

DECLARATION IN SUPPORT OF A CONVENTION
APPLICATION FOR A PATENT OR PATENT OF ADDITION

(1) Here insert (in full) Name of Company.

In support of the Convention Application made by⁽¹⁾.....
Telefonaktiebolaget LM Ericsson of S-126 25 STOCKHOLM SWEDEN
a company organized under the laws of Sweden

(hereinafter referred to as the applicant) for a Patent

(2) Here insert title of Invention.

for an invention entitled:⁽²⁾.....
A METHOD AND ARRANGEMENT FOR SUPPLYING DIRECT CURRENT TO A
TELEPHONE LINE

(3) Here insert full Name and Address, of Company official authorized to make declaration.

I,⁽³⁾ Tage Lövgren, Mickelsbergsvägen 134, S-126 63 HÄGERSTEN SWEDEN
of Ake Stavling, Högbergsgatan 11, 2trp, S-116 45 STOCKHOLM SWEDEN

do solemnly and sincerely declare as follows:

1. ~~XXXX~~ ^{We are} authorized by the applicant for the patent to make this declaration on its behalf.

2. The basic application as defined by Section 141 of the Act was made in⁽⁴⁾ Sweden on the 1st day of February 19 90, by Telefonaktiebolaget LM Ericsson on the _____ day of _____ 19 _____, by _____

(4) Here insert basic Country or Countries followed by date or dates and basic Applicant or Applicants.

3. ⁽⁵⁾ 1) Bengt Gustav Löfmark, Torpgläntan 4, S-127 41 SKÄRHOLMEN SWEDEN 2) Jan Ored Håkan Oredsson, Näckrosvägen 21, 6trp, S-171 31 SOLNA SWEDEN 3) Claes Johan Anders Lindberg, Malmvägen 41, S-191 61 SOLLENTUNA SWEDEN

(5) Here insert (in full) Name and Address of Actual Inventor or Inventors.

is/are the actual inventor of the invention and the facts upon which the applicant is entitled to make the application are as follow:

The applicant is the assignee of Bengt Gustav Löfmark, Jan Ored Håkan Oredsson and Claes Anders Lindberg

4. The basic application referred to in paragraph 2 of this Declaration was _____ the first application made in a Convention country in respect of the invention the subject of the application.

DECLARED at Stockholm, Sweden
this 15th day of August 19 91

(6) Signature.

(6) TELEFONAKTIEBOLAGET LM ERICSSON

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(10) 646836

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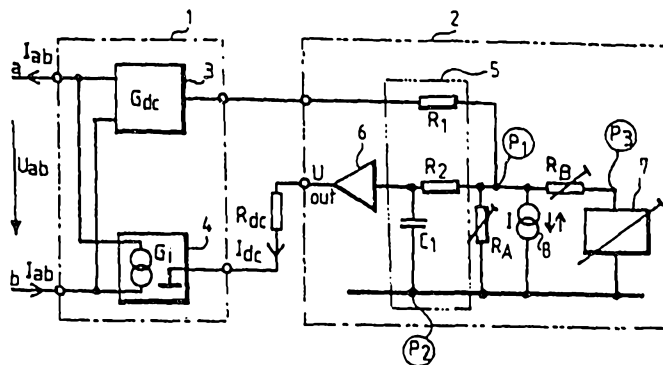
controlling a supply resistance of said circuit across said telephone line when said first current has a value greater than said limit line current value (I_{lim}) by a second adjustable resistor (R_E), wherein said second adjustable resistor (R_B) is electrically connected in series with an adjustable voltage limiter (7) and said series connection being further connected in parallel with said capacitive part of the lowpass filter; and

controlling said limit line current value (I_{lim}) at which limitation of said first current (I_{ab}) occurs, by an adjustable reference voltage level of said adjustable voltage limiter.

