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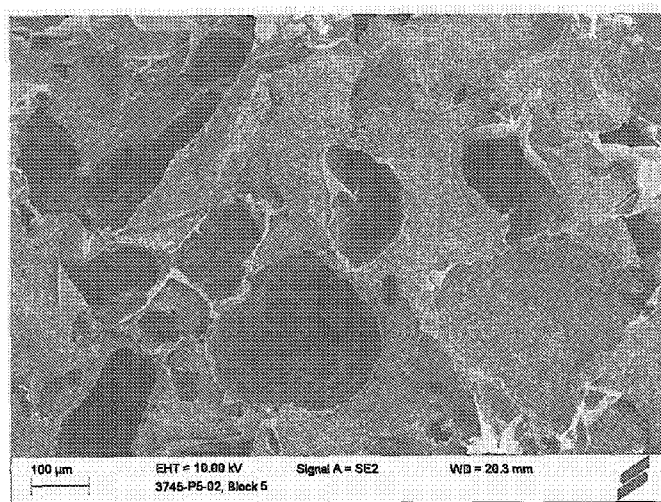


Figure 2

(57) Abstract: The present invention relates to a method for preparing a bone repair material comprising a porous block-shaped scaffold containing a crosslinked polyethylene glycol hydrogel formed by a Michael type addition of at least two precursor molecules. Said scaffold is made of a synthetic ceramic material and comprises interconnected macropores having a diameter of at least 100 μm. In addition the scaffold has a total porosity of 60 to less than 80%. The method comprises the steps : (a) mixing an aqueous solution comprising a first precursor with an aqueous solution comprising a second precursor, whereby the total concentration of the first and the second precursor in the mixture is less than the equilibrium concentration of the hydrogel, (b) adding the mixture of step a) to the porous block-shaped scaffold, and (c) vacuuming the bone repair material obtained in step c), to allow reaction between the first and the second precursor.

Bone repair material

The present invention relates to a method for preparing a sliceable bone repair material comprising a porous block-shaped scaffold containing a hydrogel. Said hydrogel is formed by Michael type addition of at least two precursor molecules. The scaffold is made of a synthetic ceramic material, comprises interconnected macropores and has a total porosity of 60 to less than 80%.

The repair of bone defects can be facilitated by placing a bone repair material as a temporary substitute in the defect site, where a loss of natural bone has occurred. The bone repair material is meant to selectively promote and guide the regeneration of natural bone structures.

Both naturally-derived and synthetically-produced bone repair materials have been used to repair such defects. Naturally-derived materials include grafts made from bones. The bone may be harvested directly from the patient, as in autograft-based procedures, or it may be harvested from a suitable donor, surrogate, or cadaver, as in allograft- or xenograft based procedures. However, autograft bone implant procedures are costly and cause additional discomfort for the patients, as they typically require an additional surgery for harvesting the graft material, which may cause significant morbidity at the donor site. Autografts may also show pronounced resorption making the outcome of the augmentation unpredictable. Allogenic bone repair materials also unify osteoconductive and osteoinductive properties, but their origin raises possible pathogenic transfers and ethical issues. Similar concerns are brought up against xenogenic graft materials.

Alternatively, naturally-derived bone repair materials may

be replaced by a completely synthetic bone repair material, which contains no organic residues. In contrast to naturally-occurring bone repair materials, synthetic bone repair materials are often less osteoconductive and
5 hardly osteoinductive. Nevertheless, much research has been and still is directed toward improved synthetic bone repair materials.

In oral surgery and orthopedics, synthetic bone repair
10 materials on a hydroxyapatite (HA) and/or tricalcium phosphate (TCP) basis are widely used.

Depending on indications, they may be applied as granules or pre-fabricated blocks. US 6,511,510 relates to a porous
15 ceramic material from calcium phosphates obtained by a sintering process. The use of granular material allows treatment of a wide range of indications. For granular material, the ceramic block material is processed by steps such as rubbing, pounding and sieving afterwards (WO
20 04/054633). Although the granular materials are applied to a wide range of indications in terms of size and area, their suitability to treat large bone defects is limited, because they tend to migrate and as a result to be encapsulated. The augmented volume defined by the applied
25 granules may collapse and fail to guide regrowth of the bone to its original dimensions. US 7,012,034 describes a block-shaped bone augmentation material based on porous β -tricalcium phosphate.

30 Different approaches addressed the problem of providing a material with bone-like mechanical properties. In US 6,994,726 a prosthetic bone implant is made of a hardened calcium phosphate cement having an apatitic phase as a

major phase, which comprises a dense cortical portion bearing the majority of load, and a porous cancellous portion allowing a rapid blood/body fluid penetration and tissue ingrowth. Alternatively, EP 1 457 214 discloses a
5 block shape organic-inorganic complex porous article with a superposed skin layer made of a degradable polymer with improved strength. The complex is mainly designed to be inserted between vertebral bodies.

10 To generally improve load bearing properties of bone repair materials, composite materials have been developed. EP 1 374 922 discloses a bioresorbable structure for use in the repair of bone defects comprising a porous bioceramic matrix of hydroxyapatite or tricalcium
15 phosphate and a polymer disposed by compression molding therein. WO 97/34546 describes a ceramic block with a plurality of channels filled containing an enforcing bio-resorbant polymer material. In order to improve their regenerative potential, bone repair materials have been
20 supplemented with bone growth inducing agents. US 10/271,140 (US 2003/0143258A1) suggests a composite comprising demineralized bone matrix mixed with a stabilizing biodegradable polymer and a bone growth factor.

25

In a typical periodontal surgical bone repair procedure an incision is made in the gum tissue to expose a bone defect adjacent to a tooth root. Once the defect and root are debrided, a bone repair material, suspended in a suitable
30 carrier is placed. The gum tissue is then closed, maintaining the repair material in place. Optionally, a barrier material may be utilized to retain the repair formulation in contact with the defect. Therefore, a bone

repair material in periodontal surgery requires formulations that can be easily shaped to size and shape of the defect. WO 2004/011053 suggests a formulation with a putty consistency. Similarly, EP 1 490 123 describes a kneadable bone replacement material on a granular calcium phosphate and hydrogel basis. When applied to the defect site, the formulation remains adhered thereto without migration or excessive expansion. These concepts however, do provide for a solid bone substitute material.

10 US 2004/002770 discloses polymer-bioceramic structures for use in orthopaedic applications. Thereby a polymer is disposed in a porous bioceramic by compression molding.

WO 2009/007034 discloses a block-shaped scaffold and a hydrogel, wherein said scaffold comprises interconnected pores. Said interconnected pores are completely filled with a hydrogel. However, it has been found that the cells have difficulties to migrate into the scaffold material due to the presence of the hydrogel.

