



- (51) International Patent Classification:
E04C 2/24 (2006.01) *E04C 2/22* (2006.01)
- (21) International Application Number:
PCT/US2014/072522
- (22) International Filing Date:
29 December 2014 (29.12.2014)
- (25) Filing Language: English
- (26) Publication Language: English
- (30) Priority Data:
14/143,338 30 December 2013 (30.12.2013) US
14/143,421 30 December 2013 (30.12.2013) US
14/583,897 29 December 2014 (29.12.2014) US
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- (81) Designated States (*unless otherwise indicated, for every kind of national protection available*): AE, AG, AL, AM, AO, AT, AU, AZ, BA, BB, BG, BH, BN, BR, BW, BY, BZ, CA, CH, CL, CN, CO, CR, CU, CZ, DE, DK, DM, DO, DZ, EC, EE, EG, ES, FI, GB, GD, GE, GH, GM, GT, HN, HR, HU, ID, IL, IN, IR, IS, JP, KE, KG, KN, KP, KR, KZ, LA, LC, LK, LR, LS, LU, LY, MA, MD, ME, MG, MK, MN, MW, MX, MY, MZ, NA, NG, NI, NO, NZ, OM, PA, PE, PG, PH, PL, PT, QA, RO, RS, RU, RW, SA, SC, SD, SE, SG, SK, SL, SM, ST, SV, SY, TH, TJ, TM, TN, TR, TT, TZ, UA, UG, US, UZ, VC, VN, ZA, ZM, ZW.
- (84) Designated States (*unless otherwise indicated, for every kind of regional protection available*): ARIPO (BW, GH, GM, KE, LR, LS, MW, MZ, NA, RW, SD, SL, ST, SZ, TZ, UG, ZM, ZW), Eurasian (AM, AZ, BY, KG, KZ, RU,

[Continued on next page]

(54) Title: BUILDING BOARDS WITH INCREASED SURFACE STRENGTH

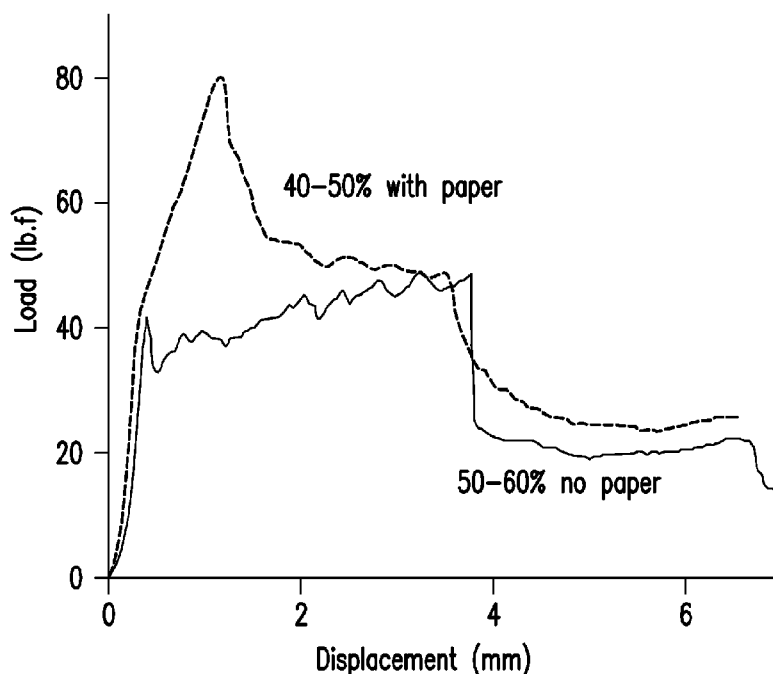


FIG. 1

(57) Abstract: Disclosed is a building board construction with increased surface strength. More specifically, increased nail pull strength is achieved via the application of an external surface coating. The surface coating is ideally applied to a paper faced gypsum building board. In one possible embodiment, the coating is formed from a water soluble polymer.



TJ, TM), European (AL, AT, BE, BG, CH, CY, CZ, DE, DK, EE, ES, FI, FR, GB, GR, HR, HU, IE, IS, IT, LT, LU, LV, MC, MK, MT, NL, NO, PL, PT, RO, RS, SE, SI, SK, SM, TR), OAPI (BF, BJ, CF, CG, CI, CM, GA, GN, GQ, GW, KM, ML, MR, NE, SN, TD, TG).

Published:

— *without international search report and to be republished upon receipt of that report (Rule 48.2(g))*

BUILDING BOARDS WITH INCREASED SURFACE STRENGTH

CROSS REFERENCE TO RELATED APPLICATIONS

[0001] This application claims priority to and is a continuation-in-part of U.S. Application Ser. No. 14/143,338, filed Dec. 30, 2013, and entitled “Building Boards with Increased Surface Strength” and to U.S. Application Ser. No. 14/143,421, filed Dec. 30, 2013, and entitled “Non-Uniform Coatings for Building Boards,” the contents of which are fully incorporated herein for all purposes.

TECHNICAL FIELD

[0002] This disclosure relates to building boards with increased surface strength. More particularly, the present invention relates to coatings and coating methods that provide for enhanced nail pull strength.

BACKGROUND OF THE INVENTION

[0003] Gypsum board is one of the most widely used and versatile building materials in the world. The basic construction for gypsum building boards has remained unchanged for quite some time. This construction includes a core of calcium sulfate dihydrate that is sandwiched between opposing paper sheets. Efforts have been made over the years to increase the strength of gypsum boards. In particular, efforts have been made to increase nail pull strength. Nail pull strength is a standard ASTM measurement. Higher nail pull strength ensures that boards can be securely fastened to associated framing members. To date, efforts to increase nail pull strength have focused on core materials, additives, and core density. The drawback with such efforts is that they require larger quantities of material and increased board weight to reinforce the core.

[0004] An example of gypsum board with increased strength is illustrated in U.S. Pub. 2004/0154264 to Colbert. This publication discloses a coated gypsum board having a facing sheet. A coating is disposed on at least a portion of the facing sheet and at least a portion of the coating penetrates into the facing sheet and/or the gypsum core. In an additional embodiment, the gypsum board further comprises a backing sheet on the second side of the gypsum core. In one aspect, the coating may penetrate into the

gypsum core to a substantially uniform depth across an area of the gypsum board. A gypsum board with such a coating exhibits a nail pull value of greater than 80 pounds.

[0005] U.S. Pub. 2005/0233657 to Grove discloses a gypsum or foam facer that is formed by the direct in-line or off-line coating of a pre-impregnated, fibrous network matting with a secondary binder system. The pre-impregnated fibrous network is preferably formed of a randomly oriented wet use chop strand fiber material impregnated with a modified urea-formaldehyde binder system. The secondary binder system preferably consists of low glass transition acrylic or styrene-butadiene-rubber resin filled predominantly with fillers combined with a plate like reinforcement or fibrous reinforcement.

[0006] Although the above referenced inventions achieve their own individual objectives, all suffer from common drawbacks. Namely, none of the background art addresses the use of coatings or coating techniques that increase nail pull strength while minimizing board weight. The building boards of the present disclosure are designed to overcome these and other deficiencies present in the background art.

SUMMARY OF THE INVENTION

[0007] The building boards of the present disclosure provide an advantage by exhibiting increased surface strength without appreciable increases to overall board weight.

[0008] Another advantage is realized by increasing the nail pull strength of a building board via the application of a surface coating.

[0009] An advantage is also recognized by selecting a surface coating that complements the tensile strength of the underlying paper face.

