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INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

(51) International Patent Classification 5 : E21B 47/022 — A1

(11) International Publication Number: **WO 94/16196**

(43) International Publication Date: 21 July 1994 (21.07.94)

(21) International Application Number: PCT/EP94/00094

(22) International Filing Date: 12 January 1994 (12.01.94)

(30) Priority Data:
93200082.1 13 January 1993 (13.01.93) EP
(34) Countries for which the regional or international application was filed: GB et al.

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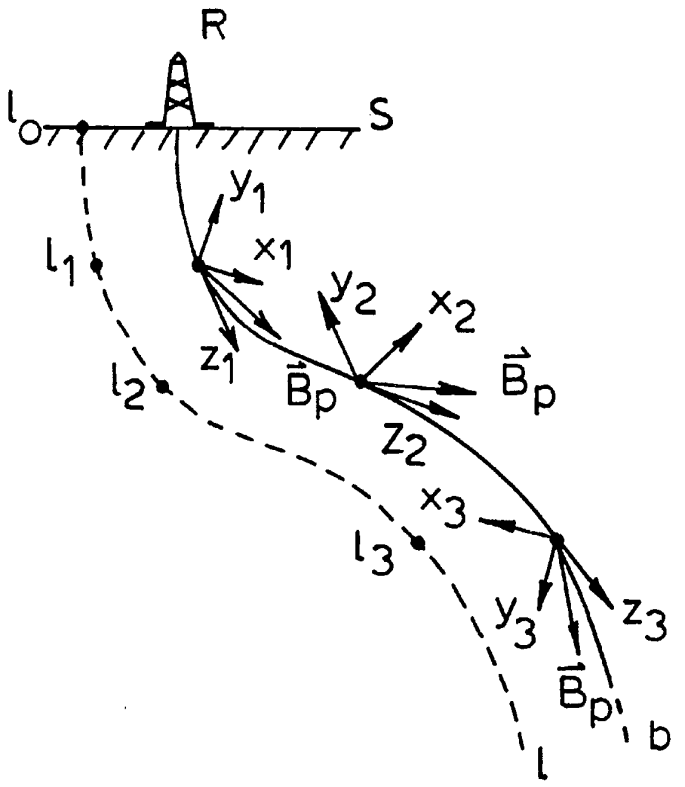
(81) **Designated States:** AT, AU, BB, BG, BR, BY, CA, CH, CN, CZ, DE, DK, ES, FI, GB, HU, JP, KP, KR, KZ, LK, LU, MG, MN, MW, NL, NO, NZ, PL, PT, RO, RU, SD, SE, SK, UA, VN, European patent (AT, BE, CH, DE, DK, ES, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE), OAPI patent (BF, BJ, CF, CG, CI, CM, GA, GN, ML, MR, NE, SN, TD, TG).

Published
With international search report.

(54) **Title:** METHOD FOR DETERMINING BOREHOLE DIRECTION

(57) **Abstract**

A method for determining the direction of a borehole during drilling comprises determination of inclination angle θ and highside angle ϕ from gravity acceleration ($\bar{g}$) measurements and determination of azimuth angle ψ from magnetic field ($\bar{B}$) measurements, the determinations being carried out in conventional XYZ-and-NEV coordinate systems coupled by Euler-angle coordinate transformations. In particular $\bar{g}$ and $\bar{B}$ are measured at least at two borehole depths such that $\phi_i \neq \phi_{i+1}$, ψ_i and ψ_{i+1} being calculated from $B_i = [\phi_i]^T [\theta_i]^T \{[\psi_i]^T B_e\} + B_p$ and $\sin^2\psi_i + \cos^2\psi_i = \sin^2\psi_{i+1} + \cos^2\psi_{i+1}$, with i as number of measurement, B_e as local earth magnetic field, and B_p as perturbating magnetic field. As a result perturbating magnetic fields, for example caused by hot spots or nearby magnetic steel components in the drilling or logging string nearby the B-measuring device, are determined accurately.



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METHOD FOR DETERMINING BOREHOLE DIRECTION

The present invention relates to a method for determining the direction of a borehole during drilling said borehole.

In particular the present invention relates to a method for determining the direction of a borehole during drilling said borehole by using a triaxial accelerometer/magnetometer-package arranged in the drill string employed, said method comprising the steps of:

- measuring gravity acceleration components g_x, g_y, g_z of the known local gravity acceleration vector $\bar{g}$ for determining inclination angle θ and highside angle φ, and
- measuring magnetic field components B_x, B_y, B_z of the total magnetic field $\bar{B}$ for determining azimuth angle ψ,

x, y and z indicating vector components in a Cartesian XYZ-coordinate system fixed to said package during said drilling, and ψ, θ, and φ indicating angles defining rotations between said XYZ-system and a Cartesian NEV-coordinate system, with N the magnetic north direction, V the vertical $\bar{g}$-direction, and E the east direction.

