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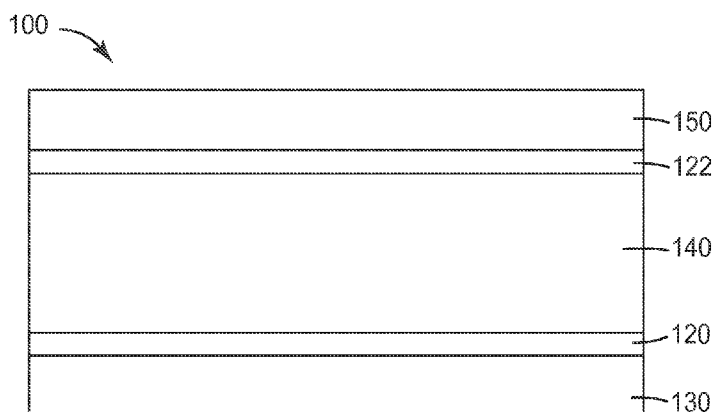


FIG. 1A

(57) Abstract: A multilayer optical film is provided comprising first optical layers of a first fluoropolymeric material and second optical layers of a second fluoropolymeric material wherein at least a portion of the first layers and at least a portion of the second layers are in intimate contact



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FLUOROPOLYMERIC MULTILAYER OPTICAL FILM AND METHODS OF MAKING AND USING THE SAME

TECHNICAL FIELD

5 This disclosure broadly relates to multilayer optical films and to methods of making and using the same.

BACKGROUND

10 Multilayer optical films have been made that have a plurality of alternating layers of at least two polymeric materials with individual layer thicknesses on the order of a few hundred nanometers or less. When the polymeric materials are selected to have a sufficient mismatch in refractive indices, these multilayer optical films cause constructive interference of wavelengths of light. This results in the multilayer optical film reflecting certain wavelengths while transmitting or absorbing other wavelengths.

15 Multilayer optical films traditionally have been constructed of alternating layers of non-fluorinated polymeric materials whose alternating layers have a refractive index difference of above 0.1. For example, multilayer optical films are commonly constructed of (poly(ethylene 2,6-naphthalate)) and (poly(methyl methacrylate)) layer pairs, which have a refractive index difference of 0.25; (poly(ethylene terephthalate)) and (copolymers
20 of poly(methyl methacrylate)) layer pairs, which have a refractive index difference of 0.16; and (poly(ethylene 2,6-naphthalate)) and coPEN (derived from naphthalenedicarboxylic acid, an additional dicarboxylic acid, and a diol) layer pairs, which can have refractive index of 0.19 for one polarization of light.

SUMMARY

25 Briefly, in one embodiment, the present disclosure provides a multilayer film comprising an optical stack, wherein the optical stack comprises first layers of a first fluoropolymeric material and second layers of a second fluoropolymeric material wherein at least a portion of the first layers and at least a portion of the second layers are in
30 intimate contact.

In another embodiment, the present disclosure provides an article comprising a multilayer optical film.

In another embodiment, the present disclosure provides a method of using a multilayer optical film for solar power applications, lighting applications, antireflection applications, and/or industrial applications.

In yet another embodiment, the present disclosure provides a method of making a multilayer optical film comprising providing a first fluoropolymeric material and a second fluoropolymeric material, coextruding the first fluoropolymeric material and the second fluoropolymeric material into a web; and alternately layering the first fluoropolymeric material and the second polymeric material to create an multilayer film.

Advantageously, these novel multilayer optical films may offer improved performance compared to traditional multilayer optical films.

The above summary is not intended to describe each embodiment. The details of one or more embodiments of the disclosure are also set forth in the description below. Other features, objects, and advantages will be apparent from the description and from the claims.

BRIEF DESCRIPTION OF DRAWINGS

FIG. 1A is a schematic side view of multilayer optical film 100 according to one exemplary embodiment of the present disclosure;

FIG. 1B is a schematic side view of a two-component optical stack 140 included in the multilayer optical film 100.

DETAILED DESCRIPTION

As used herein, the term "a", "an", "the", and "at least one of" are used interchangeably and mean one or more;

"and/or" is used to indicate one or both stated cases may occur, for example A and/or B includes, (A and B) and (A or B);

"interpolymerized" refers to monomers that are polymerized together to form a macromolecular compound;

"copolymer" refers to a polymeric material comprising at least two different interpolymerized monomers (i.e., the monomers do not have the same chemical structure) and include, for example, terpolymers (three different monomers), or tetrapolymers (four different monomers);

5 "polymer" refers to a polymeric material comprising interpolymerized monomers of the same monomer (a homopolymer) or of different monomers (a copolymer);

"light" refers to electromagnetic radiation having a wavelength in a range from 200 nm to 2500 nm;

10 "melt-processible" refers to a polymeric material that flows upon melting, heating, and/or application of pressure in normal process equipment such as extruders; and

"optical layer" refers to a layer of material having a thickness of about one quarter of a wavelength or wavelengths of light to be reflected.

FIG. 1A depicts one exemplary embodiment of the present disclosure. Multilayer optical film 100 comprises optical stack 140 and optional additional layers such as, for example, optional protective boundary layers 120 and 122, and optional skin layers 130 and 150.

Optical stack 140 will be better understood with reference to FIG. 1B. Optical stack 140 comprises first optical layers 160a, 160b, ..., 160n (collectively first optical layers 160) in intimate contact with second optical layers 162a, 162b, ..., 162n (collectively second optical layers 162).

20 Second optical layers 162 are disposed in a repeating sequence with first optical layers 160. The layer pairs (e.g., wherein first optical layers 160 are A and second optical layers 162 are B) may be arranged as alternating layer pairs (e.g., ABABAB...) as shown in FIG. 1B. In other embodiments, the layer pairs may be arranged with intermediate layers such as, for example a third optical layer, C, (e.g., ABCABC...) or in a non-alternating fashion (e.g., ABABABCAB..., ABABACABDAB..., ABABBAABAB..., etc.). Typically, the layer pairs are arranged as alternating layer pairs.

First optical layers 160 comprise a first fluoropolymeric material and second optical layers 162 comprise a second fluoropolymeric material. The fluoropolymeric materials contemplated by this disclosure include melt-processible fluoropolymers derived from interpolymerized units of fully or partially fluorinated monomers and may be semi-crystalline or amorphous. The fluoropolymeric material may include at least one of the

following monomers: tetrafluoroethylene (TFE), vinylidene fluoride (VDF), vinyl fluoride (VF), hexafluoropropylene (HFP), chlorotrifluoroethylene (CTFE), fluoroalkyl vinyl ethers, fluoroalkoxy vinyl ethers, fluorinated styrenes, fluorinated siloxanes, hexafluoropropylene oxide (HFPO), or combinations thereof.

Exemplary fluoropolymeric material include: homopolymers of TFE (e.g., PTFEs), copolymers of ethylene and TFE copolymers (e.g., ETFEs); copolymers of TFE, HFP, and VDF (e.g., THVs); homopolymers of VDF (e.g., PVDFs); copolymers of VDF (e.g., coVDFs); homopolymers of VF (e.g., PVFs); copolymers of HFP and TFE (e.g., FEPs); copolymers of TFE and propylene (e.g., TFEPs); copolymers of TFE and (perfluorovinyl) ether (e.g., PFAs); copolymers of TFE, (perfluorovinyl) ether, and (perfluoromethyl vinyl) ether (e.g., MFAs); copolymers of HFP, TFE, and ethylene (e.g., HTEs); homopolymers of chlorotrifluoroethylene (e.g., PCTFE); copolymers of ethylene and CTFE (e.g., ECTFEs); homopolymers of HFPO (e.g., PHFPO); homopolymers of 4-fluoro-(2-trifluoromethyl)styrene; copolymers of TFE and norbornene; copolymers of HFP and VDF; or combinations thereof.

