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(71) Applicant: **JOHNS MANVILLE** [US/US]; 717 Seventeenth Street, Denver, CO 80202 (US).

(72) Inventors: **CAI, Yifang**; 11997 West Coal Mine Drive, Littleton, CO 80127 (US). **HUBER, Aaron, Morgan**; 7710 Saxeborough Drive, Castle Rock, CO 80108 (US).

(74) Agent: **TOUSLEE, Robert, D.**; Johns Manville, 10100 West Ute Avenue, Littleton, CO 80127 (US).

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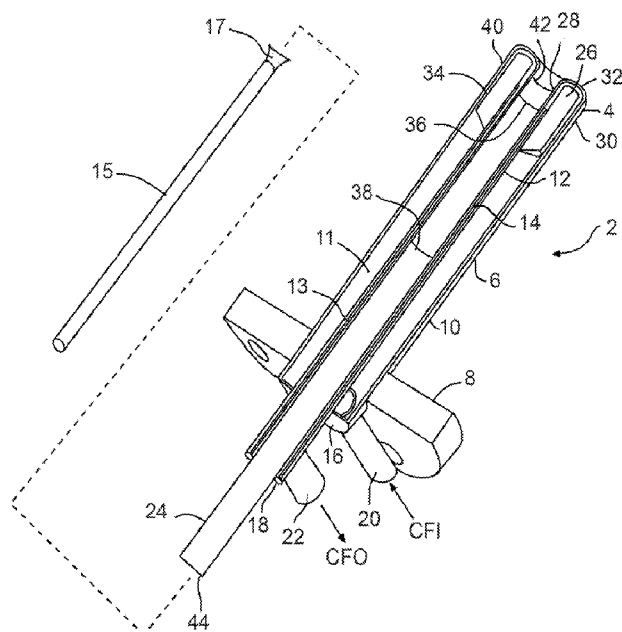


FIG. 1

(57) Abstract: Submerged combustion burners having a burner body, a burner tip connected thereto, and a protective cap and/or cladding layer. Submerged combustion melters including the burners and methods of using them to produce molten glass. The burner body has an external conduit and first and second internal conduits substantially concentric therewith, forming first and second annuli for passing a cooling fluid therethrough. The burner tip body is connected to the burner body at ends of the external and second internal conduits. The burner tip and protective cap and/or cladding layer include a generally central flow passage for a combustible mixture, the flow passage defined by an inner wall of the burner tip and protective cap.



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**SUBMERGED COMBUSTION BURNERS AND MELTERS,
AND METHODS OF USE**

5 [0001] BACKGROUND INFORMATION

[0002] Technical Field

10 [0003] The present disclosure relates generally to the field of combustion burners and methods of use, and more specifically to burners, submerged combustion melters, and methods of their use, particularly for melting glass-forming materials.

[0004] Background Art

15 [0005] A submerged combustion melter (SCM) may be employed to melt glass batch and/or waste glass materials to produce molten glass by passing oxygen, oxygen-enriched mixtures, or air along with a liquid, gaseous and/or particulate fuel (some of which may be in the glass-forming materials), directly into a molten pool of glass, usually through burners submerged in a glass melt pool. The introduction of high flow rates of
20 products of combustion of the oxidant and fuel into the molten glass, and the expansion of the gases during submerged combustion (SC), cause rapid melting of the glass batch and much turbulence.

[0006] In the context of SCMs, known oxy-fuel burners are predominately water-cooled,
25 nozzle mix designs and avoid premixing for safety reasons due to the increased reactivity of using oxygen as the oxidant versus air. One currently used submerged combustion burner employs a smooth exterior surface, half-toroid metallic burner tip of the same or similar material as the remainder of the burner. When operating and SCM with burners of this nature, the combustion burner tips are exposed to a glass and combustion gas
30 environment high and oscillating temperatures. The burner can be designed so that the oxidant (typically oxygen) or fuel flow cools the inner wall of the burner tip before combustion occurs, but the flow cannot provide cooling to the top crown and outer wall of the burner tip. Although cooling water or other coolant is typically applied to cool the burner tip, the temperatures are extremely high for typical metal alloys when the hot glass
35 (2500+°F (1,370+ °C)) or combustion products (up to 4000 °F (2,190 °C)) contact the burner tip. Also, since the burner tip section temperature is oscillating with the combustion

bubble growth, the burner tip experiences frequent rapid temperature change. Therefore, burner life can be very short due to the failure of the materials used to form the burner tip.

5 [0007] Development of submerged combustion burners having longer life and less susceptibility to the SCM environment while melting glass-forming materials would be a significant advance in the submerged combustion art.

[0008] SUMMARY

10 [0009] In accordance with the present disclosure, submerged combustion (SC) burners, melters including at least one of the submerged combustion burners, and methods of using the melters to produce molten glass are described that may reduce or eliminate problems with known SC burners, melters, and methods.

[0010] A first aspect of the disclosure is a fluid-cooled burner comprising:

a burner body (6) comprising an external conduit (10) and a first internal conduit (12) substantially concentric therewith, and positioned internal of the external conduit (10), the external conduit (10) comprising a first end, a second end, and a longitudinal bore having a longitudinal axis, the first internal conduit (12) comprising a first end, a second end, and a longitudinal bore having a longitudinal axis, and a second internal conduit (14) substantially concentric with, and positioned internal of the first internal conduit, the second internal conduit (14) comprising a first end, a second end, and a longitudinal bore having a longitudinal axis, the external conduit (10) and first internal conduit (12) forming a first annulus (11) there between for passing a cooling fluid, the first internal conduit (12) and the second internal conduit (14) forming a second annulus (13) there between for passing the cooling fluid, and a third internal conduit (15) configured to form a third annulus between the second (14) and third (15) internal conduits, the burner body comprising fuel and oxidant inlet ports near the second ends of the conduits; and

15 a burner tip (4) defined by an inner wall (28) and an outer wall (30) connected via a crown (32), the outer wall (30) removably fixed to the first end of the external conduit (10) via an outer connection, and the inner wall (28) removably fixed to the first end of the second internal conduit (14) via an inner connection, the burner tip (4) comprising a generally central burner tip flow passage configured to pass a combustible mixture therethrough, the generally central burner tip flow passage defined by the inner wall (28); and

wherein the burner comprises a protective cap (50) positioned adjacent at least a circumferential and radial portion of the burner tip body and defining a generally central

protective cap flow passage downstream of the generally central burner tip flow passage configured to pass the combustible mixture therethrough, the generally central protective cap flow passage defined by a cap inner wall (51).

Optionally, the burner tip crown (32) and inner (28) and outer (30) walls may comprise the same or different corrosion resistant and fatigue resistant material, at least one of the corrosion and/or fatigue resistance being greater than material comprising the external conduit (10) under conditions experienced during submerged combustion melting of glass-forming materials.

[0011] A second aspect of the disclosure is a submerged combustion melter comprising:
a floor, a roof, and a sidewall structure connecting the floor and roof defining an internal space, at least a portion of the internal space comprising a melting zone; and
one or more combustion burners in either the floor, the roof, the sidewall structure,
or any two or more of these, producing combustion gases and configured to emit the combustion gases from a position under a level of, and positioned to transfer heat to and produce a turbulent molten mass of glass in the melting zone, at least one of the combustion burners being a fluid-cooled combustion burner as described herein.

[0012] A third aspect of the disclosure are methods of producing molten glass comprising feeding glass-forming materials to a submerged combustion melter including at least one fluid-cooled combustion burner as described herein, feeding an oxidant and a fuel to the burner, combusting the fuel and oxidant, and melting the glass-forming materials to produce molten glass.

[0012] Certain methods within the disclosure include methods wherein the fuel may be a substantially gaseous fuel selected from the group consisting of methane, natural gas, liquefied natural gas, propane, carbon monoxide, hydrogen, steam-reformed natural gas, atomized oil or mixtures thereof, and the oxidant may be an oxygen stream comprising at least 90 mole percent oxygen.

[0013] Burners, melters, and methods of the disclosure will become more apparent upon review of the brief description of the drawings, the detailed description of the disclosure, and the claims that follow.

[0014] BRIEF DESCRIPTION OF THE DRAWINGS

[0015] The manner in which the objectives of the disclosure and other desirable characteristics can be obtained is explained in the following description and attached schematic drawings in which:

5 [0016] FIG. 1 is a longitudinal cross-section view of fluid-cooled portions of a prior art burner and burner tip, showing typical welded connections between conduits and the burner tip comprising similar mild steel or other base metals, and illustrating a central, substantially concentric fuel or oxidant conduit (not shown in other figures);

10 [0017] FIG. 2A is a perspective view, and FIG. 2B is a longitudinal sectional view of a portion of one burner embodiment in accordance with the present disclosure;

[0018] FIGS. 3, 4, 5A, and 9 are cross-sectional views of four non-limiting burner embodiments, and FIG. 5B is a plan view of the burner of FIG. 5A;

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[0019] FIGS. 6A and 6B show results of simulations using a Computational Fluid Dynamic tool for a prior art burner and a burner in accordance with the present disclosure;

20 [0020] FIG. 7 shows graphically the thermal cycling of an unprotected burner tip, and the lack thereof and much lower temperature of the burners simulated in FIGS. 6A and 6B; and

[0021] FIG. 8 is a cross-sectional view of an SCM in accordance with the present disclosure.

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[0022] It is to be noted, however, that the appended drawings are schematic only, may not be to scale, illustrate only typical embodiments of this disclosure, and are therefore not to be considered limiting of its scope, for the disclosure may admit to other equally effective embodiments.

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[0023] DETAILED DESCRIPTION

[0024] In the following description, numerous details are set forth to provide an understanding of the disclosed apparatus and methods. However, it will be understood by 35 those skilled in the art that the apparatus and methods covered by the claims may be practiced without these details and that numerous variations or modifications from the

specifically described embodiments may be possible and are deemed within the claims. All U.S. published patent applications and U.S. Patents referenced herein are hereby explicitly incorporated herein by reference. In the event definitions of terms in the referenced patents and applications conflict with how those terms are defined in the present application, the definitions for those terms that are provided in the present application shall be deemed controlling. All percentages herein are based on weight unless otherwise specified.

[0025] As explained briefly in the Background, in present SC burners employing a metallic burner tip, the burner can be designed so that the oxidant or fuel flow cools the inner wall of the burner tip before combustion occurs, but the flow cannot provide cooling to the top crown and outer wall of the burner tip. Although cooling water or other coolant is typically applied to cool the burner tip, the extremely high temperature molten glass and combustion gases contact the outer wall and crown of the burner tip. In this environment the burner tip temperature in these regions oscillates with the combustion gas bubble growth and burst cycle. Thus, the burner tip experiences not only extremely high temperatures, but also frequent rapid temperature change. Therefore, burner life can be very short due to the failure of the materials used to form the burner tip.