Such a method is known from US patent 4,163,324. Therein it is demonstrated to use a drill string comprising a drilling bit which is coupled at the one side by a non-magnetic drill collar and at the other side by a set of drill collars made of magnetic material. In turn said set is coupled to a drill pipe. The non-magnetic collar contains a survey instrument, for example a triaxial accelerometer/magnetometer package. When measuring the total magnetic field $\bar{B}$, additional to the earth's magnetic field $\bar{B}_e$ a perturbating magnetic field $\bar{B}_p$, for example from the above said bit and/or set of drill collars is included. In said patent it is assumed that for the effect of the magnetic drill string the approximation of only a $\bar{B}_p$-vector along the borehole axis Z, being $\bar{B}_{p,z}$, is sufficient. Said assumption enables to calculate in a

first step an uncorrected azimuth angle, and in a next step to apply an iteration procedure to determine at least a first order correction. In many conditions, however, the assumption of only a $\bar{B}_{p,z}$ and the approximation of $\bar{B}_{p,z}$ are far from realistic.

For example it is well known that during drilling a non-magnetic collar may become magnetised resulting in so-called hot spots encompassing perturbating magnetic field vectors having unpredictable directions.

In US patent 4,682,421 a method for determining a correct azimuth angle by calculating the perturbating erroneous magnetic field $\bar{M}$ at the location of the instrument is presented.

In particular a two-step approach of the above problem is disclosed. After determining the gravity acceleration vector $\bar{g}$ and measuring the total magnetic field $\bar{B}_m$, which is equal to $(\bar{B}_e + \bar{M})$, in a first step the cross-axial component $\bar{M}_{xy}$ of $\bar{M}$ is determined. For said first step at least three x-y-measurements are necessary since $\bar{M}_{xy}$ is derived graphically from a circle made up of said measurements. Consequently said measurements are carried out by rotating the drill string at one location along the borehole axis, being the Z-axis in the measurement coordinate system. It may be clear to those skilled in the art said rotation of the drill string at said location will delay the borehole drilling operation.

For the second step in this patent a geometrical determination of $\bar{M}_z$ is shown. However, since the application of the cosine-rule (as shown in figure 3 of said patent) for obtaining a minimum error value has to be restricted mathematically to a plane comprising all the relevant parameters including Θ and Θ_0, the determination as presented can only be considered an approximation. Consequently possible errors in $\bar{M}_z$ and ψ are dependent on errors in parameters already used in said cosine-rule.

Thus, it is an object of the present invention to overcome the problem of rotating the drill string each time the direction of the borehole has to be determined.

It is a further object of the present invention to present a method enabling determination of azimuth angles which result from straight forward calculation.

It is another object of the present invention to arrive at a method resulting in parameter values which are calculated independently thereby avoiding propagating error calculus.

Therefore the method as shown above is improved in accordance with the present invention in that $\bar{g}$ and $\bar{B}$ are measured at least at two borehole depths l_i, and l_{i+1}, such that $\varphi_i \neq \varphi_{i+1}$, in that ψ_i and ψ_{i+1} are calculated in accordance with

$\bar{B}_i = [\varphi_i]^T [\Theta_i]^T ([\psi_i]^T \bar{B}_e) + \bar{B}_p$ and

$\sin^2\psi_i + \cos^2\psi_i = \sin^2\psi_{i+1} + \cos^2\psi_{i+1}$, or one of its equivalents, with $i = 1, 2, \ldots$, $\bar{B}_e$ being the local earth magnetic field, $\bar{B}_p$ being the magnetic field perturbating $\bar{B}_e$, and $[\ ]^T$ indicating so-called "Transpose" matrices for coordinate transformations from the NEV-system to the XYZ-system under Euler-angles φ, Θ and ψ.

In a further embodiment of the present invention $\bar{g}$ and $\bar{B}$ are measured at least at three borehole lengths l_i, l_{i+1}, and l_{i+2}, such that $\varphi_i \neq \varphi_{i+1} \neq \varphi_{i+2}$, in that ψ_i, ψ_{i+1}, and ψ_{i+2} are calculated in accordance with $\bar{B}_i = [\varphi_i]^T [\Theta_i]^T ([\psi_i]^T \bar{B}_e) + \bar{B}_p$ with $i = 1, 2, 3, \ldots$.

In a preferred embodiment of the invention as shown above, a step for checking the outcome of azimuth angles obtained is provided in that the $(\sin^2\psi + \cos^2\psi) = 1$-equation is verified and compared for every ψ.

