_M)^3 / 24) \sin 3\omega t + \dots]$$

Where: P_o = Optical Output Power
 15 P_B = Optical Bias Power
 K = Unique Constant for Each Different Modulator
 V_M = Modulating Signal

Figures 4a-4c are spectral responses, respectively, of signals passing through the distortion generator, external modulator, and the 20 combined signals. As indicated in Figure 4a, an input signal with a frequency f , passes through the distortion generator with a spectral response 90. The distortion generator introduces a third order

harmonic at $3 f_1$, as shown at 96. The response of the external modulator, as indicated in Figure 4b, is such that the signal frequency f_1 , passes with a response 92 in the same direction as the response 90 through the distortion generator. However, third order harmonics generated at $3 f_1$, have a response 98 opposite in polarity to those introduced by the distortion generator. As a result, when the modulator is modulated with a signal passed through the distortion generator, an output spectra as illustrated in Figure 4c will result. In particular, the desired signal spectra at f_1 , add with a response as shown at 94. The third order harmonics cancel as indicated at 100.

An alternate embodiment of a predistortion circuit in accordance with the present invention is illustrated in Figure 5. The RF input signal applied at terminal 110 is coupled to a directional coupler 112 that splits the signal into first and second paths. In the first path, the signal is attenuated at a conventional attenuator 118 and passed to an adjustable phase shift circuit 116. In the second path, the RF input signal is again split at a directional coupler 120. One output of coupler 120 couples the signal to a distortion generator 114 that can comprise the circuit illustrated in Figure 2. The phase shifted input signal from phase shifter 116 is subtracted at a

combiner 122 from the distorted input signal from distortion generator 114. The output of combiner 122 contains the distortion components introduced by distortion generator 114.

5 The distortion components output from combiner 122 are amplified by a variable gain, low noise linear amplifier 124 and summed in a summer 128 with the original RF input signal after amplification by another variable gain amplifier 126. The gains of 10 amplifiers 124, 126 and the phase delay introduced by phase shifter 116 are set to optimize the linearization of an optical intensity modulator 130. The combined signal from summer 128 is used as a 15 modulation signal for the modulator, which modulates an optical output signal from laser 132 for transmission on an optical fiber 134.

It should now be appreciated that the present invention provides a universal predistortion circuit 20 that is useful in linearizing the output of an optical intensity modulator. The circuit is useful 25 in broadband multi-channel transmission systems, such as CATV distribution systems. The use of a predistorted modulation signal in conjunction with a conventional optical intensity modulator effectively reduces the third order nonlinearity generated by the modulator. As a result, a higher optical modulation index can be used resulting in a higher link power budget for a given source of optical power. By adjusting the phase delay and amplitude

of the modulating signal, the intrinsic third order composite triple beats of the modulator are reduced.

Although the invention has been described in connection with various preferred embodiments, those skilled in the art will appreciate that numerous adaptations and modifications may be made thereto without departing from the spirit and scope of the invention, as set forth in the following claims.

CLAIMS:

1. Apparatus for providing a predistorted signal for use in linearizing an external optical intensity modulator (30, 130), comprising:

means for splitting (12, 112) an input signal into first and second paths;

distortion generator means (14, 114) coupled to said second path for introducing odd order distortion components into said input signal that are similar to, but opposite in polarity, than distortion components introduced by said modulator;

phase shift means (16, 116) coupled to one of said paths for shifting the phase of said input signal in said first path with respect to said distorted input signal in said second path; and

means for combining (22, 122) the input signal from said first path with the distorted input signal from said second path to form a combined signal for providing said predistorted signal.

2. Apparatus in accordance with claim 1, wherein said distortion generator means (14, 114) comprise:

a diode pair (44, 46) coupled with opposite polarities in parallel;

a first current source (80) for forward biasing one of said diodes;

a second current source (82) for forward biasing the other of said diodes; and

means for coupling said diode pair (44, 46) in series with said second path.

3. Apparatus in accordance with claim 1 or 2, wherein:

said phase shift means (16, 116) is adjustable to provide a desired phase delay.

4. Apparatus in accordance with any one of claims 1 to 3, further comprising:

a variable gain amplifier (20, 124) coupled to adjustably amplify said distortion components.

