



(10) International Publication Number
WO 2010/056253 A1

(43) International Publication Date
20 May 2010 (20.05.2010)

PCT

- (51) **International Patent Classification:**
H01S 3/067 (2006.01) *H01S 3/063* (2006.01)
- (21) **International Application Number:**
PCT/US2008/083734
- (22) **International Filing Date:**
17 November 2008 (17.11.2008)
- (25) **Filing Language:** English
- (26) **Publication Language:** English
- (71) **Applicant** (*for all designated States except US*):
RAYTHEON COMPANY [US/US]; 870 Winter Street,
Waltham, MA 02451-1449 (US).
- (72) **Inventors; and**
- (75) **Inventors/Applicants** (*for US only*): **SHKUNOV, Vladimir, V.** [US/US]; 3908 W. 242nd St., Torrance, CA 90505-6405 (US). **BETIN, Alexander, A.** [US/US]; 1246 8th St., Manhattan Beach, CA 90266-6014 (US). **ROCKWELL, David, A.** [US/US]; 4482 Jasmine Ave., Culver City, CA 90232-3429 (US).
- (74) **Agents:** **HUME, Larry** et al.; Pillsbury Winthrop Shaw Pittman LLP, P.O. Box 10500, McLean, VA 22102 (US).
- (81) **Designated States** (*unless otherwise indicated, for every kind of national protection available*): AE, AG, AL, AM,

AO, AT, AU, AZ, BA, BB, BG, BH, BR, BW, BY, BZ,
CA, CH, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ,
EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN,
HR, HU, ID, IL, IN, IS, JP, KE, KG, KM, KN, KP, KR,
KZ, LA, LC, LK, LR, LS, LT, LU, LY, MA, MD, ME,
MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO,
NZ, OM, PG, PH, PL, PT, RO, RS, RU, SC, SD, SE, SG,
SK, SL, SM, ST, SV, SY, TJ, TM, TN, TR, TT, TZ, UA,
UG, US, UZ, VC, VN, ZA, ZM, ZW.

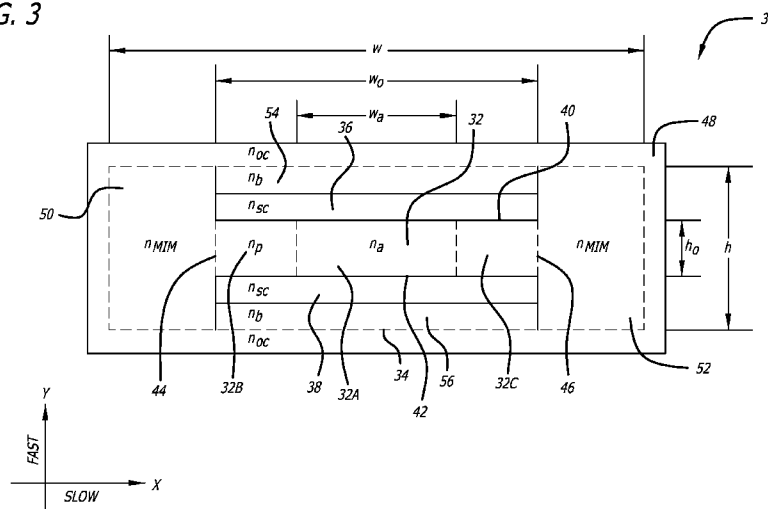
- (84) Designated States** (*unless otherwise indicated, for every kind of regional protection available*): ARIPO (BW, GH, GM, KE, LS, MW, MZ, NA, SD, SL, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, MD, RU, TJ, TM), European (AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MT, NL, NO, PL, PT, RO, SE, SI, SK, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, ML, MR, NE, SN, TD, TG).

Published:

- with international search report (Art. 21(3))
- with information concerning one or more priority claims considered void (Rule 26bis.2(d))

(54) Title: METHOD AND APPARATUS FOR GENERATION AND AMPLIFICATION OF LIGHT IN A SEMI-GUIDING HIGH ASPECT RATIO CORE FIBER

FIG. 3



(57) Abstract: A planar laser gain medium (30) and laser system (100) The laser gain medium (30) includes an active core (32) having a high aspect ratio cross-section with a fast-axis dimension and a slow-axis dimension, signal claddings (36, 38) adapted to form reflective boundaries at fast axis boundaries of the core, and a material (50, 52) adapted to minimize reflections at slow axis boundaries of the core. In the illustrative embodiment, the laser gain medium (30) is an optical fiber. The core (32) and signal claddings (36, 38) form a waveguide adapted to control modes propagating in the fast-axis direction. When the laser gain medium (30) is employed as a laser oscillator, a high reflectivity mirror (102) and an outcoupler (104) are positioned at opposite ends of the core (32) to form a laser resonator adapted to control modes in the slow axis direction

**METHOD AND APPARATUS FOR GENERATION
AND AMPLIFICATION OF LIGHT IN
A SEMI-GUIDING HIGH ASPECT RATIO CORE FIBER**

[0001] This application is related to U.S. Patent Application No. 11/891,328, filed August 9, 2007, which is incorporated herein by reference in its entirety.

BACKGROUND

[0002] High energy and high power laser systems generate optical beams for applications such as laser weapons, industrial lasers for materials processing, and long range lidar/ladar systems. (Energy and power are related, but fundamentally different, physical parameters. The challenges in scaling lasers to higher energy and power are often similar, but not always so. The present disclosure can be adapted to either energy or power scaling. Throughout the remainder of this discussion, the term power will be used with the understanding that this disclosure can also be used to increase energy.) One of the most challenging problems for scaling laser output power has proven to be beam quality reduction, which arises from the increased cross-sectional area of the active medium, as well as from thermal effects, optical damage, and nonlinear processes that are initiated in the laser materials at high optical intensities.

[0003] Solid-state lasers (SSLs) have many packaging advantages when compared to liquid or gas lasers. Diode pumped SSLs appear to be among the most power-efficient laser designs. In general, there are two alternative routes to diode-pumped SSL systems today. Bulk active elements for SSL applications are shaped as rods or slabs, or, recently, as planar waveguides (PWGs) that allow for a large beam cross-section to eliminate optical damage and to provide a more favorable thermal geometry. Bulk elements are usually made of a heat conducting crystalline material to

facilitate cooling. Large size crystals, however, suffer from poor optical quality, and are expensive to manufacture. This factor limits the power scalability of crystalline bulk systems.

[0004] Active elements of SSLs can also be made from glass. Glass is inexpensive, clear, isotropic and a low-absorbing material. Cooling bulk glass elements is complicated, however, because of the low thermal conductivity of glass.

[0005] The optical fiber configuration solves this thermal management problem: the large surface-area-to-volume ratio can maintain a low core temperature even at high lateral gradient. Fiber lasers have proven to be more power-effective SSL devices than bulk rods or slabs. They include a small active core that provides for excellent spatial overlap between absorbed pump power and the signal beam and ensures heavily saturated operation, both of which make fiber lasers highly efficient. Moreover, fibers can be designed to minimize power lost due to fluorescence and amplified spontaneous emission (ASE). In addition, fiber designs are compact, flexible, and lightweight. Exceptional power efficiency and significant packaging benefits have positioned fiber lasers as one of the most promising candidates for high power laser applications, including airborne high-energy weapons and lidar/ladar sensors.

[0006] On the other hand, the small cross-sectional area of fibers, which is advantageous for beam quality, heat dissipation, and gain saturation, becomes a real problem if one wishes to scale the output power to higher levels. Optical damage and nonlinear optical effects both arise at high light intensity. So, when attempting to increase laser output while maintaining high beam quality (BQ), the dilemma of choosing between bulk crystal or glass active elements and fiber gain elements has not yet been resolved.

[0007] Considering the specific case of fiber-based lasers and amplifiers, the applicability of traditional active fibers for building high-energy laser and long distance lidar/ladar sources is limited. Single transverse mode operation is typically necessary for high intensity on target, for accurate pointing, and for beam control, but such operation usually requires that the core diameter be small. However, if the core

is too small, optical damage can preclude reliable operation. In modern silica glass fibers, reliable operation requires intensities to be maintained below $2 \text{ W}/\mu\text{m}^2$ ($200 \text{ MW}/\text{cm}^2$) for CW (continuous wave) applications and about $2 \text{ GW}/\text{cm}^2$ for nanosecond-range pulses. Nonlinear phase modulation and various types of stimulated scattering occur for common fibers at power levels of several hundred watts, resulting in spectral broadening, locking longitudinal modes, and degraded coherence. Thermal damage of pump combiners represents another challenge.

[0008] Large mode area (LMA) fibers are commonly used for high power fiber lasers to overcome damage and nonlinearity problems. However, the increased core size cannot generally be made to operate only in a single mode, because the numerical aperture (NA) required for single-mode operation at large core sizes is lower than can be reliably achieved. Specifically, in existing fibers, the limited fine control of the core index increment restricts the NA to levels above 0.05. Another problem with the low-NA fibers is that they are sensitive to bending, and this fact complicates packaging. Different guiding-core structures and shapes to spread the mode size have been studied, including the addition of extra refractive index walls between the circular core and cladding. Coiling a fiber to strip out higher-order modes has been proposed and successfully used to select the lowest-order mode for LMA fiber lasers. Such efforts have resulted in the ability to raise the core diameter up to $30\text{-}50 \mu\text{m}$. For core sizes larger than that, straight rod-like fibers have been shown to be useful for a high quality output beam.

[0009] The highest power reported for a nearly single-transverse mode fiber laser is presently about 3 kW. This power level approaches the practical limits estimated to be as high as 5-10 kilowatts for the CW regime. In the q-switched regime with nsec pulse durations, the state of the art is a few mJ, or peak powers of a few MW. Weapons-class applications, however, typically set 100 kW as a threshold for the laser system to become practically significant, and typical ladar sensor applications require peak powers of 10 MW or more. Few solutions have been proposed that can scale the output power of individual fiber lasers to this level. Most known proposed solutions involve combining parallel single-mode or LMA fiber channels. In

principle, with this approach, the output power increases in proportion to the number of channels. However, maintaining a high beam quality and achieving a high combining efficiency (which means that the total combined power is equal to the sum of the powers of the individual fibers) have proven to be a challenge when addressing high power lasers.

[0010] In spite of extended efforts, fiber combining schemes have never reached the power levels achieved by direct LMA fiber sources. Nonlinear optical, thermal, and gain-saturation effects have so far limited the output power of fiber-combining schemes to a level that is nearly an order of magnitude below that possible with LMA designs. This suggests that fiber combining methods may not be capable of meeting the requirements of the intended applications.

[0011] An analysis of the present state of the art suggests that existing methods of raising fiber-laser output powers (either singly or combination) above 10 to 20 kilowatts are not capable of also delivering a high output beam quality.

[0012] Hence, a need exists in the art for an improved system or method for generating or amplifying higher output power laser beams than can be achieved with prior approaches, while maintaining high output beam quality.

SUMMARY

[0014] The need in the art is addressed by the laser gain medium and laser system of the present disclosure. The novel laser gain medium includes an active core having a high aspect ratio cross-section with a fast axis and a slow axis, claddings adapted to form reflective boundaries at fast-axis boundaries of the core, and a material adapted to minimize reflections at slow-axis boundaries of the core (the fast-axis direction is along the thin dimension of the core, while the slow-axis direction is along the wide dimension of the core). In an illustrative embodiment, the laser gain medium is an optical fiber. The core and claddings form a waveguide adapted to control modes propagating in the fast-axis direction. When the laser gain medium is employed as a laser oscillator, a high reflectivity mirror and an outcoupler are positioned at opposite ends of the core to form a laser

resonator adapted to control modes in the slow-axis direction. When the laser gain medium is employed as a laser amplifier, the slow-axis beam quality of the output beam depends on that of the input beam and on the homogeneity of the fiber gain medium.