[0026] The burners of the present disclosure solve this problem by providing a protective cap comprising materials selected from refractory, ceramic, exotic alloys, and the like, over at least portions or regions of the burner tip. The protective cap is able not only to withstand both the high and highly oscillating temperatures and abrasive nature in this environment, but also can be formed at least on the critical areas of the burner tip to protect it from the high oscillating temperatures.

[0027] FIG. 1 illustrates schematically a prior art SC burner having a fluid-cooled portion 2 composed of a burner tip 4 attached to a burner body 6. A burner main flange 8 connects the burner to an SCM superstructure, not illustrated. Burner body 6 comprises an external conduit 10, a first internal conduit 12, a second internal conduit 14, and end plates 16, 18. A coolant fluid inlet conduit 20 is provided, along with a coolant fluid exit conduit 22, allowing ingress of a cool coolant fluid as indicated by the arrow denoted "CFI", and warmed coolant fluid egress, as indicated by an arrow denoted "CFO", respectively. A first annulus 11 is thus formed between substantially concentric external conduit 10 and first internal conduit 12, and a second annulus 13 is formed between substantially concentric first and second internal conduits 12, 14. A proximal end 24 of second internal

conduit 14 may be sized to allow insertion of a fuel or oxidant conduit 15 (depending on the burner arrangement), which may or may not include a distal end nozzle 17. When conduit 15 and optional nozzle 17 are inserted internal of second internal conduit 14, a third annulus is formed there between. In certain embodiments, oxidant flows through the
5 third annulus, entering through a port 44, while one or more fuels flow through conduit 15. In certain other embodiments, one or more fuels flow through the third annulus, entering through port 44, while oxidant flows through conduit 15.

[0028] Still referring to FIG. 1, fluid-cooled portion 2 of the burner includes a ceramic or
10 other material insert 26 fitted to the distal end of first internal conduit 12. Insert 26 has a shape similar to but smaller than burner tip 4, allowing coolant fluid to pass between burner tip 4 and insert 26, thus cooling burner tip 4. Burner tip 4 includes an inner wall 28, an outer wall 30, and a crown 32 connecting inner wall 28 and outer wall 30. In prior art
15 burners, welds at locations 34 and 36, and optionally at 38, 40 and 42, connect burner tip 4 to external conduit 10 and second internal conduit 14, using conventional weld materials to weld together similar base metal parts, such as carbon steel, stainless steel, or titanium. Despite the use of coolant and even titanium (which ordinarily is considered
20 quite corrosion-resistant), the operating life of SC burners as illustrated and described in relation to FIG. 1 are very limited in the SCM environment, where temperatures of molten glass may reach 1370°C, combustion products may reach 2,190°C, temperatures may oscillate 500°C several times a second, and the turbulence of the molten glass caused by the combustion gases emanating from the burners themselves contribute to form a highly erosive environment in contact with the burner tip.

[0029] It has now been discovered that provision of a protective cap over substantial
25 portions or all of the burner tip not only removes direct contact of substantial regions of the burner tip with the SCM environment and reduces the temperature of at least the protected regions of the burner tip, but surprisingly also reduces or eliminates the oscillating temperature of the burner tip. Careful selection of protective cap material and
30 geometry, and optionally the burner tip material and type of connections between the burner tip walls and conduits forming the burner body, may significantly increase the operating life of SC burners used to melt glass-forming materials in an SCM. Optionally, the burner tip crown and inner and outer walls may comprise the same or different corrosion resistant and fatigue resistant material, at least one of the corrosion and/or
35 fatigue resistance being greater than material comprising the external conduit under conditions experienced during submerged combustion melting of glass-forming materials.

[0030] Various terms are used throughout this disclosure. As used herein, a “cap” or “protective cap” covers and/or is adjacent substantial portions of a burner tip. “Submerged” as used herein means that combustion gases emanate from a combustion burner through the burner tip and protective cap under the level of the molten glass; the burners may be floor-mounted, roof-mounted, wall-mounted, or in melter embodiments comprising more than one submerged combustion burner, any combination thereof (for example, two floor mounted burners and one wall mounted burner). “SC” as used herein means “submerged combustion” unless otherwise specifically noted, and “SCM” means submerged combustion melter unless otherwise specifically noted.

[0031] As used herein the phrase “combustion gases” as used herein means substantially gaseous mixtures comprised primarily of combustion products, such as oxides of carbon (such as carbon monoxide, carbon dioxide), oxides of nitrogen, oxides of sulfur, and water, as well as partially combusted fuel, non-combusted fuel, and any excess oxidant. Combustion products may include liquids and solids, for example soot and unburned liquid fuels.

[0032] “Oxidant” as used herein includes air (“air” includes gases having the same molar concentration of oxygen as air); oxygen-enriched air (air having oxygen concentration greater than 21 mole percent), and “pure” oxygen, such as industrial grade oxygen, food grade oxygen, electronic grade oxygen, and cryogenic oxygen. Oxygen-enriched air may have 50 mole percent or more oxygen, and in certain embodiments may be 90 mole percent or more oxygen.

[0033] The term “fuel”, according to this disclosure, means a combustible composition comprising a major portion of, for example, methane, natural gas, liquefied natural gas, propane, hydrogen, steam-reformed natural gas, atomized hydrocarbon oil, combustible powders and other flowable solids (for example coal powders, carbon black, soot, and the like), and the like. Fuels useful in the disclosure may comprise minor amounts of non-fuels therein, including oxidants, for purposes such as premixing the fuel with the oxidant, or atomizing liquid or particulate fuels. As used herein the term “fuel” includes gaseous fuels, liquid fuels, flowable solids, such as powdered carbon or particulate material, waste materials, slurries, and mixtures or other combinations thereof.

[0034] The sources of oxidant and fuel may be one or more conduits, pipelines, storage facility, cylinders, or, in embodiments where the oxidant is air, ambient air. Oxygen-enriched oxidants may be supplied from a pipeline, cylinder, storage facility, cryogenic air separation unit, membrane permeation separator, or adsorption unit such as a vacuum swing adsorption unit.

[0035] FIG. 2A is a perspective view, and FIG. 2B is a longitudinal sectional view of a top portion of one SC burner embodiment 100 in accordance with the present disclosure. Protective cap 50 and external conduit 10 are all that are viewable in FIG. 2A, protective cap 50 featuring in this embodiment a curvilinear cap inner wall 51 defining a protective cap central flow passage. Protective cap 50 includes a noble metal skin layer or layer 52. As better illustrated in FIG. 2B, cap embodiment 100 comprises a refractory or other high-temperature-resistant body material 54 and noble metal skin 52 over substantially the entire external surface of the refractory body 54 except a lower surface 55. This allows refractory ceramic material or other castable material to be used to pour into a pre-formed skin 52, in one method of making the protective cap. As is evident in FIG. 2B, cap 50 covers and is adjacent most if not all of outer wall 30 and crown 32 of the burner tip.

[0036] In certain embodiments, a high-temperature tape, adhesive, caulk, gasket or other high temperature resistant material, or combination of these, may be applied to the external surfaces of the burner tip where the protective cap is to be positioned adjacent thereof, and/or to the skin surface of the protective cap before installing the cap over the burner tip or portion thereof. Suitable high-temperature caulks include those that are mixtures of ceramic fibers, silica binders, fillers and an organic solvent known under the trade designation KAOWOOL[®] MOLDABLE (available from Northwest Iron Works, LLC, Veneta, Oregon) and comprise (for example) about 55 wt. percent solids formulations comprising (chemical analysis, nominal weight percent basis after firing), 24 wt. percent alumina, 65 wt. percent silica, and 11 wt. percent other ingredients.

[0037] FIGS. 3, 4, and 5A are cross-sectional views of portions of three non-limiting SC burner embodiments of the present disclosure, and FIG. 5B is a plan view of the burner of FIG. 5A. FIG. 3 illustrates burner embodiment 250, featuring a rectangular or "box" shaped protective cap, which may be easier to manufacture than the toroidal embodiment 100. The protective cap of embodiment 250 also features the provision of a landing or extension 53 of skin 52 for positioning of one or more metallic or other material partial or full circumference rings 56. Ring 56 is preferably a single circumferential metallic ring to

allow welding, brazing, or other fitting of ring 56 to landing 53 and to an SCM superstructure (not illustrated).

[0038] FIG. 3 illustrates certain dimensions of protective caps useful in SC burners of the present disclosure, including a height "H" and thicknesses t_1 , t_2 , and t_3 , and a cone angle " α " of inner wall 51 of the protective cap. Height "H", which is the length of the refractory body portion of the protective cap in a direction generally parallel to the burner longitudinal axis A_1 , generally depends on the height of the burner tip being protected, and how much of the burner tip is to be protected. "H" may range from about 0.5 cm to about 20 cm, or from about 1 to about 15 cm, or from about 2 to about 10 cm. Thicknesses t_1 and t_2 may be the same or different, and may each independently range from about 1 mm to about 10 mm, or from about 2 mm to about 7 mm. In certain embodiments thicknesses t_1 and t_2 may be substantially the same. In certain embodiments thickness t_2 may have a greater value than thickness t_1 . In certain embodiments the ratio t_2/t_1 may range from about 1.5:1.0 to about 5:1, or from about 2:1 to about 4:1. Thickness t_3 , which is the thickness of the refractory body of the protective cap in a direction substantially perpendicular to the longitudinal axis of the burner A_1 , may range from about 0.5 cm up to about 20 cm, or from about 1 to about 15 cm, or from about 2 to about 10 cm.

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[0039] Cone angle α may range from a positive value (diverging) as illustrated in FIG. 3 to a negative value (for example converging flow passage). In certain embodiments, it is preferred that cone angle α be positive as illustrated, allowing inner wall 28 of the burner tip to be cooled by flowing oxidant and/or fuel. In certain other embodiments, it may be desired to have cone angle α be negative or converging, still allowing some cooling, but also to allow formation of an increased pressure mixing region, helping to reduce the tendency for molten glass to deposit inside of the burner, or onto surfaces of the burner, which can lead to reduced heat input and/or plugging of the burner. If cone angle α is positive it may range from about 10 to about 80 degrees, or from about 15 to about 75 degrees, or from about 25 to about 70 degrees, and if negative, may have similar ranges.

