



(22) Date de dépôt/Filing Date: 1997/01/15

(41) Mise à la disp. pub./Open to Public Insp.: 1998/07/15

(45) Date de délivrance/Issue Date: 2003/12/30

(51) Cl.Int.⁶/Int.Cl.⁶ H04B 10/08

(72) Inventeurs/Inventors:

LAM, DENNIS K. W., JP;
CHAN, CHUN KIT, HK;
CHEN, LIAN-KUAN, HK;
TONG, FRANK F. K., HK

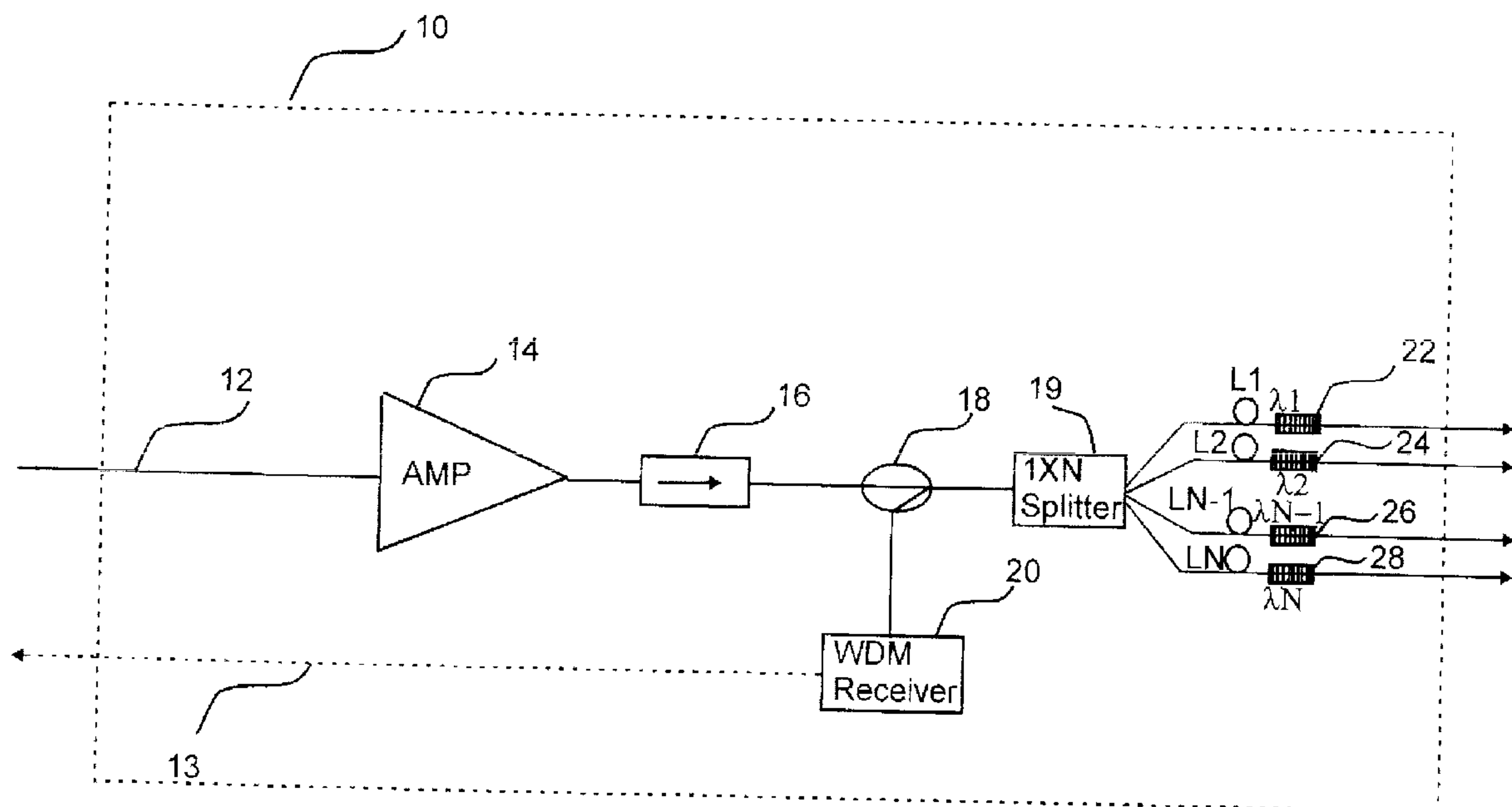
(73) Propriétaire/Owner:

JDS FITEL INC., CA

(74) Agent: TEITELBAUM & MACLEAN

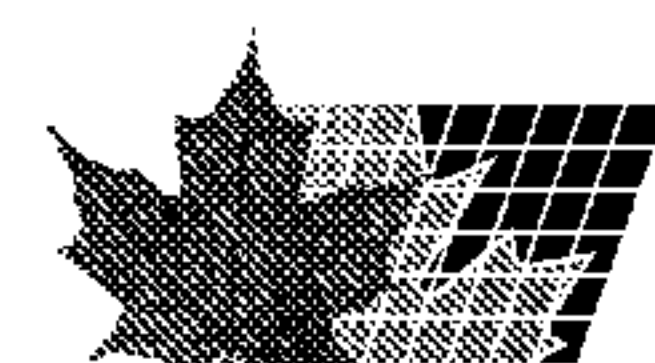
(54) Titre : SYSTÈME DE SURVEILLANCE POUR RESEAUX OPTIQUES RAMIFIES PASSIFS

(54) Title: SURVEILLANCE SYSTEM FOR PASSIVE BRANCHED OPTICAL NETWORKS



(57) Abrégé/Abstract:

A surveillance system for in-service fault identification in an amplified passive branched optical network is provided. This system does not require any wavelength tunable light source as used in multi-wavelength OTDR. Fiber-Bragg gratings are placed at some strategic positions on different fiber branches to slice and reflect the optical amplifier's residual ASE power at some wavelength other than the signal wavelengths. The conditions of the fiber link and optical amplifier at each branch can be monitored by constantly checking the reflected power level of the corresponding wavelength without suspending the in-service channels.