Thus, the invention as disclosed above has the advantage that during drilling the borehole measurement values are obtained in a substantially continuous way, both as to the determination of the borehole direction and to checking the measurement values itself. Consequently irregularities in the measuring process, for example due to unexpected formation conditions or apparatus deficiencies, are traced quickly and reliably.

In another embodiment of the present invention the perturbating field $\bar{B}_p$ is determined. Advantageously, $\bar{B}_p$ obtained results from straight forward calculations thus avoiding

approximation procedures, such as there are in iterative processes and graphical determination.

The invention will now be described by way of example in more detail with reference to the accompanying drawings, wherein:

Figure 1 shows the conventional arrangement of an accelerometer/magnetometer-package within a borehole for measuring $\bar{g}$ and $\bar{B}$ with respect to the same Cartesian coordinate frame;

Figures 2A and 2B representing the earth reference frame NEV and the tool fixed and package coupled XYZ coordinate frame;

Figure 3 shows the generally known principles of the borehole direction and coordinate frame orientations coupled by Euler angle coordinate transformations; and

Figure 4 shows schematically the method of measuring during drilling in accordance with the present invention.

Referring to figure 1 schematically a surveying instrument to be arranged within a borehole is shown. Said instrument comprises a well-known accelerometer/magnetometer-package for measuring gravity vector components g_x, g_y, g_z and magnetic field vector components B_x, B_y, B_z. The instrument is arranged in such a way that the Z-axis of the instrument is aligned with the borehole Z-axis. Accordingly X- and Y-axes of accelerometer and magnetometer instrument parts are mutually aligned as shown in this figure.

In figures 2A and 2B schematically coordinate-frames as used are shown. In figure 2A the earth reference frame NEV is shown, N giving respectively the local magnetic north direction, V the vertical direction, more in particular being the direction of the local gravity vector, and E the east direction, perpendicular to the plane made up by N and V. In figure 2B a Cartesian XYZ-axis is shown, the Z-axis being aligned with the borehole axis.

In figure 3 (which can be found e.g. in US 4,163,324) both NEV and XYZ frames are shown with respect to a borehole 1 schematically presented and with respect to each other. As shown in the figure a sequence of three rotations, i.e.:

$$NEV \xrightarrow{\psi} N,E,V \xrightarrow{\theta} N_2E_1Z \xrightarrow{\varphi} XYZ,$$

couples vectors in each of the frames, i.e. an azimuth angle ψ, an inclination angle Θ and a high-side angle φ, so-called Euler-angles, which are well-known to those skilled in the art. Said rotations are conventional coordinate transformations represented by matrices, giving for a vector P_{XYZ} and P_{NEV} a formula

$P_{NEV} = [\psi]\ [\Theta]\ [\varphi]\ P_{XYZ}$, or equivalently

$P_{XYZ} = [\varphi]^T\ [\Theta]^T\ [\psi]^T\ P_{NEV}$, with

$$[\psi] = \begin{vmatrix} \cos\psi & -\sin\psi & 0 \\ \sin\psi & \cos\psi & 0 \\ 0 & 0 & 1 \end{vmatrix} \qquad (1),$$

$$[\Theta] = \begin{vmatrix} \cos\Theta & 0 & \sin\Theta \\ 0 & 1 & 0 \\ -\sin\Theta & 0 & \cos\Theta \end{vmatrix} \qquad (2), \text{ and}$$

$$[\varphi] = \begin{vmatrix} \cos\varphi & -\sin\varphi & 0 \\ \sin\varphi & \cos\varphi & 0 \\ 0 & 0 & 1 \end{vmatrix} \qquad (3), \text{ whereas}$$

$[\psi]^T$, $[\Theta]^T$, and $[\varphi]^T$ are the corresponding so-called "Transpose" matrices. As stated above for any P_{XYZ}-P_{NEV}-vector couple, the same can be applied on the gravity vector $\bar{g}$, being (0,0,g), and $\bar{B}$, being $(B_N,0,B_V)$, both in the NEV-frame.

Thus,
$$\begin{vmatrix} g_x \\ g_y \\ g_z \end{vmatrix} = [\varphi]^T\ [\Theta]^T\ [\psi]^T \begin{vmatrix} 0 \\ 0 \\ g \end{vmatrix} \qquad (4), \text{ and}$$

$$\begin{vmatrix} B_x \\ B_y \\ B_z \end{vmatrix} = [\varphi]^T [\theta]^T [\psi]^T \begin{vmatrix} B_N \\ 0 \\ B_V \end{vmatrix} \qquad (5).$$

For the specific example of the gravity vector it is noted that the inclination angle θ and the high-side angle φ can be determined easily for every measurement location as can be read for example in the above-mentioned US 4,163,324.