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[0040] Burner embodiment 270 illustrated in FIG. 4 features a protective cap having curvilinear skin 52 covering a curvilinear refractory body 54. Embodiment 270 also stresses that protective caps within the present disclosure may have one or more holes 62 through skin 52 leading to cavities 60 in refractory body 54. Finally, embodiment 270 emphasizes that in certain embodiments refractory body 54 may comprise more than one

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refractory or other material 64 as a solid core, layer or other composite member. In certain embodiments, solid core 64 may be wholly or partially replaced with a gas such as air. In certain embodiments, core 64 may exist as a plurality of regions 64 dispersed in a matrix refractory material 54.

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[0041] FIGS. 5A and 5B illustrate burner embodiment 300, featuring a protective cap that does not cover the entire burner tip, but includes open regions 70, which may be randomly or non-randomly spaced about the circumference of the cap. In essence embodiments such as illustrated in FIGS. 5A and 5B may be characterized as comprising
10 two or more sub-caps 52 separated by open regions 70. This may be beneficial for easier replacement of sections of the cap, or for use of sections of different materials.

[0042] FIG. 9 is a longitudinal cross-sectional view of a portion of another non-limiting SC burner embodiment 350 of the present disclosure. The cap of embodiment 350 does not
15 have a refractory body, but features a cladding layer or layers 52 over burner tip outer wall 30, a portion of crown 32, and optionally a portion of external conduit 10. Cladding layer may be one or more layers of one or more high-temperature resistant materials, such as ceramic materials, noble metal(s), or combinations thereof (such as as ceramic material supported by a metal grid work). It is theorized that cladding layer 52, which may
20 vary in thickness from about 1 mm to about 1 cm or more (depending on the material used and temperature reduction desired), would dampen out the very short time frame, high spikes in temperature of the burner tip (evidenced by the results of simulations in FIG. 7, upper curve), and that the contact resistance alone between cladding 52 and the burner tip and optionally portions of external conduit 10 would create a beneficial
25 temperature reduction of the burner tip. It is further theorized that smoothing out the temperature spikes that ordinarily occur without a cap or cladding (FIG. 7, upper curve) would significantly reduce thermal fatigue of the burner tip.

[0043] FIGS. 6A and 6B show results of simulations using a Computational Fluid Dynamic
30 (CFD) tool for a prior art burner such as illustrated in FIG. 1 and an identical burner except having a protective cap such as illustrated in FIGS 2A and 2B. For equal amounts and flow velocities of oxidant (oxygen) and fuel (natural gas), the simulation results showed that the case with the protective cap (FIG. 6B) predicted much lower burner tip temperatures than the case without any protective material as shown in FIG. 6A. In fact,
35 with the protective cap, FIG. 6B shows the highest temperature predicted on the burner

tip decreased by almost a factor of 3 and the highest temperature region became the burner tip inner wall where the oxygen flow provided the cooling before combustion.

5 [0044] FIG. 7 shows graphically the thermal cycling of a simulated unprotected burner tip as predicted by CFD (upper curve), and the lack thereof and much lower temperature of the simulated burner having a protective cap (lower curve).

10 [0045] FIG. 8 is a cross-sectional view of an SCM embodiment 550 in accordance with the present disclosure. Embodiment 550 of FIG. 8 comprises a peripheral wall 502 of melter 550, wall 502 having an inlet 504, a batch feed chute 515, and a melter discharge 506 through which molten glass exits the melter. Melter 550 also comprises a roof (not illustrated), a floor 8, a feed end 9, and a discharge end 11.

15 [0046] Melter wall 2 forms an expanding melting zone 514 formed by a first trapezoidal region, and a narrowing melting zone 516 formed by a second trapezoidal region of wall 2. The first trapezoid forming expanding melting zone 514 and the second trapezoid forming narrowing melting zone 516 share a common base in this embodiment, indicated at B, at an intermediate location between the melter inlet 504 and discharge 506. Common base B defines the location of the maximum width, W_M , of melter 550. The
20 primary importance of these melting zones is that no 90-degree corners are present in the melter where there may be stagnation of molten glass flow. While this is preferred, other shaped melters may benefit from use of the burners of the present disclosure, and the present disclosure is not limited to SCMs having shape of embodiment 550.

25 [0047] Melter 550 includes submerged combustion burners 510. In embodiment 550, burners 510 are floor-mounted burners, illustrated in rows substantially perpendicular to the longitudinal axis, A_2 , of melter 550. In certain embodiments, burners 510 are positioned to emit combustion products into molten glass in the melting zones 514, 516 in a fashion so that the gases penetrate the melt generally perpendicularly to the floor. In
30 other embodiments, one or more burners 510 may emit combustion products into the melt at an angle to the floor, where the angle may be more or less than 45 degrees, but in certain embodiments may be 30 degrees, or 40 degrees, or 50 degrees, or 60 degrees, or 70 degrees, or 80 degrees.

35 [0048] Melter apparatus in accordance with the present disclosure may also comprise one or more wall-mounted submerged combustion burners, as indicated at 525 in FIG. 8,

and/or one or more roof-mounted burners (not illustrated). Roof-mounted burners may be useful to pre-heat the melter apparatus melting zones 514, 516, and serve as ignition sources for one or more submerged combustion burners 510. Melter apparatus having only wall-mounted, submerged-combustion burners are also considered within the present disclosure. Roof-mounted burners may be oxy-fuel burners, but as they are only used in certain situations, are more likely to be air/fuel burners. Most often they would be shut-off after pre-heating the melter and/or after starting one or more submerged combustion burners 510. In certain embodiments, if there is a possibility of carryover of batch particles to the exhaust, one or more roof-mounted burners could be used to form a curtain to prevent particulate carryover. In certain embodiments, all submerged combustion burners 510 are oxy/fuel burners (where "oxy" means oxygen, or oxygen-enriched air, as described earlier), but this is not necessarily so in all embodiments; some or all of the submerged combustion burners may be air/fuel burners. Furthermore, heating may be supplemented by electrical heating in certain embodiments, in certain melter zones.

[0049] Optionally, the burner tip crown and inner and outer walls may comprise the same or different corrosion resistant and fatigue resistant material, at least one of the corrosion and/or fatigue resistance being greater than material comprising the external conduit under conditions experienced during submerged combustion melting of glass-forming materials. Applicant's co-pending International Application Number PCT/US13/42153 filed on even date herewith, describes use of corrosion-resistant and/or fatigue resistant materials for the burner tip components connected to a dissimilar (and in certain embodiments, lower cost) material as the burner body, and methods of attachment. More particularly, at least one of the corrosion and/or fatigue resistance of the outer wall of the burner tip is greater than material comprising the external conduit under conditions experienced during submerged combustion melting of glass-forming materials.

[0050] Burner tips and skins of burner protective caps may comprise same or different noble metals or other exotic corrosion and/or fatigue-resistant materials, such as platinum (Pt), ruthenium (Ru), rhodium (Rh), palladium (Pd), silver (Ag), osmium (Os), iridium (Ir), and gold (Au); alloys of two or more noble metals; and alloys of one or more noble metals with a base metal. As described in the above-mentioned '42153 application, in certain embodiments the burner tip may comprise a platinum/rhodium alloy attached to the base metals comprising the burner body using a variety of techniques, such as brazing, flanged fittings, interference fittings, friction welding, threaded fittings, and the like, as further

described herein with regard to specific embodiments. Threaded connections may eliminate the need for 3rd party forgings and expensive welding or brazing processes – considerably improving system delivery time and overall cost. It will be understood, however, that the use of 3rd party forgings, welding, and brazing are not ruled out for
5 burners described herein, and may actually be preferable in certain situations.

[0051] When in alloyed form, alloys of two or more noble metals may have any range of noble metals. For example, alloys of two noble metals may have a range of about 0.01 to about 99.99 percent of a first noble metal and 99.99 to 0.01 percent of a second noble
10 metal. Any and all ranges in between 0 and 99.99 percent first noble metal and 99.99 and 0 percent second noble metal are considered within the present disclosure, including 0 to about 99 percent of first noble metal; 0 to about 98 percent; 0 to about 97 percent; 0 to about 96; 0 to about 95; 0 to about 90; 0 to about 80; 0 to about 75; 0 to about 70; 0 to about 65; 0 to about 60; 0 to about 55; 0 to about 50; 0 to about 45; 0 to about 40; 0 to
15 about 35; 0 to about 30; 0 to about 25; 0 to about 20; 0 to about 19; 0 to about 18; 0 to about 17; 0 to about 16; 0 to about 15; 0 to about 14; 0 to about 13; 0 to about 12; 0 to about 11; 0 to about 10; 0 to about 9; 0 to about 8; 0 to about 7; 0 to about 6; 0 to about 5; 0 to about 4; 0 to about 3; 0 to about 2; 0 to about 1; and 0 to about 0.5 percent of a first noble metal; with the balance comprising a second noble metal, or consisting
20 essentially of a second noble metal (for example with one or more base metals present at no more than about 10 percent, or no more than about 9 percent base metal, or no more than about 8, or about 7, or about 6, or about 5, or about 4, or about 3, or about 2, or no more than about 1 percent base metal).

[0052] In certain noble metal alloy embodiments comprising three or more noble metals, the percentages of each individual noble metal may range from equal amounts of all noble metals in the composition (about 33.33 percent of each), to compositions comprising, or consisting essentially of, 0.01 percent of a first noble metal, 0.01 percent of a second noble metal, and 99.98 percent of a third noble metal. Any and all ranges in
25 between about 33.33 percent of each, and 0.01 percent of a first noble metal, 0.01 percent of a second noble metal, and 99.98 percent of a third noble metal, are considered within the present disclosure.
30

[0053] The choice of a particular material is dictated among other parameters by the chemistry, pressure, and temperature of fuel and oxidant used and type of glass melt to
35 be produced. The skilled artisan, having knowledge of the particular application,

pressures, temperatures, and available materials, will be able design the most cost effective, safe, and operable burners for each particular application without undue experimentation.

5 [0054] The terms "corrosion resistant" and "fatigue resistant" as used herein refer to two different failure mechanisms that may occur simultaneously, and it is theorized that these failure mechanisms may actually influence each other in profound ways. It is preferred that the burner tips with protective caps will have a satisfactory service life of at least 12 months under conditions existing in a continuously operating SCM adjacent to the
10 protective cap, and it is especially preferred that they have a service life greater than 12 months.