5. Apparatus in accordance with claim 4, wherein:

 said variable gain amplifier (20) is coupled in said second path between said distortion generator (14) means and said combining means (22).

6. Apparatus in accordance with claim 4 or 5, further comprising:

 an attenuator (18) coupled between said distortion generator means (14) and said amplifier (20).

7. Apparatus in accordance with any one of claims 4 to 6, wherein:

 said variable gain amplifier (124) is coupled to amplify said combined signal provided by said combining means (122).

8. Apparatus in accordance with any of the preceding claims, wherein:

 said combining means (122) subtracts the phase shifted input signal from the distorted input signal to provide said combined signal comprising primarily said distortion components.

9. Apparatus in accordance with any of the preceding claims, further comprising:

 means for summing (128) said input signal with said combined signal from said combining means (122) to provide said predistorted signal for said external optical intensity modulator (30, 130).

10. Apparatus in accordance with claim 9, further comprising:

 amplifier means (126) for amplifying said input signal prior to summation with said distortion components.

11. Apparatus in accordance with any of the preceding claims, wherein:

 said predistorted signal is coupled to a Mach Zehnder modulator (30, 130) for modulating an output of said laser (32, 132).

12. Apparatus in accordance with any of the preceding claims, wherein:

 said distortion generator means (14, 114) provide odd order distortion components.

13. Apparatus in accordance with any of claims 4 to 12 comprising:

 means for adjusting the gain of said amplifier (20, 126) to provide said distortion components at a level necessary to linearize the output off said modulator (30, 130); and

 means for coupling (22, 126) the amplified distortion components to a modulating signal input of said modulator (30, 130).

14. Apparatus in accordance with any of the preceding claims, wherein:

 said phase shift means (16, 116) is shifting the phase of said input signal to compensate for a phase shift introduced by said distortion means (14, 114).

15. Apparatus in accordance with any of the preceding claims, wherein:

 said phase shift means (16, 116) is coupled to said first path.

16. Apparatus in accordance with any of the preceding claims, wherein:

 said external optical intensity modulator is an analog modulator.

17. Apparatus in accordance with any of the preceding claims, wherein:

 said predistorted signal is used for modulating an output of a light source by said external optical intensity modulator.

18. Apparatus in accordance with claim 17, wherein:

 said light source is a solid state laser (32, 132).

19. A method for linearizing the output of an external optical intensity modulator (30, 130), comprising the steps of:

 splitting an input signal into first and second paths;
 distorting said input signal in said second path with odd order distortion components similar to but opposite in polarity than distortion components introduced by said modulator;

 adjusting the phase of said input signal in said first path with respect to said input signal in said second path to compensate for a phase shift introduced in said distorted input signal in said second path; and

 combining said input signal from said first path with said distorted input signal from said second path to form a combined signal for providing a predistorted signal.

20. The method in accordance with claim 19, further comprising the steps of:

 variably amplifying said distorted input signal in said second path.

21. The method in accordance with any of the preceding method claims, wherein:

 said external optical intensity modulator is an analog modulator.

22. The method in accordance with any of the preceding method claims, comprising the further step of:

 using said predistorted signal for modulating an output of a light source by said external optical intensity modulator.

23. The method in accordance with claim 22, wherein:

 said light source is a solid state laser (32, 132).