INTERNATIONAL APPLICATION PUBLISHED UNDER THE PATENT COOPERATION TREATY (PCT)

<p>(51) International Patent Classification ⁵ : H04M 19/00</p>	<p>A1</p>	<p>(11) International Publication Number: WO 91/11876 (43) International Publication Date: 8 August 1991 (08.08.91)</p>
<p>(21) International Application Number: PCT/SE90/00804 (22) International Filing Date: 5 December 1990 (05.12.90) (30) Priority data: 9000366-6 1 February 1990 (01.02.90) SE (71) Applicant: TELEFONAKTIEBOLAGET LM ERICSSON [SE/SE]; S-126 25 Stockholm (SE). (72) Inventors: LÖFMARK, Bengt, Gustav ; Torpgläntan 4, S-127 41 Skärholmen (SE). OREDSSON, Jan, Ored, Håkarn ; Näckrosvägen 21, 6trp, S-171 31 Solna (SE). LINDBERG, Claes, Johan, Anders ; Malmvägen 41, S-191 61 Sollentuna (SE).</p>		<p>(74) Agents: LÖVGREN, Tage et al.; Telefonaktiebolaget LM Ericsson, S-126 25 Stockholm (SE). (81) Designated States: AU, BR, CA, FI, JP, KR, NO. Published With international search report. 646836</p>

(54) Title: A METHOD AND ARRANGEMENT FOR SUPPLYING DIRECT CURRENT TO A TELEPHONE LINE



(57) Abstract

The present invention relates to a method and an arrangement for supplying direct current to a telephone line (ab). According to the invention, the current supply characteristic is programmable. The arrangement comprises a direct current supply circuit which detects the line voltage (U_{ab}) and supplies a line current (I_{ab}) in accordance with a preprogrammed current supply characteristic. The circuit includes a first more high-voltage part (1) and a second more low-voltage part (2), in which programming of the current supply characteristic takes place. For the purpose of achieving programming, a first resistive component (R_A) having a programmable resistance is arranged essentially parallel with a capacitor (C_1) in the second part (2). The first resistive component determines the supply resistance of the circuit for low line currents. For the purpose of programming the characteristic, the circuit also includes a voltage limiting element (7) having a programmable reference voltage connected in series with a second resistive component (R_B) having a programmable resistance, which are arranged substantially in parallel with the capacitor (C_1). The reference voltage determines a limit line current (I_{lim}) at which current limitation occurs and the second resistive component (R_B) determines, together with the first resistive component (R_A) the supply resistance of the circuit at current limitation. Finally, the polarity of the idling voltage (E) of the circuit is also programmable.

A METHOD AND ARRANGEMENT FOR SUPPLYING DIRECT CURRENT TO A TELEPHONE LINE

TECHNICAL FIELD

5 The present invention relates to the supply of direct current to a telephone line in a telecommunication system. More particularly, but not exclusively, the invention relates to a method and an arrangement for varying the current supply characteristic within the framework of a given pattern by programming.

PRIOR ART

10 In a telephone exchange, a SLIC-circuit (Subscriber Line Interface Circuit) is responsible, among other things, for supplying direct current to the telephone line and its subscriber, corresponding to the SLIC-circuit. Current supply is achieved in the SLIC-circuit with the aid of an electronic control system, which detects the
15 line voltage and delivers a corresponding line current. In this way it is possible to imitate the function of a conventional, resistively supplied system, although constant current supply can also be achieved. The supply resistance, and therewith also the supply current, can be determined through the selection of
20 external resistors. The current supply function of an SLIC-circuit of known kind is found described in Ericsson Review No. 4, 1983.

Also belonging to the known technology is the line circuit BIMOS Line Interface Circuit (BLIC) found described in IEEE Journal of
25 Solid-State Circuits, Vol Sc-21, No. 2, April 1986 pages 252-258. The line circuit includes a DC-loop operative to supply direct current to a corresponding telephone line. The line circuit (BLIC) operates in the opposite manner to the aforesaid SLIC-circuit, since it senses line current and supplies line voltage.

