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DIFFERENTIAL FROTH FLOTATION OF SULFIDE ORES

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This invention relates to a process of froth flotation in which certain metalliferous sulfides are depressed by means of novel inorganic chemical agents or compounds exhibiting a selective depressing action for the sulfides.

In the flotation of sulfides and certain precious metals such as gold and silver which behave toward sulfide collectors in the same manner as sulfides, it is sometimes desirable to remove certain materials which have the property of float- 10 ing with oily collectors or frothers which are hydrocarbons or water-insoluble alcohols or mixtures thereof. The most important minerals of this class are molybdenite, graphite and carbons. Another group of minerals comprises some of the 15 hydrous magnesium or aluminum-containing silicates which exhibit strongly hydrophobic surfaces. The principal minerals of this class are the various talcs, sericite, the micas and pyrophillite. Chlorites for the most part are only 20 weakly hydrophobic and are unsuitable for the processes of the present invention although there are occasional chlorites which exhibit a greater water-repellency and are about on the borderline of utility. These minerals, although chemically 25 quite different, behave identically in froth flotation and are characterized by ready floatability with hydrocarbon collectors or alcohol collectors or frothers.

Unfortunately, when molybdenite, carbon, and 30 strongly hydrophobic hydrous silicates containing magnesium or aluminum, are associated with sulfide minerals, or in the case of carbon, with free precious metals, a differential flotation is difficult because the oily hydrocarbon and alco- 35 hol collectors and frothers also show some collecting activity for the sulfide minerals and prevent a sharp separation. An even more serious problem is presented by the fact that, chemically, molybdenite, graphite and carbons and 40 strongly hydrophobic hydrous silicates containing magnesium or aluminum may have to be removed from bulk sulfide or precious metal concentrates. This is due to the fact that molybdenite and carbons are often present in com- 45 paratively small amounts which makes a preliminary bulk sulfide float necessary. Talc and mica also are often present in sulfide concentrates and a high degree of removal is economically desirable. However, the problem of sepa- 50 ration by flotation is greatly complicated in the case of such concentrates because they usually contain the residue of the sulfide flotation collectors used in floating concentrates. For example, they may contain xanthates, dithiophos- 55

phates or the like. The presence of small amounts of the original sulfide collector enhances the tendency of the sulfides to float and makes the separation of molybdenite, carbon or strongly hydrophobic hydrous silicates containing magnesium or aluminum from such concentrates even more difficult than in the case of original ores.

The present invention is based on our discovery that inorganic compounds of phosphorus, arsenic and antimony containing oxygen and sulfur in the bivalent state exert a strong depressant action on sulfide minerals other than molybdenite in the presence of hydrocarbon and alcohol collectors and depress these minerals so vigorously that even in the presence of sulfide promoters it is possible to float molybdenite, carbons and strongly hydrophobic hydrous silicates containing magnesium or aluminum away from the sulfides without serious contamination of the concentrate by the sulfides and with a high degree of removal of the molybdenite, carbons and strongly hydrophobic hydrous silicates containing magnesium or aluminum.

The exact chemical composition of the novel depressants has not been fully determined and it is possible that in some instances at least they are not a single pure compound but are mixtures. They are, however, characterized, in addition to phosphorus, arsenic or antimony respectively, by the presence of bivalent sulfur, oxygen and a cation. In the initial preparation of the depressants, the cation is ammonium or an alkaliforming metal. The depressants may be used as such or they may be transformed into their corresponding heavy metal compounds by reaction with a heavy metal salt. For example, they may be transformed into copper compounds by reaction with copper sulfate or into simple compounds of iron, lead, chromium, aluminum or molybdenum by reacting with ferrous sulfate. lead nitrate, chromium nitrite, aluminum sulfate and ammonium molybdenite. The frothers and collectors for the molybdenite, carbons and strongly hydrophobic hydrous silicates containing magnesium or aluminum are the usual collectors and frothers used in floating these metals, that is to say, hydrocarbons, such as for example. fuel oils and various alcohols such as alcohols of from 5 to 10 carbon atoms, terpene alcohols and the like, also combined oily and synthetic frothers, such as mixtures of higher paraffin alcohols and hydrocarbons. It should be noted that the depression effected

by the novel agents of the present invention may be temporary or permanent depending on the specific requirements in any individual case. Thus, for example, if the original ore is treated which contains sulfides and either molybdenite, 5 carbons, or strongly hydrophobic hydrous silivates containing magnesium or aluminum, the first float will be effected in the presence of a hydrocarbon and/or alcohol frother or collector with the sulfides temporarily depressed by the io novel reagents of the present invention. Thereafter, the sulfides in the tailing may be activated by suitable reagents which are well-known in the art, for example, copper sulfate, and a sulfide concentrate obtained. Where bulk sul- 15 fide concentrates are treated to remove molybdenite, carbon or strongly hydrophobic hydrous silicates containing magnesium or aluminum, it is not necessary that the depression be temporary as the flotation in the presence of the novel de- 20 pressants of the present invention is then the final flotation step.

A number of methods of preparing the depressants are possible. Typical reactions are the following:

Thiophosphoryl chloride and sodium hydroxide Thiophosphoryl chloride and calcium hydroxide Thiophosphoryl chloride and sodium silicate Thiophosphoryl chloride and sodium carbonate Thiophosphoryl chloride and ammonium hydroxide

Thiophosphoryl chloride and ammonium phosphate

Thiophosphoryl chloride and sodium phosphate Thiophosphoryl chloride and sodium borate Phosphorus sulfides and sodium hydroxide Phosphorus sulfides and calcium hydroxide Phosphorus sulfides and sodium silicate Phosphorus sulfides and soduim carbonate Phosphorus sulfides and ammonium hydroxide Phosphorus sulfides and ammonium carbonate Phosphorus sulfides and ammonium phosphate Phosphorus sulfides and sodium phosphate Phosphorus sulfides and sodium borate Phosphorus sulfides and calcium cyanide Phosphorus sulfides and sodium cyanide Arsenic sulfide and sodium hydroxide Arsenic sulfide and potassium hydroxide Arsenic sulfide and calcium hydroxide Arsenic oxide, sulfur and sodium hydroxide Arsenic oxide, sulfur and potassium hydroxide Antimony oxide, sulfur and sodium hydroxide Antimony oxide, sulfur and potassium hydroxide

It is an advantage of the present invention that the depressants may be prepared with widely varying quantities of reagents. This simplifies manufacture and eliminates the necessity for extremely exact control.