Abstract of the Disclosure

A surveillance system for in-service fault identification in an amplified passive branched
5 optical network is provided. This system does not require any wavelength tunable light source as
used in multi-wavelength OTDR. Fiber-Bragg gratings are placed at some strategic positions on
different fiber branches to slice and reflect the optical amplifier's residual ASE power at some
wavelength other than the signal wavelengths. The conditions of the fiber link and optical
amplifier at each branch can be monitored by constantly checking the reflected power level of the
10 corresponding wavelength without suspending the in-service channels.

A PASSIVE SURVEILLANCE SYSTEM FOR PASSIVE BRANCHED OPTICAL NETWORKS

5 **Field of the Invention**

This invention relates to optical test apparatus, and in particular to an apparatus for detecting and monitoring losses and/or faults in optical fibres. The invention also provides a means of testing optical networks.

10

Background of the Invention

It is well known that faults in optical fibres can be located by an optical time domain reflectometer (OTDR). An OTDR typically launches a pulse of light into an optical fibre, and backscattered light is monitored for abrupt changes indicative of a loss or fault. The distance of the loss or fault from the launch end of the fibre can be determined from the time interval between the launch and the return of the backscattered peak. Once a period of time sufficient to receive all detectable backscattered light has passed, a further pulse may be launched into the fibre. The pulse width may be varied for different dynamic range or resolution requirements. Thus, for a given amplitude, an increase in the pulse width enables a greater length of fibre to be monitored, that is to say it increases the dynamic range of the OTDR. The dynamic range of an OTDR is the loss after which an event, backscatter or reflection can still be detected.

The OTDR is an extremely useful form of optical test equipment since, from connection to a single end of an optical fibre network, the location of losses and reflections can be determined, and their amplitude measured, to a high degree of accuracy. For loss measurements, both point-losses and end-to-end fibre or network losses can be measured. In duplex networks, the amplitude of any reflections is important, since these may cause crosstalk. In some known schemes it is possible using wavelength division multiplexing (WDM) techniques, to take these

measurements at a particular wavelength i.e. 1650 nm whilst the network is carrying data at another wavelength i.e. 1550 nm.

As of late, there has been a demand for an OTDR system that conveniently and
5 inexpensively allows for the reliability testing of individual optical fibres within optical networks of optical fibers. Methods used heretofore in conventional OTDR are not suitable, since the Rayleigh back-scattered light from different branches cannot be differentiated at the OTDR. Notwithstanding, recently, several methods based on multi-wavelength OTDR have been proposed in:

10 a paper by I. Sankawa, "Fault Location Technique for In-Service Branched Optical Fiber Networks", published in IEEE Photon. Technol. Lett., vol. 2, no 10, pp 766-768, 1990;
a paper by Y. Koyamada, et al, entitled "Recent Progress in OTDR Technologies for Maintaining Optical fiber Networks", IOOC'95, Paper FA1-4, Hong Kong, 1995.
a paper by K. Tanaka, et al, "Measuring the Individual Attention Distribution of Passive
15 Branched Optical Networks", IEEE Photon. Technol. Lett., vol. 8, no. 7, pp. 915-917, 1996; and,
a paper by M. Shigehara, et al., "Optical Fiber Identification System Using Fiber Bragg Gratings", Technical Digest, OFC'96 Paper WK13, San Jose, 1996; all of which are incorporated herein by reference.

20 However, these proposed OTDR systems require a wavelength-tunable pulsed light source for the test signals and thus impose high cost and complexity. For the schemes proposed by Sankawa, and Koyamada et al., strong monitoring signals from the wavelength-tunable light sources may deplete the gain of the in-line optical amplifiers and result in system penalty; whereas this invention, in contrast provides an in-service fault detection system using optical
25 amplifiers on passive branched optical networks (PBONs) and on a concatenated link without requiring an extra light source.

Two known systems that address OTDR in optical networks are disclosed in United States patent numbers 5,491,573 and 5,491,574 in the name of Shipley. Another United States
30 patent in the same field is patent number 5,329,392 in the name of Cohen. In view of the

limitations of these aforementioned inventions, it is an object of one aspect of this invention to provide a novel passive surveillance scheme for fault identification in optically-amplified PBON using fiber Bragg gratings (FBG) without using any extra light source for the test signals. The invention further obviates the use of a tunable OTDR pulsed light source.

5

It is a further object of the invention to provide an inexpensive device for testing an optical network of waveguides in the presence of traffic.

More generally, it is an object of this invention to provide a passive surveillance system
10 that is compatible with the use of optical amplifiers and which utilizes otherwise unused spectrum provided by a rare earth doped optical amplifier.

