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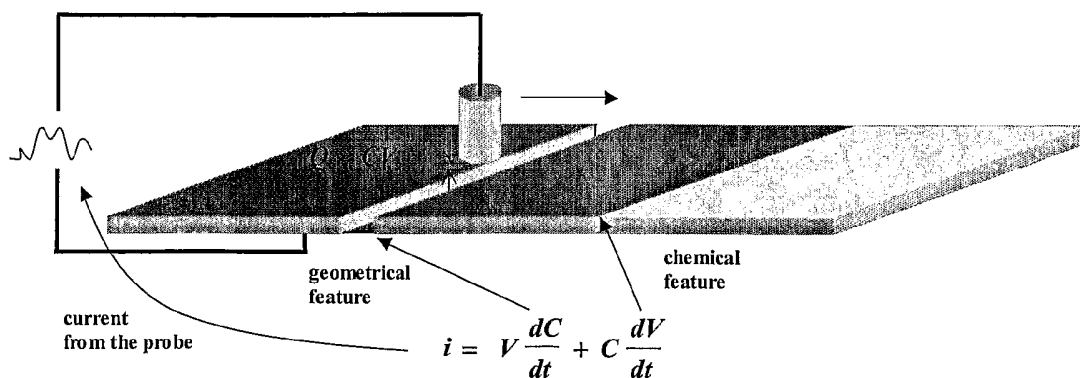
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(54) Title: MEASUREMENT OF MOTIONS OF ROTATING SHAFTS USING NON-VIBRATING CONTACT POTENTIAL DIFFERENCE SENSOR



(57) Abstract: An apparatus having a non-vibrating contact potential probe. The non-vibrating contact potential probe is capable of measuring the chemical and geometrical irregularities on a rotating shaft. The chemical and geometrical information can be used to determine various properties of the rotating shaft.

MEASUREMENT OF MOTIONS OF ROTATING SHAFTS USING NON-VIBRATING CONTACT POTENTIAL DIFFERENCE SENSOR

CROSS-REFERENCE TO RELATED PATENT APPLICATIONS

[0001] This application is an application claiming the benefit under 35 U.S.C. 119(e) of U.S. Provisional Application Number 60/490,161, filed 07/25/2003, incorporated herein by reference in its entirety.

BACKGROUND OF THE INVENTION

[0002] Many mechanical systems include rotating shafts for coupling or transmitting rotational energy from one location to another. Examples include but are not limited to the shafts used in cars, boats, planes, power generation turbines and compressors. In many cases it is necessary or desirable to measure the motion of the shaft in operation. Specific measurements of interest include but are not limited to rotational velocity, rotational acceleration, rotational vibration (also called torsional vibration), lateral vibration, twist and torque. These measurements may be necessary to control the motion of the shaft during operation, to monitor the shaft or machine for motions that indicate problems or potential failures, or to evaluate and optimize the performance of the machine during design or manufacture.

[0003] Contact potential difference (CPD) measurements have been used as one form of sensor technology. CPD refers to the fact that different metals have different electron energies and work functions, and that when two metals are placed in electrical contact, electrons flow from the metal with the lower work function to the metal with the higher work function. If two different metals are connected electrically and then brought in close proximity, then an electric field is formed between them as a result of their CPD.

[0004] "Vibrating CPD sensor" refers to the vibration of one metal relative to the other in a parallel plate capacitor system. That is, the vibrating CPD sensor operates by electrically connecting two metals and vibrating one metal of known work function (the probe) over the second metal of unknown work function. The vibration induces changes in capacitance over time. A time varying signal is generated that is a function of the capacitance and the voltage that results from the CPD between the two metals. A variable electrical potential is applied

between the two metals and adjusted until the time-varying current is eliminated. The resulting applied voltage is the CPD between the two metals. The work function of the unknown metal can then be calculated as the work function of the probe plus or minus the applied potential. Non-vibrating CPD sensors (nvCPD) are also known. Such probes are not vibrated, but rather the probe and the testing surface are moved relative to each other. This translation makes high speed scanning possible.