In some embodiments, the representative melt-processible copolymers comprising interpolymerized monomers of tetrafluoroethylene described above include additional monomers, which may be fluorinated or non-fluorinated. Examples include: ring opening compounds such as 3- or 4-membered rings that undergo ring opening under the conditions of polymerization such as, e.g., epoxides; olefinic monomers such as, e.g., propylene, ethylene, vinylidene fluoride, vinyl fluoride, and norbornene; and perfluoro(vinyl ether)s of the formula $\text{CF}_2=\text{CF}-(\text{OCF}_2\text{CF}(\text{R}_f))_a\text{OR}'_f$ where R_f is a perfluoroalkyl having 1 to 8, typically 1 to 3, carbon atoms, R'_f is a perfluoroaliphatic, typically perfluoroalkyl or perfluoroalkoxy of 1 to 8, typically 1 to 3, carbon atoms, and a is an integer from 0 to 3. Examples of the perfluoro(vinyl ether)s having this formula include:

$$\text{CF}_2=\text{CFOCF}_3, \quad \text{CF}_2=\text{CFOCF}_2\text{CF}_2\text{CF}_2\text{OCF}_3, \quad \text{CF}_2=\text{CFOCF}_2\text{CF}_2\text{CF}_3,$$

$$\text{CF}_2=\text{CFOCF}_2\text{CF}(\text{CF}_3)\text{OCF}_2\text{CF}_2\text{CF}_3, \quad \text{and}$$

$$\text{CF}_2=\text{CFOCF}_2\text{CF}(\text{CF}_3)\text{OCF}_2\text{CF}(\text{CF}_3)\text{OCF}_2\text{CF}_2\text{CF}_3.$$

Particularly useful may be melt-processible fluoropolymers comprising at least three, or even at least four, different monomers.

Exemplary melt-processible copolymers of tetrafluoroethylene and other monomer(s) discussed above include those commercially available as: copolymers of

tetrafluoroethylene, hexafluoropropylene, and vinylidene fluoride sold under the trade designation "DYNEON THV 220", "DYNEON THV 230", "DYNEON THV 500", "DYNEON THV 500G", "DYNEON THV 510D", "DYNEON THV 610", "DYNEON THV 815", "DYNEON THVP 2030G" by Dyneon LLC., Oakdale, MN; copolymers of
5 tetrafluoroethylene, hexafluoropropylene, and ethylene sold under the trade designation "DYNEON HTE 1510" and "DYNEON HTE 1705" by Dyneon LLC., and "NEOFLON EFEP" by Daikin Industries, Ltd., Osaka, Japan; copolymers of tetrafluoroethylene, hexafluoropropylene, and ethylene sold under the trade designation "AFLAS" by Asahi Glass Co., Ltd., Tokyo, Japan; copolymers of tetrafluoroethylene and norbornene sold
10 under the trade designation "TEFLON AF" by E.I. du Pont de Nemours and Co., Wilmington, DE; copolymers of ethylene and tetrafluoroethylene sold under the trade designation "DYNEON ET 6210A" and "DYNEON ET 6235" by Dyneon LLC., "TEFZEL ETFE" by E.I. du Pont de Nemours and Co., and "FLUON ETFE" by Asahi Glass Co., Ltd.; copolymers of ethylene and chlorotrifluoroethylene sold under the trade
15 designation "HALAR ECTFE" by Solvay Solexis Inc., West Deptford, NJ; homopolymers of vinylidene fluoride sold under the trade designation "DYNEON PVDF 1008" and "DYNEON PVDF 1010" by Dyneon LLC.; copolymers of polyvinylidene fluoride sold under the trade designation "DYNEON PVDF 11008", "DYNEON PVDF 60512", "DYNEON FC-2145" (a copolymer of HFP and VDF) by Dyneon LLC., homopolymers
20 of vinyl fluoride sold under the trade designation "DUPONT TEDLAR PVF" by E.I. du Pont de Nemours and Co.; MFAs sold under the trade designation "HYFLON MFA" by Solvay Solexis Inc.; or combinations thereof.

Exemplary layer pairs of the present disclosure include: homopolymers of vinylidene fluoride and (copolymers of tetrafluoroethylene, hexafluoropropylene, and
25 vinylidene fluoride) layer pairs; (copolymers of ethylene and chlorotrifluoroethylene) and (copolymers of tetrafluoroethylene, hexafluoropropylene, and vinylidene fluoride) layer pairs; (copolymers of tetrafluoroethylene, hexafluoropropylene, and ethylene) and (copolymers of tetrafluoroethylene, hexafluoropropylene, and vinylidene fluoride) layer
pairs; (copolymers of tetrafluoroethylene, hexafluoropropylene, and ethylene) and
30 (copolymers of ethylene and tetrafluoroethylene) layer pairs; (copolymers of tetrafluoroethylene, hexafluoropropylene, and ethylene) and copolymers of tetrafluoroethylene and norbornene layer pairs; (copolymers of ethylene and

tetrafluoroethylene) and (copolymers of tetrafluoroethylene, hexafluoropropylene, and vinylidene fluoride) layer pairs; or combinations thereof.

By appropriate selection of the first optical layers and the second optical layers, optical stack 140 can be designed to reflect or transmit a desired bandwidth of light. It will be understood from the foregoing discussion that the choice of a second optical layer is dependent not only on the intended application of the multilayer optical film, but also on the choice made for the first optical layer, as well as the processing conditions.

As light passes through optical stack 140, the light or some portion of the light will be transmitted through an optical layer, absorbed by an optical layer, or reflected off the interface between the optical layers.

The light transmitted through an optical layer is related to absorbance, thickness, and reflection. Transmission (T) is related to absorbance (A) in that $A = -\log T$, and $\%A + \%T + \% \text{reflection} = 100\%$. Reflection is generated at each interface between the optical layers. Referring again to FIG. 1B, first optical layers 160 and second optical layers 162 have respective refractive indices that are different, n_1 and n_2 , respectively. Light may be reflected at the interface of adjacent optical layers, for example, at the interface between first optical layer 160a and second optical layer 162a; and/or at the interface between second optical layer 162a and first optical layer 160b. Light that is not reflected at the interface of adjacent optical layers typically passes through successive layers and is either absorbed in a subsequent optical layer, reflected at a subsequent interface, or is transmitted through the optical stack 140 altogether. Typically, the optical layers of a given layer pair are selected such as to be substantially transparent to those light wavelengths at which reflectivity is desired. Light that is not reflected at a layer pair interface passes to the next layer pair interface where a portion of the light is reflected and unreflected light continues on, and so on. In this way, an optical layer stack with many optical layers (e.g., more than 50, more than 100, more than 1000, or even more than 2000 optical layers) is capable of generating a high degree of reflectivity.

In general, the reflectivity of the interface of adjacent optical layers is proportional to the square of the difference in index of refraction on the first optical layer and the second optical layer at the reflecting wavelength. The absolute difference in refractive index between the layer pair ($|n_1 - n_2|$) is typically 0.1 or larger. Higher refractive index differences between the first optical layer and the second optical layer are desirable,

because more optical power (e.g., reflectivity) can be created, thus enabling more reflective bandwidth. However, in the present disclosure, the absolute difference between the layer pair may be less than 0.20, less than 0.15, less than 0.10, less than 0.05, or even less than 0.03, depending on the layer pair selected. For example, poly(methyl methacrylate) and DYNEON HTE 1705 have an absolute refractive index difference of 0.12.

