



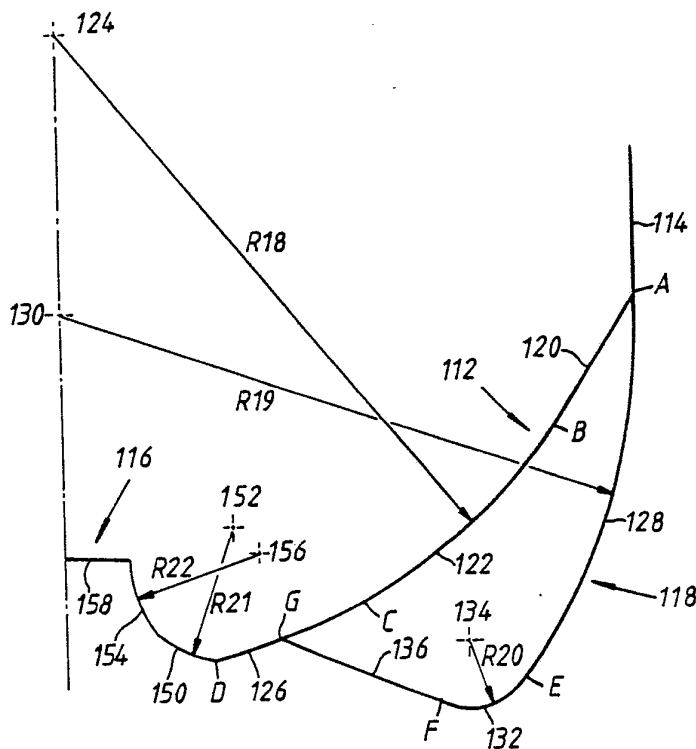
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<p>(21) International Application Number: PCT/GB87/00102 (22) International Filing Date: 12 February 1987 (12.02.87) (31) Priority Application Numbers: 8603709 8604660 (32) Priority Dates: 14 February 1986 (14.02.86) 25 February 1986 (25.02.86) (33) Priority Country: GB (71) Applicant (for all designated States except US): NOR- DERNEY INVESTMENTS LIMITED [GB/GB]; P.O. Box 23, Ordnance House, Saint Helier, Jersey (GB). (71)(72) Applicant and Inventor: OKHAI, Aziz, A. [GB/GB]; 43 Dundee Road, Dundee (GB).</p>		<p>(74) Agent: FITZPATRICKS; 4 West Regent Street, Glas- gow G2 1RS (GB). (81) Designated States: AT (European patent), AU, BE (Eu- ropean patent), BR, CH (European patent), DE (Eu- ropean patent), DK, FI, FR (European patent), GB (European patent), IT (European patent), JP, KR, LU (European patent), NL (European patent), NO, SE (European patent), US.  <b>Published</b> <i>With international search report.</i></p>

(54) Title: IMPROVEMENTS IN OR RELATING TO PLASTICS CONTAINERS

(57) Abstract

A container of blow-moulded oriented thermoplastic material includes a base structure comprising a convex annular surface (which may be divided into a plurality of feet (118) by radial webs (112)) and a central re-entrant portion (116). In blow-moulding the container, a moulded preform is enclosed within a mould, heated, and stretched such that its bottom surface impinges upon a projecting surface of the mould bottom corresponding to the topmost surface (158) of the re-entrant portion. After blow-moulding, the material of the re-entrant portion (116) remains unoriented and relatively thick in comparison to the material of the remainder of the base. The unoriented material in the base is substantially confined to the re-entrant portion (116) which itself is strengthened by its relatively thick walls and the base thus exhibits improved creep and stress cracking properties.



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IMPROVEMENTS IN OR RELATING TO PLASTICS CONTAINERSDescription

The present invention is concerned with plastics containers and particularly with blow-moulded plastic bottles made from oriented thermoplastic materials such as PET and intended for use as containers for carbonated beverages.

The use of blow-moulded bottles as containers for pressurized liquids such as carbonated soft drinks, beers, ciders etc. presents a number of problems. In particular, the internal pressure generated by such liquids tends to distort the thin, flexible walls which are characteristic of blow-moulded bottles. This applies particularly to the base portion of the bottle.

Previously, this problem has been obviated by the use of a hemispherical base which distributes the pressure as evenly as possible and thus prevents distortion. Such a base is, however, inherently unstable and some means is required to allow the bottle to be free-standing. One approach is to attach a basecup to the hemispherical base, but this obviously increases manufacturing costs. There are also problems with adhesion and inaccurate positioning of the basecup which may result in a bottle which does not stand vertically.

Accordingly attempts have been made to produce a one-piece, blow-moulded bottle which is usable with pressurized liquids.

There have been many proposals for designs of such bottles, generally including either bases having a central concave portion, or a generally convex base with a plurality of stabilizing feet blown out therefrom, however none of these have been totally satisfactory in use. Problems encountered include creep and distortion of the bottle material, stress cracking, and poor resistance to impact. A typical bottle base is shown in

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Fig 1 of the accompanying drawings and comprises a generally hemispherical section 2 having stabilizing feet 4 blown out therefrom. Such bottles are blow-moulded from an injection moulded preform as follows: the preform is heated, enclosed within a mould corresponding to the desired shape of the bottle, stretched by a stretch-rod inserted through the neck of the preform, and then blown. The stretch-rod stretches the preform to the full length of the mould so that the bottom of the preform impinges upon the bottom of the mould. The material which contacts the bottom of the mould at this stage is "frozen" so that when the bottle is blown the material around the centre of the base remains unoriented and relatively weak. In a bottle such as that of Fig 1 this area of unoriented material extends well into the feet 4 of the base so that the base structure is weakened and becomes subject to creep and distortion. Additionally, the transition from unoriented to oriented material is relatively abrupt, creating weak points where the transition occurs and reducing the resistance of the base to stress cracking or the like. These problems can obviously be overcome by making the base thicker; however this increases the amount of material required and hence the weight of the bottle. Thus, the advantages of a one piece bottle over a conventional base cupped bottle are substantially reduced.

It is an object of the present invention to obviate or mitigate these disadvantages.