[0010] Still yet another advantage is achieved by increasing nail pull strength via the application of certain water soluble or dispersible polymer coatings.

[0011] A further advantage is accomplished by applying polymer coatings after board production via wet coating techniques.

[0012] A further advantage is the discovery that beneficial nail pull strengths can be achieved with coating weights below those found in the prior art.

[0013] Another possible advantage is attained by providing a coating that is applied in a non-uniform manner across the surface of the board.

[0014] A further advantage is realized by applying thicker surface coatings in locations that typically encounter greater loads.

[0015] Yet another advantage is recognized by reducing both board weight and cost via the targeted application of surface coatings.

[0016] Another advantage is realized by providing a building board with increased nail pull strength that can be made inexpensively.

[0017] Various embodiments of the invention may have none, some, or all of these advantages. Other technical advantages of the present invention will be readily apparent to one skilled in the art.

BRIEF DESCRIPTION OF THE DRAWINGS

[0018] For a more complete understanding of the present disclosure and its advantages, reference is now made to the following descriptions, taken in conjunction with the accompanying drawings, in which:

[0019] FIG. 1 is a graph of load versus displacement for a paper faced board and a non-paper faced board.

[0020] FIG. 2 is a is a graph of load versus displacement for a paper faced board indicating the mode of failure in each region of the measurement

[0021] FIG. 3 is an SEM cross section of a paper faced board after peak load in a nail pull measurement.

[0022] FIG. 4 is a chart indicating the normal variation of nail pull strength across the width of a composite building board.

[0023] FIG. 5 is a chart plotting nail pull index versus dry weight coverage as applied via an airless spray coating technique.

[0024] FIG. 6 is a chart plotting nail pull resistance versus board weight for both airless and air atomized spray coating techniques.

[0025] FIG. 7 is a chart plotting nail pull versus distance from the edge of the board.

DETAILED DESCRIPTION OF THE DRAWINGS

[0026] The present disclosure relates to increasing the surface strength of building board via the application of external coatings. The coating is ideally applied to a paper faced building board to increase nail pull strength. In one possible embodiment, the coating is formed from a water soluble polymer. In yet another embodiment, the coating is applied in a non-uniform manner to account for varying loads across the surface of the board. The various details of the present disclosure, and the manner in which they interrelate, are described in greater detail hereinafter.

[0027] In a preferred but non-limiting example, the building board is a gypsum based building board. The general construction of gypsum board is well known and includes a core of calcium sulfate dihydrate that is sandwiched between opposing paper sheets. This core is initially deposited in the form of a slurry of calcium sulfate hemihydrate ($\text{CaSO}_4 \cdot \frac{1}{2}\text{H}_2\text{O}$) and water. Once the slurry is deposited, it is rehydrated to form gypsum.

[0028] It is also known in the art to use various additives within the gypsum core. One such additive is starch. Starch can be added prior to rehydration. Starch functions as a binder within set gypsum and yields boards with higher compressive and flexural strength. It also strengthens the edges of the resulting board and improves paper bond to the core. The gypsum core contemplated herein may optionally include additives such as starch.

[0029] The gypsum core of the present disclosure may also include a plurality of internal voids to reduce the overall weight of the board. It is known in the art to form voids within the interior of gypsum board as a means for reducing the board weight. One technique is described in U.S. Pat. 6,706,128 to Sethuraman. Sethuraman '128 discloses a method for adding air bubbles of different relative stabilities, whereby the air bubbles do not rupture before the slurry sets sufficiently to prevent the slurry from filling the void spaces left behind by ruptured bubbles. The result is a gypsum board with internal voids and with reduced weight. Other suitable techniques for void formation will be apparent to those of ordinary skill in the art.

[0030] In accordance with one embodiment, a coating is applied to one of the paper liners. Although the coating can be applied to either, or both, of the liners, it is preferred that the coating is applied to the liner forming the decorative outer face of the building board. Any of a variety of wet coating techniques (e.g., spray coating, slot die coating, roll coating, or dip coating) can be used. As explained below, the coating is designed to increase nail pull strength without appreciably increasing the weight of the building board. The coating may form the decorative external face of the board. In this regard, various known matting agents may also be added to reduce gloss of the coating and otherwise make it more aesthetically pleasing. However, the coating need not form the external face of the resulting board. Rather, the coating may be used as a primer or pre-primer to ensure adequate adhesion to subsequently applied coatings.

[0031] FIG. 1 plots load (in pounds force) versus nail displacement in millimeters. The top most line shows that 40-50% of the nail pull strength is attributed to the paper liner. This reflects the increased nail pull strength achieved by providing a paper face. The lower line reflects that in the absence of a paper liner 50-60% of the nail pull strength is attributed to the core materials. Overall this chart demonstrates that paper facing contributes more significantly to the nail pull peak load than previously realized. The present disclosure capitalizes on this finding by increasing nail pull strength via the application of surface coatings.

[0032] Surface strength is further increased by selecting a coating material that complements the tensile properties of underlying paper liner. The best coating materials are not the strongest materials but those which have the highest strength at the elongation required to match the failure of the paper. By utilizing such coatings, the destruction of the liner is delayed for as long as possible while the board is under load. It will also preferably to select coatings that best adhere to the paper and serve to reinforce the cellulose fibers within the paper itself. The preferred coating materials are listed below in Table 1.

[0033] It is also known that peak nail pull strength occurs immediately prior to the destruction or tearing of the paper face. This is demonstrated in FIG. 2, which plots load versus displacement in a nail pull test. This plot contains descriptions of the failure

processes occurring during the test based on a series of SEM cross sections taken at various points during the test. FIG. 2 illustrates that the failure mechanism can be broken down into four segments. In the first segment, the load causes microcracks to develop within the board. Next, under increasing loads, the microcracks propagate and internal voids are compressed. In the third segment, there is a compression of the core and a shear failure of the liner. Finally, at the peak load, the paper tears.

[0034] FIG. 3 contains a cross sectional scanning electron microscope image of a composite building board immediately after peak load in a nail pull test. It can be seen on the right side of the image that the paper has just failed at the paper surface in tensile strain. This indicates that a coating which can reinforce the surface of the paper or better distribute the tensile load can serve to significantly increase the peak nail pull strength.

[0035] Table 1 contains various polymers used as coatings on building boards and the effect on board nail pull strength. The percentage nail pull (NP) increase is measured relative to an uncoated board.

Table 1				
Number	Coating	Method	Coverage (g/sf)	% NP increase
1	Nanocellulose (Strong & Hard)	Blade	2	1
2	Titebond Wood glue (Hard)	Blade	3.5	-1
3	Bostic Wood Glue (Flexible)	Blade	3.5	15
4	PVOH 24-203 (Low Mn, 88% H)	Blade	1.5	5
5	PVOH 09-523 (High Mn, 88% H)	Blade	1.5	13
6	PVOH 03-325 (High Mn, 98% H)	Blade	1.5	10
7	PVOH 09-523 (High Mn, 88% H)	Blade	2	14
8	PVOH 09-523 (High Mn, 88% H)	Blade	1	7
9	PVOH 09-523 (High Mn, 88% H)	Blade	0.5	5
10	VAE 10A (Tg = 5)	Blade	2	13
11	VAE EU (Tg = 10)	Blade	2	16
12	VAE 909 (Tg = 15)	Blade	2	18
13	VAE 909 (Tg = 15)	Blade	2	21

Table 1				
Number	Coating	Method	Coverage (g/sf)	% NP Increase
14	VAE 909 (T _g = 15)	Mayer Rod	4	19
15	VAE 909 (T _g = 15)	Mayer Rod	2	19
16	VAE 909 (T _g = 15)	Mayer Rod	1	21
17	VAE 909 IR Annealed	Mayer Rod	2	9
18	VAE 909 IR Annealed	Mayer Rod	1	6
19	VAE 10A IR Annealed	Mayer Rod	1	10
20	VAE (T _g = 28)	Mayer Rod	2	0
21	SBR 246 (T _g = 15)	Mayer Rod	4	14

Some illustrative examples are listed below.