Summary of the Invention

15 In accordance with one aspect of the invention, a surveillance scheme for in-service fault identification in optically amplified passive branched optical networks and concatenated links is provided. In a preferred embodiment fiber Bragg gratings are disposed at strategic positions on different fiber branches to slice and reflect the optical amplifier's residual amplified spontaneous emission (ASE) power at some wavelengths other than at signal or traffic wavelengths. In yet
20 another embodiment fiber Bragg gratings are disposed at strategic positions along a waveguide to slice and reflect the optical amplifier's residual ASE power at some wavelengths other than at signal or traffic wavelengths.

In accordance with another broad aspect of the invention, in an optically-amplified
25 passive branched optical network having a plurality of optical branch paths each path having a fiber Bragg grating for passing traffic signal wavelengths of light and reflecting other test wavelengths of light, a surveillance method is provided for in-service fault identification. The method comprises the steps of:
monitoring the optically-amplified passive branched optical network to detect the test
30 wavelengths of light, wherein the test wavelengths of light are generated by the amplifier and are

confined to its normally unused portion of its amplifying spectrum outside of the wavelengths of traffic signal wavelengths.

5 In accordance with another broad aspect of the invention a broad band light source is provided having a plurality of test wavelengths of light. Light centered at these test wavelengths is launched into an optical network having fiber Bragg gratings at branch paths or on concatenated paths. Fiber Bragg gratings on different branch paths are designed to reflect different test wavelengths backwards to a receiver and detection circuit optically coupled to a main trunk. The amplitudes of the reflected test wavelengths of light are continuously monitored
10 to determine if a fault exists on a particular branch. Conveniently, by providing a constant beam of test wavelengths of light having wavelengths that are different than those for normal data transmission, monitoring can occur continuously along with data transmission on the same optical branch paths.

15 In accordance with yet one other aspect of the invention, a method and system for retrofitting an existing optical fibre network with fault detection means is provided. The method comprises the steps of in-situ provision of fiber in-line Bragg gratings at predetermined locations on predetermined optical waveguides disposed within the network; and further comprising the steps of providing a broadband light source preferably in the form of an ASE power spectrum
20 associated with an optical amplifier in the network; and, detecting signal levels of test signals reflected from the in-line fiber Bragg gratings.

Brief Description of the Drawings

25 Embodiments of the invention will now be described in conjunction with the drawings, in which:

Fig. 1a is a circuit diagram of a surveillance scheme of a 1xN stage system in accordance with the invention;

Fig. 1b is circuit diagram of a surveillance system of an M-ary tree-branched PBON;

Fig. 2 is a circuit diagram of a single feeder optical system having Bragg gratings spaced along its length;

Fig. 3 is a graph of wavelength versus amplitude of the transmitted spectrum of branch 1 in a 1x4 stage PBON;

5 Fig. 3a is a graph of wavelength versus amplitude of the reflection spectrum wherein no faults are present in branch 1 and branch 2; and,

Fig. 3b is a graph of wavelength versus amplitude of the reflection spectrum wherein branch 1 is broken to simulate a fault and no fault is present in branch 2.

10 Detailed Description

Referring now to Fig. 1a, a network is shown having an input path **12** coupled to an erbium doped fiber amplifier (EDFA) **14**. An optical isolator **16** is coupled to the output of the EDFA **14** for preventing unwanted back reflections from entering the output end of the amplifier. A 3-port
 15 optical circulator **18**, via ports 1 and 2, optically couples light exiting the isolator **16** with a 1XN splitter **19** which splits an input optical signal into N signals paths. Alternatively, the optical circulator **18** can be replaced with an optical coupler (not shown). Further, when the optical circulator **18** is used in place of an optical coupler, the optical isolator **16** may in some instances be removed where adequate isolation is provided by the circulator **18**. As is shown in the
 20 example of the figure, the signal paths are of varying lengths $L_1=4.4$ km, $L_2=8.8$ km, .. L_{N-1} and L_N . The N optical signal paths are equipped to be monitored and each have a fiber Bragg grating (FBG) designed to reflect a different wavelength of incident light in the form of a unique test signal backwards towards the optical circulator **18**. For example the grating **22** is designed to reflect light of wavelength λ_1 backwards and to pass light of other wavelengths of light
 25 incident upon it; the second grating **24** is designed to reflect light of wavelength λ_2 incident upon it, and to pass other wavelengths of light. A wavelength division multiplexing (WDM) receiver **20** is coupled to port 3 of the optical circulator **18** for receiving and detecting signal strength of reflected ASE light reflected from any of the gratings **22** ... **28**.

In operation the EDFA's **14** residual amplified spontaneous emission (ASE) power is utilized as a broadband light source to provide constant monitoring signals. The fiber Bragg gratings **22, 24...28** are placed at strategic, predetermined locations on different branches for example grating **22** on a first branch, grating **24** on a second branch, and so on, and are used to

5 “slice and reflect” the ASE power at wavelengths outside the signal/ traffic wavelengths of (1525-1540 nm and 1556-1566 nm). Since each FBG is designed to reflect a different centre wavelength, each of the N-branches can be monitored constantly and simultaneously by detecting the reflected power level of the corresponding wavelength without suspending or adversely affecting the in service data channels.