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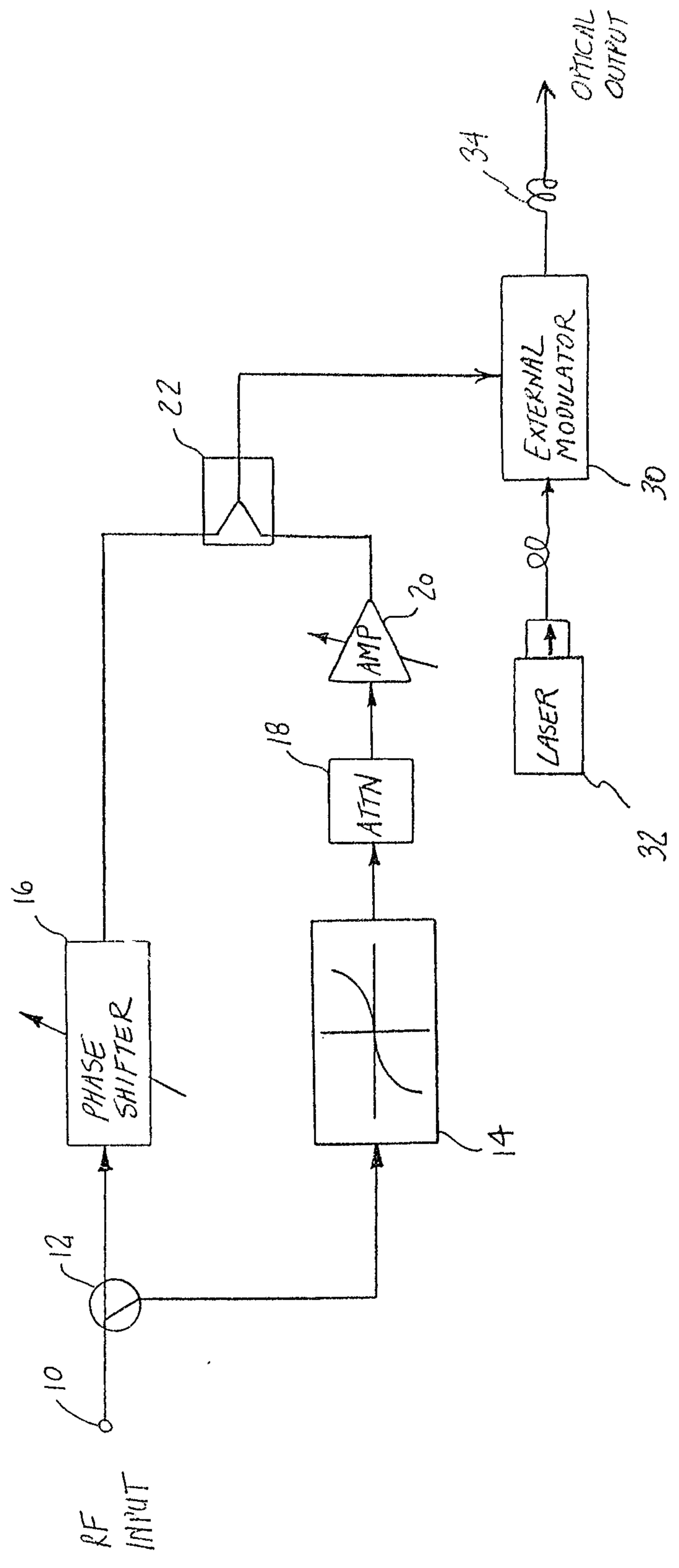


FIG 1

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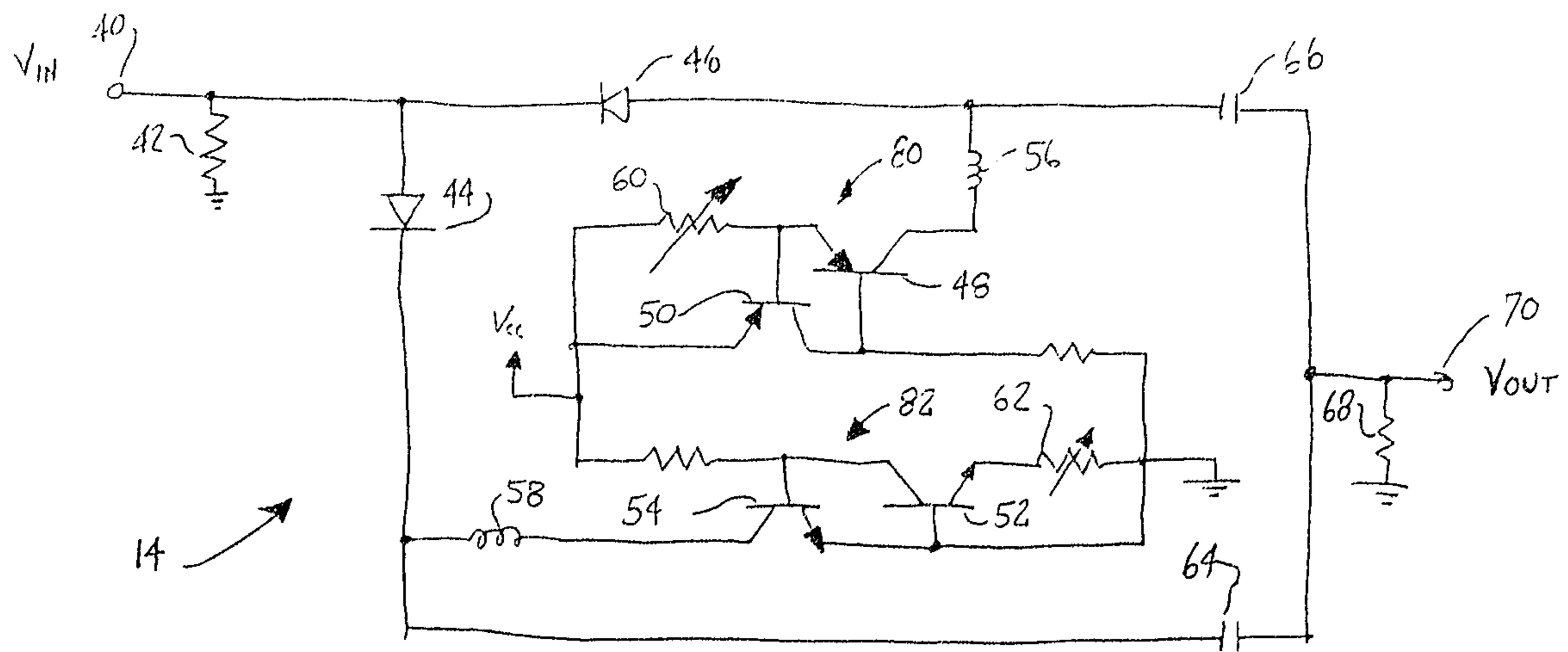