It was a problem of the present invention to provide a method for preparing a bone repair material which is easy to handle and suitable for treatment of large oral bone defects, which has osteoconductive and osteoinductive properties.

The problem is solved by a method according to claim 1. Further preferred embodiments are subject of dependent claims 2 to 5.

It was found that the method according to claim 1 results in a bone repair material having a long shelf stability. In addition, after reconstitution of the dried hydrogel, that is the xerogel, to a hydrogel having a water content of at least 40% by weight, the bone repair material shows excellent osteoconductive and osteoinductive properties.

In such a bone repair material the total volume of the hydrogel is smaller than the total volume of the interconnected macropores.

Due to the new method for preparing the bone repair material according to the present invention, which is described below in detail, the cross-linked hydrogel is distributed within the block-shaped scaffold. The inner surface of the pores is more than 50%, preferably more than 60% covered by a thin layer of the dried hydrogel, that is a xerogel, whereas the interior space of the pore is not filled with hydrogel. After drying the hydrogel, only 1 to 15%, preferably 2 to 15%, most preferably 2 to 5%, of the total volume of the interconnected macropores is filled with the dried cross-linked hydrogel. The expression "dried" hydrogel means, that it contains only small amounts of water, preferably less than 10%, most preferably less than 5%. The xerogel has a high porosity and an enormous surface area along with a small pore size. The so obtained bone repair material has, due to the low water content, an excellent shelf stability.

The bone repair material is prepared as follows: As starting material porous block-shaped synthetic scaffold is taken comprising interconnected pores. Said scaffold has a total porosity of 60 to less than 80%.

In a first step an aqueous solution comprising the first precursor A is mixed with an aqueous solution of a second precursor B, whereby the concentration of the first precursor A and the second precursor B together is less than the equilibrium concentration of the swollen hydrogel, preferably less than 5% by weight, most preferably less than 4%, resulting in a mixture in which the total concentration of the reactive groups at the PEG

molecules in the mixture is not high enough to allow the cross-linking reaction to reach the point of gelation, i.e. a gel does not form. Thus, depending on their molecular weights and on their architecture (number of arms), the total concentration and the individual concentrations of the first precursor A and the second precursor B may differ.

In a second step the mixture obtained in step one is added to the block-shaped synthetic ceramic scaffold, preferably by soaking the block-shaped synthetic ceramic scaffold in the mixture. Finally, water is removed from the bone repair material obtained in the previous step, resulting in a gradual increase of the concentration of the precursors, allowing the cross-linking reaction of the two precursors. The water may be removed for example by placing the bone repair material in vacuum. The method is preferably carried out at room temperature. However, the temperature can be used to influence rate the rate of evaporation and of the crosslinking. Preferably, the bone repair material is dried slowly, most preferably within 4 to 20 hours. Preferably, the vacuum is gradually increased over time, most preferably overnight in order to avoid foaming. In a preferred embodiment the bone repair material according to the present invention comprises a xerogel with a water content of less than 10% by weight, most preferably less than 5% by weight.

In a preferred embodiment the first precursor A has a concentration of 0.5% to 4.5% by weight, preferably of 1.5 to 4.5% by weight, most preferably 2.0 to 2.5% by weight, and the second precursor B has a concentration of 0.5% to 4.5% by weight, preferably of 0.5 to 3.0% by weight, most preferably 2.0 to 2.5%, before mixing them together, and

the total concentration of the first precursor A and the second precursor B in solution added to synthetic ceramic scaffold is at least 2% by weight and less than 5% by weight, preferably less than 4% by weight.

5 Before use, the bone repair material has to be reconstituted by the surgeon by soaking the dried bone repair material in water, in aqueous saline solution, in a buffer solution or in blood. In the latter case the cells and factors from the blood are incorporated directly into
10 the block. However, due to the fact that the pores of the block are not completely filled with the hydrogel, blood can also enter the bone repair material after soaking in water, aqueous saline solution, or a buffer solution.

The term reconstituted hydrogel (also called rehydrated
15 hydrogel) stands for a hydrogel obtained after rehydration of a dried hydrogel (xerogel).

The hydrogel comprised in the bone repair material according to the present invention has in its hydrated or reconstituted (rehydrated) form preferably a water content
20 of more than 80% by weight, preferably of more than 90% by weight, most preferably between 90 and 98% by weight. In a most preferred embodiment of the present invention the hydrogel with a PEG concentration of about 5% has a water content of 95% and a hydrogel with a PEG concentration of
25 about 8% has a water content of about 92% by weight.

A dried hydrogel, also called xerogel, is the dry form of a hydrogel. Such a dry form of a hydrogel may be obtained by dehydrating a hydrogel under vacuum.

The equilibrium concentration is the ratio between the
30 mass of the free precursor molecules and the mass of the swollen hydrogel at equilibrium. A swollen hydrogel at equilibrium is the cross-linked network of precursor

molecules which is hydrated or reconstituted (rehydrated) with the amount of liquid it spontaneously takes up under physiological conditions (salt concentration, for example PBS buffer, and temperature, 37°C). The water content of the hydrogel is dependent on the affinity of the polymer, that is PEG, and the density of the crosslinking points of the hydrogel. A swollen PEG hydrogel has preferably a water content of more than 90% by weight.

If the concentration of the precursor molecules in the bone repair material is clearly lower than the equilibrium concentration, that is 80% (90%), almost no crosslinking occurs. Due to the method which is disclosed above, it is possible to increase the concentration of the precursor molecules by evaporating the water and, therefore, allowing the precursor molecules to crosslink. Best results were obtained for bone repair material, wherein the ratio of the total concentration of the precursor molecules and the equilibrium concentration of the total of the precursor molecules in the swollen hydrogel is less 0.9 to 0.95, since this bone repair material showed good osteoconductive properties and had no tendency to break.

Dependent on the porosity of the material, the PEG content (that is the total concentration of the at least two precursors) is adjusted in order to obtain good results. In a preferred embodiment the ratio between the scaffold and total of the precursor molecules is greater than 21:1 by weight, preferably greater than 35:1, and most preferably greater than 60:1. Such a combination allows very good cell integration and an optimal bone repair material stability. Optimal results are achieved for a bone repair material having a scaffold with a porosity from 65 to 70% and a ratio between the scaffold and the total of the precursor molecules of more than 60:1 by

weight.

Due to the ratio between the scaffold and the total of the precursor molecules in combination with the total porosity of the scaffold, only 30 to 60, preferably 20 to 45% of the total volume of the interconnected macropores is filled with cross-linked hydrogel after rehydration, that is, the reconstituted hydrogel, which results in excellent osteoconductive and osteoinductive properties. Due to the fact that 40 to 70%, preferably 55 to 80% of the total volume of the interconnected macropores is empty, that means is filled with air, blood and/or tissue fluids, the cells can easily migrate into the scaffold material and therefore nutrient and oxygen supply, neo-vascularisation, cell immigration, colonization and bone deposition is facilitated.