By selecting the appropriate layer pairs, the layer thickness, and/or the number of layer pairs, the optical stack can be designed to transmit or reflect the desired wavelengths. The thickness of each layer may influence the performance of the optical stack by either changing the amount of reflectivity or shifting the reflectivity wavelength range. The optical layers typically have an average individual layer thickness of about one quarter of the wavelength of interest, and a layer pair thickness of about one half of the wavelength of interest. The optical layers can each be a quarter-wavelength thick or the optical layers can have different optical thicknesses, as long as the sum of the optical thicknesses for the layer pair is half of a wavelength (or a multiple thereof). For example, to reflect 400 nanometer (nm) light, the average individual layer thickness would be about 100 nm, and the average layer pair thickness would be about 200 nm. Similarly, to reflect 800 nm light, the average individual layer thickness would be about 200 nm, and the average layer pair thickness would be about 400 nm. First optical layers 160 and second optical layers 162 may have the same thicknesses. Alternatively, the optical stack can include optical layers with different thicknesses to increase the reflective wavelength range. An optical stack having more than two layer pairs can include optical layers with different optical thicknesses to provide reflectivity over a range of wavelengths. For example, an optical stack can include layer pairs that are individually tuned to achieve optimal reflection of normally incident light having particular wavelengths or may include a gradient of layer pair thicknesses to reflect light over a larger bandwidth. The normal reflectivity for a particular layer pair is primarily dependent on the optical thickness of the individual layers, where optical thickness is defined as the product of the actual thickness of the layer times its refractive index. The intensity of light reflected from the optical layer stack is a function of its number of layer pairs and the differences in refractive indices of optical layers in each layer pair. The ratio $n_1 d_1 / (n_1 d_1 + n_2 d_2)$ (commonly termed the "f-ratio") correlates with reflectivity of a given layer pair at a specified wavelength. In the f-ratio,

n_1 and n_2 are the respective refractive indexes at the specified wavelength of the first and second optical layers in a layer pair, and d_1 and d_2 are the respective thicknesses of the first and second optical layers in the layer pair. By proper selection of the refractive indexes, optical layer thicknesses, and f-ratio, one can exercise some degree of control over the intensity of first order reflection. For example, first order visible reflections of violet (400 nanometers wavelength) to red (700 nanometers wavelength) can be obtained with layer optical thicknesses between about 0.05 and 0.3 nanometers. In general, deviation from an f-ratio of 0.5 results in a lesser degree of reflectivity.

The equation $\lambda/2 = n_1d_1 + n_2d_2$ can be used to tune the optical layers to reflect light of wavelength λ at a normal angle of incidence. At other angles, the optical thickness of the layer pair depends on the distance traveled through the component optical layers (which is larger than the thickness of the layers) and the indices of refraction for at least two of the three optical axes of the optical layer. The optical layers can each be a quarter-wavelength thick or the optical layers can have different optical thicknesses, as long as the sum of the optical thicknesses is half of a wavelength (or a multiple thereof). An optical stack having more than two layer pairs can include optical layers with different optical thicknesses to provide reflectivity over a range of wavelengths. For example, an optical stack can include layer pairs that are individually tuned to achieve optimal reflection of normally incident light having particular wavelengths or may include a gradient of layer pair thicknesses to reflect light over a larger bandwidth.

A typical approach is to use all or mostly quarter-wave film stacks. In this case, control of the spectrum requires control of the layer thickness profile in the film stack. A broadband spectrum, such as one required to reflect visible light over a large range of angles in air, still requires a large number of layers if the layers are polymeric, due to the relatively small refractive index differences achievable with polymer films compared to inorganic films. Layer thickness profiles of such optical stacks can be adjusted to provide for improved spectral characteristics using the axial rod apparatus taught in U.S. Pat. No. 6,783,349 (Neavin et al.) combined with layer profile information obtained with microscopic techniques.

A desirable technique for providing a multilayer optical film with a controlled spectrum include:

- 1) The use of an axial rod heater control of the layer thickness values of coextruded polymer layers as taught in U.S. Pat. No. 6,783,349 (Neavin et al.).
- 2) Timely layer thickness profile feedback during production from a layer thickness measurement tool such as e.g., an atomic force microscope, a transmission electron microscope, or a scanning electron microscope.
- 3) Optical modeling to generate the desired layer thickness profile.
- 4) Repeating axial rod adjustments based on the difference between the measured layer profile and the desired layer profile.

The basic process for layer thickness profile control involves adjustment of axial rod zone power settings based on the difference of the target layer thickness profile and the measured layer profile. The axial rod power increase needed to adjust the layer thickness values in a given feedblock zone may first be calibrated in terms of watts of heat input per nanometer of resulting thickness change of the layers generated in that heater zone. Fine control of the spectrum is possible using 24 axial rod zones for 275 layers. Once calibrated, the necessary power adjustments can be calculated once given a target profile and a measured profile. The procedure may be repeated until the two profiles converge.

For example, the layer thickness profile (layer thickness values) of the optical stack may be adjusted to be approximately a linear profile with the first (thinnest) optical layers adjusted to have about a quarter wave optical thickness (index times physical thickness) for 340 nm light and progressing to the thickest layers, which were adjusted to be about a quarter wave thick optical thickness for 420 nm light.

Increasing the number of optical layers in the optical stack may also provide more optical power. For example, if the refractive index between the layer pairs is small, the optical stack may not achieve the desired reflectivity, however by increasing the number of layer pairs, sufficient reflectivity may be achieved. In one embodiment of the present disclosure, the optical stack comprises at least 2 first optical layers and at least 2 second optical layers, at least 5 first optical layers and at least 5 second optical layers, at least 50 first optical layers and at least 50 second optical layers, at least 200 first optical layers and at least 200 second optical layers, at least 500 first optical layers and at least 500 second optical layers, or even at least 1000 first optical layers and at least 1000 second optical layers.

Birefringence (e.g., caused by stretching) of optical layers is another effective method for increasing the difference in refractive index of the optical layers in a layer pair. Optical stacks that include layer pairs, which are oriented in two mutually perpendicular in-plane axes are capable of reflecting an extraordinarily high percentage of incident light depending on, e.g., the number of optical layers, f-ratio, and the indices of refraction, and are highly efficient reflectors.

As mentioned, the optical stack of this disclosure may be designed to reflect or transmit at least a specific bandwidth (i.e., wavelength range) of interest. In one embodiment, the optical stack of the present disclosure transmits at least one of the following: at least a portion of the wavelengths between about 400-700 nm, between about 380-780 nm, or even between about 350-800 nm; at least a portion of the wavelengths greater than about 700 nm, greater than about 780 nm, or even greater than about 800 nm; at least a portion of the wavelengths between about 700-2500 nm, between about 800-1300 nm, or even between about 800-1100 nm; at least a portion of the wavelengths between about 300-400 nm, or even between about 250-400 nm; at least a portion of the wavelengths less than about 300 nm; or combinations thereof. By "at least a portion" is meant to comprise not only the entire range of wavelengths, but also a portion of the wavelengths, such as a bandwidth of at least 2 nm, 10 nm, 25 nm, 50 nm, or 100 nm. By "transmits" is meant that at least 30, 40, 50, 60, 70, 80, 85, 90, 92, or 95 percent of the wavelengths of interest are transmitted at a 90 degree angle of incidence.