[0036] Comparing the nail pull enhancement of coatings Numbers 1, 2, and 3 in Table 1 above indicates that strength alone is not sufficient for significant nail pull enhancement. Nanocellulose is an extremely high strength material that is effective at paper strengthening when applied as a coating. While the tensile strength of the material is high, however, the elongation at break is quite low and thus the material does not add to nail pull strength. This is because the coating fails before the paper in the nail pull test and the peak load in the nail pull test comes at the point of paper failure. Similarly, comparing the Bostic and Titebond wood adhesives indicates that the tougher, more flexible adhesive provides a significant enhancement to nail pull. On the other hand, the strong, hard, and brittle Titebond has no significant effect.

[0037] If there is a large coat weight of a very hard material, the nail pull can be increased, but at high cost. When hard epoxy resins were tested the nail pull strength could be increased significantly, but the peak load was entirely being derived from the strength of the coating and thus a large coat weight was needed to achieve the result. In the case of the very thin, ductile coatings, the coating ideally fails at the same time as the paper and serves to increase the strength of the paper itself as they are too thin to provide the strength on their own.

[0038] From poly vinyl alcohol (PVOH) coatings Numbers 4-9 in Table 1, several conclusions can be reached. For one, the high molecular weight material is significantly stronger than the low molecular weight material and thus increases the nail pull strength more (presumably they have a similar degree of ductility/elongation). Secondly, the percent hydrolysis does not seem to have a major impact. Finally, it was shown that the effect can occur on even very low coat weights of ~ 1 g/ft².

[0039] Low viscosity vinyl acetate ethylene ("VAE") copolymer coatings are designed to penetrate into paper and increase the toughness of paper. They are strong and flexible coatings which can be either cross linked or not cross linked. When cast and dried in air (film Numbers 10-16 in Table 1), the strength increases with glass transition temperature ("T_g" measured in degrees Celsius). This implies the low T_g material is actually a bit too soft. After IR cross-linking (film Numbers 17-19 in Table 1), however, the low T_g film is a bit stronger than the high T_g film. This implies that the trade-off between strength and ductility can be tuned either by the polymer T_g or by the degree of cross linking in the VAE system. Based on the nail pull data versus coverage, there seems to be little effect of film thickness on the nail pull enhancement.

[0040] From Table 1, the preferred coating polymers are the high molecular weight poly vinyl alcohol (numbers 5-9), the vinyl acetate ethylene with T_g = 15 (numbers 12-15), and the styrene butadiene copolymer (number 21). It is also beneficial to provide polymer coatings with a tensile modulus above 500 psi and an elongation at break of greater than 500% at room temperature. The coating may also have a viscosity of between 20 to 2000 centipoise. VAE based coatings are preferably less than 100 microns thick. In the preferred embodiment, the VAE coatings are between 20-30 microns thick as applied to the surface of the board. For PVA based coatings, 10 microns is preferred. Coating thicknesses greater than 1 g/ft² are also preferred with thicknesses of approximately 1.5 g/ft² being most preferred.

[0041] It is also preferred to apply the selected coating to the surface of the paper in an uneven or non-uniform manner. Ideally, the coating is thicker in those areas that are likely to encounter the greatest surface loads. In other words, the coating coverage is greater in those areas with the lowest nail pull strength. FIG. 4 contains a plot of the

nail pull strength of an uncoated composite building board across the width of the board. The plotted line shows that the nail pull strength is weakest in the area around the center of the board. Likewise, the edges of the board demonstrate the greatest degree of nail pull strength. In accordance with the invention, the coatings described above can be applied in greater amounts along the center line of the board and in lesser amounts along the edges. In some embodiments, the anticipated nail pull strength may dictate that no coatings be applied in select areas. The objective of this targeted application is to effectively smooth out the plotted line in FIG. 4 so as to achieve a more uniform nail pull strength across the entire board surface. Other plots with varying shapes, beyond that of FIG. 4, could similarly be generated based upon varying board geometry, core materials, and/or intended uses. Surface coating thicknesses would be varied depending upon the anticipated nail pull strength variance across the board surface.

Polymer Coating Formulations

[0042] In addition to the above referenced polymer coatings, the present inventors also tested a number polymer formulations. These formulations broadly included a polymer as a major component in addition to a silica and a defoamer. Various coating techniques were also tested. Table 2 lists formulation 909 #17/02, which consists primarily of an emulsion polymer sold by Celanese Corporation of Dallas, Texas under the trademark Dur-o-Set®. In particular, this formulation consists of approximately 89.9% of Dur-o-Set 909 (as a percentage of total solids). Dur-o-Set 909 is a cross linking polymer. Namely, the polymer cross-links with itself when heated. Dur-o-Set 909 works well because the cross-linking does not result in brittleness, which is detrimental to nail pull strength. This formulation further includes water and silica. In the exemplary formulation, the formulation includes approximately 9.9% of an Acematt® HK400 untreated fine-grained precipitated silica from Evonik Industries AG. A blue dye was included for testing purposes so that the distribution of the coating upon the board could be more readily observed. In practice, the dye would be replaced by defoamer, such as the Foamaster® 111 brand defoamer from BASF Corporation is utilized. Table 2 lists also lists the components on a total weight basis and solid weight basis (in grams). Approximately 25.0% of the formulation of Table 2 included solids.

Table 2 909 #17/02			
909 #17/02	Weight (g)	Solids (g)	Total solids (%)
Water	131.7	0	0.0
Dur-o-set 909	112.5	56.3	89.9
HK400 silica	6.2	6.2	9.9
Blue dye	0.1	0.1	0.2
Total	250.6	62.6	100.0

The second formulation, 405 #17/02, is listed in Table 3 and is the same in most respects as the 909 #17/02 formulation. However, the Dur-o-Set 909 polymer is replaced with EcoVAE 405, which is a vinyl acetate/ethylene emulsion that is similarly sold by Celanese Corporation. However, EcoVAE 405 is a non-cross linking polymer. EcoVAE 405 is desirable because it creates a ductile polymer that complements the strength of the underlying paper and increases nail pull strength. Approximately 27.2% of the formulation of Table 3 included solids.

Table 3 405 #17/02			
405 #17/02	Weight (g)	Solids (g)	Total solids (%)
Water	131.7	0	0.0
EcoVAE 405	112.5	61.9	90.8
HK400 silica	6.2	6.2	9.1
Blue dye	0.1	0.1	0.1
Total	250.6	68.2	100.0

[0043] Table 4 lists the results of applying both coating formulations to a gypsum board and testing for nail pull improvement. In each case the coating was applied via a draw down coating technique via the use of a Meyer rod. The thickness of the wet coating along with the corresponding board weight are also listed. Nail pull improvement is listed as nail pull index improvement (NPI). NPI is computed in accordance with the following equation: $NPI = NP/Wt \times 0.05$, where NP is average nail pull resistance in pounds force and Wt is the weight of the board in lbs/MSF.