30 Also known to the prior art is a feedback loop for the supply of direct current in a MALC-system. This system is described in MOTOROLA, Technical Developments, Volume 7, October 1987, pages

77-79. The supply characteristics illustrated in Figure 1 can be divided into three parts, voltage supply $V_L=V_F$, current supply $I_L=I_F$ and resistive supply, said circuit being similar to a current source having an internal resistance R_F . Figure 2
5 illustrates the circuit with which the supply characteristic illustrated in Figure 1 is obtained. The parameters V_F , R_F and I_F are programmable. The circuit produces a constant voltage $V_L=V_F$, since the circuit includes a transconductance amplifier OTA, so that very high voltage amplification is achieved.

10 DISCLOSURE OF THE INVENTION

The primary drawback with the SLIC-circuit is that the supply characteristic cannot be programmed. Consequently, when delivering SLIC-circuits to different countries, it is necessary to produce different circuits for countries in which different
15 requirements of current supply characteristics prevail. The circuits are different, inter alia, because the resistor R_3 , which is connected externally, varies.

A further drawback with the SLIC-circuit is that the equivalent inductance of the circuit is not constant when the current supply
20 resistance varies. This means that the reaction times of the current supply loop are dependent on the current supply characteristic and can be unfavourably long in certain instances.

The problem with the d.c. supply feedback loop of the MALC-system resides in the configuration of the current supply characteristic.
25 At constant line voltage, $V_L=V_F$ in Figure 1, infinite amplification is required, which in turn makes it difficult to maintain a stable DC-loop. At constant current, $I_L=I_F$ in Figure 1, problems can occur together with subscriber equipment with current limitation. If current limitation in the subscriber equipment
30 occurs at the same current as the current limitation in the DC-loop, low-frequency self-oscillation can occur.

Accordingly, the object of the present invention is to provide a direct current supply circuit which detects line voltage and

supplies line current, and the current supply characteristic of which is suitable for supplying direct current to the subscriber line, while enabling the current supply to be varied by programming.

5 A further object of the invention is to provide a current supply circuit having short reaction times, so that the circuit is able to react quickly to a change in line voltage, by changing the line current in a corresponding manner.

10 The desired functions of the direct current supply are obtained with the inventive method and the inventive current supply circuit. The circuit includes a voltage converter for detection and level-adjustment of the line voltage, a lowpass filter which comprises a capacitor and intended to filter-off speech signals, a buffer amplifier connected to the lowpass filter, and a resistor
15 connected to the output of said amplifier. The output voltage from the buffer amplifier delivers current through the resistor to a current amplifier, which supplies the actual line current.

Programming of the current supply characteristic is achieved by arranging a first resistive component having a programmable
20 resistance substantially in parallel with the capacitor in the lowpass filter. For the same purpose, a voltage limiting element having a programmable reference voltage is also connected in series with a second resistive component having a programmable resistance, which are arranged substantially parallel with said
25 capacitor. Finally, a current generator is also arranged substantially in parallel with the capacitor. The generator generates a current having a programmable direction and optionally also a programmable magnitude. Thus, all changes in the current supply characteristic are effected by shunt coupling of the capacitor in
30 the lowpass filter. The circuit hereby supplies the line current in accordance with a predetermined current supply characteristic.

The current supply characteristic according to the present invention includes four programmable parameters. The first of

these parameters is the supply resistance to low line currents, the second is an interruption point at which current limitation occurs, the third is the supply resistance of the circuit at current limitation and the fourth is the open circuit voltage of the circuit, wherein the polarity of the idling voltage can be programmed and optionally also its size. Thus, these four parameters are programmed with the aid of said programmable components. Because all changes in the current supply characteristic are effected as a shunt coupling of the capacitor included in the lowpass filter, the equivalent inductance of the current supply circuit, seen from the line side, will be constant, independently of both the current supply characteristic and the operation point. The advantage afforded by the constant inductance is that the reaction time of the current supply loop will be short. A constant inductance is obtained because the amplification-bandwidth-product in the current supply circuit becomes constant when shunt coupling the capacitor.

The advantage afforded when the current supply characteristic can be programmed is that one and the same circuit can be manufactured for different countries in which different requirements on current supply characteristic prevail. The desired current supply characteristic can then be programmed, for instance in conjunction with an operational start.