The depressants of the present invention may be prepared in wet form and used immediately in froth flotation or they may be reduced to dry form by suitable means such as spray drying or other methods. The dry product has an advantage that it can be shipped more readily and economically than can the wet slurries. The form in which the depressants of the present invention will be used in any particular case is largely a matter of economics. In some instances it is cheaper to prepare the depressant at the place of use. In other cases, shipment of the dry material prepared at a central point is more economical. The possibility of use of the depressants of the present invention in these various 75 pressant beyond the point of practicability.

forms adds greatly to the flexibility of the process of recovering molybdenum, carbon or strongly hydrophobic hydrous silicates containing magnesium or aluminum and is one of the additional advantages of the invention.

When bulk sulfide concentrates are treated, it is often of advantage to subject the concentrate to a preliminary treatment with acid and alkali; for example, sulfuric or sulfurous acids and then lime. This often removes frother collector coatings from the minerals and aids in the subsequent selective separation. Other mineral acids may be used such as hydrochloric acid. The sequence of treatment appears more or less immaterial. Thus the acid conditioning may be first or an alkaline conditioning with alkali may precede it. When treatment with acid and alkali is used on a concentrate, the addition of the depressant, collector, and frother, if necessary, are ordinarily made after the acid and alkali conditioning is completed.

We have found that in moylbdenite flotations somewhat improved results are obtainable if the ore is conditioned before floating with a salt of a 25 polyvalent metal, particularly a salt of calcium such as calcium chloride. This conditioning is in place of the treatment with acid described above.

The invention will be described in the following 30 specific examples which set forth the preparation of typical depressants and their use in the process of the present invention.

40 gm. of sodium hydroxide (NaOH) is dissolved in 80 ml. water. 25 gm. of thiophosphoryl chloride is added to the solution, the entire contents being shaken until all thiophosphoryl chloride has reacted. This may require as long 40 as two or three hours, depending upon the intensity of agitation.

EXAMPLE 2

13 gm. of sodium hydroxide is dissolved in 75 $_{
m 45}$ ml. of water. 10 gm. of phosphorus suifide (chiefly P2S5, but containing other homologues among which may be P₄S₃) is added slowly to the solution so as to keep the reacting temperature under control. This reaction proceeds rapidly, 50 being completed in about 5 minutes.

EXAMPLE 3

12 gm. of calcium oxide (CaO) is reacted with 50-80 ml. of water. To the slurry is added 10 gm. 55 of phosphorus sulfide (chiefly P₂S₅) and the mass vigorously stirred at 70-75° C. until reaction is complete.

EXAMPLE 4

To 7 parts by weight of sodium hydroxide (NaOH) add 4 parts by weight of sulphur (S) and 5 parts by weight of water. Stir and heat until all sulfur has gone into solution (that is combined with the sodium hydroxide in aqueous 65 solution). Adding a small amount of additional water, as heating continues, generally facilitates the dissolution of the sulfur. After all sulfur is in solution, add sufficient water to bring the total water added up to 70 parts by weight. Then add 8 parts by weight of arsenic trioxide (As₂O₃) and boil until the reaction is complete. The quantities of sodium hydroxide, sulfur, and arsenic trioxide may vary within certain limits without decreasing the efficiency of the resulting de-

EXAMPLE 5

To 10 parts by weight of arsenic sulfide add 11.6 parts by weight of lime (CaO); add 75 ml. of water and boil; finally dilute to the desired concentration.

EXAMPLE 6

To 7 parts by weight of potassium hydroxide, add 25 parts by weight of water. Boil. To the boiling solution add small increments of sulfur alternating with small increments of antimony trioxide until a total of 2 parts by weight of sulfur and 10 parts by weight of antimony trioxide have been added.

EXAMPLE 7

A material obtained by flotation concentration consisting of molybdenite and other sulfides, chiefly those of copper and iron (Utah Copper Company general flotation concentrate) was tested in a 5000-gm. minerals separation flotation machine. To the charge of about 5000 gms. of suitably prepared material were added the following agents:

10 ml. sulfuric acid (commercial)—66° Bé. 12 gm. calcium oxide (commercial) 250 ml. depressant of Example 3 20 drops kerosene

The pulp was thoroughly agitated in a minerals separation flotation machine after the addition of each of the agents, and the pH values were taken after the incorporation of the first three and at the conclusion of the roughing period.

pH after calcium oxide addition	11.6
pH after sulfuric acid addition	6.6
pH after depressant of Ex. 3 addition	9.9
pH at end of roughing period	9.7

Flotation (10 minutes' floating time) produced a rougher concentrate, a middling and a rougher tailing. The rougher concentrate was cleaned twice in a Fagergren flotation machine making a first cleaner tailing, a second cleaner tailing, and a cleaner concentrate. Most of the sulfides of copper and iron were depressed in the flotation machine and drawn off as rougher tailing, while most of the molybdenite was removed as a froth concentrate. The Fagergren flotation machine was used for grading up or cleaning the flotation machine rougher concentrate.

The effectiveness of this invention treating a flotation concentrate containing molybdenite and other sulfides such as those of copper and iron for the selective flotation separation of molybdenite from other sulfides, may be seen from the following metallurgical data.

	Per	Per Cen	t Assays	Per Cer	ıt Distr.
	Cent Weight	Cu	MoS ₂	Сп	MoS ₂
Heading Rougher Tailing Middling Ist Cleaner Tailing 2nd Cleaner Tailing Cleaner Concentrate	100.0 94.6 1.7 1.5 .3	39. 28 40. 20 34. 70 32. 05 31. 00 4. 00	1. 72 .02 1. 24 5. 05 4. 75 83. 20	100.0 96.9 1.5 1.2 .2	100.00 1.11 1.22 4.31 .70 92.66

EXAMPLE 8

Suitably ground material (Utah Copper Company, Arthur Plant Crude Ore Heading) was treated in a 5000-gram minerals separation flotation machine. To the charge of about 5000 gms. 75 pany, Arthur Plant, general flotation concen-

(dry basis) of ore and water were added the following agents:

5 ml. depressant of Ex. 3 (CaO, H₂O, P₂S₅)

6 dps. burner oil

6 dps. frother consisting of a mixture of paraffine alcohols from 7 to 10 carbon atoms.

The pulp was thoroughly agitated and a rougher molybdenite concentrate was removed as a froth concentrate. This concentrate was later cleaned in a Fagergren flotation machine to form (1) molybdenite cleaner tailing; (2) molybdenite cleaner concentrate. To the material remaining in the minerals separation flotation machine were added 3 ml. of 2.5 per cent xanthate solution, and a rougher copper concentrate was removed as a froth concentrate. (Xanthate is the copper collector used to float the copper after the flotation of the molybdenite.) This concentrate was later cleaned in a Fagergren flotation machine to form (3) copper cleaner tailing, (4) copper cleaner concentrate. The tailing (5) was removed from the machine as waste material.