Figure 1 shows an electron microscopy picture of a block-shaped scaffold which does not comprise a cross-linked polyethylene glycol hydrogel, whereas Figure 2 shows an electron microscopy picture of a bone repair material according to the present invention containing a dried cross-linked polyethylene glycol hydrogel, that is a xerogel.

Beside the good osteoconductive properties the bone repair material according to the present invention has an excellent stability. In contrast thereto bone repair material having completely filled pores, has a tendency to break upon rehydration or swelling. Especially bone repair material, wherein only 20 to 30% of the total volume of the interconnected pores is filled with the hydrated or reconstituted cross-linked hydrogel, showed no tendency to break at all.

The scaffold of the bone repair material according to the present invention has interconnected pores and is made of a synthetic ceramic material. Preferably said synthetic ceramic material is a material comprising calcium phosphate. The synthetic ceramic material may be made of apatite, tricalcium phosphate or a mixture thereof. Apatite and tricalcium phosphate (TCP) or combinations thereof, are efficient bone substitutes that enhance bone ingrowth. Eventually, the material gets resorbed and substituted by bone. Hydroxyapatite and β -tricalcium phosphate, and combinations thereof are especially preferred. These materials can be manufactured with well defined reproducible morphologies with respect to grain size and porosity.

The scaffold material according to the present invention has a porous morphology. Said scaffold material is a highly porous calcium phosphate with interconnected pores of a size range that allows fast ingrowth of natural bone. A person skilled in the art can determine the pore volume and the interconnectivity with micro CT. Methods to characterize calcium phosphate blocks with regard to the porosity have been described in Biomaterials, 2005 Nov; 26(31):6099- 105 and in Biomaterials 27 (2006), 2776-2786.

For the preferred scaffold material according to this invention the total porosity lies in the range of 60 to less than 80%, preferably from 60 to 75%, most preferably of 65%. Porosity is the percentage of void space per volume unit of scaffold material. Specific surface density is defined as the scaffold surface per scaffold volume. The preferred scaffold material according to this invention has a specific surface density of at least

20/mm, more preferably above 30/mm. The material will be integrated in newly formed bone and will eventually be degraded and replaced by natural bone. In the present invention the term porosity means only open pores, e.g.
5 pores which are accessible from outside. Closed pores do not fall within said definition.

The expression the total volume of the interconnected macropores means the void space of all macropores. Typically, the void space of all macropores is measured by
10 mercury intrusion porosimetry according to ISO 15901-1.

The porous structure may be obtained by various processes. Usually a powder is suspended in an aqueous solution to result in a slurry. To form a porous structure, a pore
15 forming agent may be added. Alternatively a sponge-like polymeric matrix with a determined pore structure or an aggregate of spherical objects is coated with the slurry. After drying the slurry, the ceramic material undergoes a sintering process at high temperatures between 800°C and
20 1300°C, depending on grain size and nanoporosity desired. During sintering the pore forming material is burned out and a porous ceramic scaffold remains. Depending on the process and the pore forming agent or material, the porosity of the block-shaped material can be adjusted to
25 result in a desired distribution and interconnectivity of pores of various sizes. They can be classified as nanopores (diameter below 1 µm), micropores (diameter between 1 and 100 µm) and macropores (diameter above 100 µm). For the purpose of tissue regeneration, a substantial
30 amount of interconnected micropores and macropores is desired in order to allow cells to migrate into the scaffold material. Preferably more than 90%, most preferably 95%, of the volume of the pores of the block-

shaped scaffold are micropores and macropores. Micropores are mostly not connected to other micropores but to macropores. Their main function is to change the surface structure and area.

- 5 In a preferred embodiment of the invention, the diameter of the pores lies between 0.05 and 750 μm . More preferably, the diameter of the micropores is between 1 and 100 μm and the diameter of the macropores is between 100 and 1000 μm . Most preferably, the diameter of the
- 10 micropores is between 5 and 100 μm and the diameter of the macropores is between 100 to 500 μm . The pores of the preferred scaffold material according to this invention have a mean diameter between 100 and 750 μm , preferably 300 and 600 μm . The preferred embodiment further has
- 15 highly interconnected pores. The interconnectivity can be defined as connective density (equivalent to the terms connectivity or interconnectedness) as described in Bone, 1993 Mar-Apr; 14(2): 173-82. The scaffold material according to this invention has a connectivity, which is
- 20 above 20 per mm^3 . In terms of connections per pore, which is equal to the ratio of interconnectedness and the number of pores per volume, the scaffold material according to this invention has a connectivity per pore, which is at least 2, more preferably 3 or more. As described above,
- 25 the porosity does not need to be of random distribution, but may be obtained by a highly repeated spacing structure such as tubuli. A tubular structure with a suitable stabilizing polymer may be preferred, if high mechanical strength is required.
- 30 In addition to the composition and porosity, a suitable architecture of the block-shaped ceramic scaffold

material may further enhance bone regeneration and improve the handling properties. A first portion of the block oriented to the remaining bone, which needs to be augmented, preferably has a cancellous structure with a high proportion of macropores, thereby facilitating the integration of bone tissue into the block. A second portion of the block-shaped ceramic scaffold material oriented to the surrounding soft tissue preferably has a dense structure in order to reduce the risk of soft tissue ingrowth into the area of bone augmentation. Therefore, the ceramic scaffold material subject to this invention preferably is manufactured to contain a gradient in its porosity and/or crystallinity and/or ceramic composition.

As mentioned above, the bone repair material according to the present invention comprises a cross-linked polyethylene glycol hydrogel. It could be shown that the porous block-shaped scaffold comprising a homogenously distributed cross-linked hydrogel has a waxy consistency, resulting in a bone repair material with excellent handling properties. The bone repair material is no longer brittle since the hydrogel stabilizes the pores, that is, it can be shaped with a scalpel, which is appreciated by the practitioner for fitting the block to the bone defect site.