[0055] In certain embodiments the crown of the burner tip may include at least one physical convolution sufficient to increase surface area and fatigue resistance of the
15 crown compared to a smooth, half-toroid crown of the same composition, as disclosed in Applicant's co-pending International Application Number PCT/US13/42159 filed on even date herewith. In these embodiments, the protective cap might be adjacent only a portion of the burner tip crown.

20 [0056] Certain embodiments may comprise a burner tip insert shaped substantially the same as but smaller than the burner tip and positioned in an internal space defined by the burner tip, the insert configured so that a cooling fluid may pass between internal surfaces of the burner tip and an external surface of the insert. In these embodiments a first or distal end of the first internal conduit would be attached to the insert.

25 [0057] In certain embodiments, the inner and outer walls of the burner tip body may extend beyond the first end of the third internal conduit, at least partially defining a mixing region for oxidant and fuel.

30 [0058] Conduits of burner bodies and associated components (such as spacers and supports between conduits, but not burner tips and skin of the protective caps) used in SC burners, SCMs and processes of the present disclosure may be comprised of metal, ceramic, ceramic-lined metal, or combination thereof. Suitable metals include carbon steels, stainless steels, for example, but not limited to, 306 and 316 steel, as well as
35 titanium alloys, aluminum alloys, and the like. High-strength materials like C-110 and C-125 metallurgies that are NACE qualified may be employed for burner body components.

(As used herein, "NACE" refers to the corrosion prevention organization formerly known as the National Association of Corrosion Engineers, now operating under the name NACE International, Houston, Texas.) Use of high strength steel and other high strength materials may significantly reduce the conduit wall thickness required, reducing weight of
5 the burners.

[0059] Suitable materials for the glass-contact refractory, which may be present in SC melters and downstream flow channels, and refractory burner blocks (if used), include fused zirconia (ZrO_2), fused cast AZS (alumina-zirconia-silica), rebonded AZS, or fused
10 cast alumina (Al_2O_3). The melter geometry and operating temperature, burner and burner tip geometry, and type of glass to be produced, may dictate the choice of a particular material, among other parameters.

[0060] The term "fluid-cooled" means use of a coolant fluid (heat transfer fluid) to transfer
15 heat away from the burner exterior conduit and burner tip. Heat transfer fluids may be any gaseous, liquid, or some combination of gaseous and liquid compositions that functions or is capable of being modified to function as a heat transfer fluid. Gaseous heat transfer fluids may be selected from air, including ambient air and treated air (for example, air treated to remove moisture), inorganic gases, such as nitrogen, argon, and helium,
20 organic gases such as fluoro-, chloro- and chlorofluorocarbons, including perfluorinated versions, such as tetrafluoromethane, and hexafluoroethane, and tetrafluoroethylene, and the like, and mixtures of inert gases with small portions of non-inert gases, such as hydrogen. Heat transfer liquids may be selected from liquids that may be organic, inorganic, or some combination thereof, for example, salt solutions, glycol solutions, oils
25 and the like. Other possible heat transfer fluids include steam (if cooler than the expected glass melt temperature), carbon dioxide, or mixtures thereof with nitrogen. Heat transfer fluids may be compositions comprising both gas and liquid phases, such as the higher chlorofluorocarbons.

[0061] In certain embodiments of the present disclosure, burner tip 4 may be joined to
30 burner body 6 using flanges. When joined in this way, critical design features are the thickness of the flange, the width of the flange, and the shape of the area surrounding the junction as this location is typically cooled with a coolant fluid and pressure drop needs to be minimized. In addition, when using flanges, careful selection of gasket material is
35 necessary to ensure sealing and the ability to expose the flange to an oxygen or oxygen-enriched environment. In addition, or in certain alternative embodiments, plastically

deformable features may be positioned on one or more of the flange faces to enable joint sealing.

[0062] In other embodiments, brazing compounds and methods may be used to attach burner tip 4 to burner body 6. Brazing allows the joining of dissimilar metals and also allows for repairs to be made by removing the braze material. For these embodiments to be successful, the mating surfaces must be parallel or substantially so, and of sufficient overlap to ensure that the brazing material can properly flow between the portions of the burner tip and burner body being joined. This may be achieved in certain embodiments using a flange at right angles to both the burner tip walls 28, 30, and the conduits forming burner body 6. In other embodiments brazing may be successfully achieved by making the burner tip walls 28, 30 and conduits 14, 10 overlap with sufficient gaps to allow brazing material to enter the gaps.

[0063] Braze compounds, sometimes referred to as braze alloys, to be useful in embodiments of the present disclosure, must have liquidus and solidus temperatures above the highest temperature of the burner tip. The highest temperature of the burner tip will be a temperature equal to the melt temperature existing in the SCM reduced by the flow of coolant through the burner tip, as well as by the flow of combustion gases through the burner tip. The highest temperature of the burner tip during normal operating conditions depends on the type of glass being made, which makes the selection of braze alloy not a simple matter. For Na-Ca-Si soda-lime window glass (Glass 1), typical melt temperature may range from about 1275 °C to about 1330 °C; for Al-Ca-Si E glass having low sodium and zero boron (Glass 2), the melt temperature may range from about 1395 °C to about 1450 °C; for B-Al-Si glass, zero sodium, zero potassium, high Si (Glass 3), the melt temperature may be about 1625 °C; and for B-Al-Ca-Si E glass used for reinforcement fiber (Glass 4), the melt temperature maybe about 1385 °C. This information was taken from Rue, D., *Energy Efficient Glass Melting – The Next Generation Melter*, p. 63, GTI Project Number 20621, March, 2008 (U.S. Dept. of Energy). Based on these temperatures, and assuming a drop in burner tip temperature of 300 °C due to coolant and gas flow through the burner tip without the protective cap, Table 1 lists the possible braze alloys that may be used.

Table 1. Braze Alloys

5

Glass Type	Glass Melt T, (°C)	Possible Braze Alloys ¹	Solidus T, (°C) ²
1	1275 - 1330	Pt Pd Ti Au/Pd (92/8, PALORO (BAU-8)) Ni/Pd (40/60, PALNI) Pd/Co (65/35, PALCO BPD-1) Pd/Ni/Au (34/36/30, PALNIRO 4 (AMS- 4785)) Cu Au	1769 1555 1670 1200 1238 1219 1135 1083 1064
2	1395 - 1450	Pt Pd Ti Au/Pd (92/8, PALORO (BAU-8)) Ni/Pd (40/60, PALNI) Pd/Co (65/35, PALCO BPD-1)	1769 1555 1670 1200 1238 1219
3	1625	Pt Ti	1769 1670
4	1385	Pt Pd Ti Au/Pd (92/8, PALORO (BAU-8)) Ni/Pd (40/60, PALNI) Pd/Co (65/35, PALCO BPD-1) Pd/Ni/Au (34/36/30 PALNIRO 4 (AMS- 4785))	1769 1555 1670 1200 1238 1219 1135

¹ PALORO, PALNI, and PALNIRO are registered trademarks, and PALCO is a trademark of Morgan Technical Ceramics and/or Morgan Advanced Ceramics, Inc.

² From Internet website of Morgan Technical Ceramics and The Morgan Crucible Company plc, England

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[0064] In yet other embodiments, burner tip walls and conduit 14, 10 may be threaded together, in certain embodiments accompanied by a sealant surface of flange upon which sealants, gaskets or O-rings may be present. Threaded joints may be straight or tapered such as NPT. In certain threaded embodiments the sealing surfaces of burner tip walls
5 28, 30 may be malleable enough compared to conduits 14, 10 to deform and form their own seals, without sealants, gaskets, or O-rings.

[0065] In still other embodiments, burner tip walls 28, 30 may be interference or “press” fit to their respective conduit 14, 10 of burner body 6. In these embodiments, the walls
10 and/or conduits are machined to sufficiently close tolerances to enable deformation of one or both surfaces as the two parts are forcefully joined together.

[0066] In yet other embodiments, burner tip walls 28, 30 may be friction welded together. In these embodiments, either the burner tip walls or burner body conduits, or both, may
15 be spun and forced into contact until sufficient temperature is generated by friction to melt a portion of either or both materials, welding walls 28, 30 to conduits 14, 10, respectively. These embodiments may include one or more additional metals serving as an intermediate between walls 28, 30 and conduits 14, 10 to facilitate friction welding.

[0067] The thickness of crown 32 and inner and outer walls 28, 30 in the various
20 embodiments illustrated herein is not critical, especially due to the presence of the protective cap, and need not be the same for every region of the crown and walls. Suitable thicknesses may range from about 0.1 cm to about 1 cm, or larger. Thicker crowns and walls, or thicker regions of crowns and walls, will generally be stronger and
25 exhibit more fatigue resistance, but may be more difficult to install, for example if deformable interference fittings are to be employed.

[0068] In using burners in SCMs of the present disclosure, a cooling fluid is made to flow through first and second annuli in the burner body, while flowing an oxidant or fuel into
30 one or more inlet ports and through the third annulus defined by the second and third internal conduits, while either fuel or oxidant flows through the substantially concentric central third internal conduit. The burner body, burner tip body, and protective cap are configured such that flow of oxidant fuel causes the oxidant to intersect flow of the fuel in a mixing region at least partially defined by the generally central burner tip and burner cap
35 flow passages, combusting at least some of the fuel in the mixing region to form a flame

and combustion products, and directing the flame and/or combustion products into solid and/or partially molten glass forming materials above the mixing region.

[0069] Burner tips and protective caps described herein may be made using a variety of processes, including molding, machining, net-shape cast (or near-net shape cast) using rapid prototype (RP) molds and like processes. The matching or substantially matching burner tip inserts may similarly be RP molded and cast of the same or substantially similar shape, thereby ensuring proper cooling water velocity just under the surface of the burner tip material (inside the crown and inner and outer walls of the burner tips). Net-shape or near-net shape casting methods of making a variety of molds for producing a variety of complex products are summarized in patents assigned to 3D Systems, Inc., Rock Hill, South Carolina, U.S.A., for example U.S. Patent No. 8,285,411.

[0070] In general, central internal conduit 15 may have an inner diameter (ID) ranging from about 1 inch up to about 5 inches (2.5 cm to 13 cm), or from about 2 inches up to about 4 inches (5 cm to 10 cm).

[0071] The total quantities of fuel and oxidant used by burners of the present disclosure may be such that the flow of oxygen may range from about 0.9 to about 1.2 of the theoretical stoichiometric flow of oxygen necessary to obtain the complete combustion of the fuel flow. Another expression of this statement is that the combustion ratio may range from about 0.9 to about 1.2.