[0005] Several options exist to monitor the motion of a rotating shaft. The most common method of measuring rotary shaft motion is to use an encoder. An encoder is a device that attaches to a shaft and converts rotary motion into electrical pulses. Encoders can provide precise information on shaft motion, but they are relatively expensive and require substantial effort to mount on a shaft. Lower-cost or temporary encoders for measuring rotary motion can be built by mounting some sort of target to the shaft and then detecting the presence or location of the target using a separate sensor. For example, magnetic targets can be mounted to a shaft and detected using Hall Effect sensors, or a patterned tape can be mounted on the shaft and motion detected using an optical sensor. These techniques require the effort and expense of modifying the shaft so that its motion can be detected, and are limited to detecting rotary motion. It is also possible to measure shaft motion without modifying the shaft by mounting optical or eddy current sensors above a gear to detect the presence or motion of gear teeth. This technique is limited in that it can only be used at the locations of gears in the system.

[0006] Several techniques also exist for measuring lateral vibrations of a rotating shaft. These include the use of laser interferometers or eddy current sensors to detect the distance between the sensor and the surface of the shaft. Vibrations can also be detected using accelerometers mounted to various locations on the machine. These techniques are limited to measuring lateral vibration and, in the case of accelerometers, measuring machine vibrations and not the vibration of the shaft itself. In general, it can be expensive, time-consuming, and difficult to precisely measure both the lateral and rotary motions of a rotating shaft.

SUMMARY OF THE INVENTION

[0007] The present invention generally relates to measurement methods and systems. More specifically, the present invention relates to measurement methods and systems using non-vibrating contact potential difference sensors.

[0008] The present invention relates to a system and method of measuring the motion of a rotating shaft using one or more non-vibrating contact potential difference (nvCPD) sensor(s), described herein before. The nvCPD sensor(s) are mounted in proximity to a rotating shaft. The output of the sensor is generated by small physical or chemical changes on the surface of the shaft. These changes occur naturally in all shafts, but they can also be induced onto the shaft surface by creating physical or chemical marks. Such marker features generate a pattern that can be detected by the nvCPD sensor. This pattern repeats with each rotation of the shaft. The output of the sensor(s) can be processed in either the time or frequency domains to extract the rotational velocity, the rotational acceleration, and/or rotational (torsional) vibration of the shaft. Comparison of the phases of signals from two or more sensors can be used to measure the twist and torque applied to the shaft. In addition, a bias voltage can be applied to the nvCPD sensor so that the output results predominantly from changes in the distance between the sensor and the surface of the shaft. The output of the biased sensor can be processed in either the time or frequency domains to detect and measure lateral vibrations or motions of the shaft.

BRIEF DESCRIPTION OF THE DRAWINGS

[0009] FIGURE 1 illustrates the theory of operation for a Non-Vibrating Contact Potential Difference (nvCPD) sensor;

[0010] FIGURE 2 is a drawing of a nvCPD sensor mounted above a rotating shaft with a sample output showing periodic signal from the shaft surface; and

[0011] FIGURE 3 is a comparison of the phase changes between two sensors at opposite ends of a shaft which can be used to measure twist in the shaft, and calculate the applied torque.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0012] The present invention provides methods and systems for using nvCPD sensors to detect features, for example, including but not limited to physical or chemical features, on a surface that is in motion relative to the sensor itself. FIG. 1 illustrates the theory of operation for a nvCPD sensor. In a preferred embodiment, the output of an nvCPD sensor is an electrical current that is a function of both chemical changes on a surface and changes in the capacitance between the sensor and surface. The nvCPD sensor can therefore be used to detect both chemical and physical changes on a surface. In one embodiment, an nvCPD

sensor can be built to have a variable and automatically adjustable bias voltage that can be used to automatically alter the sensor so that it detects predominantly capacitance changes between the sensor and surface. These capacitance changes can be used to measure the distance between the sensor and a moving surface. The apparatus is capable of monitoring the performance of the rotating shaft and to detect abnormal motions which can indicate an impending breakdown. The shaft data collected by the nvCPD sensor can be compared to historical or theoretical data on shaft performance and thus used to determine if the system is likely to experience a breakdown at some point in the future. In an exemplary embodiment, this is done by looking at torsional or lateral vibrations in the frequency domain and examining how the vibrations change over time.

[0013] The nvCPD apparatus of the present invention utilizes a probe as a first metal surface and a testing surface as a second metal. These two metals are then placed in close proximity and moved relative to each other so that a somewhat consistent gap is maintained between them. Changes in capacitance or voltage between the two metals result in currents into or out of the probe. These currents indicate changes in either the capacitance between the probe and surface or changes in the voltage between the probe and surface. Changes in the voltage result from chemical changes on the measured surface that result in changes in the surface work function and resulting CPD.