In one embodiment, the optical stack of the present disclosure reflects at least one of the following: at least a portion of the wavelengths between about 400-700 nm, between about 380-780 nm, or even between about 350-800 nm; at least a portion of the wavelengths greater than about 700 nm, greater than about 780 nm, or even greater than about 800 nm; at least a portion of the wavelengths between about 700-2500 nm, between about 800-1300 nm, or even between about 800-1100 nm; at least a portion of the wavelengths between about 300-400 nm, or even between about 250-400 nm; at least a portion of the wavelengths less than about 300 nm; or combinations thereof. By "reflects" is meant that at least 30, 40, 50, 60, 70, 80, 85, 90, 92, or 95 percent of the wavelengths of interest are reflected at a 90 degree angle of incidence.

Layer pairs, number of layers, and thickness of layers may be selected so that the optical stack reflects a first bandwidth of light and transmits a second bandwidth of light.

For example, the optical stack may transmit visible wavelengths (e.g., 400-700 nm) and reflect infrared wavelengths (e.g., 700-2500 nm), transmit ultraviolet wavelengths (e.g., 250-400 nm) and reflect infrared wavelengths, or transmit infrared wavelengths and reflect UV wavelengths.

5 In addition to the optical stack described above, additional layers such as those shown in FIG. 1A may optionally be applied in the multilayer optical film to modify or enhance the physical, chemical, and/or optical characteristics of the multilayer optical film. A non-limiting listing of coatings or layers that may optionally be used in multilayer optical films according to the present invention is detailed in the following paragraphs.

10 In one embodiment, the multilayer optical films comprise one or more optical layers. It will be appreciated that multilayer optical films can consist of a single optical stack or can be made from multiple optical stacks that are subsequently combined to form the multilayer optical film. Additional optical layers that may be added include, e.g.,:
15 polarizers, mirrors, clear to colored films, colored to colored films, cold mirrors, or combinations thereof.

 In one embodiment, the multilayer optical film comprise one or more non-optical layers such as, for example, one or more skin layers or one or more interior non-optical layers, such as, for example, protective boundary layers between packets of optical layers. Non-optical layers can be used to give the multilayer optical film structure or to protect it
20 from harm or damage during or after processing. For some applications, it may be desirable to include sacrificial protective skins, wherein the interfacial adhesion between the skin layer(s) and the optical stack is controlled so that the skin layers can be stripped from the optical stack before use.

 Typically, one or more of the non-optical layers are placed so that at least a
25 portion of the light to be transmitted or reflected by optical layers also travels through these layers (i.e., these layers are placed in the path of light which travels through or is reflected by the first and second optical layers). The non-optical layers may or may not affect the reflective or transmissive properties of the optical stack over the wavelength region of interest. Generally, they should not affect the optical properties of the optical
30 stack.

 Materials may be chosen for the non-optical layers that impart or improve properties such as, for example, tear resistance, puncture resistance, toughness,

weatherability, and/or chemical resistance of the multilayer optical film. When selecting a material for use in, for example a tear resistant layer, many factors should be considered such as, percent elongation at break, Young's modulus, tear strength, adhesion to interior layers, percent transmittance and absorbance in the wavelength(s) of interest, optical clarity and haze, weatherability, and permeability to various gases and solvents. Examples of materials that may be used as tear resistant layers include: polycarbonate, blends of polycarbonates and copolyesters, copolymers of polyethylene, copolymers of polypropylene, copolymers of ethylene and tetrafluoroethylene, copolymers of hexafluoropropylene, tetrafluoroethylene and ethylene, and poly(ethylene terephthalate).

The non-optical layers may be of any appropriate material and can be the same as one of the materials used in the optical stack. Of course, it is important that the material chosen not have optical properties too deleterious to those of the optical stack(s). The non-optical layers may be formed from a variety of polymers, including any of the polymeric materials used in the first and second optical layers. In some embodiments, the material selected for the non-optical layers is similar to or the same as the polymeric material selected for the first optical layers and/or the polymeric material selected for the second optical layers.

An optional UV-absorbing layer may be applied to the multilayer optical film to shield the multilayer optical film from UV-radiation that may cause degradation. Solar light, in particular UV radiation from 280 to 400 nm, can induce degradation of plastics, which in turn results in color change and deterioration of optical and mechanical properties. Inhibition of photo-oxidative degradation is important for outdoor applications wherein long term durability is mandatory. The absorption of UV-radiation by poly(ethylene terephthalate)s, for example, starts at around 360 nm, increases markedly below 320 nm, and is very pronounced at below 300 nm. Poly(ethylene naphthalate)s strongly absorb UV-radiation in the 310-370 nm range, with an absorption tail extending to about 410 nm, and with absorption maxima occurring at 352 nm and 337 nm. Chain cleavage occurs in the presence of oxygen, and the predominant photooxidation products are carbon monoxide, carbon dioxide, and carboxylic acids. Besides the direct photolysis of the ester groups, consideration has to be given to oxidation reactions, which likewise form carbon dioxide via peroxide radicals.

The UV-absorbing layer comprises a polymer and a UV-absorber. Typically, the polymer is a thermoplastic polymer, but this is not a requirement. Examples of suitable polymers include polyesters (e.g., poly(ethylene terephthalate)), fluoropolymers, polyamides, acrylics (e.g., poly(methyl methacrylate)), silicone polymers (e.g., thermoplastic silicone polymers), styrenic polymers, polyolefins, olefinic copolymers (e.g., copolymers of ethylene and norbornene available as TOPAS COC), silicone copolymers, urethanes, or combinations thereof (e.g., a blend of polymethyl methacrylate and polyvinylidene fluoride).

The UV-absorbing layer shields the multilayer optical film by absorbing UV-light. In general, the UV-absorbing layer may include any polymer composition (i.e., polymer plus additives) that is capable of withstanding UV-radiation for an extended period of time.

A variety of UV light absorbing and stabilizing additives are typically incorporated into the UV-absorbing layer to assist in its function of protecting the multilayer optical film. Non-limiting examples of the additives include one or more compounds selected from UV light absorbers, hindered amine light stabilizers, antioxidants, and combinations thereof.

UV-stabilizers such as UV-absorbers are chemical compounds that can intervene in the physical and chemical processes of photoinduced degradation. The photooxidation of polymers from UV-radiation can therefore be prevented by use of a UV-absorbing layer that contains at least one UV-absorber to effectively absorb light at wavelengths less than about 400 nm. UV-absorbers are typically included in the UV-absorbing layer in an amount that absorb at least 70 percent, typically 80 percent, more typically greater than 90 percent, or even greater than 99 percent of incident light in a wavelength region from 180 to 400 nm.

Typical UV-absorbing layer thicknesses are from 10 to 500 micrometers, although thinner and thicker UV-absorbing layers may also be used. Typically, the UV-absorber is present in the UV-absorbing layer in an amount of from 2 to 20 percent by weight, but lesser and greater levels may also be used.

One exemplary UV-absorbing compound is a benzotriazole compound, 5-trifluoromethyl-2-(2-hydroxy-3- α -cumyl-5-tert-octylphenyl)-2H-benzotriazole. Other exemplary benzotriazoles include, e.g., 2-(2-hydroxy-3,5-di- α -cumylphenyl)-2H-

benzotriazole, 5-chloro-2-(2-hydroxy-3-tert-butyl-5-methylphenyl)-2H-benzotriazole, 5-chloro-2-(2-hydroxy-3,5-di-tert-butylphenyl)-2H-benzotriazole, 2-(2-hydroxy-3,5-di-tert-amylphenyl)-2H-benzotriazole, 2-(2-hydroxy-3- α -cumyl-5-tert-octylphenyl)-2H-benzotriazole, 2-(3-tert-butyl-2-hydroxy-5-methylphenyl)-5-chloro-2H-benzotriazole.