[0072] The velocity of the fuel in the various burner embodiments of the present disclosure depends on the burner geometry used, but generally is at least about 15 meters/second (m/s). The upper limit of fuel velocity depends primarily on the desired penetration of flame and/or combustion products into the glass melt and the geometry of the burner, burner tip, and protective cap; if the fuel velocity is too low, the flame temperature may be too low, providing inadequate temperature in the melter, which is not desired, and if the fuel flow is too high, flame and/or combustion products might impinge on a melter wall or roof, or cause carryover of melt into the exhaust, or be wasted, which is also not desired. Similarly, oxidant velocity should be monitored so that flame and/or combustion products do not impinge on an SCM wall or roof, or cause carryover of melt into the exhaust, or be wasted. Oxidant velocities depend on fuel flow rate and fuel velocity, but in general should not exceed about 200 ft/sec at 400 scfh flow rate. The

pressure in mixing region 150 of burners in accordance with the present disclosure should not exceed about 10 psig (170 kPa absolute pressure).

5 [0073] Additionally, certain burner embodiments of this disclosure may also be provided with stabilization of the flame with an auxiliary injection of fuel and/or oxidant gases. For example, a portion of the oxidant may be premixed with fuel as a primary oxidant, usually air, in conduit 15, in addition to a secondary or tertiary oxidant injection in the third annulus.

10 [0074] SC burners and methods of the present disclosure are intended to be used, for example, to replace combustion burners in existing SCMs, and/or to be used as the main source of energy in new SCMs.

15 [0075] Certain SCMs and method embodiments of this disclosure may include fluid-cooled panels such as disclosed in Applicant's co-pending U.S. Patent Application Serial No. 12/817,754, filed June 17, 2010. In certain system and process embodiments, the SCM may include one or more adjustable flame submerged combustion burners comprising one or more oxy-fuel combustion burners, such as described in Applicant's co-pending U.S. Patent Application Serial No. 13/268,028, filed October 7, 2011. In
20 certain systems and processes, the SCM may comprise a melter exit structure designed to minimize impact of mechanical energy, such as described is Applicant's co-pending U.S. Patent Application Serial No. 13/458,211, filed April 27, 2012. In certain systems and processes, the flow channel may comprise a series of sections, and may comprise one or more skimmers and/or impingement (high momentum) burners, such as described in
25 Applicant's co-pending U.S. Patent Application Serial Nos. 13/268,130, filed October 7, 2011, and 13/493,170, filed June 11, 2012. Certain systems and processes of the present disclosure may utilize measurement and control schemes such as described in Applicant's co-pending U.S. Patent Application Serial No. 13/493,219, filed June 11, 2012, and/or feed batch densification systems and methods as described in Applicant's
30 co-pending U.S. Patent Application Serial No. 13/540,704, filed July 3, 2012. Certain SCMs and processes of the present disclosure may utilize devices for delivery of treating compositions such as disclosed in Applicant's co-pending U.S. Patent Application Serial No. 13/633,998, filed October 3, 2012.

35 [0076] Although only a few exemplary embodiments of this disclosure have been described in detail above, those skilled in the art will readily appreciate that many

modifications are possible in the exemplary embodiments without materially departing from the novel teachings and advantages of this disclosure. Accordingly, all such modifications are intended to be included within the scope of this disclosure as defined in the following claims. In the claims, no clauses are intended to be in the means-plus-
5 function format allowed by 35 U.S.C. § 112, paragraph 6 unless “means for” is explicitly recited together with an associated function. “Means for” clauses are intended to cover the structures, materials, and/or acts described herein as performing the recited function and not only structural equivalents, but also equivalent structures.

What is claimed is:

Claim 1. A fluid-cooled combustion burner comprising:

a burner body (6) comprising an external conduit (10) and a first internal conduit (12) substantially concentric therewith, and positioned internal of the external conduit (10), the external conduit (10) comprising a first end, a second end, and a longitudinal bore having a longitudinal axis, the first internal conduit (12) comprising a first end, a second end, and a longitudinal bore having a longitudinal axis, and a second internal conduit (14) substantially concentric with, and positioned internal of the first internal conduit, the second internal conduit (14) comprising a first end, a second end, and a longitudinal bore having a longitudinal axis, the external conduit (10) and first internal conduit (12) forming a first annulus (11) there between for passing a cooling fluid, the first internal conduit (12) and the second internal conduit (14) forming a second annulus (13) there between for passing the cooling fluid, and a third internal conduit (15) configured to form a third annulus between the second (14) and third (15) internal conduits, the burner body comprising fuel and oxidant inlet ports near the second ends of the conduits; and

a burner tip (4) defined by an inner wall (28) and an outer wall (30) connected via a crown (32), the outer wall (30) removably fixed to the first end of the external conduit (10) via an outer connection, and the inner wall (28) removably fixed to the first end of the second internal conduit (14) via an inner connection, the burner tip (4) comprising a generally central burner tip flow passage configured to pass a combustible mixture therethrough, the generally central burner tip flow passage defined by the inner wall (28); and

wherein the burner comprises a protective cap (50) positioned adjacent at least a circumferential and radial portion of the burner tip body and defining generally central protective cap flow passage downstream of the generally central burner tip flow passage configured to pass the combustible mixture therethrough, the generally central protective cap flow passage defined by a cap inner wall (28).

Claim 2. The fluid-cooled combustion burner of claim 1 wherein the protective cap comprises materials and thickness sufficient to lower the maximum temperature of an unprotected burner tip body by at least 200°C.

Claim 3. The fluid-cooled combustion burner of claim 1 wherein the cap is positioned over the entire circumference of the burner tip crown and outer wall.

Claim 4. The fluid-cooled combustion burner of claim 1 wherein the cap is positioned over the entire burner tip crown and outer wall.

5 Claim 5. The fluid-cooled combustion burner of claim 1 wherein the cap comprises a refractory body having an outer surface and at least one noble metal layer adjacent at least a portion of the outer surface.

10 Claim 6. The fluid-cooled combustion burner of claim 5 wherein the refractory is selected from the group consisting of alumina, silicon nitride, and combinations thereof, and the noble metal is selected from the group consisting of platinum, rhodium, and alloys thereof.

15 Claim 7. The fluid-cooled combustion burner of claim 4 wherein the burner tip crown and a top portion of the protective cap each have substantially concentric half-toroid shapes.

Claim 8. The fluid-cooled combustion burner of claim 4 wherein the protective cap has an external rectangular shape.

20 Claim 9. The fluid-cooled combustion burner of claim 5 wherein the noble metal layer extends over at least a portion of a lower end of the refractory body and substantially perpendicular to the longitudinal axis of the external conduit, forming a space sufficient to land one or more metallic members suitable for securing the protective cap to a melter structure.

25 Claim 10. The fluid-cooled combustion burner of claim 1 wherein the generally central protective cap flow passage expands from inlet to outlet in a curvilinear configuration with a tangent angle α ranging from about 20 to about 80 degrees.

30 Claim 11. The fluid-cooled combustion burner of claim 5 wherein the noble metal layer has a thickness ranging from about 5 mm to about 25 mm, and the refractory body has a length in the direction parallel to the longitudinal axis of the external conduit ranging from about 1 cm to about 10 cm, and a thickness in the direction perpendicular to the longitudinal axis of the external conduit ranging from about 1 cm to about 5 cm.

35 Claim 12. The fluid-cooled combustion burner of claim 5 wherein the refractory body comprises two or more layers of refractory, the layers being the same or different.

Claim 13. The fluid-cooled combustion burner of claim 5 comprising one or more cavities in the protective cap.

- 5 Claim 14. The fluid-cooled combustion burner of claim 1 wherein the protective cap comprises two or more sub-caps separated by regions of no cap.

Claim 15. The fluid-cooled combustion burner of claim 1 wherein:

- 10 the first, second, and third internal conduits and the external conduit comprises the same or different materials selected from the group consisting of carbon steel, stainless steel, and titanium; and

- 15 the inner and outer walls and crown comprise the same or different corrosion resistant and fatigue resistant material, at least one of the corrosion and/or fatigue resistance being greater than material comprising the external conduit under conditions experienced during submerged combustion melting of glass-forming materials, the corrosion resistant and fatigue resistant material selected from the group consisting of noble metals, alloys of two or more noble metals, alloys of one or more base metals with one or more noble metals, copper, copper alloys, and combinations thereof.

- 20 Claim 16. A submerged combustion melter comprising:

 a floor, a roof, and a sidewall structure connecting the floor and roof defining an internal space, at least a portion of the internal space comprising a melting zone; and

- one or more combustion burners in either the floor, the roof, the sidewall structure, or any two or more of these, producing combustion gases and configured to emit the combustion gases from a position under a level of, and positioned to transfer heat to and produce, a turbulent molten mass of glass in the melting zone;
- 25 at least one of the combustion burners being a fluid-cooled combustion burner of claim 1.

- 30 Claim 17. A submerged combustion melter comprising:

 a floor, a roof, and a sidewall structure connecting the floor and roof defining an internal space, at least a portion of the internal space comprising a melting zone; and

- one or more combustion burners in either the floor, the roof, the sidewall structure, or any two or more of these, producing combustion gases and configured to emit the combustion gases from a position under a level of, and positioned to transfer heat to and produce, a turbulent molten mass of glass in the melting zone;
- 35

at least one of the combustion burners being a fluid-cooled combustion burner of claim 5.

Claim 18. A submerged combustion melter comprising:

- 5 a floor, a roof, and a sidewall structure connecting the floor and roof defining an internal space, at least a portion of the internal space comprising a melting zone; and
one or more combustion burners in either the floor, the roof, the sidewall structure, or any two or more of these, producing combustion gases and configured to emit the combustion gases from a position under a level of, and positioned to transfer heat to and
10 produce, a turbulent molten mass of glass in the melting zone;
at least one of the combustion burners being a fluid-cooled combustion burner of claim 6.

Claim 19. A submerged combustion melter comprising:

- 15 a floor, a roof, and a sidewall structure connecting the floor and roof defining an internal space, at least a portion of the internal space comprising a melting zone; and
one or more combustion burners in either the floor, the roof, the sidewall structure, or any two or more of these, producing combustion gases and configured to emit the combustion gases from a position under a level of, and positioned to transfer heat to and
20 produce, a turbulent molten mass of glass in the melting zone;
at least one of the combustion burners being a fluid-cooled combustion burner of claim 7.

Claim 20. A method of producing molten glass comprising feeding glass-forming materials to the submerged combustion melter of claim 16, feeding an oxidant and a fuel to the burner, combusting the fuel and oxidant, and melting the glass-forming materials to produce molten glass.