BRIEF DESCRIPTION OF THE DRAWINGS

[0015] Fig. 1a is a simplified schematic showing a cross-sectional view of a conventional cladding-pumped (double-clad) active fiber.

[0016] Fig. 1b is a simplified schematic of a typical fiber laser system.

[0017] Fig. 2a is a simplified schematic of a fiber designed in accordance with an illustrative embodiment of the present disclosure.

[0018] Fig. 2b is a simplified schematic of a fiber coiled around a cylinder designed in accordance with an illustrative embodiment of the present disclosure.

[0019] Fig. 3 is a simplified schematic of a cross-sectional view of a fiber designed in accordance with an illustrative embodiment of the present disclosure, showing the refractive indices over a fiber slice.

[0020] Fig. 4a is a simplified schematic showing a cross-sectional view of a fiber designed in accordance with an alternative embodiment of the present disclosure, for the case of asymmetrical location of the core inside the fiber foil.

[0021] Fig. 4b is a simplified schematic showing a cross-sectional view of a fiber designed in accordance with an alternative embodiment of the present disclosure, in which the inner cladding is made from a liquid or gel material.

[0022] Fig. 5a is a simplified schematic showing a top view of a laser resonator designed in accordance with an illustrative embodiment of the present disclosure, where the resonator components are integrated into the glass foil and where the resonator reflector is implemented as a planar version of a Porro prism.

[0023] Fig. 5b is a simplified schematic showing an example of an optimized resonator geometry for the illustrative laser configuration of Fig. 5a.

[0024] Fig. 6 is a simplified schematic of an alternative laser resonator architecture for planar mode selection designed in accordance with an illustrative embodiment of the

present disclosure.

[0025] Fig. 7 is a simplified schematic of a multi-sectional laser system designed in accordance with an illustrative embodiment of the present disclosure.

[0026] Fig. 8 is a simplified schematic of a fiber assembly with a novel pumping scheme designed in accordance with an illustrative embodiment of the present teachings.

[0027] Fig. 9 is a simplified schematic of a fiber assembly with an alternate pumping scheme designed in accordance with an illustrative embodiment of the present teachings.

DETAILED DESCRIPTION

[0028] Illustrative embodiments and exemplary applications will now be described with reference to the accompanying drawings to disclose the advantageous teachings of the present disclosure.

[0029] While the present disclosure is described herein with reference to illustrative embodiments for particular applications, it should be understood that the disclosure is not limited thereto. Those having ordinary skill in the art and access to the teachings provided herein will recognize additional modifications, applications, and embodiments within the scope thereof and additional fields in which the present disclosure would be of significant utility.

[0030] Fig. 1a is a simplified schematic of a conventional cladding-pumped active fiber 10. Active fibers are typically manufactured in a double-clad configuration, having a small round core 12 capable of propagating a single mode or perhaps a few modes. The core 12 is surrounded by two claddings: an inner cladding 14 that directly surrounds the core 12, and an outer cladding 16 that surrounds the inner cladding 14. The core 12 and inner cladding 14 are doped with phosphorus and/or other dopants to produce total internal reflection (TIR) at the core-cladding interface by making the refractive index n_{core} of the core 12 larger than the refractive index n_1 of the surrounding inner cladding 14, $n_1 <$

n_{core} Rare-earth ions such as Yb, Nd, Er, Tm, Ho and others, as well as their combinations, are used for activating the core 12 for light amplification. The inner cladding 14 is imbedded into another cladding 16, of even lower refractive index $n_2 < n_1$, for trapping pump light inside the inner core via TIR. Varying the refractive index using various dopants, as described above, is only one way to achieve a prescribed reflection at the core-cladding interface. An alternative approach well known in the existing art is to use photonic bandgap (PBG) or photonic crystal (PC) micro-structures, whereby the signal is trapped in the core due to Bragg scattering from a pattern of holes or rods contained within the cladding.

[0031] Fig. 1b is a simplified schematic of a typical fiber laser system 20. Diode lasers 22 provide pump radiation that is pumped into the inner cladding of the fiber 10, typically at an end of the fiber 10 via pump coupling optics 24. Lasing is excited in the fiber core, usually between a Bragg grating reflector 26 located at the pump entry end of the fiber 10 and an outcoupler 28 at the opposite end. As discussed above, traditional active fibers are not capable of providing simultaneous high power output and good beam quality for high-energy laser applications.

[0032] In accordance with the present teachings, the contradiction between high output power and good beam quality is resolved by means of making a laser that is incapable of propagating and/or amplifying any light except for the single lowest-order transverse mode, even for a large beam cross-section and for conditions of strong thermal and nonlinear optical effects in the active medium. The combination of (a) single-mode guiding for the fast-axis direction, along with (b) resonator mode selection for the orthogonal slow-axis direction, allows for a solution for the problem of power limitation by restricted fiber mode size. Making the mode-selectors purely refractive, in combination with extra tools for fine tuning the resonator mode, allows for a system that is robust to high power operation.

[0033] Fig. 2a is a simplified schematic of a semi-guiding, high aspect-ratio core (SHARC) fiber 30 designed in accordance with an illustrative embodiment of the present disclosure. The novel fiber 30 includes a thin, doped, high aspect-ratio core 32 (the width can exceed the core thickness by a factor greater than 50), buried inside a flexible ribbon-

like glass foil 34. The idea is to accommodate higher power by expanding a conventional single mode or LMA fiber core in one dimension only, instead of two dimensions, as would be the case if one simply increased the radius of a circular core. For a high aspect-ratio core, the coordinate along the expanded dimension is traditionally referred to as the slow axis, while the narrow dimension is denoted the fast axis. The cross-sectional area of the expanded core is specified to maintain a constant and safe intensity level as the total beam power is increased. The damage-limited output power increases proportionally to the increase of the slow-axis core dimension.

[0034] The use of a planar structure for the fiber core 32 allows for an increase in the core cross-sectional area, and therefore output power, without a corresponding increase in the signal intensity. If desired, the claddings and protective jacket can maintain a circular shape even for a high-aspect ratio planar core. In the preferred embodiment, however, both the inner pump-light cladding and the outer cladding are made planar as well. The entire structure of the SHARC fiber 30 looks, then, like a ribbon. SHARC fibers are especially attractive for high-power applications because of the effective heat transfer through the planar surfaces. It is more effective as compared to the radial heat flow in traditional circular-core fibers: the same core volume provides a much larger surface area for the SHARC fiber configuration. Moreover, the thin foil 34 diminishes the path length for heat across the foil 34 along the fast-axis direction, greatly decreasing the active core temperature as compared to bulk active elements.

[0035] In an illustrative embodiment described more fully below, the thin glass foil 34 has an embedded planar core with planar signal claddings and a mode-index matching (MIM) material along the core edges. The MIM material has a refractive index such that the core is optically “open” (i.e. there are no reflections) at the core-MIM material interface, allowing the amplified signal to overfill the active portion of the core in the slow-axis direction. The foil may be covered by low-index outer-cladding material for guiding the pump light and isolating it from the outside environment.

[0036] In the preferred embodiment, the SHARC fiber 30 is made from optical glass (although crystals and other host materials can be used without departing from the scope of the present teachings). Different types of glass can be employed, including silica and

phosphate glasses. The great advantage of a glass material is that there is practically no limit to the core length, and high-quality glass shows very small intrinsic losses. A glass SHARC fiber is still very thin and flexible, retaining all of the advantages of fibers, including the possibility of coiling around a cylinder at packaging, as shown in Fig. 2b. Fig. 2b is a simplified schematic of a SHARC fiber 30 designed in accordance with an illustrative embodiment of the present disclosure, showing the fiber 30 coiled around a cylinder 31.

[0037] High aspect ratio cores have been used to increase the power of edge-emitting semiconductor diode lasers and, more recently, planar waveguide bulk crystalline active slabs and bulk phosphate glass waveguide lasers. See, for example, the following references:

- 1) U.S. Patent 5,651,021. Richard; James and McInnes; Alasdair. *Diode pumped slab laser*, January 18, 1996;
- 2) D. Shepherd, et al. *High-power planar dielectric waveguide laser*. J. of Physics. D: Applied Physics, **34**, 2420-2432 (2001);
- 3) U.S. Patent 6,160,824. Meissner; Helmuth E. and Meissner; Oliver R. *Laser-pumped compound waveguide lasers and amplifiers*, November 2, 1998;
- 4) U.S. Patent 4,791,648. Vojak; Bruce A. and Sheem; Sang K. *Laser having a substantially planar waveguide*, February 4, 1987;
- 5) X.Ye, et al. *Diode Pumped 18W Long Nd:Glass Waveguide laser*. Proceedings of 21st Annual Conf. on Advanced Solid State Photonics, Report **TuB17** (2006).

[0038] These planar structures share the major problem of how to provide and sustain good beam quality operation in the slow-axis direction, a challenge that is addressed by the present disclosure. As is true for all guided laser media (and unguided media as well), good beam quality typically requires that some means be employed to control the modes that are allowed to exist. The present disclosure incorporates mode control that is embodied in both the method and design.

[0039] A key challenge for a SHARC fiber design is maintaining a single-mode output beam. Diffraction processes with respect to the slow and fast axes, respectively, become decoupled from one another when the core width greatly exceeds the core height. In accordance with the present teachings, light remains trapped by total internal reflection across the fast axis, but the propagation along the slow axis looks like planar 2-D diffraction for the guided mode. The beam quality problem can therefore be split and treated separately and differently for the two axes.

[0040] One major departure of the present disclosure from conventional fiber, bulk, and waveguide laser designs is that waveguiding techniques are employed to control the beam quality only in the fast-axis direction. Specifically, along the fast axis the present disclosure achieves single-mode propagation by optimizing the core and cladding dimensions and the refractive-index profile in that direction, and in some cases by optimizing the radius at which the SHARC fiber is coiled. In the slow-axis direction, conventional waveguiding is not used. Instead, this disclosure teaches how to use a combination of waveguiding techniques in the fast-axis direction and several different approaches in the slow-axis direction.

[0041] Slow-axis beam-quality control depends on whether the fiber is being used as a laser oscillator or laser amplifier. For both a laser oscillator and a laser amplifier, the refractive index and the waveguide thickness should both be homogeneous. In addition, for a laser oscillator, an optimized planar resonator operating in the slow-axis direction should discriminate against higher-order resonator modes. Optimization involves specifying the properties of the resonator mirrors (radii of curvature, size, and spacing) and the index profile along the slow-axis direction. For a homogeneous laser amplifier, an input signal with a high beam quality will ensure a high beam quality at the output. Although this homogeneity requirement appears to be common with conventional amplifiers, a SHARC fiber amplifier actually allows a looser tolerance. This looser tolerance arises from the combination of the finite spatial width (in the slow-axis direction) and the long length of the gain stripe, along with the fact that the amplified signal will, by design, overfill the width of the gain stripe. Under these conditions, only that portion of the signal beam that has the highest beam quality will be efficiently amplified along the entire

length of the fiber, while the distorted portions propagate out of the gain region.

Fiber structure

[0042] Fig. 3 is a simplified schematic of a cross-sectional view of an illustrative SHARC fiber 30 designed in accordance with an illustrative embodiment of the present disclosure, including a refractive index map (proportions are not to scale for improved clarity). The SHARC fiber 30 includes a high aspect-ratio core 32 of width w_0 and height (or thickness) h_0 , with a top wide interface 40, a bottom wide interface 42, and two narrow edge interfaces 44 and 46.