[0014] The charge Q on a capacitor is given by the equation:

$Q=CV$; where C is the capacitance and V is the voltage.

Differentiating both sides yields:

$$\frac{dQ}{dt} = i = \frac{d(CV)}{dt} = C \frac{dV}{dt} + V \frac{dC}{dt}$$

where i is the current into or out of the probe tip.

if

Φ_p = work function of the probe, and

Φ_s = work function of the surface to be measured, then

$CPD = (\Phi_p - \Phi_s)/e$, where e is the charge of an electron.

In a vibrating CPD sensor CPD (V) is fixed, so the current out is:

$$i = V \frac{dC}{dt}; \quad \text{where the change in capacitance is provided by the vibrating motion.}$$

[0015] With a non-vibrating CPD sensor, both voltage (V) and capacitance (C) change as the probe moves relative to the surface. The current out of the probe tip is given by:

$$i = C \frac{dV}{dt} + V \frac{dC}{dt}$$

The first term, $C \frac{dV}{dt}$, is the current due to changes in the voltage between the probe and surface. This voltage is due to the CPD. Since the work function of the probe is fixed, changes in voltage are the result of changes in the work function of the surface being

measured. The second term, $V \frac{dC}{dt}$, is the current due to changes in the capacitance between the probe tip and the surface being measured. Changes in capacitance are usually due to changes in the distance between the probe tip and surface. If the sensor is firmly attached to a fixed reference surface, then the signal from this term is the result of changes in sensor-surface gap due to motion of the surface. This unique sensor output that contains information about both the chemistry and motion of the measured surface has important advantages in monitoring the motion of a rotating shaft.

[0016] In an exemplary embodiment, one or more nvCPD sensors are placed in close proximity to a moving shaft and the output of each nvCPD sensor is converted into a series of digital values. FIG. 2 illustrates a sample output showing a periodic signal from the shaft surface. As can be seen in FIG. 2, the signal exhibits a periodic or repeating pattern, which in essence represents one revolution of the shaft or component being rotated. These values are processed in either the time or frequency domains to determine the frequency at which the signal repeats. This frequency determines the rotational velocity of the shaft. Changes in the frequency determine the rotational acceleration of the shaft. Multiple position, velocity or acceleration measurements can be used to detect and measure rotational vibrations of the shaft.

[0017] A CPD sensor can also be built so that a bias voltage can be applied to each sensor to increase the magnitude of the output signal that is due to capacitance changes. This component can be made much larger than the output component that is due to chemical changes on the shaft surface. As a result, the output current can be made largely a function of the distance between the sensor and the shaft surface. This output can be processed in the time or frequency domains to detect the frequency and magnitude of any lateral vibrations or motions of the shaft. This information can be combined with information about the rotational velocity to determine if the lateral vibrations are at the same frequency as the rotation of the shaft or at some multiple of the shaft frequency. This information can be useful for determining the source of the vibration.

[0018] In addition, a biased sensor can be used to extract a signal which consists solely of height data. If two scans are acquired of the same surface with different bias voltages, then one scan can be subtracted from the other to eliminate chemistry information from the signal.

[0019] Looking at the equation for the current out of the probe tip:

$$i = C \frac{dV}{dt} + V \frac{dC}{dt}$$

if two scans of the same surface are made with two different bias voltages, b_1 and b_2 , then the resulting currents are:

$$i_{b1} = C \frac{dV}{dt} + (V_{CPD} + V_{b1}) \frac{dC}{dt}$$

$$i_{b2} = C \frac{dV}{dt} + (V_{CPD} + V_{b2}) \frac{dC}{dt}$$

Subtracting the second scan from the first results in a signal that is solely dependant on capacitance (height) changes:

$$i_{b1} - i_{b2} = (V_{b1} - V_{b2}) \frac{dC}{dt}$$

[0020] This technique can be used to extract height information from the combined height and data information present in the nvCPD sensor signal. This height information can be used to measure lateral (radial) motion of a shaft such as vibration or wobble.

[0021] In order to make quantitative measurements of shaft motion or vibration, it is necessary to know the approximate mean or starting distance between the probe tip and the surface of the shaft. This may be accomplished in several ways, some of which are described below, however these embodiments are not to be considered limiting, but merely exemplary.