FIG 2

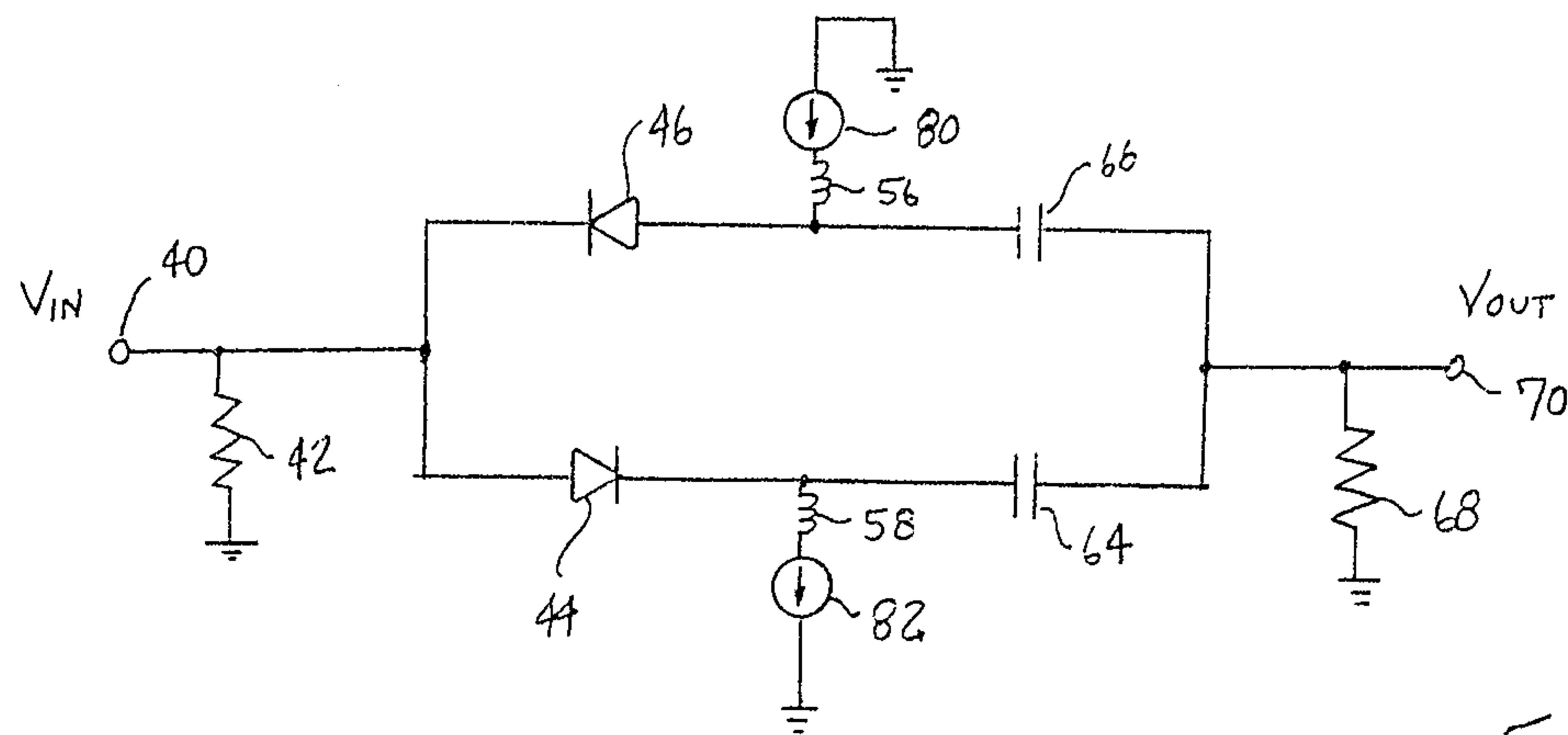


FIG 3