The inventive current supply characteristic has advantages over the characteristic in the MALC-system. The inventive circuit does not generate a constant line voltage and consequently does not have infinite amplification, therewith avoiding stability problems. Instead, there is used in accordance with the invention a negative resistance wherewith a sufficiently low current supply resistance is generated for the voltage drop to be practically negligible. For the purpose of avoiding the aforesaid problem associated with constant current supply, the current supply will always have a resistive character, even with current limitation. Furthermore, the responsiveness to tolerances in the components is smaller compared with the d.c. supply circuit of the MALC-system. This is because the inventive circuit, in a fundamental

state, in which the first and the second resistive components are infinitely large, has a d.c. voltage amplification through the lowpass filter and buffer amplifier which is identical to one, whereas corresponding amplification in the realization with the transconductance amplifier is determined by the quotient between two resistances and is thus determined by the tolerances thereof.

BRIEF DESCRIPTION OF THE DRAWINGS

The inventive method and arrangement will now be described in more detail with reference to an exemplifying embodiment thereof and with reference to the accompanying drawings, in which Figure 1 illustrates an inventive current supply circuit, and Figure 2 illustrates the supply characteristic of the current supply circuit.

BEST MODE OF CARRYING OUT THE INVENTION

Figure 1 illustrates the inventive direct current supply circuit. This circuit is connected to a telephone line ab for supplying direct current thereto, said circuit detecting the line voltage U_{ab} and, via a feedback loop, supplying corresponding line current I_{ab} in accordance with a preprogrammed direct current supply characteristic.

The circuit includes a more high-voltage part 1 and a second more low-voltage part 2, in which programming of the current supply characteristic takes place. A voltage converter 3 in the more high-voltage part 1 is connected to the telephone line ab for the purpose of detecting line voltage U_{ab} . The line voltage U_{ab} is adapted in the voltage converter 3 to a lower voltage level capable of being handled in the more low-voltage part 2, in which programming of the current supply characteristic takes place. The voltage converter 3 delivers across its output to the low-voltage part a voltage which corresponds to the line voltage multiplied by a conversion factor G_{dc} which is much smaller than one. The output voltage U_{out} from said more low-voltage part supplies current I_{dc} to a current amplifier 4, via a resistor R_{dc} , which amplifies the



current I_{dc} with a factor G_1 and supplies the actual line current I_{ab} . The voltage converter 3 and the current amplifier 4 in the more high-voltage part 1 are included in the aforementioned SLIC-circuit.

5 The more low-voltage part includes a lowpass filter 5 comprising an RC-circuit. The function of the lowpass filter is to block signals at speech frequency. The lowpass filter 5 includes a first and a second resistor R_1 , R_2 and a capacitor C_1 . The second resistor R_2 is much more low-ohmic than the first resistor R_1 and
10 may optionally be zero ohm. One terminal of the first resistor R_1 is connected to the output of the voltage converter 3 and the other terminal is connected to one terminal of the second resistor R_2 . One terminal of the capacitor C_1 is connected to the other terminal of the second resistor R_2 . Also connected to this latter
15 terminal is the input of a buffer amplifier 6. The output of the buffer amplifier 6 is connected to said resistor R_{dc} . The function of the buffer amplifier 6 is to form a buffer between the more low-voltage part 2 and the resistor R_{dc} , so that said resistor will not be loaded to a greater extent than the more low-voltage part 2. As
20 beforementioned, the output voltage U_{out} from the buffer amplifier 6 supplies current to the current amplifier 4, through the resistor R_{dc} . The more low-voltage part 2 forms, together with the resistor R_{dc} said feedback loop.