Figure 4 shows schematically the method for determining the direction of a borehole during drilling said borehole. From a rig R at the earth's surface S a borehole b is drilled. For reason of clarity a parallel curve 1 is drawn (as dashed line) for indicating borehole depths (or borehole lengths, or borehole locations) l_0, l_1,....., which are measured along the borehole, with l_0 at S, at which locations $\bar{g}$- and $\bar{B}$-measurements are carried out. Schematically, x_i, y_i, z_i, are shown, demonstrating the variable positioning of the survey instrument in the borehole. Furthermore, the perturbating magnetic field $\bar{B}_p$ is shown. This $\bar{B}_p$ is considered dependent on drill string features as explained before, resulting in turn in a rotation and translation of said vector according to the rotation and translation of the XYZ-frame with the survey instrument in the drill string.

From the above it may be clear that at every borehole depth or location l_i the total magnetic field $\bar{B}_i$ can be written as $\bar{B}_i = \bar{B}_e + \bar{B}_p$. However, to calculate this vector sum, a common base or common coordinate frame has to be chosen. As explained above conventionally the XYZ-frame and NEV frame are employed.

In order to arrive at the direction of the borehole, besides θ_i, and φ_i angles, azimuth angles ψ_i have to be determined. Thereto the above-mentioned vector sum can be expressed as

$$\begin{vmatrix} B_x \\ B_y \\ B_z \end{vmatrix}_i = [\varphi]_i^T \, [\Theta]_i^T \left\{ [\psi]_i^T \begin{vmatrix} B_N \\ 0 \\ B_V \end{vmatrix} \right\} + \begin{vmatrix} B_{px} \\ B_{py} \\ B_{pz} \end{vmatrix} \qquad (6)$$

for any borehole depth l_i or measurement number i. From this equation it can be seen easily, that B_x, B_y and B_z are known because they are measured, that the φ- and Θ-matrices are known since φ and Θ are determined in the above-mentioned way, that B_N and B_V are known from geomagnetic data bases and that consequently azimuth angle ψ and magnetic field perturbation vector components B_{px}, B_{py}, B_{pz} have yet to be obtained.

In accordance with the invention for at least two borehole depths l_i and l_{i+1}, which can be written as l_1 and l_2, the components of $\bar{g}$ and $\bar{B}$ are measured. Then, for two measurements the following equations are obtained by rewriting the above equation (6):

$$\begin{vmatrix} B_{x1} \\ B_{y1} \\ B_{z1} \end{vmatrix} = [\varphi_1]^T \, [\Theta_1]^T \begin{Bmatrix} B_N \cos \psi_1 \\ -B_N \sin \psi_1 \\ B_V \end{Bmatrix} + \begin{vmatrix} B_{px} \\ B_{pz} \\ B_{py} \end{vmatrix} \qquad (7), \text{ and}$$

$$\begin{vmatrix} B_{x2} \\ B_{y2} \\ B_{z2} \end{vmatrix} = [\varphi_2]^T \, [\Theta_2]^T \begin{Bmatrix} B_N \cos \psi_2 \\ -B_N \sin \psi_2 \\ B_V \end{Bmatrix} + \begin{vmatrix} B_{px} \\ B_{py} \\ B_{pz} \end{vmatrix} \qquad (8).$$

By well known straight forward calculation of the above equations (7) and (8) it can be seen that the resulting 6 scalar equations for each of the vector components x, y and z, can be considered to comprise 7 unknown parameters, i.e. $\cos \psi_1$, $\sin \psi_1$, $\cos \psi_2$, $\sin \psi_2$, B_{px}, B_{py} and B_{pz}.

In order to arrive uniquely at ψ_1 and ψ_2, as seventh scalar equation $\sin^2\psi_1 + \cos^2\psi_1 = \sin^2\psi_2 + \cos^2\psi_2$ is taken. It may be

clear to those skilled in the art that also the equivalent equations $\sin \psi_1^2 + \cos \psi_1^2 = 1$, or $\sin \psi_2^2 + \cos \psi_2^2 = 1$, can be used. It is mathematically self-evident that $\varphi_1 \neq \varphi_2$, and thus the drill string should have been rotated. Substantially always this criterion is satisfied because the drill string is always rotated between survey location during drilling the borehole. Thus, advantageously the rotations of the drill string usually occurring during the drilling operation, are used, rather than stopping the drilling operation and subsequently rotating as referred to above. After having calculated the values for said 7 parameters ψ_i-values are obtained in accordance with

$$\psi_i = \arctan\left(\frac{\sin \psi_i}{\cos \psi_i}\right) \quad (9).$$

Based on the same idea, for three measurements at correspondingly three measurement locations, for example l_1, l_2 and l_3, the following equations are obtained two of which being identical to the above (7) and (8):