Table 4			
Formulation	Wet thickness (μm)	Board weight (lbs/ MSF)	Nail pull index improvement (%)
909 #17/02	40	1407	8.7
	60	1415	9.2
	80	1409	10.6
	100	1381	8.5
405 #17/02	40	1388	3.6
	60	1395	6.5
	80	1401	7.1
	100	1403	11.0

[0044] Tables 5-6 illustrate the 909 #20/02 coating and the 405 #20/02 coatings. These coatings generally correspond to the coating formulations noted above in Tables 2-3. The 909 #20/02 formulation included 24.9% total solids. The 405 #20/02 formulation included 27.1% total solids. In each instance, the coating was applied to the board using an airless spray coating technique. This resulted in much higher coating weights.

Table 5			
909 #20/02	Weight (g)	Solids (g)	Total solids (%)
Water	5268.6	0	0.0
Dur-o-set 909	4465	2232.5	89.9
HK400 silica	248.1	248.1	10.0
Blue dye	4.0	4.0	0.2
Total	9985.7	2484.6	100.0

Table 6			
405 #20/02	Weight (g)	Solids (g)	Total solids (%)
Water	5268.6	0	0.0
EcoVAE 405	4465	2455.8	90.7
HK400 silica	248.1	248.1	9.2
Blue dye	4.0	4.0	0.1
Total	9985.7	2707.9	100.0

[0045] Table 7 shows the 909 #20/02 and 405 #20/02 formulations applied via an airless spray coating alternatively using low and high pressure settings. In each case

the resulting dry coverage (in grams per square foot) was 2.1 g/ft² or less. The resulting normalized nail pull index (NPI) ranged from a high of 11.4 to a low of 5.2.

Table 7 Airless Spray Coatings				
Formulation	Pressure setting	Actual dry coverage (g ft ⁻²)	Board weight (lbs/ MSF)	Nail pull index improvement (%)
909 #20/02	Low	0.7	1374	5.7
	High	0.8	1373	5.4
	Low	0.9	1386	6.2
	High	1.1	1389	8.5
	Low	1.8	1399	11.4
	High	1.7	1404	10.4
	Low	2.1	1413	10.8
	High	2.0	1385	10.1
405 #20/02	Low	0.9	1382	5.2
	High	0.7	1377	6.7
	Low	1.0	1383	7.9
	High	1.1	1393	8.5
	Low	1.8	1395	10.0
	High	1.4	1401	9.7
	Low	2.0	1392	8.6
	High	2.3	1402	9.6

[0046] Air atomized spray coatings were also investigated. The results of this investigation are listed below in Tables 8-11. Table 8 sets forth a coating formulation including water, Dur-o-set 909, HK400 Silica, and a Foamaster ® 111 brand defoamer from BASF Corporation. A small amount of a Surfynol 104PG50 surfactant was also included. The total solids was approximately 25%.

Table 8			
909 #15/08	Weight (g)	Solids (g)	Total solids (%)
Water	2875.0	0	0.0
Dur-o-set 909	2425.0	1212.5	89.2
HK400 silica	135.9	135.9	10.0
Foamaster 111	9.9	9.9	0.7
Surfynol 104PG50	0.9	0.9	0.1
Total	2061.5	721.5	100.0

[0047] A formulation including a latex binder was also tested as noted in Table 9. The specific latex binder employed was the latex binder (DL 490NA from Styron).

Table 9			
SBR #03/09	Weight (g)	Solids (g)	Total solids (%)
Water	2875.0	0	0.0
Latex DL 490NA	2425.0	1115.5	88.4
HK400 silica	135.9	135.9	10.8
Foamaster 111	9.9	9.9	0.8
Surfynol 104PG50	0.9	0.9	0.1
Total	2061.5	721.5	100.0

[0048] The results from the two coating, each applied via an air atomized spray coating, are listed below. This table lists the pressure of the air atomized spray coating apparatus as well as the resulting dry coverage of the board. Normalized nail pull is also listed.

Table 10				
Air Atomized Spray Coatings				
Formulation	Atomizing air pressure (bar)	Actual dry coverage (g/ft²)	Board weight (lb/MSF)	Nail pull index improvement (%)
909 #15/08	1.2	1.6	1399	8.0
	1.5	2.1	1398	8.6
	2.0	2.1	1397	9.6
SBR #03/09	1.2	1.4	1375	9.6
	2	1.5	1378	8.3
	2	2.4	1374	10.1

[0049] FIG. 5 plots the results of the 909 #20/02 and 405 #20/02 formulations as applied via an airless spray coating technique. The figure plots nail pull index relative to actual dry coverage of the board. It was determined that lower atomizing air pressures worked better as they left a sufficient amount of the board uncoated and thereby permitted entrained water vapor to escape through the surface of the board during drying. Coatings applied via higher pressures resulted in less desirable, finer spray patterns and often resulted in too much of the surface being coated. The present inventors have discovered that leaving approximately 20% of the board face uncoated

yields sufficient permeation. In the preferred embodiment, between 10% and 20% of the board surface is uncoated. Nail pull index improvements of 10% or greater were achieved. FIG. 6 plots nail pull resistance versus board weight for the Dur-o-Set 909 and EcoVAE 405 formulations. Both airless sprays and air atomized spraying techniques were employed. Again, significant improvements in nail pull strength were realized.

[0050] In one particular test of the 909 #15/08 formulation, the coating was applied with an airless spray coater mounted in-line at a gypsum wallboard factory with approximately a 30 psi pressure. The coating was applied to the gypsum board having an uncoated weight of 1440 lb/MSF (pounds per 1000 square feet). The resulting coated weight of the board was 1448 lb/MSF. The increase in nail pull index was between 8-10%. Thus, the 909 #15/08 formulation can increase nail pull strength by as much as about 10% while contributing very little to board weight. FIG. 7 illustrates nail pull variation across the surface of the production boards with and without the coating.

[0051] Table 11 includes data relating to the air atomized coating of a Styron Latex DL 490NA Styrene-butadiene polymer. Table 12 includes data relating to the air atomized coating with the Dur-o-Set 909. In each case, atomizing air pressures of 2 bar would prove problematic in a factory setting as they would fail to allow sufficient permeation. Air pressures of around 1.2 bars were considered ideal as they provided a sufficiently coarse spray pattern.

Table 11			
Air Atomized Styron Latex DL 490NA SBR			
Air Pressure (bar)	Dry Coverage g/ft²	Board Weight lb/MSF	Nail Pull Index % increase
Control 1	-	1376	-
1.2	1.4	1375	9.6
2.0	1.5	1378	8.3
2.0	2.4	1374	10.1

Table 12 Air Atomized Dur-o-Set 909 VAE			
Air Pressure (bar)	Dry Coverage g/ft ²	Board Weight lb/MSF	Nail Pull Index % increase
Control 5	-	1397	-
1.2	1.6	1399	8.0
		1394	11.0
1.5	2.1	1395	11.4
		1398	8.6
2.0	2.1	1397	9.6
		1388	8.2

[0052] Although this disclosure has been described in terms of certain embodiments and generally associated methods, alterations and permutations of these embodiments and methods will be apparent to those skilled in the art. Accordingly, the above description of example embodiments does not define or constrain this disclosure. Other changes, substitutions, and alterations are also possible without departing from the spirit and scope of this disclosure.

WHAT IS CLAIMED IS:

1. A composite building board with enhanced nail pull strength, the composite building board comprising:

first and second liners, the first liner having an exterior face forming a decorative outer face of the building board;

a set plaster core positioned between and bonded with the first and second liners, the set plaster core formed from a cementitious slurry of predominantly calcium sulfate hemi-hydrate, the set plaster core being formed with a plurality of internal voids, the internal voids functioning to decrease the overall weight of the building board;

a polymer based coating applied to the decorative outer face of the building board wherein the coating comprises less than 10 grams per square foot of polymer.