The results of the test just described may be 25 seen from the following metallurgical tabulation:

	Ler	Per Cen	t Assays	Per Cer	nt Distr.
	Cent Weight	Cu	MoS ₂	Cu	Mo8,
Heading MoS: Cleaner Tailing MoS: Cleaner Concen-	100.0 1.04	1.254 7.100	.050	100.00 5.90	100.00 7.63
trate Cu Cleaner Tailing Cu Cleaner Concentrate Tailing	.26 4.81 3.79 90.10	2.900 1.175 27.150 .095	8.650 .060 .450 .004	. 64 4. 55 82. 05 6. 86	45.09 5.81 34.27 7.21

EXAMPLE 9

Suitably ground material (Utah Copper Company, Arthur Plant, general flotation concentrate) was treated in a laboratory Fagergren flotation machine. To the charge of about 500 gm. (dry basis) of concentrate and water were added 45 the following agents in amounts designated:

1.2 gm. CaO

1 ml. of reaction product made by reacting 11.6 gm. CaO, 5 gm. red phosphorus, 4 gm. sulfur in 30 ml. water, boiling vigorously to effect solution, diluting to 100 ml. using H2O.

2 dps. burner oil.

In the flotation that followed, substantially all the molybdenite was removed as a froth concen-55 trate, making (1) a rougher tailing and a rougher The rougher concentrate concentrate. cleaned making (2) a cleaner tailing, and (3) a cleaner concentrate containing substantially all the molybdenite, the depressed copper and iron 60 sulfides remaining in the rougher tailing.

The results of this test are given in the following metallurgical tabulation:

85		Per Cent	Per Cen	t Assays	Per Cent Distr.		
	Product	Weight	Cu	MoS ₂	Cu	MoS:	
70	Heading Rougher tailing Cleaner tailing Cleaner Concentrate	100.00 92.14 5.80 2.06	32. 95 34. 00 23. 55 12. 30	1. 506 . 03 5. 84 56. 70	100.00 95.08 4.16 .76	100. 00 1. 86 20. 58 77. 56	

EXAMPLE 10

Suitably ground material (Utah Copper Com-

trate) was treated in a laboratory Fagergren flotation machine. To the charge of about 500 gm. of concentrate (dry basis) and water were added the following agents in the amounts designated:

1 ml. sulfuric acid (H2SO4) 66° Bé.

1 gm. lime (CaO)

25 ml. of the reaction product (2 gm. CsO 20 ml. H2O and 1 gm. arsenic sulfide) made up to 50 ml. for testing

2 dps. molybdenite collector (burner oil, modified)

In the flotation that followed, substantially all the molybdenite was removed as a froth concentrate, making (1) a rougher tailing and a rougher concentrate. The rougher concentrate was cleaned, making (2) a cleaner tailing and (3) a cleaner concentrate containing substantially all the molybdenite, the depressed copper and iron sulfides remaining in the rougher tailing.

Fourth.—Adding to the pulp in the flotation machine 0.30 gm. of copper sulfate, 0.075 gm. of xanthate and 2 dps. of frother consisting of a mixture of paraffine alcohols from 5 to 10 carbon 5 atoms, thereby recovering the zinc as a rougher froth concentrate, the rougher tailing (pulp remaining in the machine) being considered waste and drawn out of the machine. The rougher concentrates may be graded up as desired by 10 methods known to the art.

EXAMPLE 12

The following test shows that by the use of this invention it is feasible to concentrate by flotation, ore containing molybdenum sulfide, copper sulfide, lead sulfide, and gangue obtaining three separate concentrates: a molybdenite concentrate, a copper concentrate and a lead concentrate.

Product	Material, Per Cent	. Ass	Assay, Per Cent		Distribution, Per Cent		
Frontes	Weight	MoS ₂	Cu	Pb	MoS ₂	Cu	Pb
Heading (Computed). Rougher Tailing Rougher MoS ₂ Cone Rougher Cu Cone Rougher Pb Cone	83, 15	0.609 .034 40.800 .670 .140	0. 977 0. 055 1. 100 10. 700 2. 250	5.012 .06 1.35 .95 48.60	100.00 4.60 87.02 6.08 2.30	100.00 5.25 1.60 67.39 25.76	100.00 1.00 .24 1.50 97.26

The results of this test may be seen from the following metallurgical tabulation:

	 Per Cent	Per Cen	t Assays	Per Cer	nt Distr.
	Weight	Cu	MoS ₃	Cu	MoS ₂
Heading	 100.00 83.68 14.17 1.95	31. 76 31. 50 37. 10 4. 20	1, 130 . 040 2, 280 56, 100	100.00 83.19 16.56 .25	100.00 2.34 22.26 75.40

EXAMPLE 11

The following test shows that by the use of this invention, it is feasible to concentrate by flotation an ore containing molybdenum sulfide, copper sulfide, zinc sulfide, and gangue, obtaining three separate concentrates: a molybdenite concentrate, a copper concentrate and a zinc concentrate.

Procedure

First.—500 gm. ore ground in laboratory ball mill, using 0.22 gm. lime (CaO).

Second.—Pulp subjected to flotation using a Fagergren laboratory flotation machine adding 5 ml. of the depressant of Ex. 3, 2 dps. of burner oil and 3 dps. of frother consisting of a mixture of paraffine alcohols from 5 to 10 carbon atoms, thereby recovering the molybdenite as a rougher froth concentrate.

Third.—Adding to the pulp in the flotation machine 0.16 gm. xanthate and 2 dps. of frother consisting of a mixture of paraffine alcohols from 5 to 10 carbon atoms, thereby recovering the copper in the form of a rougher froth concentrate.

Fourth.—Adding to the pulp in the flotation

Product	Material, Per Cent		ay, Per	Cent	· Distribution, Per Cent		
Troduct	Weight	MoS ₂	Cu	Zn	MoS;	.Cu	Zn
Heading (Computed) Rougher Tailing Rougher MoS ₂ Conc Rougher Cu Conc Rougher Zn Conc	88.03	0.328 .014 20.700 .86 .09	0.856 .060 2,400 13.750 1.175	3. 554 . 08 3. 500 2. 90 49. 40	100,00 3,66 81,41 13,41 1,52	100.00 6.19 3.63 82.59 7.59	100.00 1.97 1.27 4.19 92.57

Procedure

First.—500 gm. ore ground in laboratory ball mill using 0.22 gm. lime (CaO).