Accordingly, the invention provides a container of blow-moulded oriented thermoplastic material which is formed by enclosing a heated moulded preform within a mould corresponding to the shape of the container, and stretching it to the full length of the mould so that its bottom surface impinges upon the bottom surface of the mould prior to blow-moulding, said

container comprising a generally cylindrical body portion and a base portion closing the bottom end of said body portion wherein said base portion is a figure of rotation formed by rotating a generally convex curve extending from the bottom of said side wall to the central longitudinal axis of the container about said central axis so as to define an annular convex surface having a central re-entrant portion, and wherein said preform, when stretched prior to blow-moulding, impinges upon a projecting central portion of the bottom of the mould corresponding to said re-entrant portion, such that, when blow-moulded, the material in the vicinity of said re-entrant portion remains unoriented and relatively thick in comparison with the oriented material of the remainder of the base portion.

Preferably the base portion is provided with a plurality of radial webs extending from the bottom of the body portion towards the centre of the base portion and dividing said annular convex surface into a plurality of feet spaced around the circumference of the base.

According to a second aspect of the invention, a plastic container comprises a generally cylindrical body portion and a base portion closing the bottom end of said body portion, said base portion comprising an annular convex surface having a central re-entrant portion, the walls of said re-entrant portion being substantially thicker than the walls of the remainder of said base portion.

The ratio of the thickness of the walls of the re-entrant portion to the walls of the remainder of the base portion is preferably in the range 1.2:1 to 10:1, and the angle of divergence of the side walls of the re-entrant portion is preferably less than  $60^{\circ}$ . It is also preferred that the diameter of the re-entrant portion is in the range 5% to 30% of the overall base diameter and more preferably in the range 10% to 20% thereof.

Embodiments of the invention will now be described, by way of example only, with reference to the accompanying drawings in which:

Fig 1 illustrates the prior art, as discussed above;

Fig 2 is a diametrical cross-section of the base portion of a container forming the basis of the present invention;

Fig 3 is a perspective view of the base of Fig 2;

Figs 4 to 9 show variations of the base of Figs 2 and 3;

Figs 10 and 11 are diametrical cross-sections of further modified base portions;

Figs 12 and 13 are respectively a sectional side and a bottom view of a particularly preferred embodiment of the invention;

Figs 14 and 15 are sectional side views of containers similar to that of Figs 12 and 13; and

Fig 16 shows a conventional plastics container for comparison with Figs 14 and 15.

Referring now to the accompanying drawings, Figs 2 and 3 show the base of a blow-moulded container, such as a bottle 10 having a generally cylindrical side wall 11 of radius  $R_1$ , an upper neck portion (not shown) and a base portion 12 closing the bottom end of the wall 11. In diametrical cross-section the base 12 comprises first and second downwardly convex semicircular portions 14 and 16, having radii  $R_2$  equal to half the radius  $R_1$ , extending downwardly from the side wall 11 and converging at the mid-point of the base portion 12 to form a cusp 18.

The shape of the base 12 is shown in Fig 2 wherein each of the "longitudinal" lines 20 corresponds to the sectional outline of Fig 1 and is essentially a figure of revolution of one of the semicircular portions 14 and 16 about the central longitudinal axis of the bottle 10,

defining an annular convex surface having a central re-entrant portion.

In blow-moulding a base of this shape, stretching the preform causes the bottom thereof to contact the base of the mould only at the point of the cusp 18 so that unoriented material in the base portion 12 is restricted virtually to that point only. Variations in this basic shape are shown in Figs 4 to 7.

The base 12 of Fig 4 comprises first and second circular arcs 26, 28, having radii  $R_4$  greater than half  $R_1$ , and converging at a point 30, and that of Fig 5 comprises first and second semi-elliptical portions 32, 34 - each having a bottom portion 36 of radius  $R_5$ , again greater than half  $R_1$ , and outer and inner peripheral portions 38 of radius  $R_6$ , less than half  $R_1$  - converging at point 40.

Fig 6 shows a base similar to that of Fig 1 having semicircular portions 48 wherein straight line portions 45, 46 are incorporated into the outer and inner walls of the semicircular portions 48. The straight line portions 45 thus form an upwardly diverging frusto-conical section around the outside of the base and the straight line portions 46 form a downwardly diverging frusto-conical section around the central re-entrant portion. Such straight line portions may similarly be incorporated into the bases of Figs 4 and 5, and more than one straight line portion may be incorporated into both the inner and outer walls.

Fig 7 shows a further modification of the basic shape of Fig 1 wherein the semicircular portions 50, 52 are provided with peripheral, outwardly convex projections 50, of radius  $R_8$ . These projections 50 serve to increase the effective base diameter from  $D_1$  to  $D_2$  and so improve the stability of the bottle. The projections 50 may form a continuous peripheral rim or may be formed

as a plurality of discrete "blisters" spaced around the circumference of the base. This modification can also be applied to the bases of Figs 4, 5 and 6.

Fig 8 illustrates a further feature which may be incorporated into any of the bases described; that is, an upwardly concave portion 54 of radius R9 formed in the bottom of each convex portion 56. This further strengthens the base and gives some improvement in stability.

The shape of the convex portions of the base may be further varied as shown in Fig 8 to increase the effective base diameter and hence the stability of the bottle. In Fig 9, each convex portion 69 comprises a first convex arcuate portion AB of radius R14 (greater than half the radius R1 of the cylindrical body portion) and centre of curvature 70, extending from the bottom of the cylindrical wall of the bottle, a second convex arcuate portion BC of radius R15, less than R1, and centre 72 which forms the apex of the convex portion 69, and a third convex arcuate portion CD of radius R16, greater than R1 and centre 74, extending upwardly towards the centre of the bottle. A cusp 76 is formed by arcs DE of radius R17, half R1 or less than R16. Additionally, the portions AB and CD may be replaced by, or include, generally straight-lined portions as previously described in relation to Fig 6.

As previously explained, the bases described thus far substantially eliminate any unoriented material from and are useful in many applications. It has been found, however, that they may not be sufficiently strong to prevent their re-entrant portions being blown out by the internal pressures generated by more highly pressurized liquids, especially in larger bottle sizes. This can be prevented by thickening the wall of the re-entrant portion, which may be accomplished by reintroducing an

amount of unoriented material into the re-entrant portion.