10

By way of example, the following experiment was performed wherein FBGs were designed to have centre wavelengths for λ_1 and λ_2 equal to 1557.5 nm and 1559 nm respectively. Branches N-1 and N for this 4 branch experiment were left unmonitored. The 3-dB bandwidth and reflectivity of each FBG was 0.9 nm and 90% respectively. The insertion loss and

15 the directivity from the amplifier **14** output to the monitoring WDM receiver **20** of the circulator **18** was 1 dB and 60 dB, respectively.

A signal was launched into input fibre **12**, comprising two data channels at 1550 nm and 1545 nm with transmitted power 4 dBm prior to splitting. The output ASE power was

20 approximately -20 dBm at the wavelengths λ_1 and λ_2 . Fig. 3 shows the transmitted power at branch 1 after grating **22**. The notch at a wavelength of $\lambda_1=1557.5$ nm indicates that the ASE power at this wavelength is reflected back to the circulator **18**. Fig. 3a illustrates the reflected spectrum with no faults in either branch 1 or branch 2. ASE power at both wavelengths λ_1 and λ_2 is received at the circulator **18**. As a means of simulating the fault identification process, the

25 fibre of branch 1 was intentionally disconnected from the network and the reflected spectrum is shown in Fig. 3b. The drop in reflected power at λ_1 is about 6 dB at a wavelength of λ_1 received at the circulator port 3, indicating a fault at branch 1; and, residual ASE spectrum shown in Fig. 3b is due to the broadband back-scattered light from the fault.

The single stage 1xN PBON shown in Fig. 1a can be cascaded with a plurality of other stages as is shown in Fig. 1b. Here, an optical fibre trunk **12** includes a headend **8** with a plurality of data channels launched into the headend **8** having a first stage **10a** cascaded with a second stage **10b**. Of course, numerous other stages may be added. The monitoring information at each 1xN stage can then be transmitted back to network operators via telephone lines or on a specific subcarrier (SCM) in the upstream channel. Since the return path for each stage is independent by using the isolator or the circulator, the reflection wavelength of the FBG in different stages can be duplicated. Therefore, even with a limited number of test channels per stage due to the limited ASE spectrum, it is possible to implement a large number of monitoring channels in a large and expansive network. Conveniently, the circulator **18b** prevents signals from traveling to an earlier upstream stage **10a**. Since separate receivers **20a**, **20b** are used at each stage same Bragg fibre gratings can also be utilized, for example, grating 22a and 22b can have the same wavelength response, and similarly, gratings 24a and 24b can have the same wavelength response.

Turning now to Fig. 2, a single feeder configuration **30** is shown wherein a plurality of fibre Bragg gratings (FBGs) of different center wavelengths are used to locate a fault along the feeder. A first stage of an M stage single feeder comprises an EDFA **14** followed in series by an isolator **16** having a coupler or circulator **18** for directing data signals and ASE power from the amplifier to fibres L1 and L2 connected in series. FBGs **22** and **24** designed to reflect wavelengths of light of λ_1 and λ_2 are disposed after L1 and L2 respectively, along the light guiding path. If a fault is present between the circulator **18** and the FBG **22** the signal energy detected at the receiver **20** will be attenuated. The presence of full signal energy from the ASE at the wavelength λ_1 and attenuated energy at the wavelength λ_2 indicates a fault between FBG 22 and FBG 24. If a fault exists between the FBG **22** and the FBG **24** signal energy of wavelength λ_2 will be attenuated while energy at the wavelength λ_1 will not be attenuated. As in the previous embodiments described heretofore, all of the ASE signals are extracted using an optical circulator or optical coupler and are detected by a detection means such as a WDM receiver. If the received ASE power at any designated monitoring wavelength deteriorates after certain time, or is below the detection limit, this indicates that there might be a fault or a progressive degradation at the corresponding fibre section or branch.

Design Considerations

The unused portion of the ASE spectrum of the EDFA **14** is approximately 25 nm which
 5 can accommodate about 10 monitoring or test wavelengths using FBGs with central wavelength
 separation of 0.8 nm and an individual passband of 0.5 nm. These values coincide with those of
 commercially available array waveguide demultiplexers that can be used in the receiver **20**. In
 practice, for example in a communications system, it may be desirable to maximize the number
 of branches within a network and the fiber span of each branch so as to support more users and
 10 have a wider geographic coverage. Considering a 1xN stage system, the fiber span L of each
 branch can be expressed as

$$L \leq \{P - 2C - 20\log_{10}N + 10\log_{10}R - D\}/2\alpha \quad (\text{in km}) \quad (1)$$

15 where P is the ASE power in dBm at the specific monitoring wavelength, N is the number of
 branches, C is the insertion loss of the circulator or the splitting loss of the coupler in dB, α is the
 fiber attenuation in dB/km, R is the reflectivity of the FBG, and D is the detection threshold of
 the monitoring receiver in dBm. In Figure 5 a plot of L versus N for $C=1$ dB (using a circulator),
 $R=95\%$, $D=-50$ dBm, $\alpha=0.2$ dB/km and $P=-20, -24, -28$ dBm. For example, if $L=20$ km, the
 20 maximum N allowed is approximately 10 for a single stage. More branches consequently result
 in a shorter fiber span because of the increased splitting loss. For the single feeder instance, the
 maximum L is primarily limited by the fiber loss and the FBG insertion loss I and is given by

$$L \leq \{P - 2C - 2(K-1)I + 10\log_{10}R - D\}/2\alpha \quad (\text{in km}) \quad (2)$$

25

where K is the number of FBGs placed on the feeder.