25

The cross-linked polyethylene glycol hydrogels in this invention are based on the base catalyzed Michael type addition between a first precursor molecule and a second precursor molecule. In order to obtain a cross-linked network, at least one of the two precursors has more than two chains. The first precursor molecule has alpha, beta unsaturated carbonyl residues and the second precursor

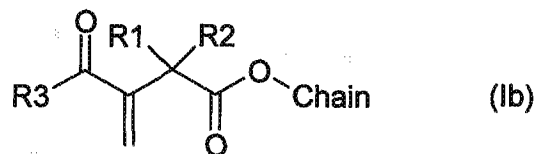
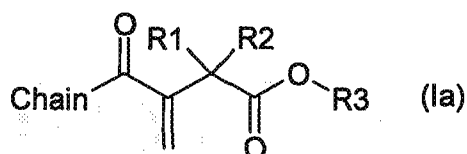
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molecule has nucleophilic groups. The resulting linkage between the first precursor molecule and the second precursor molecule is an ester, which is unstable in contact with water. Alternatively, non-hydrolyzable linkages may be formed if maleimid or vinylsulfone groups are used. The PEG-thiol can be replaced by peptides with two cystein ends that are for example MMP sensitive to produce non-hydrolyzable but enzymatically degradable gels. The rate of the hydrolysis reaction depends on the temperature on the chemical surrounding of the ester (for example acrylate vs methacrylate on precursor A, the number of methylene groups between O and S in precursor B) and the value of the pH, which is 7.4 in most tissues. When sufficient bonds have hydrolyzed, the cross-linked network degrades or breaks down. Therefore, the time of degradation of the network can be influenced by the number of hydrolysable bonds present per unit of volume. Such cross-linked polyethylene glycol hydrogels are described for example in EP 1 609 491.

The first precursor A preferably comprises a core which carries n chains with a conjugated unsaturated group or a conjugated unsaturated bond attached to any of the last 20 atoms of the chain. The later statement does not necessarily mean that the chains comprise at least 20 atoms; the chains may also be shorter, in which case the conjugated unsaturated group or a conjugated unsaturated bond is attached to an atom, which is closer to the end of the chain. In a preferred embodiment said conjugated unsaturated group or conjugated unsaturated bond is terminal. This means that said group is attached to the last atom of the chain, i.e. the one atom of the chain which is the furthest away from the core of the precursor molecule A. The core of the first precursor A can be a

single atom such as a carbon or a nitrogen atom or a small molecule such as an ethylene oxide unit, an amino acid or a peptide, a sugar, a multifunctional alcohol, such as pentaerythritol, D-sorbitol, glycerol or oligoglycerol, such as hexaglycerol. The chains are polyethylene glycol chains. Beside the chains, the core of precursor A may be additionally substituted with linear or branched alkyl residues or polymers which have no conjugated unsaturated groups or bonds. In a preferred embodiment the first precursor A has 2 to 10 chains, preferably 2 to 8, more preferably 2 to 6, most preferably 2 to 4 chains.

The conjugated unsaturated bonds are preferably acrylate groups, acrylamide groups, quinine groups, 2- or 4-vinylpyridinium groups, vinylsulfone groups, maleimide groups or itaconate ester groups of formula Ia or Ib



wherein R1 and R2 are independently hydrogen, methyl, ethyl, propyl or butyl, and R3 is a linear or branched C1 to C10 hydrocarbon chain, preferably methyl, ethyl, propyl or butyl.

In a most preferred embodiment the precursor A has a core which carries 2 to 6 polyethylene glycol chains, each chain having a terminal acrylate group (also called a multi-arm PEG acrylate). The core of the precursor A is preferably a pentaerythritol moiety.

The second precursor B comprises a core carrying m chains

each having a thiol or an amine group attached to any of the last 20 atoms at the end of the chain. The later statement does not necessarily mean that the chains comprise at least 20 atoms; the chains may also be shorter, in which case the thiol or the amine group is attached to an atom, which is closer to the end of the chain. In a preferred embodiment said thiol or amine group is terminal or attached to the second to last carbon atom of the chain. The expression "terminal" means that said group is attached to the last atom of the chain, i.e. the one atom of the chain which is the furthest away from the core of the precursor molecule A. For example it would also be possible to incorporate a cysteine residue into the chain. Preferably the thiol group is terminal. The core of the second precursor B can be a single atom such as a carbon or a nitrogen atom or a small molecule such as an ethylene oxide unit, an amino acid or a peptide, a sugar, a multifunctional alcohol, such as pentaerythritol, D-sorbitol, glycerol or oligoglycerol, such as hexaglycerol. The chains are polyethylene glycol chains. In a preferred embodiment the second precursor B has 2 to 10 chains, preferably 2 to 8, more preferably 2 to 6, most preferably 2 to 4 chains.

In a most preferred embodiment the precursor B has a core which carries 2 to 4 polyethylene glycol chains, each chain having a terminal thiol group (also called a multi-arm PEG-thiol. The core of the precursor B is preferably an ethylene oxide group or a CH_2 -group.

The first precursor A compound has n chains, whereby n is greater than or equal to 2, and the second precursor B

compound has m chains, whereby m is greater than or equal to 2. The first precursor A and/or the second precursor B may comprise further chains which are not functionalized.

5 The sum of the functionalized chains of the first and the second precursor, that means $m+n$, is greater than or equal to 5. Preferably the sum of $m+n$ is equal to or greater than 6 to obtain a well formed three-dimensional network. Such molecules having a core and two or more end groups
10 are also referred to as multi-arm polymers.

Beside the number of chains, their length is a crucial parameter to adjust thy hydrolysis/degradation time of the hydrogel network and the mechanical properties of the bone
15 repair material subject to this invention.

The number of atoms in the backbone (only carbon and oxygen atoms; hydrogen atoms are not counted) connecting two adjacent cross-linking points is at least about 20
20 atoms, preferably between 50 and 5000 atoms, more preferably between about 50 and 2000 atoms, most preferably between 60 and 1000 atoms, and ideally between 200 and 800 atoms. A cross-linking point is here defined as a point in which 3 or more backbone chains of the
25 polymer network are connected.

In a preferred embodiment the first precursor has four polyethylene glycol chains having each an acrylate group as terminal group and a molecular weight of 15 kDa. The second precursor has four polyethylene glycol chains
30 having each a thiol group as terminal group or attached to the second to last carbon atom of the chain and a

molecular weight of 2 kDa. Such a hydrogel has an equilibrium concentration of about 8% by weight.

In a further preferred embodiment the first precursor has four polyethylene glycol chains having each an acrylate group as terminal group and a molecular weight of 15 kDa. The second precursor has two polyethylene glycol chains having each a thiol group as terminal group or attached to the second to last carbon atom of the chain and a molecular weight of 3.4 kDa. Such a hydrogel has an equilibrium concentration of about 5% by weight.

The precursors forming the cross-linked polyethylene glycol hydrogel are dissolved or suspended in aqueous solutions. Since no organic solvents are necessary, only aqueous solutions and/or suspensions are present. These are easy to handle and do not require any laborious precautions as might be the case if organic solvents were present. Furthermore, organic solvents are an additional risk for the health of the staff and the patients exposed to these solvents. The present invention eliminates said risk.