$$\begin{bmatrix} B_{x1} \\ B_{y1} \\ B_{z1} \end{bmatrix} = [\varphi_1]^T [\theta_1]^T \begin{Bmatrix} B_N \cos \psi_1 \\ -B_N \sin \psi_1 \\ B_V \end{Bmatrix} + \begin{bmatrix} B_{px} \\ B_{py} \\ B_{pz} \end{bmatrix} \quad (7),$$

$$\begin{bmatrix} B_{x2} \\ B_{y2} \\ B_{z2} \end{bmatrix} = [\varphi_2]^T [\theta_2]^T \begin{Bmatrix} B_N \cos \psi_2 \\ -B_N \sin \psi_2 \\ B_V \end{Bmatrix} + \begin{bmatrix} B_{px} \\ B_{py} \\ B_{pz} \end{bmatrix} \quad (8), \text{ and}$$

$$\begin{bmatrix} B_{x3} \\ B_{y3} \\ B_{z3} \end{bmatrix} = [\varphi_3]^T [\theta_3]^T \begin{Bmatrix} B_N \cos \psi_3 \\ -B_N \sin \psi_3 \\ B_V \end{Bmatrix} + \begin{bmatrix} B_{px} \\ B_{py} \\ B_{pz} \end{bmatrix} \quad (10).$$

From the 9 scalar equations which are found by reformulating the above equations (7), (8) and (10), it can be to seen in the same way as shown above that for the 9 unknown parameters the system of equations is complete and no further equations are necessary for solving them uniquely. For the present system of equations $\cos \psi_1$, $\sin \psi_1$, $\cos \psi_2$, $\sin \psi_2$, $\cos \psi_3$, $\sin \psi_3$, B_{px}, B_{py} and B_{pz} again can be considered as independent variables. Again ψ_i-values are obtained in accordance with the above equation (9).

Analogously to the case of only two measurements it is noted that $\varphi_1 \neq \varphi_2 \neq \varphi_3$ and no further specific rotation actions are necessary.

In a further embodiment of the present invention a check-procedure is comprised.

In case of having carried out measurements at two locations l_1 and l_2, the equivalents $\sin^2\psi_1 + \cos^2\psi_1 = \sin^2 \psi_2 + \cos^2 \psi_2$, being $\sin^2 \psi_1 + \cos^2 \psi_1 = 1$ or $\sin^2 \psi_2 + \cos^2 \psi_2 = 1$, are employed for check purposes. If significant deviations from 1 appear, at a next borehole depth a new set of $\bar{B}$ and $\bar{g}$ measurements is taken and the check-procedure can be repeated. Advantageously, also for such a check no additional rotations are required. Again only different highside angles have to be measured.

As to the case having carried out measurements at at least three locations and consequently using 9 equations for determining azimuth angles ψ_1, ψ_2 and ψ_3, now $\sin^2 \psi_i + \cos^2 \psi_i = 1$-equalities, or one of its equivalents being $\sin^2 \psi_i + \cos^2 \psi_i = \sin^2 \psi_{i+1} + \cos^2 \psi_{i+1}$ for respective i-value, are applied for the first time. The same observations are made as to the use and application of said check-procedure.

In a next step $\bar{B}_p$ can be determined accurately and reliably. In most cases $\bar{B}_p$ is coupled to drill string characteristics. Besides such $\bar{B}_p$- determinations sudden changes in $\bar{B}_p$ can be traced, for example caused by tool failure, magnetic storms, extraneous magnetic fields, etc.

As explained above, for the one or the other determination procedure, only two or three measurement sets repectively are

required. It may be clear that normal operation conditions cover several thousands of feet or several kilometers borehole depths and a plurality of measurement sets are obtained. Consequently borehole directions can be determined and followed quickly and reliably without special operational effort.

Various modifications of the present inventions will become apparent to those skilled in the art from the foregoing description. Such modifications are intended to fall within the scope of the appended claims.

C L A I M S

1. A method for determining the direction of a borehole during drilling said borehole by using a triaxial accelerometer/magnetometer-package arranged in the drill string employed, said method comprising the steps of,