Advantageously, this invention makes use of otherwise unused ASE power within a
 predetermined bandwidth available when commercially available optical amplifiers are used for

amplification. However, although perhaps less economical, other constant broadband light sources may be envisaged for monitoring test wavelengths of light reflected from Bragg fiber gratings without departing from the spirit and scope of this invention.

- 5 Further, advantageously, this invention is particularly compatible with existing optical networks where insitu writing of gratings is possible. By writing or providing optical gratings within optical fibres that currently exist, a system is provided wherein fault detection is achievable. Of course, numerous other embodiments can be envisaged, without departing from the spirit and scope of the invention.

Claims

What is claimed is:

1. A method of monitoring an optical waveguide including one or more other waveguides, carrying at least one data channel and at least one test channel comprising the steps of:
 - a) providing at least one fiber Bragg grating spaced apart in-line along the waveguide each of said at least one fiber Bragg gratings having a different predetermined centre wavelength for reflecting incident light at the different predetermined wavelength, said different predetermined centre wavelength corresponding to the at least one test channel;
 - b) providing a broadband light source comprising the predetermined centre wavelengths;
 - c) tapping light that has reflected backwards from the at least one fibre Bragg gratings; and,
 - d) determining if any of the tapped light that corresponds to any of the at least one test channels is attenuated below a predetermined threshold, thereby indicating a fault.

2. A method of monitoring an optical waveguide as defined in claim 1, further comprising the step of providing an amplifier for amplifying the data channels, and for generating test signals corresponding to the test channels by utilizing an ASE spectrum of the amplifier as the broadband light source.

3. In an amplified passive branched optical network having a plurality of optical branch paths, the branch paths each having a grating for passing traffic signal wavelengths of light and reflecting a unique other test wavelength of light, a surveillance method is provided for in-service fault identification, the method comprising the steps of: monitoring the amplified passive branched network to detect the test wavelengths of light confined to an amplifier's ASE spectrum, wherein the test wavelengths of light are generated by the amplifier by ASE and are confined to its normally unused portion of spectrum, outside of the wavelengths of traffic signal wavelengths.

4. A method as defined in claim 3, wherein the step of monitoring the amplified passive branched optical network to detect the test wavelengths of light comprises the step of determining if the detected test wavelengths of light have a magnitude less than a predetermined threshold.

5. A system for fault identification in an optical network comprising:

a network of branched optical paths, the branched paths each having an in-line fiber grating for transmitting signal wavelengths and for reflecting other test wavelengths of light, at least some of the in-line fiber gratings having a different reflection spectrum than other of the gratings;

an optical amplifier at or near an input end of the network of branched optical paths, for amplifying at least some transmitting signal wavelengths and for generating a source of test wavelengths of light including a plurality of wavelengths within the reflection spectrum of the at least some gratings; and,

means disposed between an output end of the amplifier and the network of branch paths for coupling test wavelengths reflected by the in-line fiber gratings out of the network for analysis.

6. A system as defined in claim 5, wherein the means for coupling test wavelengths is optically coupled to a WDM receiver.

7. A system for fault identification in an optical network comprising:

a network of branch paths, the branch paths each having an in-line fiber grating for transmitting signal wavelengths and for reflecting other test wavelengths of light, at least some of the in-line fiber gratings having a different reflection spectrum than other of the gratings; and, means for transmitting signal wavelengths and for providing a broadband source of other wavelengths of test light including a plurality of wavelengths within the reflection spectrum of the at least some gratings.