All influence of the current supply characteristic takes place
25 between a first node P_1 , between the first and the second resistor R_1 , R_2 , and a second node P_2 at the other connection of the capacitor C_1 , i.e. substantially parallel with said capacitor. Four components are responsible for variation of the current supply characteristic, these components being a first resistive
30 component R_A having programmable resistance, a second resistive component R_B having programmable resistance, a voltage limiting element 7 having a programmable reference voltage, and a current circuit 8 which generates a generator current I in a programmable direction or sense, and optionally also a programmable magnitude.
35 The first resistive component R_A is connected between said first and second nodes P_1 , P_2 . The second resistive component R_B is con-

ected between said first node P_1 and the one connection of the voltage limiting element 7. The other connection on the voltage limiting element is connected to the second node P_2 . Referring once more to the second resistor R_2 in the lowpass filter, the purpose of this resistor is to attenuate noise and interference that can occur in the voltage limiting element 7, and in other respects has no influence on the current supply characteristic. The current circuit 8 is connected between said first and said second nodes P_1 , P_2 , in order to generate said generator current I which determines the open circuit voltage E of the current supply circuit. The voltage E is a function of said current I , the first resistor R_1 in the lowpass filter 5 and the conversion factor G_{dc} in the voltage converter 3, $E = I \cdot R_1 / G_{dc}$. The current direction determines the polarity of the voltage.

Figure 2 illustrates the current supply characteristic which can be obtained with the described circuit. The Figure also indicates how the characteristic can be changed with the aid of the earlier mentioned programmable components in the more low-voltage part 2 of the current supply circuit.

The current supply characteristic in Figure 2 shows the line current I_{ab} as a function of the line voltage U_{ab} . The appearance of the characteristic depends on the supply resistance R_{feed} of the current supply circuit (internal resistance) which can be varied by varying the aforesaid variable parameters. Thus, the line current I_{ab} is a function of the circuit supply resistance R_{feed} and of the line voltage U_{ab} , $I_{ab} = (R_{feed}, U_{ab})$. In order to enable the circuit to be understood more readily, it can be said to be in a fundamental state with respect to the supply resistance when the first and the second resistive components R_A , R_B are very high-ohmic, i.e. the lines which connect these components are considered as being clipped. When in the fundamental state, the supply resistance is determined by the conversion factor G_{dc} , the current amplification factor G_i and the resistance R_{dc} , $R_{feed} = R_{dc} / (G_i \cdot G_{dc})$. Referring back to Figure 2, in which the resistive components R_A , R_B have resistance values which can be used in practice, so that these will also determine the circuit supply

resistance. The characteristic exhibits two mutually connected lines, a first line A and a second line AB. The lines A, AB illustrate that the circuit has different supply resistance, depending on the line voltage U_{ab} , by the fact that the magnitude of the supply resistance is corresponded by the slope of the lines and by the fact that the lines shown in the Figure have different slopes.

The circuit supply resistance to line currents I_{ab} is smaller than a limit line current I_{lim} determined by the first resistive component R_A , $R_{feed} \approx R_{dc} \cdot (1 + R_1/R_A) / (G_i \cdot G_{dc})$. (The circuit supply resistance also includes the supply resistance in the fundamental state, although this is ignored because it is constant.) In the Figure, the slope of the first line A denotes the circuit supply resistance for the lower current region $I_{ab} < I_{lim}$. The size of the slope is corresponded by the inverted value of the supply resistance, wherein a large slope (almost vertical) will thus indicate low-ohmic supply resistance. In its simplest form, the first resistive component R_A is a resistor. The current supply to the telephone line ab will be more high-ohmic than in the fundamental state. This resistance can be given different values, by program control. In the illustrated embodiment, the resistive component R_A is a string of silicon-integrated resistances, where the desired resistance is obtained with the aid of transistors. As beforementioned, different values give different supply resistances and therewith impart different slopes to the first line A. If the first resistive component R_A is low-ohmic, the supply resistance will be high-ohmic and the first line A will have a gentler or small slope, whereas if the component R_A is high-ohmic, the supply resistance will be low-ohmic and the line A will have a steep or large slope. It is also possible to achieve a more low-ohmic supply (the line A is almost perpendicular) by forming the first resistive component R_A from a negative resistance, generated with the aid of a resistor in combination with a positive or negative feedback amplifier. The resistor is connected between the input and the output of the feedback amplifier. Different values of the negative resistance are obtained by varying the amplifier feedback, which can also be program con-



trolled. The limit line current I_{lim} is corresponded by a limit voltage U_{lim} . Thus, the circuit supply resistance is controlled between the open circuit voltage E and said limit voltage U_{lim} by the first resistive component R_A .