5 Additional exemplary UV-absorbing compounds include 2-(4,6-diphenyl-1-3,5-triazin-2-yl)-5-hexyloxy-phenol, and those sold under the trade designation "TINUVIN 1577" and "TINUVIN 900" by Ciba Specialty Chemicals Corp., Tarrytown, NY. In addition, UV-absorber(s) can be used in combination with hindered amine light stabilizer(s) (HALS) and/or antioxidants. Exemplary HALSs include those sold under the trade designation
10 "CHIMASSORB 944" and "TINUVIN 123" by Ciba Specialty Chemicals Corp.. Exemplary antioxidants include those sold under the trade designation "IRGANOX 1010" and "ULTRANOX 626" by Ciba Specialty Chemicals Corp..

In addition to adding UVA, HALS, and antioxidants to the UV-absorbing layer, the UVA, HALS, and antioxidants can be added to other layers including the first or
15 second optical layers of the present disclosure.

In another embodiment, an optional IR-absorbing layer may be applied to the multilayer optical film to shield the multilayer optical film from IR radiation. The IR-absorbing layer comprises a polymer and an IR-absorber. The IR-absorbing layer may be coated onto the multilayer optical film or may be extrusion blended into a polymer layer.
20 Exemplary IR-absorbing compounds include: indium tin oxide; antimony tin oxide; IR-absorbing dyes such as those sold under the trade designation "EPOLIGHT 4105", "EPOLIGHT 2164", "EPOLIGHT 3130", and "EPOLIGHT 3072" by Epolin, Inc., Newark, NJ; heteropolyacids such as those described in U.S. Pat. No. 4,244,741 (Kruse); metal complexes such as those described in U.S. Pat. No. 3,850,502 (Bloom); nickel
25 complex dyes such as SDE8832 by H.W. Sands Corp., Jupiter, FL; and palladium complex dyes such as SDA5484 also by H.W. Sands Corp..

To further enhance the reflectance and/or transmissive performance or visual characteristics of the multilayer optical film, additional additives may be added to at least one of the layers. For example, the multilayer optical film may be treated with inks, dyes
30 or pigments to alter the appearance or to customize the multilayer optical film for specific applications. Thus, for example, the multilayer optical films may be treated with inks or other printed indicia such as those used to display product information, advertisements,

decoration, or other information. Various techniques may be used to print on the multilayer optical film, such as, e.g., screen printing, letterpress, and offset. Various types of ink may also be used including, e.g., one or two component inks, oxidatively drying and UV-drying inks, dissolved inks, dispersed inks, and 100% ink systems. The appearance of the multilayer optical film may also be colored such as, e.g., laminating a dyed layer onto the multilayer optical film, applying a pigmented coating to the surface of the multilayer optical film, including a pigment in one or more of the layers (e.g., the first or second optical layers, the additional optical layers or the non-optical layers) or combinations thereof. Both visible and near IR compounds are contemplated in the present disclosure, and include, for example, optical brighteners such as compounds that absorb in the UV and fluoresce in the visible range.

Other additives that may be included in the multilayer optical film include particulates. For example, carbon black particles can be dispersed in the polymeric or coated onto substrates to provide shading. Additionally, or alternately, small particle non-pigmentary zinc oxide, indium tin oxide, and titanium oxide can also be used as blocking, reflecting, or scattering additives to minimize UV-radiation degradation. The nanoscale particles are transparent to visible light while either scattering or absorbing harmful UV-radiation thereby reducing damage to thermoplastics. U.S. Pat. No. 5,504,134 (Palmer et al.) describes attenuation of polymer substrate degradation due to UV radiation through the use of metal oxide particles in a size range of about 0.001 micrometer to about 0.20 micrometer in diameter, and more typically from about 0.01 to about 0.15 micrometers in diameter. U.S. Pat. No. 5,876,688 (Laundon) teaches a method for producing micronized zinc oxide that are small enough to be transparent when incorporated as UV blocking and/or scattering agents in paints, coatings, finishes, plastic articles, and cosmetics, which are well suited for use in the present invention. These fine particles such as zinc oxide and titanium oxide with particle size ranged from 10-100 nm that can attenuate UV-radiation are commercially available from Kobo Products, Inc., South Plainfield, NJ.

The multilayer optical films may optionally comprise an abrasion resistant layer. The abrasion resistant layer may comprise any abrasion resistant material that is transparent to the wavelengths of interest. Examples of scratch resistant coatings include: a thermoplastic urethane sold under the trade designation "TECOFLEX" by Lubrizol Advanced Materials, Inc., Cleveland, OH containing 5 weight percent of a UV-absorber

sold under the trade designation "TINUVIN 405" by Ciba Specialty Chemicals Corp., 2 weight percent of a hindered amine light stabilizer sold under the trade designation "TINUVIN 123", and 3 weight percent of a UV-absorber sold under the trade designation "TINUVIN 1577" by Ciba Specialty Chemicals Corp.; and a scratch resistant coating
5 consisting of a thermally cured nano-silica siloxane filled polymer sold under the trade designation "PERMA-NEW 6000 CLEAR HARD COATING SOLUTION" by California Hardcoating Co., Chula Vista, CA.

The abrasion resistant layer may optionally include at least one antisoiling component. Examples of antisoiling components include fluoropolymers, silicone
10 polymers, titanium dioxide particles, polyhedral oligomeric silsesquioxanes (e.g., as sold under the trade designation "POSS" by Hybrid Plastics of Hattiesburg, MS), or combinations thereof. The abrasion resistant layer may also comprise a conductive filler, typically a transparent conductive filler.

The multilayer optical films of the present disclosure may optionally comprise one
15 or more boundary films or coatings to alter the transmissive properties of the multilayer optical film towards certain gases or liquids. These boundary films or coatings inhibit the transmission of water vapor, organic solvents, oxygen, and/or carbon dioxide through the film. Boundary films or coatings may be particularly desirable in high humidity environments, where components of the multilayer optical film may be subject to
20 distortion due to moisture permeation.

Additional optional layers may also be considered, for example, antistatic coatings or films, and anti-fogging materials.

The optional additional layers can be thicker than, thinner than, or the same thickness as the various optical layers of the optical stack. The thickness of the optional
25 additional layers is generally at least four times, typically at least 10 times, and can be at least 100 times or more, the thickness of at least one of the individual optical layers. The thickness of the additional layers can be varied to make a multilayer optical film having a particular thickness.

In the multilayer optical film, the optional additional layers may be applied via
30 co-extrusion or any adhesion techniques known in the art including, e.g., the use of adhesives, temperature, pressure, or combinations thereof. If present, an optional tie layer facilitates adhesion between layers of the multilayer optical film, primarily between the

optical stack and the optional additional layers. The tie layer may be organic (e.g., a polymeric layer) or inorganic. Exemplary inorganic tie layers include metal oxides such as e.g., titanium dioxide, aluminum oxide, or combinations thereof. The tie layer may be provided by any suitable means, including solvent casting and powder coating techniques.

5 In order that it does not degrade performance of the multilayer optical film, the optional tie layer is typically substantially not absorptive of light over the wavelengths of interest.