2. The composite building board as described in claim 1 wherein the coating comprises less than 2 grams per square foot of polymer and the nail pull strength is greater than 10% higher than the uncoated building board.

3. The composite building board as described in claim 2 wherein the coating polymer comprises a synthetic polymer.

4. The composite building board as described in claim 2 wherein the coating polymer comprises a polymer selected from acrylics and acrylic copolymers, vinyl acetate polymers and copolymers, styrene-butadiene polymers and copolymers, or polyvinyl alcohols.

5. The composite building board of claim 2 wherein the coating polymer comprises one of the following:

a copolymer containing vinyl acetate and ethylene;

a copolymer containing styrene and butadiene; or

a poly vinyl alcohol.

6. The composite building board of claim 5 wherein the coating is less than 100 microns thick.

7. The building board as described in claim 3 wherein the coating polymer has a glass transition temperature below 30 degrees Celsius.

8. The building board as described in claim 3 wherein the coating polymer has a glass transition temperature above 5 degrees Celsius and below 25 degrees Celsius.

9. The building board as described in claim 1 wherein the coating polymer comprises one of the following:

- a copolymer containing vinyl acetate and ethylene;
- a copolymer containing styrene and butadiene;
- or a poly vinyl alcohol.

10. The composite building board of claim 9 wherein the coating is less than 100 microns thick.

11. The composite building board of claim 3 wherein the coating is less than 100 microns thick.

12. The building board as described in claim 11 wherein the coating is less than 50 microns thick.

13. The composite building board of claim 3 wherein the coating polymer has a tensile modulus above 500 psi and an elongation at break of greater than 500% at room temperature.

14. The building board as described in claim 13 wherein the coating polymer has an elongation at break of between approximately 500% and 10,000%.

15. The building board as described in claim 14 wherein the coating polymer has a tensile modulus between approximately 500psi and 10,000psi.

16. The building board as described in claim 15 wherein the coating polymer further comprises at least one of the following:

- a copolymer containing vinyl acetate and ethylene;
- a copolymer containing styrene and butadiene;
- or a poly vinyl alcohol.

17. The building board as described in claim 16 wherein the coating is less than 100 microns thick.

18. The building board as described in claim 2 wherein the coating is an aqueous solution.

19. The building board as described in claim 2 wherein the coating is an aqueous dispersion.

20. The building board as described in claim 19 wherein the coating has a percent solids between 10% and 60%.

21. The building board as described in claim 20 wherein the coating has a viscosity between 25 and 2000 centipoise.

22. The building board as described in claim 21 wherein the coating is applied by spray coating.

23. The building board as described in claim 22 wherein the coating polymer comprises one of the following:

- a copolymer containing vinyl acetate and ethylene;

a copolymer containing styrene and butadiene;
or a poly vinyl alcohol.

24. The building board as described in claim 23 wherein the coating is less than 100 microns thick.

25. The building board as described in claim 2 wherein the coating is not uniform across the width of the board.

26. The building board as described in claim 25 wherein the coating is more than 20% thicker in the center of the board than at the edges.

27. The building board as described in claim 26 wherein the coating polymer comprises one of the following:

a copolymer containing vinyl acetate and ethylene;
a copolymer containing styrene and butadiene;
or a poly vinyl alcohol.

28. The building board as described in claim 27 wherein the coating is less than 100 microns thick.

29. A composite building board with enhanced nail pull strength, the composite building board comprising:

an exterior face forming a decorative outer face of the building board;
a set plaster core positioned beneath the exterior face, the set plaster core formed from a cementitious slurry of predominantly calcium sulfate hemi-hydrate;
a polymer based coating applied to the decorative outer face of the building board wherein the coating comprises less than 10 grams per square foot of polymer.

30. The composite building board as described in claim 1 wherein the first and second liners are formed from paper.

31. A composite building board with enhanced nail pull strength, the composite building board comprising:

an exterior face;

a set plaster core positioned beneath the exterior face, the set plaster core formed from a cementitious slurry of predominantly calcium sulfate hemi-hydrate,

a polymer based coating applied to the exterior face of the building board in a non-uniform manner.

32. The composite building board as described in claim 31 wherein the composite building board includes a center line and opposing lateral edges and wherein the polymer based coating is thicker along the center line.

33. The composite building board as described in claim 31 wherein the composite building board includes a center line and opposing lateral edges and wherein the polymer based coating is thinner along the opposing lateral edges.

34. The composite building board as described in claim 31 wherein the polymer coating includes thicker and thinner areas and wherein the thicker areas comprises less than 10 grams per square foot of polymer coating.

35. The composite building board as described in claim 31 wherein the set plaster core is formed with a plurality of internal voids.

36. The composite building board as described in claim 31 wherein the exterior face is formed from paper.

37. A composite building board with enhanced nail pull strength, the composite building board comprising:

first and second liners, the first liner having an exterior face forming a decorative outer face of the building board;

a set plaster core positioned between and bonded with the first and second liners, the set plaster core formed from a cementitious slurry of predominantly calcium sulfate hemi-hydrate, the set plaster core being formed with a plurality of internal voids, the internal voids functioning to decrease the overall weight of the building board;

a polymer based coating applied to the decorative outer face of the building board, the polymer based coating being applied in an uneven manner across the outer face.

38. The composite building board as described in claim 37 wherein the coating comprises less than 10 grams per square foot of polymer.

39. The composite building board as described in claim 37 wherein the coating polymer comprises a synthetic polymer.

40. The composite building board as described in claim 37 wherein the composite building board includes a center line and opposing lateral edges and wherein the polymer based coating is thicker along the center line.

41. The composite building board as described in claim 37 wherein the composite building board includes a center line and opposing lateral edges and wherein the polymer based coating is thinner along the opposing lateral edges.