Second.—Pulp subjected to flotation using a Fagergren laboratory flotation machine adding 5 ml. of the depressant of Ex. 3, 3 dps. of burner oil and 2 dps. of frother consisting of a mixture of aliphatic alcohols from 7 to 10 carbon atoms, thereby recovering the molybdenite (MoS₂) as a rougher froth concentrate.

Third.—Adding to the pulp in the flotation machine 0.30 gm. xanthate and 4 dps. of frother consisting of a mixture of paraffine alcohols from 5 to 10 carbon atoms, thereby recovering the copper in the form of a rougher froth concentrate.

machine 0.05 gm. xanthate, 0.10 gm. of copper sulfate and 1 dp. of frother consisting of a mixture of paraffine alcohols from 5 to 10 carbon atoms, thereby recovering the lead as a rougher froth concentrate, the rougher tailing (pulp remaining in the machine) being considered waste and drawn out of the machine. The rougher concentrates may be graded up as desired by methods known to the art.

EXAMPLE 13.

The following metallurgical results were obtained using the antimony agent and treating at mineral aggregate composed principally of

molybdenite and other sulfides such as those of copper and iron:

	Per Cent Weight		ays, Cent	Distril Per	Cent
	weight	Cu	MoS ₂	Cu	MoS ₂
Heading (computed) Rougher Tailing Cleaner Tailing Cleaner Conc	100.00 91, 19 5, 57 3, 24	34, 030 35, 800 22, 300 4, 250	1. 67 . 20 7. 60 33. 10	100.00 95.95 3.64 .41	100. 00 10. 78 25. 15 64. 07

Procedure

500 gm. of general flotation concentrate (Utah 15 Copper Co.) were subjected to flotation in the presence of an antimony agent (prepared by reacting 2 gm. Sb2O3, 1 gm. KOH and 1 gm. S in aqueous solution) whereby a rougher molybdenite concentrate and a rougher tailing were produced, the rougher molybdenite concentrate being subsequently cleaned, making a cleaner tailing and a cleaner concentrate.

EXAMPLE 14

A talcose lead-zinc ore containing galena, sphalerite and pyrite was treated with lime and copper sulfate and floated with sodium ethyl xanthate, a solution of thiocarbanilide in dicresyldithiophosphoric acid, and pine oil to give a bulk lead-zinc concentrate assaying 43.9% Pb, 4.1% Zn, 10.9% Fe and 16.5% insoluble mostly This concentrate was treated with 0.33 lb./ton of the reaction product of 1 part CaO and 1 part P2S5 and floated for 5 minutes without additional reagents to remove talc. Marked depression of sulfides took place resulting in a sulfide tailing assaying 52.6% Pb, 4.6% Zn, 13.0% Fe and 1.1% insoluble, representing recoveries of $90.2\,\%$ of the lead, $91.1\,\%$ of the zinc and $97.0\,\%$ of the iron but only 4.4% of insoluble originally 40 contained in the concentrate.

EXAMPLE 15

A lead concentrate was floated from a micaceous lead-zinc ore containing galena, sphalerite, and pyrite by the use of lime, sodium cyanide, copper sulfate, sodium ethyl xanthate, a solution of thiocarbanilide in dicresyldithiophosphoric acid, and pine oil. This concentrate, containing 43.1% insoluble mostly as micaceous material which floated readily with the sulfides and 19.6% Pb and 3.92% Zn, was conditioned with 0.37 lb./ton of a depressant formed by reacting in water 12 parts caustic soda with 9.0 parts sulfur, and 12 parts As₂O₃ in 70 parts of hot water and then refloated with 0.6 lb./ton pine oil. The resulting concentrate assayed 43.9% of Pb, 3.8% Zn and 6.7% insoluble, representing a recovery of 89.7% of the lead and 1.2% of the zinc.

EXAMPLE 16

From a carbonaceous gold ore assaying about 0.20 oz. Au/ton and about 1.5% C. and containing gold in association with pyrite, iron oxides, chalcopyrite and quartz a concentrate was floated using 0.3 lb./ton potassium ethyl xanthate, 0.03 lb./ton of a 1:1 mixture of sodium diethyl and disecondary butyl dithiophosphates and 0.05 lb./ton pine oil. This concentrate assayed 1.150 oz. Au/ton, 1.72% C., and 64.7% insoluble and represented a recovery of 91.3% of the gold. This amount of carbon interfered with cyanidation of the concentrate, causing reprecipitation of the gold to give cyanidation tailings assaying .53 oz. Au/ton.

A portion of the concentrate was conditioned with 2.5 lb./ton of a depressant prepared by reacting a 1:1 mixture of CaO and P₂S₅ at 70-80° C. in water to depress sulfides and refloated using in stages 0.12 lb./ton of a mixture of paraffine alcohols from 5 to 10 carbon atoms and 0.18 lb./ton fuel oil to remove the carbonaceous material. 89.7% of the gold remained in the sulfide tailing while the major portions of the carbon were removed in the froth. The sulfide tailing was subjected to cyanidation to give a tailing of 0.23 oz. Au/ton.

EXAMPLE 17

A 1:1 mixture of chalcocite and sericite and a 1:1 mixture of chalcocite and pyrophilite (all minerals minus 150 mesh and plus 325 mesh) were floated as follows:

(a) With 0.25 lb./ton of a mixture of paraffine alcohols from 5 to 10 carbon atoms alone and

(b) With 0.25 lb./ton of a mixture of paraffine alcohols from 5 to 10 carbon atoms and 1 lb./ton of a depressant formed by reacting 10 parts CaO with 1.0 part P₂S₅ in water at 70-80° C.

(c) With 0.25 lb./ton of a mixture of paraffine alcohols from 5 to 10 carbon atoms alone and with 0.1 lb./ton sodium secondary butyl xanthate and 0.1 lb./ton sodium secondary butyl dithiophosphate

(d) As in (c) but with 2.5 lb./ton of the depressant described in (b).