[0022] In one exemplary embodiment, when the sensor is installed, a piece of material of known thickness can be inserted between the probe tip and shaft surface to adjust the probe to a known height. The piece of material is sometimes called a feeler gauge or spacer.

[0023] In another exemplary embodiment, the sensor is moved towards the shaft surface until the probe tip makes contact. This results in a large signal output from the sensor that can be automatically detected by signal processing. The sensor can then be moved a known distance away from the shaft surface.

[0024] In another exemplary embodiment, a time-varying bias signal can be applied to the sensor or shaft. The output of the sensor will vary with the capacitance between the probe tip and the shaft surface. The output can be compared to a calibrated curve to determine the approximate distance between the probe tip and shaft.

[0025] In some instances the shaft may not be well-grounded or electrically connected to other mechanical components. Thus, in one exemplary embodiment, an electrical connection is added between the shaft and a ground point.

[0026] In another embodiment, information from multiple sensors can be combined to determine twist of the shaft. As illustrated in FIG. 3, the signals for two probes located at different locations will exhibit a phase shift dependent on the twist of the shaft being rotated. Material properties of the shaft can be used to calculate the torque on the shaft between the two points.

[0027] It should be understood that various changes and modifications preferred in to the embodiment described herein would be apparent to those skilled in the art. Such changes and modifications can be made without departing from the spirit and scope of the present invention and without demising its attendant advantages.

WHAT IS CLAIMED IS:

1. An apparatus for monitoring motion of a rotating shaft comprising:
at least one non-vibrating contact potential probe;
a source of data regarding the state of the shaft;
the data indicating whether the shaft is in a state selected from the group consisting of a normal state and an abnormal state;
a mechanism for measuring contact potential difference between the shaft and the at least one non-vibrating contact potential probe; and
an output signal characteristic of the contact potential difference.
2. The apparatus of Claim 1 further comprising a system component for altering the signal output by the at least one non-vibrating contact potential probe.
3. The apparatus of Claim 2, wherein the system component for altering the signal comprises a bias voltage source which applies a voltage to the at least one non-vibrating contact potential probe.
4. The apparatus of Claim 1, wherein the at least one non-vibrating contact potential probe comprises a plurality of probes.
5. The apparatus of Claim 4, wherein the plurality of probes comprise a first probe and a second probe located a fixed distance apart.
6. The apparatus of Claim 1, wherein the abnormal state indicated by the data is torsional or lateral vibration.
7. The apparatus of Claim 1 further comprising an electrical connection between the shaft and either the non-vibrating contact potential sensor or a ground point.
8. A method of measuring rotation of a component comprising the steps of:
providing a non-vibrating contact potential probe;
rotating the component with respect to the non-vibrating contact potential probe;
monitoring the relative motion between the non-vibrating capacitance probe and the component;
measuring the change in voltage and the change in current due to the relative motion; and
outputting a signal comprising voltage information and current information characteristic of an operating state of the component undergoing rotation.

9. The method of Claim 8 further comprising the step of converting the signal to digital values.
10. The method of Claim 8 further comprising the step of processing the signal in a domain to determine a frequency at which the signal repeats.
11. The method of Claim 8 further comprising the step of altering the signal to make a capacitance portion of the signal much larger than a chemical portion of the signal.
12. The method of Claim 11, wherein the step of altering the signal comprises applying a bias voltage to the non-vibrating contact potential probe wherein the magnitude of the capacitance portion of the signal is increased.
13. The method of Claim 12 further comprising the step of comparing the altered signal with an unaltered signal to determine at least one of magnitude and frequency of lateral vibrations in the component.
14. The method of Claim 8, wherein the step of providing a non-vibrating contact potential probe includes providing a first non-vibrating contact potential probe and a second non-vibrating contact potential probe.
15. The method of Claim 14 further comprising the step of spacing the first non-vibrating contact potential probe a fixed distance from the second non-vibrating contact potential probe, wherein the change in the phase of repetition of the signal at the two locations indicates a twist.
16. The method of Claim 8 further comprising the step of forming an irregularity on the surface of the component.
17. A process for using surface variations on a shaft to determine at least one characteristic of the shaft, the process comprising the steps of:
providing a non-vibrating contact potential probe;
rotating the shaft with respect to the non-vibrating contact potential probe;
outputting a signal caused by motion of the shaft relative to the non-vibrating contact potential probe; and
interpreting the signal to determine at least one characteristic of the shaft.
18. The process of Claim 17 further comprising the step of altering the signal to make a capacitance portion of the signal much larger than a chemical portion of the signal

19. The process of Claim 18, wherein the step of altering the signal comprises applying a bias voltage to the non-vibrating contact potential probe wherein the magnitude of the capacitance portion of the signal is increased.