[0043] In the illustrative embodiment of Fig. 3, the core 32 is shown divided into three adjacent regions: an active core region 32A of width w_a and refractive index n_a that is doped with a laser-active ion, and passive core regions 32B and 32C on either edge of the active core region 32A having a refractive index n_p . This division is optional, and is shown here to represent the most general case. In practice, the active core region 32A could be as much as 100% of the full core width, or $w_a = w_0$; the relative width of the active core region is a design parameter that can be specified to optimize mode discrimination and/or mode-index matching.

[0044] An inner cladding 34 of height h and width w , comprised of two signal claddings 36 and 38 and two edge sections 50 and 52, surrounds the core 32. The first signal cladding 36 lies above the core 32 in contact with the top interface 40, and the second signal cladding 38 lies below the core 32 in contact with the bottom interface 42. The edge sections 50 and 52 are to the sides of the core 32 and claddings 36 and 38, in contact with the narrow interfaces 44 and 46, respectively.

[0045] In an illustrative embodiment, the laser gain medium is configured as a thin glass foil. This foil has an embedded planar core with planar signal claddings, and a mode-index matching (MIM) material along the core edges. The MIM material has a refractive index such that the core is optically “open” (i.e. there are no reflections) at the core-MIM material interface, allowing the amplified signal to overfill the active portion of the core in the slow-axis direction.

[0046] The inner cladding 34 may be surrounded by an outer cladding 48 having a refractive index n_{oc} . The outer cladding 48 could be a polymer, a glass, or even air, depending on the application. The fiber 30 may also include optional ballast regions 54 and 56, having a refractive index n_b , above and below the signal claddings 36 and 38, respectively, lying between the signal cladding and the outer cladding 48. The homogeneity of the core regions 32 and the shape and flatness of the interfaces 40 and 42 with the signal claddings 36 and 38 should be controlled for the best signal beam quality. However, the homogeneity and shapes of the other regions and interfaces are not so critical and could even be curved.

[0047] In accordance with the present teachings, total internal reflection is used to trap light in the core 32 in the fast-axis direction. The signal claddings 36 and 38 have an index of refraction n_{sc} that is smaller than the indices of refraction $n_a \approx n_p$ of the core 32, such that light in the core 32 is trapped by TIR at the top and bottom interfaces 40 and 42. Alternatively, instead of TIR arising from a core-cladding refractive-index difference, some other mechanism such as a photonic band gap (PBG) structure can be employed to accomplish the guiding function.

[0048] In a preferred embodiment, the numerical aperture (NA) and the thickness h_0 of the core 32 are matched to make the core 32 single-mode in the fast-axis direction. This can be done by satisfying the well known condition, $h_0 \approx \lambda / (2 \Delta n \cdot n_a)^{1/2}$, where λ is the wavelength of the laser and Δn is the core-cladding index difference. Alternatively, the SHARC fiber 30 can be designed analogous to a LMA fiber, whereby the core guides a few fast-axis modes, and the SHARC fiber 30 is wound around a cylinder (as shown in Fig. 2b) at a prescribed coil radius to remove the higher-order modes. For reference, a standard core/cladding combination gives $h_0 \approx 5 - 10 \mu\text{m}$ at a $NA_{core} \approx 0.2$ for single-mode circular fibers. The core size becomes about 20-30 μm for a $NA_{core} \approx 0.05$ for a LMA fiber core that simultaneously guides a few modes and where coiling is used for stripping off higher modes. Similar approximate relations between the core thickness and its NA can be used for the SHARC fiber 30 of the present disclosure. TIR from the lower-index cladding, then, facilitates beam quality with respect to the fast axis in the SHARC fiber 30.

[0049] Given the uniqueness of the slow-axis mode control employed in this disclosure, it is appropriate to describe how this affects the fiber design. Referring to Fig. 3, the best mode control can be obtained when the refractive index is essentially constant across the slow-axis interfaces 44 and 46 of the core 32, because this will minimize reflections. The refractive index n_{MIM} of the mode-index matching (MIM) material 50 and 52 at the edges of the core 32 can be controlled by specifying the appropriate dopant concentrations in those sections 50 and 52 of the fiber 30. It is useful to note that the effective index, n_{mode} , of any given mode is typically not either n_a or n_{sc} , but lies somewhere between those limits. The reason for this is that the electromagnetic fields that constitute the mode extend beyond the core 32 into the signal cladding 36 and 38, and also possibly into the surrounding ballast material 54 and 56. Hence, the objective of minimizing reflections at the edges of the core 32 can be achieved by designing the fiber such that $n_{MIM} \approx n_{mode}$. Thus, the material at the slow-axis edges does not actually function as “cladding”; it is chosen to provide a neutral condition, i.e. to lie in the middle between guiding and anti-guiding to eliminate trapping the light at the edges. The term “modes” for the illustrative SHARC fiber laser design should be clarified: the SHARC fiber has waveguide modes along the fast axis, while having laser resonator modes along the slow axis or having no modes at all for the slow-axis direction if an amplifier configuration is applied.

[0050] In a preferred embodiment, the following two conditions should be fulfilled to reach the design goal of optically open edges: 1) the indices, $n_{sc} < n_{MIM} < n_{ap}$, should all be different, and 2) the guided-mode index n_{mode} should match n_{MIM} , the index at the edges of the core.

[0051] In practice, either imperfect mode matching between n_{mode} and n_{MIM} , or some other possible effects arising at the edges of the core, may be sufficient to cause the formation of modes as opposed to free diffraction in the slow-axis direction. The impact of any such modes can be minimized by ensuring that these undesired modes are leaky, i.e. that the power in such a mode will tend to migrate to the MIM material outside of the core edges, away from the gain stripe. One way to make modes leaky is

to purposely violate the nominal equality between n_{mode} and n_{MIM} by making n_{MIM} slightly larger.

[0052] Any suitable refractive index n_b can be used for the ballast material in sections 54 and 56, immediately above and below the signal claddings 36 and 38, respectively. For example, the signal claddings 36 and 38 can extend to the top and bottom surfaces of the inner cladding 34, which essentially corresponds to $n_b = n_{sc}$. Alternatively, the material for the ballast sections 54 and 56 can be chosen to be the same as the material on the core edges, $n_b = n_{MIM}$. The index for the areas 54 and 56 can also be chosen to lie between those values, or slightly beyond this range. A final choice becomes a matter of performance optimization, manufacturing convenience, and outer cladding requirements for pump guiding. The outer cladding 48 may be used to guide the pump light and also to isolate the pump light from the external environment. The refractive index of the outer cladding, n_{oc} , should be less than the index of any material that constitutes the inner cladding 34.

[0053] Different variants for the core location inside the foil 34 are possible. As an example, the core can be centered in the fiber structure (as shown in Fig. 3), or it can be placed near one of the outer surfaces of the fiber (as shown in Fig. 4a) depending on thermal management and foil doping requirements. Fig. 4a is a simplified schematic showing a cross-sectional view of a fiber 30' designed in accordance with an alternative embodiment of the present disclosure, in which the core 32 is near the lower surface of the fiber structure 30'.

[0054] Another design variant is shown in Fig. 4b. Fig. 4b is a simplified schematic showing a cross-sectional view of a fiber 30'' designed in accordance with an alternative embodiment of the present disclosure. In this embodiment, the guiding core 32 and signal claddings 36 and 38 are embedded within an inner cladding 50' made of a liquid or gel mode-index matched material. In this case, the design exploits the same basic idea of separating mode control for slow and fast axes, but it is based on a liquid or gel for the mode-index matching material. The soft MIM material 50' is fixed in place by a flexible external cover 48' that has a low index to serve as the outer cladding and to trap pump light. The signal claddings 36 and 38 are deposited as thin layers over

large surfaces of the solid-state foil-type core 32.

Laser resonator architectures

[0055] In accordance with the present teachings, the novel SHARC fiber core is disposed within a laser resonator that is specially designed to control the planar resonator mode (in the slow-axis direction) that can propagate along the fiber. Methods for mode selection in a laser resonator with a circular cross-section active medium are well known in the art. See, for example, *Lasers* by A. Siegman, published by University Science Books, Mill Valley, p. 558 – 565, p. 47 – 48, 1986. Similar approaches can be used to control modes in the SHARC fiber of the present disclosure with respect to the slow axis.

[0056] Fig. 5a is a simplified schematic of a laser system 100 designed in accordance with an illustrative embodiment of the present disclosure. The novel laser system 100 forms a laser resonator by positioning two reflectors, a large high reflectivity (HR) reflector 102 and a small, semi-transparent outcoupler 104, at opposite ends of the high-aspect ratio active core 32. The lowest-order planar resonator mode is favored over other higher-order modes by a proper choice of Fresnel number of the planar resonator, which is controlled by the resonator length and the size and/or curvature of the reflectors 102 and 104.

[0057] In a preferred embodiment, the HR mirror 102 and outcoupler 104 are integrated into the glass foil 34 of the fiber to avoid misalignment and surface damage issues and thereby to increase robustness and reliability. The idea here is to make a long and narrow fiber-like foil with the planar resonator along the slow axis having marginal stability, thereby obtaining strong discrimination against higher-order modes. Such a ribbon fiber physically resembles old-fashioned magnetic tapes but made of glass foil.

[0058] In a preferred embodiment, the outcoupler 104 has a low reflectivity of a few percent. Analysis shows that the lasing efficiency for that case remains high even for strong linear loss in the resonator. The linear loss appears either due to material absorption, or due to light scattering by imperfections, including scattering at small

angles that couples the lowest-order resonator mode to the higher-order resonator modes. In a preferred embodiment, the size of the outcoupler 104 is chosen to produce a planar-resonator Fresnel number less than 1. For the embodiment on the Fig. 5a, the HR mirror 102 is implemented as a planar version of a Porro prism retroreflector. Other implementations of a planar HR mirror may also be used without departing from the scope of the present teachings.

[0059] Fig. 5b is a simplified schematic showing an example of an optimized resonator geometry for the illustrative laser configuration of Fig. 5a. The active core width w_a is taken constant along the fiber. Analysis shows that the best discrimination against higher-order modes takes place when: 1) the mode overfills the active portion of the core so that its average size d exceeds about twice the active-core width w_a , and 2) the mode size d exceeds the outcoupler size as well by a factor of about two.

[0060] In an illustrative embodiment, these two conditions can be satisfied by specifying a resonator length L that scales with the core width as $L \geq w_a^2 (\pi n / 4 \lambda)$ and by selecting the outcoupler size to be equal to the core width w_a (in this equation, n is the effective refractive index of the propagating mode). The size d of the lowest-order mode remains, then, almost constant along the fiber too, being about twice the width of both the active core and the outcoupler, $d \approx 2w_a$. As an example, for w_a values of about a few millimeters, which could provide a high-power laser in a range of tens of kilowatts output, the corresponding SHARC fiber length L would range about ten meters.

[0061] Fig. 6 is a simplified schematic of an alternative laser architecture 100' for planar-resonator mode selection designed in accordance with an illustrative embodiment of the present disclosure. In this design, which can provide mode control using a shorter resonator, the planar resonator is implemented as an unstable resonator that incorporates a curved outcoupler reflector 104' to select the lowest-order mode. The outcoupler 104' has a curvature such that the reflected beam is divergent, producing a similar mode selection effect as the resonator of Fig. 5a. The high-reflectivity mirror 102' can be made flat, concave or implemented as a TIR Porro prism reflector (as shown on the Fig. 5a). A planar version of the Porro prism reflector can be easily manufactured

by properly cutting the foil 34.

[0062] An advantage of this laser configuration is that it can be made much shorter than the configuration shown in Fig. 5a. The lasing mode can be made wide even for a short unstable resonator. Standard conditions are known for introducing a strong loss for higher-order modes while maintaining an acceptable moderate loss for the lowest-order mode. The reflector sizes, width of the active core, and reflector curvatures should all be chosen properly for mode selection.