This may be achieved simply by truncating the central cusp 18, as at dotted line 78 of Fig 2. In this way the bottom of the preform, when stretched, contacts a projecting surface of the bottom of the mould so that a limited amount of relatively thick unoriented material is present around the centre of the base when the bottle is blown. This strengthens the re-entrant portion but will not materially affect the overall strength of the base so long as the unoriented material is restricted substantially to the re-entrant portion itself.

It has also been found that the shape and size of the re-entrant portion is important in obtaining a sufficiently strong structure. For example, by simply truncating the cusp 18 of Fig 2 as described, the sides of the re-entrant portion diverge at a relatively large angle so that its resistance to deformation is limited. It is preferred, therefore to modify the shape of the re-entrant portion such as is shown in Figs 10 and 11.

The base of Fig 10 comprises first and second downwardly convex portions 80, 82 as before. In this case, however, the re-entrant portion has been modified to take the form of a truncated cone 84 having relatively steep sides 86, 88 and closed by a substantially flat top surface 90. The remainder of the convex portions 80,82 may each comprise, for example, an arcuate bottom portion 92 and a straight line outer side wall 94. As illustrated, the base is further provided with peripheral stabilizing feet 96 spaced around its circumference.

The base of Fig 11 comprises first and second convex portions 98, 100, somewhat similar to those of Fig 9, and having its central re-entrant portion modified in a similar manner to that of Fig 10 so as to define a flat-topped, truncated cone 102 extending upwardly from the points 104, 106. This base is further modified by the

introduction of radial webs 108 extending from the base of the side walls 110 of the container to the base of the central truncated cone 102. These serve to further strengthen the base by dividing the annular surface defined by rotation of the convex portions 98, 100 into a plurality of segments.

As explained above, when moulding the bases of Figs 10 and 11, the stretched preform impinges upon the projecting surface of the mould-bottom corresponding to the top surface of the truncated cones 84, 102 such that the material in the vicinity of this surface remains unoriented and relatively thick when the bottle is blown, such unoriented material being largely confined to the cones 84, 102 themselves.

A further advantage which arises from moulding a bottle in this shape is that a gradual transition between unoriented and oriented material is obtained so that the weak points created by the abrupt transition observed in conventional bottles are eliminated. Thus, in the present case, the strength of the base will not be so greatly affected if the unoriented material does extend beyond the central truncated cone. This factor is particularly relevant to the enhanced resistance of the base to stress cracking.

Figs 12 and 13 show a particularly preferred embodiment of the invention somewhat similar to that of Fig 11. As in Fig 11, the base is divided into segments by radial webs 112 extending from the vertical side wall 114 of the bottle to the bottom of the central re-entrant portion 116, thereby defining a plurality of stabilizing feet 118. Each web 112 comprises a first straight line portion 120 extending downwardly and inwardly from point A to point B at an angle of  $32^{\circ}$  to the vertical, an arcuate portion 122 of radius R18 and centre 124 extending from point B to point C, and a second straight line portion 126 extending from point C to point D at an

angle of  $17^{\circ}$  to the horizontal. In profile, the feet 118 each comprise a first arcuate portion 128 of radius R19 and centre 130 extending from point A to point E, a second arcuate portion 132 of radius R20 and centre 134 extending from point E to point F, and a straight line portion 136 extending upwardly and inwardly at an angle of  $20^{\circ}$  to the horizontal to meet the second straightline portion of the web 112 at point G. The feet 118 themselves preferably comprise generally planar lateral and bottom surfaces 138 and 140 and a curved outer surface 148.

The central re-entrant portion 116 is radiused into the web 112 at point D by an arcuate portion 150, radius R21 and centre 152, and the side walls thereof are defined by a further arcuate portion 154, radius R22 and centre 156. The upper end of the re-entrant portion is closed by a substantially flat surface 158. As is best seen in Fig 13, the webs 112 define generally convex strips of material 160 such that the feet 118 are spaced from one another around the circumference of the base. As illustrated the base is provided with six feet 118.

Suitable dimensions for a two litre bottle as shown in Figs 12 and 13 are as follows: overall radius of base - 53 mm; R18 - 60 mm; R19 - 60 mm; R20 - 5 mm; R21 - 10 mm; R22 - 10 mm. The top surface 158 of the re-entrant portion 116 is 10 mm in diameter and the re-entrant portion 116 itself is 7.5 mm deep. A one litre bottle might have a base radius of 44.3 mm with the other dimensions scaled accordingly.

In some cases, it may be preferable to replace the flat top surface 158 of the re-entrant portion 116 with an upwardly domed surface. The profile of the radial webs 112 may also be varied to comprise different combinations of arcuate and/or straight line portions.

The diameter of the re-entrant portion 116 should be in a range of 5% to 30% of the overall base diameter and

preferably in the range 10% to 20% and the angle of divergence of the sidewalls of the re-entrant portion 116 is preferably less than  $60^{\circ}$ . Additionally, as previously stated, the unoriented material forming the walls of the re-entrant portion 116 is thicker than the walls of the remainder of the base and the ratio of the thicknesses of these walls should be in the range 1.2:1 to 10:1.

Outside this range the base may be blown out due to internal pressure so that the thickness of the base as a whole would have to be increased, increasing the weight and cost of the bottle.

Figs 14 and 15 show bottles similar to that of Figs 12 and 13 which were subjected to comparative tests with a conventional one piece blow-moulded bottle as shown in Fig 16. The test procedures and results are detailed below.

#### Examples 1 and 2

Polyethylene phthalate resin (I.V. 0.76, available from ICI Ltd) was injection moulded to form preforms of 36 grams for a 1 litre volume bottle and of 53 grams for a 2 litre volume bottle. The injection moulding machine was model XL225 sold by HUSKY Co with a mould for 32 pieces. The temperature for moulding was about  $260^{\circ}\text{C}$  to  $280^{\circ}\text{C}$ . 1 litre volume bottles corresponding to the shape shown in Fig 14 (Example 1) and 2 litre volume bottles corresponding to the shape shown in Fig 15 (Example 2) were made from the above preforms under the following conditions:

Blow moulding machine:            Corpoplast Co B-40  
Blow moulding temperature:    about  $90^{\circ}\text{C}$   
Blow moulding pressure:        about 40 bar

Ten each of the bottles of Examples 1 and 2 were measured by the following methods. The results are shown as an average of ten bottles in Table 1.