Claim 21. A method of producing molten glass comprising feeding glass-forming materials to the submerged combustion melter of claim 17, feeding an oxidant and a fuel to the burner, combusting the fuel and oxidant, and melting the glass-forming materials to produce molten glass.

Claim 22. A method of producing molten glass comprising feeding glass-forming materials to the submerged combustion melter of claim 18, feeding an oxidant and a fuel

to the burner, combusting the fuel and oxidant, and melting the glass-forming materials to produce molten glass.

Claim 23. A method of producing molten glass comprising feeding glass-forming materials to the submerged combustion melter of claim 19, feeding an oxidant and a fuel to the burner, combusting the fuel and oxidant, and melting the glass-forming materials to produce molten glass.

Claim 24. The method of claim 20 comprising:

flowing an oxidant into the one or more oxidant inlet ports and through the third annulus;

flowing a fuel into the one or more fuel inlet ports in the third internal conduit, the burner body and burner tip body configured such that flow of oxidant out of the third annulus and flow of fuel out of the third internal conduit causes the oxidant to intersect flow of the fuel in a mixing region at least partially defined by the generally central burner tip flow passage and the generally central protective cap flow passage;

combusting at least some of the fuel in the mixing region to form a flame and combustion products; and

directing the flame and combustion products into solid and/or partially molten glass forming materials above the mixing region.

Claim 25. The method of claim 24 wherein the oxidant is an oxygen stream comprising at least 90 mole percent oxygen.

Claim 26. The method of claim 20 comprising:

flowing a fuel into the one or more fuel inlet ports and through the third annulus;

flowing an oxidant into the one or more oxidant inlet ports and through the third internal conduit, the burner body and burner tip body configured such that flow of oxidant out of the oxidant conduit and flow of fuel out of the third annulus causes the oxidant to intersect flow of the fuel in a mixing region at least partially defined by the generally central burner tip flow passage and the generally central protective cap flow passage;

combusting at least some of the fuel in the mixing region to form a flame and combustion products; and

directing the flame and combustion products into solid and/or partially molten glass forming materials above the mixing region.

Claim 27. The method of claim 26 wherein the oxidant is an oxygen stream comprising at least 90 mole percent oxygen.

Claim 28. A fluid-cooled combustion burner comprising:

a burner body (6) comprising an external conduit (10) and a first internal conduit (12) substantially concentric therewith, and positioned internal of the external conduit (10), the external conduit (10) comprising a first end, a second end, and a longitudinal bore having a longitudinal axis, the first internal conduit (12) comprising a first end, a second end, and a longitudinal bore having a longitudinal axis, and a second internal conduit (14) substantially concentric with, and positioned internal of the first internal conduit, the second internal conduit (14) comprising a first end, a second end, and a longitudinal bore having a longitudinal axis, the external conduit (10) and first internal conduit (12) forming a first annulus (11) there between for passing a cooling fluid, the first internal conduit (12) and the second internal conduit (14) forming a second annulus (13) there between for passing the cooling fluid, and a third internal conduit (15) configured to form a third annulus between the second (14) and third (15) internal conduits, the burner body comprising fuel and oxidant inlet ports near the second ends of the conduits; and

5 a burner tip (4) defined by an inner wall (28) and an outer wall (30) connected via a crown (32), the outer wall (30) removably fixed to the first end of the external conduit (10) via an outer connection, and the inner wall (28) removably fixed to the first end of the second internal conduit (14) via an inner connection, the burner tip (4) comprising a generally central burner tip flow passage configured to pass a combustible mixture therethrough, the generally central burner tip flow passage defined by the inner wall (28);
10 and

wherein the burner comprises a protective cladding layer or layers (52) positioned adjacent at least a circumferential and radial portion of the burner tip body.

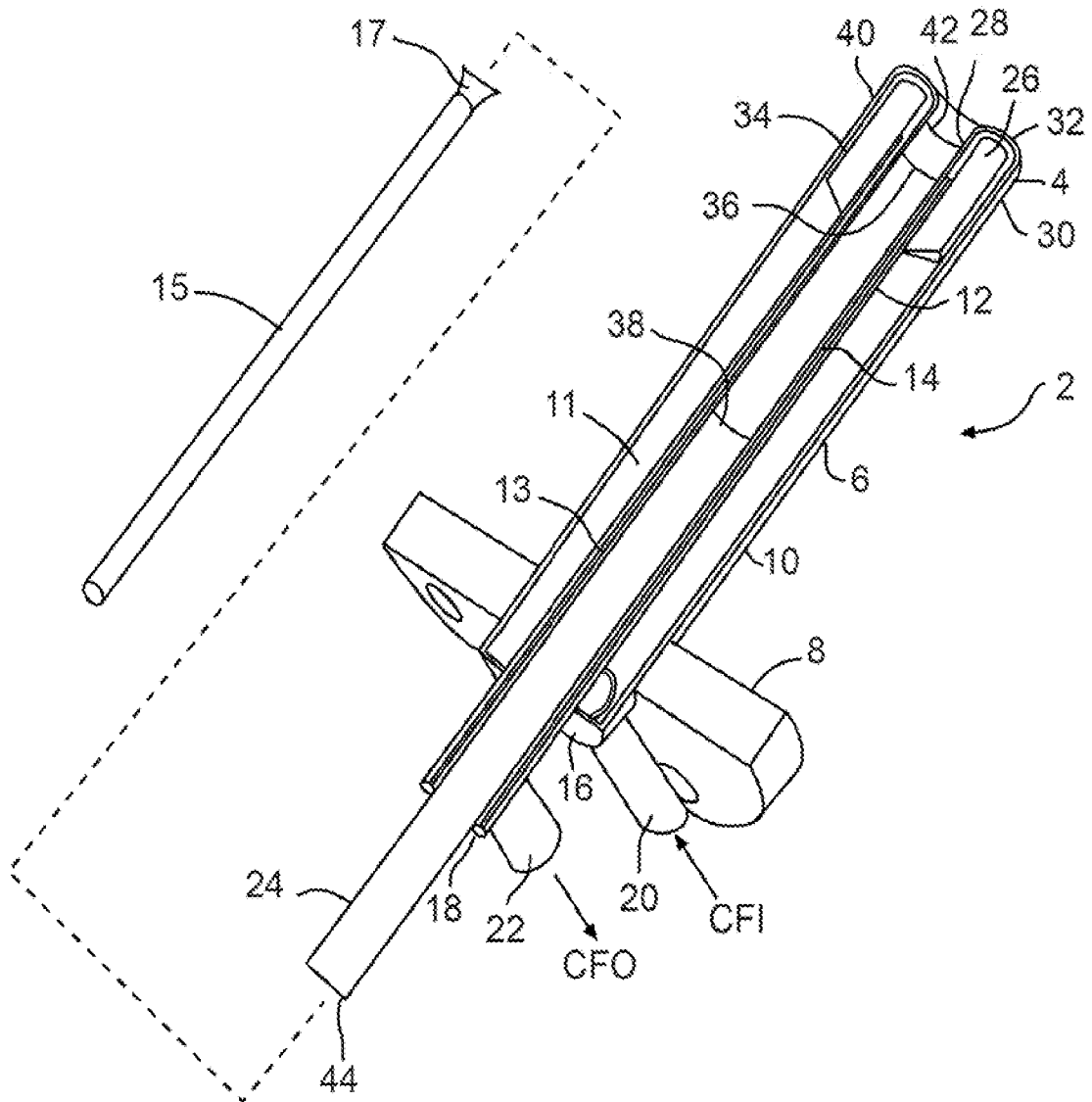


FIG. 1
(Prior Art)