[0063] Another advantage of the resonator configuration shown in Fig. 6 is that it makes it possible to increase the core cross-section area even further without necessarily increasing the foil length. Hence, the unstable resonator configuration can be even more power-scalable than the long cavity configuration.

[0064] Fig. 7 is a simplified schematic of an illustrative multi-sectional laser system 110 designed in accordance with an alternative embodiment of the present disclosure. In this embodiment, two or more separate sections of SHARC fibers 30A and 30B are interconnected sequentially, end to end, by either bulk or integrated focusing optics 112. A different method of mode selection is proposed here. This version does not involve matching the planar-resonator length to the size and curvature of the reflectors. Moreover, the edges of the core need not be optically open (i.e. reflections can be tolerated at the core edges). These differences simplify the fiber core structure and, eventually, ease the fiber manufacturing. The lowest-order mode is selected by designing the interconnections such that a huge propagation loss is induced for any planar core mode except for the lowest-order one.

[0065] In accordance with the teachings of the present disclosure, this is achieved by setting the orientations of the slow axes for neighboring ribbons to be orthogonal to each other. At the same time, the interconnecting optics 112 should be set to focus the output light of one ribbon core into the input of the next ribbon core. For bulk optics, a positive lens 112 can be positioned in the middle between the opposite section ends, which are spaced at a distance S equal to twice the focal length of the lens, $S = 2F$, as shown in Fig. 7. The focal length F is chosen according to the relation $F \approx h_0 d / \lambda$, where h_0 is the active core thickness, d is the slow axis width of

the lasing mode, and λ is the lasing wavelength. Alternatively, an integrated version of the interconnection can be made using a glass gradient index (GRIN) lens. The fiber core ends can be fused to the GRIN lens on opposite sides with orthogonal orientation of the slow axes. The separation S between the fiber section ends is chosen to be equal to the single focal distance F of the GRIN lens, $S = F$, which is determined by a different relation $F \approx h_0 dn / \lambda$, where n is the refractive index of the lens material.

[0066] For both of the above optical realizations, the interconnector 112 transforms the near field from one core output to the far field at the next core input. If the relations for the focal lengths listed above are satisfied, the lowest-order planar-core mode (which is smooth over the entire area $h_0 \times d$ in the near field) is transformed into the focal spot of the same dimensions, $d \times h_0$, but with a rotation of the axes by 90° . The smaller dimension, the fast-axis height h_0 , is transformed by the lens into the larger far-field spot of dimension d , while the larger dimension, the core width w_m , which corresponds to the d/h_0 lower divergence, appears in the focal plane as narrow as $F\lambda/h_0 = d$. Hence, 90° rotated ribbon orientations for the neighboring fibers provide, at the proper choice of the interconnectors, minimal loss for the lowest-order propagating mode, matching input- and output-beam spots accurately.

[0067] The interconnector essentially serves as a spatial filter to cut off the higher modes of the multimode cores that could appear due to fluorescence and ASE, as well as due to aberrations of the lowest mode by thermal and population distortions developed in every SHARC fiber section. If the planar core is manufactured as optically closed by TIR reflections at the edges, waveguide modes appear in the core channel with respect to the slow axis, too. For the slow-axis mode of number M , the angular divergence at the core output is M times above the diffraction limit, $\theta_M \approx M\theta_{Diff} \approx M(\lambda/d)$. As a result, in the far field the corresponding beam spot occupies a dimension $F\theta_M \approx Mh_0$, which is M times broader than the core thickness h_0 . The effective loss factor for core-to-core coupling per every interconnector is about $1/M$ for the M -th mode. This provides a huge round-trip resonator loss factor for the higher-order modes, about $(1/M)^{2N}$, for the sectional flat fiber containing N interconnectors. The beauty of the spatial filter proposed is that it is robust against

high power radiation, since it does not absorb rejected light, but directs it into the cladding.

Pumping schemes

[0068] Both double-clad (cladding-pumped) and single-clad configurations are possible for the SHARC fiber of the present disclosure. In the illustrative embodiment of Fig. 4a, the glass foil 34 itself serves for pump guiding by means of TIR trapping at the outer borders with air (or with a cooling liquid as in the embodiment of Fig. 4b). The signal cladding is transparent for pump light, having a lower refractive index than the other materials within the inner cladding.

[0069] Alternatively, an advanced SHARC design may include an extra outer cladding (as shown in Fig. 3) to minimize pump beam loss by leaking through the sidewalls. The extra cladding can be desirable also if a solid-state cooling technique is used for heat removal through large surfaces of the ribbon to eliminate pump power loss due to partial absorption at reflection from a thermo-optical interface border.

[0070] All pumping techniques that are presently known for fiber lasers can be applied to the SHARC fiber of the present disclosure. In addition, the planar character of the active medium allows for advanced techniques that are not applicable to standard fibers.

[0071] Fiber lasers are typically pumped through the fiber ends. One obvious disadvantage of this standard method is a thermal overload of the splicing points and/or tapered multi-core bundles that combine the pump power into the common inner cladding. Overheating occurs due to the concentration of the pump power in a limited and finely structured area.

[0072] To solve this problem, alternative side-pumping schemes have been described, involving multiple pigtailed diode bars that are distributed along the fiber length. The fiber-pigtail ends were polished at a high angle of about 85° to the fiber axis, and optically connected to the outer cladding at the same angular tilt to match the NA of the pump-guiding channel. Using such multiple distributed pump-entry points allows

one to control the pump intensity and, hence, the thermal load along the fiber length by proper choice of location and relative pump power at the pumping points. In particular, the thermal load can be made essentially homogeneous along the fiber comparing to the single-entry end-pumping case. A similar pumping scheme can be applied to the present disclosure. For more detailed descriptions of side-pumping schemes, see the following references:

A High-Brightness Laser Beam From a Phase-Locked Multicore Yb-Doped Fiber laser Array by P. K. Cheo, *et al.*, IEEE PTL **13**, 439 (2001);

Recent Advances in High-Power Multicore Fiber Lasers by P. K. Cheo, *et al.*, Proceedings of SPIE, Vol. 5335, p. 106-115 (2004); and

Nonlinear mode competition and phasing in Yb-doped fiber amplifier by E. Bovhove, *et al.*, Proceedings of SPIE, Vol. 5335, p. 151-157 (2004).

[0073] Fig. 8 is a simplified schematic of a fiber assembly 120 with a novel pumping scheme designed in accordance with an illustrative embodiment of the present teachings. The fiber assembly 120 includes a SHARC fiber 30, as described above, with a plurality of pump-entry fiber pigtails 122 for coupling pump energy to the fiber 30.

[0074] Fig. 8 shows just one of a large number of pump-entry pigtails 122. In accordance with the present teachings, the fiber pigtails 122 each include a rectangular or high aspect ratio core 124 and look like freeway “on-ramps”, coupling pump light into the edges of the fiber 30. Pump-diode light can be coupled into the on-ramp fiber pigtails 122 using techniques similar to those known in the art for coupling diode laser radiation into fiber pigtails. The difference in this case is that the pigtail on-ramps 122 are an integral part of the SHARC fiber 30 and also have rectangular cores 124 to match the anamorphic properties of the diode pump beams. These pump on-ramps 122 could be located along both edges of the fiber 30, and for typical fiber parameters (core and cladding sizes, laser-ion concentration, etc.) the pump absorption length can be as short as about 0.5 m.

[0075] The output of an edge-emitting diode bar also has a very high aspect ratio that typically requires reformatting the beam shape to match the conventional round core of typical pigtail fibers. The high aspect ratio pigtail fiber 122 of the present disclosure allows one to eliminate or simplify reformatting optics, up to direct butt coupling of the bar to the pigtail core.

[0076] Fig. 9 is a simplified schematic of a fiber assembly 120' with an alternate pumping scheme designed in accordance with an illustrative embodiment of the present teachings. In this embodiment, glass prisms 60 are used to couple pump energy into the fiber 30. (Only one prism 60 is shown in Fig. 9.) The prisms 60 are placed in optical contact with the large surfaces of the inner cladding 34 (rather than attempting to couple the pump light through the outer cladding), or glued to it, and are distributed along the length of the fiber 30. The pump-coupling prisms 60 should be specially designed to be protected against leaking already coupled pump light back to the prism 60. For direct pumping from diode-laser bars, an anti-reflective (AR) coating can be deposited over the entire prism face except for a narrow line near the prism edge, through which the prism is placed in contact with the foil surface. The pump beam is then focused at a slanted angle as a narrow stripe onto the uncoated portion near the edge.

[0077] Optionally, a prism 60 may also be used to couple pump power that is delivered from diode bars through a fiber pigtail 62. As shown in Fig. 9, the prism 60 includes a few pigtail fibers 62 fused inside the prism 60 at a large angle to the polished prism surface to be attached to the foil surface. The pigtail fibers 62 can be conventional large, multi-mode fibers. The numerical aperture (NA) of the pump-fiber core should be no more than half of the NA of the planar pump guiding channel in the foil. The coupled fiber tilt angle with respect to the main core should be close to the NA of the pump fiber core to maximize coupling efficiency. In this embodiment, the perpendicular face of the prism 60, right behind the pump fiber tip as shown in Fig. 9, is polished out to the level of the pigtail fiber core side. The thickness h of the inner cladding 34 should be chosen to be less than the pump pigtail fiber diameter. This minimizes pump loss due to reflection of the pump from the inner

cladding 34 back into the prism 60. The remaining portion of the contact face of the prism 60, beyond the pump core footprints, should be coated with a HR coating 64 (for large angles of incidence) to protect the prism 60 against back coupling of pump light from the upstream prisms. The pumping prisms 60 should be positioned beyond the planar area of the active core 32 near the fiber sides. This helps to avoid signal loss due to outcoupling light back into the prisms 60, and to protect the diode bars.

[0078] In the illustrative embodiments of Figs. 8 and 9, the on-ramp fibers 122 and the prisms 60 are oriented facing the HR reflector 102 of the planar laser resonator to protect the fiber pigtails 62 against back coupling of the pump radiation. With this orientation, the main stream of the pump power is practically unidirectional, propagating downstream from the outcoupler end of the resonator to the HR reflector 102. The downstream pump cannot be back-coupled to the prisms 60 due to the protecting reflector 64 and due to the pigtail fibers' tilt orientation.

[0079] However, residual upstream pump energy that returns by the HR mirror 102 can still be coupled to the diode bars. To secure diode bar protection, the on-ramp entry regions and the pumping prisms can be concentrated closer to the outcoupler 104. This provides strong pump absorption on the way from the pumping points to the HR 102 and back. It results also in a concentration of pump energy closer to the outcoupler 104, where maximal power extraction is desired.

[0080] In the prism coupling embodiment, the input pump beams' orientation can be tilted relative to the laser resonator axis to control the pump absorption rate inside the foil. Stronger tilts for the prism located at the side of the core may increase the absorption rate per unit length of the fiber because of the longer path length where it crosses the core. The same method can be used for the preferred on-ramp implementation of the pumping scheme.

Fine tuning and additional improvements

[0081] In the illustrative embodiments described above, single-mode guiding methods in the fast-axis direction on one hand, and resonator and/or gain-guiding methods in the slow-

axis direction on the other, are used to achieve beam quality with the SHARC fiber laser. Alternatively, the SHARC fiber of the present disclosure can be designed to allow a few fast-axis modes (by, for example, increasing the thickness h_0 of the core), and then stripping methods can be employed to remove the higher-order modes. Coiling round-core fibers with a favorable coil radius to strip higher-order modes out of the core is a known method of mode control for fiber lasers. See, for example *Single-mode operation of a coiled multimode amplifier*, by J. P. Koplow *et al.*, Opt. Lett. **25**, 442 (2000).