Ch	alcocite-Serici	te					
Treatment	per cent floated						
Treatment	Chalcocite Sericit						
a b c d	21. 3 4. 5 90. 8 9. 3	92. 3 90. 4 92. 0 91. 1					
Chalcocite-Pyrophilite							
		-					
(Treatment	per cent	floated					
Treatment		floated Pyrophilite					

EXAMPLE 18

One part arsenic sulfide was reacted with 4 parts sodium hydroxide in aqueous solution and diluted to a total of 100 volume parts of water. This depressant was used on a copper-molybdenite concentrate obtained by the flotation treatment of a copper ore from Utah. The following testing procedure was used on this concentrate:

An aqueous pulp of the flotation concentrate containing 500 gm. dry solids was conditioned in a laboratory Fagergren flotation machine with 14.64 lb. per ton 66° Bé. sulphuric acid, then conditioned with 9.6 lb. per ton commercial lime (CaO). Next was added sufficient depressant to give 3.0 lb. per ton (As₂O₃ basis) followed by 70 0.16 lb. per ton modified burner oil and higher alcohol frother as required. The froth was removed for a period of 7 minutes, constituting the rougher molybdenite concentrate. The major portion of the copper and iron sulphides remained 75 in the machine as the rougher tailing.

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The following table summarizes the metallurgical results obtained in this test:

Product	Weight, Per Cent	Assays, Per Cent		Distril Per	5	
		Cu	MoS ₂	Cu	Mo82	
Heading Rougher Tailing Rougher MoS ₂ Conc.	100, 00 89, 45 10, 55	34, 250 35, 350 25, 400	2, 21 , 13 20, 20	100.00 92.33 7.67	100.00 5.27 94.73	10

EXAMPLE 19

A depressant was prepared by treating 5.0 parts As₂S₅ with 50 volume parts of concentrated NH4OH. The mixture was agitated and allowed to stand overnight and then excess As₂S₅ was removed. 30 ml. of the resulting solution were used in a test on the ore employed in Example 18. Other details of the testing procedure were the same as described in Example 18. The following metallurgy was obtained.

Product	Weight, Per Cent	l C₁	s, Per ent		bution, Cent
	l d con	Cu	MoS ₃	Cu	MoS ₂
Heading Rougher Tailing Rougher MoS ₂ Conc.	100.0 94.8 5.2	34. 33 35. 70 9. 30	2.17 .16 38.70	100.0 98.6 1.4	100. 0 6. 9 93. 1

EXAMPLE 20

7.5 parts NaOH, 4 parts sulfur, and 20 parts water were reacted together with gentle heating until a red solution was formed and then 10 35 parts As₂O₃ were added and the reaction continued. The product was diluted to a total of 500 volume parts with water. This depressant was tested on the concentrate used in Example 18 and the test was identical to Example 18 except 40 that the quantities of acid and lime were 7.32 lb. and 4.0 lb. instead of 14.64 lb. and 9.6 lb., respectively, per ton of ore. Results follow:

Product	Weight,	Assay C	s, Per ent	Distri Per	bution, Cent
	Per Cent	Cu	MoSa	Cu	MoS ₂
Heading Rougher Tailing Rougher MoS ₂ Conc.	100.00 94.01 5.99	36. 450 36. 750 16. 700	1. 92 0. 03 35. 00	100.00 97.19 2.81	100.00 1.32 98.32

EXAMPLE 21

3.0 parts quick lime (84% available CaO), 6.0 parts sulfur, 0.9 part NaOH, and 75.0 parts of water were boiled together until the lime and sulfur dissolved and the resulting product then was boiled with about 4.5 parts of AsaO₂. The concentrate and testing procedure were identical to Example 18 except that the quantities of acid and lime were 7.32 ib. and 6.0 lb., respectively, per ton of ore. Results are listed below:

Product	Weight, Per Cent	Assays, Per Cent		Distribution, Per Cent	
ŧ'		Cu	MoS	Cu	MoS ₂
Heading Rougher Tailing Rougher MoS ₂ Conc	100, 00 91, 56 8, 44	33. 400 35. 000 11. 100	1. 56 0. 02 22, 45	100.00 97.15 2.85	100.00 0.94 99.06

EXAMPLE 22

56 lb. sulfur, 75 lb. NaOH and 50 gallons water

were reacted by boiling. 75 lb. As₂O₃ were then added and boiled with the mixture. A flotation test using this depressant in the procedure and on the concentrate described in Example 18 was conducted with the following metallurgical results:

Product .	Weight, Per Cent	Assays, Per Cent		Distribution, Per Cent	
		Cu	MoS ₂	Cu	MoS ₃
Heading Rougher Tailing Rougher MoS ₂ Conc.	100. 00 94. 81 5. 19	35. 700 37. 116 9. 850	1.86 0.02 42.10	100.00 98.57 1.43	100, 00 0. 86 99, 14

EXAMPLE 23

A depressant was prepared by mixing 50 gallons of the depressant described in Example 20 and 25 gallons of the depressant described in Example 22. The resulting product was used in a flotation test on the concentrate described in Example 1 and with the same testing procedure. Metallurgical results follow:

	Product	Weight,	Assays, Per Cent		Distribution, Per Cent	
0		Tel Cent	Cu	MoS ₂	Cu	MoS ₃
	HeadingRougher TailingRougher MoS ₂ , Conc	100. 0 96. 2 3. 8	32, 500 32, 700 6, 900	1.50 .05 47.20	100. 0 99. 2 0. 8	100.0 2.6 97.4

The above reaction products are typical of the class coming under the invention. Any alkaliforming metal may be used in place of the calcium, sodium, and ammonium radical used in these examples. Salts of strong bases and weak acids can be reacted as well as the hydroxides. Alkali and alkaline-earth cyanides form depressants, with arsenic and sulphur, and with phosphorus and sulphur of unknown composition.

EXAMPLE 24

The preliminary acid-lime treatment is not always necessary, particularly in treating ores; however, in treating concentrates containing residual collector agents such treatment is frequently essential in obtaining commercial results. This is demonstrated in the following two tests which compare the results obtained with and without the acid-lime treatment on the concentrate and with the testing method used in Example 18. The depressant used was that used in Example 23.

1	Heading:	
60	Per Cent Cu 33.500	33.500
•	Per Cent MoS ₂ 1.720	1.720
1	Rougher Tailings:	
	Per Cent Wgt 95,960	92,480
65	Per Cent Cu 34.000	34.400
,	Per Cent Distr. Cu 98.910	95.070
	Per Cent MoS ₂ 0.070	0.060
	Per Cent Distr. MoS ₂ 3.530	3.190
70 F	Rougher MoS ₂ Conc.:	
	Per Cent Wgt 4.040	7.520
	Per Cent Cu 9.000	21.900
	Per Cent Distr. Cu 1.090	4.930
	Per Cent MoS ₂ 45.300	22,200
75	Per Cent Distr. MoS ₂ 96.470	96.810

Agents added, lb. per ton:		
Sulphuric Acid	14.64	
Lime (Commercial)	10.00	
Depressant (As ₂ O ₃ basis)	3.00	3.000
Modified Burner Oil		0.160
Alcohol Frother	0.16	0.160

The above two tests show marked improvement in the grade of the rougher molybdenum concentrate in both tests. While better results were obtained with the acid-lime treatment, good results, in fact nearly 1300 percent increase in grade, were obtained without the use of acid and lime. The quality of the froth favors the acidlime treatment.