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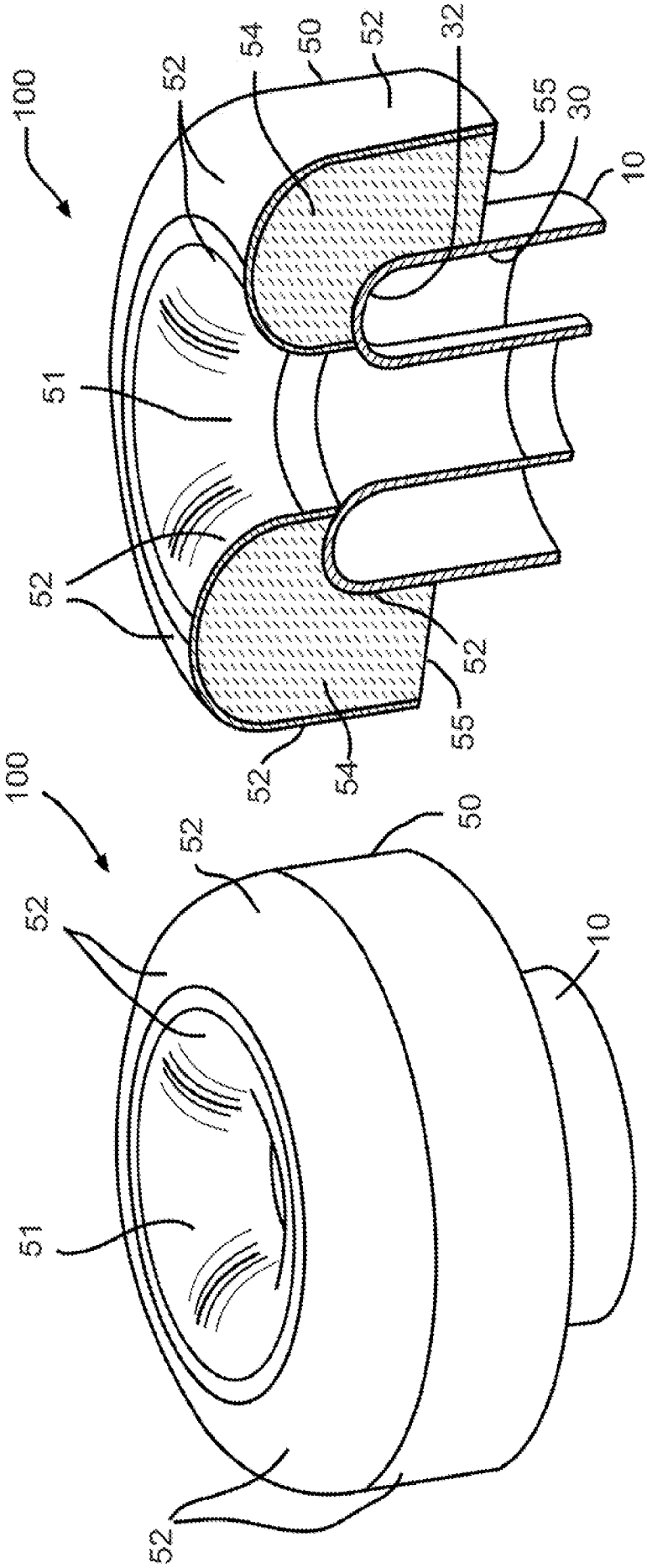
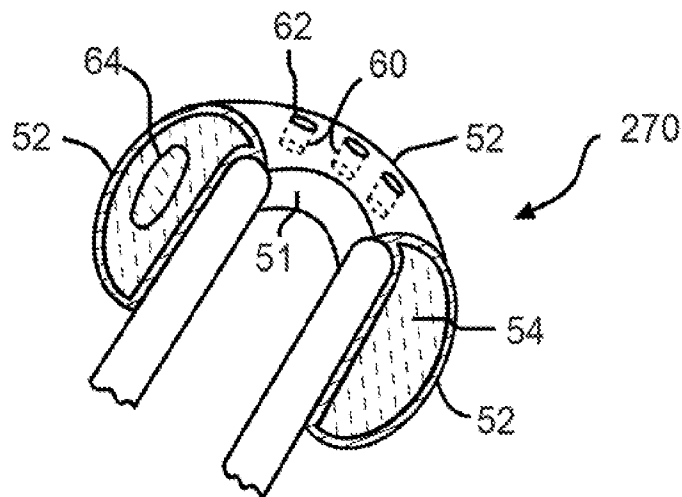
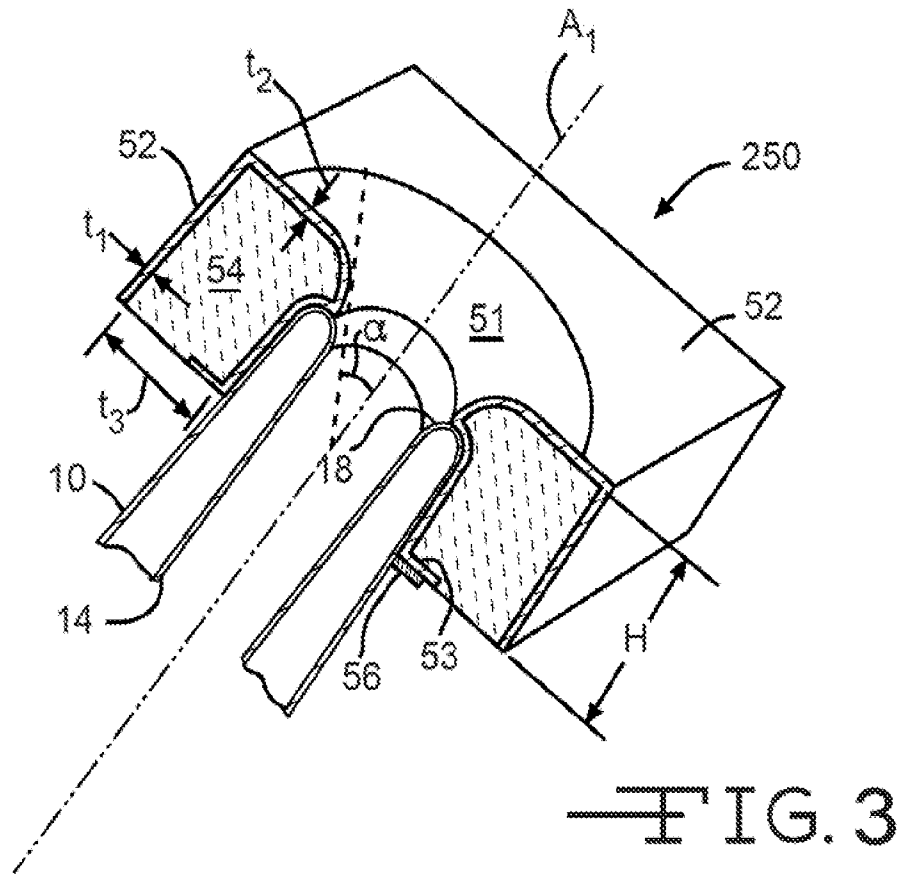


FIG. 2B

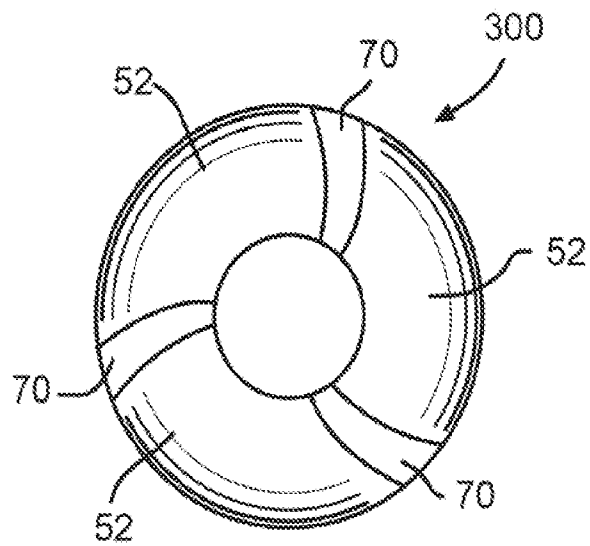
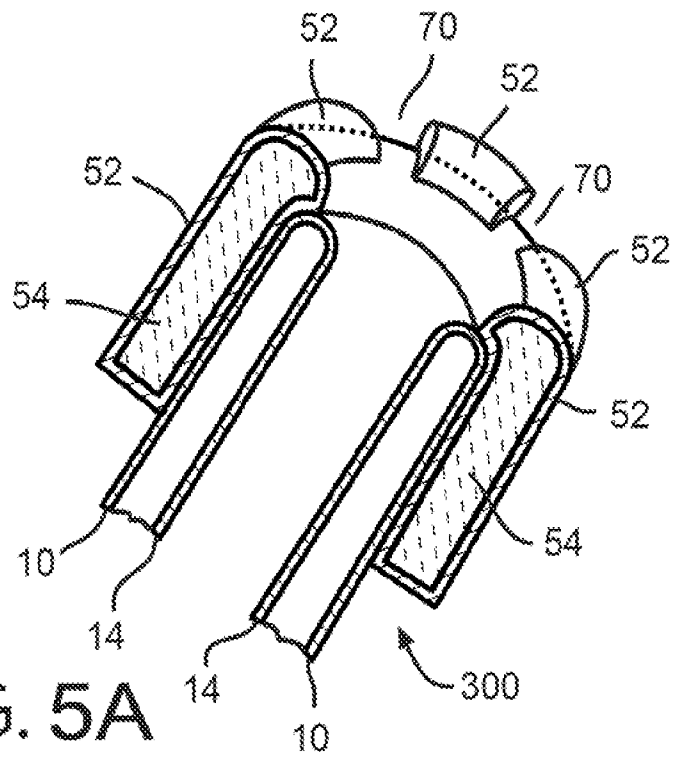
FIG. 2A

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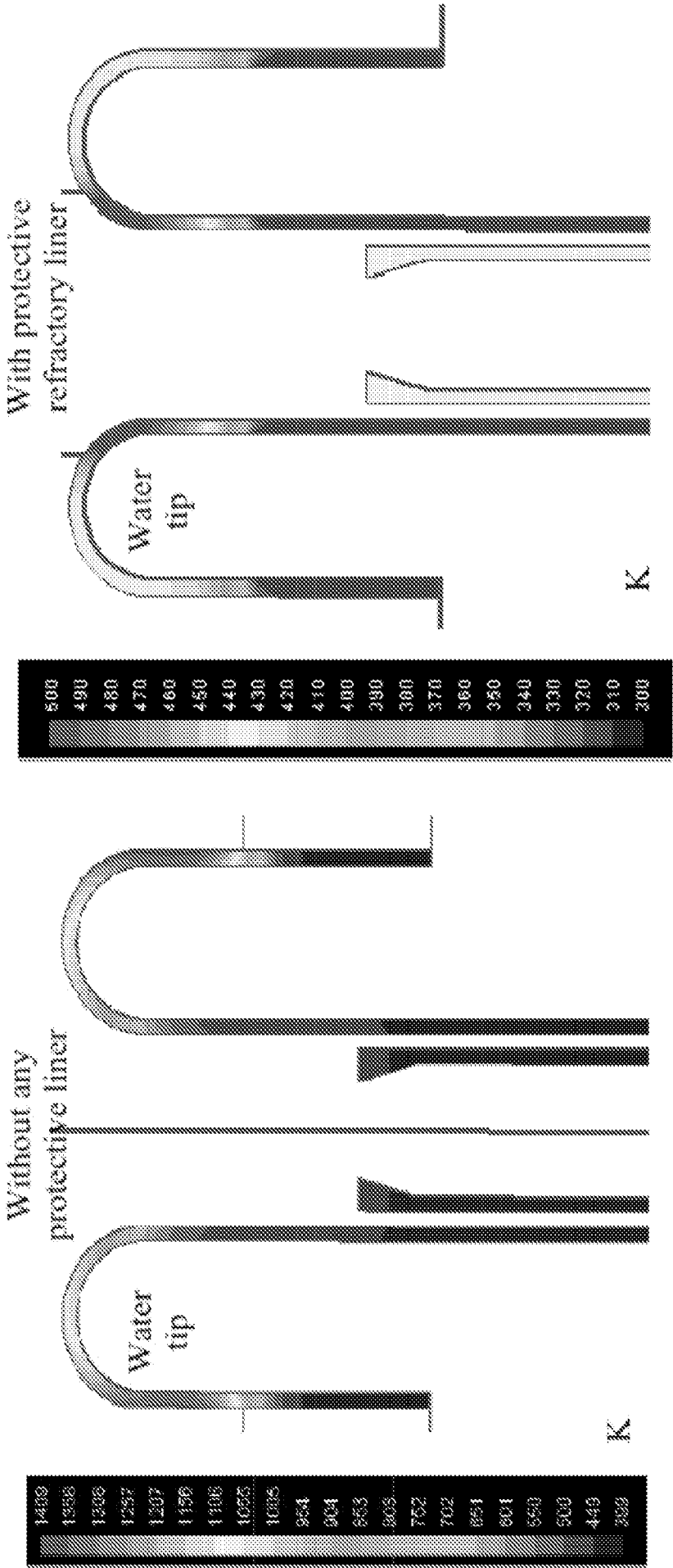