5 The voltage limiting element 7 functions to limit current at line currents which are higher than the limit current I_{lim} , so that the line current I_{ab} in said upper current interval will increase at a slower rate than in the lower current interval. The voltage limiting element 7 consists, for instance, of a negative feedback
10 comparator, the reference voltage of which, which is program controlled, determines the limit current I_{lim} at which current limitation occurs. The reference voltage can be programmed, by applying a programmable current to a resistor. When the voltage on the comparator input, at a third node P_3 inbetween the second
15 resistive component R_B and the voltage limiter 7, reaches the programmed reference voltage, the voltage is unable to increase further, but instead passes a current through the comparator. This current passing through the comparator also flows through the second resistive component R_B , which therewith also determines the
20 circuit supply resistance, which therewith increases so that said current limitation occurs. The first resistive component R_A parallel with the second resistive component R_B determines the supply resistance of the circuit at said current limitation, i.e. at line currents which exceed the limit current I_{lim} . The decrease
25 in the slope of the second line AB in Figure 2 shows that the circuit supply resistance will increase with current limitation. The second resistive component R_B can be varied by programming, so that the slope of the line AB, and thereby the supply resistance of the current at current limitation, is varied. The aforesaid
30 second component R_B may comprise, for instance, the same type of component as that used for the first resistive component R_A , when this is positive.

Since the current supply circuit includes a lowpass filter 5, the internal impedance in the circuit becomes complex. The impedance
35 consists of the earlier mentioned supply resistance R_{feed} in series with an inductance L_{feed} . The reactive element in the

lowpass filter is a capacitor C_1 . The first resistive component R_A is a linear shunt to said capacitor, whereas the second resistive component R_B is a non-linear shunt to the same capacitor. Since all changes in the current supply characteristic, both linear and non-linear, are reflected by shunt-coupling of this capacitor, the equivalent inductance, seen from the line side ab, will be constant, independently of both current supply characteristic and operation point. This is achieved because the product of the amplification and bandwidth in the circuit is constant at said shunt coupling to the capacitor.

That the impedance includes an inductance is due to the fact that the circuit between the line ab and the two first nodes P_1 , P_2 can be considered as a gyrator which transforms current to voltage and vice versa. A current in the section between the nodes P_1 , P_2 will thus correspond to a voltage on the line ab (the generator current I determines the idling voltage E) and a voltage corresponds to a line current I_{ab} (the voltage limiting element 7 results in current limitation on the line ab). A shunt-connected resistance therewith transforms to a series resistance on the line and, in the same way, the parallel capacitance C_1 is transformed to a series inductance L_{feed} .

THE CLAIMS DEFINING THE INVENTION ARE AS FOLLOWS:

1. A method of controlling a current supply in a circuit for supplying a first direct current (I_{ab}) to a 2-wire telephone line (ab) comprising the steps of:
 detecting and controlling a first voltage level (U_{ab}) across said telephone line;

filtering-out speech signals from said telephone line through a low-pass filter (5) comprising a capacitive part to provide a filtered signal;

generating a second current (I_{dc}) corresponding to said filtered signal;

amplifying said second current to provide said first current (I_{ab});

controlling an open circuit voltage (E) across said telephone line by generating a third selectable current (I) and electrically connecting said selectable current in parallel with said capacitive part of the lowpass filter;

controlling a supply resistance of said circuit across said telephone line when said first current (I_{ab}) has a value less than a limit line current value (I_{lim}) by a first adjustable resistor (R_A) electrically connected in parallel with said capacitive part of the lowpass filter;

controlling a supply resistance of said circuit across said telephone line when said first current has a value greater than said limit line current value (I_{lim}) by a second adjustable resistor (R_B), wherein said second adjustable resistor (R_B) is electrically connected in series with an adjustable voltage limiter (7) and said series connection being further connected in parallel with said capacitive part of the lowpass filter; and

controlling said limit line current value (I_{lim}) at which limitation of said first current (I_{ab}) occurs, by an adjustable reference voltage level of said adjustable voltage limiter.