The optical stack can be fabricated by methods well-known to those of skill in the art by techniques such as e.g., co-extruding, laminating, coating, vapor deposition, or combinations thereof. In co-extrusion, the polymeric materials are co-extruded into a web.

10 In co-extrusion, it is preferred that the two polymeric materials have similar rheological properties (e.g., melt viscosities) to prevent layer instability or nonuniformity. In lamination, sheets of polymeric materials are layered together and then laminated using either heat, pressure, and/or an adhesive. In coating, a solution of one polymeric material is applied to another polymeric material. In vapor deposition, one polymeric material is
15 vapor deposited onto another polymeric material. Additionally, functional additives may be added to the first optical layer, the second optical layer, and/or the optional additional layers to improve processing. Examples of functional additives include processing additives, which may e.g., enhance flow and/or reduce melt fracture.

Further considerations relating to the selection of materials and manufacturing of
20 optical stacks and multilayer optical films can be obtained with reference to U.S. Pat. Nos. 5,552,927 (Wheatley et al.); 5,882,774 (Jonza et al.); 6,827,886 (Neavin et al.); and 6,830,713 (Hebrink et al.).

Typically, the polymeric materials of the first and second optical layers and the optional additional layers are chosen to have similar rheological properties (e.g., melt
25 viscosities) so that they can be co-extruded without flow disturbances. The first and second optical layers and the optional additional layers used also should have sufficient interfacial adhesion so that the multilayer optical film does not delaminate.

The ability to achieve the desired relationships among the various indices of refraction (and thus the optical properties of the optical stack) is influenced by processing
30 conditions used to prepare the optical stack. In one embodiment, the multilayer optical films are generally prepared by co-extruding the individual polymeric materials to form a multilayer optical film and then orienting the multilayer optical film by stretching at a

selected temperature, optionally followed by heat-setting at a selected temperature. Alternatively, the extrusion and orientation steps may be performed simultaneously.

The multilayer optical film may be stretched in the machine direction, as with a length orienter, or in width using a tenter. The pre-stretch temperature, stretch
5 temperature, stretch rate, stretch ratio, heat set temperature, heat set time, heat set relaxation, and cross-stretch relaxation are selected to yield a multilayer optical film having the desired refractive index relationship. These variables are interdependent, thus, for example, a relatively low stretch rate could be used if coupled with, e.g., a relatively low stretch temperature. It will be apparent to one of ordinary skill how to select the
10 appropriate combination of these variables to achieve the desired multilayer optical film. If a film is stretched, in general, a stretch ratio in the range from 1:2 to 1:10, or 1:3 to 1:7 in the one stretch direction and from 1:0.2 to 1:10 or even 1:0.2 to 1:7 orthogonal to this one stretch direction is preferred. In some embodiments the overall draw ratio is greater than 3:1, greater than 4:1 or even greater than 6:1.

15 The multilayer optical film is generally a compliant sheet of material. For purposes of the present disclosure, the term compliant is an indication that the multilayer optical film is dimensionally stable yet possesses a pliable characteristic that enables subsequent molding or shaping into various forms. In one embodiment, the multilayer optical film may be thermoformed into various shapes or structures for specific end use applications.

20 The multilayer optical film of the present disclosure may find a number of uses. In one embodiment of the present disclosure, the multilayer optical film is an article, such as a UV mirror (i.e., reflects UV wavelengths), an IR mirror (i.e., reflects IR wavelengths), and/or a visible mirror (i.e., reflects visible wavelengths). In another embodiment, the multilayer optical film of the present disclosure may find use in areas where reflection
25 and/or transmission of various wavelengths is desirable. The multilayer optical films may be positioned onto a pane of glass or between two or more panes of glass to be used, for example, in buildings and automobiles to reflect infrared wavelengths, thus lowering heat loads. Further, the multilayer optical films may be positioned onto other substantially transparent plastics to provide reflective properties.

30 The multilayer optical film of the present disclosure may be used in architectural applications, greenhouse applications, solar power applications, lighting, fenestration products, and/or other applications. The multilayer optical films of the present disclosure

may offer advantages including: non- or reduced flammability, improved corrosion resistance, and/or improved UV- and weathering-stability as compared to multilayer optical films made with optical stacks not comprising fluoropolymeric optical layers.

In one embodiment, the multilayer optical film may be used in architectural applications as for example a roof covering, a partial roof covering, a façade covering, or a dome covering. The multilayer optical film used in architectural applications may be designed so as to transmit visible light, but reflect infrared wavelengths, allowing for a transparent covering that will decrease heat load in buildings. In another embodiment, the multilayer optical film used in greenhouse applications may be designed so as to transmit UV wavelengths to allow for maximum plant growth. In another embodiment, the multilayer optical film may be used in solar power applications. For example, in solar power applications, the multilayer optical film may be used in solar cells, solar collection (thermal heating), solar photovoltaic cells, concentrated photovoltaic, or concentrated solar power applications. In another embodiment the multilayer optical film may be used in lighting applications such as shatter resistant lamp covers or reflectors. In another embodiment the multilayer optical film may be used in fenestration products (i.e., products that fill openings in a building, such as windows, doors, skylights, or curtain walls, which e.g., are designed to permit the passage of light). In another embodiment, the multilayer optical film may be used for antireflection applications such as, e.g., mirrors. In another embodiment, the multilayer optical film may be used for industrial applications such as, e.g., protective coatings. For further discussion, see U.S. Prov. Appl. 61/141603 (Attorney Docket No. 64816US002) filed concomitantly with the present disclosure.

In another embodiment, the multilayer optical film of the present disclosure may be converted into glitter in any of a variety of desired shapes and sizes. The glitter may be incorporated into a matrix material (e.g., a cross-linked polymeric material) or a coating composition. The size and shape of the glitter is typically chosen to optimize the appearance of the glitter or to suit a particular end use application. Typically, the glitter used in a coating composition is in pieces wherein the largest dimension of each piece is at least twice the thickness of the multilayer optical film and not more than the maximum thickness of the coating.

Advantages and embodiments of this disclosure are further illustrated by the following examples, but the particular materials and amounts thereof recited in these

examples, as well as other conditions and details, should not be construed to unduly limit this disclosure. All materials are commercially available or known to those skilled in the art unless otherwise stated or apparent.

EXAMPLES

The following specific, but non-limiting examples will serve to illustrate the disclosure.

Examples 1-12: Cast films of various fluorinated polymeric materials were made as follows. The fluorinated polymeric material was delivered at a rate X into a single screw extruder, which was run at a screw speed of Y. The extrudate was extruded at a suitable temperature and was cast onto a three-roll stack at a roll speed of Z and was wound. The thickness of each film was measured to be 500 micrometer (μm) thick with a micrometer gauge. Shown in Table 1 below is the Example, delivery rate in kilograms per hour (kg/hr), screw speed in revolutions per minute (rpm), and roll speed in meters per minute (m/min) for each of the samples tested. All fluorinated polymeric materials were obtained from Dyneon LLC., Oakdale, MN. Each of the cast films was measured with a spectrophotometer (LAMBDA 950 UV/VIS/NIR from PerkinElmer, Inc., Waltham, MA).