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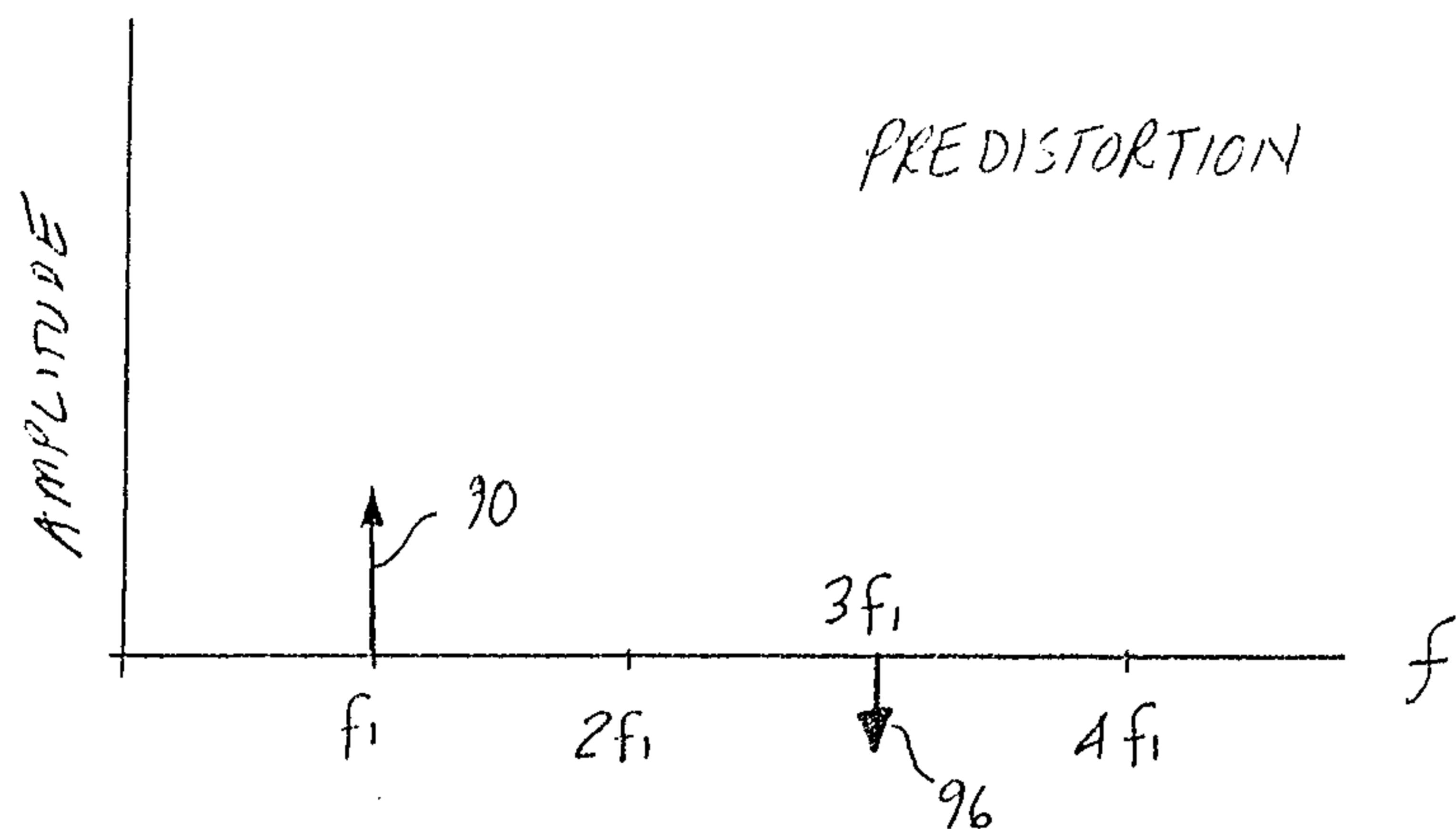