2. A method according to Claim 1, characterized in that setting of the current supply characteristic is effected by programming the current direction of the third selectable generator current (I), the resistance of the first resistive component (R_A), the reference voltage of the adjustable voltage limiter, and the resistance of the voltage-limiting element (7), and the resistance of the



adjustable
second resistor (R_B).

3. . . A method according to Claim 2, characterized in that the magnitude of the ~~generator~~ ^{third selectable} current (I) is also programmable.

4. A device for supplying a first direct current (I_{ab}) to a 2-wire telephone line (ab) comprising:

a voltage converter (3) electrically connected to detect and control a first voltage level across said telephone line and having an output to provide a reduced voltage level corresponding to said first voltage level;

a low-pass filter (5) to substantially filter out speech signals from the telephone line and having an input and an output, said low-pass filter consisting of a first resistive part comprising a first resistor (R_1) and a second capacitive part comprising a capacitor (C_1) and a second resistor (R_2), and said low-pass filter input being electrically connected to said voltage converter output;

a current generator (8) electrically connected in parallel with said second capacitive part (C_1, R_2) of the low-pass filter and having an output to provide a selectable generator current (I) wherein said selectable generator current (I) determines an open circuit voltage (E) across said telephone line;

a first adjustable resistor (R_A) electrically connected in parallel with said second capacitive part of the low-pass filter wherein said first adjustable resistor determines a supply resistance of said device across said telephone line when said first direct current (I_{ab}) has a value less than a limit line current value (I_{lim});

an adjustable voltage limiter (7) connected in series relation with a second adjustable resistor (R_B), said series connection being in parallel with said second capacitive part of the low-pass filter, said voltage limiter having an adjustable reference voltage value which determines the limit line current value (I_{lim}) at which limitation of said first current occurs, said first and second adjustable resistor determines a supply resistance of said device across said telephone line when said first direct current has a value greater than said line limit current value;

a buffer amplifier (6) electrically connected to said low-pass filter output



and having an output to provide a second voltage;

a buffer output resistor (R_{dc}) electrically connected to said buffer amplifier output to provide a second current (I_{dc}) corresponding to said second voltage; and

a current amplifier (4) electrically connected to receive said second current and having an output electrically connected to supply said first direct current to said telephone line.

5. A circuit according to Claim 4, characterized in that said first ~~resistive~~
^{adjustable resistor}
1 ~~component~~ (R_A) is a resistor in combination with a positive or negative feedback amplifier.

6. A circuit according to Claim 4, characterized in that said ^{adjustable}
~~limiting~~
1 ~~element~~ (7) consists of a negative feedback comparator.

DATED this 5th day of November, 1993
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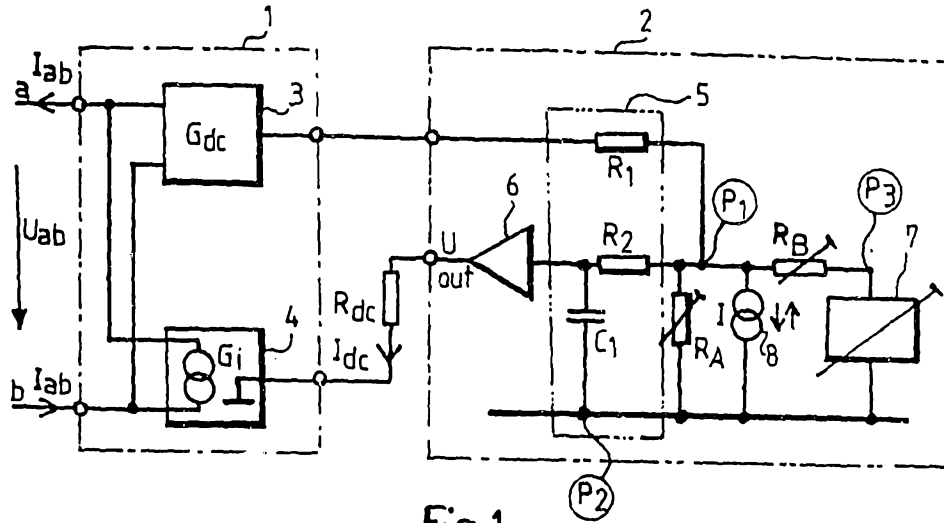