42. The composite building board as described in claim 37 wherein the first and second liners are formed from paper.

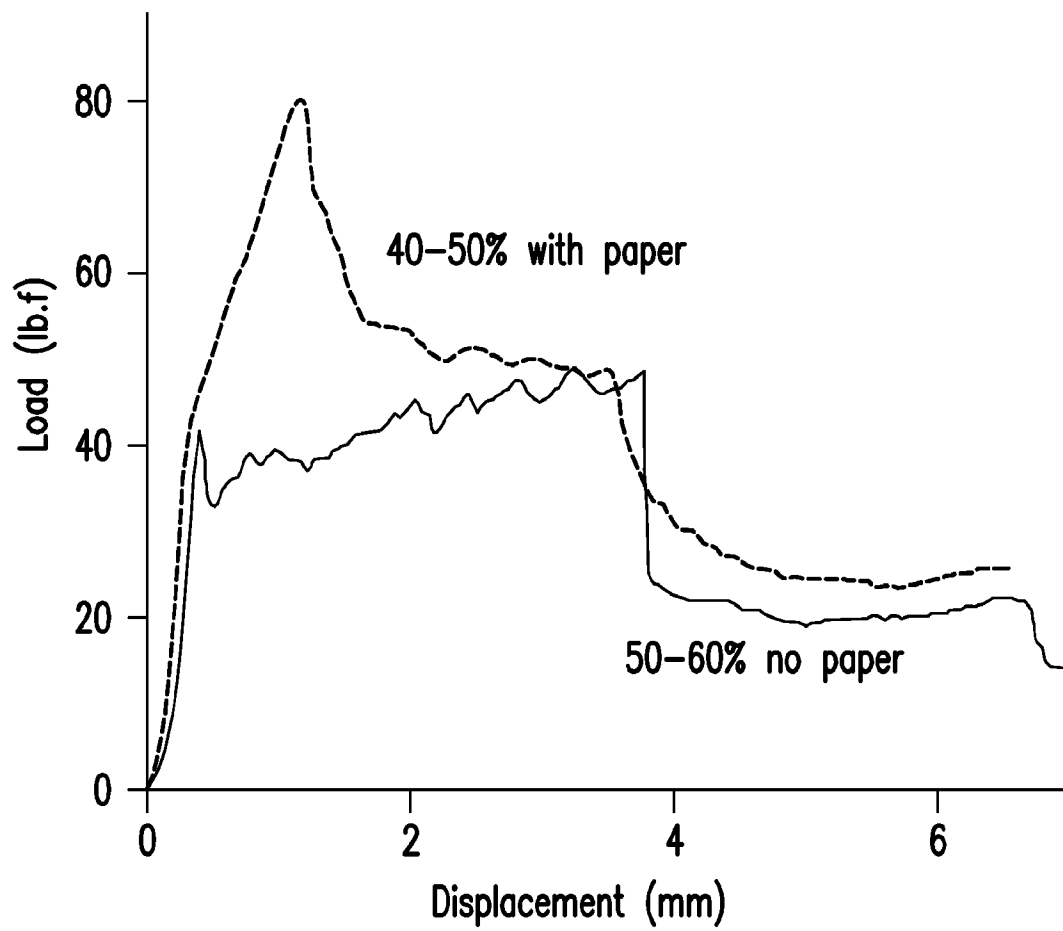
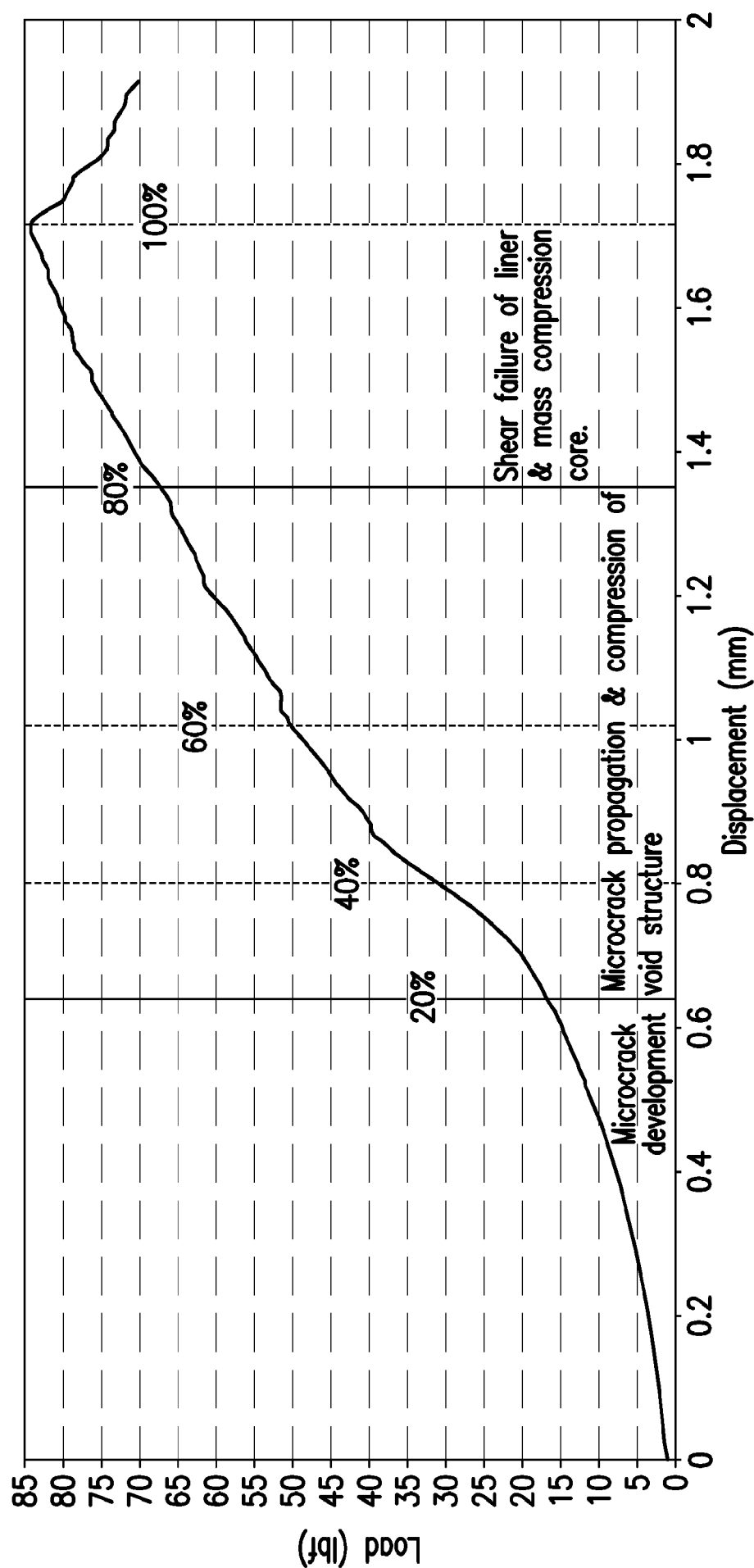