Said aqueous solution comprising the first and the second precursor can have a neutral pH or can be acidic, such as diluted acetic acid. To said solution or suspension optionally a bioactive agent may be added. Optionally said solution or suspension has to be diluted further in order to obtain a total polyethylene glycol concentration of less than 8, preferably less than 5% by weight (depending on the precursor used), in order to make sure that no

gelation occurs. In a next step the pH of the suspension or solution is increased to a range of 7.0 to 9.5, preferably 8.0 to 9.5. Said suspension or solution is added to the scaffold. Then the bone repair material is dried under vacuum. Since water evaporates the concentration of the precursors increases and reaches the minimal gelation concentration and therefore gelation occurs. Typically, after drying under vacuum for 12 to 20 hours, the xerogel contained in the bone repair material according to the present invention has a water content of less than 10%, preferably of less than 5%. Before use said bone repair material, the xerogel has to be reconstituted by the surgeon, by rehydrating the dried hydrogel (xerogel) with water or with a buffered solution or soaking it for a few minutes in blood in order to allow the hydrogel to swell. Such a reconstituted swelled hydrogel comprises typically about 5% to 8% PEG in total and has a water content of 92 to 95% by weight.

In a most preferred embodiment the cross-linked hydrogel comprised in the porous block-shaped scaffold has a pH in a range of 7.0 to 9.5, preferably from 8.0 to 9.5, most preferably from 8.6 to 9.5. The expression the hydrogel "has" a pH of for example 8.6 means that the hydrogel is formed at a pH of 8.6 or is after its formation brought to a pH of 8.6. That is, the pH is measured either a) in the buffered solution before adding said buffered solution to the precursors; or b) directly after mixing the precursor before crosslinking occurs; or c) in the buffered solution before adding the buffered solution to the dried product. Alternatively, the pH of the hydrogel can also be determined by calculation based on the projected amounts and concentrations of the reagents in the reaction mixture. Preferably the pH of the hydrogel is measured

right after mixing the precursors, before soaking the scaffold with the mixture and before drying the bone repair material. Alternatively, the pH of the final product is adjusted by rehydrating the dried bone repair
5 material in a buffered solution having the desired pH.

Surprisingly, it has been found that in the case of a bone repair material comprising a hydrogel having a pH in the range of 8.0 to 9.5, preferably 8.6 to 9.5 the replacement of the hydrogel by newly formed bone is much faster than
10 for hydrogels having a pH of about 7.6. Therefore, the bone regeneration takes place faster, leading to a shorter healing time. Although a difference of pH of about 0.5 to 1 may seem fairly small, it has to be noted that the pH is based on a logarithmic scale and that, therefore, a
15 difference in pH of 1 corresponds to a difference in proton or hydroxide concentration by a factor 10.

The desired pH is achieved by addition of a basic catalyst or buffer regulating the pH. The concentration and the pH of the buffering agent may also be used to adjust the
20 speed of gelation. For example, it may be used to increase the speed of gelation for not so dense gels. The final concentration in the mixture that is added to the bone repair material, e.g. triethanolamine, is preferably between 0.005 mol/l and 0.1 mol/l, preferably 0.01 mol/l.

25 In a further embodiment of the present invention the cross-linked polyethylene glycol hydrogel contained in the block-shaped scaffold is at the same time a matrix for sustained release of one or several bioactive agents, which promote the osteoconductive and/or osteoinductive
30 properties of the composite bone repair material. As used herein, a bioactive agent is not limited by its origin or

the way it is produced and therefore can be extracted, synthetically or recombinantly produced and may have been subject to further processing or purification, such as but not limited to, splicing, fragmentation, enzymatic
5 cleavage or chemical modification. Examples of suitable biologically active agents are BMPs (e.g. BMP-2, BMP-7), PTH, VEGF, Enamel Matrix Derivatives (EMD) or proteins contained therein, TGF-beta, IGF, Dentonin, and cell recognition sequences such as RGD, KRSR, etc. Most
10 preferred the bioactive agent is BMP or RGD.

The bioactive agent may be covalently bound to the hydrogel, e.g. this can be achieved by a thiol moiety present in the bioactive agent, which reacts with the conjugated unsaturated group or bond present in precursor
15 A upon mixing. A thiol moiety is present, e.g., in the amino acid cysteine. The bioactive agent is subsequently released from the hydrogel as the unstable ester linkage between the PEG and the bioactive agent is hydrolyzed.

Alternatively, the bioactive agents may simply be
20 entrapped or precipitated into the bone repair material. The bioactive agent can be added when mixing the other components of the composition. The bioactive agent is then released by diffusion during and/or after degradation of the hydrogel. It is also possible to adsorb the bioactive
25 agent on the block-shaped scaffold prior to the soaking with the solutions comprising the first precursor A and the second precursor B.

The mechanical strength of the block shaped scaffold can be further enhanced by embedding one or more additional
30 stabilizing polymers, fibrous or filamentous supplements such as carboxymethyl cellulose, hydroxyethyl cellulose,

alginates, xanthan gum etc.

In a preferred embodiment the surgeon is provided with a kit comprising repair material with the scaffold containing the xerogel (dried hydrogel) and a buffered solution, which is stored in a separate container or compartment. Before use, the surgeon soaks the bone repair material in the buffered solution in order to rehydrate the xerogel to reconstituted hydrogel in the bone repair material. The hydrogel is reconstituted in less than 5 minutes.

Examples

Example 1:

15 Gelation experiments loose hydrogels

6.4 mg of 4-arm PEG with acrylate end groups ($M_n=15$ kDa) and 3.3 mg of linear PEG with propylthiol endgroups ($M_n=3.5$ kDa) were dissolved in 64 μ l of 0.04% aqueous acetic acid. To the solution 25 μ l of 0.10 M triethanolamine were added, yielding a solution containing 9.8 wt% PEG. At 25°C the solution yielded a soft, elastic hydrogel in 6.5 min.

3.3 mg of 4-arm PEG with acrylate end groups ($M_n = 15$ kDa) and 1.7 mg of linear PEG with propylthiol end groups ($M_n = 3.5$ kDa) were dissolved in 69 μ l of 0.04% aqueous acetic acid. To the solution, 25 μ l of 0.1 M triethanolamine were added, yielding a solution containing 5.0 wt% PEG. At 25°C the solution yielded an elastic hydrogel, softer than the 9.8 wt% hydrogel in 16 min.