EXAMPLE 25

A copper-molybdenum concentrate obtained by flotation treatment of a Utah ore was treated in 500 gm. Fagergren flotation machine. To the charge of about 500 gm. of concentrate (dry basis) and water were added the following agents in 20 the amounts designated:

1 ml. sulphuric (H₂SO₄) 66° Bé.

1 gm. lime (CaO)

25 ml. of the reaction produce (2 gm. CaO 20 ml. H₂O and 1 gm. arsenic sulphide) made up to 50 ml. for testing.

2 dps. molybdenite collector (burner oil, modified)

In the flotation that followed, substantially all the molybdenite was removed as a froth concentrate, making (1) a rougher tailing and a rougher concentrate. The rougher concentrate was cleaned, making (2) a cleaner tailing and (3) a cleaner concentrate containing substantially all the molybdenite, the depressed copper and iron 35 the 14-day test period were as follows: sulphides remaining in the rougher tailing.

The results of this test may be seen from the following metallurgical tabulation

TOHOWING INCUMIN	urgicai	vabula	01011.			
	Per Cent	Per Cen	t Assays	Per Cer	nt Distr.	40
	Weight	Cu	MoS ₂	Cu	MoS ₃	٠.
Heading Rougher Tailing Cleaner Tailing Cleaner Concentr	100.00 83.68 14.17 1.95	31.76 31.50 37.10 4.20	1. 130 . 040 2. 280 56. 100	100.00 83.19 16.56 , 25	100.00 2.34 22.26 75.40	45

EXAMPLE 26

Samples of the copper molybdenum concentrate described in Example 18 were obtained daily over a 14-day period and a laboratory flotation test conducted on each sample thus obtained. 14.64 lb./ton sulfuric acid and 10.00 lb./ton lime were used in each test. The depressant used was the same as that described in Example 23. The average of the 14-day laboratory test series are as follows:

Conditioning Agents, Per Ton	14-Day Aver- age Results, 14.64 Lb. H ₂ SO ₄ , 10.00 Lb. Lime
Heading: Per Cent Cu Per Cent MoS ₂	34. 543 1. 49
Rougher Tailing: Per Cent Wgt	94.01
Per Cent Cu	
Per Cent CuPer Cent Distr. Cu	98.46
Per Cent MoS ₂	0.075
Per Cent Distr. MoS2	3.44
Rougher MoS ₂ Concentrate:	
Per Cent Wgt	5, 99
Per Cent Cu	8. 681
Per Cent Distr. Cu	1.54
Per Cellt MOS2	.] 41.0%
Per Cent Distr. MoS2	. 96.56
Agents, Lb. Per Ton:	1
Depressant	3.0
Depressant MoS ₂ Collector	0.16
Alcohol Frother	0.16

EXAMPLE 27

Samples of copper-molybdenum concentrate obtained by the flotation of a Utah ore were treated as in Example 18 with a depressant consisting of a 1:1 mixture of a NaSH and As2O3 in solution. A flotation test using 4.8 lb./ton of depressant according to the procedure of Example 18 was conducted. The feed to flotation assayed about 33.5% Cu and 1.27% MoS2. Metallurgical results follow:

Concper cent Cu assay	22.81
Concper cent MoS2 assay	16.09
Concper cent Cu-distribution	4.47
Concper cent MoS2-distribution	85.64

A cleaner float was conducted on the concentrate from this test to produce a concentrate assaying 9.72% Cu and 28.04% MoS₂, representing a recovery of about 1% of the total copper and 74.71% of the total MoS₂.

EXAMPLE 27a

It was found that calcium chloride was an effective conditioning agent and may be used in place of acid. The 14-day samples described in Example 23 were conditioned with 6.0 lb./ton calcium chloride and then with 2.0 lb./ton lime instead of the H2SO4-lime combination used in Example 23. The depressant, MoS2 collector and frother were the same as in Example 23. Average results of

Heading	
---------	--

Per cent wgt		9:	2.
Per cent Cu		35	5
Per cent Cu-d	lst	9	7.
Per cent MoS2			0
Per cent MoS2	-dist		2.

Per cent MoS2_____

Per cent Cu__

Let cent Mo	1.10
Per cent Cu	11.936
Per cent Cu-dist	2.50
Per cent MoS2	23.43
Per cent MoS2-dist	97.06

EXAMPLE 28

Other effective compounds for conditioning the 60 pulp prior to the depression of copper minerals art: magnesium chloride, magnesium sulfate, sodium chloride, sodium sulfide, ammonium chloride, barium chloride, calcium acetate, and calcium hypochlorite. Following the conditioning 65 operation with these compounds, lime is added for pH adjustment.

Examples of the use of several of these conditioning agents follow employing 500 gram charges of Utah Copper Co. general flotation concen-70 trate in a laboratory Fagergren flotation machine. The pulp was agitated first with a specified conditioning agent, next with lime, then with 3.0 lb./ton (As2O3 equivalent) of the mixed depressant of Example 23 and floated for 7 min-75 utes with 0.16 lb./ton of modified burner oil

Product	Weight,	Assays, Per Cent		Distribution, Per Cent	
	Per Cent	Cu	MoS ₂	Cu	MoS ₂
CONDITIONER, 2.0	GM. MgC	lı; MOI	OIFIER	, 0.5 GM	. LIME
Heading (calc.)	100. 00 90. 67 9. 33	28. 443 30. 150 11. 850	1. 91 0. 07 19. 80	100.00 96.11 3.89	100, 00 3, 32 96, 68
CONDITIONE MOI	R, 2.0 GM DIFIER, 1	. CALC	IUM AC LIME	DETATI	G;
Heading (calc.) Rougher tailing Rougher conc	100.00 95.88 4.12	32, 202 33, 100 11, 300	1. 93 0. 09 44. 80	100.00 98.55 1.45	100.00 4.47 95.53
CONDITIONER, 0.1 MOI	GM. Cus	O4.5H2O),5 GM.	PLUS LIME	1.5 GM	. CaCl ₂ ;
Heading (calc.) Rougher tailing Rougher concentrate	100. 00 94. 85 5. 15	30. 460 31. 500 11. 300	2. 05 0. 10 37. 90	100, 00 98, 09 1, 91	100.00 4.64 95.36
CONDITIONER, 1.5	GM. C	ALCIUI	M HYI LIME	OCHLO	ORITE;
Heading (calc.) Rougher tailing Rougher concentrate	100. 00 93. 94 6. 06	37. 643 39. 000 16. 000	2. 23 0. 05 36. 00	100.00 97.33 2.67	100.00 2.11 97.89

EXAMPLE 29

Heavy metals may replace the alkali-forming metals in the preparation of depressants. For example, the depressants may be prepared as described and then reacted with a metal salt prior to adding to the pulp as in the following comparative tests:

Identical 500 gm. samples of the concentrate described in Example 18 were floated in exactly the same manner, except that in the first test the depressant used in Example 20 was employed and in the second test the reaction product of this depressant with copper sulfate was used. Acid-lime conditioning was employed in both tests as shown in the table of results.