(1) Thickness of the wall

The thickness of the walls of the portions 170 and 171 in Fig 14 and of the portions 180 and 181 in Fig 15 was measured by a micrometer after cutting the bottom.

(2) Density

In order to know the degree of orientation, the portions or pieces where the wall thickness was measured were subject to measurement of their density by a density-gradient tube.

(3) Internal pressure test

Into the bottles, water was charged in an amount of 1 litre (Example 1) or 2 litres (Example 2) and sodium bicarbonate and citric acid were added in such an amount that the carbonic acid gas volume corresponds to 4 volumes. After the bottles were allowed to stand at 40°C for 24 hours, the degree of deformation of the bottom of the bottles was determined visually. The standards of the estimation of the deformation were the following A, B, and C:

A: Substantially no deformation

B: Deformation was observed but self-standing ability was kept

C: Significant deformation and impossibility of self standing

(4) Creep test

The same procedures as those of the internal pressure test were repeated, that is, the bottles were charged with water and kept at 4 volumes of the carbonic acid gas volume and allowed to stand at 40°C for 24 hours. Then, the increased volume of the bottles was determined in percent based on the original volume of the bottles.

Comparative Example

2 litre volume bottles having the shape as shown in Fig 16 were commercially obtained and measured by the same methods as those of Examples 1 and 2. The results are shown in Table 1.

Table 1

	Example 1	Example 2	Comparative Example
Weight of bottle (g)	36	53	57
Volume of bottle (l)	1	2	2
Wall thickness (mm) (measured portions)			
- Re-entrant portion	2.00 (130)	2.05 (140)	2.00(150)
- Adjacent portion	0.28 (131)	1.05 (141)	2.32(151)
Density at 23°C, 50% [g/cc]			
- Re-entrant portion	1.330 (130)	1.330 (140)	1.330(150)
- Adjacent portion	1.350 (131)	1.340 (141)	1.330(151)
Estimation of Internal pressure test	A	B	B
Creep [%]	2.8	3.8	6.0

As seen in the above, it was found that the bottles of Examples 1 and 2 are not deformed and keep their self-standing ability even under a high internal pressure due to contents such as carbonated drinks. Moreover, in the bottles of Examples 1 and 2, even if the wall thickness of the portions 171 (in Fig 14) and 181 (in Fig 15) is smaller than that of the corresponding portion 191 (in Fig 16) of the bottle of Comparative Example, the bottles of the Examples 1 and 2 have no problem of internal pressure deformation and stress cracking, which allows the bottle weight to be reduced. Further, the creep characteristics are superior in the bottles of Examples 1 and 2 to that of Comparative Example.

By controlling the presence of unoriented material in the base structure and the thickness of the walls of the re-entrant portion, the present invention provides a one piece blow-moulded plastic container having materially improved creep and stress cracking properties when compared with existing one piece bottles, so allowing a significant reduction in the weight of the bottle and hence in production costs.

In addition, the preferred embodiment illustrated in Figs 12 and 13 provides a wider effective base diameter than existing bottles and is therefore more stable on filling lines during the bottling process. The webs 112 also help to brace the base against deformation and the general shape of the feet 118 is chosen to minimize the effects of the internal pressure exerted thereon. These features provide a base structure which is inherently resistant to deformation and which is further enhanced by the presence of the thickened re-entrant portion 116 as described herein.

CLAIMS

1. A container of blow-moulded oriented thermoplastic material formed by enclosing a moulded preform in a mould corresponding to the shape of the container, heating the preform and stretching it to the full length of the mould so that its bottom surface impinges upon the bottom surface of the mould prior to blow-moulding said container comprising a generally cylindrical body portion and a base portion closing the bottom end of said body portion, wherein said base portion is a figure of rotation formed by rotating a generally convex curve extending from the bottom of said side wall to the central longitudinal axis of the container about said central axis so as to define an annular convex surface having a central re-entrant portion, and wherein said preform, when stretched prior to blow-moulding, impinges upon a projecting central portion of the bottom surface of the mould corresponding to said re-entrant portion, such that, when blow-moulded, the material in the vicinity of said re-entrant portion remains unoriented and relatively thick in comparison with the oriented material of the remainder of the base portion.

2. A container as claimed in claim 1 wherein said re-entrant portion, in cross-section, comprises first and second downwardly divergent side walls and a topmost surface closing the upper ends of said side walls and wherein said relatively thick unoriented material is substantially confined to said topmost surface and said side walls of the re-entrant portion.

3. A container as claimed in claim 1 or claim 2 wherein the ratio of the thickness of said unoriented material to said oriented material is in the range 1.2:1 to 10:1.

4. A container as claimed in claim 1, 2 or 3 wherein the diameter of said re-entrant portion is in the range 5% to 30% of the overall diameter of said base portion.
5. A container as claimed in claim 4 wherein the diameter of said re-entrant portion is in the range 10% to 20% of the overall diameter of said base portion.
6. A container as claimed in any of claims 2 to 5 wherein the angle of divergence of said side walls of said re-entrant portion is less than  $60^{\circ}$ .
7. A container as claimed in any preceding claim wherein said base portion includes a plurality of radial webs extending from the bottom of said body portion towards the centre of said base portion and dividing said convex annular surface into a plurality of feet spaced around the circumference of said base portion.
8. A container of plastics material comprising a generally cylindrical body portion and a base portion closing the bottom end of said body portion, said base portion comprising a generally convex annular surface having a central re-entrant portion and wherein the walls of said re-entrant portion are substantially thicker than the walls of the remainder of said base portion.
9. A container as claimed in claim 8 wherein said re-entrant portion, in cross-section, comprises first and second downwardly divergent side walls and a topmost surface closing the upper ends of said side walls.
10. A container as claimed in claim 9 wherein the ratio of the thickness of the walls of said re-entrant portion to the walls of the remainder of said base portion is in the range 1.2:1 to 10:1.
11. A container as claimed in claim 9 or claim 10 wherein the diameter of said re-entrant portion is in the range 5% to 30% of the overall diameter of said base portion.