- measuring gravity acceleration components g_x, g_y, g_z of the known local gravity acceleration vector $\bar{g}$ for determining inclination angle Θ and highside angle φ; and
- measuring magnetic field components B_x, B_y, B_z of the total magnetic field $\bar{B}$ for determining azimuth angle ψ;

x, y and z indicating vector components in a Cartesian XYZ-coordinate system fixed to said package during said drilling, and ψ, Θ and φ indicating angles defining rotations between said XYZ-system and a Cartesian NEV-coordinate system, with N the magnetic north direction, V the vertical $\bar{g}$-direction, and E the east direction wherein $\bar{g}$ and $\bar{B}$ are measured at least at two borehole depths l_i and l_{i+1}, such that $\varphi_i \neq \varphi_{i+1}$, in that ψ_i and ψ_{i+1} are calculated in accordance with

$$\bar{B}_i = [\varphi_i]^T [\Theta_i]^T \{[\psi_i]^T \bar{B}_e\} + \bar{B}_p \quad \text{and}$$

$$\sin^2\psi_i + \cos^2\psi_i = \sin^2\psi_{i+1} + \cos^2\psi_{i+1}, \quad \text{or one of its}$$

equivalents, with $i = 1, 2, \ldots$, $\bar{B}_e$ being the local earth magnetic field, $\bar{B}_p$ being the magnetic field perturbating $\bar{B}_e$, and $[\ ]^T$ indicating "Transpose" matrices for coordinate transformations from the NEV-system to the XYZ-system under Euler-angles φ, Θ, and ψ.

2. The method as claimed in claim 1, further comprising the steps of:

- checking if said equivalent $(\sin^2\psi_i + \cos^2\psi_i)$ is equal to 1,
- measuring $\bar{g}$ and $\bar{B}$ at least at one further borehole depth l_{i+2} if $(\sin^2\psi_i + \cos^2\psi_i) \neq 1$, with $\varphi_i \neq \varphi_{i+1} \neq \varphi_{i+2}$,
- calculating ψ_{i+2}, and
- carrying out a next checking step.

3. A method for determining the direction of a borehole during drilling said borehole by using a triaxial accelerometer/magnetometer-package arranged in the drill string employed, said method comprising the steps of:

- measuring gravity acceleration components g_x, g_y, g_z of the known local gravity acceleration vector $\bar{g}$ for determining inclination angle θ and highside angle φ; and
- measuring magnetic field components B_x, B_y, B_z of the total magnetic field $\bar{B}$ for determining azimuth angle ψ,

x, y and z indicating vector components in a Cartesian XYZ-coordinate system fixed to said package during said drilling, and ψ, θ and φ indicating angles defining rotations between said XYZ-system and a Cartesian NEV-coordinate system, with N the magnetic north direction, V the vertical $\bar{g}$-direction and E the east direction, wherein $\bar{g}$ and $\bar{B}$ are measured at least at three borehole depths l_i, l_{i+1} and l_{i+2}, such that $\varphi_i \neq \varphi_{i+1} \neq \varphi_{i+2}$, in that ψ_i, ψ_{i+1} and ψ_{i+2} are calculated in accordance with $\bar{B}_i = [\varphi_i]^T [\theta_i]^T ([\psi_i]^T \bar{B}_e) + \bar{B}_p$, with $i = 1, 2, 3, \ldots$, $\bar{B}_e$ being the local earth magnetic field, $\bar{B}_p$ being the magnetic field perturbating $\bar{B}_e$, and $[\ ]^T$ indicating "Transpose" matrices for coordinate transformations from the NEV-system to the XYZ-system under Euler-angles φ, θ and ψ.

4. The method as claimed in claim 3, further comprising the steps of:

- checking if $\sin^2\psi_i + \cos^2\psi_i = 1$ for at least one i or one of its equivalents ;
- measuring $\bar{g}$ and $\bar{B}$ at least at one further borehole depth l_{i+3} if $\sin^2\psi_i + \cos^2\psi_i \neq 1$, with $\varphi_i \neq \varphi_{i+1} \neq \varphi_{i+2} \neq \varphi_{i+3}$;
- calculating ψ_{i+3}, and
- carrying out a next checking step.

5. The method as claimed in any one of the claims 1 to 4, wherein the perturbating magnetic field $\bar{B}_p$ is determined.