1.32 mg of 4-arm PEG with acrylate end groups ($M_n = 15$ kDa)

and 0.69 mg of linear PEG with propylthiol end groups ($M_n = 3.5$ kDa) were dissolved in 72.4 μ l of 0.04% aqueous acetic acid. To the solution, 25 μ l of 0.1 M triethanolamine were added, yielding a solution containing 2.0 wt% PEG. At 25°C
5 the solution did not yield a hydrogel within the observation time of 4 hours.

Example 2

Degradation loose hydrogels

A gel containing 9.8 wt% PEG was placed in PBS at pH 7.4
10 and 37°C. After 6 hours the gel had swollen to 2.2-fold its original weight. After that, swelling continued at a slower pace and after 11 days the gel was completely dissolved.

A gel containing 5.0 wt% PEG was placed in PBS at pH 7.4
15 and 37°C. After 6 hours the gel had swollen to 1.1-fold its original weight. After that, swelling continued at a slower pace and after 11 days the gel was completely dissolved.

Example 3:

20 Gelation experiments denser hydrogel

7.0 mg of 4-arm acrylate end groups ($M_n = 15$ kDa) and 1.1 mg of 4-arm PEG with propylthiol end groups ($M_n = 2.3$ kDa) were dissolved in 68.4 μ l of 0.04% aqueous acetic acid. To the solution, 25 μ l of 0.2 M triethanolamine/HCl buffer
25 (pH 8.5) were added, yielding a solution containing 8.0 wt% PEG. At 25°C the solution yielded a firm hydrogel in 2 to 3 min.

Degradation denser hydrogel

The denser gel containing 8.0 wt% PEG was placed in PBS at pH 7.4 and 37°C. After 6 hours the gel had swollen to 1.2 fold its original weight and after 28 days the gel was
5 completely dissolved.

Example 4**Combination bone block and PEG hydrogel**

10

5% PEG hydrogel solution

66.7 mg of 4 arm PEG with acrylate end groups ($M_n = 15$ kDa) and 32.7 mg of linear PEG with propylthiol end groups ($M_n = 3.5$ kDa) were dissolved in 1173 μ l of 0.04% aqueous
15 acetic acid and 200 μ l of water and 500 μ l of aqueous 0.1 M triethanolamine solution were added.

3% PEG hydrogel solution

39.7 mg of 4 arm PEG with acrylate end groups ($M_n = 15$ kDa) and 19.8 mg of linear PEG with propylthiol end groups
20 ($M_n = 3.5$ kDa) were dissolved in 704 μ l of 0.04% aqueous acetic acid and 920 μ l of water and 300 μ l of aqueous 0.1 M triethanolamine solution were added.

2% PEG hydrogel solution

27.1 mg of 4 arm PEG with acrylate end groups ($M_n = 15$ kDa) and 13.2 mg of linear PEG with propylthiol end groups
25

($M_n = 3.5$ kDa) were dissolved in 470 μ l of 0.04% aqueous acetic acid and 1280 μ l of water and 200 μ l of aqueous 0.1 M triethanolamine solution were added.

1% PEG hydrogel solution

- 5 13.2 mg of 4 arm PEG with acrylate end groups ($M_n = 15$ kDa) and 6.6 mg of linear PEG with propylthiol end groups ($M_n = 3.5$ kDa) were dissolved in 235 μ l of 0.04% aqueous acetic acid and 1640 μ l of water and 100 μ l of aqueous 0.1 M triethanolamine solution were added.

10 Bone block

Immediately after mixing, the 2.0 ml of hydrogel solution was applied to a cylindrical bone block ($h = 25$ mm, $\varnothing = 14$ mm) with a porosity of 71% which absorbed the liquid completely.

- 15 The filled block was placed in an exsiccator that was heated to 37°C and the pressure was gradually reduced to 5 mbar over the course of 5 hours, after which the block was left at 5 mbar and 40°C for another 15 hours. This procedure almost completely removed the water without
20 causing foaming and, in the process of water removal, allowed for efficient gelation.

Before addition of the hydrogel solution and after drying, the blocks were weighed. For all blocks, the increase in weight was found to be between 90% and 103% of the total
25 weight of both PEG precursors.

It was observed that, upon prolonged incubation in cell medium (7 days at 37°C) some blocks broke, presumably due to the pressure of the swelling hydrogel on the thin calcium phosphate walls of the bone block.

The ratio between scaffold (bone block) and total precursor molecules is also indicated.

Scaffold [mg]	PEG-acrylate [mg]	PEG-thiol [mg]	Total Precursor [mg]	Ratio scaffold / total precursor	Wt % PEG in hydrogel	Blocks broken after 7 days
4134	66.7	32.7	99.4	41.6	5	20%
4244	39.7	19.8	59.5	71.3	3	3%
4262	27.1	13.2	40.3	106	2	0%
4387	13.2	6.6	19.8	222	1	0%

Each one of the blocks prepared with the 2% formulation, the 5% formulation, and without hydrogel were broken and the fracture surfaces were studied with SEM. Both the blocks with 2% and 5% PEG hydrogel formulation showed the presence of sheets of xerogel lining the walls of the pores. In the 5% block (Figure 4) these were thicker than in the 2% block (Figure 3).

EDX (Energy-dispersive X-ray spectroscopy) analysis showed the absence of C in areas without xerogel and the presence of C in the areas lined with xerogel.

Claims

1. Method for preparing a bone repair material comprising a porous block-shaped scaffold containing a crosslinked polyethylene glycol hydrogel formed by a Michael type addition of at least two precursor molecules, wherein said scaffold is made of a synthetic ceramic material and comprises interconnected macropores having a diameter of at least 100 μm and the scaffold has a total porosity of 60 to less than 80% comprising the steps:
 - a. mixing an aqueous solution comprising a first precursor with an aqueous solution comprising a second precursor, whereby the total concentration of the first and the second precursor in the mixture is less than the equilibrium concentration of the hydrogel
 - b. adding the mixture of step a) to the porous block-shaped scaffold
 - c. removing water from the bone repair material obtained in step c), to allow reaction between the first and the second precursor.
2. Method according to claim 1, wherein the total concentration of the first precursor and the second precursor is less than 5% by weight, preferably less than 4%.

3. Method according to claim 2, wherein the first precursor A has a concentration of 0.5 to 4.5% by weight, preferably 1.5 to 4.5% by weight, most preferably 2.0 to 2.5% by weight and the total concentration of the first precursor A and the second precursor B is at least 2% by weight.
4. Method according to claims 2 or 3, wherein the second precursor B has a concentration of 0.5 to 4.5% by weight, preferably 0.5 to 3.0% by weight, most preferably 2.0 to 2.5% by weight and the total concentration of the first precursor A and the second precursor B is at least 2% by weight.
5. Method according to any of the preceding claims, wherein the hydrogel is dried to a xerogel having a water content of less than 10% by weight, preferably to less than 5%.
6. Method according to any of the preceding claims, wherein the vacuum is gradually increased over time.
7. Method according to claim 5, wherein water or a buffer solution is added to the bone repair material to reconstitute the xerogel.