12. A container as claimed in claim 11 wherein the diameter of said re-entrant portion is in the range 10% to 20% of the overall diameter of said base portion.

13. A container as claimed in any of claims 9 to 12 wherein the angle of divergence of the side walls of said re-entrant portion is less than  $60^{\circ}$ .

14. A container as claimed in any of claims 8 to 13 wherein said base portion includes a plurality of radial webs extending from the bottom of said body portion towards the centre of said base portion and dividing said convex annular surface into a plurality of feet spaced around the circumference of said base portion.

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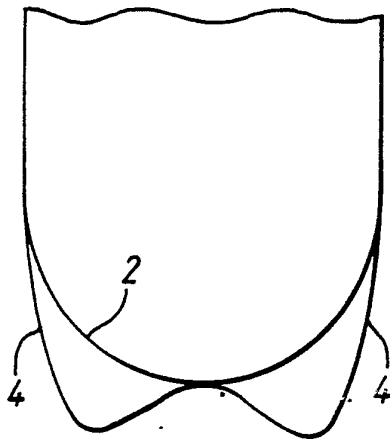


Fig. 1

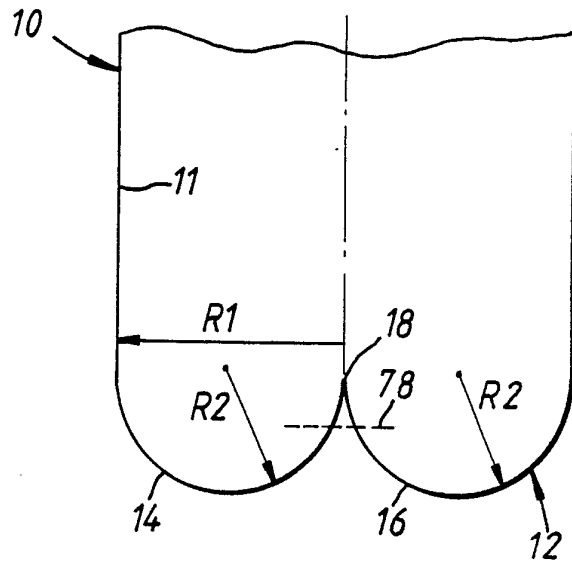


Fig. 2

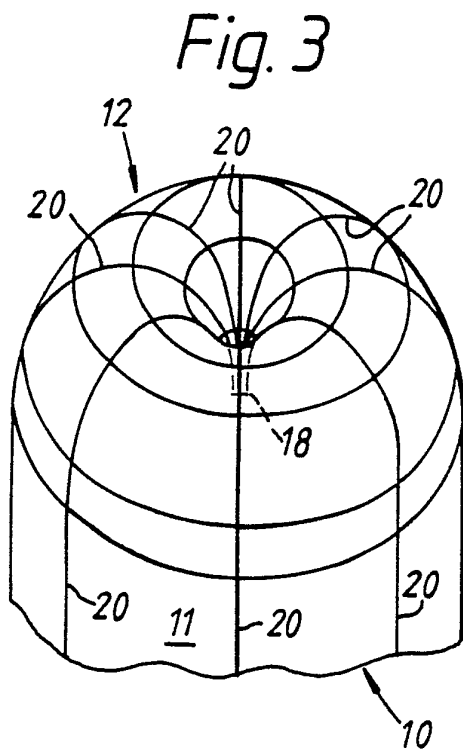


Fig. 3

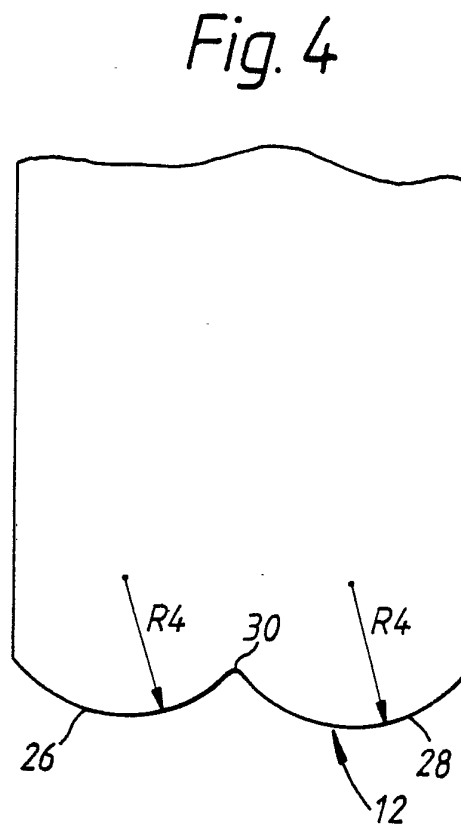


Fig. 4

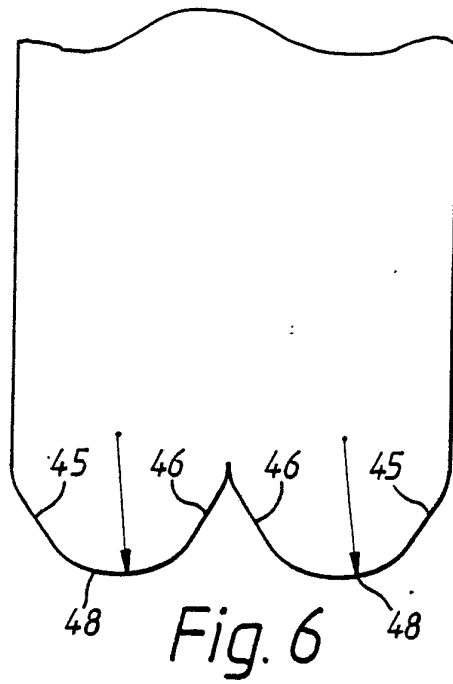
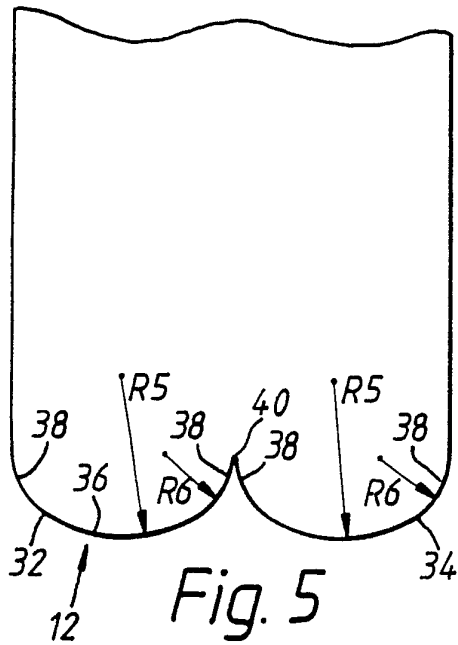