[0082] The technique of coiling a fiber around a cylinder to strip higher-order modes could also be applied to the SHARC fiber of the present disclosure. Coiling maintains the single lowest-order mode propagation for the larger thickness of a few-mode core by imposing a relatively strong bend loss to the higher-order modes. The increased thickness h_0 of a few-mode guiding core may be very attractive if targeting higher output power applications.

[0083] The slow-axis resonator mode should also be tuned to compensate for manufacturing inaccuracies of the fiber. Slow-axis mode tuning can be used to compensate for any distortions induced by thermal gradients and the non-uniform inversion density in the gain medium. Entirely new options appear for slow-axis mode control due to manufacturing flexibility, together with the mechanical flexibility of the planar core fibers. In accordance with the present teachings, mode control tuning can be achieved by varying the planar core thickness and/or by twisting the planar core.

[0084] The thickness, h_0 , of the planar core can be varied to control the slow-axis resonator Fresnel number and the mode structure. For adiabatic propagation of the trapped fast-axis mode, smooth thickness variations in the planar core effectively correspond to variations of phase velocity of the mode. Thinner regions allow a faster propagation speed of light along the fiber axis (lower effective index of the mode), while thicker regions slightly delay the light (larger mode index). This is because the phase velocity of the fiber modes increases for thinner waveguides, due to the fact that the modes then penetrate farther into the lower-index cladding. As a result, if the core is thicker at the middle of the ribbon than at the edges, the corresponding portion of

the fiber demonstrates a planar focusing effect. If the core is thinner in the middle, the effective planar lens is negative. By applying a judicious profile to the core thickness, the shape of which can be deliberately controlled, the effective lens of the “cool” unpumped resonator can be pre-set to compensate for further light-induced thermal lensing that might obtain for the “hot” pumped resonator under operational conditions.

[0085] The SHARC fiber laser system may also be tuned by adding a mechanism for applying local and/or distributed twists of the fiber ribbon to create and control an effective negative planar lens in the laser resonator. The effective negative lens power is approximately proportional to the twist angle. A twisted portion of the flat fiber provides a defocusing effect as compared to the same fiber if it were not twisted. The reason is that the optical path near the ribbon edges becomes geometrically longer compared to the path along the fiber axis. The resulting defocusing power of this “twisted fiber lens” can be easily and smoothly tuned by controlling the twist angle. Distributed twisted regions operate as a planar version of the gradient index (GRIN) lens, but with adjustable focal strength.

[0086] The beauty of the twist method is the possibility of continuously controlling the effective Fresnel number of the planar resonator in real time, using appropriate feedback to achieve resonator optimization. This option is especially attractive for compensating thermal lensing and optical distortions arising from variations in the population inversion, since light induces both lensing phenomena, and, hence, they both vary together with the pump power and power-extraction conditions. Twists are especially effective for fine-tuning the lens compensation – to eliminate errors of the pre-set lens, and to compensate for dynamic lens variations.

[0087] In a preferred embodiment, the basic foil material around and outside of the core should be fabricated using a selectively absorbing dopant to absorb leaked light at the lasing wavelength. The dopant should be spectrally selective, having no absorption band at the pump wavelength. As an example, Sm could be the absorber for an Yb-doped active core. The absorber helps to reduce the gain for higher-order modes, which are stripped out through the core-cladding interfaces due to coiling. In

addition, it helps to absorb the leaks through the edges of the optically open core. In the multi-sectional configuration shown in Fig. 7, it also reduces the gain for the higher-order modes that are rejected from the core of the next fiber section by the fiber-to-fiber interconnector. In addition, the absorber helps to reduce amplified spontaneous emission (ASE) that can be collected and accumulated in the pump-guiding foil. Leakage from the core to the foil can negatively impact laser efficiency if no cladding absorption is available. Specifically, unabsorbed ASE would be kept inside the foil by TIR reflections from the foil boundary, allowing this ASE to cross the active core multiple times and stealing a portion of pump power stored as population inversion.

[0088] In a preferred embodiment, the outcoupler end of the fiber is attached to a bulk piece of optically homogeneous glass to form a coreless end-cap. As is well known in the existing art, such an end-cap allows the beam to expand to a larger size, due to the fast-axis divergence. The larger beam size reduces the optical intensity at the output surface of the end-cap, thereby reducing the likelihood of optical damage at that surface. Since the beam divergence is so different in the fast- and slow-axis directions, the length L_{ec} of the end-cap piece allows the control of the output beam shape even for cores having a very high aspect ratio. For example, one can generate a beam with a 1:1 aspect ratio if the length is chosen as $L_{ec} = dnh_0/\lambda$.

[0089] The angular divergence of the single-mode beam radiated from the planar core is very different for the fast and slow axes, because of the high aspect ratio of the near-field intensity profile. External cylindrical collimation optics are usually used to equalize the divergence at both axes for edge emitting diode lasers. See, for example, References 1-4 listed above. An external cylindrical collimating lens set right behind the end-cap after free-space propagation can be used for the planar core fiber output as well. In a preferred embodiment, the end-cap is fabricated to have an exit surface curved with a radius $R \approx (n-1)L_{ec}$ along the fast axis coordinate to collimate the generated beam without the need for external lenses.

[0090] In a preferred embodiment, a partially reflecting outcoupler that terminates the planar resonator (see Fig. 5a) can be formed by applying a dielectric coating with a

specified reflectivity to a portion of the end-cap exit surface; the remainder of this surface will be antireflection-coated. The size and reflectance of the dielectric coating outcoupler will depend on the specific operational requirements of the SHARC fiber laser.

[0091] As an alternative, it is also possible to produce a partial reflector by means of V-grooves written into the large side surface of the SHARC fiber. V-grooves are well known in the existing art, and they can be formed, for instance, by scanning a focused CO₂ laser beam. The V-grooves should be oriented perpendicular to the fiber ribbon axis, and they could cover the entire width of the active core (in the slow-axis direction). The grooves can be made also on the opposite surfaces of the foil, one against another. The depth of the V-grooves is chosen to barely reach the core; it should be fine-tuned to provide the desired reflectivity of the outcoupler.

[0092] Additional components may also be integrated into the body of the fiber. For example, these additional components could include one or more of the following: reflectors for forming the laser cavity, end-caps, an optical modulator, polarization maintaining elements, polarization control elements, Bragg gratings, etc.

SHARC fiber as a high power amplifier

[0093] In addition to being used to form a fiber laser, the SHARC fiber gain medium of the present disclosure can also be used as a high-power single-mode optical amplifier (if the HR and outcoupler resonator reflectors are absent) in a single- or multi-pass configuration. Without the resonator components, the resonator-based mode-selection mechanism cannot function. Instead, mode control can be achieved via a gain guiding mechanism as described in *Propagation Modes in Gain-Guided Optical Fibers*, by A. E. Siegman, J. Opt. Soc. Am. A **20**, 1617 (2003).

[0094] According to this mechanism, a high-quality output beam can be produced from a high-quality input beam by ensuring that an optimum slow-axis spatial overlap of the input signal beam with the narrow gain stripe of the amplifying core is maintained along the entire length of the fiber. Under these conditions, only that portion

of the signal beam that has the highest beam quality will be efficiently amplified along the entire length of the fiber, while the distorted portions propagate out of the gain region.

[0095] A preferred method of gain guiding for the SHARC fiber is overfilling the core stripe by the input beam with respect to the slow-axis direction. In addition, the core length is chosen to exceed the Fresnel length corresponding to the input beam size. For such conditions, the higher modes, which can be excited by scattering by core imperfections or by deflection via core lens, experience much lower gain because of angular spreading and weak overlap with the gain stripe. At the same time, the high beam quality portion should stay compact to maintain good overlap with the core over the entire length.

[0096] If necessary, this mode-control mechanism can be facilitated using a pre-set planar lens produced by profiling the core thickness across the ribbon for coarse compensation of the thermal and population lens across the slow axis (as discussed above). In addition, ribbon twisting (as discussed above) can be used for precise compensation of any residual lensing and for dynamic compensation of the portion of the lens optical power, which is dependent on the pumping load.

[0097] Thus, in applications requiring an amplifier function, the gain medium is employed without the additional mirror and outcoupler. In this case the slow-axis beam quality of the output beam depends on that of the input beam and on the homogeneity of the fiber gain medium. The beam quality also benefits from the combination of the finite spatial width (in the slow-axis direction) and the long length of the gain stripe, along with the fact that the amplified signal will, by design, overfill the width of the gain stripe.

[0098] The multi-sectional axes-flipped design of the flat fiber, as shown in Fig. 7, can also be used as an optical-fiber power amplifier. Such an amplifier provides effective clean up of the propagating light by spatially filtering at the interconnectors. In fact, it is capable of amplifying the single lowest-order mode even when multimode input is presented. In a preferred embodiment, both a pre-set and a twist-induced lens can be used in separate sections of the compound amplifier as a method of loss control for the amplified beam. Loss control is useful for amplifier performance optimization, and also as a simple non-electrical method for controlling the output

power at constant pump conditions.

[0099] Electrodes can be deposited on opposite surfaces of the SHARC fiber ribbon over its length to control and to modulate the phase of the amplified radiation. A control voltage differential applied to the opposite surfaces results in density modulation due to a ponderomotive force inside isotropic glass. Having no mechanical resistance from the slow-axis direction, only minor mechanical compression is required for deep phase modulation if the compressed area is distributed along the entire fiber length. The control voltage can be modulated over a broad bandwidth, up to 10 MHz, which is determined by the propagation time of a sound wave across the fast axis.

[0100] The SHARC fibers of the present disclosure can also be used as an array of parallel amplifiers or oscillators to increase the output power of a light source. For incoherent combining of the multiple fiber channels, the output beams should be aligned parallel resulting in proportional increase of overall power. Brightness stays the same here as for each individual channel, or below this value.

[0101] For coherent combining, the brightness can be increased in proportion to the number of channels. The brightness increase, as well as the beam wavefront control option, requires separate, active, phase control for every lasing or amplifying channel.

This can be achieved by controlling the relative phases in different parallel amplifying SHARC fiber channels, which are seeded by splitting the radiation of a common single mode master oscillator. Phase control can be applied for forming a combined beam with a flat phase front by compensating static and dynamic phase increments gained in different channels. Phase control can also be used for steering the output beam and for pre-aberration of the array output to optimize its power delivery to a target.

[0102] A combined-cavity laser source can be formed using a few parallel SHARC fiber channels with strong optical coupling between them to make the laser oscillate on a single supermode by means of known supermode selection techniques. A single supermode output corresponds to a spatially coherent beam. However, if the output beam consists of a combination of supermodes, then the spatial structure of the combined beam will have a temporal variation at a bandwidth given by the phase

noise in the separate channels.

[0103] Thus, the present teachings introduce a novel laser gain medium that configures the active medium as a semi-guiding high aspect ratio core fiber, in which a thin, doped planar core is buried inside a flexible ribbon-like glass foil. The optically pumped amplifying core is designed to provide optical guiding in one direction only, across the small coordinate of the core (fast axis). If the size of the core in the fast-axis direction is big enough to allow more than one mode, the higher-order modes can be stripped out by forming the fiber into a coil with a specific radius that causes the latter modes to have a greater loss. In either case, the core is deliberately made non-guiding in the orthogonal transverse direction, aligned with the wide foil-plane coordinate (slow axis). Single-mode operation for this axis is achieved by means of additional selectors that can be integrated into the same foil, or by a gain-guiding discrimination mechanism. Three illustrative selectors were described: (1) a HR mirror and compact outcoupler designed to form a long planar laser resonator with a Fresnel number below unity, (2) a HR mirror and curved outcoupler disposed to form a short unstable resonator, and (3) a multi-sectional design including a sequence of SHARC fibers with a 90 degree flip of the core plane from one fiber to the next, which are interconnected end to end with optics that transform the near-field profile from an output of one fiber to the far-field profile at the input of the next fiber. All mode selectors are made purely refractive, adding no absorption and hence, no heating to the fiber.