FIG. 1



FAILURE MECHANISM OF NAIL PULL

FIG. 2

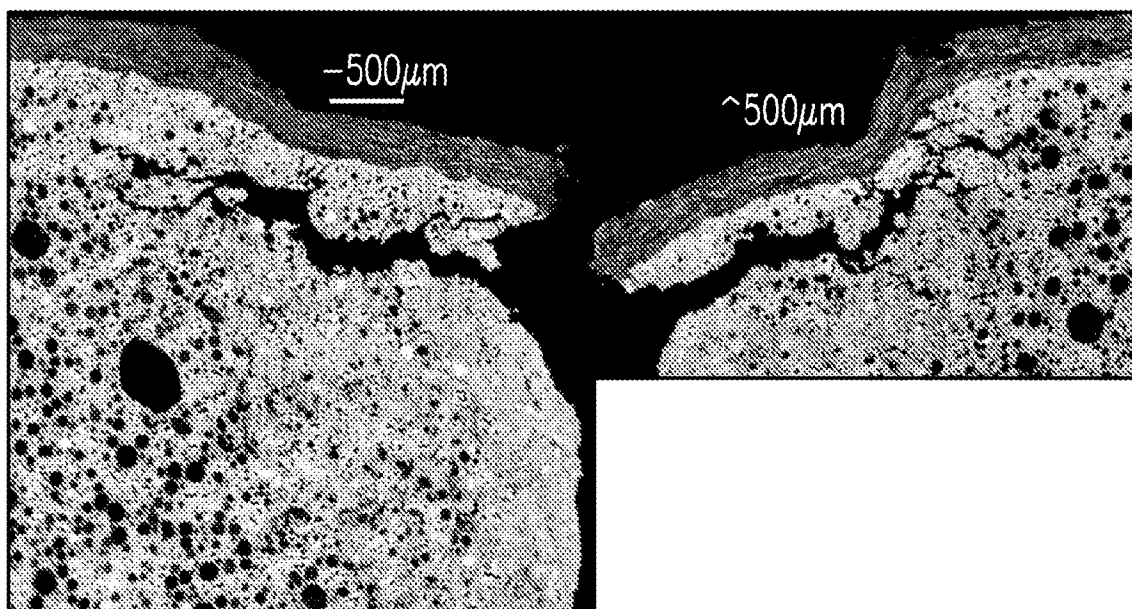


FIG. 3

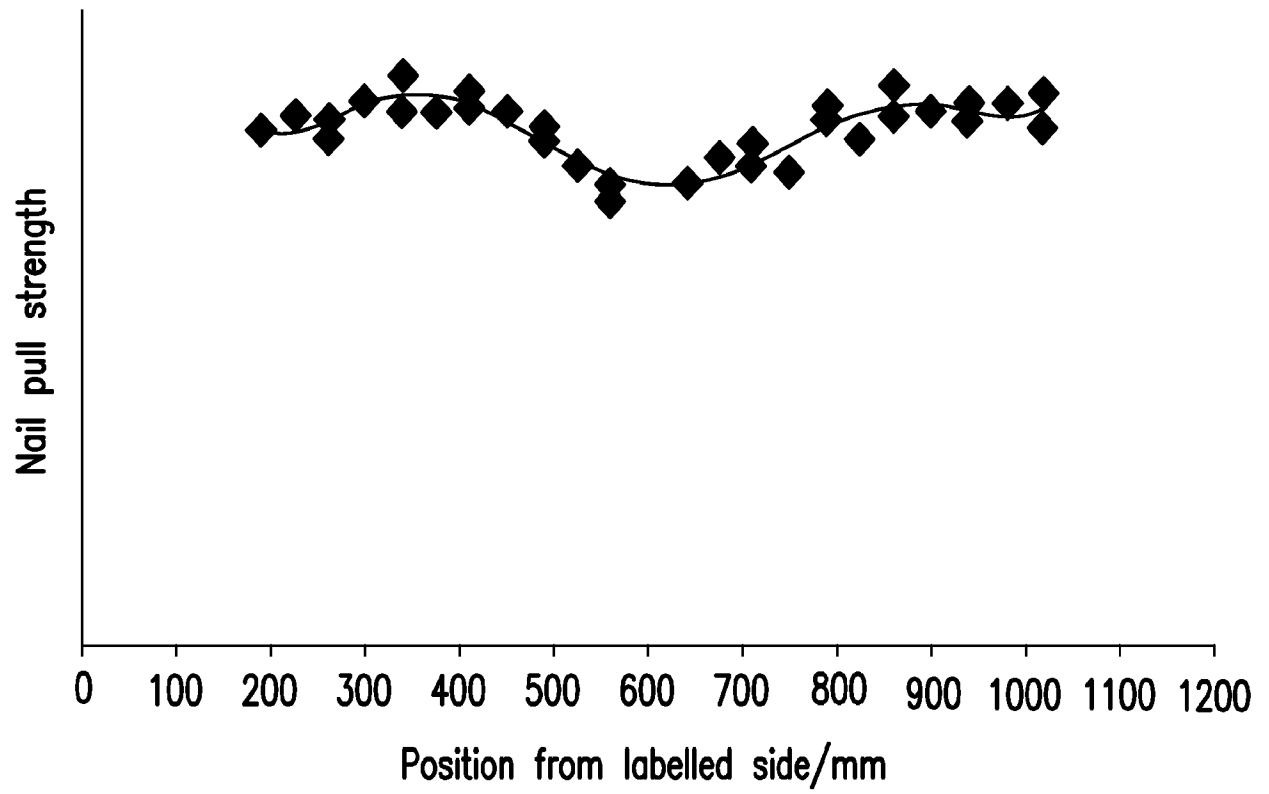


FIG. 4