Fig. 7

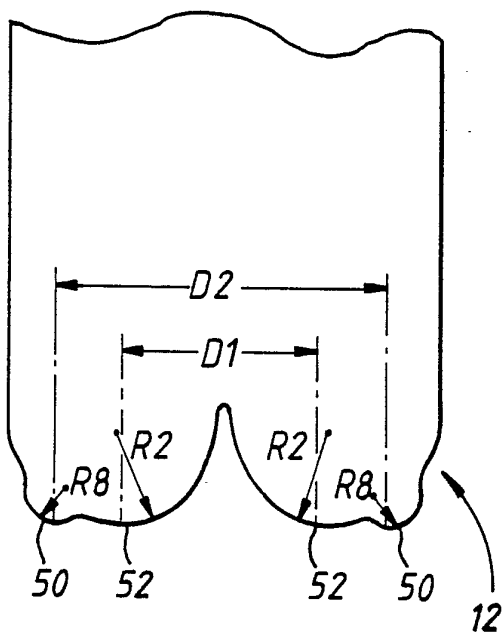
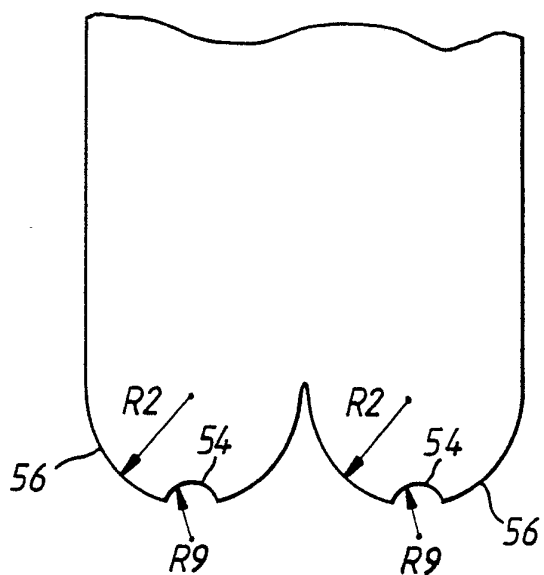


Fig. 8



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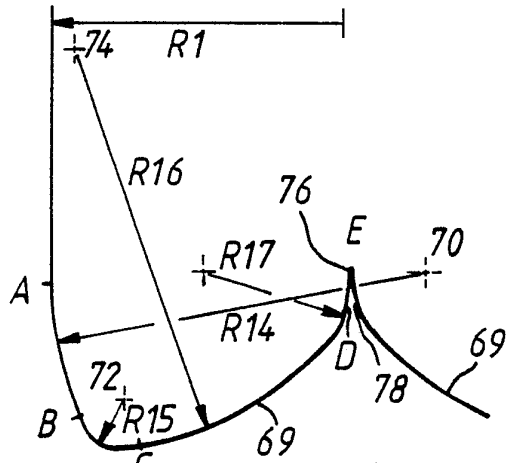