TABLE 1

EXAMPLE	DYNEON FLORINATED POLYMERIC MATERIAL	DELIVERY RATE X	SCREW SPEED Y	ROLL SPEED Z
1	ET 6235	2.9 kg/hr	20 rpm	0.20 m/min
2	ETFE 6218X	2.9 kg/hr	20 rpm	0.20 m/min
3	HTE 1705	4.6 kg/hr	26 rpm	0.32 m/min
4	HTE 1510	4.5 kg/hr	24 rpm	0.30 m/min
5	THV 220	3.9 kg/hr	18 rpm	0.24 m/min
6	THV 500	4.8 kg/hr	24 rpm	0.30 m/min
7	THV 415G	5.4 kg/hr	25 rpm	0.33 m/min
8	THVP 2030GX	4.1 kg/hr	22 rpm	0.25 m/min
9	PFA 6502T	3.5 kg/hr	30 rpm	0.20 m/min
10	FEP 6303	3.3 kg/hr	25 rpm	0.20 m/min
11	PVDF 1010/0001	4.2 kg/hr	22 rpm	0.27 m/min
12	PVDF1008/0001	4.2 kg/hr	22 rpm	0.27 m/min

Table 2 (below) reports the % transmittance for each of the fluorinated polymeric materials in Table 1 at selected wavelengths.

TABLE 2

EXAMPLE	% TRANSMITTANCE									
	250 nm	300 nm	350 nm	450 nm	550 nm	650 nm	750 nm	850 nm	950 nm	
1	33.2	52.9	64.0	73.5	80.1	84.3	87.1	89.1	90.7	
2	39.3	57.1	65.8	74.2	80.4	84.5	87.2	89.1	90.6	
3	54.1	65.5	71.1	80.3	85.7	88.8	90.8	92.1	93.1	
4	51.8	53.3	72.0	82.5	87.7	90.7	92.2	93.2	94.0	
5	85.0	89.3	92.2	94.2	94.8	95.0	95.1	95.2	95.3	
6	90.1	88.6	89.6	92.4	93.9	94.6	95.0	95.2	95.4	
7	89.7	90.6	92.3	94.3	94.9	95.3	95.3	95.4	95.6	
8	90.9	93.2	94.3	95.1	95.3	95.4	95.4	95.3	95.7	
9	85.4	80.1	82.0	87.8	91.1	93.0	93.9	94.5	95.0	
10	90.8	84.2	84.0	88.3	91.1	92.8	93.7	94.4	95.0	
11	72.0	77.2	83.4	86.4	87.8	88.7	89.2	89.7	90.5	
12	77.8	79.3	83.5	86.1	87.6	88.7	89.2	89.8	90.5	

Example 13: A coextruded film containing 151 layers was made by extruding a cast web in one operation and later orienting the film in a laboratory film-stretching apparatus. Homopolymers of vinylidene fluoride (PVDF, sold under the trade designation
5 “DYNEON PVDF 1008” by Dyneon LLC.), delivered by one extruder at a rate of 10 pounds per hour (wherein 10% of the flow of the PVDF went into two outer protective boundary layers, each boundary layer being about 10 times the thickness of the high index optical layer), and copolymers of tetrafluoroethylene, hexafluoropropylene, and vinylidene fluoride (sold under the trade designation “DYNEON THVP 2030G X” by Dyneon, LLC.)
10 delivered by another extruder at a rate of 11 pounds per hour, and PVDF for the skin layers, delivered by another extruder at a rate of 10 pounds per hour, were coextruded through a multilayer polymer melt manifold to create a multilayer melt stream having 151 layers with PVDF boundary and skin layers. This multilayer coextruded melt stream was cast onto a chill roll at 0.95 meters per minute (m/min) creating a multilayer cast web 29
15 mils (about 0.74 mm) thick and 6.5 inches (about 16.5 cm) wide. In a second attempt, the multilayer coextruded melt stream was cast onto a chill roll at 3.1 m/min creating a multilayer cast web 9 mils (about 0.23 mm) thick and 5.75 inches (about 14.5 cm) wide.

The multilayer cast web was stretched using a laboratory stretching device, which uses a pantograph to grip a square section of web and simultaneously stretches the web in
20 both directions at a uniform speed. A 4 inch (about 10 cm) square of the 29 mil multilayer cast web was placed into the stretching frame and heated in an oven to 165°C in 90 seconds. The multilayer cast web was then stretched at 50 %/sec (based on the original dimensions) until the web was stretched to about 4 x 4 times the original dimensions. Immediately after stretching, the multilayer optical film was taken out of the stretching
25 device and cooled at room temperature. In a second attempt, a 4 inch (about 10 cm) square of the 9 mil multilayer cast web was placed into the stretching frame and heated in an oven to 165°C in 30 seconds. The multilayer cast web was then stretched at 25 %/sec (based on the original dimensions) until the web was stretched to about 4 x 4 times the original dimensions. Immediately after stretching, the multilayer optical film was taken
30 out of the stretching device and cooled at room temperature.

Example 14: Following the same procedure as in Example 13, multilayer cast web was constructed with copolymer of hexafluoropropylene, tetrafluoroethylene, and ethylene

(HTE, sold under the trade designation “DYNEON HTE 1705” by Dyneon LLC.), and a copolymer of ethylene and tetrafluoroethylene (sold under the trade designation “DYNEON ET 6218X” by Dyneon LLC.), having 151 layers with HTE boundary and skin layers. This multilayer coextruded melt stream was cast onto a chill roll at 0.75 m/min
5 creating a multilayer cast web 30 mils (about 0.76 mm) thick and 6.75 inches (about 17 cm) wide.

Foreseeable modifications and alterations of this invention will become apparent to those skilled in the art without departing from the scope and spirit of this invention. This invention should not be restricted to the embodiments that are set forth in this application
10 for illustrative purposes.

What is claimed is:

1. A multilayer optical film comprising an optical stack, wherein the optical stack comprises:
 - a) first optical layers comprising a first fluoropolymeric material; and
 - b) second optical layers comprising a second fluoropolymeric material,wherein at least a portion of the first optical layers and at least a portion of the second optical layers are in intimate contact.
2. A multilayer optical film according to claim 1, wherein the refractive index difference between the first fluoropolymeric material and the second fluoropolymeric material is less than 0.20.
3. A multilayer optical film according to any one of the previous claims, wherein the refractive index difference between the first fluoropolymeric material and the second fluoropolymeric material is less than 0.10.
4. A multilayer optical film according to any one of the previous claims, wherein the fluoropolymeric material comprises a homopolymer or a copolymer derived from interpolymers of at least one of the following monomers: TFE, VDF, VF, HFP, CTFE, fluoroalkyl vinyl ethers, fluoroalkoxy vinyl ethers, fluorinated styrenes, HFPO, fluorinated siloxanes, or combinations thereof.
5. A multilayer optical film according to any one of the previous claims, wherein the fluoropolymeric material is selected from the group consisting of: copolymers of ethylene and tetrafluoroethylene; copolymers of tetrafluoroethylene, hexafluoropropylene, and vinylidene fluoride; homopolymers of vinylidene fluoride; copolymers of vinylidene fluoride; copolymers of tetrafluoroethylene and propylene; copolymers of tetrafluoroethylene and perfluorovinyl ether; copolymers of hexafluoropropylene, tetrafluoroethylene, and ethylene; homopolymers of chlorotrifluoroethylene; copolymers of ethylene and chlorotrifluoroethylene;

homopolymers of hexafluoropropylene oxide; homopolymers of 4-fluoro-(2-trifluoromethyl)styrene; and copolymers of tetrafluoroethylene and norbornene.