WO 94/16196 PCT/EP94/00094

FIG.1

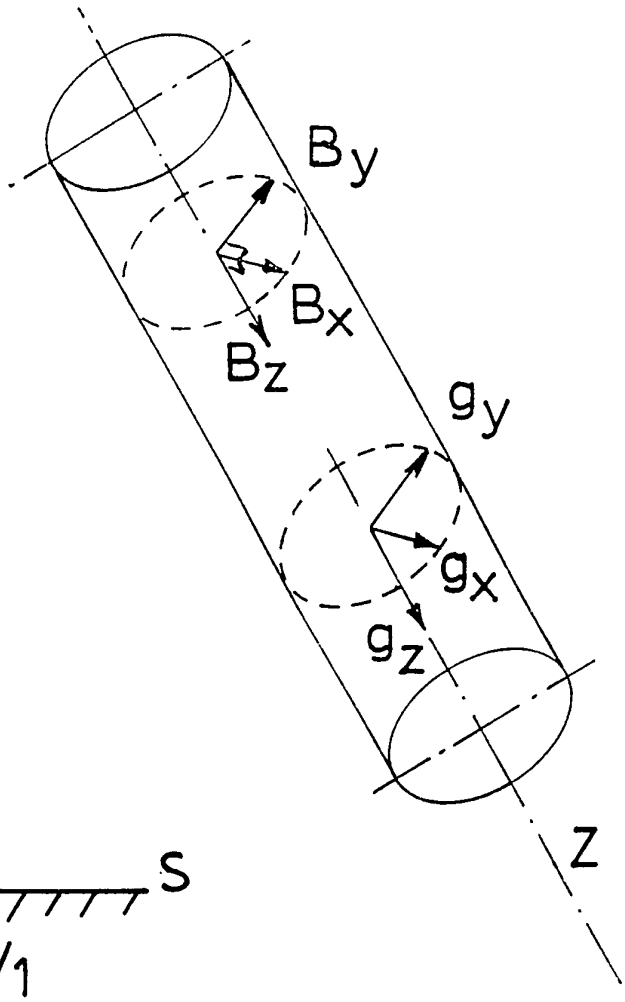


FIG.4

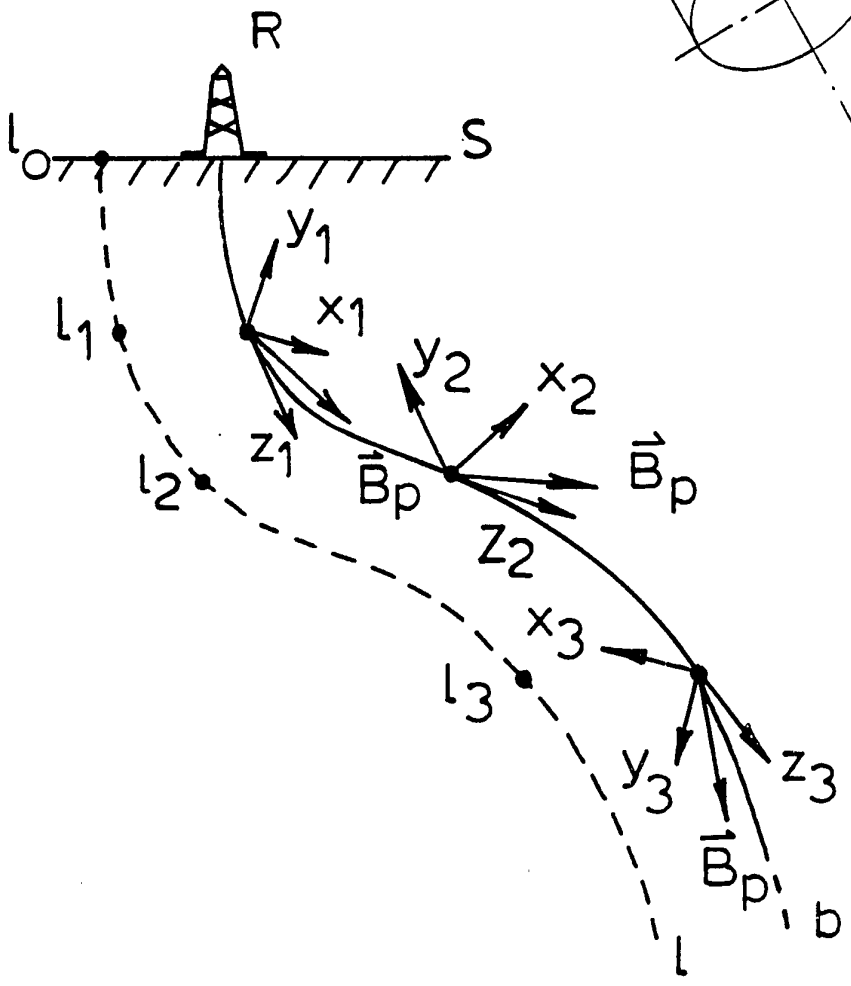
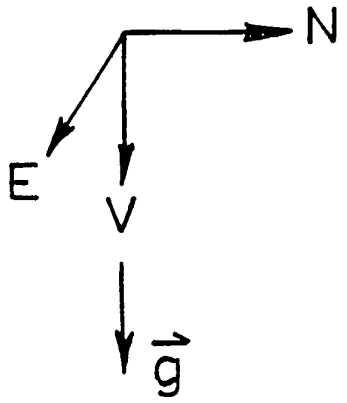