8. A system as defined in claim 7, further comprising means for receiving and detecting the test wavelengths of light.

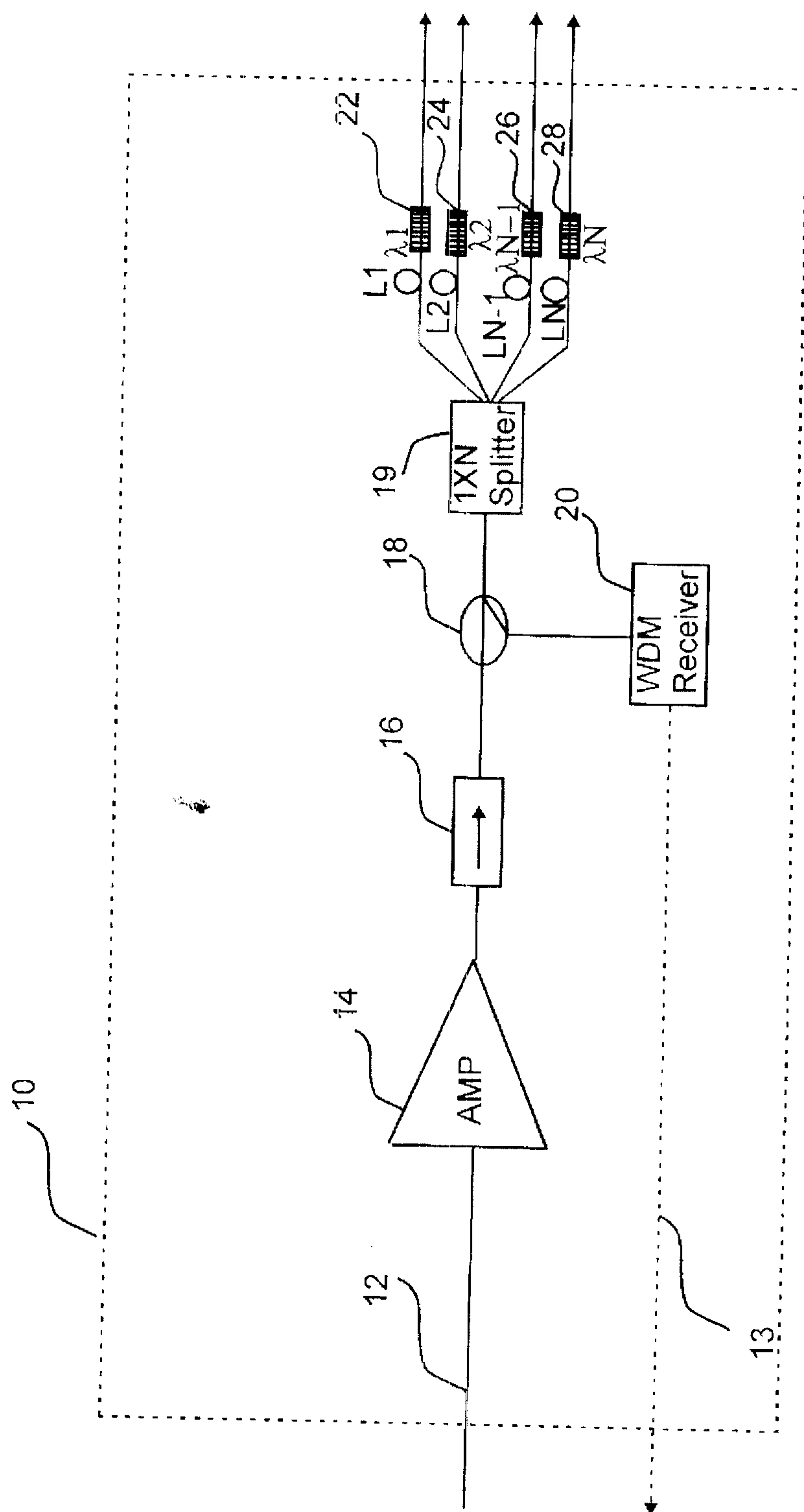


Fig. 1a

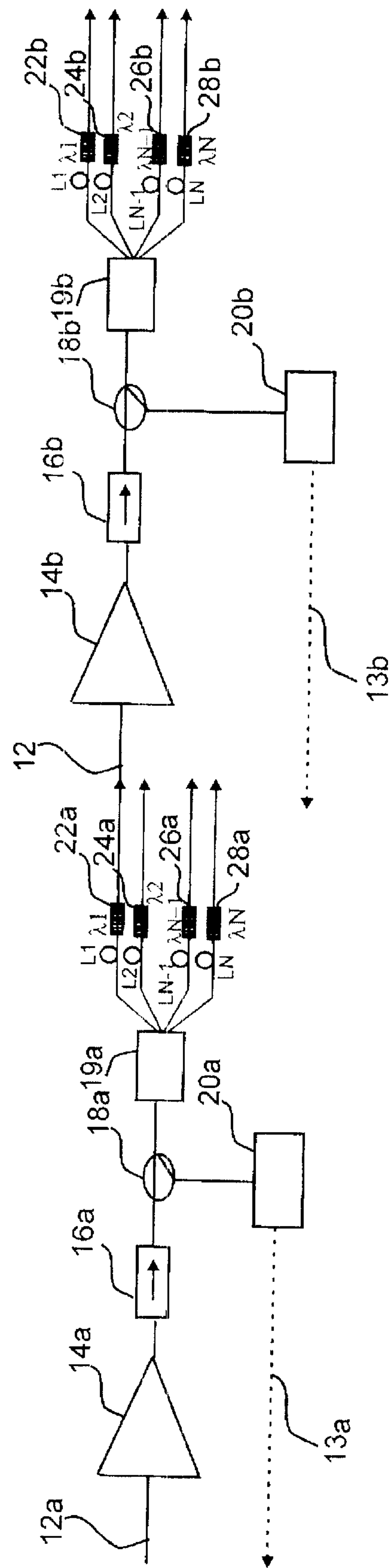


Fig. 1b

2195153

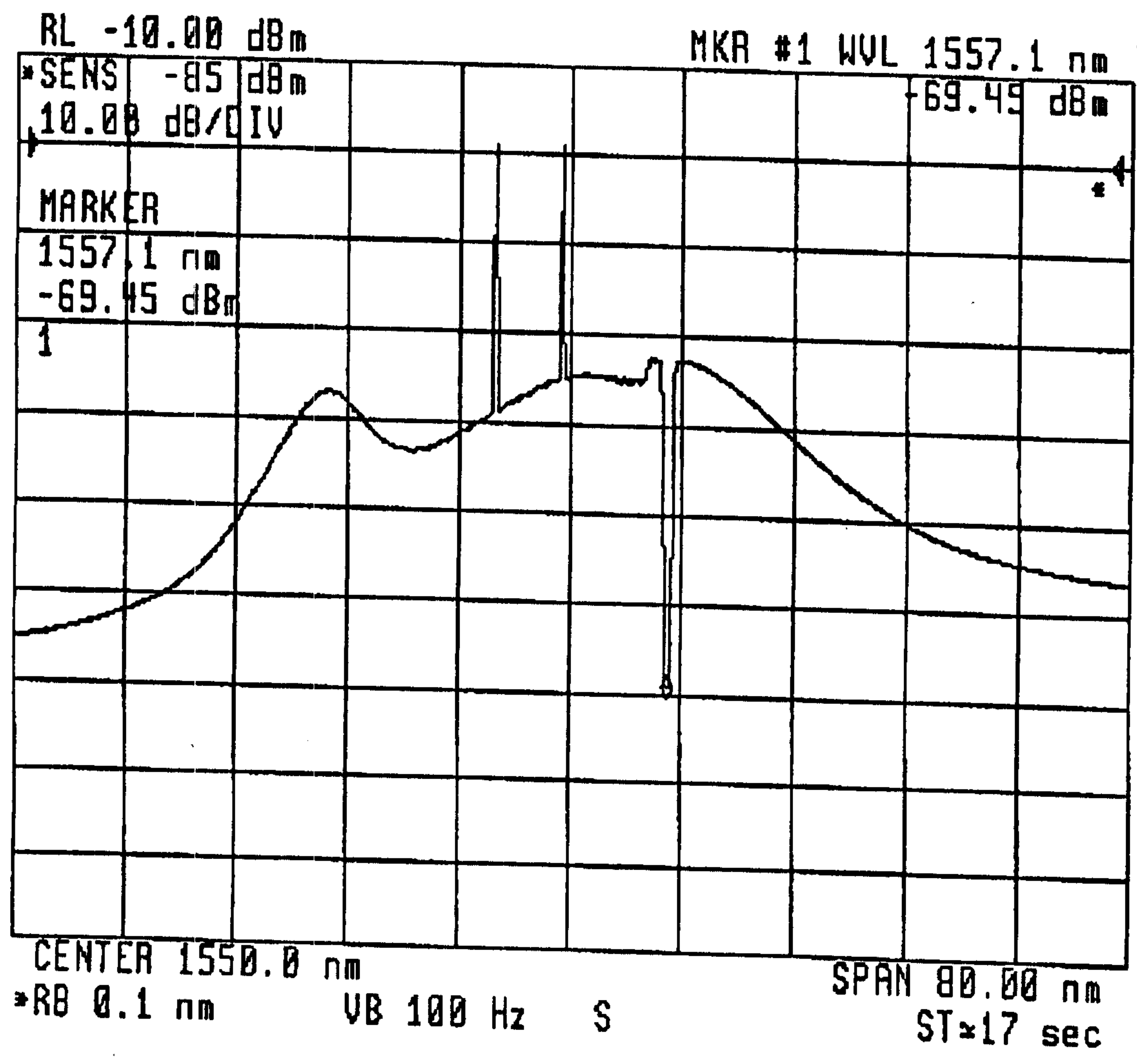