FIG. 6B

FIG. 6A
(Prior Art)

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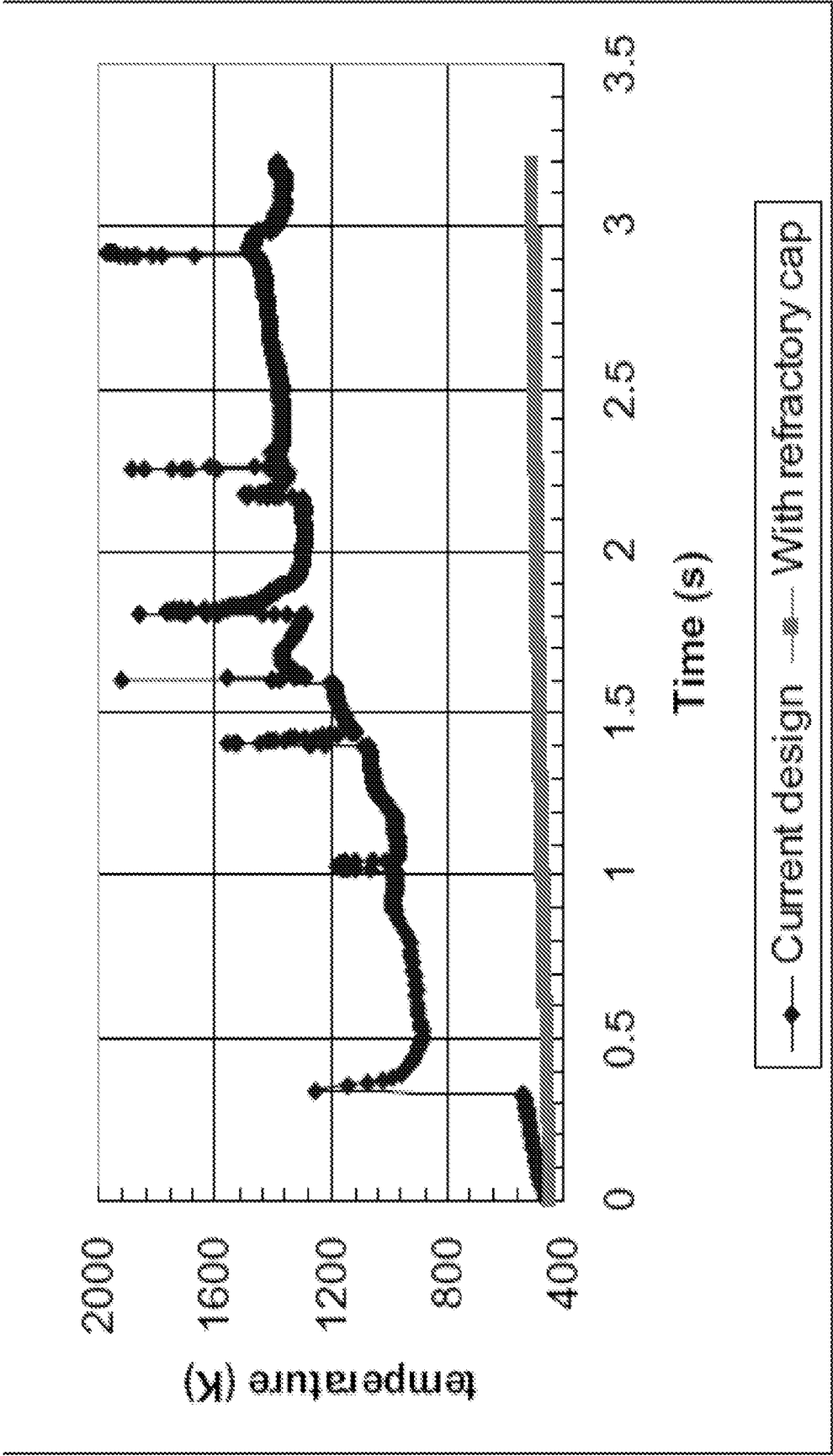


FIG. 7

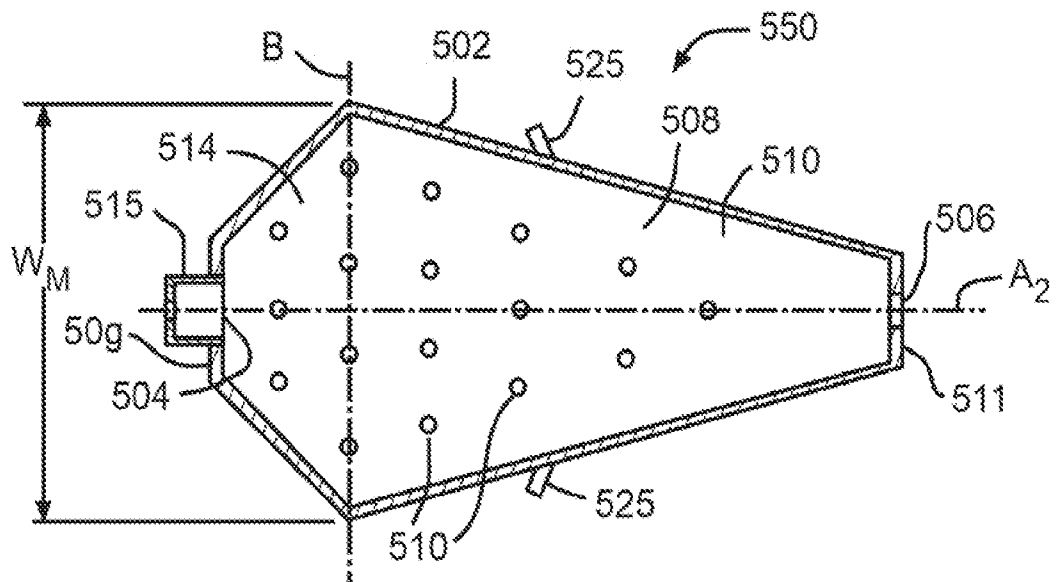


FIG. 8

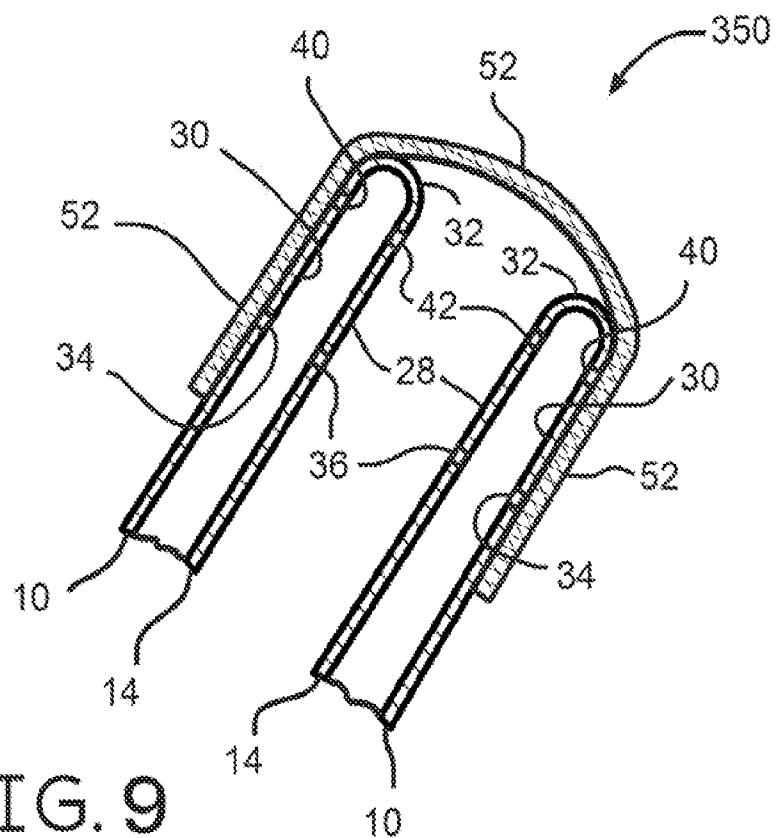


FIG. 9

INTERNATIONAL SEARCH REPORT

International application No
PCT/US2013/042254

A. CLASSIFICATION OF SUBJECT MATTER INV. C03B5/167 C03B5/235 F23D14/78 F27D99/00 ADD.		
According to International Patent Classification (IPC) or to both national classification and IPC		
B. FIELDS SEARCHED Minimum documentation searched (classification system followed by classification symbols) C03B F23D F27D C05B		
Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched		
Electronic data base consulted during the international search (name of data base and, where practicable, search terms used) EPO-Internal, WPI Data		
C. DOCUMENTS CONSIDERED TO BE RELEVANT		
Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y A	US 2005/236747 A1 (RUE DAVID M [US] ET AL) 27 October 2005 (2005-10-27) paragraphs [0028], [0030]; figures	1-4, 16, 20, 26-28 5-15, 17-19, 21-25
Y A	----- DE 10 2008 006572 A1 (SIEMENS AG [DE]) 30 July 2009 (2009-07-30) paragraph [0007]; figures	1-4, 16, 20, 26-28 5-15, 17-19, 21-25
A	----- JP S61 99017 A (TOKYO GAS CO LTD) 17 May 1986 (1986-05-17) the whole document	1-28
A	----- US 3 563 683 A (HESS FREDERIC O) 16 February 1971 (1971-02-16) figures	1-28

☐ Further documents are listed in the continuation of Box C. ☒ See patent family annex.		
* Special categories of cited documents :		
"A" document defining the general state of the art which is not considered to be of particular relevance "E" earlier application or patent but published on or after the international filing date "L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified) "O" document referring to an oral disclosure, use, exhibition or other means "P" document published prior to the international filing date but later than the priority date claimed "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention "X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone "Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art "&" document member of the same patent family		
Date of the actual completion of the international search 8 October 2013	Date of mailing of the international search report 17/10/2013	
Name and mailing address of the ISA/ European Patent Office, P.B. 5818 Patentlaan 2 NL - 2280 HV Rijswijk Tel. (+31-70) 340-2040, Fax: (+31-70) 340-3016	Authorized officer Haegeman, Marc	

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/US2013/042254

Patent document cited in search report	Publication date	Patent family member(s)	Publication date
US 2005236747	A1	27-10-2005	NONE
DE 102008006572	A1	30-07-2009	DE 102008006572 A1 30-07-2009
		WO 2009095144 A2	06-08-2009
JP S6199017	A	17-05-1986	NONE
US 3563683	A	16-02-1971	NONE