	Original Depressant	Depressant Reacted With CuSO ₄
Heading:		;
Per Cent Cu	34, 760	34, 760
Per Cent MoS ₂	1, 178	1, 178
Rougher Tailing:		
Per Cent Wgt	95, 34	96, 93
Per Cent Cu	35, 600	35, 450
Per Cent Distr. Cu	97, 55	98, 91
Per Cent MoS	0.04	0.01
Per Cent Distr. MoS2	3, 25	3, 29
Rougher Concentrate:		0.20
Per Cent Wgt	4.66	3, 07
Per Cent Cu	18.35	12.40
Per Cent Distr. Cu.	2.45	1. 19
Per Cent MoS	24.35	37, 40
Per Cent Distr. MoS2	96.75	96, 71
A frante added (lb. non ton).	******	00.11
Sulphuric Acid.	7.32	7. 32
Lime	6.00	6.00
Depressant (As2O2 basis)	3.00	3.00
Modified Burner Oil	.16	. 16
Higher Alcoholic Frother		
Trigmen Altoonionic Plottici	. 16	. 16

EXAMPLE 30

A depressant was prepared by reacting 0.2 gm. CuS (finely powdered) with 8 cc. of the depres-

16 reacted residue was filtered off and discarded. The tests described below compare equal quantities of both depressants (As2O3 basis) in the treatment of a copper-molybdenum concentrate obtained by flotation of a Utah ore.

	Original Depressant	Cu8 Reaction Product
Heading:		
Per Cent Cu	31.700	31,700
Per Cent MoS ₁	1.02	
Rougher Tailing:		1.02
Per Cent Wat	95, 80	95, 87
Per Cent Cu	31.450	PU. 01
Per Cent Distr. Cii	07:39	
Per Cent MoS2	0.08	0.04
Per Cent Distr. MoS2	6.49	3, 18
Rougher Concentrate:	0, 15	9, 10
Per Cent Wgt	4.20	4, 12
Per Cent Cn	10 000 1	21, 100
Per Cent Distr. Cu	2.68	21.100
Per Cent MoS2	26.40	28.00
Per Cent Distr. MoS2	93.51	96. 82
Agents added (lb. per ton):	20.01	80.02
Sulphurie Acid	7.32	7.32
Lime		6.00
Depressant (As ₂ O ₃ basis)	3.00	3.00
Modified Burner Oil	.16	
Higher Alcohol Frother		.16
TIBEC MOUNT FLOWER.	.16	1.16

The same depressant was reacted with zinc. sulphate and the reaction product added to the pulp. The feed to the flotation machine was 30 Utah Copper Company general flotation concentrate. Details of the testing are listed below.

5		Original Depressant	Depressant Reacted With ZnSO ₄
	Heading:		
	Per Cent Cu	38, 310	38, 310
_	Per Cent MoS	1,573	1.573
)	Rougher Tailing:		2.0.0
	Per Cent Wgt	95.78	96. 61
	Per Cent Cu	30 350	39.350
	Per Cent Distr. Cu	98.43	99.18
	Per Cent MoS	0.11	0.10
	Per Cent Distr. MoS2	6.69	6.15
	Rougher Concentrate:		
5	Per Cent Wgt	4.22	3.99
u	Per Cent Cu	14.000	9.000
	Per Cent Distr. Cu	1.57	0.82
	Per Cent MoS2	34.70	43.70
	Per Cent Distr. MoS:	93. 31	93.85
	Agents added (lb. per ton): Sulphuric Acid.		
	Sulphuric Acid	7.32	7.32
_	Lime	6.00	6.00
0	Depressant (As ₂ O ₂ basis)	3.00	3.00
	Modified Burner Oil	.16	. 16
	Higher Alcohol Frother	.16	.16

Other metals tested include iron, lead, chromium, aluminum, molybdenum, etc. The products of the reactions of the above depressant with the following are specific examples: ferrous sulphate, lead nitrite, chromium nitrite, aluminum sul-60 phate, ammonium molybdate.

EXAMPLE 31

Other metals may replace the alkali-forming 65 metals in the preparation of depressants. For example, the depressants may be prepared as described and then reacted with a metal salt prior to adding to the pulp as in the following comparative tests:

Identical 500 gm. samples of the concentrate described in Example 18 were floated in exactly the same manner, except that in the first test the depressant used in Example 20 was employed and in the second test the reaction product of this sant described in Example 29. A trace of un- 75 depressant with copper sulfate was used. Acid-

lime conditioning was employed in both tests as shown in the table of results.

	Original Depressant	Depressant Mixed with CuSO ₄	5
Heading: Per Cent Cu Per Cent MoS2.	34. 760 1. 178	34.760 1.178	10
Per Cent Wgt	95.34	96. 93 35. 450	
Per Cent Cu	97. 55 0. 04	98. 91 0. 04	
Per Cent Distr. MoS ₂	3. 25	3.29	
Per Cent Wgt	18.35	3.07 12.40 1.19	15
Per Cent Distr. Cu Per Cent MoS ₂ Per Cent Distr. MoS ₂	24.35	37.40 96.71	
Agents added (lb. per ton): Sulphuric Acid	7.32	7.32	
Depressant (As ₂ O ₃ basis)	3.00	6.00 3.00	20
Modified Burner Oil Higher Alcohol Frother		.16	

EXAMPLE 32

The metallic salt used in forming a metallic type depressant need not be soluble in water as indicated by the following:

A depressant was prepared by reacting 0.2 gm. CuS (finely powdered) with 8 cc. of the depressant described in Example 20. A trace of unreacted residue was filtered off and discarded. The tests described below compare equal quantities of both depressants (As2O3 basis) in the treatment of a copper-molybdenum concentrate obtained by flotation of a Utah ore according to the procedure of Example 31.