Fig.1

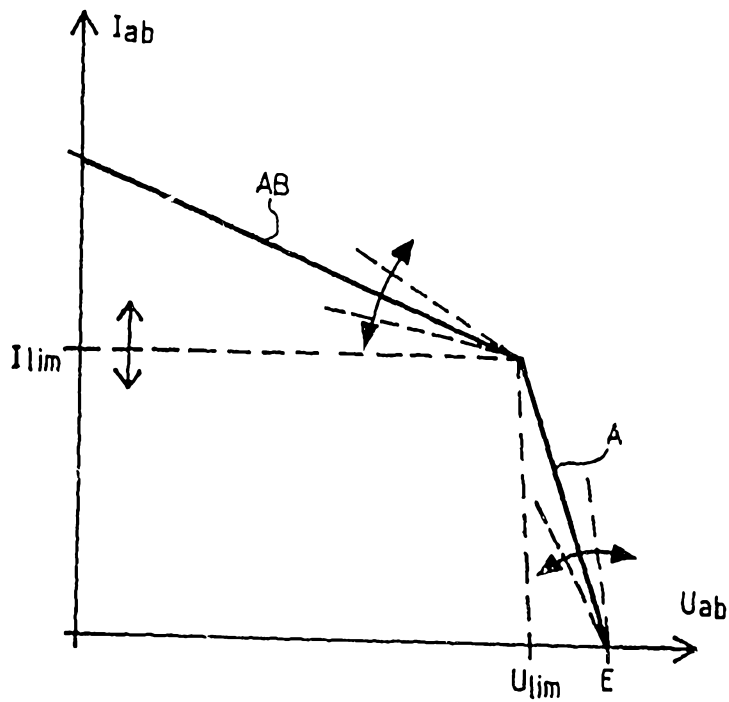


Fig.2

INTERNATIONAL SEARCH REPORT

International Application No PCT/SE 90/00804

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) ⁶		
According to International Patent Classification (IPC) or to both National Classification and IPC		
IPC5: H 04 M 19/00		
II. FIELDS SEARCHED		
Minimum Documentation Searched ⁷		
Classification System	Classification Symbols	
IPC5	H 04 M	
Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in Fields Searched ⁸		
SE,DK,FI,NO classes as above		
III. DOCUMENTS CONSIDERED TO BE RELEVANT⁹		
Category ¹⁰	Citation of Document, ¹¹ with indication, where appropriate, of the relevant passages ¹²	Relevant to Claim No. ¹³
A	US, A, 4631360 (J.H. JOHANSSON ET AL) 23 December 1986, see figure 1 -- -----	1-6
<p>* Special categories of cited documents:¹⁰</p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason ("A" specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance, the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance, the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art</p> <p>"&" document member of the same patent family</p>		
IV. CERTIFICATION		
Date of the Actual Completion of the International Search		Date of Mailing of this International Search Report
20th February 1991		1991-03-07
International Searching Authority		Signature of Authorized Officer
SWEDISH PATENT OFFICE		<i>Roland Landström</i> ROLAND LANDSTRÖM

**ANNEX TO THE INTERNATIONAL SEARCH REPORT
ON INTERNATIONAL PATENT APPLICATION NO.PCT/SE 90/00804**

This annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the Swedish Patent Office EDP file on **91-01-31**. The Swedish Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US-A- 4631360	86-12-23	AU-B- 562139	87-05-28
		AU-D- 2030783	84-04-04
		EP-A-B- 0119234	84-09-26
		JP-T- 59501569	84-08-30
		SE-B-C- 433284	84-05-14
		SE-A- 8205342	84-03-18
		WO-A- 84/01249	84-03-29