Fig. 3

2195153

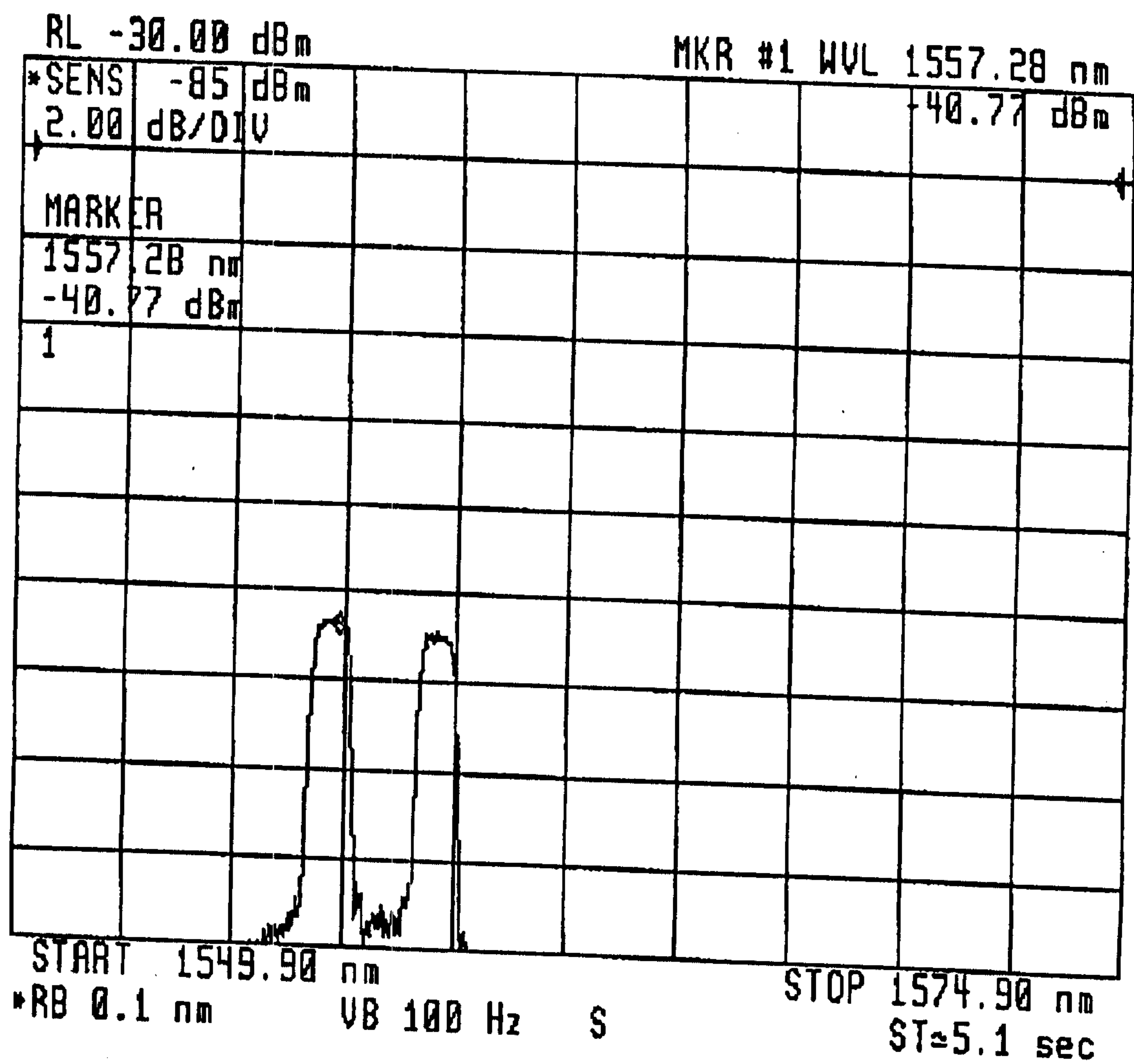


Fig. 3a

2195153

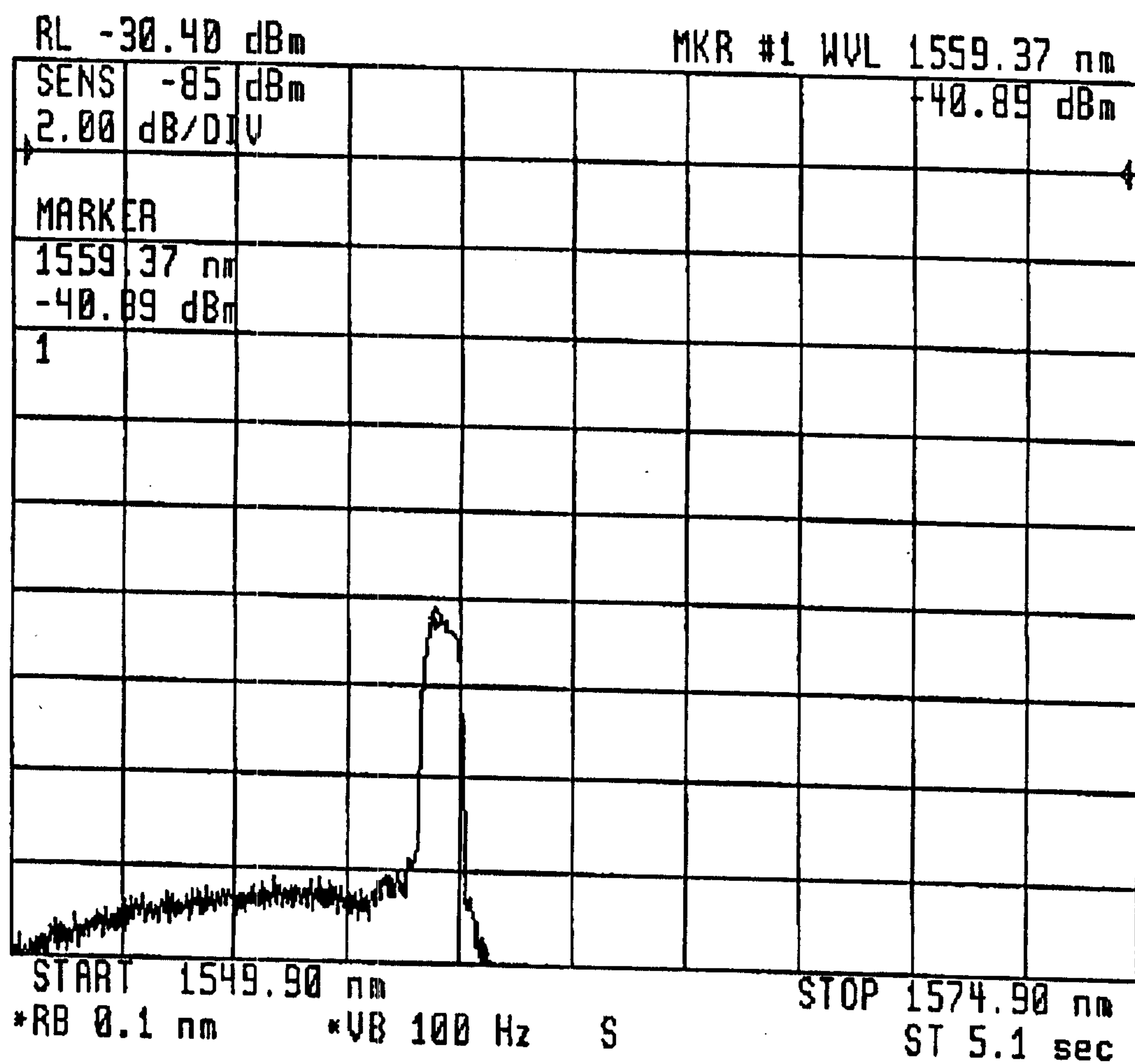


Fig. 3b