31.700 1.02	31.700
1.02	
	1.02
	ł
95, 80	95.87
31, 450	
97.32	
0.08	0.04
6.49	3, 18
0. 10	3.20
4, 20	4, 13
	21, 100
	28.00
	96.82
	19. 800 2. 68 26. 40 93. 51

Thus, even with an insoluble metallic compound such as copper sulfide a potent depressant was prepared.

EXAMPLE 33

The same depressant was reacted with zinc sulphate and the reaction product added to the pulp,

following the method of Example 31. Details of the testing are listed below.

	Original Depres- sant	Depressant Reacted WithZnSO ₄
Heading:		
Per Cent Cu	38, 310	38.310
Per Cent MoS ₂	1,573	1,573
Rougher Tailing:		1
Per Cent Wgt	95.78	96, 61
Per Cent Cu	39, 350	39, 350
Per Cent Distr. Cu	98.43	99, 18
Per Cent MoS	0.11	0.10
Per Cent Distr. MoS	6,69	6.15
Rougher Concentrate:	0.00	1
	4, 22	3,39
Per Cent Wgt	14,000	9,000
Per Cent Cu	1.57	0.82
Per Cent Distr. Cu	34.70	43.70
Per Cent MoS		93.85
Per Cent Distr. MoS2	93, 31	83.80

EXAMPLE 34

The metal salt depressants apparently are 20 formed in the flotation pulp by treating the ore with an alkali salt depressant in the presence of a suitable metal salt compound. As illustrated by the following comparative metallurgical results, effective depressants result from this method of treatment. In obtaining the results, given in the following table, the depressant of Example 20 was used according to the procedure of Example 31. In the first test this alkali type depressant was used alone; in the second test copper sulfate was added to the cell after the acid treatment followed by treatment with the alkali depressant. Excellent results were obtained in both tests with improved recovery and grade in the second test.

Heading: 39,87% Cu; 1.742% MoS2

rinal essant th SO ₄ ded Cell
95, 50
41.20
98. 52
1.69
4, 50
13, 20
1.48
37.50
98.31

EXAMPLE 35

Several metal salts were added to the pulp as described in Example 34. The testing method was that used in Example 31 and the alkali depres- 55 sant was that used in Example 20. The metal salts were added after the treatment with acid as indicated above. In the first test the alkali type depressant only was used; an improvement in the concentrate grade of MoS2 was obtained in all following tests employing the metal salts.

Heading: 35.91% Cu; 1.529% MoS2

Metal Salts Used	None	CuSO ₄	FeSO ₄	ZnSO4	Pb(No3):	Cr(No3):	Al ₂ (8O ₄) ₃
Metal Salt Added (lb. per ton). Rougher Tailing: Per Cent Wt. Per Cent Cu. Per Cent Distr. Cu. Per Cent MoS2. Per Cent Distr. MoS2. Rougher Concentrate: Per Cent Wt. Per Cent U. Per Cent Distr. Cu. Per Cent Distr. Cu. Per Cent MoS2. Per Cent MoS2.	None 91, 32 37, 70 96, 31 , 050 2, 66 6, 86 13, 65 3, 69 17, 40 97, 34	0.10 93.57 38.00 98.81 .050 3.03 6.43 6.70 1.19 23.40	0. 40 91. 77 37. 60 97. 05 . 040 2. 46 8. 23 12. 750 2. 95 17. 80 97. 54	0. 40 91. 95 38. 10 97. 36 . 040 8. 05 11. 80 2. 64 18. 20 97. 54	0. 40 92. 35 37. 90 97. 63 . 040 2. 46 7. 65 11. 10 2. 37 18. 90 97. 50	0. 40 92. 65 38. 50 98. 21 2. 50 7. 35 8. 85 1. 79 20. 40 96. 17	0. 40 93. 28 38. 00 98. 72 0. 04 2. 63 6. 72 6. 80 1. 28 20. 40 97. 38

This application is in part a continuation of our earlier now abandoned copending application Serial No. 530,350, filed April 10, 1944.

We claim:

1. A froth flotation process which comprises subjecting an aqueous pulp containing a mineral included in the group consisting of molybdenum sulfide, carbon, strongly hydrophobic hydrous aluminum-containing silicates and strongly hyleast on sulfide mineral, to froth flotation in the presence of an inorganic compound of an element selected from the group consisting of phosphorus, arsenic and antimony, said compound containing bivalent sulfur and an inorganic cation, said 15 compound being present in amounts sufficient to depress the sulfide minerals without substantial depression of molybdenum sulfide, carbon, strongly hydrophobic hydrous aluminum-containing silicates and strongly hydrophobic hydrous mag- 20 nesium silicates and an oil collector for said minerals selected from the group consisting of hydrocarbons, water insoluble alcohols and mixtures, the collector being present in sufficient amounts to float molybdenum, sulfide, carbon, strongly hydrophobic hydrous aluminum-containing silicates and strongly hydrophobic hydrous magnesium silicates, removing a concentrate relatively rich in the said minerals and relatively poor in the depressed sulfide mineral.

2. A process according to claim 1 in which the depressant is a compound of phosphorus.

- 3. A process according to claim 2 in which the only mineral floated in the presence of the inorganic compound of phosphorus is molybdenite.
- 4. A process according to claim 3 in which the ore is conditioned with an acid and an alkali prior to flotation.
- 5. A process according to claim 4 in which the ore is additionally conditioned with a soluble salt 40 of calcium.
- 6. A process according to claim 1 in which the only mineral floated in the presence of the inorganic compound of phosphorus, arsenic or antimony is molybdenite.

- 7. A process according to claim 6 in which the ore is conditioned with an acid and an alkali prior
- 8. A process according to claim 7 in which the ore is additionally conditioned with a soluble salt of calcium.

9. A process according to claim 1 in which the depressant is a compound of arsenic.

10. A process according to claim 9 in which the drophobic hydrous magnesium silicates and at 10 only mineral floated in the presence of the inorganic compound of arsenic is molybdenite.

11. A process according to claim 1 in which the ore pulp contains molybdenite and a sulfide of

12. A process according to claim 11 in which the depressant is a compound of phosphorus.

13. A process according to claim 12 in which the depressant is a reaction product of phosphorus pentasulfide and an alkali-forming hydroxide.

14. A process according to claim 13 in which the alkali-forming metal hydroxide is sodium hy-

15. A process according to claim 13 in which the alkali-forming metal hydroxide is calcium hy-25 droxide.

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