- 5 6. A multilayer optical film according to any one of the previous claims wherein the optical stack comprise layer pairs selected from the group consisting of:
homopolymers of vinylidene fluoride and (copolymers of tetrafluoroethylene, hexafluoropropylene, and vinylidene fluoride) layer pairs; (copolymers of ethylene and chlorotrifluoroethylene) and (copolymers of tetrafluoroethylene, hexafluoropropylene, and vinylidene fluoride) layer pairs; (copolymers of
10 hexafluoropropylene, tetrafluoroethylene, and ethylene) and (copolymers of tetrafluoroethylene, hexafluoropropylene, and vinylidene fluoride) layer pairs;
(copolymers of hexafluoropropylene, tetrafluoroethylene, and ethylene) and (copolymers of ethylene and tetrafluoroethylene) layer pairs; (copolymers of
15 hexafluoropropylene, tetrafluoroethylene, and ethylene) and (copolymers of tetrafluoroethylene and norbornene) layer pairs; and (copolymers of ethylene and tetrafluoroethylene) and (copolymers of tetrafluoroethylene, hexafluoropropylene, and vinylidene fluoride) layer pairs.
- 20 7. A multilayer optical film according to any one of the previous claims wherein at least one of the first fluoropolymeric material or the second fluoropolymeric material is birefringent.
- 25 8. A multilayer optical film according to any one of the previous claims wherein the optical stack comprises at least 5 first optical layers and at least 5 second optical layers.
9. A multilayer optical film according to any one of the previous claims wherein the optical stack comprises at least 50 first optical layers and at least 50 second optical layers.

30

10. A multilayer optical film according to any one of the previous claims wherein the multilayer optical film comprises a draw ratio, wherein the overall draw ratio is greater than 3:1.
- 5 11. A multilayer optical film according to any one of the previous claims wherein the overall draw ratio is greater than 4:1.
12. A multilayer optical film according to any one of the previous claims wherein the overall draw ratio is greater than 6:1.
- 10 13. A multilayer optical film according to any one of the previous claims further comprising at least one of the following:
- a) a printing;
 - b) an adhesive;
 - 15 c) a tear resistant layer;
 - d) a UV-absorbing layer;
 - e) a skin layer; or
 - f) a protective boundary layer.
- 20 14. A multilayer optical film according to any one of the previous claims, further comprising a UV-absorbing compound, an IR-absorbing compound, or combinations thereof, wherein the first optical layers, the second optical layers, or an optional additional layer comprises the UV-absorbing compound, an IR-absorbing compound, or combinations thereof.
- 25 15. A multilayer optical film according to any one of the previous claims, further comprising a functional additive, optionally, wherein the functional additive is a processing additive.
- 30 16. A multilayer optical film according to any one of the previous claims, wherein the multilayer film transmits at least one of the following:
- a) at least a portion of the wavelengths between about 400-700 nm;

- b) at least a portion of the wavelengths greater than about 700 nm;
- c) at least a portion of the wavelengths less than about 300 nm or
- d) at least a portion of the wavelengths between about 300-400 nm.

5 17. A multilayer optical film according to any one of the previous claims, wherein the multilayer film reflects at least one of the following:

- a) at least a portion of the wavelengths between about 400-700 nm;
- b) at least a portion of the wavelengths greater than about 700 nm;
- c) at least a portion of the wavelengths less than about 300 nm; or
- 10 d) at least a portion of the wavelengths between about 300-400 nm.

18. An article comprising the multilayer optical film according to any one of the previous claims.

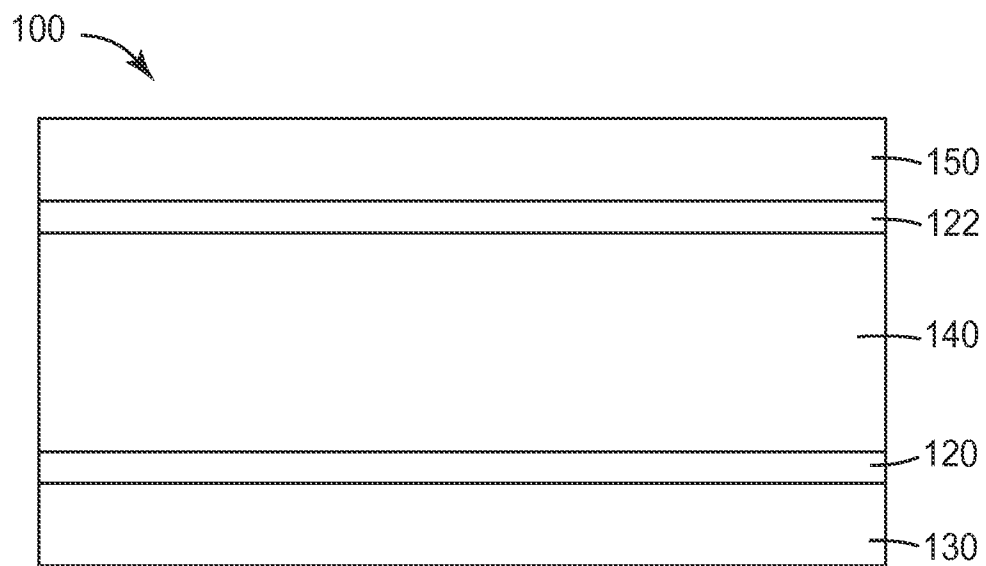
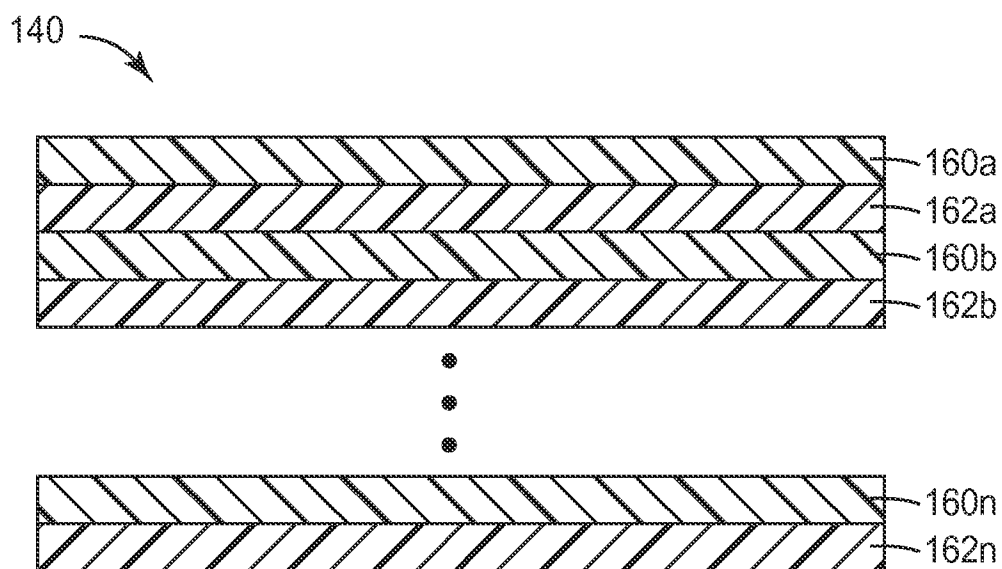
15 19. A method of using a multilayer optical film, wherein the article according claim 18 is used in at least one of the following:

- a) solar power technology;
- b) lighting applications;
- c) antireflection applications; or
- 20 d) industrial applications.

20. A method of making a multilayer optical film comprising:

- a) providing a first optical layer comprising fluoropolymeric material; and
- b) providing a second optical layer comprising fluoropolymeric material.
- 25 c) coextruding the first optical layer and the second optical layer into a web; and
- d) alternately layering the first optical layers and the second optical layers to create an multilayer film.

30 21. The method of claim 20 wherein at least one of first optical layers or second optical layers is birefringent.

*FIG. 1A**FIG. 1B*