[0104] The SHARC fiber of the present disclosure is scalable in output power with a high beam quality to much higher levels than conventional designs. Analysis shows that the novel SHARC fiber laser is capable of generating up to 100 kW of high beam quality light per channel, providing maximal power efficiency at small size and light weight. As an example, for a single-mode channel with core thickness $h_0 \approx 20 \mu\text{m}$, and assuming a wavelength of $1 \mu\text{m}$, the SHARC fiber resonator length L should be chosen according to the scaling law $L \approx 1.2 \cdot 10^4 w_a^2$, where w_a is the width of the active core stripe and of the outcoupler. As a quantitative example, a 5 mm core width corresponds to a 30 m long resonator. The same analysis demonstrates that for an active core width w_a more than 1.5 mm, the output power of the flat fiber laser is

limited by the optical damage inside the fiber core. This limitation for the high power end results in the following scaling law: $P_{out} \approx (2h_0d) \cdot I_{max}$, where $2h_0d$ represents the area of the amplified beam, and I_{max} should be chosen as a fraction of the threshold intensity for bulk optical damage in the fiber core. If I_{max} is taken as a quarter of the damage threshold to guarantee safe operation, then for a CW laser/amplifier $I_{max} \approx 0.5 \text{ W}/\mu\text{m}^2$. As an example, for a $20 \mu\text{m}$ by 5 mm core size, the expected maximal output power per single SHARC fiber channel is about 100 kW . For such a case, the output beam size along the slow axis is about 1 cm .

[0105] For an active core width w_a less than 1.5 mm , SHARC fiber laser/amplifier operation will probably be limited by the available heat sink density, not by optical damage. This is because, for such core widths, the heat flow density Q through the ribbon surfaces will exceed the practical limit of about $100 \text{ W}/\text{cm}^2$. However, for wider core strips with w_a greater than 1.5 mm , the heat-sink density should be less than $100 \text{ W}/\text{cm}^2$ if the output beam stays below optical damage threshold. Analysis shows that the required heat flow Q rapidly decreases as the second power of the core width: $Q \approx (P_{out}/2Lw_a)(1-\eta)/\eta \propto 1/w_a^2$. As an example, for 100 kW output power with a 5 mm wide core channel, the heat sink density drops down below $10 \text{ W}/\text{cm}^2$ making thermal management possible by air cooling. The possibility of employing air cooling allows laser designers to eliminate the heavy and expensive water cooling heat exchanger, and this makes the SHARC fiber laser design even more attractive.

[0106] Thus, the present disclosure has been described herein with reference to a particular embodiment for a particular application. Those having ordinary skill in the art and access to the present teachings will recognize additional modifications, applications and embodiments within the scope thereof.

[0107] It is therefore intended by the appended claims to cover any and all such applications, modifications and embodiments within the scope of the present disclosure.

STATEMENT OF INDUSTRIAL APPLICABILITY

[00100] The appended claims have applicability to laser systems, and more specifically, to systems and methods for generating and amplifying laser energy.

CLAIMS

WHAT IS CLAIMED IS:

1. A laser system (100) comprising:
 - an active core (32) having a high aspect ratio cross-section with a fast-axis dimension and a slow-axis dimension;
 - first and second signal claddings (36, 38) positioned in contact with said core (32) to form reflective boundaries at fast-axis boundaries (40, 42) of said core (32); and
 - a material (50, 52) positioned in contact with said core (32) to minimize reflections at slow-axis boundaries (44, 46) of said core (32).
2. The laser system of Claim 1 wherein said core (32), claddings (36, 38), and material (50, 52) form an optical fiber.
3. The laser system of Claim 1 wherein said claddings (36, 38) have a refractive index less than a refractive index of said core (32) such that energy in said core (32) is trapped by total internal reflection at said fast axis boundaries (40, 42).
4. The laser system of Claim 1 wherein said claddings (36, 38) include a micro-structure adapted to trap light in said core according to principles of photonic bandgaps.
5. The laser system of Claim 1 wherein a thickness of said core (32) is chosen to control a fast-axis mode profile and a number of fast-axis modes propagating in said core (32).
6. The laser system of Claim 5 wherein said thickness is matched to a numerical aperture of said core (32) such that said core (32) is a single-mode planar waveguide in said fast-axis direction.

7. The laser system of Claim 1 wherein said material (50, 52) has a refractive index that is approximately equal to an effective refractive index of a mode propagating in said core (32).

8. The laser system of Claim 1 wherein said system (100) further includes a high reflectivity mirror (102) and an outcoupler (104) positioned at opposite ends of said core (32) to form a laser resonator adapted to control modes along said slow axis of said core (32).

9. The laser system of Claim 8 wherein said mirror (102) and outcoupler (104) are integrated into a glass foil (34) surrounding said core (32), claddings (36, 38), and material (50, 52).

10. The laser system of Claim 1 wherein a thickness of said core (32) is varied to provide an effective lens adapted to compensate for thermal lensing effects.

11. The laser system of Claim 2 wherein said system (100) further includes a mechanism for applying local and/or distributed twists of said fiber (30) to create and control an effective negative planar lens.

FIG. 1a
(Prior Art)

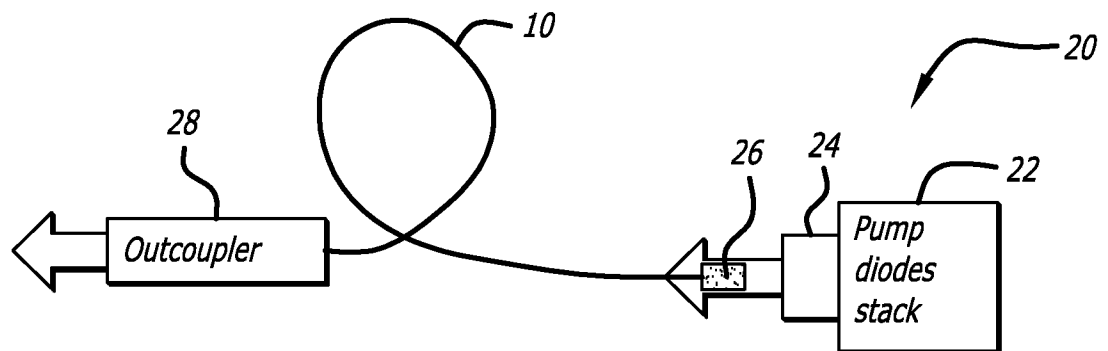
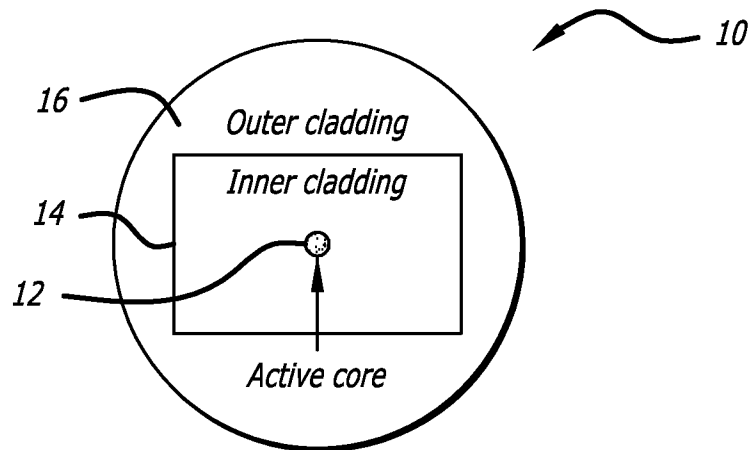


FIG. 1b
(Prior Art)

2/6

FIG. 2a

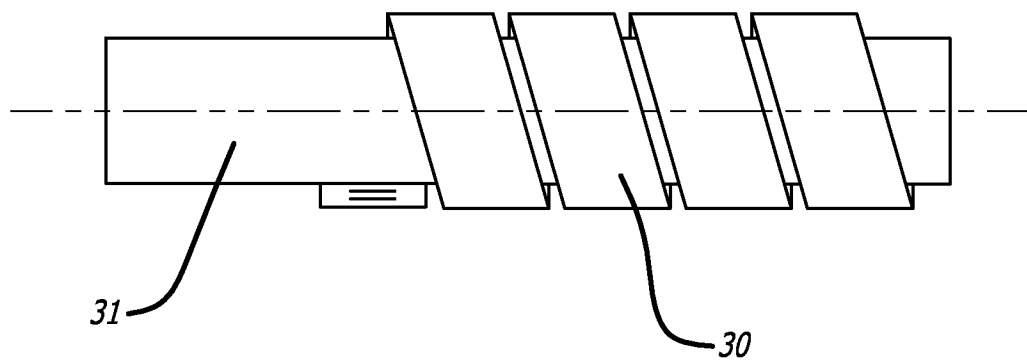
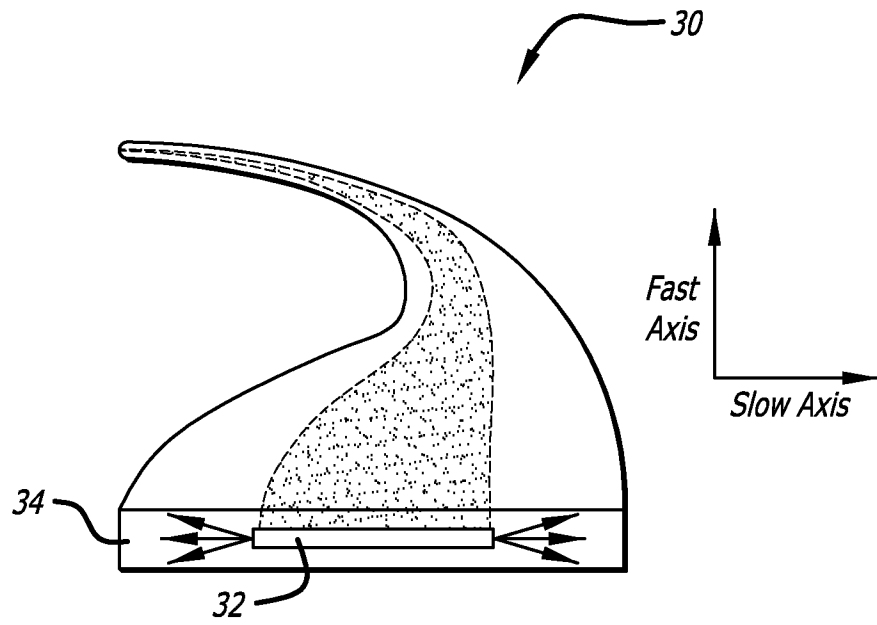
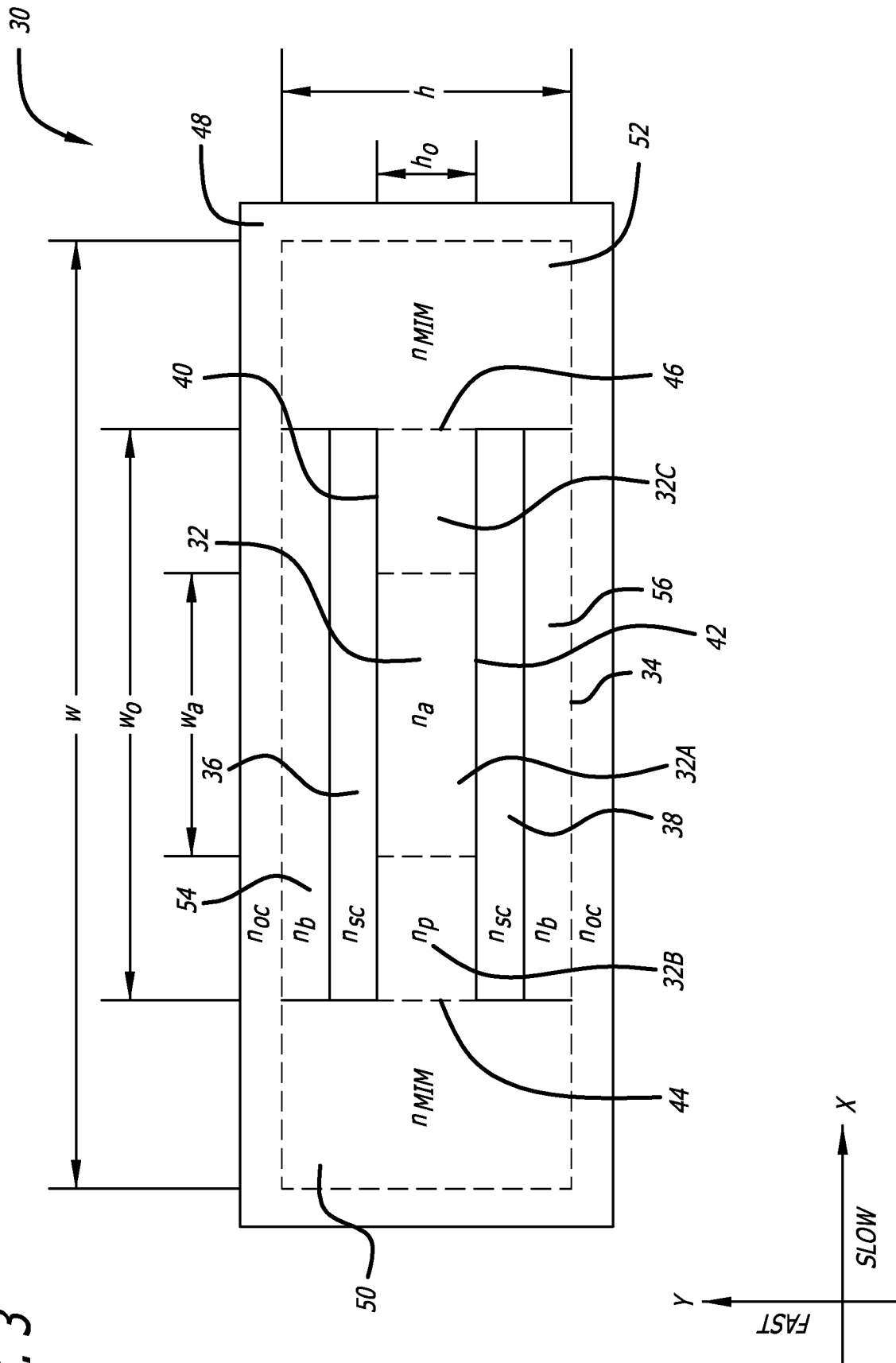