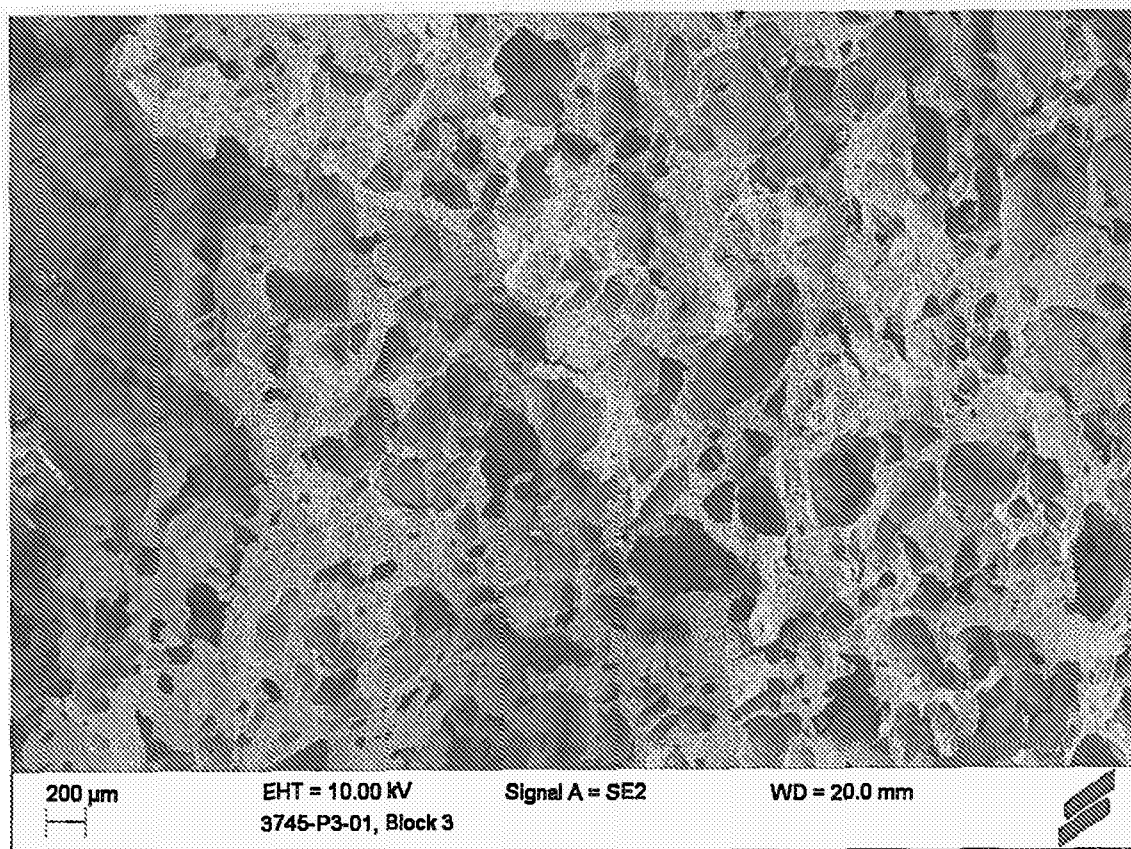


Figure 1

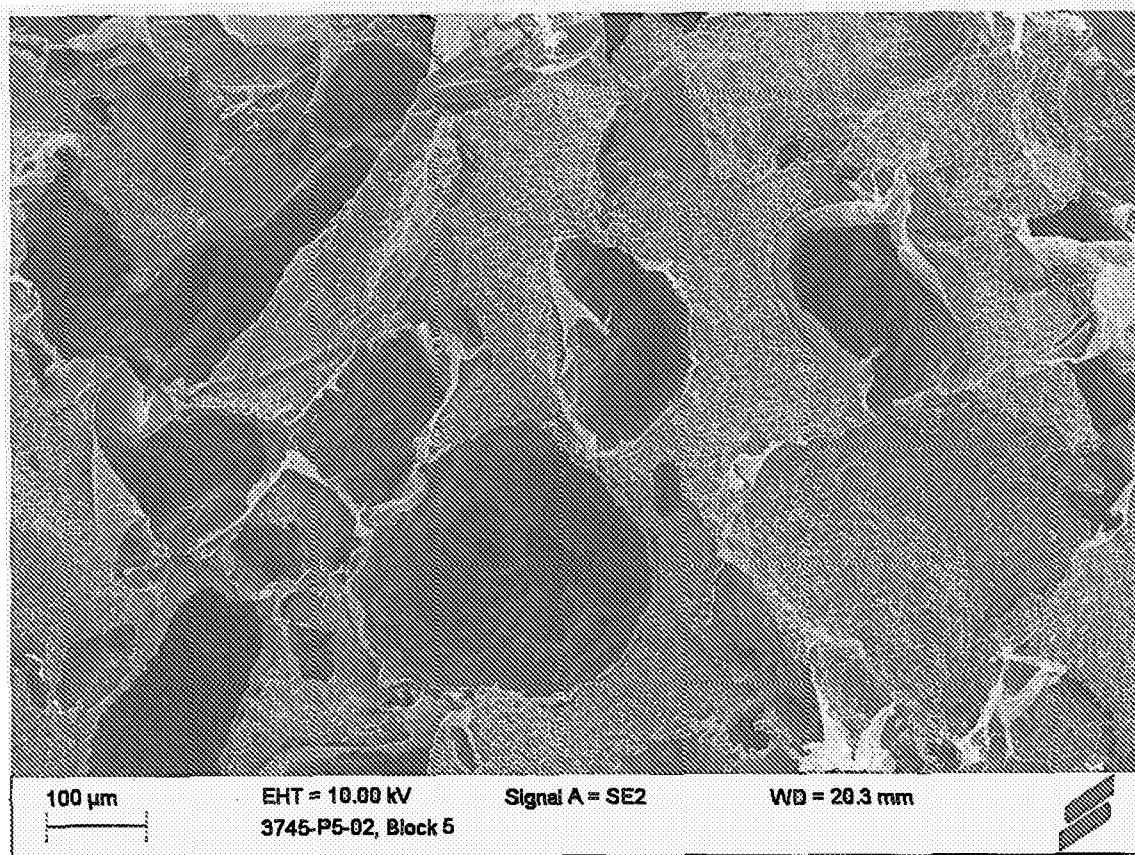


Figure 2

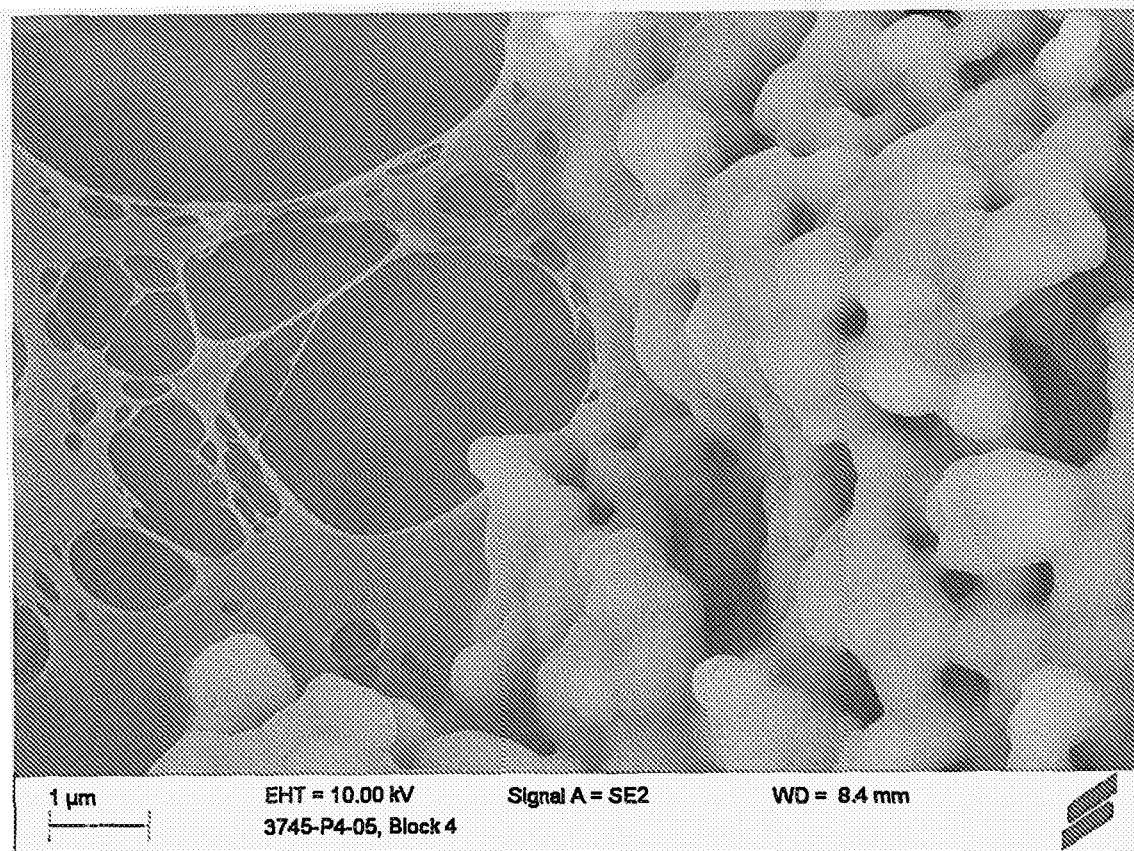


Figure 3

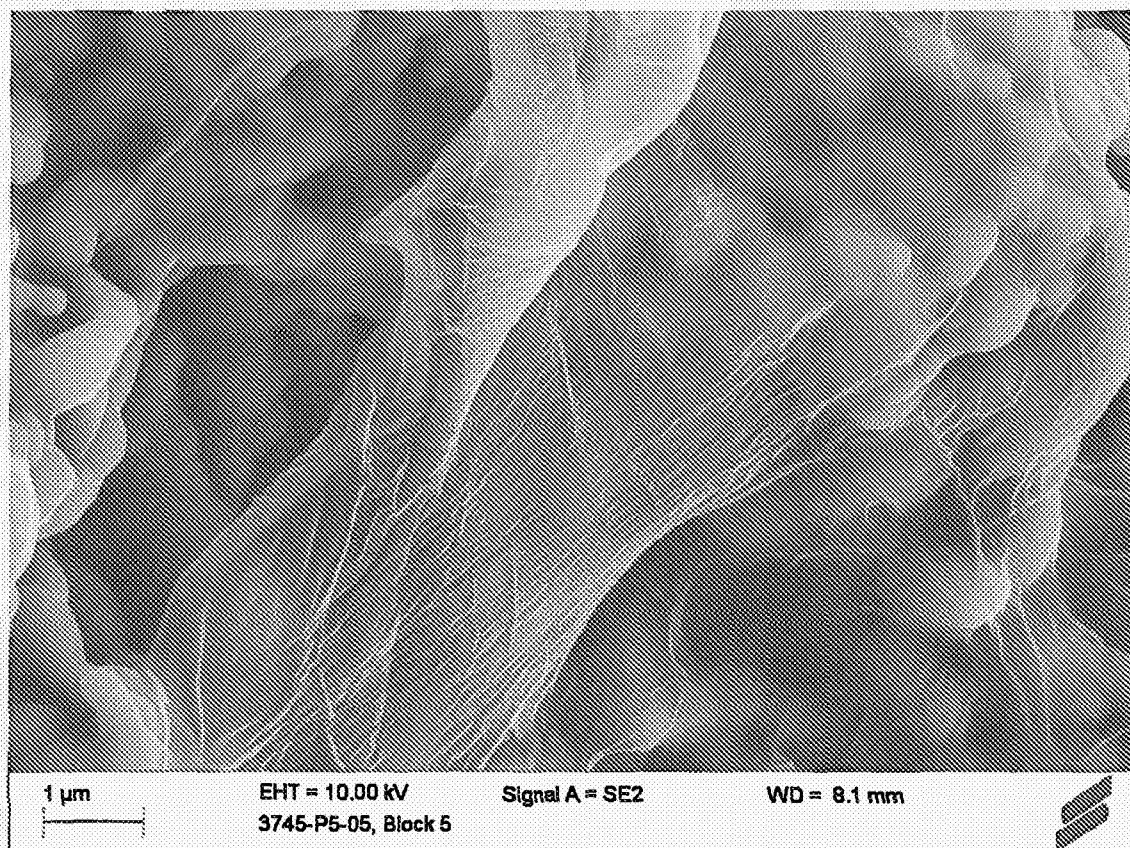


Figure 4

INTERNATIONAL SEARCH REPORT

International application No
PCT/CH2013/000030

A. CLASSIFICATION OF SUBJECT MATTER
INV. A61L24/00
ADD.

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
A61L

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

EPO-Internal, BIOSIS, EMBASE, WPI Data

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Further documents are listed in the continuation of Box C.



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Date of the actual completion of the international search

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Menidjel, Razik

INTERNATIONAL SEARCH REPORT

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