FIG 4a

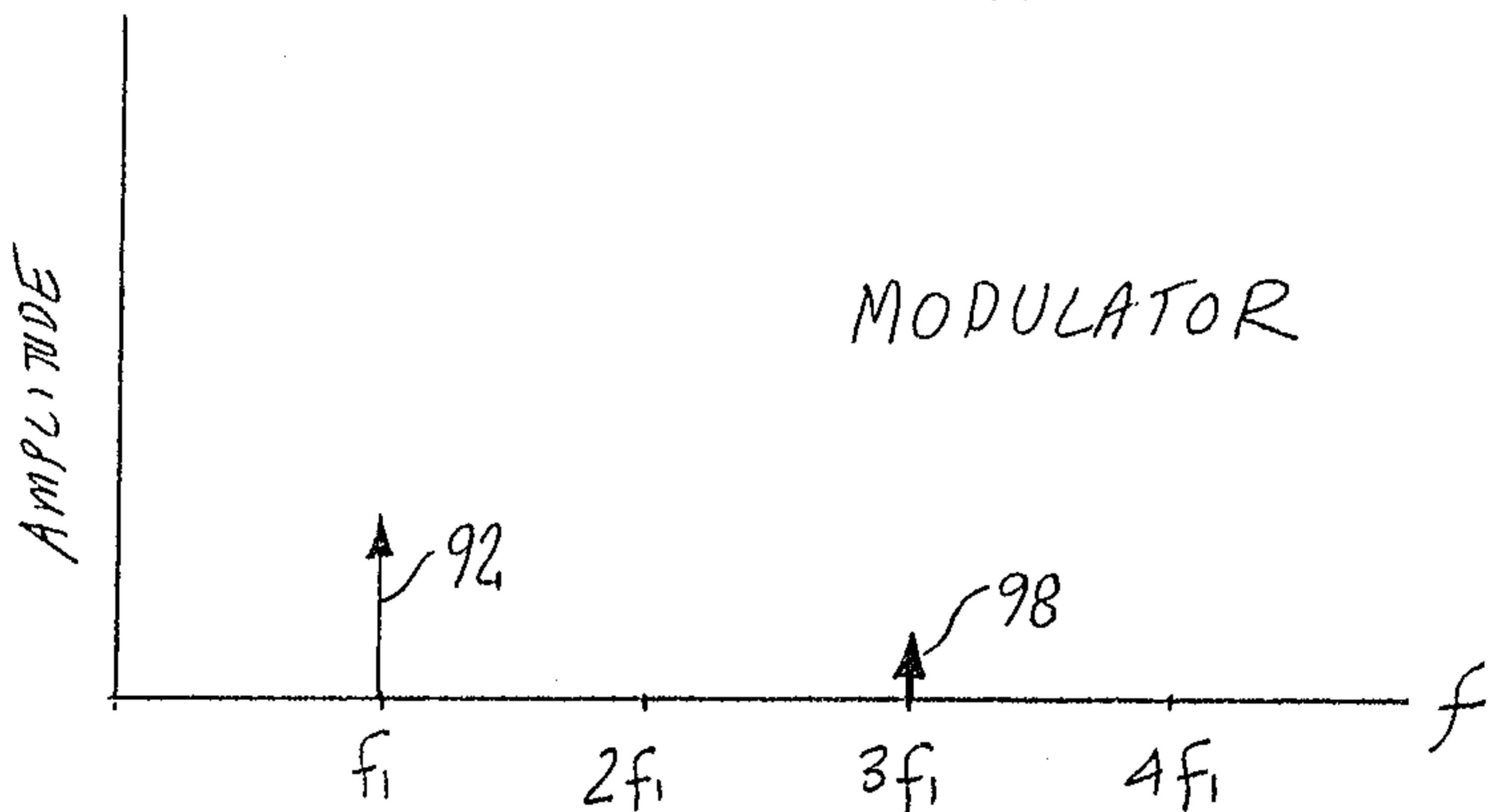


FIG 4b

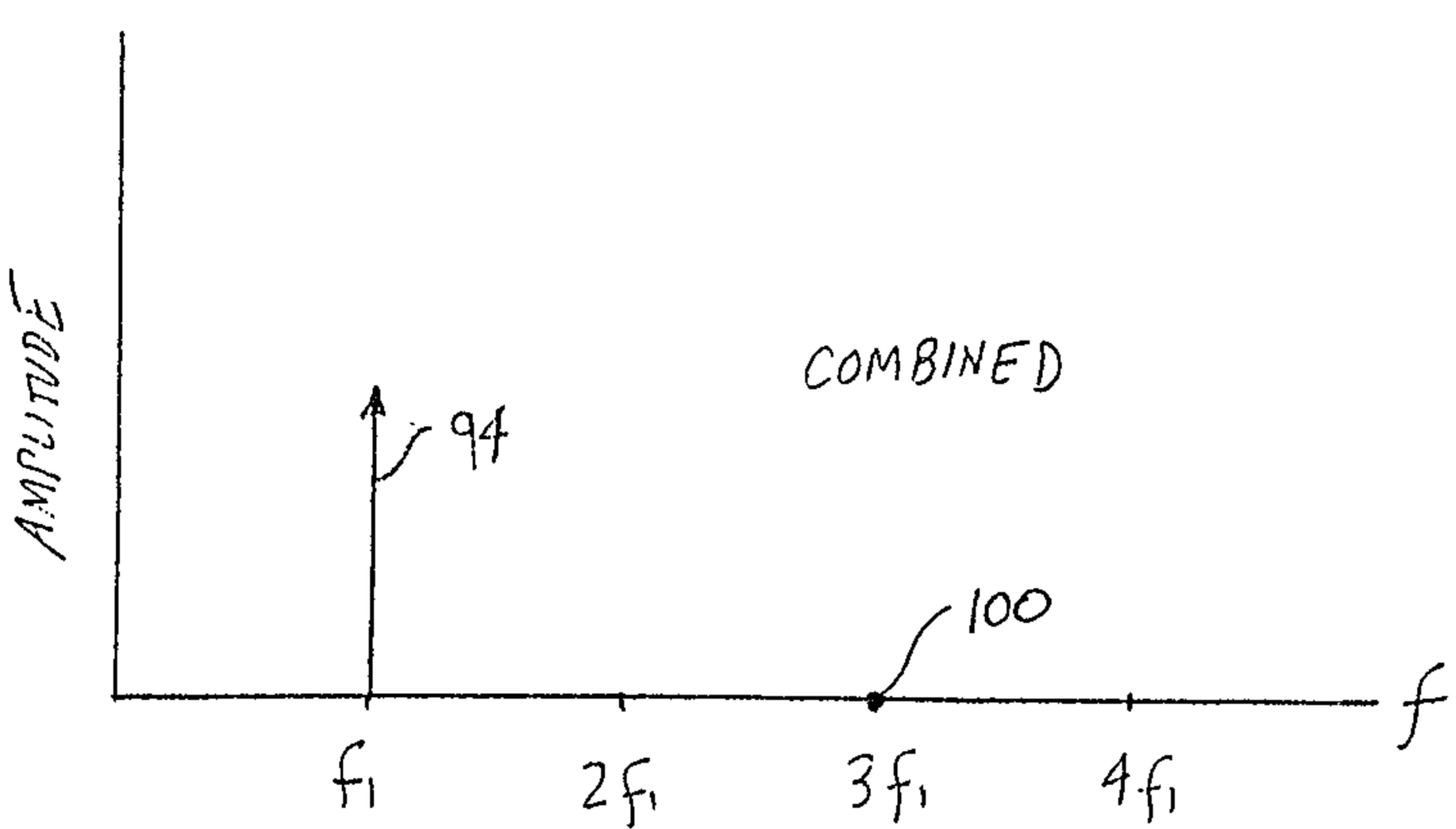