FIG. 2b

FIG. 3



4/6

FIG. 4a

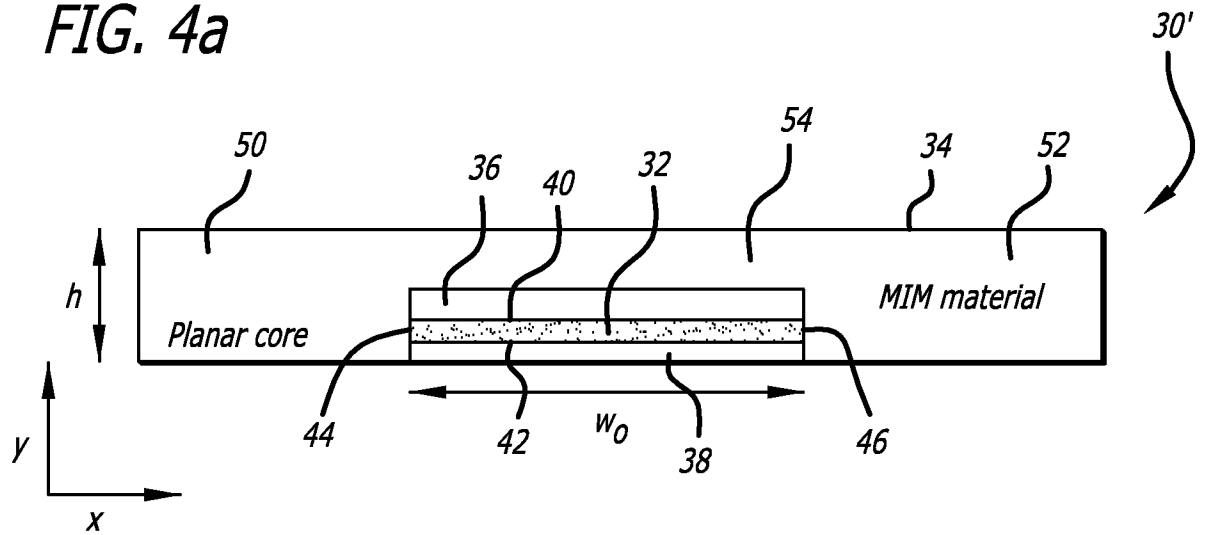
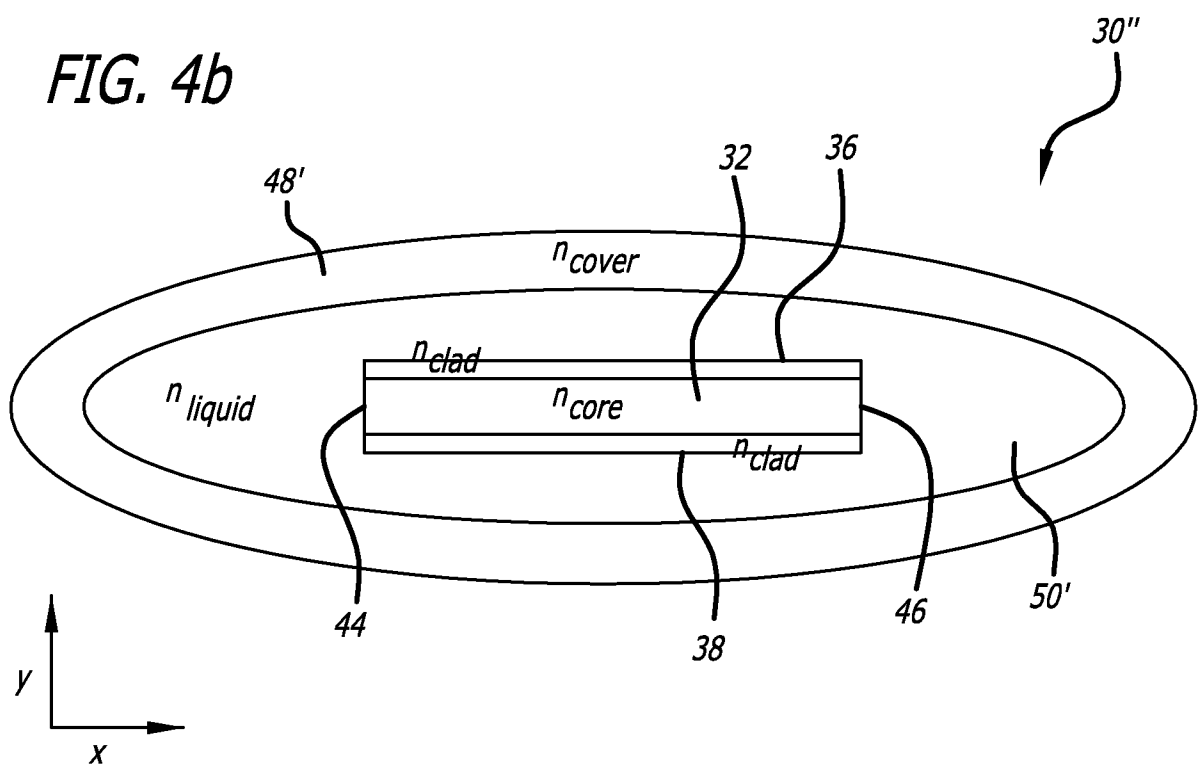