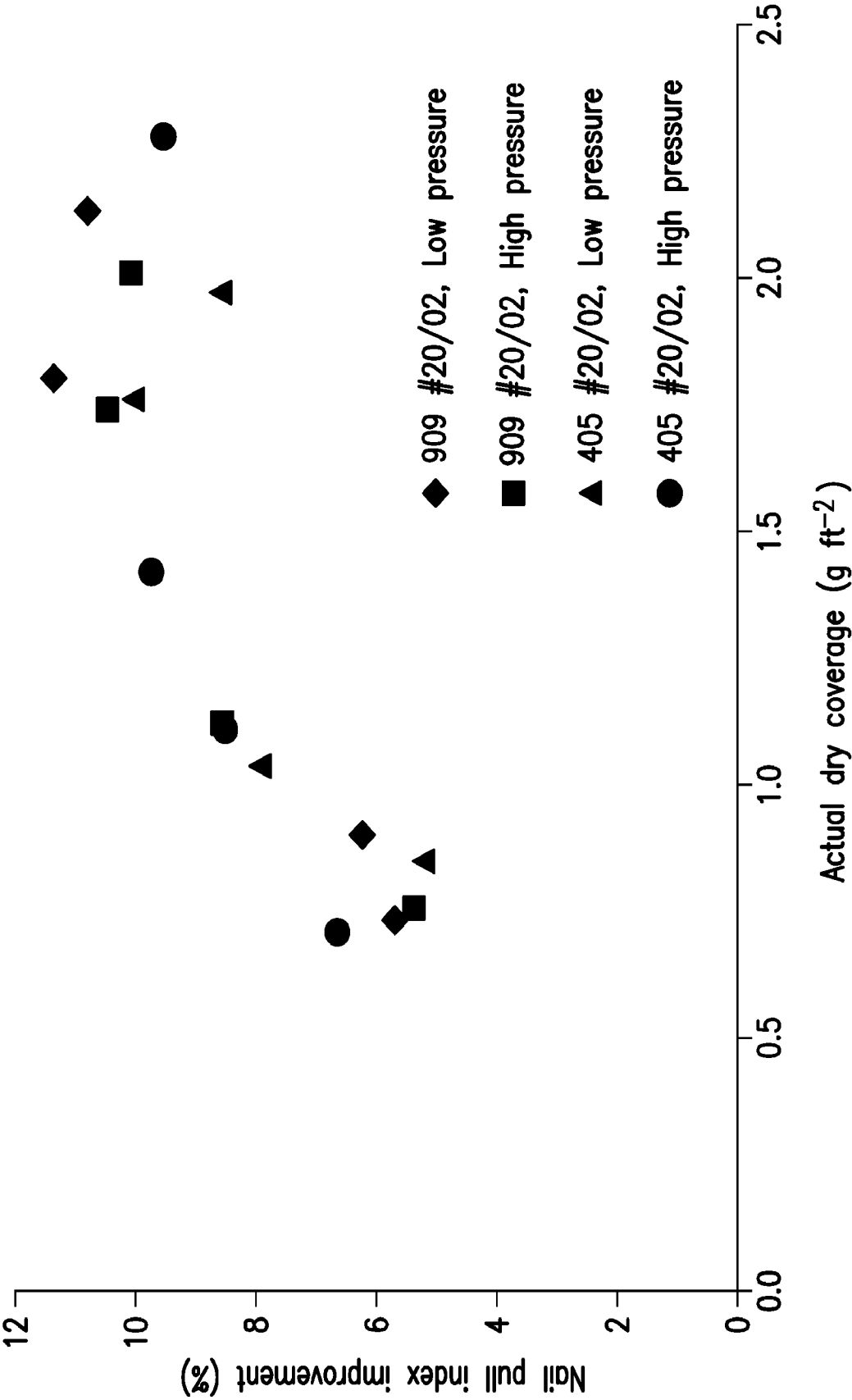


FIG. 5

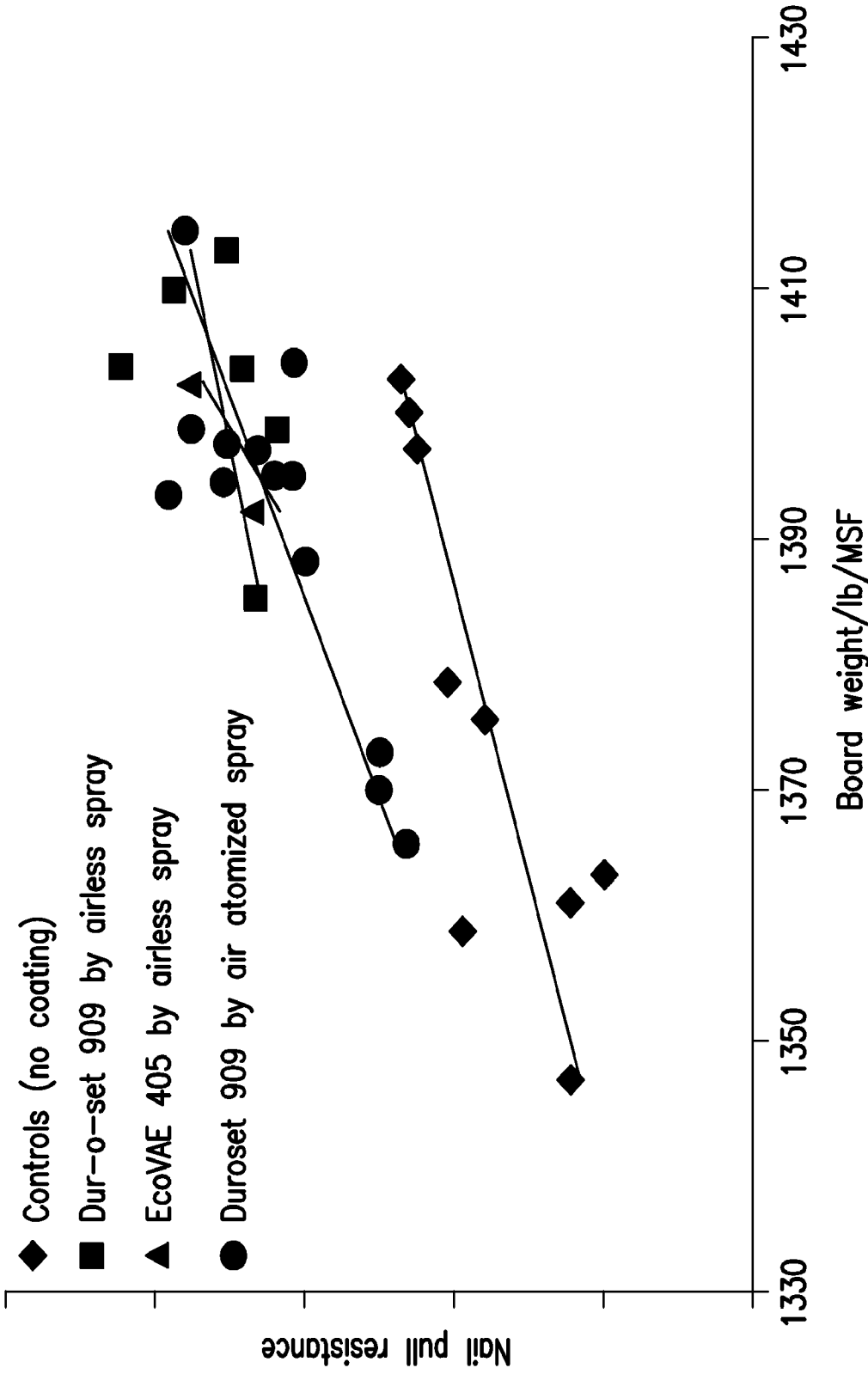


FIG. 6

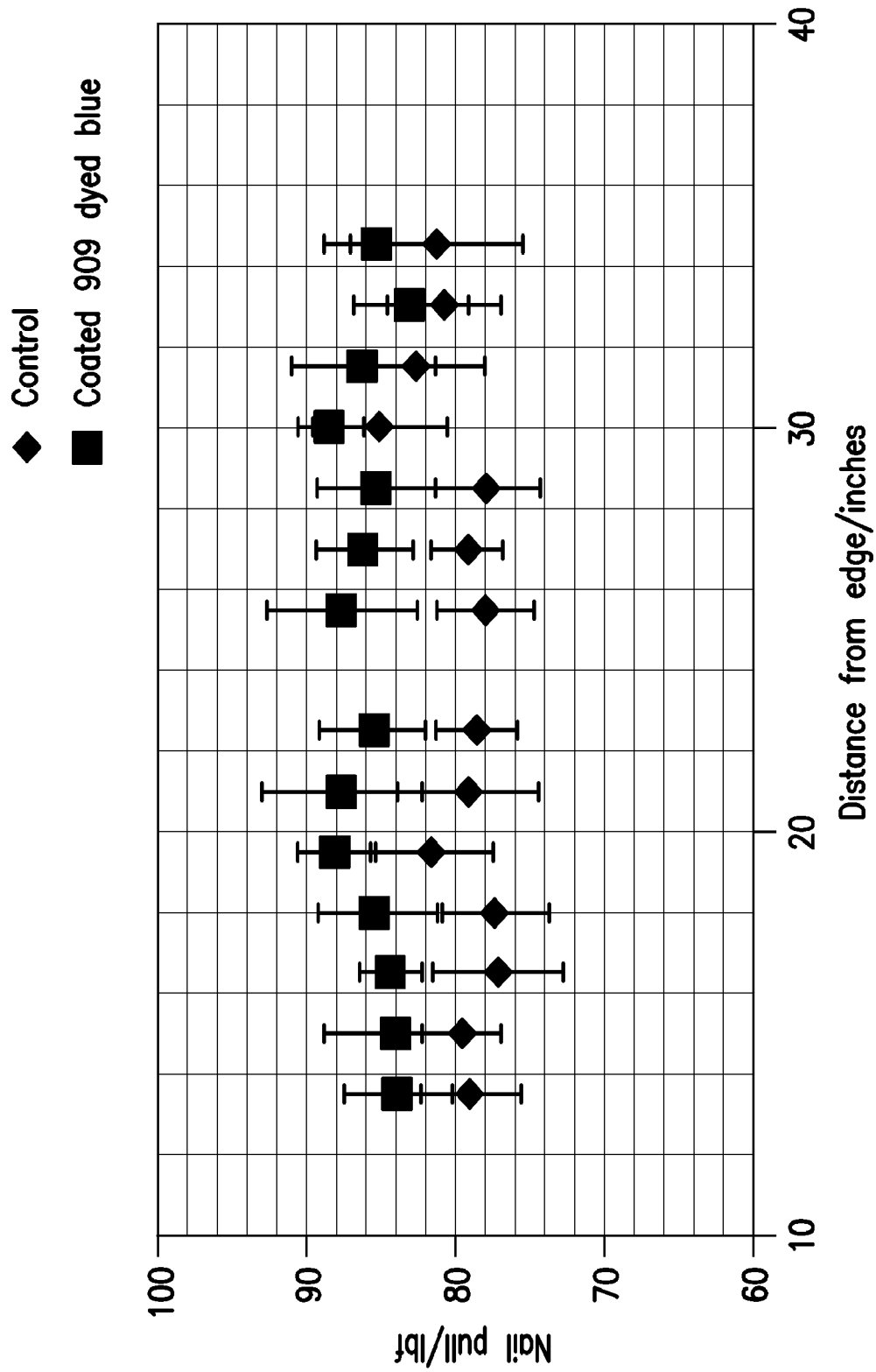


FIG. 7