Fig. 9

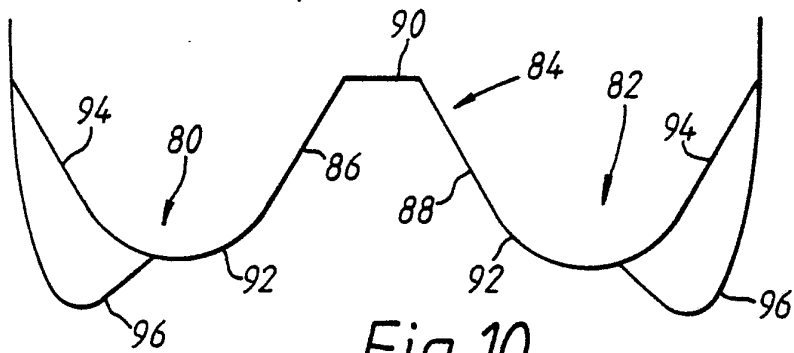


Fig. 10

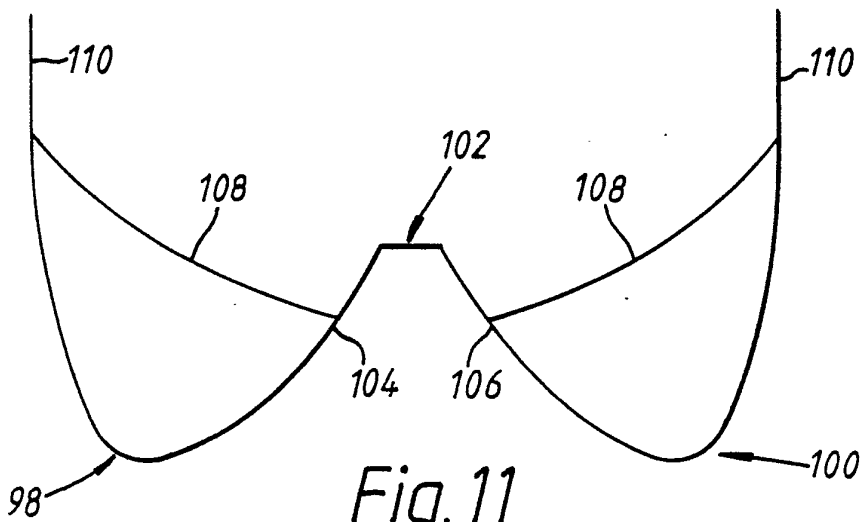


Fig. 11

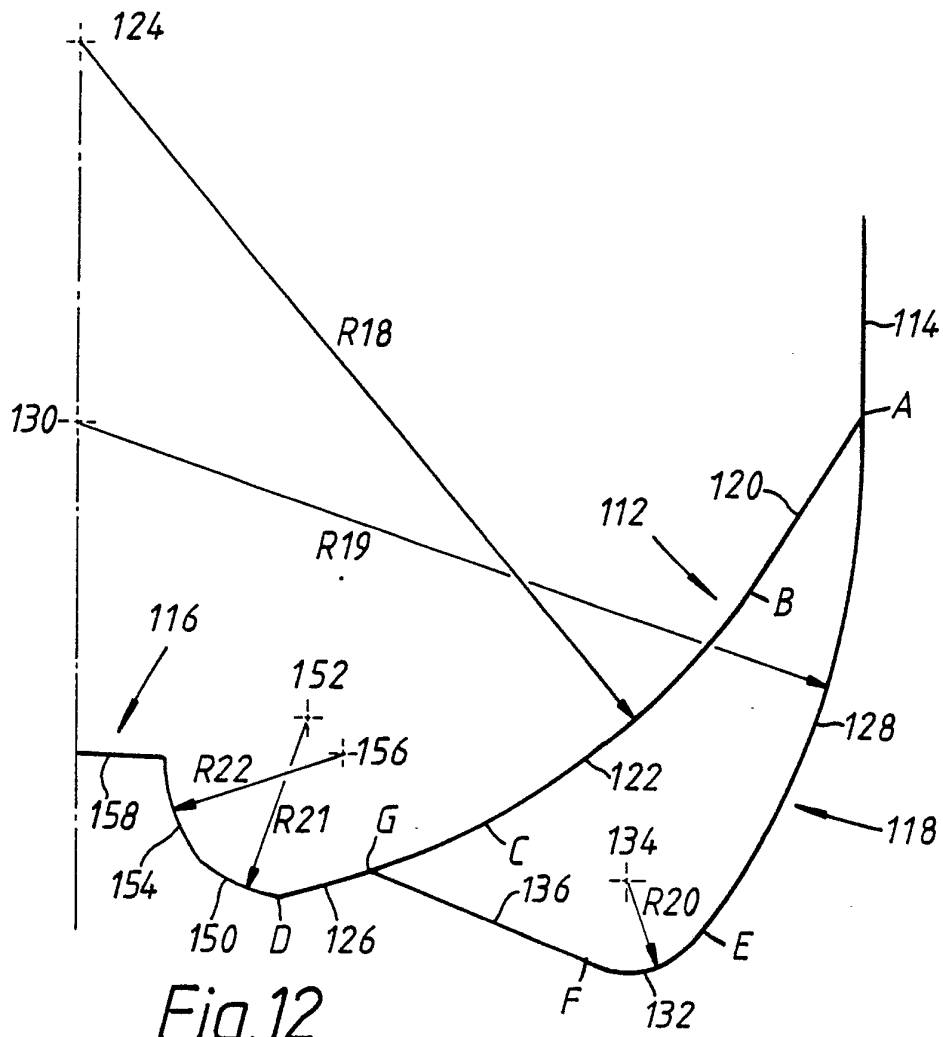


Fig. 12

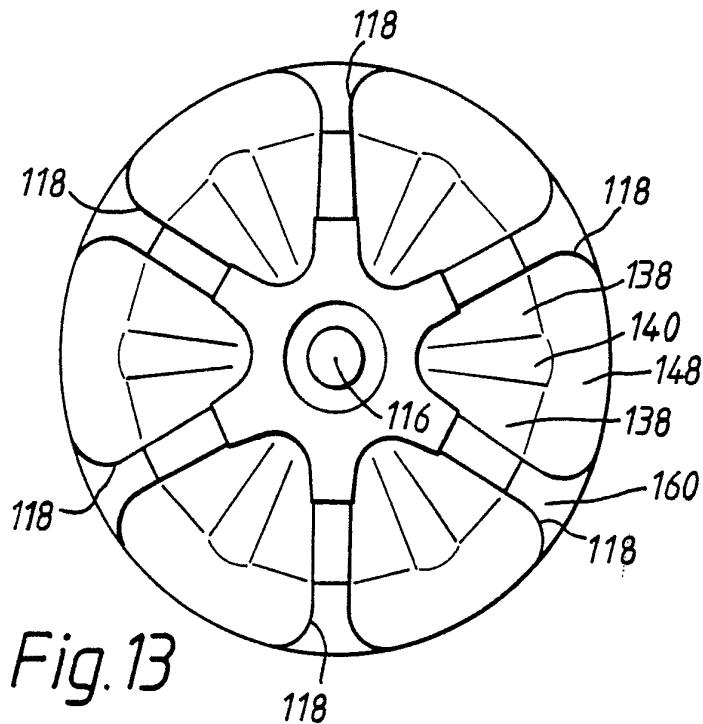
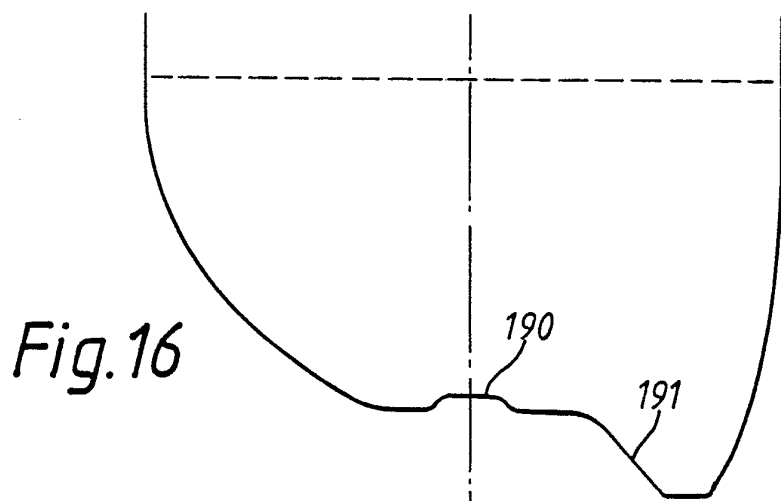
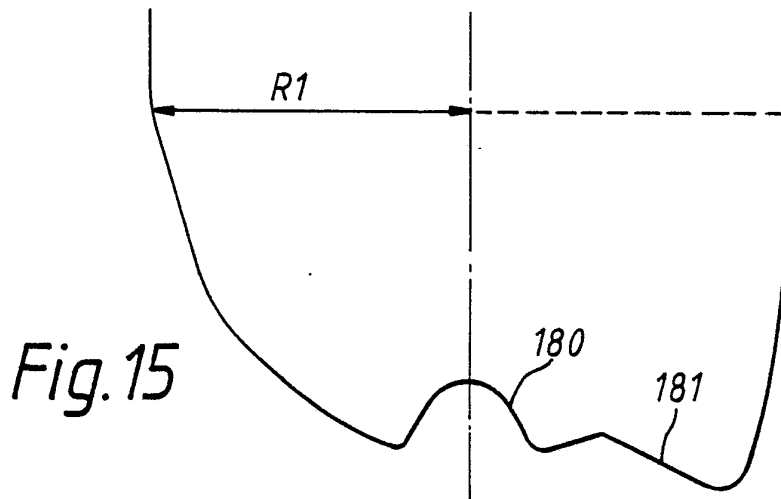
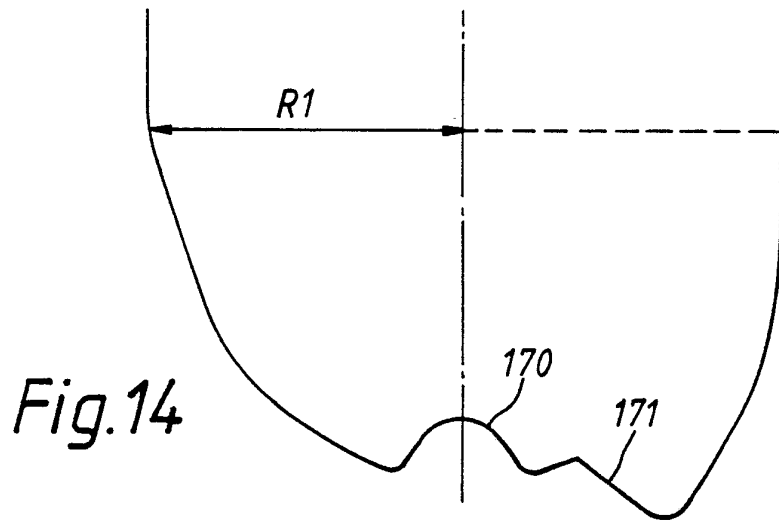


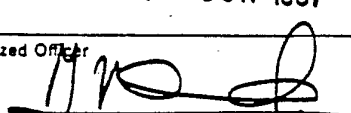
Fig. 13

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# INTERNATIONAL SEARCH REPORT

International Application No PCT/GB 87/00102

<b>I. CLASSIFICATION OF SUBJECT MATTER</b> (if several classification symbols apply, indicate all) *		
According to International Patent Classification (IPC) or to both National Classification and IPC		
IPC <sup>4</sup> : B 29 C 49/12; B 65 D 1/02		
<b>II. FIELDS SEARCHED</b>		
Minimum Documentation Searched <sup>7</sup>		
Classification System	Classification Symbols	
IPC <sup>4</sup>	B 29 C; B 65 D	
Documentation Searched other than Minimum Documentation to the Extent that such Documents are Included in the Fields Searched <sup>8</sup>		
<b>III. DOCUMENTS CONSIDERED TO BE RELEVANT <sup>9</sup></b>		
Category <sup>6</sup>	Citation of Document, <sup>11</sup> with indication, where appropriate, of the relevant passages <sup>12</sup>	Relevant to Claim No. <sup>13</sup>
Y	EP, A, 0042132 (HENKEL KG) - 23 December 1981 see page 6, lines 16-25; page 8, lines 1-20; figures 5,6	1,2,8,9
Y	EP, A, 0002082 (SOLVAY) 30 May 1979 see page 4, line 24 - page 5, line 9; figures 1-3	1,2,8,9
A	US, A, 3865530 (JESSELALLEE) 11 February 1975 see figures 1-3	1,2
A	FR, A, 2217219 (MONSANTO CO.) 6 September 1974 see page 9, lines 25-33; figures 1,2	1
A	FR, A, 2471921 (AOKI) 26 June 1981 see figures 3-9	7,14
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<p>* Special categories of cited documents: <sup>10</sup></p> <p>"A" document defining the general state of the art which is not considered to be of particular relevance</p> <p>"E" earlier document but published on or after the international filing date</p> <p>"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)</p> <p>"O" document referring to an oral disclosure, use, exhibition or other means</p> <p>"P" document published prior to the international filing date but later than the priority date claimed</p> <p>"T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention</p> <p>"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step</p> <p>"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.</p> <p>"&amp;" document member of the same patent family</p>		
<b>IV. CERTIFICATION</b>		
Date of the Actual Completion of the International Search	Date of Mailing of this International Search Report	
27th April 1987	1 - JUN 1987	
International Searching Authority	Signature of Authorized Officer	
EUROPEAN PATENT OFFICE	M. VAN MOL 	

## ANNEX TO THE INTERNATIONAL SEARCH REPORT ON

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 INTERNATIONAL APPLICATION NO.            PCT/GB 87/00102 (SA 16122)  
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This Annex lists the patent family members relating to the patent documents cited in the above-mentioned international search report. The members are as contained in the European Patent Office EDP file on 13/05/87

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		JP-A- 57027729	15/02/82
		AT-B- E8974	15/09/84
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		JP-A- 57039252	04/03/82

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