FIG. 4b



5/6

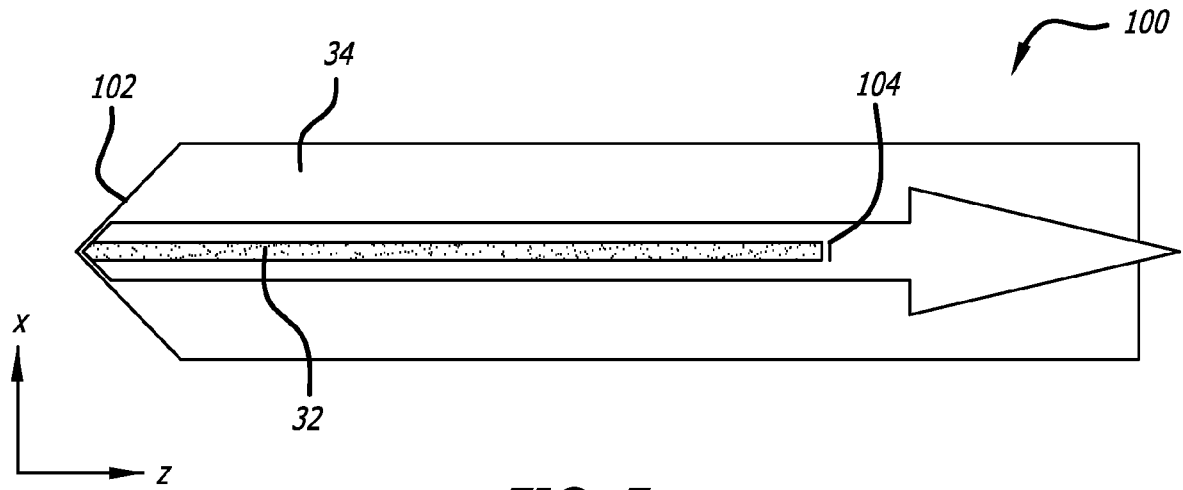


FIG. 5a

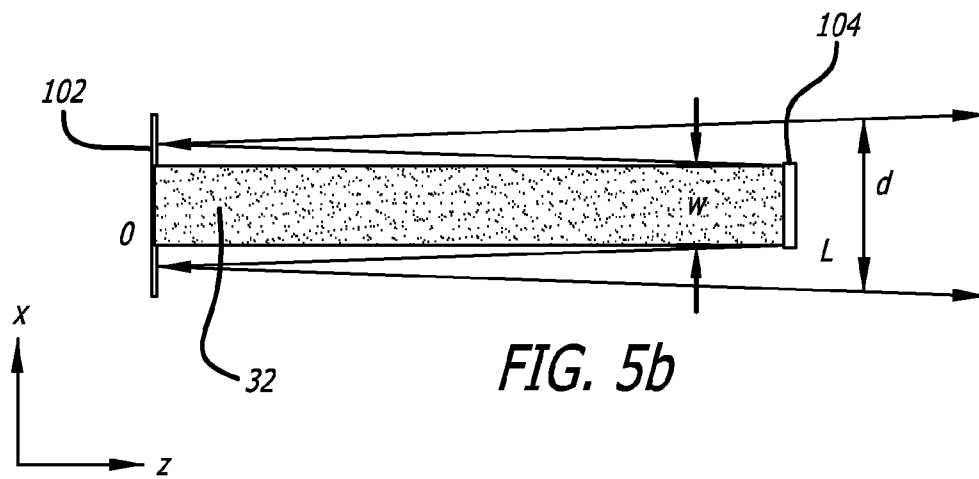


FIG. 5b

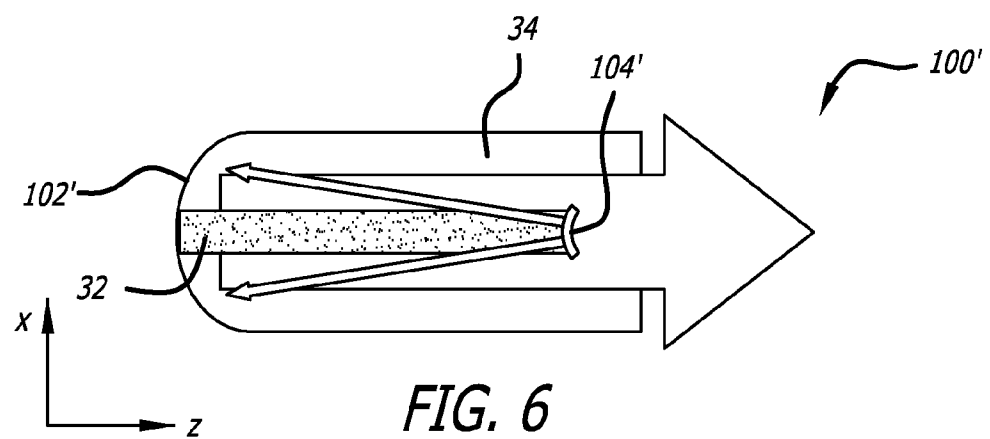


FIG. 6

FIG. 7

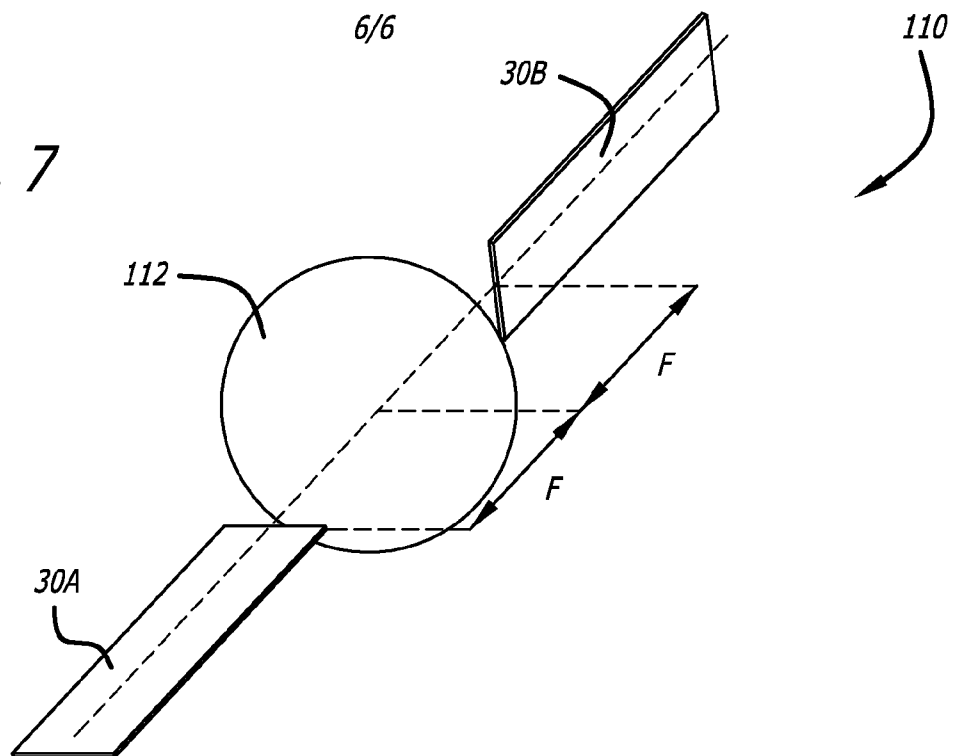


FIG. 8

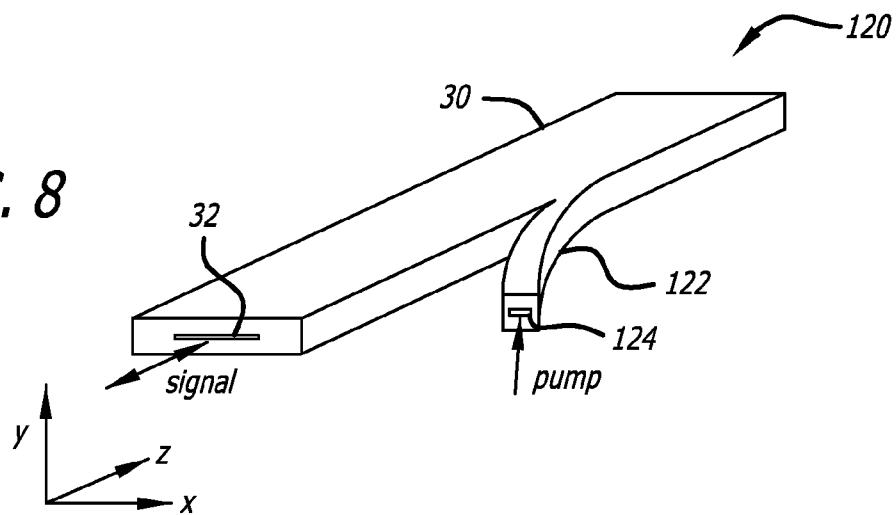
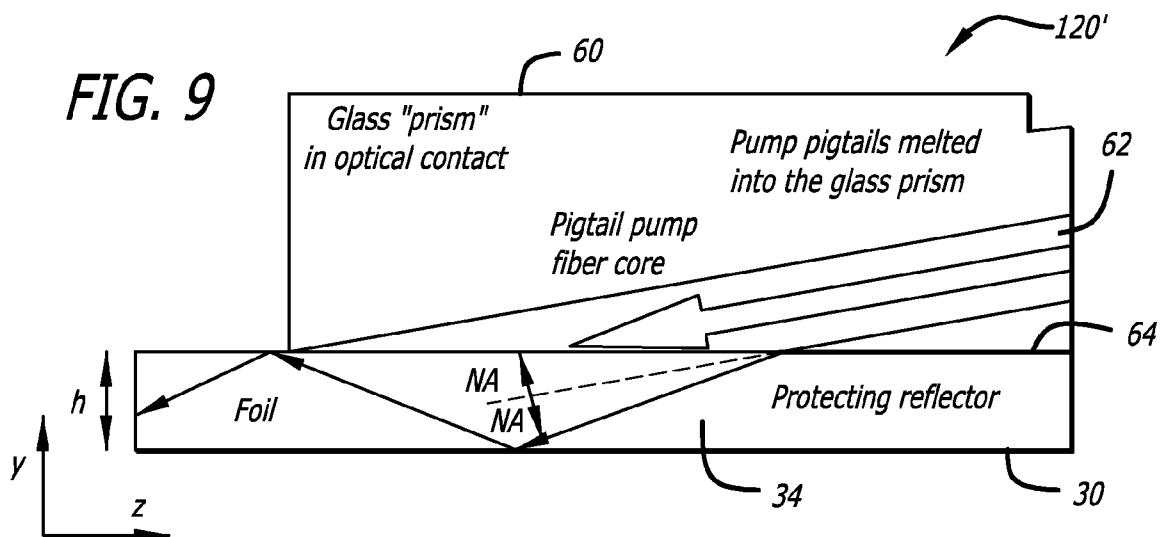


FIG. 9



INTERNATIONAL SEARCH REPORT

International application No

PCT/US2008/083734

A. CLASSIFICATION OF SUBJECT MATTER
INV. H01S3/067 H01S3/063

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
H01S

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal, INSPEC, WPI Data, COMPENDEX

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	WO 00/27000 A (MAXIOS LASER CORP [US]; MEISSNER HELMUTH E [US]; MEISSNER OLIVER R [US]) 11 May 2000 (2000-05-11) cited in the application the whole document	1-11
A	EP 0 277 768 A (AMOCO CORP. [US]) 10 August 1988 (1988-08-10) cited in the application the whole document	1-11
A	WO 94/24734 A (COMMW OF AUSTRALIA [AU]; RICHARDS JAMES [AU]; MCINNES ALASDAIR [AU]) 27 October 1994 (1994-10-27) cited in the application the whole document	1-11
----- -/--		

☒ Further documents are listed in the continuation of Box C.

☒ See patent family annex.

* Special categories of cited documents :

A document defining the general state of the art which is not considered to be of particular relevance

E earlier document but published on or after the international filing date

L document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

O document referring to an oral disclosure, use, exhibition or other means

P document published prior to the international filing date but later than the priority date claimed

T later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

X document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone

Y document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

G document member of the same patent family

Date of the actual completion of the international search

27 January 2009

Date of mailing of the international search report

09/02/2009

Name and mailing address of the ISA/

European Patent Office, P.B. 5818 Patentlaan 2
NL - 2280 HV Rijswijk
Tel. (+31-70) 340-2040,
Fax: (+31-70) 340-3016

Authorized officer

Lendroit, Stéphane

INTERNATIONAL SEARCH REPORT

International application No

PCT/US2008/083734

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	SHEPHERD D P ET AL: "High-power planar dielectric waveguide lasers" JOURNAL OF PHYSICS D (APPLIED PHYSICS) IOP PUBLISHING UK, vol. 34, no. 16, 21 August 2001 (2001-08-21), pages 2420-2432, XP002511994 ISSN: 0022-3727 cited in the application the whole document	1-11
A	US 7 193 771 B1 (SMITH DUANE D [US] ET AL) 20 March 2007 (2007-03-20) figure 15	1-11
A	DE 102 11 352 A1 (IMRA AMERICA INC [US]) 26 September 2002 (2002-09-26) figure 1	1-11
A	US 2004/095968 A1 (AVIZONIS PETRAS V [US] ET AL) 20 May 2004 (2004-05-20) figure 9d	1-11
A	GB 2 366 447 A (SOUTHAMPTON PHOTONICS LTD [GB]) 6 March 2002 (2002-03-06) figure 3	1-11
A	WO 2004/066458 A (TRUMPF INC [US]; TRUMPF WERKZEUGMASCHINEN GMBH [DE]; SCHLUETER HOLGER) 5 August 2004 (2004-08-05) figure 2b	1-11
A	US 2002/024727 A1 (WILCOX RUSSELL B [US] ET AL WILCOX RUSSEL B [US] ET AL) 28 February 2002 (2002-02-28) figure 1	1-11

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/US2008/083734

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
WO 0027000	A	11-05-2000	AU 1461400 A US 6160824 A	22-05-2000 12-12-2000
EP 0277768	A	10-08-1988	AT 107438 T AU 589311 B2 AU 1114188 A CN 88100570 A DE 3850131 D1 DE 3850131 T2 IE 880296 L JP 2851040 B2 JP 63222492 A US 4791648 A	15-07-1994 05-10-1989 11-08-1988 24-08-1988 21-07-1994 22-09-1994 04-08-1988 27-01-1999 16-09-1988 13-12-1988
WO 9424734	A	27-10-1994	CA 2160998 A1 EP 0698307 A1 US 5651021 A	27-10-1994 28-02-1996 22-07-1997
US 7193771	B1	20-03-2007	NONE	
DE 10211352	A1	26-09-2002	JP 2002323636 A JP 2005203809 A JP 2008158547 A US 2005232313 A1 US 2002172486 A1	08-11-2002 28-07-2005 10-07-2008 20-10-2005 21-11-2002
US 2004095968	A1	20-05-2004	AT 398849 T AU 2003285158 A1 EP 1563576 A2 WO 2004047339 A2	15-07-2008 15-06-2004 17-08-2005 03-06-2004
GB 2366447	A	06-03-2002	GB 2335074 A	08-09-1999
WO 2004066458	A	05-08-2004	EP 1586144 A2 JP 2006516811 T	19-10-2005 06-07-2006
US 2002024727	A1	28-02-2002	NONE	