FIG 4c

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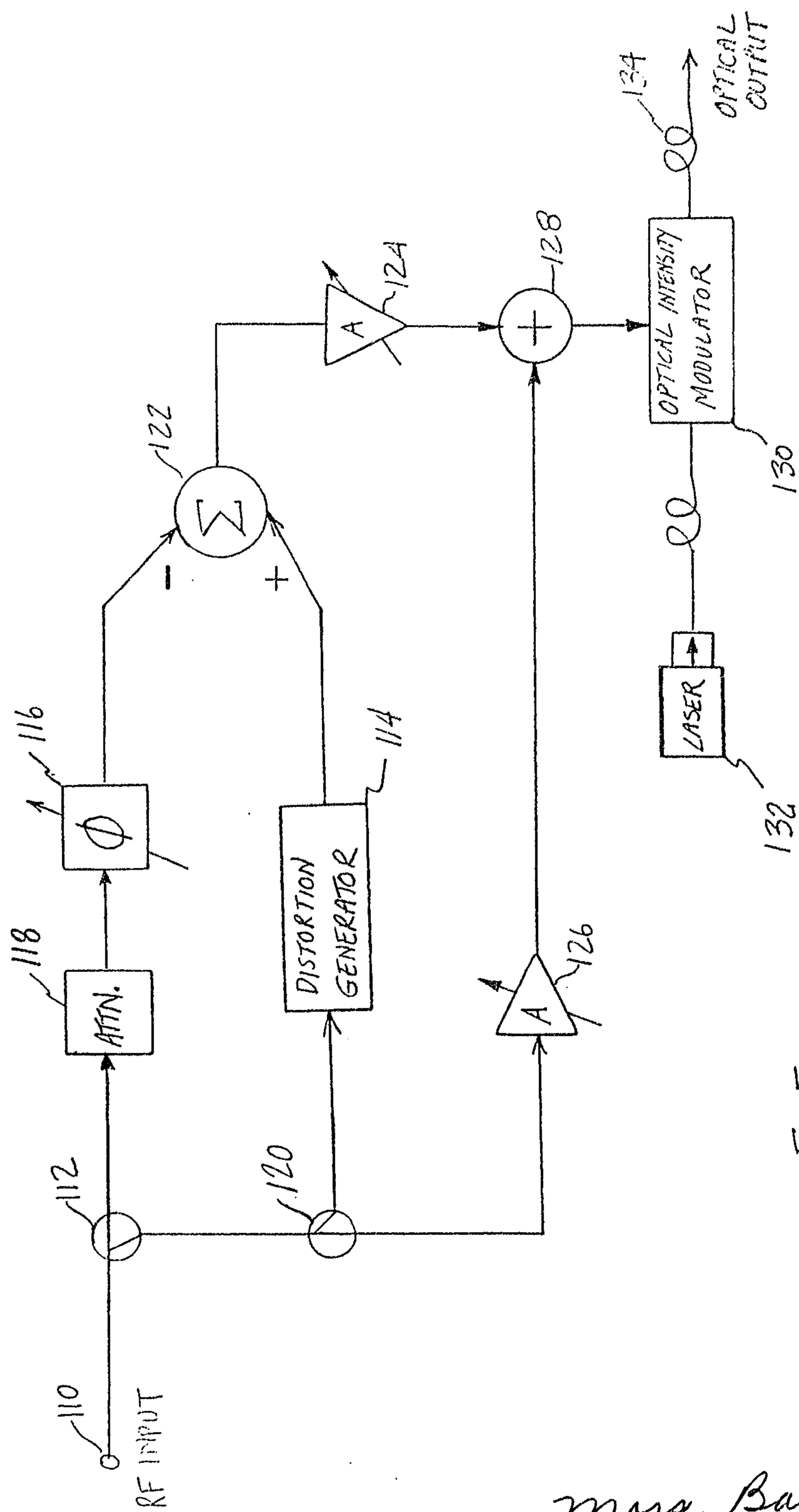


FIG 5

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