20. The process of Claim 17 comprising a first non-vibrating contact potential sensor and a second non-contact potential sensor and further comprising the step of spacing the first non-vibrating contact potential probe a fixed distance from the second non-vibrating contact potential probe, wherein the change in the phase of repetition of the signal at the two locations indicates a twist.

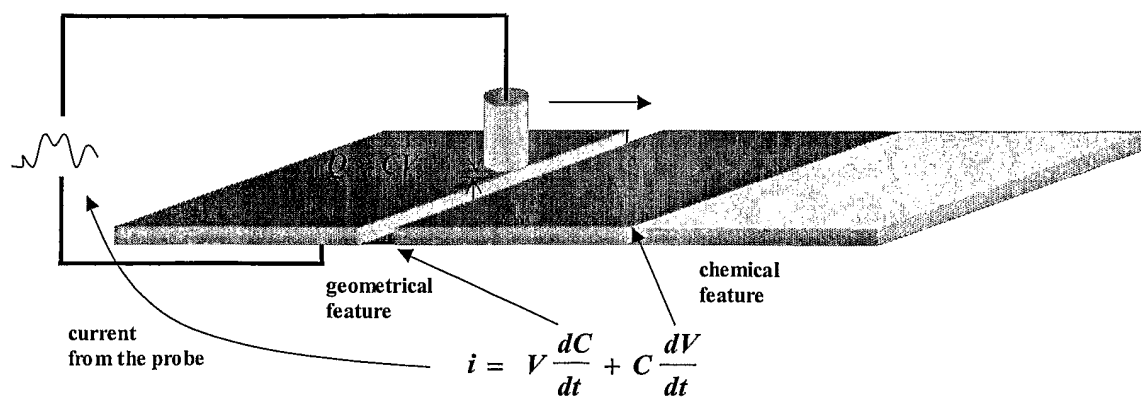


FIGURE 1

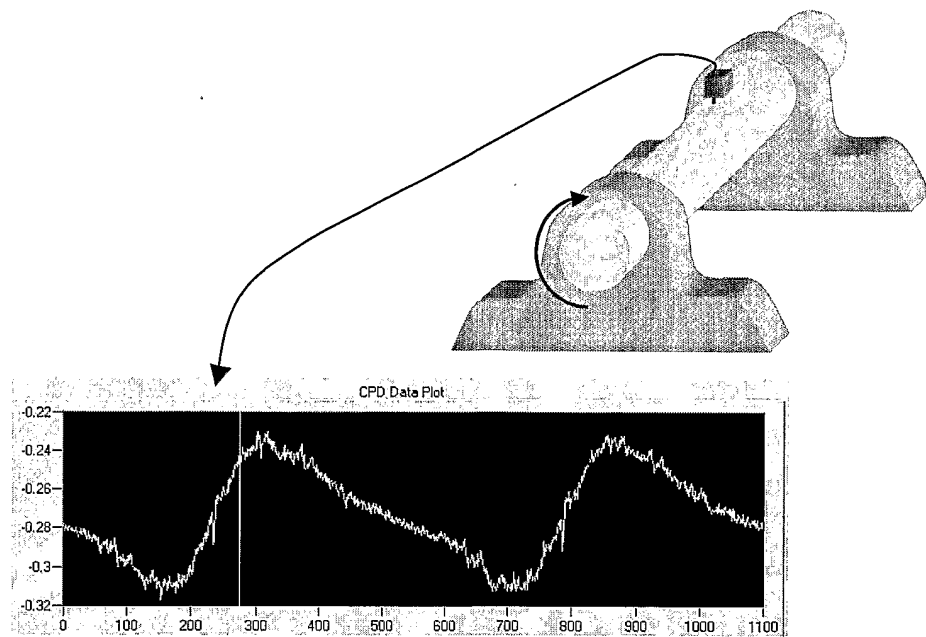


FIGURE 2

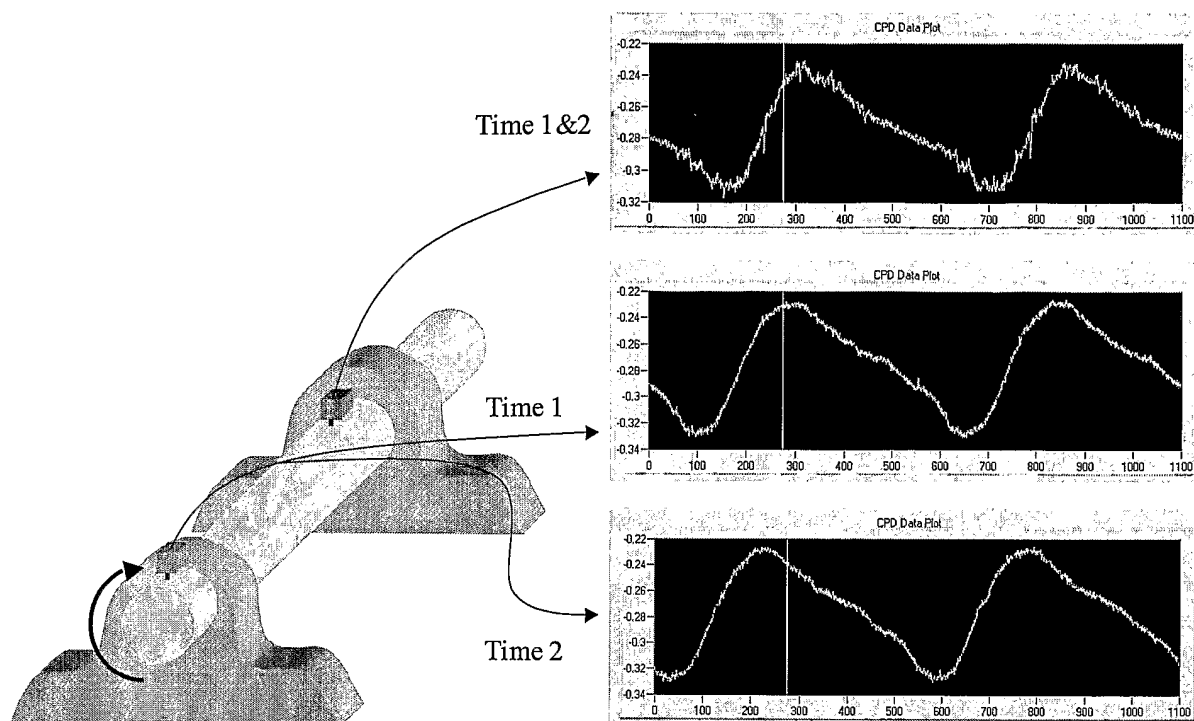


FIGURE 3

INTERNATIONAL SEARCH REPORT

International Application No
PCT/US2004/023983

A. CLASSIFICATION OF SUBJECT MATTER
IPC 7 G01H1/00

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 7 G01R G01N G01H

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category °	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 5 974 869 A (ZHARIN ANATOLY ET AL) 2 November 1999 (1999-11-02) column 1, line 66 - column 2, line 67 column 4, line 65 - column 5, line 47 column 6, lines 27-53 figures 1-10	1-20
Y	US 6 546 814 B1 (GLESMANN JONATHAN M ET AL) 15 April 2003 (2003-04-15) figures 3,4,12-18 column 14, line 42 - column 15, line 48	1-20
A	US 4 973 910 A (WILSON MAHLON S) 27 November 1990 (1990-11-27) column 2, line 39 - column 5, line 63 figures 1-4	1-20
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☒ Further documents are listed in the continuation of box C.

☒ Patent family members are listed in annex.

° Special categories of cited documents :

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19/11/2004

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INTERNATIONAL SEARCH REPORT

International Application No
PCT/US2004/023983

C.(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT		
Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	EP 1 039 277 A (MERITOR HEAVY VEHICLE SYS LTD) 27 September 2000 (2000-09-27) column 2, paragraph 9 - column 5, paragraph 19 figures 1-5 -----	1-20
A	EP 1 304 463 A (GEN ELECTRIC) 23 April 2003 (2003-04-23) column 5, paragraph 19 - column 10, paragraph 34 figures 1-5 -----	1-20

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Information on patent family members

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