FIG.2A



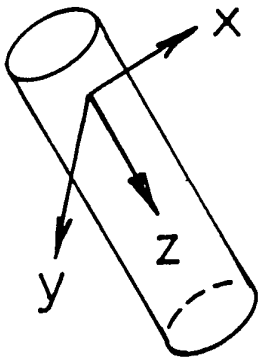


FIG.2B

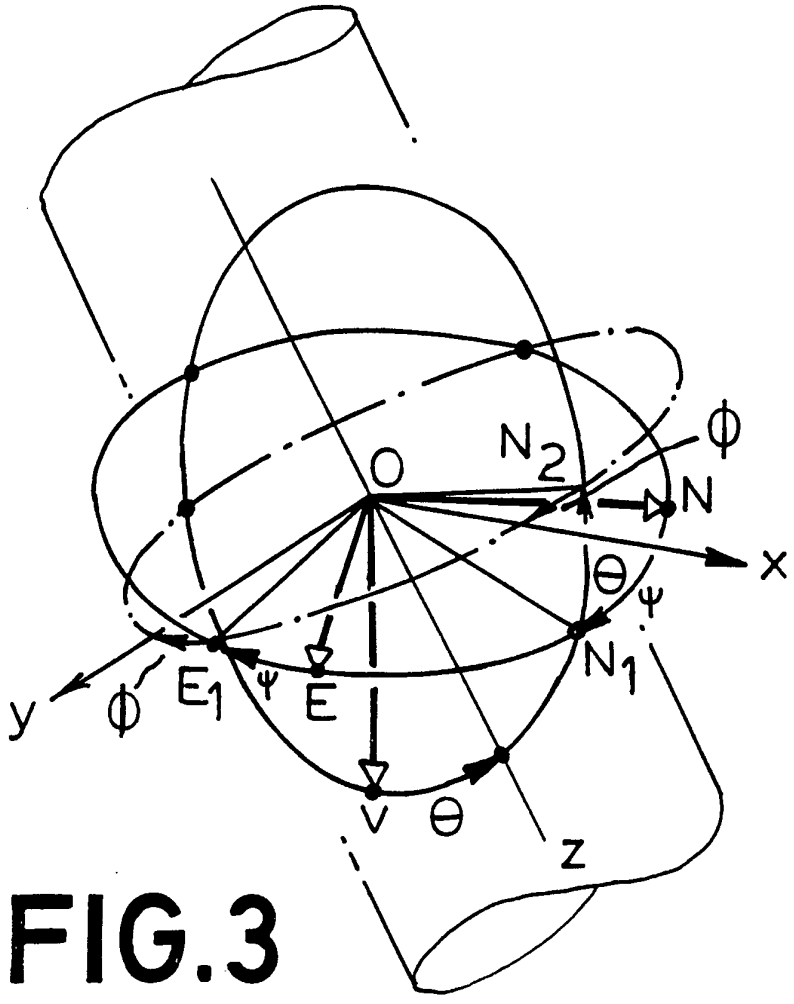


FIG.3

INTERNATIONAL SEARCH REPORT

Intern ıal Application No
PCT/EP 94/00094

A. CLASSIFICATION OF SUBJECT MATTER
IPC 5 E21B47/022

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 5 E21B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US,A,4 682 421 (VAN DONGEN ET AL.) 28 July 1987 cited in the application see the whole document	1
A	US,A,4 163 324 (RUSSELL ET AL.) 7 August 1979 cited in the application see the whole document	1
A	EP,A,0 387 991 (RUSSELL ET AL.) 19 September 1990 see abstract	1
A	WO,A,92 10642 (INSTITUT FRANCAIS DE PETROLE ET AL.) 25 June 1992 see abstract	1

-/--

[X] Further documents are listed in the continuation of box C.

[X] Patent family members are listed in annex.

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"P" document published prior to the international filing date but later than the priority date claimed

"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

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"&" document member of the same patent family

Date of the actual completion of the international search	Date of mailing of the international search report
17 March 1994	30. 03. 94

Name and mailing address of the ISA	Authorized officer
European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Tx. 31 651 epo nl, Fax: (+31-70) 340-3016	Hoekstra, F

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C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US,A,4 709 486 (WALTERS) 1 December 1987 see abstract -----	1

INTERNATIONAL SEARCH REPORT

Information on patent family members

Inter nal Application No
PCT/EP 94/00094

Patent document cited in search report	Publication date	Patent family member(s)		Publication date
US-A-4682421	28-07-87	AU-B-	570356	10-03-88
		AU-A-	5389886	04-09-86
		CA-A-	1259187	12-09-89
		EP-A,B	0193230	03-09-86
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WO-A-9210642	25-06-92	FR-A-	2670532	19-06-92
		CA-A-	2076047	13-06-92
		GB-A-	2256492	09-12-92
US-A-4709486	01-12-87	NONE		